



Missione 4 – Istruzione e Ricerca – Componente 1 – Potenziamento dell'offerta dei servizi di istruzione: dagli asili nido alle Università – Investimento 1.3: “Piano per le infrastrutture per lo sport nelle scuole”, finanziato dall'Unione europea – Next Generation EU

**REALIZZAZIONE DI UNA PALESTRA A SERVIZIO DELLA STRUTTURA SCOLASTICA I.T.T. “G. Malafarina” – Comune di Soverato (CZ) –
CUP C35E22000040006 - CIG: 9543843464**



**Finanziato
dall'Unione europea**
NextGenerationEU



Amministrazione
Provinciale di
Catanzaro



CODICE ELABORATO:
SOVESTR002

NOME ELABORATO:
TABULATI DEI CALCOLI - PALESTRA

R.U.P. : Ing. Antonio Leone

I Progettisti:

Arch. Giovanni B. Giannotti
(mandataria)

GIANNOTTI
ARCHITECTURE & DESIGN

Via A. De Gasperi n°2 88068 - Soverato (CZ)

OMARCH S.R.L.
(mandante)

arch. Fabio Montesano
arch. Roberto Carpino
arch. Domenico Conaci
arch. Antonio Marra
dott. geol. Giuseppe Scala

OMARCH
OFFICINA MEDITERRANEA DI ARCHITETTURA

Via Otranto n°2 88100 - Catanzaro (CZ)

Arch. Danilo Cosco
(giovane prof. mandante)



PROGETTO ESECUTIVO

LUGLIO 2023

REVISIONE N°:

1 Risultati di Calcolo.

1.1 Risultati Condizioni.

Asta	: numerazione interna dell'asta.
Imp.	: impalcato al quale appartiene l'asta considerata.
Fili	: fili fissi ai quali appartiene l'asta considerata.
Nodo	: numerazione interna del nodo.
Nodo Vinc.	: numerazione interna del nodo vincolato.
X	: distanza dal nodo iniziale misurata lungo l'asse dell'asta.
Cinematismi nodali	: valore dello spostamento. Per le azioni sismiche è riferito allo spettro elastico:
V _x	: traslazione X rispetto al sistema di riferimento globale.
V _y	: traslazione Y rispetto al sistema di riferimento globale.
V _z	: Traslazione Z rispetto al sistema di riferimento globale.
R _x	: rotazione attorno all'asse X del sistema di riferimento globale.
R _y	: rotazione attorno all'asse Y del sistema di riferimento globale.
R _z	: rotazione attorno all'asse Z del sistema di riferimento globale.
Sollecitazioni:	
N	: valore dello Sforzo Normale nel punto considerato.
M _T	: valore del Momento Torcente nel punto considerato.
M _{XZ}	: valore del Momento Flettente X-Z nel punto considerato.
T _{XZ}	: valore del Taglio X-Z nel punto considerato.
M _{XY}	: valore del Momento Flettente X-Y nel punto considerato.
T _{XY}	: valore del Taglio X-Y nel punto considerato.
Reazioni:	
R _x	: reazione vincolare in direzione X (riferimento globale);
R _y	: reazione vincolare in direzione Y (riferimento globale);
R _z	: reazione vincolare in direzione Z (riferimento globale);
R _{fx}	: reazione vincolare intorno ad X (riferimento globale);
R _{fy}	: reazione vincolare intorno ad Y (riferimento globale);
R _{fz}	: reazione vincolare intorno ad Z (riferimento globale).
Parete/Piastra	: numerazione dei fili fissi per impalcato della parete/piastra intesa come insieme di elementi bidimensionali;
Sollecitazioni:	
N1-1	: valore dello Sforzo Normale sulla faccia di normale parallela all'asse 1 in direzione 1 nel punto considerato;
N2-2	: valore dello Sforzo Normale sulla faccia di normale parallela all'asse 2 in direzione 2 nel punto considerato;
N1-2	: valore dello Sforzo Normale sulla faccia di normale parallela all'asse 1 in direzione 2 nel punto considerato;
M1-1	: valore dello Momento Flettente sulla faccia di normale parallela all'asse 1 nel punto considerato;
M2-2	: valore dello Momento Flettente sulla faccia di normale parallela all'asse 2 nel punto considerato;
M1-2	: valore dello Momento Torcente sulle faccie nel punto considerato;
T1-3	: valore del Taglio sulla faccia di normale parallela all'asse 1 in direzione 3 nel punto considerato;
T2-3	: valore del Taglio sulla faccia di normale parallela all'asse 2 in direzione 3 nel punto considerato;
Modo:	
f	: valore della frequenza del modo i-esimo;
T	: valore del periodo del modo i-esimo;
G _x	: valore del coefficiente di partecipazione del modo i-esimo;

1.1.1 Risultati Condizioni (Carichi Permanenti - G1).

1.1.1.1 Sollecitazioni SLU

Tabella 1.I

Asta	Imp.	Fili	X [cm]	Sollecitazioni					
				N [daN]	Mt [daNm]	Mxz [daNm]	Txz [daN]	Mxy [daNm]	Txy [daN]
1	Fondazio ne	1, 2	0	-22.11	4.57	30.92	-424.46	2.72	-1.07
			42	-22.04	4.57	-95.10	-186.05	3.06	-0.62
			83	-21.99	4.57	-126.88	29.55	3.25	-0.33
2	Fondazio ne	1, 2	0	-21.43	-17.09	-140.66	-51.34	3.23	-1.75
			42	-21.39	-17.08	-120.51	145.54	3.93	-1.60
			83	-21.36	-17.08	-21.62	328.31	4.58	-1.56
3	Fondazio ne	1, 15	0	48.28	35.01	0.18	-331.97	6.12	10.06
			40	47.78	35.02	-83.87	-90.91	2.12	10.07
			80	47.31	35.03	-71.37	154.25	-1.86	9.94
4	Fondazio ne	1, 15	0	52.07	154.71	-122.79	43.71	-1.88	-10.29
			40	51.62	154.72	-55.53	295.72	2.25	-10.55
			80	51.20	154.73	113.72	557.14	6.53	-10.96
5	Fondazio ne	2, 3	0	-53.92	-13.22	-29.37	-226.56	3.81	4.71
			35	-53.92	-13.22	-82.64	-83.48	2.19	4.69
			69	-53.93	-13.22	-87.71	53.08	0.58	4.63
6	Fondazio ne	2, 3	0	-35.81	-2.48	-92.21	2.26	0.58	-1.19
			35	-35.85	-2.48	-68.58	134.06	1.00	-1.28
			69	-35.89	-2.48	-0.04	262.74	1.46	-1.40
7	Fondazio ne	3, 4	0	-22.77	-1.21	-0.44	-192.03	1.27	1.41
			35	-22.83	-1.21	-44.82	-65.64	0.81	1.26
			69	-22.90	-1.21	-45.90	59.06	0.40	1.10
8	Fondazio ne	3, 4	0	-11.85	1.82	-43.16	-23.77	0.40	-0.03
			35	-11.92	1.82	-29.95	100.18	0.44	-0.21
			69	-12.00	1.82	26.00	224.14	0.54	-0.40
9	Fondazio ne	4, 5	0	-3.31	5.25	29.56	-198.52	0.47	0.43
			35	-3.39	5.25	-17.50	-74.38	0.36	0.22
			69	-3.48	5.25	-21.71	49.95	0.32	0.01
10	Fondazio ne	4, 5	0	2.95	1.94	-18.06	-45.44	0.32	0.31
			35	2.87	1.94	-12.20	79.50	0.25	0.09
			69	2.78	1.94	36.93	205.39	0.25	-0.13
11	Fondazio ne	5, 6	0	7.11	3.18	38.62	-195.66	0.25	0.04
			35	7.03	3.18	-7.03	-68.96	0.27	-0.19
			69	6.95	3.18	-8.86	58.36	0.38	-0.43
12	Fondazio ne	5, 6	0	8.86	-0.38	-7.74	-39.78	0.38	0.63
			35	8.78	-0.38	0.63	88.34	0.20	0.39
			69	8.71	-0.37	53.35	217.36	0.11	0.15
13	Fondazio ne	6, 7	0	33.59	3.98	54.23	-217.24	0.12	0.63
			35	33.52	3.98	1.63	-87.74	-0.05	0.39
			69	33.47	3.98	-6.28	41.81	-0.15	0.15
14	Fondazio ne	6, 7	0	34.68	1.63	-4.34	-55.49	-0.15	-0.13
			35	34.64	1.64	-1.12	74.17	-0.06	-0.37
			69	34.62	1.64	46.87	204.03	0.11	-0.61
15	Fondazio ne	7, 8	0	13.85	4.56	50.39	-225.20	0.11	-0.06
			35	13.83	4.56	-4.92	-95.49	0.17	-0.31
			69	13.82	4.56	-15.56	33.74	0.32	-0.56
16	Fondazio ne	7, 8	0	14.79	-1.00	-14.93	-63.62	0.32	0.35
			35	14.79	-1.00	-14.63	65.36	0.24	0.10
			69	14.80	-1.00	30.18	194.44	0.25	-0.15
17	Fondazio ne	8, 9	0	13.95	-3.03	29.89	-188.45	0.25	0.24
			35	13.96	-3.03	-12.85	-59.32	0.21	0.00
			69	13.97	-3.03	-11.05	69.78	0.25	-0.24

18	Fondazio ne	8, 9	0	10.99	-8.79	-15.77	-30.53	0.25	0.24
			35	11.01	-8.79	-4.00	98.85	0.20	0.01
			69	11.04	-8.79	52.48	228.71	0.24	-0.22
19	Fondazio ne	9, 10	0	30.18	-5.30	47.94	-198.40	0.23	0.68
			35	30.22	-5.29	1.92	-68.40	0.03	0.46
			69	30.26	-5.29	0.70	61.33	-0.09	0.24
20	Fondazio ne	9, 10	0	26.79	-6.77	-6.00	-39.53	-0.09	0.01
			35	26.85	-6.77	2.69	89.96	-0.06	-0.20
			69	26.91	-6.77	56.03	219.25	0.05	-0.40
21	Fondazio ne	10, 11	0	-3.34	-0.75	55.77	-228.21	0.05	-0.55
			35	-3.27	-0.75	-0.75	-99.59	0.28	-0.75
			69	-3.20	-0.75	-13.09	27.94	0.57	-0.94
22	Fondazio ne	10, 11	0	-7.99	-1.90	-16.28	-64.38	0.57	0.23
			35	-7.92	-1.90	-16.65	62.23	0.52	0.05
			69	-7.86	-1.90	26.57	188.27	0.54	-0.12
23	Fondazio ne	11, 12	0	-16.00	0.39	25.91	-230.23	0.61	0.48
			35	-15.94	0.39	-31.87	-104.73	0.47	0.33
			69	-15.89	0.39	-46.42	20.42	0.38	0.19
24	Fondazio ne	11, 12	0	-26.96	2.09	-48.45	-65.89	0.39	-1.42
			35	-26.92	2.09	-49.55	59.72	0.90	-1.54
			69	-26.88	2.09	-7.09	186.82	1.45	-1.64
25	Fondazio ne	12, 13	0	-40.88	2.27	-6.90	-256.69	1.64	1.57
			35	-40.86	2.27	-73.23	-127.40	1.12	1.50
			69	-40.85	2.27	-94.45	5.03	0.61	1.46
26	Fondazio ne	12, 13	0	-59.71	15.63	-91.35	-55.43	0.61	-4.70
			35	-59.72	15.63	-86.96	81.86	2.24	-4.70
			69	-59.76	15.63	-34.10	225.85	3.85	-4.66
27	Fondazio ne	13, 14	0	-22.51	13.80	-26.02	-325.54	4.62	1.02
			42	-22.57	13.80	-123.47	-141.31	4.17	1.15
			83	-22.64	13.80	-141.46	57.53	3.64	1.40
28	Fondazio ne	13, 14	0	-25.52	-5.32	-115.14	-49.82	3.67	0.72
			42	-25.61	-5.32	-91.27	168.29	3.29	1.11
			83	-25.72	-5.32	27.95	409.55	2.72	1.68
29	Fondazio ne	14, 16	0	54.59	-38.74	3.33	-346.63	-6.43	-9.73
			40	53.98	-38.75	-85.98	-102.89	-2.54	-9.79
			80	53.39	-38.76	-77.75	144.58	1.33	-9.69
30	Fondazio ne	14, 16	0	53.99	-146.95	-116.45	16.72	1.36	9.44
			40	53.43	-146.96	-59.48	270.75	-2.44	9.69
			80	52.90	-146.98	100.23	533.94	-6.36	10.07
31	Fondazio ne	15, 17	0	43.72	38.80	47.55	-306.66	10.23	30.59
			33	43.39	38.81	-16.78	-82.53	0.21	30.18
			66	43.08	38.83	-6.13	147.75	-9.68	29.70
32	Fondazio ne	15, 17	0	40.38	195.96	-72.13	170.23	-9.69	-37.40
			33	40.08	195.97	22.98	407.03	2.74	-37.95
			66	39.79	195.99	197.37	650.61	15.36	-38.58
33	Fondazio ne	16, 18	0	45.65	-43.16	43.75	-298.03	-10.00	-29.52
			33	45.23	-43.17	-17.47	-72.48	-0.33	-29.11
			66	44.82	-43.19	-3.26	159.25	9.20	-28.64
34	Fondazio ne	16, 18	0	44.37	-192.09	-63.53	134.34	9.22	35.57
			33	43.98	-192.11	20.00	372.61	-2.61	36.12
			66	43.60	-192.12	183.28	617.63	-14.63	36.74
35	Fondazio ne	17, 19	0	85.62	-41.52	141.39	-473.86	17.93	46.39
			33	85.36	-41.50	26.00	-225.04	2.73	45.71
			66	85.13	-41.48	-6.62	27.65	-12.24	45.02
36	Fondazio	17, 19	0	74.34	146.24	-35.70	62.60	-12.24	-42.26

	ne								
			33	74.14	146.26	27.20	319.06	1.82	-42.99
			66	73.96	146.28	175.37	579.26	16.13	-43.76
37	Fondazio ne	18, 20	0	85.16	32.29	137.18	-457.14	-17.29	-44.88
			33	84.81	32.27	27.58	-206.77	-2.59	-44.20
			66	84.49	32.25	1.27	47.59	11.88	-43.50
38	Fondazio ne	18, 20	0	77.92	-148.63	-33.03	37.89	11.89	41.94
			33	77.63	-148.65	22.02	296.11	-2.07	42.67
			66	77.37	-148.67	162.93	558.16	-16.28	43.46
39	Fondazio ne	19, 21	0	38.30	-69.36	144.14	-497.11	14.35	42.46
			33	38.14	-69.35	23.40	-234.61	0.47	41.68
			66	38.00	-69.33	-10.55	28.87	-13.16	40.90
40	Fondazio ne	19, 21	0	29.70	118.14	-26.47	29.03	-13.16	-39.89
			33	29.57	118.16	26.72	293.41	0.13	-40.67
			66	29.45	118.18	167.33	558.65	13.69	-41.49
41	Fondazio ne	20, 22	0	38.86	65.04	138.09	-491.74	-14.51	-42.80
			33	38.62	65.02	19.48	-227.16	-0.52	-42.00
			66	38.39	65.01	-11.60	38.73	13.21	-41.21
42	Fondazio ne	20, 22	0	30.63	-122.22	-30.90	28.43	13.21	39.56
			33	30.41	-122.24	22.57	295.61	0.02	40.37
			66	30.21	-122.26	164.43	564.11	-13.43	41.21
43	Fondazio ne	21, 23	0	61.08	-88.77	157.37	-532.48	15.12	42.11
			33	60.98	-88.75	25.38	-267.81	1.36	41.29
			66	60.90	-88.73	-19.57	-5.11	-12.14	40.49
44	Fondazio ne	21, 23	0	52.79	91.66	-24.79	23.72	-12.14	-41.31
			33	52.73	91.68	26.12	284.42	1.63	-42.11
			66	52.69	91.70	162.73	543.06	15.66	-42.92
45	Fondazio ne	22, 24	0	62.64	80.22	151.43	-537.29	-14.88	-41.58
			33	62.45	80.20	18.48	-268.84	-1.30	-40.73
			66	62.29	80.18	-26.08	-1.71	12.00	-39.89
46	Fondazio ne	22, 24	0	54.14	-101.73	-34.19	-2.91	12.00	40.41
			33	53.99	-101.75	8.79	262.98	-1.47	41.25
			66	53.87	-101.77	139.33	527.84	-15.22	42.10
47	Fondazio ne	23, 25	0	-5.15	-127.73	173.99	-656.60	14.08	39.75
			33	-5.19	-127.71	-0.45	-401.42	1.10	38.95
			66	-5.22	-127.70	-91.44	-150.93	-11.63	38.19
48	Fondazio ne	23, 25	0	-19.96	36.26	-66.98	-108.75	-11.62	-23.84
			33	-20.00	36.28	-62.08	137.79	-3.63	-24.58
			66	-20.05	36.29	23.69	381.59	4.60	-25.31
49	Fondazio ne	24, 26	0	-0.08	99.30	137.05	-609.60	-13.68	-38.84
			33	-0.20	99.28	-20.65	-346.81	-1.00	-38.00
			66	-0.31	99.26	-92.11	-86.86	11.40	-37.18
50	Fondazio ne	24, 26	0	-12.99	-61.77	-90.57	-68.05	11.40	22.36
			33	-13.10	-61.79	-70.38	190.06	3.89	23.15
			66	-13.23	-61.81	34.88	447.77	-3.88	23.95
51	Fondazio ne	25, 26	0	69.94	22.14	-168.05	-345.26	-1.91	-2.81
			49	68.88	22.14	-254.53	-22.51	-0.56	-2.74
			97	67.87	22.14	-199.43	238.78	0.76	-2.70
52	Fondazio ne	25, 26	0	65.50	11.92	-208.59	-160.83	0.75	1.07
			49	64.54	11.92	-233.04	52.53	0.23	1.09
			97	63.63	11.92	-162.66	231.01	-0.31	1.10
53	Fondazio ne	25, 26	0	69.95	4.60	-142.21	-102.56	-0.31	-0.36
			49	69.10	4.60	-153.45	52.54	-0.13	-0.37
			97	68.30	4.60	-93.02	193.32	0.06	-0.40
54	Fondazio ne	25, 26	0	74.31	1.96	-71.36	-89.76	0.05	0.00

			49	73.57	1.96	-82.20	43.87	0.06	-0.05
			97	72.88	1.96	-28.70	175.30	0.11	-0.12
55	Fondazio ne	25, 26	0	77.52	0.83	-11.59	-109.39	0.10	0.03
			49	76.89	0.83	-32.53	23.17	0.11	-0.05
			97	76.32	0.83	11.68	158.62	0.16	-0.16
56	Fondazio ne	25, 26	0	79.50	0.46	20.16	-130.08	0.15	0.10
			49	78.99	0.46	-9.34	9.12	0.13	-0.02
			97	78.55	0.46	29.84	152.16	0.18	-0.15
57	Fondazio ne	25, 26	0	80.54	0.28	33.04	-145.23	0.17	0.13
			49	80.16	0.28	-2.03	1.39	0.14	-0.01
			97	79.84	0.28	35.03	151.08	0.19	-0.17
58	Fondazio ne	25, 26	0	81.02	0.32	35.22	-153.25	0.18	0.19
			49	80.77	0.32	-2.38	-1.09	0.13	0.02
			97	80.57	0.32	34.55	152.96	0.16	-0.15
59	Fondazio ne	25, 26	0	81.25	0.96	33.84	-155.59	0.16	0.11
			49	81.12	0.96	-4.10	-0.21	0.15	-0.07
			97	81.06	0.96	33.80	156.00	0.23	-0.24
60	Fondazio ne	25, 26	0	81.66	-2.97	33.04	-156.90	0.23	0.26
			49	81.66	-2.97	-5.23	-0.34	0.14	0.08
			97	81.72	-2.97	32.69	156.14	0.14	-0.09
61	Fondazio ne	25, 26	0	81.78	0.87	31.50	-153.37	0.15	0.13
			49	81.90	0.87	-5.18	2.61	0.12	-0.04
			97	82.10	0.87	33.83	157.67	0.18	-0.20
62	Fondazio ne	25, 26	0	81.95	0.10	34.83	-151.30	0.18	0.15
			49	82.20	0.10	-1.39	2.39	0.14	0.00
			97	82.52	0.10	36.72	154.10	0.18	-0.15
63	Fondazio ne	25, 26	0	81.84	-0.13	36.18	-150.03	0.18	0.13
			49	82.23	-0.13	-0.52	-0.94	0.15	-0.01
			97	82.68	-0.13	34.57	144.86	0.19	-0.13
64	Fondazio ne	25, 26	0	81.16	-0.57	30.89	-152.12	0.19	0.13
			49	81.68	-0.57	-8.55	-10.22	0.16	0.02
			97	82.25	-0.57	20.04	127.46	0.17	-0.06
65	Fondazio ne	25, 26	0	79.52	-0.80	9.78	-159.98	0.17	0.11
			49	80.16	-0.80	-35.56	-26.41	0.14	0.04
			97	80.86	-0.80	-16.72	104.02	0.13	0.00
66	Fondazio ne	25, 26	0	76.64	-0.37	-34.49	-177.71	0.13	0.07
			49	77.40	-0.37	-89.70	-48.44	0.11	0.05
			97	78.23	-0.37	-81.57	83.41	0.08	0.05
67	Fondazio ne	25, 26	0	72.70	0.99	-106.87	-202.02	0.09	0.39
			49	73.59	0.99	-171.82	-62.14	-0.11	0.42
			97	74.53	0.99	-165.16	93.86	-0.33	0.48
68	Fondazio ne	25, 26	0	67.62	1.98	-185.24	-222.27	-0.32	-1.36
			49	68.61	1.98	-250.59	-39.95	0.32	-1.28
			97	69.67	1.98	-218.29	181.35	0.92	-1.18
69	Fondazio ne	25, 26	0	72.11	2.47	-214.77	-256.25	0.93	2.30
			49	73.21	2.47	-275.48	17.93	-0.22	2.43
			97	74.38	2.47	-186.93	359.58	-1.45	2.60
70	Fondazio ne	25, 28	0	25.92	-83.19	45.90	-513.00	8.31	24.20
			43	25.87	-83.17	-105.96	-202.28	-1.77	23.25
			85	25.83	-83.15	-126.28	106.62	-11.45	22.32
71	Fondazio ne	25, 28	0	30.83	106.63	-124.26	4.56	-11.46	-30.08
			43	30.80	106.65	-56.29	316.11	1.53	-31.04
			85	30.80	106.67	145.33	633.84	14.94	-32.08
72	Fondazio ne	26, 27	0	27.98	55.72	31.60	-448.15	-6.90	-27.12
			33	27.85	55.70	-73.73	-190.29	1.92	-26.31

			66	27.74	55.68	-93.88	68.29	10.46	-25.49
73	Fondazio ne	26, 27	0	33.25	-107.45	-99.56	80.98	10.47	37.71
			33	33.16	-107.47	-29.86	341.80	-2.11	38.55
			66	33.07	-107.49	126.44	605.99	-14.98	39.43
74	Fondazio ne	27, 29	0	-4.98	88.90	123.16	-517.85	-13.47	-41.05
			33	-5.06	88.88	-3.72	-250.86	-0.07	-40.16
			66	-5.14	88.86	-42.16	18.13	13.04	-39.28
75	Fondazio ne	27, 29	0	-3.89	-95.04	-44.36	7.25	13.04	37.90
			33	-3.98	-95.06	2.75	278.65	0.39	38.78
			66	-4.07	-95.09	139.89	552.83	-12.56	39.70
76	Fondazio ne	28, 30	0	-12.24	-82.28	146.65	-547.88	13.17	38.02
			37	-12.24	-82.26	-2.83	-270.70	-0.55	37.12
			73	-12.25	-82.24	-50.66	9.09	-13.94	36.25
77	Fondazio ne	28, 30	0	-5.44	107.84	-56.25	-5.69	-13.94	-37.46
			37	-5.45	107.86	-6.78	277.37	-0.10	-38.35
			73	-5.46	107.88	146.73	564.45	14.07	-39.29
78	Fondazio ne	29, 31	0	36.30	96.52	142.31	-555.45	-14.09	-40.85
			33	36.22	96.49	4.53	-279.50	-0.77	-39.92
			66	36.15	96.47	-42.06	-2.80	12.25	-39.00
79	Fondazio ne	29, 31	0	36.87	-90.52	-42.27	-23.29	12.26	39.10
			33	36.81	-90.54	-4.15	254.49	-0.80	40.02
			66	36.77	-90.56	125.88	533.78	-14.16	40.97
80	Fondazio ne	30, 32	0	0.28	-87.67	141.91	-543.69	14.09	40.95
			34	0.27	-87.65	2.22	-271.76	0.21	40.06
			69	0.26	-87.63	-44.11	1.45	-13.36	39.19
81	Fondazio ne	30, 32	0	0.93	104.58	-50.69	11.57	-13.36	-39.19
			34	0.92	104.60	0.30	286.51	0.21	-40.06
			69	0.91	104.62	145.83	563.64	14.09	-40.97
82	Fondazio ne	31, 33	0	-5.52	96.22	130.41	-551.72	-12.61	-39.86
			33	-5.56	96.20	-5.45	-271.77	0.39	-38.92
			66	-5.60	96.18	-48.96	8.03	13.08	-38.00
83	Fondazio ne	31, 33	0	-3.43	-91.32	-50.98	-18.82	13.08	37.29
			33	-3.47	-91.34	-10.99	261.31	0.62	38.21
			66	-3.51	-91.36	121.60	542.32	-12.15	39.16
84	Fondazio ne	32, 34	0	3.05	-96.25	142.75	-573.48	14.10	41.10
			35	3.04	-96.23	-6.76	-293.23	0.08	40.18
			69	3.03	-96.21	-59.58	-12.95	-13.63	39.28
85	Fondazio ne	32, 34	0	2.04	102.69	-56.78	-1.22	-13.63	-38.78
			35	2.04	102.71	-8.77	279.76	-0.09	-39.68
			69	2.03	102.73	136.42	562.10	13.76	-40.62
86	Fondazio ne	33, 35	0	32.41	93.94	126.09	-548.39	-13.67	-40.09
			33	32.38	93.92	-8.46	-267.23	-0.60	-39.14
			66	32.35	93.90	-50.34	13.32	12.16	-38.21
87	Fondazio ne	33, 35	0	35.58	-92.28	-53.67	-15.79	12.16	38.76
			33	35.57	-92.30	-12.61	264.68	-0.78	39.69
			66	35.57	-92.32	121.09	545.67	-14.04	40.64
88	Fondazio ne	34, 36	0	3.76	-88.40	127.07	-552.17	13.77	40.24
			35	3.75	-88.38	-14.63	-269.40	0.06	39.30
			69	3.74	-88.36	-58.86	12.95	-13.34	38.38
89	Fondazio ne	34, 36	0	3.33	104.47	-62.28	-7.10	-13.34	-38.20
			35	3.32	104.49	-16.00	275.59	-0.01	-39.12
			69	3.32	104.51	128.01	559.42	13.65	-40.07
90	Fondazio ne	35, 37	0	-8.73	92.04	125.30	-540.80	-12.49	-39.73
			33	-8.72	92.02	-6.81	-260.01	0.46	-38.79
			66	-8.72	92.00	-46.42	19.81	13.11	-37.88

91	Fondazio ne	35, 37	0	-4.83	-94.36	-50.89	-8.07	13.11	37.55
			33	-4.83	-94.38	-7.46	271.27	0.57	38.47
			66	-4.83	-94.40	128.16	550.64	-12.28	39.40
92	Fondazio ne	36, 38	0	5.39	-81.13	119.51	-545.51	13.68	40.11
			35	5.39	-81.11	-19.66	-261.34	0.00	39.15
			69	5.39	-81.09	-60.86	22.45	-13.34	38.22
93	Fondazio ne	36, 38	0	3.47	114.81	-68.91	-0.84	-13.34	-37.84
			35	3.47	114.83	-20.20	283.43	-0.13	-38.78
			69	3.48	114.85	126.81	569.06	13.42	-39.74
94	Fondazio ne	37, 39	0	31.27	91.22	130.87	-533.98	-13.81	-40.37
			33	31.27	91.20	0.66	-255.40	-0.64	-39.43
			66	31.29	91.18	-37.89	21.50	12.22	-38.52
95	Fondazio ne	37, 39	0	34.52	-94.24	-42.29	2.56	12.22	39.32
			33	34.54	-94.26	4.05	278.13	-0.91	40.23
			66	34.58	-94.28	141.16	552.69	-14.33	41.15
96	Fondazio ne	38, 40	0	8.44	-67.12	107.44	-527.11	13.46	39.47
			34	8.45	-67.10	-24.42	-242.89	0.11	38.51
			69	8.46	-67.08	-58.94	41.41	-12.92	37.57
97	Fondazio ne	38, 40	0	3.96	128.71	-76.62	10.17	-12.92	-36.98
			34	3.97	128.73	-24.34	295.45	-0.10	-37.92
			69	3.99	128.75	125.98	582.65	13.05	-38.89
98	Fondazio ne	39, 41	0	-9.89	96.62	144.35	-564.13	-12.81	-39.99
			33	-9.85	96.60	3.23	-291.60	0.24	-39.08
			66	-9.81	96.58	-48.46	-22.14	12.99	-38.21
99	Fondazio ne	39, 41	0	-7.99	-88.15	-48.62	-35.24	12.99	40.02
			33	-7.96	-88.17	-16.17	231.56	-0.36	40.88
			66	-7.92	-88.20	103.98	496.29	-13.99	41.75
100	Fondazio ne	40, 42	0	10.47	-49.24	98.32	-515.65	13.10	40.22
			35	10.49	-49.21	-29.47	-225.02	-0.61	39.24
			69	10.51	-49.19	-56.86	66.48	-13.98	38.28
101	Fondazio ne	40, 42	0	10.06	159.32	-88.85	80.23	-13.98	-39.52
			35	10.09	159.34	-10.65	373.59	-0.18	-40.49
			69	10.12	159.37	169.23	669.69	13.96	-41.48
102	Fondazio ne	41, 44	0	-14.37	100.90	107.42	-581.99	-13.98	-39.08
			33	-14.34	100.88	-41.31	-319.87	-1.23	-38.22
			66	-14.32	100.86	-104.03	-60.68	11.24	-37.40
103	Fondazio ne	41, 44	0	-22.76	-60.84	-103.56	-41.00	11.24	22.60
			33	-22.74	-60.86	-74.58	216.57	3.65	23.39
			66	-22.73	-60.88	39.37	474.08	-4.20	24.19
104	Fondazio ne	42, 43	0	15.02	-43.94	136.89	-315.30	13.95	37.79
			23	15.04	-43.92	87.18	-116.90	5.34	37.11
			46	15.07	-43.91	83.11	81.54	-3.12	36.45
105	Fondazio ne	43, 44	0	105.49	22.45	-205.03	-449.84	-6.44	-8.63
			49	104.13	22.45	-329.04	-75.81	-2.22	-8.67
			97	102.86	22.45	-291.15	218.44	2.01	-8.72
106	Fondazio ne	43, 44	0	95.02	1.23	-277.00	-167.83	2.01	2.21
			49	93.82	1.23	-299.66	64.70	0.95	2.15
			97	92.70	1.23	-220.69	252.63	-0.09	2.11
107	Fondazio ne	43, 44	0	90.26	-4.52	-185.32	-90.72	-0.09	-0.14
			49	89.21	-4.52	-189.77	67.56	-0.01	-0.17
			97	88.23	-4.52	-122.04	207.66	0.08	-0.19
108	Fondazio ne	43, 44	0	90.48	-0.37	-89.80	-83.16	0.09	0.12
			49	89.57	-0.37	-98.00	47.73	0.03	0.12
			97	88.73	-0.37	-43.48	175.43	-0.03	0.13
109	Fondazio	43, 44	0	90.82	-0.09	-20.55	-101.92	-0.03	0.03

	ne								
			49	90.05	-0.09	-38.79	26.74	-0.05	0.05
			97	89.35	-0.09	6.30	158.62	-0.08	0.10
110	Fondazio ne	43, 44	0	91.14	-0.16	19.09	-125.89	-0.08	-0.02
			49	90.51	-0.16	-9.10	10.33	-0.08	0.03
			97	89.95	-0.16	30.11	151.06	-0.11	0.11
111	Fondazio ne	43, 44	0	91.05	-0.24	34.94	-143.98	-0.11	-0.07
			49	90.56	-0.24	0.07	0.96	-0.10	0.02
			97	90.15	-0.24	36.63	149.49	-0.13	0.11
112	Fondazio ne	43, 44	0	90.58	-0.28	37.58	-153.86	-0.13	-0.09
			49	90.24	-0.28	-0.49	-2.44	-0.11	0.01
			97	89.97	-0.28	35.68	151.15	-0.14	0.13
113	Fondazio ne	43, 44	0	89.90	-0.60	35.46	-158.07	-0.14	-0.12
			49	89.70	-0.60	-3.73	-2.93	-0.11	0.00
			97	89.57	-0.60	32.83	153.19	-0.14	0.12
114	Fondazio ne	43, 44	0	89.08	1.41	33.60	-155.94	-0.14	-0.11
			49	89.02	1.41	-4.18	0.69	-0.11	0.02
			97	89.03	1.41	34.29	157.34	-0.15	0.15
115	Fondazio ne	43, 44	0	88.31	-0.59	33.11	-154.60	-0.15	-0.15
			49	88.39	-0.59	-4.11	1.60	-0.11	-0.01
			97	88.53	-0.59	34.47	156.86	-0.14	0.12
116	Fondazio ne	43, 44	0	87.30	0.16	35.21	-152.14	-0.14	-0.12
			49	87.52	0.16	-1.38	1.67	-0.11	0.00
			97	87.80	0.16	36.40	153.41	-0.14	0.13
117	Fondazio ne	43, 44	0	85.97	0.41	36.00	-150.46	-0.15	-0.13
			49	86.32	0.41	-0.90	-1.42	-0.11	-0.01
			97	86.74	0.41	33.93	144.26	-0.13	0.10
118	Fondazio ne	43, 44	0	84.04	0.71	30.14	-151.85	-0.14	-0.12
			49	84.53	0.71	-9.20	-10.10	-0.10	-0.02
			97	85.08	0.71	19.42	127.43	-0.11	0.07
119	Fondazio ne	43, 44	0	81.28	0.83	9.30	-158.93	-0.12	-0.11
			49	81.90	0.83	-35.55	-25.48	-0.08	-0.03
			97	82.58	0.83	-16.27	104.88	-0.08	0.03
120	Fondazio ne	43, 44	0	77.61	1.06	-35.00	-174.92	-0.09	-0.18
			49	78.36	1.06	-88.86	-45.67	-0.01	-0.13
			97	79.17	1.06	-79.37	86.17	0.04	-0.09
121	Fondazio ne	43, 44	0	73.60	0.77	-106.16	-200.34	0.03	0.28
			49	74.47	0.77	-170.30	-60.50	-0.11	0.30
			97	75.39	0.77	-162.87	95.32	-0.26	0.31
122	Fondazio ne	43, 44	0	69.88	2.98	-186.04	-224.83	-0.26	-1.81
			49	70.86	2.98	-252.72	-42.89	0.62	-1.82
			97	71.90	2.98	-221.97	177.89	1.51	-1.84
123	Fondazio ne	43, 44	0	72.35	2.86	-224.94	-238.23	1.51	2.24
			49	73.44	2.86	-276.99	35.50	0.42	2.21
			97	74.59	2.86	-179.93	377.00	-0.65	2.20
124	Fondazio ne	43, 45	0	45.59	-109.18	143.99	-674.10	4.81	25.70
			33	45.63	-109.16	-31.61	-390.36	-3.51	24.77
			66	45.69	-109.13	-113.86	-108.24	-11.54	23.86
125	Fondazio ne	43, 45	0	47.17	69.58	-62.83	-9.27	-11.54	-38.66
			33	47.25	69.60	-19.44	272.34	1.37	-39.58
			66	47.35	69.62	116.92	554.30	14.59	-40.51
126	Fondazio ne	44, 46	0	23.87	57.78	35.47	-458.06	-6.40	-26.38
			33	23.88	57.76	-73.14	-200.04	2.17	-25.58
			66	23.90	57.74	-96.45	59.05	10.48	-24.78
127	Fondazio ne	44, 46	0	36.10	-120.27	-116.00	146.17	10.49	37.67

			33	36.13	-120.29	-24.69	407.87	-2.08	38.49
			66	36.17	-120.31	153.59	673.35	-14.92	39.34
128	Fondazio ne	45, 47	0	9.37	-132.77	136.52	-615.88	13.01	41.00
			33	9.47	-132.75	-20.24	-334.21	-0.37	40.07
			66	9.58	-132.72	-84.21	-53.51	-13.44	39.16
129	Fondazio ne	45, 47	0	15.59	68.85	-48.58	-9.00	-13.44	-38.97
			33	15.70	68.87	-5.30	271.53	-0.43	-39.87
			66	15.82	68.89	130.63	552.47	12.88	-40.80
130	Fondazio ne	46, 48	0	-1.23	99.84	145.40	-554.56	-13.41	-40.00
			33	-1.18	99.82	6.62	-286.12	-0.35	-39.14
			66	-1.14	99.80	-43.26	-15.80	12.43	-38.30
131	Fondazio ne	46, 48	0	10.18	-93.02	-33.74	7.03	12.43	36.20
			33	10.23	-93.04	13.46	279.53	0.34	37.04
			66	10.28	-93.07	150.99	554.41	-12.02	37.91
132	Fondazio ne	47, 49	0	60.04	-120.36	139.29	-565.97	14.37	41.20
			33	60.17	-120.34	-1.19	-285.49	0.93	40.27
			66	60.33	-120.32	-49.34	-6.40	-12.21	39.38
133	Fondazio ne	47, 49	0	68.00	69.01	-35.31	-16.51	-12.21	-40.07
			33	68.18	69.03	5.11	261.60	1.16	-40.96
			66	68.38	69.06	137.20	539.05	14.83	-41.86
134	Fondazio ne	48, 50	0	55.57	110.00	165.26	-572.34	-13.56	-39.43
			33	55.64	109.98	21.92	-296.31	-0.69	-38.56
			66	55.72	109.96	-30.37	-20.49	11.89	-37.71
135	Fondazio ne	48, 50	0	66.65	-77.81	-25.32	-1.50	11.89	40.14
			33	66.75	-77.83	19.65	274.17	-1.49	40.98
			66	66.88	-77.85	155.58	549.75	-15.16	41.84
136	Fondazio ne	49, 51	0	30.33	-129.21	157.57	-582.58	13.36	41.43
			33	30.55	-129.19	10.84	-306.85	-0.17	40.55
			66	30.78	-129.17	-45.36	-34.00	-13.41	39.71
137	Fondazio ne	49, 51	0	40.25	62.26	-25.71	-37.44	-13.41	-41.40
			33	40.49	62.28	6.54	232.77	0.39	-42.23
			66	40.75	62.29	127.57	500.58	14.46	-43.06
138	Fondazio ne	50, 52	0	26.17	131.22	177.73	-607.89	-13.72	-42.05
			33	26.32	131.20	22.41	-333.74	0.01	-41.20
			66	26.47	131.18	-42.91	-62.46	13.48	-40.40
139	Fondazio ne	50, 52	0	38.94	-62.05	-21.47	-36.59	13.47	42.80
			33	39.11	-62.07	10.80	231.94	-0.78	43.59
			66	39.29	-62.09	131.26	497.86	-15.30	44.39
140	Fondazio ne	51, 53	0	76.97	-152.05	156.90	-565.53	16.23	43.72
			33	77.25	-152.03	13.97	-301.15	1.93	42.91
			66	77.56	-152.01	-42.48	-41.38	-12.10	42.15
141	Fondazio ne	51, 53	0	86.34	32.11	-7.30	-38.64	-12.09	-44.21
			33	86.68	32.13	22.13	216.68	2.62	-44.94
			66	87.04	32.15	135.09	467.52	17.56	-45.64
142	Fondazio ne	52, 54	0	43.71	156.00	164.65	-589.08	-15.43	-43.49
			33	43.91	155.98	13.62	-326.86	-1.21	-42.72
			66	44.12	155.97	-51.69	-69.57	12.77	-41.99
143	Fondazio ne	52, 54	0	51.16	-33.34	-14.76	-55.44	12.76	44.04
			33	51.39	-33.36	8.71	197.15	-1.88	44.73
			66	51.64	-33.38	114.78	445.21	-16.76	45.41
144	Fondazio ne	53, 55	0	42.26	-195.95	184.50	-626.48	14.99	37.63
			33	42.66	-195.93	18.31	-381.40	2.68	36.98
			66	43.06	-195.91	-68.17	-143.48	-9.43	36.42
145	Fondazio ne	53, 55	0	44.87	-44.98	-5.84	-158.70	-9.41	-28.95
			33	45.29	-44.96	-19.99	72.33	0.23	-29.44

			66	45.73	-44.95	41.03	296.88	10.01	-29.85
146	Fondazio ne	54, 56	0	51.28	191.65	166.77	-607.37	-15.86	-38.72
			33	51.55	191.63	6.49	-364.86	-3.19	-38.08
			66	51.83	191.62	-74.87	-129.02	9.29	-37.52
147	Fondazio ne	54, 56	0	49.56	37.34	-14.61	-128.17	9.27	28.87
			33	49.87	37.33	-18.92	101.43	-0.34	29.36
			66	50.19	37.32	51.59	325.27	-10.10	29.78
148	Fondazio ne	55, 57	0	52.02	-149.73	99.67	-533.08	6.30	10.04
			40	52.58	-149.71	-59.99	-271.44	2.39	9.65
			80	53.16	-149.70	-117.61	-19.32	-1.39	9.39
149	Fondazio ne	55, 57	0	53.15	-40.09	-76.89	-145.77	-1.36	-9.66
			40	53.76	-40.08	-86.04	99.44	2.50	-9.76
			80	54.40	-40.07	1.39	340.58	6.38	-9.71
150	Fondazio ne	56, 70	0	54.90	146.99	109.77	-546.94	-6.34	-10.17
			40	55.32	146.97	-55.41	-285.35	-2.38	-9.76
			80	55.76	146.96	-118.42	-32.60	1.44	-9.48
151	Fondazio ne	56, 70	0	53.36	37.28	-74.88	-148.85	1.42	9.59
			40	53.83	37.27	-84.99	97.61	-2.43	9.73
			80	54.33	37.26	2.08	340.56	-6.30	9.72
152	Fondazio ne	57, 58	0	-25.32	-3.76	25.15	-402.48	-2.49	1.99
			42	-25.22	-3.76	-91.72	-163.97	-3.19	1.40
			83	-25.13	-3.77	-114.31	51.70	-3.68	0.99
153	Fondazio ne	57, 58	0	-22.85	15.22	-140.89	-54.93	-3.66	1.36
			42	-22.78	15.22	-122.26	141.78	-4.17	1.10
			83	-22.72	15.22	-25.01	324.14	-4.59	0.96
154	Fondazio ne	58, 59	0	-59.95	16.33	-33.77	-222.37	-3.84	-4.51
			35	-59.91	16.33	-85.67	-79.75	-2.28	-4.56
			69	-59.90	16.33	-89.55	56.30	-0.70	-4.56
155	Fondazio ne	58, 59	0	-41.43	3.04	-93.40	-5.33	-0.69	1.37
			35	-41.43	3.04	-72.47	125.97	-1.17	1.41
			69	-41.46	3.04	-6.82	254.21	-1.67	1.48
156	Fondazio ne	59, 60	0	-27.37	2.59	-7.04	-186.03	-1.48	-1.66
			35	-27.41	2.59	-49.40	-59.90	-0.92	-1.56
			69	-27.46	2.59	-48.51	64.81	-0.40	-1.44
157	Fondazio ne	59, 60	0	-15.81	1.39	-48.53	-14.96	-0.40	0.24
			35	-15.86	1.39	-32.24	109.36	-0.51	0.38
			69	-15.93	1.39	27.01	234.14	-0.66	0.54
158	Fondazio ne	60, 61	0	-6.64	-2.17	27.78	-186.92	-0.59	-0.37
			35	-6.71	-2.17	-15.08	-61.52	-0.49	-0.20
			69	-6.78	-2.17	-14.57	64.51	-0.46	-0.01
159	Fondazio ne	60, 61	0	-2.37	-0.79	-12.17	-28.67	-0.46	-0.47
			35	-2.44	-0.79	-0.18	98.31	-0.33	-0.27
			69	-2.51	-0.79	55.81	226.39	-0.27	-0.06
160	Fondazio ne	61, 62	0	26.61	-6.88	58.71	-218.79	-0.27	-0.69
			35	26.54	-6.88	5.44	-90.05	-0.07	-0.48
			69	26.48	-6.88	-3.39	38.85	0.06	-0.26
161	Fondazio ne	61, 62	0	30.40	-5.85	0.87	-56.67	0.06	0.03
			35	30.35	-5.85	3.58	72.37	0.01	0.26
			69	30.32	-5.85	50.83	201.54	-0.11	0.49
162	Fondazio ne	62, 63	0	11.72	-10.09	56.10	-229.22	-0.13	0.08
			35	11.70	-10.10	-0.73	-100.36	-0.20	0.32
			69	11.67	-10.10	-13.22	27.77	-0.35	0.57
163	Fondazio ne	62, 63	0	15.03	-5.51	-8.18	-75.71	-0.35	-0.45
			35	15.02	-5.51	-12.28	51.85	-0.24	-0.20
			69	15.01	-5.51	27.57	179.09	-0.21	0.06

164	Fondazio ne	63, 64	0	16.63	-3.68	30.59	-198.66	-0.21	-0.29
			35	16.63	-3.68	-16.05	-71.79	-0.16	-0.03
			69	16.63	-3.68	-19.00	54.67	-0.19	0.23
165	Fondazio ne	63, 64	0	16.97	3.65	-19.05	-54.95	-0.19	-0.24
			35	16.98	3.65	-16.20	71.51	-0.15	0.02
			69	17.00	3.65	30.34	198.35	-0.20	0.28
166	Fondazio ne	64, 65	0	16.04	5.48	27.48	-179.48	-0.20	-0.07
			35	16.07	5.47	-12.51	-52.29	-0.22	0.19
			69	16.09	5.47	-8.58	75.21	-0.33	0.45
167	Fondazio ne	64, 65	0	13.43	10.20	-13.72	-28.15	-0.33	-0.58
			35	13.46	10.20	-1.37	99.91	-0.17	-0.33
			69	13.50	10.19	55.29	228.72	-0.11	-0.07
168	Fondazio ne	65, 66	0	32.35	6.04	50.07	-201.27	-0.09	-0.54
			35	32.40	6.04	2.90	-72.14	0.05	-0.29
			69	32.46	6.04	0.26	56.89	0.11	-0.05
169	Fondazio ne	65, 66	0	29.32	7.19	-4.19	-37.57	0.11	0.19
			35	29.39	7.19	5.08	91.37	0.01	0.42
			69	29.48	7.19	58.82	220.21	-0.18	0.66
170	Fondazio ne	66, 67	0	0.15	0.75	55.81	-227.49	-0.19	0.16
			35	0.24	0.75	-0.54	-99.24	-0.28	0.39
			69	0.33	0.75	-12.83	27.96	-0.45	0.61
171	Fondazio ne	66, 67	0	-4.55	1.98	-14.42	-66.57	-0.45	-0.16
			35	-4.46	1.98	-15.59	59.76	-0.44	0.06
			69	-4.38	1.98	26.72	185.56	-0.49	0.27
172	Fondazio ne	67, 68	0	-12.41	-0.22	24.84	-227.14	-0.57	-0.53
			35	-12.32	-0.22	-31.91	-101.88	-0.42	-0.33
			69	-12.24	-0.22	-45.52	23.04	-0.34	-0.15
173	Fondazio ne	67, 68	0	-23.14	-1.78	-46.84	-67.99	-0.34	1.33
			35	-23.07	-1.78	-48.71	57.41	-0.83	1.50
			69	-23.01	-1.78	-7.09	184.28	-1.37	1.65
174	Fondazio ne	68, 69	0	-37.13	-1.63	-8.18	-252.10	-1.58	-1.49
			35	-37.07	-1.63	-72.98	-123.06	-1.08	-1.37
			69	-37.03	-1.63	-92.76	9.11	-0.63	-1.27
175	Fondazio ne	68, 69	0	-55.18	-15.14	-89.37	-57.49	-0.64	4.23
			35	-55.16	-15.14	-85.75	79.50	-2.11	4.30
			69	-55.16	-15.14	-33.77	223.13	-3.60	4.32
176	Fondazio ne	69, 70	0	-20.94	-12.13	-27.01	-323.22	-4.38	-0.82
			42	-20.97	-12.13	-123.62	-139.53	-4.04	-0.86
			83	-21.00	-12.13	-141.00	58.70	-3.66	-1.00
177	Fondazio ne	69, 70	0	-25.14	4.93	-118.31	-45.59	-3.68	-0.55
			42	-25.19	4.93	-92.83	171.82	-3.40	-0.83
			83	-25.25	4.93	27.71	412.37	-2.96	-1.29
178	Primo Impalcato	1, 2	0	222.11	0.07	35.00	-2.06	96.86	54.55
			83	222.11	0.07	21.68	-29.99	51.52	54.55
			166	222.11	0.07	-14.86	-57.92	6.17	54.55
179	Primo Impalcato	1, 15	0	60.31	6.77	-25.17	48.00	-115.16	-129.64
			80	60.31	6.77	2.37	21.28	-12.10	-129.64
			159	60.31	6.77	8.67	-5.43	90.96	-129.64
180	Primo Impalcato	2, 3	0	173.19	-0.12	-12.34	18.47	7.73	10.35
			69	173.19	-0.12	-7.59	-4.71	0.59	10.35
			138	173.19	-0.12	-18.84	-27.90	-6.55	10.35
181	Primo Impalcato	3, 4	0	172.92	-0.15	-17.62	30.30	-6.18	-1.29
			69	172.92	-0.15	-4.72	7.11	-5.29	-1.29
			138	172.92	-0.15	-7.81	-16.07	-4.40	-1.29
182	Primo	4, 5	0	172.59	-0.06	-7.45	24.16	-4.26	-2.18

	Impalcato								
			69	172.59	-0.06	1.22	0.98	-2.76	-2.18
			138	172.59	-0.06	-6.11	-22.21	-1.26	-2.18
183	Primo Impalcato	5, 6	0	172.32	-0.01	-5.96	23.11	-1.24	-0.92
			69	172.32	-0.01	1.99	-0.08	-0.61	-0.92
			138	172.32	-0.01	-6.06	-23.26	0.03	-0.92
184	Primo Impalcato	6, 7	0	220.18	0.00	-5.98	23.85	0.03	-0.21
			69	220.18	0.00	2.48	0.67	0.18	-0.21
			138	220.18	0.00	-5.06	-22.52	0.32	-0.21
185	Primo Impalcato	7, 8	0	165.71	0.00	-4.97	21.79	0.31	-0.02
			69	165.71	0.00	2.06	-1.39	0.33	-0.02
			138	165.71	0.00	-6.89	-24.58	0.34	-0.02
186	Primo Impalcato	8, 9	0	165.75	0.00	-6.88	24.48	0.35	0.25
			69	165.75	0.00	2.01	1.29	0.17	0.25
			138	165.75	0.00	-5.10	-21.89	0.00	0.25
187	Primo Impalcato	9, 10	0	225.71	0.01	-5.16	22.63	0.04	0.98
			69	225.71	0.01	2.45	-0.56	-0.64	0.98
			138	225.71	0.01	-5.93	-23.74	-1.31	0.98
188	Primo Impalcato	10, 11	0	178.49	0.06	-6.00	22.13	-1.37	2.17
			69	178.49	0.06	1.28	-1.05	-2.87	2.17
			138	178.49	0.06	-7.45	-24.24	-4.37	2.17
189	Primo Impalcato	11, 12	0	178.84	0.16	-7.69	15.57	-4.51	1.19
			69	178.84	0.16	-4.95	-7.61	-5.33	1.19
			138	178.84	0.16	-18.20	-30.80	-6.15	1.19
190	Primo Impalcato	12, 13	0	179.13	0.13	-19.34	28.72	-6.53	-10.73
			69	179.13	0.13	-7.53	5.53	0.88	-10.73
			138	179.13	0.13	-11.71	-17.65	8.28	-10.73
191	Primo Impalcato	13, 14	0	228.06	-0.08	-14.17	53.83	6.71	-55.58
			83	228.06	-0.08	18.97	25.91	52.91	-55.58
			166	228.06	-0.08	28.89	-2.02	99.11	-55.58
192	Primo Impalcato	14, 16	0	58.25	-6.60	-26.32	48.71	105.87	120.90
			80	58.25	-6.60	1.78	22.00	9.75	120.90
			159	58.25	-6.60	8.65	-4.71	-86.36	120.90
193	Primo Impalcato	15, 17	0	-6.59	0.95	-1.10	31.17	81.32	35.95
			66	-6.59	0.95	12.15	8.99	57.59	35.95
			132	-6.59	0.95	10.77	-13.18	33.86	35.95
194	Primo Impalcato	16, 18	0	-8.59	-1.08	-3.27	33.60	-77.52	-33.97
			66	-8.59	-1.08	11.59	11.43	-55.10	-33.97
			132	-8.59	-1.08	11.81	-10.75	-32.68	-33.97
195	Primo Impalcato	17, 19	0	37.63	0.07	4.43	21.82	31.02	22.97
			66	37.63	0.07	11.52	-0.35	15.86	22.97
			132	37.63	0.07	3.97	-22.53	0.70	22.97
196	Primo Impalcato	18, 20	0	32.22	-0.09	5.67	19.73	-33.34	-24.51
			66	32.22	-0.09	11.38	-2.45	-17.16	-24.51
			132	32.22	-0.09	2.45	-24.62	-0.99	-24.51
197	Primo Impalcato	19, 21	0	-26.31	-0.08	1.27	22.18	1.87	2.90
			66	-26.31	-0.08	8.59	0.00	-0.04	2.90
			132	-26.31	-0.08	1.28	-22.17	-1.96	2.90
198	Primo Impalcato	20, 22	0	-33.32	0.05	-2.15	25.87	-2.04	-3.06
			66	-33.32	0.05	7.61	3.70	-0.02	-3.06
			132	-33.32	0.05	2.73	-18.48	2.00	-3.06
199	Primo Impalcato	21, 23	0	41.58	-0.03	1.25	21.62	-2.49	-1.31
			66	41.58	-0.03	8.20	-0.56	-1.63	-1.31
			132	41.58	-0.03	0.52	-22.73	-0.77	-1.31
200	Primo Impalcato	22, 24	0	25.61	0.02	3.31	17.79	2.70	1.33

			66	25.61	0.02	7.73	-4.38	1.82	1.33
			132	25.61	0.02	-2.48	-26.56	0.94	1.33
201	Primo Impalcato	23, 25	0	-10.85	0.03	2.82	7.57	0.06	0.12
			66	-10.85	0.03	0.49	-14.61	-0.01	0.12
			132	-10.85	0.03	-16.47	-36.78	-0.09	0.12
202	Primo Impalcato	24, 26	0	-29.11	-0.02	-3.42	16.18	0.13	0.11
			66	-29.11	-0.02	-0.06	-5.99	0.06	0.11
			132	-29.11	-0.02	-11.33	-28.17	-0.02	0.11
203	Primo Impalcato	25, 28	0	67.67	-0.01	-14.93	28.24	-0.95	-0.21
			85	67.67	-0.01	-3.06	-0.32	-0.78	-0.21
			170	67.67	-0.01	-15.47	-28.88	-0.60	-0.21
204	Primo Impalcato	26, 27	0	26.19	0.02	-11.47	27.55	0.76	0.55
			66	26.19	0.02	-0.60	5.38	0.39	0.55
			132	26.19	0.02	-4.37	-16.80	0.03	0.55
205	Primo Impalcato	27, 29	0	-32.52	0.01	-11.67	31.68	-0.68	-0.07
			66	-32.52	0.01	1.92	9.50	-0.63	-0.07
			132	-32.52	0.01	0.88	-12.67	-0.58	-0.07
206	Primo Impalcato	28, 30	0	-14.62	-0.02	-11.88	32.10	0.23	0.00
			73	-14.62	-0.02	2.59	7.57	0.23	0.00
			146	-14.62	-0.02	-0.83	-16.96	0.22	0.00
207	Primo Impalcato	29, 31	0	20.58	0.01	-2.63	23.95	0.16	-0.11
			66	20.58	0.01	5.86	1.77	0.23	-0.11
			132	20.58	0.01	-0.29	-20.40	0.31	-0.11
208	Primo Impalcato	30, 32	0	-20.56	0.01	4.78	13.91	0.17	0.09
			69	-20.56	0.01	6.42	-9.11	0.11	0.09
			137	-20.56	0.01	-7.70	-32.12	0.05	0.09
209	Primo Impalcato	31, 33	0	-31.42	0.01	-8.69	27.94	-0.44	-0.08
			66	-31.42	0.01	2.43	5.77	-0.40	-0.08
			132	-31.42	0.01	-1.08	-16.41	-0.35	-0.08
210	Primo Impalcato	32, 34	0	-26.85	0.01	-0.07	16.84	0.01	0.07
			69	-26.85	0.01	3.55	-6.35	-0.03	0.07
			138	-26.85	0.01	-8.83	-29.53	-0.08	0.07
211	Primo Impalcato	33, 35	0	30.65	0.01	-6.90	28.43	0.40	-0.02
			66	30.65	0.01	4.54	6.25	0.42	-0.02
			132	30.65	0.01	1.35	-15.92	0.44	-0.02
212	Primo Impalcato	34, 36	0	-33.79	0.01	0.09	15.96	-0.12	0.02
			69	-33.79	0.01	3.10	-7.22	-0.14	0.02
			138	-33.79	0.01	-9.88	-30.41	-0.15	0.02
213	Primo Impalcato	35, 37	0	-17.29	0.02	-7.29	26.88	-0.32	-0.02
			66	-17.29	0.02	3.14	4.71	-0.30	-0.02
			132	-17.29	0.02	-1.07	-17.47	-0.29	-0.02
214	Primo Impalcato	36, 38	0	-41.48	0.01	0.10	15.04	-0.21	0.00
			69	-41.48	0.01	2.48	-8.14	-0.21	0.00
			138	-41.48	0.01	-11.14	-31.33	-0.21	0.00
215	Primo Impalcato	37, 39	0	50.72	0.01	-7.21	23.92	0.48	0.02
			66	50.72	0.01	1.26	1.74	0.46	0.02
			132	50.72	0.01	-4.91	-20.44	0.45	0.02
216	Primo Impalcato	38, 40	0	-49.98	-0.01	-0.35	14.71	-0.31	-0.32
			69	-49.98	-0.01	1.85	-8.30	-0.09	-0.32
			137	-49.98	-0.01	-11.72	-31.32	0.14	-0.32
217	Primo Impalcato	39, 41	0	-2.57	0.02	-10.05	34.65	-0.29	0.20
			66	-2.57	0.02	5.50	12.47	-0.42	0.20
			132	-2.57	0.02	6.42	-9.70	-0.55	0.20
218	Primo Impalcato	40, 42	0	-59.22	-0.04	-0.54	24.32	0.02	-1.10
			69	-59.22	-0.04	8.25	1.14	0.77	-1.10

			138	-59.22	-0.04	1.04	-22.04	1.53	-1.10
219	Primo Impalcato	41, 44	0	6.20	-0.02	2.00	7.46	-0.60	-0.68
			66	6.20	-0.02	-0.39	-14.72	-0.15	-0.68
			132	6.20	-0.02	-17.43	-36.89	0.30	-0.68
220	Primo Impalcato	42, 43	0	-69.16	0.07	14.58	-50.18	1.50	1.09
			23	-69.16	0.07	2.15	-57.91	1.25	1.09
			46	-69.16	0.07	-12.05	-65.64	1.00	1.09
221	Primo Impalcato	43, 45	0	-3.87	0.00	-10.54	26.69	0.25	0.42
			66	-3.87	0.00	-0.24	4.52	-0.03	0.42
			132	-3.87	0.00	-4.58	-17.66	-0.31	0.42
222	Primo Impalcato	44, 46	0	62.53	0.03	-17.63	33.41	1.02	0.66
			66	62.53	0.03	-2.89	11.23	0.58	0.66
			132	62.53	0.03	-2.80	-10.94	0.15	0.66
223	Primo Impalcato	45, 47	0	-61.40	0.01	-3.91	21.93	0.55	0.78
			66	-61.40	0.01	3.25	-0.24	0.03	0.78
			132	-61.40	0.01	-4.23	-22.42	-0.49	0.78
224	Primo Impalcato	46, 48	0	1.12	-0.01	-9.67	32.15	-0.59	-0.66
			66	1.12	-0.01	4.23	9.97	-0.15	-0.66
			132	1.12	-0.01	3.49	-12.20	0.28	-0.66
225	Primo Impalcato	47, 49	0	3.79	0.03	-3.19	26.50	-1.23	1.24
			66	3.79	0.03	6.98	4.33	-2.05	1.24
			132	3.79	0.03	2.52	-17.85	-2.87	1.24
226	Primo Impalcato	48, 50	0	63.01	-0.04	2.34	17.18	0.96	-1.38
			66	63.01	-0.04	6.36	-5.00	1.87	-1.38
			132	63.01	-0.04	-4.26	-27.17	2.78	-1.38
227	Primo Impalcato	49, 51	0	-51.53	0.06	5.31	14.18	-2.30	-3.05
			66	-51.53	0.06	7.35	-8.00	-0.29	-3.05
			132	-51.53	0.06	-5.25	-30.17	1.72	-3.05
228	Primo Impalcato	50, 52	0	0.55	-0.06	-2.51	29.71	2.31	3.43
			66	0.55	-0.06	9.79	7.54	0.04	3.43
			132	0.55	-0.06	7.44	-14.64	-2.22	3.43
229	Primo Impalcato	51, 53	0	20.53	-0.08	-0.36	26.39	0.56	-22.93
			66	20.53	-0.08	9.74	4.21	15.69	-22.93
			132	20.53	-0.08	5.20	-17.96	30.82	-22.93
230	Primo Impalcato	52, 54	0	2.11	0.08	10.32	16.27	-1.38	22.74
			66	2.11	0.08	13.74	-5.90	-16.38	22.74
			132	2.11	0.08	2.53	-28.08	-31.39	22.74
231	Primo Impalcato	53, 55	0	-18.53	-0.95	13.10	9.34	33.65	-36.28
			66	-18.53	-0.95	11.94	-12.84	57.60	-36.28
			132	-18.53	-0.95	-3.85	-35.02	81.54	-36.28
232	Primo Impalcato	54, 56	0	-5.02	1.01	13.57	5.99	-34.04	35.86
			66	-5.02	1.01	10.21	-16.19	-57.71	35.86
			132	-5.02	1.01	-7.79	-38.36	-81.39	35.86
233	Primo Impalcato	55, 57	0	54.16	-6.78	7.32	4.97	91.20	129.80
			80	54.16	-6.78	0.65	-21.74	-11.99	129.80
			159	54.16	-6.78	-27.25	-48.45	-115.18	129.80
234	Primo Impalcato	56, 70	0	62.38	6.63	4.75	8.43	-79.41	-113.20
			80	62.38	6.63	0.84	-18.28	10.59	-113.20
			159	62.38	6.63	-24.31	-44.99	100.59	-113.20
235	Primo Impalcato	57, 58	0	223.18	-0.03	35.33	-2.44	-96.81	-54.44
			83	223.18	-0.03	21.70	-30.37	-51.55	-54.44
			166	223.18	-0.03	-15.15	-58.29	-6.30	-54.44
236	Primo Impalcato	58, 59	0	176.04	0.12	-12.63	18.33	-7.85	-10.35
			69	176.04	0.12	-7.98	-4.85	-0.70	-10.35
			138	176.04	0.12	-19.33	-28.04	6.44	-10.35

237	Primo Impalcato	59, 60	0	175.78	0.15	-18.16	30.95	6.07	1.21
			69	175.78	0.15	-4.80	7.77	5.23	1.21
			138	175.78	0.15	-7.44	-15.42	4.39	1.21
238	Primo Impalcato	60, 61	0	175.45	0.05	-7.16	23.85	4.25	2.13
			69	175.45	0.05	1.30	0.67	2.79	2.13
			138	175.45	0.05	-6.24	-22.52	1.32	2.13
239	Primo Impalcato	61, 62	0	223.95	0.01	-6.13	24.44	1.26	0.95
			69	223.95	0.01	2.74	1.26	0.60	0.95
			138	223.95	0.01	-4.39	-21.92	-0.05	0.95
240	Primo Impalcato	62, 63	0	164.67	0.00	-4.24	21.22	-0.02	0.27
			69	164.67	0.00	2.40	-1.97	-0.21	0.27
			138	164.67	0.00	-6.95	-25.15	-0.39	0.27
241	Primo Impalcato	63, 64	0	164.68	0.00	-6.83	23.19	-0.39	0.00
			69	164.68	0.00	1.17	0.00	-0.39	0.00
			138	164.68	0.00	-6.83	-23.18	-0.39	0.00
242	Primo Impalcato	64, 65	0	164.71	0.00	-6.90	24.88	-0.40	-0.28
			69	164.71	0.00	2.27	1.69	-0.20	-0.28
			138	164.71	0.00	-4.56	-21.49	-0.01	-0.28
243	Primo Impalcato	65, 66	0	225.40	0.00	-4.67	22.20	-0.05	-1.00
			69	225.40	0.00	2.65	-0.98	0.64	-1.00
			138	225.40	0.00	-6.03	-24.16	1.34	-1.00
244	Primo Impalcato	66, 67	0	178.11	-0.06	-6.11	22.30	1.39	-2.24
			69	178.11	-0.06	1.28	-0.88	2.94	-2.24
			138	178.11	-0.06	-7.33	-24.06	4.49	-2.24
245	Primo Impalcato	67, 68	0	178.49	-0.16	-7.59	15.51	4.64	-1.31
			69	178.49	-0.16	-4.88	-7.67	5.54	-1.31
			138	178.49	-0.16	-18.17	-30.85	6.44	-1.31
246	Primo Impalcato	68, 69	0	178.79	-0.13	-19.33	28.63	6.83	10.85
			69	178.79	-0.13	-7.57	5.45	-0.66	10.85
			138	178.79	-0.13	-11.81	-17.74	-8.14	10.85
247	Primo Impalcato	69, 70	0	228.06	0.04	-14.29	54.42	-6.51	56.91
			83	228.06	0.04	19.34	26.49	-53.81	56.91
			166	228.06	0.04	29.75	-1.44	-101.11	56.91
248	Primo Impalcato	1	0	-545.90	-8.47	9.00	-3.77	-26.86	-25.31
			188	-632.75	-8.47	1.92	-3.77	20.72	-25.31
			376	-719.61	-8.47	-5.16	-3.77	68.29	-25.31
249	Primo Impalcato	2	0	-529.80	0.18	-36.94	21.38	-1.09	-0.57
			188	-567.71	0.18	3.25	21.38	-0.03	-0.57
			376	-605.61	0.18	43.43	21.38	1.04	-0.57
250	Primo Impalcato	3	0	-465.81	0.19	-13.13	8.31	-0.32	-0.14
			188	-503.71	0.19	2.50	8.31	-0.06	-0.14
			376	-541.61	0.19	18.13	8.31	0.20	-0.14
251	Primo Impalcato	4	0	-414.38	0.07	-0.97	1.22	0.13	0.09
			188	-452.28	0.07	1.32	1.22	-0.04	0.09
			376	-490.18	0.07	3.62	1.22	-0.21	0.09
252	Primo Impalcato	5	0	-368.92	0.01	1.71	-0.50	0.16	0.11
			188	-406.82	0.01	0.77	-0.50	-0.04	0.11
			376	-444.72	0.01	-0.17	-0.50	-0.24	0.11
253	Primo Impalcato	6	0	-330.90	-0.01	1.24	-0.29	0.11	0.07
			188	-368.80	-0.01	0.69	-0.29	-0.02	0.07
			376	-406.70	-0.01	0.13	-0.29	-0.15	0.07
254	Primo Impalcato	7	0	-321.85	0.00	0.69	-0.03	-0.01	-0.01
			188	-359.75	0.00	0.63	-0.03	0.00	-0.01
			376	-397.65	0.00	0.56	-0.03	0.01	-0.01
255	Primo	8	0	-325.65	0.00	0.75	-0.10	-0.04	-0.02

	Impalcato								
			188	-363.55	0.00	0.56	-0.10	0.00	-0.02
			376	-401.45	0.00	0.36	-0.10	0.04	-0.02
256	Primo Impalcato	9	0	-329.27	0.01	1.28	-0.31	-0.07	-0.04
			188	-367.17	0.01	0.69	-0.31	0.01	-0.04
			376	-405.07	0.01	0.11	-0.31	0.09	-0.04
257	Primo Impalcato	10	0	-351.86	-0.01	1.67	-0.40	-0.20	-0.12
			188	-389.76	-0.01	0.92	-0.40	0.03	-0.12
			376	-427.66	-0.01	0.16	-0.40	0.27	-0.12
258	Primo Impalcato	11	0	-405.12	-0.07	-1.04	1.30	-0.20	-0.13
			188	-443.02	-0.07	1.40	1.30	0.05	-0.13
			376	-480.92	-0.07	3.84	1.30	0.30	-0.13
259	Primo Impalcato	12	0	-465.52	-0.19	-13.42	8.50	0.27	0.11
			188	-503.42	-0.19	2.56	8.50	0.06	0.11
			376	-541.32	-0.19	18.55	8.50	-0.14	0.11
260	Primo Impalcato	13	0	-529.48	-0.17	-37.23	21.55	1.06	0.55
			188	-567.38	-0.17	3.30	21.55	0.02	0.55
			376	-605.28	-0.17	43.82	21.55	-1.02	0.55
261	Primo Impalcato	14	0	-558.43	8.76	10.36	-4.50	32.41	27.49
			188	-645.29	8.76	1.90	-4.50	-19.28	27.49
			376	-732.14	8.76	-6.56	-4.50	-70.97	27.49
262	Primo Impalcato	15	0	-851.28	-4.52	4.46	-2.19	83.27	114.57
			188	-914.45	-4.52	0.35	-2.19	-132.13	114.57
			376	-977.62	-4.52	-3.76	-2.19	-347.53	114.57
263	Primo Impalcato	16	0	-862.84	4.47	5.14	-2.55	-87.02	-115.17
			188	-926.01	4.47	0.35	-2.55	129.50	-115.17
			376	-989.18	4.47	-4.45	-2.55	346.03	-115.17
264	Primo Impalcato	17	0	-976.45	-0.87	2.86	-1.46	274.08	221.55
			188	-1039.62	-0.87	0.11	-1.46	-142.44	221.55
			376	-1102.79	-0.87	-2.64	-1.46	-558.95	221.55
265	Primo Impalcato	18	0	-994.84	0.97	3.65	-1.88	-272.14	-220.39
			188	-1058.01	0.97	0.11	-1.88	142.19	-220.39
			376	-1121.17	0.97	-3.42	-1.88	556.51	-220.39
266	Primo Impalcato	19	0	-1023.47	0.13	0.97	-0.48	285.56	226.53
			188	-1086.64	0.13	0.06	-0.48	-140.32	226.53
			376	-1149.81	0.13	-0.84	-0.48	-566.21	226.53
267	Primo Impalcato	20	0	-1039.33	-0.12	1.80	-0.93	-286.89	-227.09
			188	-1102.50	-0.12	0.06	-0.93	140.04	-227.09
			376	-1165.67	-0.12	-1.69	-0.93	566.96	-227.09
268	Primo Impalcato	21	0	-1072.79	0.13	-0.42	0.28	270.78	217.05
			188	-1135.95	0.13	0.11	0.28	-137.27	217.05
			376	-1199.12	0.13	0.65	0.28	-545.32	217.05
269	Primo Impalcato	22	0	-1096.63	-0.12	0.62	-0.27	-271.49	-217.35
			188	-1159.80	-0.12	0.12	-0.27	137.12	-217.35
			376	-1222.97	-0.12	-0.38	-0.27	545.73	-217.35
270	Primo Impalcato	23	0	-1160.94	0.03	-1.84	1.08	265.16	213.68
			188	-1224.11	0.03	0.18	1.08	-136.57	213.68
			376	-1287.27	0.03	2.20	1.08	-538.29	213.68
271	Primo Impalcato	24	0	-1164.49	0.00	-0.55	0.36	-265.90	-213.79
			188	-1227.66	0.00	0.12	0.36	136.03	-213.79
			376	-1290.83	0.00	0.79	0.36	537.95	-213.79
272	Primo Impalcato	25	0	-1269.47	0.03	-1.31	0.77	265.73	215.92
			188	-1332.64	0.03	0.13	0.77	-140.20	215.92
			376	-1395.81	0.03	1.57	0.77	-546.13	215.92
273	Primo Impalcato	26	0	-1221.06	0.00	0.27	-0.14	-266.83	-215.17

			188	-1284.23	0.00	0.00	-0.14	137.69	-215.17
			376	-1347.40	0.00	-0.27	-0.14	542.21	-215.17
274	Primo Impalcato	27	0	-1153.88	0.03	1.19	-0.71	-266.72	-214.03
			188	-1217.05	0.03	-0.15	-0.71	135.65	-214.03
			376	-1280.21	0.03	-1.49	-0.71	538.02	-214.03
275	Primo Impalcato	28	0	-1237.34	-0.04	0.95	-0.54	265.73	215.27
			188	-1300.50	-0.04	-0.06	-0.54	-138.99	215.27
			376	-1363.67	-0.04	-1.07	-0.54	-543.71	215.27
276	Primo Impalcato	29	0	-1114.50	-0.01	1.11	-0.61	-267.43	-214.24
			188	-1177.67	-0.01	-0.03	-0.61	135.34	-214.24
			376	-1240.84	-0.01	-1.17	-0.61	538.11	-214.24
277	Primo Impalcato	30	0	-1259.76	-0.02	0.84	-0.42	268.88	216.28
			188	-1322.93	-0.02	0.05	-0.42	-137.73	216.28
			376	-1386.10	-0.02	-0.75	-0.42	-544.34	216.28
278	Primo Impalcato	31	0	-1098.27	0.00	0.38	-0.23	-267.51	-214.32
			188	-1161.44	0.00	-0.05	-0.23	135.42	-214.32
			376	-1224.61	0.00	-0.49	-0.23	538.35	-214.32
279	Primo Impalcato	32	0	-1258.82	-0.01	0.06	-0.02	269.29	216.26
			188	-1321.99	-0.01	0.03	-0.02	-137.27	216.26
			376	-1385.16	-0.01	-0.01	-0.02	-543.84	216.26
280	Primo Impalcato	33	0	-1099.33	-0.02	0.32	-0.17	-267.50	-214.27
			188	-1162.49	-0.02	0.00	-0.17	135.33	-214.27
			376	-1225.66	-0.02	-0.33	-0.17	538.16	-214.27
281	Primo Impalcato	34	0	-1268.96	-0.02	-0.16	0.11	269.46	216.39
			188	-1332.13	-0.02	0.05	0.11	-137.35	216.39
			376	-1395.29	-0.02	0.27	0.11	-544.16	216.39
282	Primo Impalcato	35	0	-1102.69	0.00	-0.08	0.02	-267.51	-214.16
			188	-1165.86	0.00	-0.04	0.02	135.11	-214.16
			376	-1229.03	0.00	-0.01	0.02	537.73	-214.16
283	Primo Impalcato	36	0	-1280.59	-0.03	-0.19	0.13	269.77	216.40
			188	-1343.76	-0.03	0.04	0.13	-137.07	216.40
			376	-1406.92	-0.03	0.28	0.13	-543.90	216.40
284	Primo Impalcato	37	0	-1096.34	-0.02	-0.27	0.14	-267.75	-214.09
			188	-1159.50	-0.02	-0.01	0.14	134.75	-214.09
			376	-1222.67	-0.02	0.25	0.14	537.24	-214.09
285	Primo Impalcato	38	0	-1279.05	-0.04	-0.06	0.05	270.71	216.37
			188	-1342.22	-0.04	0.03	0.05	-136.06	216.37
			376	-1405.38	-0.04	0.11	0.05	-542.84	216.37
286	Primo Impalcato	39	0	-1139.96	0.01	-0.40	0.29	-268.13	-214.15
			188	-1203.13	0.01	0.15	0.29	134.47	-214.15
			376	-1266.29	0.01	0.70	0.29	537.07	-214.15
287	Primo Impalcato	40	0	-1260.00	-0.05	0.23	-0.12	272.27	216.02
			188	-1323.17	-0.05	0.00	-0.12	-133.84	216.02
			376	-1386.34	-0.05	-0.24	-0.12	-539.95	216.02
288	Primo Impalcato	41	0	-1260.55	-0.01	-0.95	0.56	-270.07	-215.17
			188	-1323.71	-0.01	0.10	0.56	134.45	-215.17
			376	-1386.88	-0.01	1.14	0.56	538.97	-215.17
289	Primo Impalcato	42	0	-1165.04	0.01	-0.49	0.13	271.22	213.01
			188	-1228.20	0.01	-0.24	0.13	-129.24	213.01
			376	-1291.37	0.01	0.01	0.13	-529.69	213.01
290	Primo Impalcato	43	0	-1132.34	0.03	-1.00	0.52	270.57	213.45
			188	-1195.50	0.03	-0.03	0.52	-130.72	213.45
			376	-1258.67	0.03	0.94	0.52	-532.00	213.45
291	Primo Impalcato	44	0	-1246.87	-0.02	0.04	-0.08	-268.51	-215.27
			188	-1310.03	-0.02	-0.10	-0.08	136.19	-215.27

			376	-1373.20	-0.02	-0.25	-0.08	540.89	-215.27
292	Primo Impalcato	45	0	-1131.96	0.03	-0.47	0.25	268.80	213.25
			188	-1195.13	0.03	-0.01	0.25	-132.10	213.25
			376	-1258.30	0.03	0.46	0.25	-533.01	213.25
293	Primo Impalcato	46	0	-1160.25	0.01	1.21	-0.72	-266.70	-212.89
			188	-1223.42	0.01	-0.15	-0.72	133.54	-212.89
			376	-1286.59	0.01	-1.50	-0.72	533.78	-212.89
294	Primo Impalcato	47	0	-1120.51	0.03	-0.55	0.28	267.61	213.88
			188	-1183.68	0.03	-0.02	0.28	-134.48	213.88
			376	-1246.84	0.03	0.51	0.28	-536.57	213.88
295	Primo Impalcato	48	0	-1124.21	0.00	0.61	-0.35	-267.01	-213.27
			188	-1187.37	0.00	-0.04	-0.35	133.93	-213.27
			376	-1250.54	0.00	-0.69	-0.35	534.87	-213.27
296	Primo Impalcato	49	0	-1105.33	-0.10	-1.43	0.73	271.58	217.16
			188	-1168.50	-0.10	-0.06	0.73	-136.68	217.16
			376	-1231.67	-0.10	1.31	0.73	-544.94	217.16
297	Primo Impalcato	50	0	-1122.88	0.12	-0.51	0.31	-272.06	-216.95
			188	-1186.05	0.12	0.07	0.31	135.80	-216.95
			376	-1249.22	0.12	0.64	0.31	543.66	-216.95
298	Primo Impalcato	51	0	-1050.15	-0.12	-2.39	1.23	285.84	226.54
			188	-1113.32	-0.12	-0.08	1.23	-140.06	226.54
			376	-1176.49	-0.12	2.24	1.23	-565.95	226.54
299	Primo Impalcato	52	0	-1179.34	0.13	-1.99	1.07	-288.92	-227.74
			188	-1242.51	0.13	0.02	1.07	139.24	-227.74
			376	-1305.68	0.13	2.03	1.07	567.40	-227.74
300	Primo Impalcato	53	0	-1001.41	0.88	-3.90	2.01	274.65	221.88
			188	-1064.58	0.88	-0.12	2.01	-142.48	221.88
			376	-1127.75	0.88	3.66	2.01	-559.60	221.88
301	Primo Impalcato	54	0	-1113.62	-0.91	-3.96	1.99	-276.71	-222.56
			188	-1176.79	-0.91	-0.22	1.99	141.70	-222.56
			376	-1239.95	-0.91	3.52	1.99	560.10	-222.56
302	Primo Impalcato	55	0	-855.67	4.53	-5.40	2.67	83.28	114.76
			188	-918.84	4.53	-0.38	2.67	-132.47	114.76
			376	-982.01	4.53	4.65	2.67	-348.21	114.76
303	Primo Impalcato	56	0	-896.63	-4.57	-5.15	2.50	-84.74	-114.28
			188	-959.79	-4.57	-0.45	2.50	130.11	-114.28
			376	-1022.96	-4.57	4.25	2.50	344.96	-114.28
304	Primo Impalcato	57	0	-540.93	8.51	-10.50	4.59	-27.87	-25.80
			188	-627.78	8.51	-1.86	4.59	20.63	-25.80
			376	-714.64	8.51	6.77	4.59	69.13	-25.80
305	Primo Impalcato	58	0	-525.66	-0.17	36.75	-21.07	-1.11	-0.58
			188	-563.56	-0.17	-2.87	-21.07	-0.02	-0.58
			376	-601.46	-0.17	-42.48	-21.07	1.06	-0.58
306	Primo Impalcato	59	0	-461.33	-0.19	13.18	-8.20	-0.31	-0.13
			188	-499.24	-0.19	-2.24	-8.20	-0.06	-0.13
			376	-537.14	-0.19	-17.67	-8.20	0.18	-0.13
307	Primo Impalcato	60	0	-402.83	-0.07	1.09	-1.21	0.16	0.11
			188	-440.74	-0.07	-1.18	-1.21	-0.05	0.11
			376	-478.64	-0.07	-3.44	-1.21	-0.26	0.11
308	Primo Impalcato	61	0	-350.89	-0.01	-1.51	0.42	0.16	0.10
			188	-388.79	-0.01	-0.72	0.42	-0.03	0.10
			376	-426.69	-0.01	0.07	0.42	-0.22	0.10
309	Primo Impalcato	62	0	-333.47	0.01	-1.08	0.31	0.00	0.00
			188	-371.37	0.01	-0.50	0.31	0.00	0.00
			376	-409.27	0.01	0.09	0.31	-0.01	0.00

310	Primo Impalcato	63	0	-334.37	0.00	-0.55	0.14	-0.06	-0.03
			188	-372.27	0.00	-0.28	0.14	0.00	-0.03
			376	-410.17	0.00	-0.01	0.14	0.06	-0.03
311	Primo Impalcato	64	0	-334.46	0.00	-0.55	0.16	-0.01	0.00
			188	-372.36	0.00	-0.26	0.16	0.00	0.00
			376	-410.26	0.00	0.03	0.16	0.01	0.00
312	Primo Impalcato	65	0	-333.64	-0.01	-1.09	0.35	-0.06	-0.03
			188	-371.54	-0.01	-0.44	0.35	0.00	-0.03
			376	-409.44	-0.01	0.21	0.35	0.07	-0.03
313	Primo Impalcato	66	0	-352.02	0.01	-1.53	0.47	-0.21	-0.13
			188	-389.92	0.01	-0.65	0.47	0.03	-0.13
			376	-427.82	0.01	0.23	0.47	0.27	-0.13
314	Primo Impalcato	67	0	-403.93	0.07	1.20	-1.23	-0.21	-0.14
			188	-441.83	0.07	-1.11	-1.23	0.05	-0.14
			376	-479.73	0.07	-3.42	-1.23	0.30	-0.14
315	Primo Impalcato	68	0	-463.36	0.20	13.91	-8.61	0.26	0.10
			188	-501.26	0.20	-2.28	-8.61	0.06	0.10
			376	-539.16	0.20	-18.47	-8.61	-0.13	0.10
316	Primo Impalcato	69	0	-527.62	0.18	38.70	-22.21	1.05	0.55
			188	-565.52	0.18	-3.05	-22.21	0.02	0.55
			376	-603.42	0.18	-44.80	-22.21	-1.00	0.55
317	Primo Impalcato	70	0	-555.44	-8.86	-10.09	4.29	31.35	27.03
			188	-642.29	-8.86	-2.02	4.29	-19.45	27.03
			376	-729.15	-8.86	6.05	4.29	-70.26	27.03
318	Fondazione	1, 71	0	-191.52	-0.16	0.00	2.40	0.34	2.09
			102	-185.83	-0.16	1.23	0.00	-1.79	2.09
			204	-180.15	-0.16	0.00	-2.40	-3.93	2.09
319	Fondazione	1, 92	0	-32.28	-0.01	0.00	2.51	-0.91	-0.31
			103	-26.59	-0.01	1.29	0.00	-0.59	-0.31
			206	-20.91	-0.01	0.00	-2.51	-0.27	-0.31
320	Primo Impalcato	92, 2	0	-186.61	-0.05	0.00	2.51	0.93	1.20
			103	-192.29	-0.05	1.29	0.00	-0.30	1.20
			206	-197.98	-0.05	0.00	-2.51	-1.54	1.20
321	Fondazione	6, 89	0	-108.93	0.00	0.00	2.09	-0.01	0.01
			100	-103.24	0.00	1.04	0.00	-0.02	0.01
			200	-97.56	0.00	0.00	-2.09	-0.02	0.01
322	Primo Impalcato	89, 7	0	-91.80	0.00	0.00	2.09	0.00	0.00
			100	-97.48	0.00	1.04	0.00	-0.01	0.00
			200	-103.17	0.00	0.00	-2.09	-0.01	0.00
323	Fondazione	9, 90	0	-101.84	0.00	0.00	2.09	0.01	0.01
			100	-96.15	0.00	1.04	0.00	0.00	0.01
			200	-90.47	0.00	0.00	-2.09	-0.02	0.01
324	Primo Impalcato	90, 10	0	-106.29	0.00	0.00	2.09	-0.03	-0.01
			100	-111.98	0.00	1.04	0.00	-0.02	-0.01
			200	-117.66	0.00	0.00	-2.09	0.00	-0.01
325	Fondazione	13, 91	0	-199.41	0.05	0.00	2.51	-1.55	-1.23
			103	-193.72	0.05	1.29	0.00	-0.29	-1.23
			206	-188.03	0.05	0.00	-2.51	0.98	-1.23
326	Primo Impalcato	88, 14	0	-193.11	0.16	0.00	2.40	-3.87	-2.04
			102	-198.80	0.16	1.23	0.00	-1.78	-2.04
			204	-204.48	0.16	0.00	-2.40	0.30	-2.04
327	Primo Impalcato	91, 14	0	-20.60	0.02	0.00	2.51	-0.30	0.29
			103	-26.29	0.02	1.29	0.00	-0.60	0.29
			206	-31.97	0.02	0.00	-2.51	-0.90	0.29
328	Primo	71, 15	0	-29.97	-0.23	0.00	2.40	2.74	2.61

	Impalcato								
			102	-35.66	-0.23	1.23	0.00	0.07	2.61
			204	-41.34	-0.23	0.00	-2.40	-2.60	2.61
329	Fondazio ne	16, 88	0	-31.58	0.23	0.00	2.40	-2.60	-2.61
			102	-25.89	0.23	1.23	0.00	0.06	-2.61
			204	-20.21	0.23	0.00	-2.40	2.73	-2.61
330	Fondazio ne	17, 72	0	-212.61	0.10	0.00	2.00	-5.44	-2.09
			100	-206.93	0.10	0.99	0.00	-3.35	-2.09
			199	-201.24	0.10	0.00	-2.00	-1.27	-2.09
331	Primo Impalcato	87, 18	0	-216.74	-0.10	0.00	2.00	-1.29	2.08
			100	-222.42	-0.10	0.99	0.00	-3.36	2.08
			199	-228.11	-0.10	0.00	-2.00	-5.44	2.08
332	Primo Impalcato	72, 19	0	-139.96	-0.12	0.00	2.00	-1.13	2.10
			100	-145.64	-0.12	0.99	0.00	-3.22	2.10
			199	-151.33	-0.12	0.00	-2.00	-5.32	2.10
333	Fondazio ne	20, 87	0	-141.43	0.12	0.00	2.00	-5.32	-2.12
			100	-135.74	0.12	0.99	0.00	-3.21	-2.12
			199	-130.05	0.12	0.00	-2.00	-1.10	-2.12
334	Fondazio ne	21, 73	0	-179.55	0.11	0.00	2.00	-5.02	-1.91
			100	-173.87	0.11	0.99	0.00	-3.11	-1.91
			199	-168.18	0.11	0.00	-2.00	-1.21	-1.91
335	Primo Impalcato	86, 22	0	-188.93	-0.11	0.00	2.00	-1.21	1.92
			100	-194.62	-0.11	0.99	0.00	-3.12	1.92
			199	-200.30	-0.11	0.00	-2.00	-5.03	1.92
336	Primo Impalcato	73, 23	0	-210.46	-0.10	0.00	2.00	-1.29	1.85
			100	-216.14	-0.10	0.99	0.00	-3.13	1.85
			199	-221.83	-0.10	0.00	-2.00	-4.97	1.85
337	Fondazio ne	24, 86	0	-205.78	0.10	0.00	2.00	-4.95	-1.84
			100	-200.10	0.10	0.99	0.00	-3.12	-1.84
			199	-194.41	0.10	0.00	-2.00	-1.29	-1.84
338	Fondazio ne	25, 74	0	-208.14	0.13	0.00	2.57	-4.72	-1.72
			103	-202.46	0.13	1.33	0.00	-2.95	-1.72
			206	-196.77	0.13	0.00	-2.57	-1.17	-1.72
339	Primo Impalcato	85, 26	0	-217.76	-0.10	0.00	2.00	-1.24	1.91
			100	-223.45	-0.10	0.99	0.00	-3.14	1.91
			199	-229.13	-0.10	0.00	-2.00	-5.04	1.91
340	Fondazio ne	27, 85	0	-195.25	0.11	0.00	2.00	-4.94	-1.86
			100	-189.56	0.11	0.99	0.00	-3.09	-1.86
			199	-183.88	0.11	0.00	-2.00	-1.24	-1.86
341	Primo Impalcato	74, 28	0	-196.90	-0.13	0.00	2.57	-1.17	1.69
			103	-202.59	-0.13	1.33	0.00	-2.92	1.69
			206	-208.27	-0.13	0.00	-2.57	-4.67	1.69
342	Primo Impalcato	84, 29	0	-200.75	-0.10	0.00	2.00	-1.23	1.88
			100	-206.43	-0.10	0.99	0.00	-3.10	1.88
			199	-212.12	-0.10	0.00	-2.00	-4.97	1.88
343	Fondazio ne	31, 84	0	-186.37	0.10	0.00	2.00	-4.98	-1.88
			100	-180.68	0.10	0.99	0.00	-3.11	-1.88
			199	-175.00	0.10	0.00	-2.00	-1.23	-1.88
344	Primo Impalcato	83, 33	0	-190.35	-0.10	0.00	2.00	-1.22	1.88
			100	-196.03	-0.10	0.99	0.00	-3.10	1.88
			199	-201.72	-0.10	0.00	-2.00	-4.97	1.88
345	Fondazio ne	35, 83	0	-194.85	0.10	0.00	2.00	-4.97	-1.88
			100	-189.17	0.10	0.99	0.00	-3.10	-1.88
			199	-183.48	0.10	0.00	-2.00	-1.23	-1.88
346	Primo Impalcato	82, 37	0	-183.37	-0.10	0.00	2.00	-1.22	1.88

			100	-189.05	-0.10	0.99	0.00	-3.09	1.88
			199	-194.74	-0.10	0.00	-2.00	-4.97	1.88
347	Fondazio ne	39, 82	0	-206.94	0.10	0.00	2.00	-4.96	-1.88
			100	-201.25	0.10	0.99	0.00	-3.09	-1.88
			199	-195.57	0.10	0.00	-2.00	-1.22	-1.88
348	Primo Impalcato	78, 43	0	-181.25	0.10	0.00	2.00	1.18	-1.87
			100	-186.94	0.10	0.99	0.00	3.04	-1.87
			199	-192.62	0.10	0.00	-2.00	4.90	-1.87
349	Primo Impalcato	81, 44	0	-220.70	-0.10	0.00	2.00	-1.21	1.92
			100	-226.38	-0.10	0.99	0.00	-3.12	1.92
			199	-232.07	-0.10	0.00	-2.00	-5.03	1.92
350	Fondazio ne	45, 78	0	-214.58	-0.10	0.00	2.00	4.96	1.88
			100	-208.89	-0.10	0.99	0.00	3.08	1.88
			199	-203.21	-0.10	0.00	-2.00	1.20	1.88
351	Fondazio ne	46, 81	0	-196.75	0.10	0.00	2.00	-4.90	-1.84
			100	-191.07	0.10	0.99	0.00	-3.07	-1.84
			199	-185.38	0.10	0.00	-2.00	-1.24	-1.84
352	Primo Impalcato	77, 47	0	-174.35	0.10	0.00	2.00	1.27	-1.83
			100	-180.03	0.10	0.99	0.00	3.09	-1.83
			199	-185.72	0.10	0.00	-2.00	4.92	-1.83
353	Primo Impalcato	80, 48	0	-189.64	-0.10	0.00	2.00	-1.27	1.83
			100	-195.32	-0.10	0.99	0.00	-3.10	1.83
			199	-201.01	-0.10	0.00	-2.00	-4.92	1.83
354	Fondazio ne	49, 77	0	-215.13	-0.10	0.00	2.00	5.04	1.92
			100	-209.45	-0.10	0.99	0.00	3.13	1.92
			199	-203.76	-0.10	0.00	-2.00	1.21	1.92
355	Fondazio ne	50, 80	0	-202.08	0.11	0.00	2.00	-5.02	-1.92
			100	-196.40	0.11	0.99	0.00	-3.10	-1.92
			199	-190.71	0.11	0.00	-2.00	-1.19	-1.92
356	Primo Impalcato	76, 51	0	-125.28	0.12	0.00	2.00	1.13	-2.10
			100	-130.96	0.12	0.99	0.00	3.22	-2.10
			199	-136.65	0.12	0.00	-2.00	5.30	-2.10
357	Fondazio ne	53, 76	0	-235.90	-0.10	0.00	2.00	5.45	2.09
			100	-230.22	-0.10	0.99	0.00	3.36	2.09
			199	-224.53	-0.10	0.00	-2.00	1.27	2.09
358	Primo Impalcato	75, 55	0	-16.05	0.23	0.00	2.40	-2.75	-2.62
			102	-21.73	0.23	1.23	0.00	-0.07	-2.62
			204	-27.42	0.23	0.00	-2.40	2.60	-2.62
359	Fondazio ne	56, 79	0	-37.15	-0.22	0.00	2.40	2.58	2.58
			102	-31.47	-0.22	1.23	0.00	-0.06	2.58
			204	-25.78	-0.22	0.00	-2.40	-2.69	2.58
360	Fondazio ne	57, 75	0	-205.72	0.16	0.00	2.40	-0.34	-2.09
			102	-200.03	0.16	1.23	0.00	1.80	-2.09
			204	-194.35	0.16	0.00	-2.40	3.94	-2.09
361	Fondazio ne	57, 93	0	-30.21	0.02	0.00	2.51	0.86	0.28
			103	-24.53	0.02	1.29	0.00	0.57	0.28
			206	-18.84	0.02	0.00	-2.51	0.29	0.28
362	Primo Impalcato	93, 58	0	-187.07	0.05	0.00	2.51	-0.95	-1.20
			103	-192.75	0.05	1.29	0.00	0.28	-1.20
			206	-198.44	0.05	0.00	-2.51	1.51	-1.20
363	Fondazio ne	61, 95	0	-115.20	0.00	0.00	2.09	0.00	-0.01
			100	-109.51	0.00	1.04	0.00	0.01	-0.01
			200	-103.83	0.00	0.00	-2.09	0.02	-0.01
364	Primo Impalcato	95, 62	0	-93.82	0.00	0.00	2.09	0.01	0.01
			100	-99.50	0.00	1.04	0.00	0.00	0.01

			200	-105.19	0.00	0.00	-2.09	-0.02	0.01
365	Primo Impalcato	96, 65	0	-91.31	0.00	0.00	2.09	-0.01	-0.02
			100	-96.99	0.00	1.04	0.00	0.01	-0.02
			200	-102.68	0.00	0.00	-2.09	0.02	-0.02
366	Fondazione	66, 96	0	-118.02	0.00	0.00	2.09	0.00	0.01
			100	-112.33	0.00	1.04	0.00	-0.01	0.01
			200	-106.65	0.00	0.00	-2.09	-0.02	0.01
367	Fondazione	69, 94	0	-198.32	-0.05	0.00	2.51	1.59	1.25
			103	-192.64	-0.05	1.29	0.00	0.30	1.25
			206	-186.95	-0.05	0.00	-2.51	-0.98	1.25
368	Primo Impalcato	79, 70	0	-192.25	-0.15	0.00	2.40	3.85	2.03
			102	-197.93	-0.15	1.23	0.00	1.77	2.03
			204	-203.62	-0.15	0.00	-2.40	-0.30	2.03
369	Primo Impalcato	94, 70	0	-20.89	-0.01	0.00	2.51	0.29	-0.31
			103	-26.57	-0.01	1.29	0.00	0.61	-0.31
			206	-32.26	-0.01	0.00	-2.51	0.94	-0.31
370	Primo Impalcato	1, 71	0	-16.57	-0.08	0.00	2.40	0.66	-1.09
			102	-22.25	-0.08	1.23	0.00	1.77	-1.09
			204	-27.94	-0.08	0.00	-2.40	2.89	-1.09
371	Primo Impalcato	1, 92	0	-173.02	-0.28	0.00	2.51	2.52	0.82
			103	-178.70	-0.28	1.29	0.00	1.68	0.82
			206	-184.39	-0.28	0.00	-2.51	0.83	0.82
372	Primo Impalcato	92, 2	0	-18.68	0.07	0.00	2.51	-0.04	-0.69
			103	-13.00	0.07	1.29	0.00	0.67	-0.69
			206	-7.31	0.07	0.00	-2.51	1.37	-0.69
373	Primo Impalcato	6, 89	0	-78.90	0.00	0.00	2.09	-0.02	-0.01
			100	-84.58	0.00	1.04	0.00	-0.01	-0.01
			200	-90.27	0.00	0.00	-2.09	0.00	-0.01
374	Primo Impalcato	89, 7	0	-96.02	0.00	0.00	2.09	-0.03	-0.01
			100	-90.34	0.00	1.04	0.00	-0.02	-0.01
			200	-84.65	0.00	0.00	-2.09	-0.01	-0.01
375	Primo Impalcato	9, 90	0	-93.39	0.00	0.00	2.09	-0.03	0.00
			100	-99.07	0.00	1.04	0.00	-0.03	0.00
			200	-104.76	0.00	0.00	-2.09	-0.03	0.00
376	Primo Impalcato	90, 10	0	-88.93	0.00	0.00	2.09	-0.01	0.03
			100	-83.25	0.00	1.04	0.00	-0.04	0.03
			200	-77.56	0.00	0.00	-2.09	-0.07	0.03
377	Primo Impalcato	13, 91	0	-7.01	-0.07	0.00	2.51	1.39	0.71
			103	-12.70	-0.07	1.29	0.00	0.67	0.71
			206	-18.38	-0.07	0.00	-2.51	-0.06	0.71
378	Primo Impalcato	88, 14	0	-18.18	0.10	0.00	2.40	2.86	1.02
			102	-12.49	0.10	1.23	0.00	1.81	1.02
			204	-6.80	0.10	0.00	-2.40	0.76	1.02
379	Primo Impalcato	91, 14	0	-185.81	0.28	0.00	2.51	0.88	-0.81
			103	-180.13	0.28	1.29	0.00	1.71	-0.81
			206	-174.44	0.28	0.00	-2.51	2.55	-0.81
380	Primo Impalcato	71, 15	0	-178.12	-0.15	0.00	2.40	-4.13	-1.62
			102	-172.43	-0.15	1.23	0.00	-2.48	-1.62
			204	-166.75	-0.15	0.00	-2.40	-0.83	-1.62
381	Primo Impalcato	16, 88	0	-179.71	0.15	0.00	2.40	-0.79	1.59
			102	-185.39	0.15	1.23	0.00	-2.42	1.59
			204	-191.08	0.15	0.00	-2.40	-4.05	1.59
382	Primo Impalcato	17, 72	0	-127.18	-0.05	0.00	2.00	3.14	2.18
			100	-132.87	-0.05	0.99	0.00	0.96	2.18
			199	-138.55	-0.05	0.00	-2.00	-1.21	2.18

383	Primo Impalcato	87, 18	0	-128.65	0.06	0.00	2.00	-1.18	-2.18
			100	-122.97	0.06	0.99	0.00	1.00	-2.18
			199	-117.28	0.06	0.00	-2.00	3.17	-2.18
384	Primo Impalcato	72, 19	0	-199.84	0.00	0.00	2.00	-1.25	-2.01
			100	-194.16	0.00	0.99	0.00	0.75	-2.01
			199	-188.47	0.00	0.00	-2.00	2.75	-2.01
385	Primo Impalcato	20, 87	0	-203.96	0.00	0.00	2.00	2.76	2.02
			100	-209.65	0.00	0.99	0.00	0.75	2.02
			199	-215.33	0.00	0.00	-2.00	-1.26	2.02
386	Primo Impalcato	21, 73	0	-197.69	0.03	0.00	2.00	2.44	1.89
			100	-203.37	0.03	0.99	0.00	0.55	1.89
			199	-209.06	0.03	0.00	-2.00	-1.33	1.89
387	Primo Impalcato	86, 22	0	-193.01	-0.03	0.00	2.00	-1.33	-1.89
			100	-187.33	-0.03	0.99	0.00	0.56	-1.89
			199	-181.64	-0.03	0.00	-2.00	2.45	-1.89
388	Primo Impalcato	73, 23	0	-166.78	-0.02	0.00	2.00	-1.26	-1.86
			100	-161.10	-0.02	0.99	0.00	0.60	-1.86
			199	-155.41	-0.02	0.00	-2.00	2.46	-1.86
389	Primo Impalcato	24, 86	0	-176.16	0.02	0.00	2.00	2.46	1.87
			100	-181.84	0.02	0.99	0.00	0.60	1.87
			199	-187.53	0.02	0.00	-2.00	-1.26	1.87
390	Primo Impalcato	25, 74	0	-183.21	0.03	0.00	2.57	2.27	1.70
			103	-188.89	0.03	1.33	0.00	0.51	1.70
			206	-194.58	0.03	0.00	-2.57	-1.24	1.70
391	Primo Impalcato	85, 26	0	-182.48	-0.02	0.00	2.00	-1.28	-1.87
			100	-176.79	-0.02	0.99	0.00	0.58	-1.87
			199	-171.11	-0.02	0.00	-2.00	2.45	-1.87
392	Primo Impalcato	27, 85	0	-204.99	0.02	0.00	2.00	2.48	1.89
			100	-210.68	0.02	0.99	0.00	0.60	1.89
			199	-216.36	0.02	0.00	-2.00	-1.29	1.89
393	Primo Impalcato	74, 28	0	-194.45	-0.03	0.00	2.57	-1.24	-1.71
			103	-188.76	-0.03	1.33	0.00	0.52	-1.71
			206	-183.08	-0.03	0.00	-2.57	2.29	-1.71
394	Primo Impalcato	84, 29	0	-173.60	-0.02	0.00	2.00	-1.28	-1.88
			100	-167.91	-0.02	0.99	0.00	0.60	-1.88
			199	-162.23	-0.02	0.00	-2.00	2.47	-1.88
395	Primo Impalcato	31, 84	0	-187.98	0.02	0.00	2.00	2.48	1.88
			100	-193.66	0.02	0.99	0.00	0.60	1.88
			199	-199.35	0.02	0.00	-2.00	-1.27	1.88
396	Primo Impalcato	83, 33	0	-182.08	-0.02	0.00	2.00	-1.28	-1.88
			100	-176.40	-0.02	0.99	0.00	0.59	-1.88
			199	-170.71	-0.02	0.00	-2.00	2.47	-1.88
397	Primo Impalcato	35, 83	0	-177.58	0.02	0.00	2.00	2.48	1.88
			100	-183.26	0.02	0.99	0.00	0.60	1.88
			199	-188.95	0.02	0.00	-2.00	-1.27	1.88
398	Primo Impalcato	82, 37	0	-194.16	-0.02	0.00	2.00	-1.27	-1.87
			100	-188.48	-0.02	0.99	0.00	0.60	-1.87
			199	-182.79	-0.02	0.00	-2.00	2.47	-1.87
399	Primo Impalcato	39, 82	0	-170.59	0.02	0.00	2.00	2.48	1.88
			100	-176.28	0.02	0.99	0.00	0.61	1.88
			199	-181.96	0.02	0.00	-2.00	-1.27	1.88
400	Primo Impalcato	78, 43	0	-201.81	0.02	0.00	2.00	1.25	1.89
			100	-196.12	0.02	0.99	0.00	-0.63	1.89
			199	-190.44	0.02	0.00	-2.00	-2.51	1.89
401	Primo	81, 44	0	-183.98	-0.02	0.00	2.00	-1.28	-1.87

	Impalcato								
			100	-178.30	-0.02	0.99	0.00	0.59	-1.87
			199	-172.61	-0.02	0.00	-2.00	2.45	-1.87
402	Primo Impalcato	45, 78	0	-168.48	-0.02	0.00	2.00	-2.49	-1.86
			100	-174.17	-0.02	0.99	0.00	-0.63	-1.86
			199	-179.85	-0.02	0.00	-2.00	1.22	-1.86
403	Primo Impalcato	46, 81	0	-207.93	0.02	0.00	2.00	2.48	1.88
			100	-213.61	0.02	0.99	0.00	0.61	1.88
			199	-219.30	0.02	0.00	-2.00	-1.26	1.88
404	Primo Impalcato	77, 47	0	-202.36	0.02	0.00	2.00	1.27	1.87
			100	-196.67	0.02	0.99	0.00	-0.60	1.87
			199	-190.99	0.02	0.00	-2.00	-2.47	1.87
405	Primo Impalcato	80, 48	0	-189.31	-0.02	0.00	2.00	-1.24	-1.87
			100	-183.63	-0.02	0.99	0.00	0.61	-1.87
			199	-177.94	-0.02	0.00	-2.00	2.47	-1.87
406	Primo Impalcato	49, 77	0	-161.58	-0.03	0.00	2.00	-2.44	-1.88
			100	-167.26	-0.03	0.99	0.00	-0.57	-1.88
			199	-172.95	-0.03	0.00	-2.00	1.31	-1.88
407	Primo Impalcato	50, 80	0	-176.87	0.03	0.00	2.00	2.44	1.88
			100	-182.55	0.03	0.99	0.00	0.57	1.88
			199	-188.24	0.03	0.00	-2.00	-1.31	1.88
408	Primo Impalcato	76, 51	0	-223.13	0.00	0.00	2.00	1.26	2.01
			100	-217.44	0.00	0.99	0.00	-0.74	2.01
			199	-211.76	0.00	0.00	-2.00	-2.74	2.01
409	Primo Impalcato	53, 76	0	-112.50	0.05	0.00	2.00	-3.14	-2.18
			100	-118.19	0.05	0.99	0.00	-0.97	-2.18
			199	-123.87	0.05	0.00	-2.00	1.21	-2.18
410	Primo Impalcato	75, 55	0	-192.32	0.15	0.00	2.40	4.14	1.62
			102	-186.63	0.15	1.23	0.00	2.49	1.62
			204	-180.94	0.15	0.00	-2.40	0.83	1.62
411	Primo Impalcato	56, 79	0	-178.84	-0.16	0.00	2.40	0.96	-1.49
			102	-184.53	-0.16	1.23	0.00	2.48	-1.49
			204	-190.21	-0.16	0.00	-2.40	4.01	-1.49
412	Primo Impalcato	57, 75	0	-2.64	0.08	0.00	2.40	-0.66	1.09
			102	-8.33	0.08	1.23	0.00	-1.78	1.09
			204	-14.01	0.08	0.00	-2.40	-2.90	1.09
413	Primo Impalcato	57, 93	0	-173.47	0.28	0.00	2.51	-2.46	-0.78
			103	-179.16	0.28	1.29	0.00	-1.66	-0.78
			206	-184.84	0.28	0.00	-2.51	-0.86	-0.78
414	Primo Impalcato	93, 58	0	-16.62	-0.07	0.00	2.51	0.05	0.70
			103	-10.93	-0.07	1.29	0.00	-0.66	0.70
			206	-5.25	-0.07	0.00	-2.51	-1.38	0.70
415	Primo Impalcato	61, 95	0	-80.92	0.00	0.00	2.09	0.06	0.03
			100	-86.60	0.00	1.04	0.00	0.04	0.03
			200	-92.29	0.00	0.00	-2.09	0.01	0.03
416	Primo Impalcato	95, 62	0	-102.30	0.00	0.00	2.09	0.03	0.00
			100	-96.61	0.00	1.04	0.00	0.03	0.00
			200	-90.93	0.00	0.00	-2.09	0.03	0.00
417	Primo Impalcato	96, 65	0	-105.12	0.00	0.00	2.09	-0.03	0.00
			100	-99.43	0.00	1.04	0.00	-0.03	0.00
			200	-93.74	0.00	0.00	-2.09	-0.03	0.00
418	Primo Impalcato	66, 96	0	-78.41	0.00	0.00	2.09	-0.06	-0.03
			100	-84.09	0.00	1.04	0.00	-0.03	-0.03
			200	-89.78	0.00	0.00	-2.09	-0.01	-0.03
419	Primo Impalcato	69, 94	0	-7.30	0.07	0.00	2.51	-1.45	-0.73

			103	-12.98	0.07	1.29	0.00	-0.70	-0.73
			206	-18.67	0.07	0.00	-2.51	0.05	-0.73
420	Primo Impalcato	79, 70	0	-23.75	-0.10	0.00	2.40	-2.80	-0.94
			102	-18.07	-0.10	1.23	0.00	-1.83	-0.94
			204	-12.38	-0.10	0.00	-2.40	-0.87	-0.94
421	Primo Impalcato	94, 70	0	-184.73	-0.29	0.00	2.51	-0.88	0.84
			103	-179.04	-0.29	1.29	0.00	-1.74	0.84
			206	-173.36	-0.29	0.00	-2.51	-2.60	0.84
422	Copertura	1, 2	0	28.34	-13.02	209.59	48.66	-17.15	-12.94
			83	28.34	-13.02	190.70	-94.13	-6.39	-12.94
			166	28.34	-13.02	53.11	-236.91	4.37	-12.94
423	Copertura	15, 1	0	-20.16	-183.32	550.60	-248.34	10.88	22.54
			80	-20.16	-183.32	303.53	-373.22	-7.04	22.54
			159	-20.16	-183.32	-42.82	-498.10	-24.96	22.54
424	Copertura	2, 3	0	27.70	3.18	53.51	-1.95	4.04	-1.62
			69	27.70	3.18	11.27	-120.48	5.15	-1.62
			138	27.70	3.18	-112.75	-239.01	6.27	-1.62
425	Copertura	3, 4	0	28.10	4.69	-111.87	79.90	6.09	1.70
			69	28.10	4.69	-97.63	-38.63	4.91	1.70
			138	28.10	4.69	-165.18	-157.16	3.74	1.70
426	Copertura	4, 5	0	28.34	2.18	-164.60	128.29	3.67	1.37
			69	28.34	2.18	-116.97	9.76	2.72	1.37
			138	28.34	2.18	-151.13	-108.77	1.77	1.37
427	Copertura	5, 6	0	28.50	0.51	-150.74	126.13	1.76	0.62
			69	28.50	0.51	-104.60	7.61	1.33	0.62
			138	28.50	0.51	-140.24	-110.92	0.91	0.62
428	Copertura	6, 7	0	47.54	0.00	-140.01	143.76	0.91	0.21
			69	47.54	0.00	-81.70	25.24	0.76	0.21
			138	47.54	0.00	-105.18	-93.29	0.62	0.21
429	Copertura	7, 8	0	33.07	0.00	-105.10	132.26	0.62	0.05
			69	33.07	0.00	-54.73	13.73	0.58	0.05
			138	33.07	0.00	-86.15	-104.80	0.54	0.05
430	Copertura	8, 9	0	33.06	-0.01	-86.18	83.10	0.54	-0.12
			69	33.06	-0.01	-69.73	-35.43	0.62	-0.12
			138	33.06	-0.01	-135.07	-153.96	0.71	-0.12
431	Copertura	9, 10	0	47.43	-0.52	-135.23	79.10	0.70	-0.52
			69	47.43	-0.52	-121.55	-39.43	1.06	-0.52
			138	47.43	-0.52	-189.64	-157.96	1.42	-0.52
432	Copertura	10, 11	0	25.94	-2.23	-189.98	125.58	1.45	-1.30
			69	25.94	-2.23	-144.22	7.05	2.34	-1.30
			138	25.94	-2.23	-180.25	-111.47	3.24	-1.30
433	Copertura	11, 12	0	25.71	-4.74	-180.80	165.13	3.31	-1.61
			69	25.71	-4.74	-107.75	46.60	4.42	-1.61
			138	25.71	-4.74	-116.49	-71.92	5.54	-1.61
434	Copertura	12, 13	0	25.32	-3.10	-117.35	245.38	5.72	1.80
			69	25.32	-3.10	11.07	126.85	4.48	1.80
			138	25.32	-3.10	57.70	8.32	3.23	1.80
435	Copertura	13, 14	0	25.81	13.07	57.32	246.65	3.56	13.39
			83	25.81	13.07	203.00	103.86	-7.58	13.39
			166	25.81	13.07	229.98	-38.93	-18.71	13.39
436	Copertura	16, 14	0	-24.72	182.25	534.05	-239.60	-30.29	-45.99
			80	-24.72	182.25	293.92	-364.48	6.27	-45.99
			159	-24.72	182.25	-45.48	-489.36	42.84	-45.99
437	Copertura	15, 17	0	-22.68	-28.20	544.91	175.20	-5.92	-7.20
			66	-22.68	-28.20	626.33	71.53	-1.17	-7.20
			132	-22.68	-28.20	639.33	-32.14	3.58	-7.20
438	Copertura	16, 18	0	-28.23	29.43	529.99	174.19	12.24	9.22
			66	-28.23	29.43	610.74	70.52	6.16	9.22
			132	-28.23	29.43	623.07	-33.16	0.08	9.22
439	Copertura	17, 19	0	-24.37	-3.29	635.47	9.95	4.57	2.74
			66	-24.37	-3.29	607.83	-93.72	2.76	2.74
			132	-24.37	-3.29	511.77	-197.39	0.95	2.74
440	Copertura	18, 20	0	-31.82	3.45	618.15	10.08	-0.76	-0.13
			66	-31.82	3.45	590.59	-93.59	-0.67	-0.13
			132	-31.82	3.45	494.61	-197.27	-0.59	-0.13
441	Copertura	19, 21	0	-25.25	1.17	509.73	-60.35	1.11	1.47
			66	-25.25	1.17	435.69	-164.02	0.14	1.47
			132	-25.25	1.17	293.23	-267.69	-0.83	1.47
442	Copertura	20, 22	0	-33.15	-1.26	492.62	-45.78	-0.45	-0.11
			66	-33.15	-1.26	428.20	-149.45	-0.37	-0.11

			132	-33.15	-1.26	295.35	-253.13	-0.30	-0.11
443	Copertura	21, 23	0	-25.52	0.64	292.61	-71.64	-0.68	0.31
			66	-25.52	0.64	211.12	-175.31	-0.88	0.31
			132	-25.52	0.64	61.20	-278.98	-1.08	0.31
444	Copertura	22, 24	0	-33.30	-0.69	295.12	-52.69	0.09	0.71
			66	-33.30	-0.69	226.14	-156.36	-0.38	0.71
			132	-33.30	-0.69	88.73	-260.03	-0.85	0.71
445	Copertura	23, 25	0	-25.40	0.15	61.39	-21.14	-0.90	0.23
			66	-25.40	0.15	13.22	-124.82	-1.05	0.23
			132	-25.40	0.15	-103.37	-228.49	-1.21	0.23
446	Copertura	24, 26	0	-32.27	-0.11	89.84	-6.83	-0.58	0.64
			66	-32.27	-0.11	51.12	-110.50	-1.01	0.64
			132	-32.27	-0.11	-56.02	-214.18	-1.43	0.64
447	Copertura	25, 28	0	-25.35	-0.19	-103.30	122.96	-1.12	0.02
			85	-25.35	-0.19	-55.52	-10.56	-1.14	0.02
			170	-25.35	-0.19	-121.24	-144.07	-1.16	0.02
448	Copertura	26, 27	0	-27.86	0.25	-51.20	80.13	-1.31	0.20
			66	-27.86	0.25	-32.52	-23.54	-1.44	0.20
			132	-27.86	0.25	-82.27	-127.21	-1.58	0.20
449	Copertura	27, 29	0	-32.00	0.35	-75.10	132.58	-1.57	-0.39
			66	-32.00	0.35	-21.81	28.91	-1.32	-0.39
			132	-32.00	0.35	-36.94	-74.77	-1.06	-0.39
450	Copertura	28, 30	0	-25.82	-0.34	-133.47	179.01	-1.10	-0.03
			73	-25.82	-0.34	-44.64	64.34	-1.07	-0.03
			146	-25.82	-0.34	-39.53	-50.33	-1.05	-0.03
451	Copertura	29, 31	0	-32.96	0.17	-22.27	126.00	-1.08	-0.23
			66	-32.96	0.17	26.67	22.32	-0.93	-0.23
			132	-32.96	0.17	7.19	-81.35	-0.78	-0.23
452	Copertura	30, 32	0	-26.36	-0.11	-56.16	159.46	-1.09	-0.30
			69	-26.36	-0.11	16.22	51.86	-0.88	-0.30
			137	-26.36	-0.11	14.89	-55.74	-0.68	-0.30
453	Copertura	31, 33	0	-34.76	0.13	22.42	105.78	-0.89	-0.36
			66	-34.76	0.13	58.02	2.11	-0.65	-0.36
			132	-34.76	0.13	25.20	-101.57	-0.41	-0.36
454	Copertura	32, 34	0	-26.74	-0.05	-2.98	134.94	-0.82	-0.33
			69	-26.74	-0.05	52.73	26.56	-0.59	-0.33
			138	-26.74	-0.05	33.67	-81.83	-0.37	-0.33
455	Copertura	33, 35	0	-35.76	0.18	43.35	86.38	-0.56	-0.41
			66	-35.76	0.18	66.14	-17.30	-0.29	-0.41
			132	-35.76	0.18	20.51	-120.97	-0.01	-0.41
456	Copertura	34, 36	0	-27.03	-0.07	14.16	122.34	-0.56	-0.41
			69	-27.03	-0.07	61.18	13.95	-0.27	-0.41
			138	-27.03	-0.07	33.41	-94.43	0.01	-0.41
457	Copertura	35, 37	0	-37.29	0.20	39.73	65.40	-0.19	-0.70
			66	-37.29	0.20	48.68	-38.27	0.27	-0.70
			132	-37.29	0.20	-10.79	-141.95	0.73	-0.70
458	Copertura	36, 38	0	-27.25	-0.15	12.25	121.26	-0.19	-0.57
			69	-27.25	-0.15	58.53	12.87	0.21	-0.57
			138	-27.25	-0.15	30.02	-95.51	0.61	-0.57
459	Copertura	37, 39	0	-39.03	0.24	10.36	58.85	0.59	-0.65
			66	-39.03	0.24	14.98	-44.82	1.02	-0.65
			132	-39.03	0.24	-48.81	-148.50	1.44	-0.65
460	Copertura	38, 40	0	-27.43	-0.24	7.18	117.97	0.46	-0.63
			69	-27.43	-0.24	51.14	10.37	0.89	-0.63
			137	-27.43	-0.24	21.39	-97.23	1.33	-0.63
461	Copertura	39, 41	0	-40.38	0.01	-26.36	57.73	1.43	-0.23
			66	-40.38	0.01	-22.47	-45.94	1.58	-0.23
			132	-40.38	0.01	-87.01	-149.62	1.73	-0.23
462	Copertura	40, 42	0	-27.61	0.00	-2.87	87.59	1.29	-0.58
			69	-27.61	0.00	20.18	-20.79	1.69	-0.58
			138	-27.61	0.00	-31.56	-129.18	2.09	-0.58
463	Copertura	41, 44	0	-52.47	-0.72	-72.78	66.76	1.84	0.58
			66	-52.47	-0.72	-62.94	-36.92	1.46	0.58
			132	-52.47	-0.72	-121.51	-140.59	1.08	0.58
464	Copertura	42, 43	0	-27.56	1.73	-57.29	44.40	2.18	-0.38
			23	-27.56	1.73	-51.23	8.27	2.27	-0.38
			46	-27.56	1.73	-53.49	-27.86	2.36	-0.38
465	Copertura	43, 45	0	-27.38	0.29	-53.15	172.59	2.37	1.01
			66	-27.38	0.29	26.54	68.91	1.71	1.01
			132	-27.38	0.29	37.81	-34.76	1.04	1.01
466	Copertura	44, 46	0	-41.57	-0.22	-111.01	161.78	1.26	0.17
			66	-41.57	-0.22	-38.44	58.11	1.15	0.17

			132	-41.57	-0.22	-34.30	-45.56	1.04	0.17
467	Copertura	45, 47	0	-27.32	0.07	37.99	197.18	1.20	1.01
			66	-27.32	0.07	133.92	93.51	0.54	1.01
			132	-27.32	0.07	161.42	-10.16	-0.13	1.01
468	Copertura	46, 48	0	-41.92	-0.02	-34.15	238.55	1.22	0.84
			66	-41.92	-0.02	89.08	134.88	0.67	0.84
			132	-41.92	-0.02	143.89	31.21	0.11	0.84
469	Copertura	47, 49	0	-27.10	-0.49	161.99	222.07	0.09	0.91
			66	-27.10	-0.49	274.34	118.40	-0.51	0.91
			132	-27.10	-0.49	318.28	14.72	-1.11	0.91
470	Copertura	48, 50	0	-40.13	0.48	145.59	260.58	0.37	0.54
			66	-40.13	0.48	283.36	156.90	0.01	0.54
			132	-40.13	0.48	352.70	53.23	-0.35	0.54
471	Copertura	49, 51	0	-26.49	-1.14	319.75	220.85	-0.79	-0.55
			66	-26.49	-1.14	431.30	117.17	-0.43	-0.55
			132	-26.49	-1.14	474.42	13.50	-0.07	-0.55
472	Copertura	50, 52	0	-38.85	1.09	354.54	256.17	-0.33	0.82
			66	-38.85	1.09	489.40	152.49	-0.87	0.82
			132	-38.85	1.09	555.83	48.82	-1.41	0.82
473	Copertura	51, 53	0	-25.30	3.21	477.24	187.21	0.21	-2.20
			66	-25.30	3.21	566.59	83.54	1.66	-2.20
			132	-25.30	3.21	587.52	-20.13	3.11	-2.20
474	Copertura	52, 54	0	-35.57	-3.42	560.25	166.30	-1.41	1.29
			66	-35.57	-3.42	635.79	62.63	-2.26	1.29
			132	-35.57	-3.42	642.91	-41.04	-3.12	1.29
475	Copertura	53, 55	0	-23.38	27.87	592.00	40.72	2.37	8.92
			66	-23.38	27.87	584.66	-62.95	-3.52	8.92
			132	-23.38	27.87	508.90	-166.63	-9.40	8.92
476	Copertura	54, 56	0	-31.04	-28.38	649.04	12.12	-0.08	-9.02
			66	-31.04	-28.38	622.83	-91.55	5.87	-9.02
			132	-31.04	-28.38	528.19	-195.23	11.82	-9.02
477	Copertura	55, 57	0	-20.72	183.68	514.92	-226.62	-13.84	-25.12
			80	-20.72	183.68	285.12	-351.50	6.13	-25.12
			159	-20.72	183.68	-43.96	-476.38	26.09	-25.12
478	Copertura	56, 70	0	-23.83	-183.27	537.41	-243.58	18.38	32.70
			80	-23.83	-183.27	294.12	-368.46	-7.62	32.70
			159	-23.83	-183.27	-48.44	-493.33	-33.62	32.70
479	Copertura	57, 58	0	24.52	13.35	209.24	50.70	18.23	13.36
			83	24.52	13.35	192.04	-92.09	7.13	13.36
			166	24.52	13.35	56.15	-234.88	-3.98	13.36
480	Copertura	58, 59	0	23.96	-2.99	56.50	-3.96	-3.65	1.80
			69	23.96	-2.99	12.88	-122.49	-4.89	1.80
			138	23.96	-2.99	-112.53	-241.01	-6.14	1.80
481	Copertura	59, 60	0	24.35	-4.63	-111.68	72.63	-5.95	-1.56
			69	24.35	-4.63	-102.46	-45.90	-4.88	-1.56
			138	24.35	-4.63	-175.02	-164.43	-3.80	-1.56
482	Copertura	60, 61	0	24.57	-2.17	-174.48	110.44	-3.73	-1.27
			69	24.57	-2.17	-139.17	-8.09	-2.85	-1.27
			138	24.57	-2.17	-185.64	-126.62	-1.98	-1.27
483	Copertura	61, 62	0	46.25	-0.49	-185.31	158.34	-1.95	-0.53
			69	46.25	-0.49	-116.95	39.81	-1.58	-0.53
			138	46.25	-0.49	-130.37	-78.72	-1.21	-0.53
484	Copertura	62, 63	0	31.80	0.02	-130.20	157.27	-1.22	-0.18
			69	31.80	0.02	-62.58	38.75	-1.10	-0.18
			138	31.80	0.02	-76.73	-79.78	-0.98	-0.18
485	Copertura	63, 64	0	31.82	0.03	-76.68	117.55	-0.98	-0.05
			69	31.82	0.03	-36.46	-0.98	-0.95	-0.05
			138	31.82	0.03	-78.03	-119.51	-0.91	-0.05
486	Copertura	64, 65	0	31.79	0.03	-78.10	78.19	-0.91	0.08
			69	31.79	0.03	-65.04	-40.34	-0.97	0.08
			138	31.79	0.03	-133.77	-158.87	-1.02	0.08
487	Copertura	65, 66	0	45.93	0.55	-133.96	77.13	-1.01	0.44
			69	45.93	0.55	-121.63	-41.39	-1.32	0.44
			138	45.93	0.55	-191.08	-159.92	-1.62	0.44
488	Copertura	66, 67	0	23.84	2.31	-191.44	126.56	-1.66	1.20
			69	23.84	2.31	-145.01	8.04	-2.48	1.20
			138	23.84	2.31	-180.35	-110.49	-3.31	1.20
489	Copertura	67, 68	0	23.60	4.89	-180.93	165.15	-3.38	1.49
			69	23.60	4.89	-107.86	46.62	-4.41	1.49
			138	23.60	4.89	-116.58	-71.90	-5.44	1.49
490	Copertura	68, 69	0	23.19	3.20	-117.47	243.27	-5.63	-2.05
			69	23.19	3.20	9.49	124.74	-4.22	-2.05

			138	23.19	3.20	54.67	6.21	-2.80	-2.05
491	Copertura	69, 70	0	23.23	-14.06	54.32	240.27	-3.14	-14.30
			83	23.23	-14.06	194.69	97.48	8.75	-14.30
			166	23.23	-14.06	216.37	-45.31	20.63	-14.30
492	Copertura	1	0	-445.57	7.14	16.77	-7.06	-25.16	-9.23
			220	-547.21	7.14	1.24	-7.06	-4.86	-9.23
			440	-648.85	7.14	-14.29	-7.06	15.44	-9.23
493	Copertura	2	0	-240.74	-0.18	18.55	-12.36	-1.16	-0.58
			220	-285.10	-0.18	-8.64	-12.36	0.12	-0.58
			440	-329.45	-0.18	-35.83	-12.36	1.40	-0.58
494	Copertura	3	0	-318.91	-0.18	1.51	-3.32	-0.88	-0.40
			220	-363.26	-0.18	-5.79	-3.32	0.01	-0.40
			440	-407.61	-0.18	-13.10	-3.32	0.90	-0.40
495	Copertura	4	0	-285.44	-0.07	-2.51	0.33	-0.58	-0.24
			220	-329.80	-0.07	-1.79	0.33	-0.05	-0.24
			440	-374.15	-0.07	-1.06	0.33	0.48	-0.24
496	Copertura	5	0	-234.90	-0.01	-1.67	0.76	-0.39	-0.16
			220	-279.25	-0.01	0.00	0.76	-0.04	-0.16
			440	-323.61	-0.01	1.66	0.76	0.32	-0.16
497	Copertura	6	0	-201.27	0.00	-0.50	0.39	-0.23	-0.10
			220	-245.62	0.00	0.36	0.39	-0.02	-0.10
			440	-289.97	0.00	1.23	0.39	0.19	-0.10
498	Copertura	7	0	-186.28	0.00	0.00	0.16	-0.09	-0.04
			220	-230.63	0.00	0.35	0.16	0.00	-0.04
			440	-274.99	0.00	0.70	0.16	0.08	-0.04
499	Copertura	8	0	-187.90	0.00	-0.01	0.17	0.03	0.01
			220	-232.25	0.00	0.37	0.17	0.00	0.01
			440	-276.60	0.00	0.75	0.17	-0.02	0.01
500	Copertura	9	0	-194.01	0.00	-0.51	0.40	0.16	0.07
			220	-238.37	0.00	0.38	0.40	0.01	0.07
			440	-282.72	0.00	1.26	0.40	-0.14	0.07
501	Copertura	10	0	-222.45	0.01	-1.65	0.74	0.34	0.14
			220	-266.80	0.01	-0.01	0.74	0.04	0.14
			440	-311.15	0.01	1.63	0.74	-0.27	0.14
502	Copertura	11	0	-276.61	0.07	-2.51	0.31	0.55	0.23
			220	-320.96	0.07	-1.82	0.31	0.05	0.23
			440	-365.31	0.07	-1.14	0.31	-0.44	0.23
503	Copertura	12	0	-317.30	0.18	1.63	-3.41	0.87	0.40
			220	-361.65	0.18	-5.88	-3.41	0.00	0.40
			440	-406.01	0.18	-13.39	-3.41	-0.87	0.40
504	Copertura	13	0	-244.59	0.18	18.74	-12.47	1.14	0.57
			220	-288.94	0.18	-8.69	-12.47	-0.11	0.57
			440	-333.29	0.18	-36.13	-12.47	-1.37	0.57
505	Copertura	57	0	-428.38	-7.18	-17.57	7.35	-24.43	-8.91
			220	-530.02	-7.18	-1.41	7.35	-4.83	-8.91
			440	-631.66	-7.18	14.75	7.35	14.77	-8.91
506	Copertura	58	0	-236.98	0.18	-18.85	12.39	-1.13	-0.57
			220	-281.33	0.18	8.41	12.39	0.12	-0.57
			440	-325.68	0.18	35.67	12.39	1.38	-0.57
507	Copertura	59	0	-313.64	0.18	-1.65	3.36	-0.85	-0.39
			220	-357.99	0.18	5.75	3.36	0.01	-0.39
			440	-402.35	0.18	13.15	3.36	0.86	-0.39
508	Copertura	60	0	-274.86	0.07	2.46	-0.29	-0.54	-0.22
			220	-319.22	0.07	1.82	-0.29	-0.05	-0.22
			440	-363.57	0.07	1.18	-0.29	0.44	-0.22
509	Copertura	61	0	-223.24	0.01	1.63	-0.70	-0.34	-0.14
			220	-267.59	0.01	0.08	-0.70	-0.04	-0.14
			440	-311.94	0.01	-1.47	-0.70	0.27	-0.14
510	Copertura	62	0	-196.65	-0.01	0.50	-0.36	-0.17	-0.07
			220	-241.00	-0.01	-0.28	-0.36	-0.01	-0.07
			440	-285.36	-0.01	-1.07	-0.36	0.15	-0.07
511	Copertura	63	0	-197.33	0.00	0.00	-0.13	-0.05	-0.03
			220	-241.68	0.00	-0.28	-0.13	0.00	-0.03
			440	-286.03	0.00	-0.55	-0.13	0.06	-0.03
512	Copertura	64	0	-197.70	0.00	0.00	-0.13	0.07	0.03
			220	-242.05	0.00	-0.28	-0.13	0.00	0.03
			440	-286.40	0.00	-0.55	-0.13	-0.07	0.03
513	Copertura	65	0	-197.64	0.00	0.52	-0.36	0.19	0.08
			220	-241.99	0.00	-0.28	-0.36	0.01	0.08
			440	-286.34	0.00	-1.08	-0.36	-0.17	0.08
514	Copertura	66	0	-223.49	-0.01	1.69	-0.72	0.36	0.15
			220	-267.84	-0.01	0.10	-0.72	0.04	0.15

			440	-312.19	-0.01	-1.49	-0.72	-0.29	0.15
515	Copertura	67	0	-275.65	-0.07	2.58	-0.29	0.57	0.24
			220	-320.00	-0.07	1.94	-0.29	0.05	0.24
			440	-364.35	-0.07	1.30	-0.29	-0.47	0.24
516	Copertura	68	0	-315.17	-0.19	-1.69	3.54	0.89	0.41
			220	-359.53	-0.19	6.10	3.54	0.00	0.41
			440	-403.88	-0.19	13.89	3.54	-0.90	0.41
517	Copertura	69	0	-241.58	-0.19	-19.65	13.02	1.17	0.58
			220	-285.94	-0.19	9.00	13.02	-0.12	0.58
			440	-330.29	-0.19	37.64	13.02	-1.40	0.58
518	Primo Impalcato	1, 74	0	-23.28	0.22	0.00	2.51	2.49	0.85
			118	-16.62	0.22	1.48	0.00	1.49	0.85
			235	-9.97	0.22	0.00	-2.51	0.48	0.85
519	Copertura	74, 2	0	-124.33	-0.07	0.00	2.51	0.37	-0.47
			118	-130.98	-0.07	1.48	0.00	0.92	-0.47
			235	-137.63	-0.07	0.00	-2.51	1.47	-0.47
520	Primo Impalcato	6, 71	0	-69.73	0.00	0.00	2.09	-0.03	-0.01
			115	-63.08	0.00	1.20	0.00	-0.01	-0.01
			231	-56.43	0.00	0.00	-2.09	0.00	-0.01
521	Copertura	71, 7	0	-71.25	0.00	0.00	2.09	-0.02	0.00
			115	-77.90	0.00	1.20	0.00	-0.02	0.00
			231	-84.56	0.00	0.00	-2.09	-0.01	0.00
522	Primo Impalcato	9, 72	0	-92.60	0.00	0.00	2.09	-0.04	-0.01
			115	-85.95	0.00	1.20	0.00	-0.03	-0.01
			231	-79.30	0.00	0.00	-2.09	-0.01	-0.01
523	Copertura	72, 10	0	-56.19	0.00	0.00	2.09	0.00	0.02
			115	-62.84	0.00	1.20	0.00	-0.03	0.02
			231	-69.49	0.00	0.00	-2.09	-0.05	0.02
524	Copertura	73, 13	0	-124.82	0.07	0.00	2.51	-0.34	0.49
			118	-131.47	0.07	1.48	0.00	-0.92	0.49
			235	-138.13	0.07	0.00	-2.51	-1.49	0.49
525	Primo Impalcato	14, 73	0	-22.77	-0.23	0.00	2.51	-2.48	-0.83
			118	-16.12	-0.23	1.48	0.00	-1.50	-0.83
			235	-9.46	-0.23	0.00	-2.51	-0.53	-0.83
526	Primo Impalcato	57, 75	0	-22.98	-0.22	0.00	2.51	-2.51	-0.86
			118	-16.33	-0.22	1.48	0.00	-1.49	-0.86
			235	-9.68	-0.22	0.00	-2.51	-0.48	-0.86
527	Copertura	75, 58	0	-121.66	0.07	0.00	2.51	-0.37	0.47
			118	-128.31	0.07	1.48	0.00	-0.91	0.47
			235	-134.96	0.07	0.00	-2.51	-1.46	0.47
528	Copertura	77, 61	0	-56.50	0.00	0.00	2.09	0.00	0.02
			115	-63.15	0.00	1.20	0.00	-0.02	0.02
			231	-69.81	0.00	0.00	-2.09	-0.05	0.02
529	Primo Impalcato	62, 77	0	-93.26	0.00	0.00	2.09	-0.04	-0.01
			115	-86.61	0.00	1.20	0.00	-0.02	-0.01
			231	-79.95	0.00	0.00	-2.09	-0.01	-0.01
530	Primo Impalcato	65, 78	0	-94.60	0.00	0.00	2.09	0.04	0.01
			115	-87.95	0.00	1.20	0.00	0.02	0.01
			231	-81.29	0.00	0.00	-2.09	0.01	0.01
531	Copertura	78, 66	0	-55.47	0.00	0.00	2.09	0.00	-0.02
			115	-62.13	0.00	1.20	0.00	0.02	-0.02
			231	-68.78	0.00	0.00	-2.09	0.05	-0.02
532	Primo Impalcato	69, 76	0	-138.91	-0.07	0.00	2.51	-1.54	-0.49
			118	-132.26	-0.07	1.48	0.00	-0.96	-0.49
			235	-125.61	-0.07	0.00	-2.51	-0.38	-0.49
533	Copertura	76, 70	0	-8.10	0.23	0.00	2.51	-0.50	0.91
			118	-14.76	0.23	1.48	0.00	-1.57	0.91
			235	-21.41	0.23	0.00	-2.51	-2.63	0.91
534	Copertura	1, 74	0	-109.12	0.02	0.00	2.51	-1.82	-0.86
			118	-115.77	0.02	1.48	0.00	-0.80	-0.86
			235	-122.43	0.02	0.00	-2.51	0.21	-0.86
535	Copertura	74, 2	0	-8.07	0.05	0.00	2.51	0.54	0.46
			118	-1.42	0.05	1.48	0.00	0.01	0.46
			235	5.23	0.05	0.00	-2.51	-0.53	0.46
536	Copertura	6, 71	0	-56.64	0.00	0.00	2.09	0.01	0.01

			115	-63.29	0.00	1.20	0.00	0.00	0.01
			231	-69.94	0.00	0.00	-2.09	-0.02	0.01
537	Copertura	71, 7	0	-55.12	0.00	0.00	2.09	0.00	0.00
			115	-48.46	0.00	1.20	0.00	0.00	0.00
			231	-41.81	0.00	0.00	-2.09	0.00	0.00
538	Copertura	9, 72	0	-41.57	0.00	0.00	2.09	0.01	0.00
			115	-48.23	0.00	1.20	0.00	0.00	0.00
			231	-54.88	0.00	0.00	-2.09	0.00	0.00
539	Copertura	72, 10	0	-77.99	0.00	0.00	2.09	-0.01	-0.03
			115	-71.33	0.00	1.20	0.00	0.02	-0.03
			231	-64.68	0.00	0.00	-2.09	0.06	-0.03
540	Copertura	73, 13	0	-7.56	-0.05	0.00	2.51	-0.59	-0.48
			118	-0.91	-0.05	1.48	0.00	-0.03	-0.48
			235	5.74	-0.05	0.00	-2.51	0.54	-0.48
541	Copertura	14, 73	0	-109.62	-0.03	0.00	2.51	1.79	0.84
			118	-116.27	-0.03	1.48	0.00	0.81	0.84
			235	-122.92	-0.03	0.00	-2.51	-0.18	0.84
542	Copertura	15, 125	0	757.83	-1.23	-85.44	-57.55	-2.93	-2.44
			75	757.83	-1.23	-155.06	-128.11	-1.10	-2.44
			150	757.83	-1.23	-277.60	-198.67	0.73	-2.44
543	Copertura	127, 16	0	777.90	3.47	-302.56	212.77	4.36	9.71
			75	777.90	3.47	-169.44	142.21	-2.93	9.71
			150	777.90	3.47	-89.24	71.65	-10.21	9.71
544	Copertura	17, 129	0	700.09	-0.33	41.47	-3.68	-0.57	-0.52
			75	700.09	-0.33	12.95	-72.35	-0.18	-0.52
			150	700.09	-0.33	-67.06	-141.02	0.21	-0.52
545	Copertura	130, 18	0	700.51	0.38	-68.37	141.19	0.57	0.62
			75	700.51	0.38	11.77	72.52	0.10	0.62
			150	700.51	0.38	40.40	3.85	-0.37	0.62
546	Copertura	19, 135	0	714.95	-0.07	62.48	-5.57	-0.18	0.00
			75	714.95	-0.07	32.55	-74.24	-0.19	0.00
			150	714.95	-0.07	-48.88	-142.91	-0.19	0.00
547	Copertura	134, 20	0	713.75	0.09	-47.24	142.08	0.31	0.07
			75	713.75	0.09	33.57	73.41	0.26	0.07
			150	713.75	0.09	62.88	4.74	0.20	0.07
548	Copertura	21, 136	0	718.25	-0.01	67.80	-14.46	-0.19	0.02
			75	718.25	-0.01	31.20	-83.13	-0.20	0.02
			150	718.25	-0.01	-56.89	-151.80	-0.22	0.02
549	Copertura	138, 22	0	718.08	-0.02	-56.52	151.71	0.17	-0.10
			75	718.08	-0.02	31.51	83.04	0.25	-0.10
			150	718.08	-0.02	68.04	14.37	0.33	-0.10
550	Copertura	23, 141	0	719.24	0.01	69.28	-18.40	-0.19	-0.01
			75	719.24	0.01	29.72	-87.07	-0.17	-0.01
			150	719.24	0.01	-61.34	-155.74	-0.16	-0.01
551	Copertura	142, 24	0	719.29	-0.05	-61.38	155.80	0.11	-0.08
			75	719.29	-0.05	29.71	87.13	0.17	-0.08
			150	719.29	-0.05	69.31	18.46	0.23	-0.08
552	Copertura	25, 145	0	722.37	0.01	71.90	-21.47	-0.09	-0.01
			75	722.37	0.01	30.05	-90.14	-0.09	-0.01
			150	722.37	0.01	-63.30	-158.81	-0.09	-0.01
553	Copertura	146, 26	0	720.02	-0.16	-61.82	156.78	-0.07	-0.13
			75	720.02	-0.16	30.02	88.11	0.03	-0.13
			150	720.02	-0.16	70.36	19.44	0.12	-0.13
554	Copertura	150, 27	0	718.41	-0.33	-61.55	155.22	-0.23	-0.18
			75	718.41	-0.33	29.11	86.55	-0.09	-0.18
			150	718.41	-0.33	68.28	17.88	0.05	-0.18
555	Copertura	28, 149	0	720.42	-0.52	69.46	-19.63	-0.09	-0.32
			75	720.42	-0.52	28.98	-88.30	0.15	-0.32
			150	720.42	-0.52	-62.99	-156.97	0.39	-0.32
556	Copertura	154, 29	0	716.57	-0.62	-60.74	152.40	-0.55	-0.38
			75	716.57	-0.62	27.80	83.73	-0.26	-0.38
			150	716.57	-0.62	64.84	15.06	0.03	-0.38
557	Copertura	30, 153	0	716.35	-0.68	64.64	-14.87	-0.01	-0.41
			75	716.35	-0.68	27.74	-83.54	0.29	-0.41
			150	716.35	-0.68	-60.67	-152.21	0.60	-0.41
558	Copertura	158, 31	0	715.82	-0.64	-60.35	151.78	-0.63	-0.39
			75	715.82	-0.64	27.74	83.11	-0.35	-0.39
			150	715.82	-0.64	64.32	14.44	-0.06	-0.39
559	Copertura	32, 157	0	715.39	-0.73	63.81	-14.06	0.07	-0.42
			75	715.39	-0.73	27.52	-82.73	0.39	-0.42
			150	715.39	-0.73	-60.28	-151.40	0.70	-0.42
560	Copertura	162, 33	0	715.08	-0.76	-60.23	151.13	-0.77	-0.45

			75	715.08	-0.76	27.37	82.46	-0.43	-0.45
			150	715.08	-0.76	63.47	13.79	-0.09	-0.45
561	Copertura	34, 161	0	715.69	-0.80	63.68	-14.32	0.11	-0.46
			75	715.69	-0.80	27.19	-82.99	0.45	-0.46
			150	715.69	-0.80	-60.80	-151.66	0.80	-0.46
562	Copertura	166, 35	0	714.46	-0.80	-59.90	150.55	-0.82	-0.48
			75	714.46	-0.80	27.26	81.88	-0.46	-0.48
			150	714.46	-0.80	62.92	13.21	-0.11	-0.48
563	Copertura	36, 165	0	715.88	-0.87	63.40	-14.40	0.11	-0.50
			75	715.88	-0.87	26.85	-83.07	0.49	-0.50
			150	715.88	-0.87	-61.21	-151.74	0.87	-0.50
564	Copertura	170, 37	0	714.40	-0.89	-59.89	150.22	-0.85	-0.52
			75	714.40	-0.89	27.03	81.55	-0.46	-0.52
			150	714.40	-0.89	62.44	12.88	-0.07	-0.52
565	Copertura	38, 169	0	715.19	-0.94	62.65	-13.56	0.06	-0.56
			75	715.19	-0.94	26.72	-82.23	0.48	-0.56
			150	715.19	-0.94	-60.70	-150.90	0.90	-0.56
566	Copertura	175, 39	0	714.63	-0.94	-59.69	149.72	-0.82	-0.59
			75	714.63	-0.94	26.85	81.05	-0.37	-0.59
			150	714.63	-0.94	61.88	12.38	0.07	-0.59
567	Copertura	40, 173	0	713.43	-1.00	60.92	-11.34	-0.06	-0.61
			75	713.43	-1.00	26.66	-80.01	0.40	-0.61
			150	713.43	-1.00	-59.11	-148.68	0.86	-0.61
568	Copertura	178, 41	0	716.87	-0.71	-61.17	151.60	-0.44	-0.39
			75	716.87	-0.71	26.78	82.93	-0.15	-0.39
			150	716.87	-0.71	63.22	14.26	0.14	-0.39
569	Copertura	42, 177	0	711.85	-1.06	58.41	-9.95	-0.20	-0.64
			75	711.85	-1.06	25.19	-78.62	0.28	-0.64
			150	711.85	-1.06	-59.52	-147.29	0.76	-0.64
570	Copertura	43, 181	0	715.35	0.04	68.70	-14.31	-0.04	0.00
			75	715.35	0.04	32.22	-82.98	-0.04	0.00
			150	715.35	0.04	-55.77	-151.65	-0.04	0.00
571	Copertura	182, 44	0	719.51	-0.34	-58.99	155.15	-0.30	-0.33
			75	719.51	-0.34	31.62	86.48	-0.05	-0.33
			150	719.51	-0.34	70.73	17.81	0.20	-0.33
572	Copertura	45, 185	0	718.02	0.01	68.47	-16.05	-0.17	-0.01
			75	718.02	0.01	30.69	-84.72	-0.16	-0.01
			150	718.02	0.01	-58.60	-153.39	-0.15	-0.01
573	Copertura	186, 46	0	719.59	-0.01	-59.40	154.77	0.14	-0.02
			75	719.59	-0.01	30.93	86.10	0.15	-0.02
			150	719.59	-0.01	69.75	17.43	0.16	-0.02
574	Copertura	47, 189	0	718.89	0.03	68.77	-17.26	-0.23	-0.02
			75	718.89	0.03	30.08	-85.93	-0.22	-0.02
			150	718.89	0.03	-60.12	-154.60	-0.21	-0.02
575	Copertura	190, 48	0	717.09	-0.05	-58.28	153.17	0.13	-0.08
			75	717.09	-0.05	30.85	84.50	0.19	-0.08
			150	717.09	-0.05	68.48	15.83	0.25	-0.08
576	Copertura	49, 193	0	719.44	0.04	68.30	-15.16	-0.28	-0.07
			75	719.44	0.04	31.18	-83.83	-0.23	-0.07
			150	719.44	0.04	-57.44	-152.50	-0.18	-0.07
577	Copertura	195, 50	0	716.67	-0.03	-54.39	150.36	0.17	0.05
			75	716.67	-0.03	32.63	81.69	0.13	0.05
			150	716.67	-0.03	68.14	13.02	0.10	0.05
578	Copertura	51, 197	0	716.78	0.10	63.69	-7.00	-0.25	-0.05
			75	716.78	0.10	32.69	-75.67	-0.21	-0.05
			150	716.78	0.10	-49.81	-144.34	-0.17	-0.05
579	Copertura	199, 52	0	712.11	-0.13	-45.93	140.48	0.02	-0.02
			75	712.11	-0.13	33.68	71.81	0.04	-0.02
			150	712.11	-0.13	61.78	3.14	0.05	-0.02
580	Copertura	53, 201	0	699.67	0.37	42.30	-4.30	0.32	0.49
			75	699.67	0.37	13.33	-72.97	-0.04	0.49
			150	699.67	0.37	-67.15	-141.64	-0.41	0.49
581	Copertura	202, 54	0	699.43	-0.78	-67.45	141.31	-0.86	-1.72
			75	699.43	-0.78	12.78	72.64	0.42	-1.72
			150	699.43	-0.78	41.51	3.97	1.71	-1.72
582	Copertura	55, 205	0	764.03	1.13	-85.61	-59.00	2.43	2.42
			75	764.03	1.13	-156.31	-129.56	0.61	2.42
			150	764.03	1.13	-279.94	-200.12	-1.20	2.42
583	Copertura	206, 56	0	773.53	-1.50	-290.68	207.21	-1.40	-3.49
			75	773.53	-1.50	-161.74	136.65	1.22	-3.49
			150	773.53	-1.50	-85.71	66.09	3.84	-3.49
584	Copertura	57, 75	0	-106.45	-0.02	0.00	2.51	1.86	0.88

			118	-113.10	-0.02	1.48	0.00	0.83	0.88
			235	-119.76	-0.02	0.00	-2.51	-0.21	0.88
585	Copertura	75, 58	0	-7.78	-0.05	0.00	2.51	-0.54	-0.45
			118	-1.13	-0.05	1.48	0.00	0.00	-0.45
			235	5.53	-0.05	0.00	-2.51	0.53	-0.45
586	Copertura	77, 61	0	-78.64	0.00	0.00	2.09	-0.01	-0.03
			115	-71.99	0.00	1.20	0.00	0.02	-0.03
			231	-65.34	0.00	0.00	-2.09	0.06	-0.03
587	Copertura	62, 77	0	-41.89	0.00	0.00	2.09	0.01	0.00
			115	-48.54	0.00	1.20	0.00	0.01	0.00
			231	-55.19	0.00	0.00	-2.09	0.00	0.00
588	Copertura	65, 78	0	-40.86	0.00	0.00	2.09	-0.01	0.00
			115	-47.51	0.00	1.20	0.00	0.00	0.00
			231	-54.17	0.00	0.00	-2.09	0.00	0.00
589	Copertura	78, 66	0	-79.99	0.00	0.00	2.09	0.01	0.03
			115	-73.33	0.00	1.20	0.00	-0.03	0.03
			231	-66.68	0.00	0.00	-2.09	-0.07	0.03
590	Copertura	69, 76	0	7.10	0.05	0.00	2.51	0.55	0.47
			118	0.45	0.05	1.48	0.00	-0.01	0.47
			235	-6.21	0.05	0.00	-2.51	-0.56	0.47
591	Copertura	76, 70	0	-123.71	0.02	0.00	2.51	-0.22	-0.92
			118	-117.05	0.02	1.48	0.00	0.87	-0.92
			235	-110.40	0.02	0.00	-2.51	1.95	-0.92
592	Copertura	79, 81	0	2.50	0.85	-10.89	19.45	28.24	32.94
			80	2.50	0.85	1.23	11.04	2.05	32.94
			159	2.50	0.85	6.67	2.62	-24.14	32.94
593	Copertura	80, 82	0	-1.37	0.14	-5.91	13.49	-9.08	-2.67
			66	-1.62	0.14	0.69	6.50	-7.31	-2.67
			132	-1.86	0.14	2.68	-0.48	-5.55	-2.67
594	Copertura	83, 84	0	-3.66	-0.01	-2.32	8.21	-0.37	-0.47
			66	-3.66	-0.01	0.80	1.23	-0.06	-0.47
			132	-3.66	-0.01	-0.70	-5.76	0.26	-0.47
595	Copertura	85, 86	0	-6.79	0.00	-1.47	7.48	0.04	0.04
			66	-6.79	0.00	1.16	0.49	0.01	0.04
			132	-6.79	0.00	-0.82	-6.49	-0.01	0.04
596	Copertura	87, 88	0	-11.26	0.00	-4.41	12.15	-0.06	0.00
			66	-11.26	0.00	1.30	5.16	-0.06	0.00
			132	-11.26	0.00	2.40	-1.82	-0.05	0.00
597	Copertura	89, 90	0	-6.27	0.00	-6.48	14.92	-0.05	-0.02
			66	-6.27	0.00	1.06	7.94	-0.04	-0.02
			132	-6.27	0.00	3.99	0.95	-0.02	-0.02
598	Copertura	91, 92	0	-4.91	0.00	-7.12	15.81	-0.03	-0.02
			66	-4.91	0.00	1.00	8.82	-0.02	-0.02
			132	-4.91	0.00	4.52	1.84	-0.01	-0.02
599	Copertura	93, 94	0	5.97	0.00	-6.30	13.75	-0.03	0.00
			66	5.97	0.00	0.48	6.77	-0.03	0.00
			132	5.97	0.00	2.64	-0.22	-0.04	0.00
600	Copertura	95, 96	0	11.62	0.00	-4.02	10.45	0.05	-0.01
			66	11.62	0.00	0.57	3.47	0.05	-0.01
			132	11.62	0.00	0.55	-3.52	0.06	-0.01
601	Copertura	97, 106	0	-1.26	0.00	-0.97	6.29	0.18	0.00
			66	-1.26	0.00	0.88	-0.70	0.18	0.00
			132	-1.26	0.00	-1.89	-7.69	0.18	0.00
602	Copertura	98, 99	0	-0.19	0.04	-4.70	11.71	-1.73	-0.91
			66	-0.19	0.04	0.72	4.73	-1.13	-0.91
			132	-0.19	0.04	1.54	-2.26	-0.53	-0.91
603	Copertura	100, 101	0	-0.63	-0.01	-0.92	6.13	0.07	-0.01
			66	-0.63	-0.01	0.82	-0.86	0.08	-0.01
			132	-0.63	-0.01	-2.05	-7.84	0.09	-0.01
604	Copertura	102, 103	0	-8.07	0.00	-0.80	6.63	0.00	-0.01
			66	-8.07	0.00	1.27	-0.36	0.01	-0.01
			132	-8.07	0.00	-1.27	-7.34	0.01	-0.01
605	Copertura	104, 105	0	-2.33	0.00	-2.49	8.58	-0.08	-0.11
			66	-2.33	0.00	0.87	1.59	-0.01	-0.11
			132	-2.33	0.00	-0.39	-5.39	0.06	-0.11
606	Copertura	107, 108	0	-3.98	-0.01	2.04	1.45	-0.92	1.39
			66	-3.98	-0.01	0.69	-5.54	-1.84	1.39
			132	-3.98	-0.01	-5.27	-12.52	-2.75	1.39
607	Copertura	109, 110	0	0.39	0.74	4.37	0.27	-16.78	-26.00
			80	0.39	0.74	1.24	-8.14	3.89	-26.00
			159	0.39	0.74	-8.58	-16.56	24.56	-26.00
608	Copertura	111, 112	0	-2.07	0.09	-2.54	8.60	-0.09	-0.12

			66	-1.80	0.09	0.84	1.62	0.00	-0.12
			132	-1.52	0.09	-0.40	-5.37	0.08	-0.12
609	Copertura	113, 114	0	0.12	0.00	-2.12	8.38	-0.06	-0.13
			66	0.12	0.00	1.11	1.40	0.02	-0.13
			132	0.12	0.00	-0.28	-5.59	0.11	-0.13
610	Copertura	115, 116	0	19.86	0.00	-1.86	7.00	-0.10	-0.15
			66	19.86	0.00	0.46	0.02	0.00	-0.15
			132	19.86	0.00	-1.84	-6.97	0.10	-0.15
611	Copertura	117, 118	0	1.92	0.00	-0.70	6.23	0.01	-0.03
			66	1.92	0.00	1.11	-0.76	0.03	-0.03
			132	1.92	0.00	-1.70	-7.74	0.06	-0.03
612	Copertura	119, 120	0	-0.22	0.03	1.08	3.01	0.21	0.45
			66	-0.22	0.03	0.77	-3.97	-0.08	0.45
			132	-0.22	0.03	-4.16	-10.96	-0.38	0.45
613	Copertura	121, 122	0	0.61	-0.47	6.31	-4.94	-4.14	-0.69
			66	0.61	-0.47	0.75	-11.93	-3.69	-0.69
			132	0.61	-0.47	-9.43	-18.91	-3.24	-0.69
614	Copertura	124, 125	0	-1385.44	0.16	-73.41	56.63	3.34	2.37
			99	-1377.58	0.16	-21.71	47.56	0.98	2.37
			198	-1369.72	0.16	20.99	38.49	-1.38	2.37
615	Copertura	125, 127	0	-252.04	-0.22	-256.61	727.49	-0.21	-0.07
			775	-252.04	-0.22	2556.12	-1.63	0.31	-0.07
			1550	-252.04	-0.22	-281.84	-730.75	0.84	-0.07
616	Copertura	126, 127	0	-1411.98	-0.48	-73.64	56.61	-14.34	-9.78
			99	-1404.12	-0.48	-21.96	47.54	-4.63	-9.78
			198	-1396.26	-0.48	20.72	38.47	5.07	-9.78
617	Copertura	128, 129	0	-1268.59	0.06	-72.82	57.83	0.56	0.50
			99	-1260.73	0.06	-19.93	48.76	0.06	0.50
			198	-1252.86	0.06	23.96	39.68	-0.43	0.50
618	Copertura	129, 130	0	-220.70	0.00	-43.10	709.50	-0.08	-0.02
			775	-220.70	0.00	2705.89	-0.09	0.07	-0.02
			1550	-220.70	0.00	-44.44	-709.68	0.22	-0.02
619	Copertura	131, 130	0	-1269.13	-0.06	-72.80	57.80	-0.77	-0.64
			99	-1261.27	-0.06	-19.93	48.73	-0.13	-0.64
			198	-1253.40	-0.06	23.93	39.66	0.51	-0.64
620	Copertura	132, 135	0	-1270.99	0.02	-73.44	58.51	-0.16	-0.03
			99	-1263.12	0.02	-19.87	49.44	-0.12	-0.03
			198	-1255.26	0.02	24.69	40.36	-0.09	-0.03
621	Copertura	133, 134	0	-1269.39	-0.02	-73.40	58.50	-0.08	-0.10
			99	-1261.53	-0.02	-19.83	49.43	0.02	-0.10
			198	-1253.67	-0.02	24.72	40.36	0.12	-0.10
622	Copertura	135, 134	0	-207.20	0.00	-24.20	709.70	-0.25	-0.03
			775	-207.20	0.00	2726.30	0.11	-0.01	-0.03
			1550	-207.20	0.00	-22.52	-709.48	0.23	-0.03
623	Copertura	137, 136	0	-1284.05	0.00	-73.87	58.83	-0.11	-0.05
			99	-1276.19	0.00	-19.99	49.76	-0.07	-0.05
			198	-1268.33	0.00	24.89	40.68	-0.02	-0.05
624	Copertura	136, 138	0	-213.57	0.01	-32.00	709.61	-0.23	-0.03
			775	-213.57	0.01	2717.85	0.02	-0.01	-0.03
			1550	-213.57	0.01	-31.61	-709.56	0.20	-0.03
625	Copertura	139, 138	0	-1283.83	0.00	-73.87	58.84	0.11	0.07
			99	-1275.97	0.00	-19.98	49.76	0.03	0.07
			198	-1268.11	0.00	24.91	40.69	-0.04	0.07
626	Copertura	140, 141	0	-1289.88	0.00	-74.01	58.97	-0.01	-0.01
			99	-1282.01	0.00	-19.99	49.90	-0.01	-0.01
			198	-1274.15	0.00	25.03	40.82	0.00	-0.01
627	Copertura	141, 142	0	-216.89	0.01	-36.31	709.59	-0.17	-0.02
			775	-216.89	0.01	2713.33	0.00	0.00	-0.02
			1550	-216.89	0.01	-36.36	-709.59	0.16	-0.02
628	Copertura	143, 142	0	-1289.96	0.01	-74.03	58.98	0.04	0.06
			99	-1282.10	0.01	-20.00	49.90	-0.02	0.06
			198	-1274.23	0.01	25.03	40.83	-0.08	0.06
629	Copertura	144, 145	0	-1294.46	0.00	-74.16	59.17	-0.02	-0.01
			99	-1286.59	0.00	-19.94	50.10	-0.01	-0.01
			198	-1278.73	0.00	25.27	41.02	0.00	-0.01
630	Copertura	145, 146	0	-217.09	0.01	-38.03	709.68	-0.09	-0.01
			775	-217.09	0.01	2712.30	0.09	0.01	-0.01
			1550	-217.09	0.01	-36.69	-709.50	0.10	-0.01
631	Copertura	147, 146	0	-1291.25	0.02	-74.07	59.05	-0.01	0.11
			99	-1283.38	0.02	-19.97	49.97	-0.13	0.11
			198	-1275.52	0.02	25.13	40.90	-0.24	0.11
632	Copertura	148, 149	0	-1291.97	0.04	-74.14	59.13	0.07	0.32

			99	-1284.10	0.04	-19.96	50.06	-0.25	0.32
			198	-1276.24	0.04	25.21	40.98	-0.57	0.32
633	Copertura	149, 150	0	-217.18	-0.11	-37.78	709.85	-0.01	0.00
			775	-217.18	-0.11	2713.91	0.08	-0.01	0.00
			1550	-217.18	-0.11	-36.50	-709.69	0.00	0.00
634	Copertura	151, 150	0	-1289.20	0.02	-74.05	59.00	0.04	0.18
			99	-1281.34	0.02	-20.00	49.93	-0.14	0.18
			198	-1273.47	0.02	25.05	40.85	-0.32	0.18
635	Copertura	152, 153	0	-1285.07	0.06	-73.98	58.90	0.07	0.42
			99	-1277.20	0.06	-20.02	49.83	-0.34	0.42
			198	-1269.34	0.06	24.93	40.76	-0.76	0.42
636	Copertura	153, 154	0	-216.18	-0.14	-35.74	709.92	0.07	0.01
			775	-216.18	-0.14	2716.47	-0.01	-0.01	0.01
			1551	-216.18	-0.14	-35.83	-709.93	-0.08	0.01
637	Copertura	155, 154	0	-1285.36	0.05	-74.00	58.90	0.11	0.39
			99	-1277.50	0.05	-20.04	49.83	-0.28	0.39
			198	-1269.64	0.05	24.92	40.76	-0.67	0.39
638	Copertura	156, 157	0	-1283.96	0.06	-73.98	58.88	0.07	0.44
			99	-1276.09	0.06	-20.04	49.81	-0.36	0.44
			198	-1268.23	0.06	24.89	40.74	-0.80	0.44
639	Copertura	157, 158	0	-216.32	-0.16	-35.39	709.99	0.14	0.02
			775	-216.32	-0.16	2717.36	0.00	-0.01	0.02
			1551	-216.32	-0.16	-35.45	-710.00	-0.15	0.02
640	Copertura	159, 158	0	-1284.54	0.05	-74.00	58.90	0.12	0.40
			99	-1276.67	0.05	-20.05	49.82	-0.28	0.40
			198	-1268.81	0.05	24.89	40.75	-0.68	0.40
641	Copertura	160, 161	0	-1284.48	0.06	-74.04	58.94	0.09	0.48
			99	-1276.62	0.06	-20.04	49.86	-0.39	0.48
			198	-1268.75	0.06	24.94	40.79	-0.87	0.48
642	Copertura	161, 162	0	-216.38	-0.18	-35.86	710.11	0.18	0.02
			776	-216.38	-0.18	2717.87	0.03	-0.01	0.02
			1551	-216.38	-0.18	-35.33	-710.05	-0.19	0.02
643	Copertura	163, 162	0	-1283.63	0.06	-73.99	58.89	0.13	0.48
			99	-1275.77	0.06	-20.05	49.82	-0.35	0.48
			198	-1267.90	0.06	24.90	40.75	-0.82	0.48
644	Copertura	164, 165	0	-1284.77	0.07	-74.09	58.99	0.11	0.53
			99	-1276.91	0.07	-20.05	49.92	-0.42	0.53
			198	-1269.04	0.07	24.99	40.84	-0.94	0.53
645	Copertura	165, 166	0	-216.37	-0.20	-36.22	710.26	0.20	0.03
			776	-216.37	-0.20	2718.62	0.08	-0.01	0.03
			1551	-216.37	-0.20	-35.00	-710.10	-0.21	0.03
646	Copertura	167, 166	0	-1282.81	0.06	-74.01	58.90	0.14	0.50
			99	-1274.95	0.06	-20.05	49.83	-0.36	0.50
			198	-1267.09	0.06	24.91	40.76	-0.86	0.50
647	Copertura	168, 169	0	-1283.59	0.07	-74.10	59.00	0.13	0.58
			99	-1275.73	0.07	-20.05	49.92	-0.44	0.58
			198	-1267.87	0.07	25.00	40.85	-1.02	0.58
648	Copertura	169, 170	0	-216.16	-0.21	-35.70	710.33	0.17	0.02
			776	-216.16	-0.21	2719.74	0.05	0.00	0.02
			1552	-216.16	-0.21	-34.94	-710.24	-0.18	0.02
649	Copertura	171, 170	0	-1282.48	0.07	-74.02	58.93	0.12	0.54
			99	-1274.62	0.07	-20.03	49.86	-0.41	0.54
			198	-1266.76	0.07	24.94	40.78	-0.95	0.54
650	Copertura	172, 173	0	-1280.31	0.08	-74.02	58.92	0.15	0.63
			99	-1272.45	0.08	-20.05	49.85	-0.47	0.63
			198	-1264.58	0.08	24.93	40.78	-1.09	0.63
651	Copertura	173, 175	0	-215.50	-0.22	-34.18	710.35	0.09	0.01
			776	-215.50	-0.22	2721.36	-0.03	0.00	0.01
			1552	-215.50	-0.22	-34.71	-710.42	-0.10	0.01
652	Copertura	174, 175	0	-1281.94	0.07	-74.05	58.96	0.18	0.60
			99	-1274.08	0.07	-20.04	49.89	-0.42	0.60
			198	-1266.22	0.07	24.98	40.82	-1.01	0.60
653	Copertura	176, 177	0	-1278.34	0.08	-73.95	58.86	0.13	0.64
			99	-1270.48	0.08	-20.04	49.79	-0.50	0.64
			198	-1262.62	0.08	24.87	40.72	-1.13	0.64
654	Copertura	177, 178	0	-215.63	-0.27	-34.65	710.41	-0.05	0.00
			776	-215.63	-0.27	2721.33	-0.10	-0.02	0.00
			1552	-215.63	-0.27	-36.19	-710.60	0.01	0.00
655	Copertura	179, 178	0	-1285.09	0.04	-74.08	58.98	0.13	0.38
			99	-1277.23	0.04	-20.05	49.91	-0.25	0.38
			198	-1269.36	0.04	24.99	40.84	-0.63	0.38
656	Copertura	180, 181	0	-1283.51	0.00	-73.85	58.82	-0.02	-0.01

			99	-1275.65	0.00	-19.97	49.75	-0.01	-0.01
			198	-1267.78	0.00	24.91	40.68	0.01	-0.01
657	Copertura	181, 182	0	-216.06	0.03	-30.87	709.40	-0.04	-0.01
			775	-216.06	0.03	2717.31	-0.19	0.02	-0.01
			1550	-216.06	0.03	-33.84	-709.78	0.07	-0.01
658	Copertura	183, 182	0	-1289.20	0.04	-74.01	59.03	0.11	0.32
			99	-1281.34	0.04	-19.92	49.96	-0.20	0.32
			198	-1273.48	0.04	25.16	40.89	-0.52	0.32
659	Copertura	184, 185	0	-1286.31	0.00	-73.91	58.89	-0.01	-0.01
			99	-1278.45	0.00	-19.97	49.81	-0.01	-0.01
			198	-1270.58	0.00	24.97	40.74	0.00	-0.01
660	Copertura	185, 186	0	-215.46	0.01	-33.64	709.55	-0.15	-0.02
			775	-215.46	0.01	2715.69	-0.04	0.00	-0.02
			1550	-215.46	0.01	-34.31	-709.63	0.15	-0.02
661	Copertura	187, 186	0	-1288.46	0.01	-73.95	58.97	-0.03	0.00
			99	-1280.59	0.01	-19.93	49.89	-0.03	0.00
			198	-1272.73	0.01	25.08	40.82	-0.03	0.00
662	Copertura	188, 189	0	-1288.35	-0.01	-74.00	58.94	0.00	-0.01
			99	-1280.49	-0.01	-20.01	49.86	0.01	-0.01
			198	-1272.62	-0.01	24.98	40.79	0.02	-0.01
663	Copertura	189, 190	0	-216.11	0.01	-35.14	709.71	-0.20	-0.03
			775	-216.11	0.01	2715.43	0.12	0.00	-0.03
			1550	-216.11	0.01	-33.33	-709.47	0.21	-0.03
664	Copertura	191, 190	0	-1285.91	0.00	-73.88	58.86	0.01	0.05
			99	-1278.04	0.00	-19.96	49.79	-0.04	0.05
			198	-1270.18	0.00	24.95	40.71	-0.10	0.05
665	Copertura	192, 193	0	-1285.32	-0.01	-73.94	58.88	0.12	0.04
			99	-1277.45	-0.01	-20.00	49.81	0.08	0.04
			198	-1269.59	-0.01	24.94	40.74	0.04	0.04
666	Copertura	193, 195	0	-213.29	0.01	-32.51	709.78	-0.16	-0.02
			775	-213.29	0.01	2718.66	0.19	0.02	-0.02
			1550	-213.29	0.01	-29.49	-709.40	0.20	-0.02
667	Copertura	194, 195	0	-1281.56	0.01	-73.78	58.79	-0.20	-0.07
			99	-1273.70	0.01	-19.94	49.72	-0.12	-0.07
			198	-1265.84	0.01	24.90	40.65	-0.05	-0.07
668	Copertura	196, 197	0	-1273.25	-0.03	-73.53	58.61	0.18	0.04
			99	-1265.39	-0.03	-19.87	49.53	0.14	0.04
			198	-1257.53	-0.03	24.79	40.46	0.11	0.04
669	Copertura	197, 199	0	-207.02	0.01	-25.02	709.83	-0.11	-0.02
			775	-207.02	0.01	2726.49	0.24	0.02	-0.02
			1550	-207.02	0.01	-21.32	-709.35	0.15	-0.02
670	Copertura	198, 199	0	-1266.89	0.02	-73.27	58.38	-0.18	0.00
			99	-1259.02	0.02	-19.83	49.31	-0.19	0.00
			198	-1251.16	0.02	24.61	40.24	-0.19	0.00
671	Copertura	200, 201	0	-1269.56	-0.06	-72.86	57.88	-0.53	-0.49
			99	-1261.70	-0.06	-19.92	48.81	-0.05	-0.49
			198	-1253.84	-0.06	24.02	39.74	0.43	-0.49
672	Copertura	201, 202	0	-221.82	0.04	-43.13	709.57	-0.12	0.00
			775	-221.82	0.04	2706.35	-0.02	-0.11	0.00
			1550	-221.82	0.04	-43.48	-709.61	-0.10	0.00
673	Copertura	203, 202	0	-1269.20	0.12	-72.80	57.82	2.30	1.72
			99	-1261.34	0.12	-19.92	48.75	0.59	1.72
			198	-1253.48	0.12	23.97	39.68	-1.11	1.72
674	Copertura	204, 205	0	-1388.96	-0.17	-73.58	56.75	-3.36	-2.44
			99	-1381.09	-0.17	-21.76	47.68	-0.95	-2.44
			198	-1373.23	-0.17	21.06	38.61	1.47	-2.44
675	Copertura	205, 206	0	-248.43	0.04	-258.88	728.43	-0.20	-0.02
			775	-248.43	0.04	2561.10	-0.69	-0.07	-0.02
			1550	-248.43	0.04	-269.60	-729.81	0.06	-0.02
676	Copertura	207, 206	0	-1401.69	0.21	-73.92	56.93	4.79	3.48
			99	-1393.82	0.21	-21.92	47.86	1.34	3.48
			198	-1385.96	0.21	21.08	38.78	-2.11	3.48
677	Copertura	79	0	-533.87	4.77	7.65	-8.84	-11.17	-2.98
			125	-591.62	4.77	-3.40	-8.84	-7.44	-2.98
			250	-649.37	4.77	-14.46	-8.84	-3.71	-2.98
678	Copertura	124	0	-863.17	4.65	2.29	-2.45	950.26	281.78
			155	-915.25	4.65	-1.51	-2.45	513.50	281.78
			310	-967.33	4.65	-5.31	-2.45	76.74	281.78
679	Copertura	80	0	-958.87	-3.93	0.34	-7.92	-325.29	-271.64
			45	-973.99	-3.93	-3.22	-7.92	-203.06	-271.64
			90	-989.11	-3.93	-6.79	-7.92	-80.82	-271.64
680	Copertura	128	0	-956.63	0.88	1.69	-1.67	929.48	210.75

			155	-1008.71	0.88	-0.90	-1.67	602.81	210.75
			310	-1060.79	0.88	-3.48	-1.67	276.14	210.75
681	Copertura	82	0	-1045.69	2.73	-0.82	-1.95	-455.94	-213.11
			43	-1060.03	2.73	-1.65	-1.95	-365.03	-213.11
			85	-1074.36	2.73	-2.49	-1.95	-274.12	-213.11
682	Copertura	132	0	-1051.77	-0.13	0.92	-0.85	934.28	208.47
			155	-1103.85	-0.13	-0.40	-0.85	611.14	208.47
			310	-1155.93	-0.13	-1.72	-0.85	288.01	208.47
683	Copertura	83	0	-1151.96	0.02	1.33	-4.83	-466.51	-207.66
			43	-1166.30	0.02	-0.73	-4.83	-377.93	-207.66
			85	-1180.63	0.02	-2.79	-4.83	-289.35	-207.66
684	Copertura	137	0	-1110.70	-0.12	0.31	-0.24	938.81	214.73
			155	-1162.78	-0.12	-0.07	-0.24	605.97	214.73
			310	-1214.86	-0.12	-0.45	-0.24	273.13	214.73
685	Copertura	84	0	-1202.42	-0.04	-1.24	2.85	-457.14	-214.85
			43	-1216.75	-0.04	-0.02	2.85	-365.49	-214.85
			85	-1231.08	-0.04	1.20	2.85	-273.85	-214.85
686	Copertura	140	0	-1172.45	-0.01	0.01	0.14	940.14	216.97
			155	-1224.53	-0.01	0.23	0.14	603.84	216.97
			310	-1276.61	-0.01	0.46	0.14	267.54	216.97
687	Copertura	85	0	-1258.64	0.02	2.90	-5.16	-453.29	-216.88
			43	-1272.97	0.02	0.70	-5.16	-360.78	-216.88
			85	-1287.30	0.02	-1.50	-5.16	-268.27	-216.88
688	Copertura	144	0	-1266.16	-0.02	0.02	0.07	941.40	217.30
			155	-1318.24	-0.02	0.12	0.07	604.59	217.30
			310	-1370.32	-0.02	0.22	0.07	267.77	217.30
689	Copertura	86	0	-1297.46	0.02	-2.54	3.12	-453.90	-216.60
			43	-1311.79	0.02	-1.21	3.12	-361.51	-216.60
			85	-1326.13	0.02	0.13	3.12	-269.11	-216.60
690	Copertura	87	0	-1269.49	-0.07	3.95	-11.79	-453.82	-216.55
			43	-1283.82	-0.07	-1.08	-11.79	-361.45	-216.55
			85	-1298.16	-0.07	-6.11	-11.79	-269.08	-216.55
691	Copertura	148	0	-1237.97	0.05	-7.83	3.99	941.11	217.19
			155	-1290.05	0.05	-1.65	3.99	604.46	217.19
			310	-1342.13	0.05	4.54	3.99	267.81	217.19
692	Copertura	88	0	-1201.62	0.04	-4.03	1.92	-454.18	-216.16
			43	-1215.96	0.04	-3.22	1.92	-361.98	-216.16
			85	-1230.29	0.04	-2.40	1.92	-269.77	-216.16
693	Copertura	152	0	-1124.73	0.03	-10.66	5.52	939.64	216.37
			155	-1176.81	0.03	-2.10	5.52	604.27	216.37
			310	-1228.89	0.03	6.45	5.52	268.90	216.37
694	Copertura	89	0	-1197.96	-0.05	2.54	-12.38	-454.26	-216.17
			43	-1212.29	-0.05	-2.74	-12.38	-362.06	-216.17
			85	-1226.63	-0.05	-8.02	-12.38	-269.85	-216.17
695	Copertura	156	0	-1105.70	0.02	-11.75	6.27	939.63	216.24
			155	-1157.78	0.02	-2.03	6.27	604.46	216.24
			310	-1209.86	0.02	7.69	6.27	269.29	216.24
696	Copertura	90	0	-1186.24	0.02	-2.24	-3.81	-454.19	-216.10
			43	-1200.57	0.02	-3.87	-3.81	-362.01	-216.10
			85	-1214.91	0.02	-5.50	-3.81	-269.83	-216.10
697	Copertura	160	0	-1119.31	0.03	-13.09	7.05	940.11	216.34
			155	-1171.39	0.03	-2.17	7.05	604.79	216.34
			310	-1223.47	0.03	8.76	7.05	269.46	216.34
698	Copertura	91	0	-1198.11	-0.04	2.15	-12.74	-454.16	-216.04
			43	-1212.44	-0.04	-3.28	-12.74	-362.00	-216.04
			85	-1226.77	-0.04	-8.72	-12.74	-269.85	-216.04
699	Copertura	164	0	-1130.98	0.04	-14.44	7.82	940.54	216.38
			155	-1183.06	0.04	-2.33	7.82	605.15	216.38
			310	-1235.14	0.04	9.79	7.82	269.76	216.38
700	Copertura	92	0	-1198.10	0.01	-1.77	-5.44	-454.30	-215.92
			43	-1212.43	0.01	-4.09	-5.44	-362.19	-215.92
			85	-1226.77	0.01	-6.41	-5.44	-270.09	-215.92
701	Copertura	168	0	-1128.85	0.06	-15.77	8.55	940.43	216.04
			155	-1180.93	0.06	-2.52	8.55	605.56	216.04
			310	-1233.01	0.06	10.73	8.55	270.69	216.04
702	Copertura	93	0	-1216.51	-0.05	-1.44	-4.81	-454.62	-215.85
			43	-1230.84	-0.05	-3.49	-4.81	-362.55	-215.85
			85	-1245.17	-0.05	-5.54	-4.81	-270.47	-215.85
703	Copertura	172	0	-1100.20	0.07	-16.85	9.12	939.50	215.25
			155	-1152.28	0.07	-2.72	9.12	605.87	215.25
			310	-1204.36	0.07	11.42	9.12	272.24	215.25
704	Copertura	94	0	-1214.72	0.03	1.64	-8.21	-454.43	-216.05

			43	-1229.05	0.03	-1.86	-8.21	-362.27	-216.05
			85	-1243.39	0.03	-5.37	-8.21	-270.11	-216.05
705	Copertura	176	0	-1089.01	0.03	-18.16	10.07	938.45	215.20
			155	-1141.09	0.03	-2.55	10.07	604.89	215.20
			310	-1193.17	0.03	13.06	10.07	271.33	215.20
706	Copertura	180	0	-1114.87	-0.03	-0.06	0.19	938.35	214.67
			155	-1166.95	-0.03	0.23	0.19	605.61	214.67
			310	-1219.03	-0.03	0.52	0.19	272.88	214.67
707	Copertura	95	0	-1310.10	0.05	-2.42	2.65	-454.88	-215.79
			43	-1324.43	0.05	-1.29	2.65	-362.83	-215.79
			85	-1338.77	0.05	-0.16	2.65	-270.78	-215.79
708	Copertura	184	0	-1146.52	-0.02	-0.06	0.08	939.09	215.46
			155	-1198.60	-0.02	0.07	0.08	605.13	215.46
			310	-1250.68	-0.02	0.20	0.08	271.16	215.46
709	Copertura	96	0	-1284.02	-0.05	2.93	-10.07	-453.45	-216.10
			43	-1298.35	-0.05	-1.37	-10.07	-361.27	-216.10
			85	-1312.69	-0.05	-5.66	-10.07	-269.09	-216.10
710	Copertura	188	0	-1146.97	-0.02	-0.25	0.24	940.20	216.21
			155	-1199.05	-0.02	0.12	0.24	605.08	216.21
			310	-1251.13	-0.02	0.49	0.24	269.96	216.21
711	Copertura	97	0	-1233.39	0.13	0.67	-1.41	-453.53	-215.85
			43	-1247.73	0.13	0.07	-1.41	-361.46	-215.85
			85	-1262.06	0.13	-0.54	-1.41	-269.39	-215.85
712	Copertura	192	0	-1120.94	0.12	-0.64	0.64	939.66	214.75
			155	-1173.02	0.12	0.36	0.64	606.79	214.75
			310	-1225.10	0.12	1.36	0.64	273.93	214.75
713	Copertura	106	0	-1203.55	-0.19	-0.72	2.30	-456.98	-214.02
			43	-1217.88	-0.19	0.26	2.30	-365.69	-214.02
			85	-1232.22	-0.19	1.24	2.30	-274.39	-214.02
714	Copertura	196	0	-1088.57	0.14	-1.25	1.21	935.16	208.67
			155	-1140.65	0.14	0.62	1.21	611.72	208.67
			310	-1192.73	0.14	2.49	1.21	288.28	208.67
715	Copertura	107	0	-1119.76	-0.71	1.31	-0.50	-466.59	-208.43
			43	-1134.10	-0.71	1.10	-0.50	-377.68	-208.43
			85	-1148.43	-0.71	0.89	-0.50	-288.77	-208.43
716	Copertura	200	0	-975.45	-0.87	-1.95	1.92	929.92	210.70
			155	-1027.53	-0.87	1.02	1.92	603.33	210.70
			310	-1079.61	-0.87	4.00	1.92	276.73	210.70
717	Copertura	108	0	-1050.89	1.74	-0.69	9.12	-454.46	-209.43
			43	-1065.22	1.74	3.20	9.12	-365.12	-209.43
			85	-1079.55	1.74	7.09	9.12	-275.79	-209.43
718	Copertura	204	0	-877.24	-4.66	-2.51	2.67	952.36	282.46
			155	-929.32	-4.66	1.63	2.67	514.55	282.46
			310	-981.40	-4.66	5.77	2.67	76.74	282.46
719	Copertura	109	0	-984.95	-7.08	1.44	6.97	-304.23	-264.84
			43	-999.28	-7.08	4.42	6.97	-191.26	-264.84
			85	-1013.61	-7.08	7.39	6.97	-78.29	-264.84
720	Copertura	110	0	-616.68	-12.28	4.66	9.22	-16.17	-12.23
			43	-636.39	-12.28	8.59	9.22	-10.96	-12.23
			85	-656.09	-12.28	12.53	9.22	-5.74	-12.23
721	Copertura	14	0	-426.64	-23.47	18.31	-11.34	46.59	29.96
			95	-470.53	-23.47	7.54	-11.34	18.14	29.96
			190	-514.42	-23.47	-3.24	-11.34	-10.32	29.96
722	Copertura	15	0	130.68	2.03	4.45	-0.08	-69.68	-728.09
			65	108.84	2.03	4.41	-0.08	403.58	-728.09
			130	87.00	2.03	4.36	-0.08	876.85	-728.09
723	Copertura	16	0	137.07	-7.84	0.59	6.20	63.58	722.70
			65	115.23	-7.84	4.62	6.20	-406.17	722.70
			130	93.39	-7.84	8.66	6.20	-875.93	722.70
724	Copertura	17	0	-38.41	0.42	3.53	-1.17	-66.38	-710.03
			65	-60.25	0.42	2.77	-1.17	395.14	-710.03
			130	-82.09	0.42	2.01	-1.17	856.66	-710.03
725	Copertura	18	0	-39.39	-0.47	4.54	-2.97	66.39	709.85
			65	-61.23	-0.47	2.61	-2.97	-395.02	709.85
			130	-83.07	-0.47	0.68	-2.97	-856.42	709.85
726	Copertura	19	0	-131.47	-0.02	1.96	-0.89	-66.94	-713.68
			65	-153.31	-0.02	1.38	-0.89	396.95	-713.68
			130	-175.15	-0.02	0.81	-0.89	860.84	-713.68
727	Copertura	20	0	-146.74	-0.06	1.89	-1.26	67.58	713.73
			65	-168.58	-0.06	1.07	-1.26	-396.34	713.73
			130	-190.42	-0.06	0.25	-1.26	-860.27	713.73
728	Copertura	21	0	-181.60	-0.04	0.61	-0.29	-67.27	-717.08

			65	-203.44	-0.04	0.42	-0.29	398.83	-717.08
			130	-225.28	-0.04	0.23	-0.29	864.93	-717.08
729	Copertura	22	0	-186.07	0.06	0.24	-0.25	67.47	717.25
			65	-207.91	0.06	0.08	-0.25	-398.74	717.25
			130	-229.75	0.06	-0.08	-0.25	-864.96	717.25
730	Copertura	23	0	-239.43	0.00	-0.18	0.14	-68.79	-719.16
			65	-261.27	0.00	-0.09	0.14	398.67	-719.16
			130	-283.11	0.00	0.00	0.14	866.12	-719.16
731	Copertura	24	0	-234.74	0.03	-1.06	0.94	68.73	719.36
			65	-256.58	0.03	-0.45	0.94	-398.86	719.36
			130	-278.42	0.03	0.16	0.94	-866.44	719.36
732	Copertura	25	0	-329.99	-0.01	-0.07	0.06	-71.56	-722.15
			65	-351.83	-0.01	-0.03	0.06	397.84	-722.15
			130	-373.67	-0.01	0.01	0.06	867.24	-722.15
733	Copertura	26	0	-274.87	0.00	-4.66	4.29	69.99	720.46
			65	-296.71	0.00	-1.88	4.29	-398.31	720.46
			130	-318.55	0.00	0.91	4.29	-866.61	720.46
734	Copertura	27	0	-241.91	-0.04	-8.24	10.43	68.17	718.86
			65	-263.75	-0.04	-1.46	10.43	-399.09	718.86
			130	-285.59	-0.04	5.31	10.43	-866.35	718.86
735	Copertura	28	0	-303.46	-0.03	13.14	-14.95	-69.30	-720.22
			65	-325.30	-0.03	3.42	-14.95	398.84	-720.22
			130	-347.14	-0.03	-6.29	-14.95	866.98	-720.22
736	Copertura	29	0	-185.71	-0.05	-15.88	18.80	65.02	716.14
			65	-207.55	-0.05	-3.66	18.80	-400.46	716.14
			130	-229.39	-0.05	8.56	18.80	-865.95	716.14
737	Copertura	30	0	-194.91	-0.06	17.76	-20.26	-64.87	-715.81
			65	-216.75	-0.06	4.59	-20.26	400.41	-715.81
			130	-238.59	-0.06	-8.58	-20.26	865.69	-715.81
738	Copertura	31	0	-172.69	-0.06	-16.56	19.86	64.35	715.63
			65	-194.53	-0.06	-3.65	19.86	-400.81	715.63
			130	-216.37	-0.06	9.26	19.86	-865.97	715.63
739	Copertura	32	0	-176.62	-0.07	19.11	-21.98	-63.87	-715.04
			65	-198.46	-0.07	4.82	-21.98	400.91	-715.04
			130	-220.30	-0.07	-9.47	-21.98	865.69	-715.04
740	Copertura	33	0	-174.15	-0.06	-19.55	22.88	63.41	714.73
			65	-195.99	-0.06	-4.68	22.88	-401.16	714.73
			130	-217.83	-0.06	10.19	22.88	-865.73	714.73
741	Copertura	34	0	-189.85	-0.08	20.88	-24.19	-63.64	-715.20
			65	-211.69	-0.08	5.16	-24.19	401.24	-715.20
			130	-233.53	-0.08	-10.56	-24.19	866.12	-715.20
742	Copertura	35	0	-173.15	-0.07	-20.76	24.63	62.88	714.27
			65	-194.99	-0.07	-4.75	24.63	-401.39	714.27
			130	-216.83	-0.07	11.26	24.63	-865.66	714.27
743	Copertura	36	0	-201.29	-0.09	22.66	-26.40	-63.31	-715.24
			65	-223.13	-0.09	5.50	-26.40	401.59	-715.24
			130	-244.97	-0.09	-11.66	-26.40	866.50	-715.24
744	Copertura	37	0	-187.91	-0.07	-22.79	26.68	62.39	713.79
			65	-209.75	-0.07	-5.45	26.68	-401.57	713.79
			130	-231.59	-0.07	11.89	26.68	-865.53	713.79
745	Copertura	38	0	-199.92	-0.09	24.44	-28.60	-62.54	-714.57
			65	-221.76	-0.09	5.85	-28.60	401.93	-714.57
			130	-243.60	-0.09	-12.74	-28.60	866.40	-714.57
746	Copertura	39	0	-193.85	-0.08	-24.19	28.93	62.10	713.57
			65	-215.69	-0.08	-5.38	28.93	-401.73	713.57
			130	-237.53	-0.08	13.42	28.93	-865.55	713.57
747	Copertura	40	0	-173.48	-0.09	25.89	-30.39	-61.14	-712.84
			65	-195.32	-0.09	6.14	-30.39	402.21	-712.84
			130	-217.16	-0.09	-13.61	-30.39	865.55	-712.84
748	Copertura	41	0	-202.11	-0.03	-16.45	20.81	63.92	715.31
			65	-223.95	-0.03	-2.92	20.81	-401.02	715.31
			130	-245.79	-0.03	10.61	20.81	-865.97	715.31
749	Copertura	42	0	-163.63	-0.11	27.38	-32.36	-60.13	-711.31
			65	-185.47	-0.11	6.34	-32.36	402.23	-711.31
			130	-207.31	-0.11	-14.70	-32.36	864.58	-711.31
750	Copertura	43	0	-186.13	-0.02	-0.30	0.17	-67.26	-716.74
			65	-207.97	-0.02	-0.18	0.17	398.62	-716.74
			130	-229.81	-0.02	-0.07	0.17	864.50	-716.74
751	Copertura	44	0	-284.56	-0.01	-10.17	10.57	70.23	719.92
			65	-306.40	-0.01	-3.30	10.57	-397.72	719.92
			130	-328.24	-0.01	3.58	10.57	-865.66	719.92
752	Copertura	45	0	-215.90	-0.01	-0.17	0.08	-68.25	-718.02

			65	-237.74	-0.01	-0.12	0.08	398.47	-718.02
			130	-259.58	-0.01	-0.07	0.08	865.18	-718.02
753	Copertura	46	0	-266.69	0.02	-0.14	-0.37	69.55	718.93
			65	-288.53	0.02	-0.38	-0.37	-397.75	718.93
			130	-310.37	0.02	-0.62	-0.37	-865.05	718.93
754	Copertura	47	0	-214.97	-0.01	-0.54	0.23	-68.21	-718.79
			65	-236.81	-0.01	-0.39	0.23	399.00	-718.79
			130	-258.65	-0.01	-0.24	0.23	866.21	-718.79
755	Copertura	48	0	-213.53	0.00	-1.64	1.71	67.98	717.38
			65	-235.37	0.00	-0.53	1.71	-398.32	717.38
			130	-257.21	0.00	0.59	1.71	-864.62	717.38
756	Copertura	49	0	-190.96	0.03	-1.44	0.69	-67.65	-717.98
			65	-212.80	0.03	-0.99	0.69	399.04	-717.98
			130	-234.64	0.03	-0.54	0.69	865.72	-717.98
757	Copertura	50	0	-189.92	-0.08	-1.81	1.33	67.53	716.39
			65	-211.76	-0.08	-0.95	1.33	-398.13	716.39
			130	-233.60	-0.08	-0.08	1.33	-863.78	716.39
758	Copertura	51	0	-166.71	0.02	-2.73	1.24	-68.04	-715.13
			65	-188.55	0.02	-1.92	1.24	396.80	-715.13
			130	-210.39	0.02	-1.11	1.24	861.63	-715.13
759	Copertura	52	0	-114.34	-0.05	-4.28	3.26	66.30	711.64
			65	-136.18	-0.05	-2.16	3.26	-396.27	711.64
			130	-158.02	-0.05	-0.04	3.26	-858.83	711.64
760	Copertura	53	0	-56.55	-0.42	-4.11	1.43	-66.96	-710.78
			65	-78.39	-0.42	-3.18	1.43	395.04	-710.78
			130	-100.23	-0.42	-2.25	1.43	857.05	-710.78
761	Copertura	54	0	-49.19	1.32	-5.35	2.81	66.47	709.75
			65	-71.03	1.32	-3.53	2.81	-394.87	709.75
			130	-92.87	1.32	-1.70	2.81	-856.20	709.75
762	Copertura	55	0	118.99	-2.01	-4.89	0.24	-70.21	-729.99
			65	97.15	-2.01	-4.74	0.24	404.29	-729.99
			130	75.31	-2.01	-4.59	0.24	878.78	-729.99
763	Copertura	56	0	114.44	2.71	-7.71	3.71	69.18	731.80
			65	92.60	2.71	-5.30	3.71	-406.49	731.80
			130	70.76	2.71	-2.89	3.71	-882.16	731.80
764	Copertura	70	0	-436.25	12.28	-20.87	9.61	31.92	13.77
			95	-480.14	12.28	-11.73	9.61	18.84	13.77
			190	-524.03	12.28	-2.60	9.61	5.76	13.77
765	Copertura	81	0	-891.68	5.15	4.15	-6.07	-764.37	-274.31
			80	-918.56	5.15	-0.71	-6.07	-544.92	-274.31
			160	-945.44	5.15	-5.57	-6.07	-325.47	-274.31
766	Copertura	126	0	-874.14	-18.99	-0.37	-3.57	-949.57	-307.25
			30	-884.22	-18.99	-1.44	-3.57	-857.39	-307.25
			60	-894.30	-18.99	-2.51	-3.57	-765.22	-307.25
767	Copertura	98	0	-989.81	-2.82	2.75	-3.80	-802.45	-210.44
			82	-1017.48	-2.82	-0.37	-3.80	-629.17	-210.44
			165	-1045.15	-2.82	-3.50	-3.80	-455.88	-210.44
768	Copertura	99	0	-1088.42	0.39	0.94	-1.17	-809.29	-208.13
			82	-1116.09	0.39	-0.03	-1.17	-637.91	-208.13
			165	-1143.75	0.39	-0.99	-1.17	-466.53	-208.13
769	Copertura	100	0	-1141.32	0.22	0.80	-0.81	-810.18	-214.38
			82	-1168.99	0.22	0.13	-0.81	-633.65	-214.38
			165	-1196.66	0.22	-0.53	-0.81	-457.13	-214.38
770	Copertura	101	0	-1195.83	-0.02	-1.26	1.64	-810.39	-216.84
			82	-1223.49	-0.02	0.08	1.64	-631.84	-216.84
			165	-1251.16	-0.02	1.43	1.64	-453.29	-216.84
771	Copertura	102	0	-1235.63	0.00	4.33	-3.67	-810.69	-216.64
			82	-1263.30	0.00	1.31	-3.67	-632.29	-216.64
			165	-1290.97	0.00	-1.72	-3.67	-453.90	-216.64
772	Copertura	103	0	-1202.01	-0.01	0.42	-0.53	-810.45	-216.55
			82	-1229.68	-0.01	-0.02	-0.53	-632.14	-216.55
			165	-1257.34	-0.01	-0.46	-0.53	-453.82	-216.55
773	Copertura	104	0	-1144.46	-0.01	8.95	-9.34	-810.17	-216.16
			82	-1172.13	-0.01	1.26	-9.34	-632.18	-216.16
			165	-1199.80	-0.01	-6.43	-9.34	-454.19	-216.16
774	Copertura	105	0	-1127.71	0.00	6.13	-6.12	-810.29	-216.18
			82	-1155.37	0.00	1.09	-6.12	-632.28	-216.18
			165	-1183.04	0.00	-3.94	-6.12	-454.26	-216.18
775	Copertura	111	0	-1133.59	0.00	9.84	-10.08	-798.89	-216.08
			80	-1160.39	0.00	1.80	-10.08	-626.54	-216.08
			160	-1187.19	0.00	-6.24	-10.08	-454.19	-216.08
776	Copertura	112	0	-1126.96	-0.01	7.92	-7.83	-809.97	-216.05

			82	-1154.63	-0.01	1.48	-7.83	-632.06	-216.05
			165	-1182.30	-0.01	-4.97	-7.83	-454.15	-216.05
777	Copertura	113	0	-1144.60	0.00	10.76	-10.35	-809.87	-215.91
			82	-1172.27	0.00	2.23	-10.35	-632.08	-215.91
			165	-1199.94	0.00	-6.29	-10.35	-454.30	-215.91
778	Copertura	114	0	-1147.42	-0.02	10.02	-10.78	-810.10	-215.85
			82	-1175.09	-0.02	1.14	-10.78	-632.36	-215.85
			165	-1202.76	-0.02	-7.73	-10.78	-454.62	-215.85
779	Copertura	115	0	-1159.17	-0.01	2.70	-2.24	-810.25	-216.06
			82	-1186.83	-0.01	0.85	-2.24	-632.34	-216.06
			165	-1214.50	-0.01	-1.00	-2.24	-454.43	-216.06
780	Copertura	116	0	-1244.31	0.00	8.33	-8.97	-810.28	-215.80
			82	-1271.98	0.00	0.94	-8.97	-632.58	-215.80
			165	-1299.65	0.00	-6.44	-8.97	-454.88	-215.80
781	Copertura	117	0	-1225.17	0.01	-0.17	1.54	-809.33	-216.09
			82	-1252.84	0.01	1.10	1.54	-631.39	-216.09
			165	-1280.50	0.01	2.38	1.54	-453.45	-216.09
782	Copertura	118	0	-1171.77	-0.04	-0.05	-0.15	-809.01	-215.85
			82	-1199.44	-0.04	-0.17	-0.15	-631.27	-215.85
			165	-1227.11	-0.04	-0.30	-0.15	-453.53	-215.85
783	Copertura	131	0	-957.94	-1.09	0.22	-3.61	-929.22	-211.35
			30	-968.02	-1.09	-0.86	-3.61	-865.82	-211.35
			60	-978.10	-1.09	-1.95	-3.61	-802.41	-211.35
784	Copertura	133	0	-1066.00	-0.13	0.22	-1.36	-933.66	-207.22
			30	-1076.08	-0.13	-0.19	-1.36	-871.50	-207.22
			60	-1086.16	-0.13	-0.60	-1.36	-809.33	-207.22
785	Copertura	139	0	-1115.03	0.15	-0.01	-0.18	-938.83	-214.39
			30	-1125.11	0.15	-0.07	-0.18	-874.51	-214.39
			60	-1135.19	0.15	-0.12	-0.18	-810.19	-214.39
786	Copertura	143	0	-1167.82	0.07	0.18	1.00	-940.47	-216.82
			30	-1177.90	0.07	0.49	1.00	-875.43	-216.82
			60	-1187.98	0.07	0.79	1.00	-810.38	-216.82
787	Copertura	147	0	-1208.85	0.00	0.89	4.40	-940.68	-216.65
			30	-1218.93	0.00	2.21	4.40	-875.68	-216.65
			60	-1229.01	0.00	3.53	4.40	-810.69	-216.65
788	Copertura	151	0	-1174.51	0.00	6.85	-8.61	-940.38	-216.54
			30	-1184.59	0.00	4.27	-8.61	-875.42	-216.54
			60	-1194.67	0.00	1.69	-8.61	-810.45	-216.54
789	Copertura	155	0	-1115.72	0.07	10.68	-7.02	-939.92	-216.26
			30	-1125.80	0.07	8.57	-7.02	-875.04	-216.26
			60	-1135.88	0.07	6.47	-7.02	-810.17	-216.26
790	Copertura	159	0	-1102.15	0.06	11.58	-8.44	-939.94	-216.08
			30	-1112.23	0.06	9.05	-8.44	-875.11	-216.08
			60	-1122.31	0.06	6.51	-8.44	-810.29	-216.08
791	Copertura	119	0	-1140.53	-0.01	-0.54	1.04	-809.44	-214.02
			82	-1168.20	-0.01	0.31	1.04	-633.21	-214.02
			165	-1195.87	-0.01	1.17	1.04	-456.98	-214.02
792	Copertura	120	0	-1062.98	0.21	-2.38	3.48	-807.58	-207.05
			82	-1090.65	0.21	0.48	3.48	-637.09	-207.05
			165	-1118.32	0.21	3.35	3.48	-466.60	-207.05
793	Copertura	121	0	-983.03	-1.01	-3.88	5.14	-801.63	-210.82
			82	-1010.69	-1.01	0.35	5.14	-628.04	-210.82
			165	-1038.36	-1.01	4.58	5.14	-454.45	-210.82
794	Copertura	122	0	-929.34	9.70	-5.02	6.58	-782.46	-290.84
			82	-957.01	9.70	0.40	6.58	-542.97	-290.84
			165	-984.68	9.70	5.82	6.58	-303.48	-290.84
795	Copertura	123	0	-524.03	12.28	-2.60	9.61	5.76	13.77
			82	-562.08	12.28	5.32	9.61	-5.58	13.77
			165	-600.12	12.28	13.24	9.61	-16.92	13.77
796	Copertura	163	0	-1103.02	0.08	12.75	-8.35	-939.68	-216.20
			33	-1113.97	0.08	10.03	-8.35	-869.24	-216.20
			65	-1124.92	0.08	7.31	-8.35	-798.80	-216.20
797	Copertura	167	0	-1101.50	0.07	14.06	-9.56	-939.62	-215.93
			30	-1111.58	0.07	11.19	-9.56	-874.84	-215.93
			60	-1121.66	0.07	8.32	-9.56	-810.06	-215.93
798	Copertura	171	0	-1116.06	0.07	14.92	-10.47	-939.49	-216.04
			30	-1126.14	0.07	11.78	-10.47	-874.68	-216.04
			60	-1136.22	0.07	8.64	-10.47	-809.87	-216.04
799	Copertura	174	0	-1121.67	0.10	16.69	-10.66	-939.53	-215.72
			30	-1131.75	0.10	13.49	-10.66	-874.82	-215.72
			60	-1141.83	0.10	10.29	-10.66	-810.10	-215.72
800	Copertura	179	0	-1132.01	0.09	14.10	-22.10	-939.97	-216.20

			30	-1142.09	0.09	7.47	-22.10	-875.11	-216.20
			60	-1152.17	0.09	0.84	-22.10	-810.25	-216.20
801	Copertura	183	0	-1217.18	0.10	3.62	10.89	-939.67	-215.66
			30	-1227.26	0.10	6.89	10.89	-874.97	-215.66
			60	-1237.34	0.10	10.16	10.89	-810.28	-215.66
802	Copertura	187	0	-1198.78	0.00	-0.64	-0.37	-939.00	-216.13
			30	-1208.86	0.00	-0.75	-0.37	-874.17	-216.13
			60	-1218.94	0.00	-0.87	-0.37	-809.33	-216.13
803	Copertura	191	0	-1143.87	0.01	0.59	1.77	-938.49	-215.81
			30	-1153.95	0.01	1.12	1.77	-873.75	-215.81
			60	-1164.03	0.01	1.65	1.77	-809.01	-215.81
804	Copertura	194	0	-1117.36	-0.22	-0.21	1.26	-937.56	-213.57
			30	-1127.44	-0.22	0.16	1.26	-873.49	-213.57
			60	-1137.52	-0.22	0.54	1.26	-809.42	-213.57
805	Copertura	198	0	-1031.86	-0.17	-0.18	3.26	-932.10	-207.49
			30	-1041.94	-0.17	0.80	3.26	-869.86	-207.49
			60	-1052.02	-0.17	1.78	3.26	-807.61	-207.49
806	Copertura	203	0	-967.81	3.13	-0.28	4.53	-929.00	-211.50
			30	-977.89	3.13	1.08	4.53	-865.55	-211.50
			60	-987.97	3.13	2.43	4.53	-802.10	-211.50
807	Copertura	207	0	-890.27	6.47	0.10	7.19	-956.08	-290.15
			30	-900.35	6.47	2.25	7.19	-869.03	-290.15
			60	-910.43	6.47	4.41	7.19	-781.99	-290.15

1.1.1.2 Piastre SLU

Tabella 2.I

Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	2.175	0.820	-0.423	-566.467	-210.972	-92.091	4.015	-3.560
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	2.325	1.578	-0.688	-563.123	-195.591	-146.844	6.500	4.375
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	2.256	1.575	0.607	-510.979	-159.219	-147.695	-4.239	4.346

1.1.2 Risultati Condizioni (Carichi Permanenti - G2).

1.1.2.1 Sollecitazioni SLU

Tabella 3.I

Asta	Imp.	Fili	X [cm]	N [daN]	Sollecitazioni				
					Mt [daNm]	Mxz [daNm]	Txz [daN]	Mxy [daNm]	Txy [daN]
1	Fondazione	1, 2	0	-29.99	-80.83	-46.01	-348.09	5.32	1.77
			42	-29.96	-80.84	-149.89	-158.76	4.47	2.25
			83	-29.95	-80.84	-183.23	-7.75	3.48	2.53
2	Fondazione	1, 2	0	-27.22	-110.16	-276.10	157.57	3.45	-3.99

	ne								
			42	-27.22	-110.17	-184.87	276.64	5.08	-3.89
			83	-27.23	-110.18	-49.46	371.33	6.70	-3.92
3	Fondazio ne	1, 15	0	54.31	133.40	-89.21	-217.11	7.94	13.64
			40	53.76	133.42	-135.91	-19.42	2.52	13.60
			80	53.24	133.44	-104.94	174.42	-2.85	13.38
4	Fondazio ne	1, 15	0	61.62	298.18	-247.33	278.46	-2.88	-14.24
			40	61.12	298.20	-98.02	472.89	2.86	-14.65
			80	60.66	298.23	129.51	672.49	8.80	-15.25
5	Fondazio ne	2, 3	0	-70.30	-83.30	-115.18	-109.01	5.32	7.16
			35	-70.34	-83.31	-141.43	-45.23	2.86	7.06
			69	-70.40	-83.32	-147.52	8.36	0.45	6.91
6	Fondazio ne	2, 3	0	-44.74	-52.27	-196.33	225.98	0.45	-2.27
			35	-44.83	-52.28	-110.17	272.44	1.26	-2.46
			69	-44.93	-52.29	-8.78	314.66	2.15	-2.68
7	Fondazio ne	3, 4	0	-26.17	-40.67	-36.62	-98.80	1.80	2.35
			35	-26.29	-40.68	-63.81	-59.40	1.03	2.10
			69	-26.42	-40.69	-77.75	-21.76	0.35	1.83
8	Fondazio ne	3, 4	0	-10.76	-19.04	-90.59	141.54	0.35	-0.34
			35	-10.90	-19.06	-35.31	178.86	0.51	-0.63
			69	-11.04	-19.07	32.98	217.04	0.78	-0.93
9	Fondazio ne	4, 5	0	1.29	-6.35	26.89	-136.82	0.64	0.78
			35	1.14	-6.36	-13.55	-97.63	0.42	0.47
			69	1.00	-6.37	-40.31	-57.47	0.32	0.14
10	Fondazio ne	4, 5	0	9.96	-2.05	-39.69	83.27	0.32	0.26
			35	9.82	-2.07	-3.81	124.89	0.28	-0.07
			69	9.68	-2.08	46.75	168.39	0.37	-0.41
11	Fondazio ne	5, 6	0	15.59	1.71	48.07	-151.69	0.33	0.18
			35	15.45	1.70	3.49	-106.67	0.33	-0.16
			69	15.33	1.69	-25.36	-60.55	0.45	-0.51
12	Fondazio ne	5, 6	0	17.68	0.69	-22.68	70.43	0.45	0.80
			35	17.57	0.68	9.77	117.83	0.23	0.45
			69	17.45	0.67	58.82	166.59	0.14	0.09
13	Fondazio ne	6, 7	0	53.76	4.41	61.33	-174.14	0.19	1.08
			35	53.66	4.40	9.81	-124.61	-0.12	0.73
			69	53.58	4.39	-24.60	-74.92	-0.31	0.37
14	Fondazio ne	6, 7	0	55.05	3.50	-21.80	55.01	-0.31	-0.36
			35	55.00	3.49	5.80	104.95	-0.12	-0.71
			69	54.96	3.48	50.68	155.27	0.18	-1.06
15	Fondazio ne	7, 8	0	25.38	6.48	51.68	-171.65	0.13	0.01
			35	25.36	6.47	1.15	-121.42	0.19	-0.35
			69	25.35	6.46	-32.16	-71.73	0.37	-0.70
16	Fondazio ne	7, 8	0	26.74	0.62	-36.00	56.51	0.37	0.38
			35	26.74	0.60	-7.97	105.96	0.30	0.02
			69	26.75	0.59	37.13	155.56	0.36	-0.34
17	Fondazio ne	8, 9	0	25.61	-2.66	35.10	-140.85	0.36	0.49
			35	25.63	-2.67	-4.94	-91.30	0.25	0.13
			69	25.66	-2.68	-27.94	-42.02	0.26	-0.22
18	Fondazio ne	8, 9	0	21.46	-9.74	-33.97	82.65	0.27	0.28
			35	21.50	-9.75	3.04	131.97	0.23	-0.06
			69	21.55	-9.76	57.11	181.59	0.31	-0.40
19	Fondazio ne	9, 10	0	48.84	-8.76	54.13	-147.50	0.35	1.16
			35	48.90	-8.77	11.78	-98.09	0.00	0.83
			69	48.98	-8.78	-13.67	-49.46	-0.23	0.51
20	Fondazio ne	9, 10	0	44.37	-6.67	-19.62	73.02	-0.23	-0.11

			35	44.47	-6.68	13.83	120.86	-0.13	-0.42
			69	44.59	-6.69	63.64	167.91	0.06	-0.73
21	Fondazio ne	10, 11	0	0.54	3.61	65.99	-191.94	0.04	-0.64
			35	0.67	3.59	7.66	-146.37	0.31	-0.94
			69	0.80	3.58	-35.30	-102.91	0.69	-1.24
22	Fondazio ne	10, 11	0	-5.72	10.62	-34.10	39.17	0.69	0.22
			35	-5.59	10.60	-13.39	80.75	0.67	-0.06
			69	-5.47	10.59	21.41	120.90	0.73	-0.33
23	Fondazio ne	11, 12	0	-16.85	20.55	31.24	-223.39	0.88	1.04
			35	-16.73	20.54	-39.13	-184.69	0.57	0.78
			69	-16.62	20.52	-96.38	-147.21	0.34	0.55
24	Fondazio ne	11, 12	0	-32.28	38.19	-81.58	10.67	0.34	-2.26
			35	-32.17	38.18	-71.47	48.19	1.16	-2.47
			69	-32.08	38.17	-48.18	87.34	2.04	-2.66
25	Fondazio ne	12, 13	0	-51.85	50.09	-20.71	-292.17	2.39	2.92
			35	-51.78	50.08	-114.38	-250.17	1.41	2.76
			69	-51.72	50.07	-192.86	-203.74	0.48	2.65
26	Fondazio ne	12, 13	0	-78.27	91.02	-150.04	-12.11	0.49	-7.06
			35	-78.24	91.01	-145.21	41.69	2.94	-7.13
			69	-78.24	91.01	-120.10	105.96	5.40	-7.15
27	Fondazio ne	13, 14	0	-29.24	104.18	-52.18	-357.46	6.78	3.27
			42	-29.27	104.17	-181.63	-261.70	5.41	3.34
			83	-29.31	104.17	-266.32	-141.06	3.98	3.57
28	Fondazio ne	13, 14	0	-34.96	78.43	-159.44	-28.43	4.01	-2.09
			42	-35.03	78.43	-140.75	124.38	4.79	-1.67
			83	-35.11	78.42	-50.81	315.28	5.36	-1.03
29	Fondazio ne	14, 16	0	62.69	-137.18	-85.43	-232.94	-8.35	-13.19
			40	61.97	-137.20	-138.16	-34.20	-3.10	-13.20
			80	61.29	-137.22	-112.92	160.16	2.12	-13.01
30	Fondazio ne	14, 16	0	64.02	-287.60	-233.60	231.37	2.15	13.13
			40	63.38	-287.62	-102.94	425.86	-3.13	13.51
			80	62.76	-287.65	105.86	625.07	-8.61	14.09
31	Fondazio ne	15, 17	0	46.61	110.22	-10.29	-216.68	14.34	43.52
			33	46.25	110.24	-53.80	-46.78	0.08	42.92
			66	45.90	110.27	-40.55	127.50	-13.97	42.23
32	Fondazio ne	15, 17	0	44.99	312.05	-166.45	410.52	-13.99	-54.33
			33	44.67	312.08	-1.43	590.34	4.06	-55.12
			66	44.35	312.11	224.02	776.74	22.40	-56.02
33	Fondazio ne	16, 18	0	49.85	-116.86	-14.85	-207.72	-14.05	-42.07
			33	49.36	-116.88	-55.46	-38.27	-0.26	-41.47
			66	48.90	-116.91	-39.45	135.57	13.31	-40.79
34	Fondazio ne	16, 18	0	50.80	-307.56	-152.73	355.67	13.34	51.71
			33	50.35	-307.58	-5.85	535.03	-3.86	52.50
			66	49.92	-307.61	201.29	720.94	-21.33	53.40
35	Fondazio ne	17, 19	0	104.53	-38.46	125.39	-448.91	25.85	66.89
			33	104.24	-38.43	8.79	-257.32	3.94	65.92
			66	104.00	-38.40	-43.91	-61.72	-17.65	64.94
36	Fondazio ne	17, 19	0	90.00	216.28	-90.53	234.91	-17.66	-60.25
			33	89.79	216.32	19.89	434.89	2.39	-61.27
			66	89.61	216.35	197.10	639.68	22.78	-62.35
37	Fondazio ne	18, 20	0	103.75	25.26	119.66	-418.53	-24.92	-64.70
			33	103.34	25.23	13.05	-227.30	-3.73	-63.73
			66	102.97	25.20	-29.76	-31.89	17.13	-62.73
38	Fondazio ne	18, 20	0	94.80	-215.41	-86.15	204.02	17.14	59.74
			33	94.46	-215.44	14.08	403.87	-2.74	60.78

			66	94.16	-215.48	181.06	608.56	-22.98	61.89
39	Fondazio ne	19, 21	0	42.86	-96.09	154.61	-501.26	20.21	59.91
			33	42.71	-96.05	23.49	-293.21	0.63	58.81
			66	42.57	-96.02	-38.65	-83.31	-18.60	57.73
40	Fondazio ne	19, 21	0	31.66	155.04	-57.57	164.99	-18.61	-56.26
			33	31.54	155.08	31.79	376.86	0.14	-57.35
			66	31.42	155.12	191.44	590.81	19.25	-58.49
41	Fondazio ne	20, 22	0	44.30	91.10	144.67	-485.48	-20.42	-60.34
			33	44.03	91.07	18.79	-277.29	-0.70	-59.21
			66	43.77	91.03	-38.01	-66.92	18.66	-58.09
42	Fondazio ne	20, 22	0	33.63	-159.96	-60.64	162.97	18.66	55.77
			33	33.38	-159.99	28.21	375.72	0.07	56.90
			66	33.15	-160.03	187.71	591.01	-18.90	58.08
43	Fondazio ne	21, 23	0	73.21	-136.17	184.03	-560.14	21.20	59.34
			33	73.11	-136.14	34.59	-345.80	1.81	58.20
			66	73.04	-136.10	-44.31	-132.75	-17.21	57.08
44	Fondazio ne	21, 23	0	61.66	110.28	-42.82	138.89	-17.21	-58.55
			33	61.61	110.31	37.99	350.66	2.30	-59.66
			66	61.59	110.35	188.50	561.12	22.17	-60.79
45	Fondazio ne	22, 24	0	75.61	125.32	177.61	-561.72	-20.87	-58.57
			33	75.40	125.29	27.96	-345.50	-1.74	-57.38
			66	75.21	125.25	-50.43	-129.94	17.00	-56.20
46	Fondazio ne	22, 24	0	63.97	-122.45	-50.05	102.24	17.00	57.19
			33	63.81	-122.49	19.21	317.29	-2.06	58.37
			66	63.68	-122.53	159.39	532.04	-21.52	59.56
47	Fondazio ne	23, 25	0	-10.47	-188.59	211.91	-711.35	19.97	55.99
			33	-10.49	-188.55	11.51	-503.96	1.68	54.88
			66	-10.50	-188.52	-121.21	-301.26	-16.26	53.83
48	Fondazio ne	23, 25	0	-32.15	47.31	-76.50	-45.22	-16.25	-32.63
			33	-32.18	47.34	-58.52	153.58	-5.31	-33.64
			66	-32.22	47.37	24.60	349.74	5.96	-34.66
49	Fondazio ne	24, 26	0	-2.85	155.08	168.20	-647.10	-19.36	-54.66
			33	-2.97	155.04	-10.08	-433.97	-1.52	-53.48
			66	-3.10	155.01	-118.48	-223.56	15.94	-52.35
50	Fondazio ne	24, 26	0	-21.55	-70.61	-105.91	8.41	15.94	30.74
			33	-21.69	-70.65	-68.64	217.15	5.61	31.84
			66	-21.83	-70.68	37.46	425.77	-5.08	32.96
51	Fondazio ne	25, 26	0	98.75	25.88	-274.14	-455.38	-2.61	-3.78
			49	97.28	25.88	-398.51	-78.13	-0.79	-3.73
			97	95.89	25.88	-368.08	184.37	1.02	-3.70
52	Fondazio ne	25, 26	0	90.54	12.17	-396.87	-98.52	1.01	1.44
			49	89.22	12.17	-399.77	71.77	0.31	1.43
			97	87.98	12.17	-337.60	172.73	-0.38	1.41
53	Fondazio ne	25, 26	0	95.71	4.82	-310.64	40.61	-0.39	-0.45
			49	94.53	4.82	-276.20	93.25	-0.16	-0.49
			97	93.43	4.82	-224.38	114.78	0.10	-0.57
54	Fondazio ne	25, 26	0	101.68	3.62	-188.29	78.68	0.09	0.04
			49	100.66	3.62	-148.22	83.13	0.10	-0.06
			97	99.72	3.62	-108.07	80.53	0.15	-0.19
55	Fondazio ne	25, 26	0	106.44	1.88	-76.18	49.88	0.15	0.08
			49	105.57	1.88	-52.45	47.31	0.14	-0.07
			97	104.79	1.88	-29.13	48.78	0.22	-0.24
56	Fondazio ne	25, 26	0	109.55	1.01	-11.05	12.26	0.21	0.17
			49	108.86	1.01	-3.34	19.98	0.17	-0.02
			97	108.24	1.01	9.77	34.57	0.23	-0.23

57	Fondazio ne	25, 26	0	111.29	0.75	17.59	-16.83	0.23	0.21
			49	110.77	0.75	14.42	4.45	0.18	-0.01
			97	110.33	0.75	23.06	31.62	0.24	-0.25
58	Fondazio ne	25, 26	0	112.15	0.50	25.02	-33.95	0.24	0.28
			49	111.80	0.50	16.18	-1.90	0.17	0.03
			97	111.54	0.50	23.90	33.94	0.21	-0.22
59	Fondazio ne	25, 26	0	112.57	0.40	23.56	-40.68	0.21	0.17
			49	112.39	0.40	13.09	-2.10	0.19	-0.09
			97	112.31	0.40	21.85	38.25	0.29	-0.34
60	Fondazio ne	25, 26	0	113.19	-0.65	21.51	-40.98	0.29	0.37
			49	113.19	-0.64	11.58	0.24	0.18	0.11
			97	113.28	-0.64	21.73	41.46	0.19	-0.15
61	Fondazio ne	25, 26	0	113.38	0.01	21.91	-37.48	0.19	0.20
			49	113.56	0.01	13.50	2.88	0.15	-0.05
			97	113.82	0.01	24.34	41.46	0.23	-0.29
62	Fondazio ne	25, 26	0	113.57	-0.42	24.90	-33.24	0.24	0.23
			49	113.93	-0.42	17.50	2.57	0.18	0.00
			97	114.37	-0.42	26.61	34.47	0.24	-0.22
63	Fondazio ne	25, 26	0	113.30	-0.92	24.77	-31.04	0.24	0.19
			49	113.84	-0.92	16.32	-4.21	0.20	-0.01
			97	114.46	-0.92	19.44	16.43	0.25	-0.20
64	Fondazio ne	25, 26	0	112.14	-1.70	11.70	-35.93	0.25	0.19
			49	112.86	-1.70	-2.33	-22.37	0.20	0.02
			97	113.66	-1.70	-11.57	-16.17	0.23	-0.12
65	Fondazio ne	25, 26	0	109.59	-2.33	-30.16	-51.39	0.23	0.17
			49	110.48	-2.33	-55.24	-51.93	0.18	0.05
			97	111.46	-2.33	-81.82	-56.92	0.18	-0.04
66	Fondazio ne	25, 26	0	105.39	-1.63	-112.71	-83.53	0.19	0.12
			49	106.45	-1.63	-154.97	-88.70	0.15	0.06
			97	107.60	-1.63	-198.37	-86.65	0.13	0.03
67	Fondazio ne	25, 26	0	100.07	0.40	-237.92	-127.17	0.13	0.52
			49	101.29	0.40	-296.27	-107.37	-0.12	0.53
			97	102.60	0.40	-337.73	-54.83	-0.39	0.57
68	Fondazio ne	25, 26	0	93.80	1.91	-361.33	-157.80	-0.38	-1.67
			49	95.19	1.91	-415.73	-54.04	0.42	-1.60
			97	96.64	1.91	-402.74	123.09	1.17	-1.49
69	Fondazio ne	25, 26	0	102.26	2.64	-373.27	-219.08	1.18	2.93
			49	103.80	2.64	-418.02	54.98	-0.28	3.07
			97	105.42	2.64	-301.04	449.32	-1.82	3.26
70	Fondazio ne	25, 28	0	27.33	-100.54	46.46	-488.68	11.10	33.28
			43	27.28	-100.50	-108.08	-239.21	-2.77	31.97
			85	27.25	-100.45	-157.12	8.51	-16.08	30.69
71	Fondazio ne	25, 28	0	35.02	166.38	-171.64	159.93	-16.09	-42.37
			43	35.01	166.42	-50.54	410.95	2.20	-43.71
			85	35.01	166.47	178.73	669.31	21.08	-45.15
72	Fondazio ne	26, 27	0	29.35	64.16	33.55	-427.43	-9.10	-37.34
			33	29.21	64.13	-73.00	-218.44	3.04	-36.21
			66	29.09	64.09	-110.48	-8.54	14.80	-35.08
73	Fondazio ne	26, 27	0	37.84	-164.72	-127.77	215.48	14.81	53.36
			33	37.72	-164.76	-21.68	427.94	-2.99	54.53
			66	37.62	-164.80	155.13	644.18	-21.19	55.77
74	Fondazio ne	27, 29	0	-8.12	106.49	139.72	-523.59	-19.11	-57.89
			33	-8.22	106.45	3.05	-304.43	-0.21	-56.65
			66	-8.32	106.42	-60.97	-83.38	18.28	-55.42
75	Fondazio	27, 29	0	-6.34	-145.80	-74.18	133.49	18.28	53.37

	ne								
			33	-6.44	-145.83	6.68	356.94	0.47	54.61
			66	-6.55	-145.87	161.76	583.28	-17.76	55.90
76	Fondazio ne	28, 30	0	-18.17	-96.66	170.53	-567.42	18.65	53.61
			37	-18.16	-96.62	4.69	-340.78	-0.69	52.35
			73	-18.15	-96.59	-77.95	-111.57	-19.57	51.12
77	Fondazio ne	28, 30	0	-9.20	160.96	-95.48	132.70	-19.57	-52.75
			37	-9.20	160.99	-4.72	365.36	-0.10	-53.99
			73	-9.21	161.03	171.78	602.51	19.85	-55.30
78	Fondazio ne	29, 31	0	43.69	121.25	156.66	-566.62	-19.91	-57.74
			33	43.59	121.21	7.30	-338.58	-1.07	-56.44
			66	43.51	121.17	-66.73	-110.04	17.34	-55.15
79	Fondazio ne	29, 31	0	44.67	-134.02	-73.59	98.78	17.34	55.17
			33	44.61	-134.06	-3.15	328.32	-1.08	56.46
			66	44.56	-134.10	143.31	559.47	-19.93	57.78
80	Fondazio ne	30, 32	0	-1.57	-112.91	158.75	-562.07	19.89	57.73
			34	-1.58	-112.87	4.77	-336.80	0.33	56.49
			69	-1.59	-112.84	-71.82	-110.27	-18.81	55.27
81	Fondazio ne	30, 32	0	-0.73	147.38	-87.48	154.32	-18.81	-55.23
			34	-0.74	147.42	4.42	382.75	0.31	-56.46
			69	-0.75	147.45	175.01	613.79	19.87	-57.74
82	Fondazio ne	31, 33	0	-9.09	126.29	144.63	-564.24	-17.80	-56.10
			33	-9.13	126.26	-3.31	-332.46	0.50	-54.78
			66	-9.18	126.22	-74.82	-101.01	18.36	-53.48
83	Fondazio ne	31, 33	0	-6.08	-129.75	-80.58	100.50	18.36	52.54
			33	-6.13	-129.78	-9.19	332.26	0.81	53.83
			66	-6.18	-129.82	138.85	565.07	-17.18	55.16
84	Fondazio ne	32, 34	0	2.19	-130.96	166.00	-609.81	19.89	57.93
			35	2.18	-130.92	-4.03	-375.88	0.13	56.63
			69	2.17	-130.88	-93.38	-142.06	-19.19	55.37
85	Fondazio ne	32, 34	0	0.79	145.99	-87.55	121.56	-19.19	-54.64
			35	0.78	146.03	-5.19	356.17	-0.12	-55.91
			69	0.77	146.07	158.41	592.45	19.40	-57.23
86	Fondazio ne	33, 35	0	38.63	127.83	143.32	-566.85	-19.29	-56.63
			33	38.58	127.79	-5.27	-333.88	-0.83	-55.30
			66	38.55	127.75	-77.11	-101.69	17.21	-53.99
87	Fondazio ne	33, 35	0	42.98	-126.77	-81.50	97.37	17.21	54.68
			33	42.96	-126.80	-11.08	329.48	-1.05	55.98
			66	42.96	-126.84	136.04	562.27	-19.75	57.31
88	Fondazio ne	34, 36	0	3.18	-123.65	150.50	-588.67	19.42	56.68
			35	3.18	-123.61	-11.73	-351.90	0.09	55.36
			69	3.17	-123.58	-92.39	-115.74	-18.78	54.06
89	Fondazio ne	34, 36	0	2.60	138.15	-94.51	114.41	-18.78	-53.83
			35	2.59	138.19	-14.27	350.96	0.01	-55.12
			69	2.59	138.23	147.82	588.93	19.26	-56.46
90	Fondazio ne	35, 37	0	-13.20	129.57	142.75	-562.60	-17.61	-55.89
			33	-13.19	129.53	-4.51	-329.99	0.61	-54.56
			66	-13.19	129.50	-75.18	-98.49	18.41	-53.28
91	Fondazio ne	35, 37	0	-8.00	-124.95	-78.38	103.18	18.40	52.92
			33	-8.00	-124.98	-6.21	334.24	0.73	54.20
			66	-8.01	-125.02	142.25	565.55	-17.37	55.51
92	Fondazio ne	36, 38	0	5.45	-120.75	140.87	-582.34	19.28	56.50
			35	5.45	-120.71	-18.90	-343.94	0.02	55.16
			69	5.45	-120.67	-96.51	-106.02	-18.78	53.85
93	Fondazio ne	36, 38	0	2.73	145.20	-101.02	117.63	-18.79	-53.36

			35	2.73	145.24	-19.33	356.17	-0.15	-54.67
			69	2.74	145.28	144.95	596.50	18.94	-56.03
94	Fondazio ne	37, 39	0	37.53	134.13	149.88	-561.32	-19.48	-57.04
			33	37.53	134.10	2.74	-330.72	-0.88	-55.73
			66	37.54	134.06	-68.60	-101.88	17.30	-54.46
95	Fondazio ne	37, 39	0	41.66	-119.32	-68.42	110.73	17.30	55.57
			33	41.69	-119.36	5.69	338.33	-1.25	56.83
			66	41.73	-119.39	154.79	565.21	-20.21	58.12
96	Fondazio ne	38, 40	0	9.63	-111.51	128.46	-563.29	18.97	55.61
			34	9.64	-111.47	-23.46	-323.82	0.16	54.26
			69	9.65	-111.43	-93.36	-84.24	-18.20	52.94
97	Fondazio ne	38, 40	0	3.22	152.83	-106.62	126.05	-18.20	-52.22
			34	3.24	152.86	-22.27	366.89	-0.09	-53.54
			69	3.25	152.90	144.98	610.17	18.48	-54.89
98	Fondazio ne	39, 41	0	-13.84	146.54	166.31	-596.17	-18.07	-56.28
			33	-13.79	146.50	6.76	-371.20	0.29	-55.01
			66	-13.75	146.47	-79.05	-149.36	18.24	-53.79
99	Fondazio ne	39, 41	0	-11.81	-106.86	-69.96	67.70	18.23	56.55
			33	-11.77	-106.89	-11.39	286.97	-0.63	57.76
			66	-11.74	-106.93	119.23	504.37	-19.89	58.98
100	Fondazio ne	40, 42	0	12.04	-96.95	121.16	-549.79	18.52	56.69
			35	12.05	-96.91	-25.99	-303.09	-0.81	55.32
			69	12.07	-96.87	-87.88	-55.45	-19.66	53.98
101	Fondazio ne	40, 42	0	10.94	196.73	-110.66	185.92	-19.66	-55.84
			35	10.96	196.77	-3.53	435.66	-0.17	-57.19
			69	10.99	196.81	190.30	688.53	19.80	-58.58
102	Fondazio ne	41, 44	0	-21.23	155.20	134.03	-622.37	-19.86	-55.18
			33	-21.20	155.16	-35.83	-407.57	-1.85	-53.98
			66	-21.18	155.13	-135.33	-195.92	15.77	-52.84
103	Fondazio ne	41, 44	0	-33.72	-71.72	-125.90	42.29	15.76	31.10
			33	-33.71	-71.75	-77.28	252.23	5.31	32.21
			66	-33.71	-71.79	40.59	462.24	-5.50	33.31
104	Fondazio ne	42, 43	0	16.82	-76.07	167.79	-359.10	19.78	54.56
			23	16.84	-76.04	104.70	-189.47	7.34	53.62
			46	16.86	-76.01	80.62	-19.90	-4.89	52.70
105	Fondazio ne	43, 44	0	149.33	26.56	-328.16	-570.50	-8.93	-11.83
			49	147.44	26.56	-493.33	-135.12	-3.16	-11.87
			97	145.68	26.56	-480.95	163.71	2.62	-11.91
106	Fondazio ne	43, 44	0	132.47	1.37	-485.02	-97.16	2.62	2.87
			49	130.81	1.37	-481.71	93.38	1.24	2.82
			97	129.25	1.37	-406.35	203.56	-0.12	2.78
107	Fondazio ne	43, 44	0	124.94	-2.26	-361.67	55.42	-0.12	-0.19
			49	123.49	-2.26	-319.17	110.43	-0.02	-0.21
			97	122.13	-2.26	-259.20	130.37	0.08	-0.21
108	Fondazio ne	43, 44	0	125.08	-3.04	-207.74	85.75	0.09	0.12
			49	123.82	-3.04	-164.98	86.73	0.03	0.14
			97	122.65	-3.04	-124.04	79.97	-0.05	0.18
109	Fondazio ne	43, 44	0	125.73	-0.65	-85.86	58.96	-0.04	0.01
			49	124.66	-0.65	-58.66	52.41	-0.06	0.08
			97	123.69	-0.65	-33.66	50.57	-0.12	0.16
110	Fondazio ne	43, 44	0	126.42	-0.07	-11.41	16.55	-0.11	-0.06
			49	125.54	-0.07	-2.20	21.91	-0.10	0.04
			97	124.77	-0.07	11.52	35.11	-0.15	0.16
111	Fondazio ne	43, 44	0	126.48	-0.17	20.70	-16.55	-0.15	-0.11
			49	125.80	-0.17	17.54	4.20	-0.12	0.02

			97	125.23	-0.17	26.10	31.54	-0.17	0.17
112	Fondazio ne	43, 44	0	125.94	-0.23	28.22	-35.64	-0.17	-0.15
			49	125.46	-0.23	18.74	-2.89	-0.13	0.01
			97	125.08	-0.23	26.24	34.01	-0.18	0.19
113	Fondazio ne	43, 44	0	125.03	-0.26	25.78	-43.21	-0.18	-0.18
			49	124.75	-0.26	14.41	-3.34	-0.13	0.00
			97	124.56	-0.26	22.93	38.43	-0.18	0.19
114	Fondazio ne	43, 44	0	123.88	0.42	22.70	-42.70	-0.18	-0.17
			49	123.80	0.42	12.31	0.00	-0.14	0.02
			97	123.81	0.42	22.72	42.71	-0.20	0.22
115	Fondazio ne	43, 44	0	122.79	-0.01	22.59	-39.20	-0.20	-0.21
			49	122.90	-0.01	13.73	2.62	-0.14	-0.02
			97	123.10	-0.01	24.79	42.60	-0.18	0.18
116	Fondazio ne	43, 44	0	121.33	0.45	25.16	-34.83	-0.18	-0.18
			49	121.63	0.45	17.33	2.30	-0.14	0.01
			97	122.02	0.45	26.62	35.45	-0.19	0.20
117	Fondazio ne	43, 44	0	119.35	0.87	24.57	-32.35	-0.19	-0.19
			49	119.84	0.87	15.78	-4.33	-0.14	-0.01
			97	120.42	0.87	19.13	17.45	-0.18	0.16
118	Fondazio ne	43, 44	0	116.45	1.35	10.68	-35.81	-0.18	-0.18
			49	117.13	1.35	-3.00	-21.11	-0.13	-0.02
			97	117.90	1.35	-11.34	-13.75	-0.16	0.13
119	Fondazio ne	43, 44	0	112.32	1.56	-30.95	-49.86	-0.16	-0.17
			49	113.18	1.56	-54.99	-49.18	-0.11	-0.04
			97	114.13	1.56	-79.91	-52.88	-0.12	0.08
120	Fondazio ne	43, 44	0	106.99	1.88	-113.35	-79.13	-0.13	-0.26
			49	108.02	1.88	-153.15	-82.99	-0.03	-0.16
			97	109.14	1.88	-193.45	-79.66	0.03	-0.08
121	Fondazio ne	43, 44	0	101.46	0.66	-237.34	-124.99	0.03	0.33
			49	102.67	0.66	-294.35	-104.08	-0.15	0.39
			97	103.95	0.66	-333.99	-50.73	-0.35	0.43
122	Fondazio ne	43, 44	0	96.90	1.35	-363.64	-166.43	-0.36	-2.29
			49	98.26	1.35	-422.12	-62.24	0.75	-2.27
			97	99.70	1.35	-413.05	115.16	1.85	-2.27
123	Fondazio ne	43, 44	0	102.35	6.84	-395.90	-185.88	1.85	2.62
			49	103.87	6.84	-424.35	88.83	0.58	2.62
			97	105.47	6.84	-290.53	484.85	-0.70	2.63
124	Fondazio ne	43, 45	0	53.44	-133.45	166.57	-713.56	6.14	35.31
			33	53.49	-133.41	-28.92	-471.55	-5.30	34.01
			66	53.55	-133.38	-144.92	-231.71	-16.31	32.74
125	Fondazio ne	43, 45	0	55.49	116.84	-84.29	116.38	-16.31	-54.70
			33	55.58	116.88	-6.47	355.35	1.95	-55.98
			66	55.68	116.92	150.21	594.36	20.64	-57.29
126	Fondazio ne	44, 46	0	23.57	69.84	32.81	-427.36	-8.35	-36.22
			33	23.57	69.81	-73.48	-216.72	3.41	-35.11
			66	23.57	69.77	-110.10	-4.88	14.82	-34.00
127	Fondazio ne	44, 46	0	41.02	-182.32	-147.92	298.58	14.82	53.30
			33	41.03	-182.35	-14.08	513.29	-2.95	54.44
			66	41.06	-182.39	191.30	732.14	-21.11	55.63
128	Fondazio ne	45, 47	0	10.35	-163.40	161.71	-655.35	18.47	57.86
			33	10.47	-163.36	-15.26	-417.33	-0.41	56.55
			66	10.59	-163.32	-114.00	-181.26	-18.86	55.28
129	Fondazio ne	45, 47	0	18.47	117.13	-74.16	103.28	-18.86	-54.79
			33	18.60	117.17	-1.30	338.38	-0.57	-56.05
			66	18.73	117.21	149.09	573.22	18.14	-57.35

130	Fondazio ne	46, 48	0	-4.79	120.84	166.85	-568.76	-19.03	-56.48
			33	-4.76	120.80	15.70	-346.97	-0.59	-55.28
			66	-4.73	120.76	-62.00	-123.63	17.46	-54.11
131	Fondazio ne	46, 48	0	10.91	-146.39	-58.95	133.07	17.46	51.05
			33	10.95	-146.43	22.05	358.31	0.42	52.23
			66	10.99	-146.47	177.76	585.72	-17.01	53.44
132	Fondazio ne	47, 49	0	72.96	-152.41	156.79	-583.47	20.23	58.14
			33	73.11	-152.37	2.81	-349.95	1.26	56.84
			66	73.29	-152.33	-74.51	-118.86	-17.29	55.59
133	Fondazio ne	47, 49	0	83.68	103.73	-63.54	110.82	-17.28	-56.41
			33	83.89	103.77	10.85	340.02	1.54	-57.66
			66	84.12	103.81	160.64	567.80	20.78	-58.92
134	Fondazio ne	48, 50	0	65.85	136.05	188.19	-589.36	-19.16	-55.83
			33	65.90	136.01	31.34	-361.29	-0.94	-54.62
			66	65.98	135.98	-50.40	-134.22	16.89	-53.43
135	Fondazio ne	48, 50	0	81.01	-117.38	-50.55	124.37	16.89	56.56
			33	81.12	-117.41	27.81	350.56	-1.97	57.74
			66	81.25	-117.45	180.70	576.01	-21.22	58.94
136	Fondazio ne	49, 51	0	33.61	-174.91	183.56	-619.97	18.76	58.36
			33	33.87	-174.88	16.15	-394.94	-0.29	57.12
			66	34.14	-174.84	-77.67	-174.08	-18.94	55.93
137	Fondazio ne	49, 51	0	46.72	82.62	-51.86	64.55	-18.94	-58.36
			33	47.01	82.66	5.30	281.66	0.51	-59.52
			66	47.31	82.70	133.57	495.46	20.35	-60.69
138	Fondazio ne	50, 52	0	28.15	176.42	206.80	-650.42	-19.26	-59.20
			33	28.30	176.38	29.04	-427.35	0.08	-58.02
			66	28.46	176.34	-75.76	-208.39	19.04	-56.88
139	Fondazio ne	50, 52	0	45.00	-83.24	-46.51	67.90	19.03	60.36
			33	45.17	-83.28	11.46	283.02	-1.07	61.48
			66	45.36	-83.31	139.84	494.63	-21.54	62.61
140	Fondazio ne	51, 53	0	94.25	-223.22	178.80	-626.86	22.89	62.25
			33	94.57	-223.19	6.58	-417.47	2.54	61.10
			66	94.93	-223.15	-97.49	-213.75	-17.45	60.02
141	Fondazio ne	51, 53	0	106.32	22.59	-37.40	38.00	-17.43	-63.76
			33	106.72	22.63	7.97	236.63	3.78	-64.79
			66	107.16	22.66	118.11	430.56	25.33	-65.80
142	Fondazio ne	52, 54	0	50.80	228.86	190.90	-659.11	-21.81	-61.90
			33	51.01	228.82	7.65	-452.24	-1.57	-60.80
			66	51.24	228.79	-108.33	-251.42	18.32	-59.77
143	Fondazio ne	52, 54	0	60.44	-23.44	-44.92	16.10	18.32	63.39
			33	60.69	-23.47	-7.27	211.49	-2.77	64.38
			66	60.96	-23.50	94.05	402.04	-24.18	65.36
144	Fondazio ne	53, 55	0	48.57	-314.80	206.35	-741.17	21.86	54.68
			33	49.03	-314.77	-7.09	-553.05	3.98	53.75
			66	49.52	-314.74	-159.62	-371.97	-13.62	52.94
145	Fondazio ne	53, 55	0	49.54	-120.57	-41.90	-138.44	-13.60	-41.23
			33	50.04	-120.54	-58.64	36.68	0.13	-41.93
			66	50.56	-120.52	-18.41	207.04	14.07	-42.54
146	Fondazio ne	54, 56	0	59.45	310.58	187.47	-723.18	-23.07	-56.23
			33	59.74	310.55	-20.53	-538.24	-4.67	-55.31
			66	60.06	310.52	-168.60	-359.83	13.45	-54.51
147	Fondazio ne	54, 56	0	54.70	111.81	-51.01	-105.48	13.43	41.13
			33	55.04	111.79	-57.19	67.66	-0.26	41.83
			66	55.39	111.76	-6.93	236.77	-14.17	42.46
148	Fondazio	55, 57	0	62.23	-292.27	106.45	-630.14	8.52	14.01

	ne								
			40	62.88	-292.24	-104.22	-430.27	3.07	13.42
			80	63.56	-292.22	-236.58	-235.56	-2.17	13.02
149	Fondazio ne	55, 57	0	61.81	-139.13	-112.99	-162.75	-2.14	-12.99
			40	62.52	-139.11	-139.29	31.43	3.07	-13.18
			80	63.27	-139.09	-87.76	229.63	8.31	-13.16
150	Fondazio ne	56, 70	0	65.09	289.39	121.10	-647.91	-8.54	-14.18
			40	65.54	289.36	-96.75	-448.72	-3.03	-13.56
			80	66.03	289.34	-236.44	-254.06	2.27	-13.13
151	Fondazio ne	56, 70	0	60.85	136.27	-106.68	-170.70	2.24	12.90
			40	61.37	136.25	-136.04	23.89	-2.94	13.14
			80	61.93	136.23	-87.33	222.83	-8.18	13.18
152	Fondazio ne	57, 58	0	-34.57	80.17	-54.25	-312.16	-5.00	-0.46
			42	-34.49	80.17	-143.05	-122.06	-4.66	-1.14
			83	-34.42	80.17	-160.95	29.91	-4.08	-1.59
153	Fondazio ne	57, 58	0	-29.74	106.21	-267.97	143.70	-4.05	3.47
			42	-29.70	106.22	-182.35	263.51	-5.44	3.21
			83	-29.67	106.23	-52.32	358.48	-6.75	3.12
154	Fondazio ne	58, 59	0	-79.19	91.81	-120.53	-103.34	-5.40	-6.94
			35	-79.19	91.82	-144.85	-39.69	-3.01	-6.93
			69	-79.22	91.83	-149.08	13.55	-0.62	-6.87
155	Fondazio ne	58, 59	0	-53.12	49.83	-192.57	204.27	-0.61	2.52
			35	-53.18	49.84	-114.00	250.17	-1.50	2.63
			69	-53.25	49.85	-20.41	291.66	-2.44	2.79
156	Fondazio ne	59, 60	0	-33.29	35.25	-49.36	-81.94	-2.09	-2.69
			35	-33.38	35.26	-70.88	-43.29	-1.20	-2.50
			69	-33.48	35.27	-79.38	-6.25	-0.37	-2.29
157	Fondazio ne	59, 60	0	-17.01	19.03	-98.47	148.61	-0.37	0.60
			35	-17.12	19.04	-40.81	185.61	-0.61	0.84
			69	-17.25	19.05	29.80	223.87	-0.95	1.11
158	Fondazio ne	60, 61	0	-4.22	13.50	25.44	-127.96	-0.81	-0.67
			35	-4.35	13.51	-11.87	-88.21	-0.63	-0.39
			69	-4.47	13.52	-35.22	-47.02	-0.54	-0.10
159	Fondazio ne	60, 61	0	1.52	3.47	-32.33	96.12	-0.54	-0.56
			35	1.39	3.48	8.22	139.18	-0.40	-0.26
			69	1.27	3.50	63.99	184.32	-0.36	0.06
160	Fondazio ne	61, 62	0	44.11	-5.94	66.25	-171.25	-0.38	-1.17
			35	43.99	-5.93	15.20	-124.66	-0.04	-0.84
			69	43.89	-5.92	-19.65	-77.36	0.20	-0.51
161	Fondazio ne	61, 62	0	49.12	-7.15	-14.80	53.16	0.20	0.22
			35	49.04	-7.14	11.81	101.18	0.07	0.55
			69	48.97	-7.13	55.12	149.93	-0.18	0.90
162	Fondazio ne	62, 63	0	22.85	-10.15	60.96	-181.16	-0.14	0.02
			35	22.80	-10.14	6.91	-132.30	-0.21	0.38
			69	22.76	-10.13	-30.36	-83.89	-0.41	0.74
163	Fondazio ne	62, 63	0	27.45	-6.17	-25.01	37.07	-0.40	-0.51
			35	27.42	-6.16	-3.91	85.21	-0.29	-0.14
			69	27.40	-6.15	33.80	133.35	-0.31	0.23
164	Fondazio ne	63, 64	0	29.74	-3.28	36.92	-153.42	-0.31	-0.55
			35	29.73	-3.27	-7.73	-105.50	-0.18	-0.17
			69	29.73	-3.26	-35.92	-58.00	-0.19	0.20
165	Fondazio ne	63, 64	0	30.21	3.29	-36.00	57.71	-0.19	-0.22
			35	30.22	3.30	-7.91	105.19	-0.18	0.15
			69	30.25	3.31	36.62	153.07	-0.29	0.53
166	Fondazio ne	64, 65	0	28.85	6.05	33.65	-133.76	-0.29	-0.25

			35	28.89	6.07	-4.21	-85.68	-0.27	0.13
			69	28.93	6.08	-25.49	-37.64	-0.38	0.51
167	Fondazio ne	64, 65	0	25.20	10.00	-31.03	83.63	-0.38	-0.76
			35	25.26	10.01	6.13	131.93	-0.18	-0.39
			69	25.33	10.02	60.03	180.70	-0.11	-0.02
168	Fondazio ne	65, 66	0	51.85	6.81	54.25	-149.53	-0.15	-0.97
			35	51.94	6.82	11.05	-100.86	0.12	-0.60
			69	52.04	6.83	-15.47	-52.89	0.27	-0.25
169	Fondazio ne	65, 66	0	47.88	5.33	-20.40	79.29	0.27	0.42
			35	48.00	5.34	15.11	126.60	0.06	0.77
			69	48.15	5.35	66.83	173.24	-0.26	1.12
170	Fondazio ne	66, 67	0	5.06	-3.81	64.84	-188.82	-0.24	0.06
			35	5.22	-3.79	7.53	-143.56	-0.33	0.41
			69	5.37	-3.78	-34.52	-100.33	-0.53	0.75
171	Fondazio ne	66, 67	0	-1.26	-10.29	-32.18	38.27	-0.53	-0.12
			35	-1.10	-10.28	-11.82	79.70	-0.54	0.22
			69	-0.95	-10.27	22.60	119.74	-0.68	0.54
172	Fondazio ne	67, 68	0	-12.23	-20.14	29.29	-217.36	-0.82	-1.09
			35	-12.08	-20.13	-39.02	-178.74	-0.50	-0.78
			69	-11.93	-20.12	-94.24	-141.31	-0.28	-0.48
173	Fondazio ne	67, 68	0	-27.33	-37.76	-79.77	9.34	-0.28	2.14
			35	-27.19	-37.74	-70.14	46.83	-1.07	2.42
			69	-27.06	-37.73	-47.33	85.93	-1.95	2.68
174	Fondazio ne	68, 69	0	-47.08	-49.52	-23.36	-284.03	-2.31	-2.81
			35	-46.96	-49.51	-114.24	-242.11	-1.38	-2.58
			69	-46.87	-49.50	-189.97	-195.78	-0.52	-2.38
175	Fondazio ne	68, 69	0	-72.35	-90.93	-148.40	-13.20	-0.53	6.40
			35	-72.28	-90.93	-143.98	40.46	-2.77	6.56
			69	-72.23	-90.92	-119.34	104.50	-5.05	6.67
176	Fondazio ne	69, 70	0	-27.22	-102.57	-55.84	-356.10	-6.47	-3.03
			42	-27.19	-102.56	-184.80	-260.71	-5.22	-2.98
			83	-27.18	-102.55	-269.18	-140.46	-3.97	-3.07
177	Fondazio ne	69, 70	0	-34.35	-79.41	-167.05	-20.86	-4.00	2.37
			42	-34.36	-79.41	-145.30	131.66	-4.93	2.10
			83	-34.39	-79.41	-52.35	322.56	-5.71	1.62
178	Primo Impalcato	1, 2	0	316.21	-0.16	-5.69	285.37	150.76	85.45
			83	316.21	-0.16	90.77	-53.27	79.73	85.45
			166	316.21	-0.16	-94.25	-391.91	8.71	85.45
179	Primo Impalcato	1, 15	0	106.56	10.40	-41.96	310.34	-178.36	-203.16
			80	106.56	10.40	75.84	-13.98	-16.85	-203.16
			159	106.56	10.40	-64.19	-338.31	144.67	-203.16
180	Primo Impalcato	2, 3	0	274.15	-0.25	-90.09	286.85	11.14	16.02
			69	274.15	-0.25	10.71	5.33	0.09	16.02
			138	274.15	-0.25	-82.74	-276.19	-10.97	16.02
181	Primo Impalcato	3, 4	0	273.70	-0.35	-81.31	291.32	-10.36	-2.12
			69	273.70	-0.35	22.58	9.80	-8.90	-2.12
			138	273.70	-0.35	-67.79	-271.72	-7.44	-2.12
182	Primo Impalcato	4, 5	0	273.16	-0.19	-67.54	287.06	-7.23	-3.50
			69	273.16	-0.19	33.41	5.54	-4.81	-3.50
			138	273.16	-0.19	-59.89	-275.98	-2.39	-3.50
183	Primo Impalcato	5, 6	0	272.75	-0.08	-59.61	273.67	-2.38	-1.50
			69	272.75	-0.08	32.10	-7.85	-1.34	-1.50
			138	272.75	-0.08	-70.45	-289.37	-0.30	-1.50
184	Primo Impalcato	6, 7	0	325.15	-0.03	-70.18	281.69	-0.26	-0.34
			69	325.15	-0.03	27.06	0.17	-0.02	-0.34

			138	325.15	-0.03	-69.94	-281.35	0.21	-0.34
185	Primo Impalcato	7, 8	0	262.14	-0.01	-70.13	292.52	0.13	-0.05
			69	262.14	-0.01	34.58	11.00	0.16	-0.05
			138	262.14	-0.01	-54.95	-270.52	0.20	-0.05
186	Primo Impalcato	8, 9	0	262.19	0.03	-54.94	270.49	0.21	0.40
			69	262.19	0.03	34.58	-11.03	-0.06	0.40
			138	262.19	0.03	-70.16	-292.55	-0.34	0.40
187	Primo Impalcato	9, 10	0	333.33	0.08	-69.94	281.39	-0.21	1.59
			69	333.33	0.08	27.10	-0.13	-1.31	1.59
			138	333.33	0.08	-70.11	-281.65	-2.40	1.59
188	Primo Impalcato	10, 11	0	282.02	0.19	-70.35	287.51	-2.54	3.50
			69	282.02	0.19	30.91	5.99	-4.96	3.50
			138	282.02	0.19	-62.08	-275.53	-7.38	3.50
189	Primo Impalcato	11, 12	0	282.57	0.35	-62.51	267.36	-7.59	2.01
			69	282.57	0.35	24.84	-14.16	-8.98	2.01
			138	282.57	0.35	-82.06	-295.68	-10.36	2.01
190	Primo Impalcato	12, 13	0	283.01	0.25	-83.49	278.09	-10.97	-16.57
			69	283.01	0.25	11.26	-3.43	0.46	-16.57
			138	283.01	0.25	-88.23	-284.95	11.90	-16.57
191	Primo Impalcato	13, 14	0	324.04	0.14	-92.35	384.90	9.44	-87.04
			83	324.04	0.14	86.85	46.26	81.80	-87.04
			166	324.04	0.14	-15.44	-292.38	154.15	-87.04
192	Primo Impalcato	14, 16	0	103.52	-10.13	-44.27	310.43	164.14	189.79
			80	103.52	-10.13	73.61	-13.89	13.25	189.79
			159	103.52	-10.13	-66.35	-338.21	-137.63	189.79
193	Primo Impalcato	15, 17	0	30.98	0.82	-70.83	286.45	130.48	63.67
			66	30.98	0.82	29.36	17.17	88.46	63.67
			132	30.98	0.82	-48.17	-252.11	46.44	63.67
194	Primo Impalcato	16, 18	0	20.62	-1.02	-72.45	289.49	-123.77	-59.27
			66	20.62	-1.02	29.75	20.21	-84.65	-59.27
			132	20.62	-1.02	-45.78	-249.07	-45.53	-59.27
195	Primo Impalcato	17, 19	0	94.91	0.02	-54.43	272.08	42.75	33.12
			66	94.91	0.02	36.28	2.80	20.89	33.12
			132	94.91	0.02	-50.73	-266.48	-0.97	33.12
196	Primo Impalcato	18, 20	0	81.40	-0.03	-53.22	269.26	-46.32	-35.50
			66	81.40	-0.03	35.62	-0.02	-22.89	-35.50
			132	81.40	-0.03	-53.25	-269.30	0.54	-35.50
197	Primo Impalcato	19, 21	0	6.98	-0.12	-54.14	271.71	0.90	3.02
			66	6.98	-0.12	36.33	2.43	-1.09	3.02
			132	6.98	-0.12	-50.93	-266.85	-3.08	3.02
198	Primo Impalcato	20, 22	0	-12.03	0.10	-58.27	276.75	-1.19	-3.25
			66	-12.03	0.10	35.52	7.47	0.96	-3.25
			132	-12.03	0.10	-48.41	-261.81	3.11	-3.25
199	Primo Impalcato	21, 23	0	94.25	-0.03	-51.50	268.59	-3.82	-2.01
			66	94.25	-0.03	36.91	-0.69	-2.50	-2.01
			132	94.25	-0.03	-52.41	-269.97	-1.17	-2.01
200	Primo Impalcato	22, 24	0	65.59	0.02	-49.29	263.51	4.15	2.08
			66	65.59	0.02	35.77	-5.77	2.77	2.08
			132	65.59	0.02	-56.91	-275.05	1.40	2.08
201	Primo Impalcato	23, 25	0	19.46	0.05	-50.12	239.19	0.05	0.35
			66	19.46	0.05	18.88	-30.09	-0.18	0.35
			132	19.46	0.05	-89.84	-299.37	-0.41	0.35
202	Primo Impalcato	24, 26	0	-14.14	-0.04	-58.45	264.79	0.20	-0.10
			66	-14.14	-0.04	27.44	-4.49	0.27	-0.10
			132	-14.14	-0.04	-64.38	-273.77	0.33	-0.10

203	Primo Impalcato	25, 28	0	125.62	-0.02	-90.58	341.35	-1.67	-0.48
			85	125.62	-0.02	52.18	-5.45	-1.27	-0.48
			170	125.62	-0.02	-99.84	-352.25	-0.86	-0.48
204	Primo Impalcato	26, 27	0	60.54	0.04	-65.60	275.04	1.47	0.99
			66	60.54	0.04	27.06	5.76	0.81	0.99
			132	60.54	0.04	-58.00	-263.52	0.16	0.99
205	Primo Impalcato	27, 29	0	-19.45	0.02	-66.91	280.42	-0.85	0.05
			66	-19.45	0.02	29.31	11.14	-0.88	0.05
			132	-19.45	0.02	-52.20	-258.14	-0.91	0.05
206	Primo Impalcato	28, 30	0	12.36	-0.03	-92.73	319.24	0.31	-0.14
			73	12.36	-0.03	31.60	21.40	0.42	-0.14
			146	12.36	-0.03	-61.49	-276.44	0.52	-0.14
207	Primo Impalcato	29, 31	0	54.83	0.01	-57.43	271.99	0.19	-0.12
			66	54.83	0.01	33.23	2.71	0.27	-0.12
			132	54.83	0.01	-53.85	-266.57	0.35	-0.12
208	Primo Impalcato	30, 32	0	4.07	0.00	-52.73	268.37	0.41	0.16
			69	4.07	0.00	35.39	-11.11	0.30	0.16
			137	4.07	0.00	-67.94	-290.59	0.19	0.16
209	Primo Impalcato	31, 33	0	-17.05	0.02	-64.63	277.44	-0.72	-0.11
			66	-17.05	0.02	29.62	8.16	-0.65	-0.11
			132	-17.05	0.02	-53.86	-261.12	-0.57	-0.11
210	Primo Impalcato	32, 34	0	-4.78	0.01	-56.91	272.06	0.12	0.08
			69	-4.78	0.01	33.69	-9.46	0.07	0.08
			138	-4.78	0.01	-69.97	-290.98	0.01	0.08
211	Primo Impalcato	33, 35	0	69.28	0.01	-62.97	277.82	0.52	-0.02
			66	69.28	0.01	31.52	8.54	0.53	-0.02
			132	69.28	0.01	-51.70	-260.74	0.54	-0.02
212	Primo Impalcato	34, 36	0	-14.54	0.02	-57.13	271.17	-0.05	0.01
			69	-14.54	0.02	32.86	-10.35	-0.05	0.01
			138	-14.54	0.02	-71.41	-291.87	-0.06	0.01
213	Primo Impalcato	35, 37	0	1.87	0.01	-63.23	276.73	-0.55	-0.01
			66	1.87	0.01	30.55	7.45	-0.55	-0.01
			132	1.87	0.01	-53.40	-261.83	-0.54	-0.01
214	Primo Impalcato	36, 38	0	-25.33	0.01	-57.11	269.93	-0.13	0.00
			69	-25.33	0.01	32.02	-11.59	-0.13	0.00
			138	-25.33	0.01	-73.10	-293.11	-0.13	0.00
215	Primo Impalcato	37, 39	0	95.27	0.00	-63.41	271.40	0.56	0.01
			66	95.27	0.00	26.85	2.12	0.55	0.01
			132	95.27	0.00	-60.62	-267.16	0.54	0.01
216	Primo Impalcato	38, 40	0	-37.24	0.00	-57.67	270.98	-0.23	-0.27
			69	-37.24	0.00	32.23	-8.50	-0.04	-0.27
			137	-37.24	0.00	-69.31	-287.98	0.14	-0.27
217	Primo Impalcato	39, 41	0	19.35	0.01	-67.83	289.50	-0.56	0.10
			66	19.35	0.01	34.38	20.22	-0.63	0.10
			132	19.35	0.01	-41.14	-249.06	-0.69	0.10
218	Primo Impalcato	40, 42	0	-50.14	-0.04	-52.85	285.05	0.03	-1.22
			69	-50.14	-0.04	46.71	3.53	0.86	-1.22
			138	-50.14	-0.04	-47.98	-277.99	1.70	-1.22
219	Primo Impalcato	41, 44	0	34.91	-0.04	-48.96	249.70	-0.78	-1.20
			66	34.91	-0.04	26.98	-19.58	0.01	-1.20
			132	34.91	-0.04	-74.80	-288.86	0.80	-1.20
220	Primo Impalcato	42, 43	0	-63.89	0.11	-26.25	15.01	1.68	1.72
			23	-63.89	0.11	-33.59	-78.83	1.29	1.72
			46	-63.89	0.11	-62.51	-172.67	0.89	1.72
221	Primo	43, 45	0	22.58	-0.01	-61.62	275.71	-0.18	0.29

	Impalcato								
			66	22.58	-0.01	31.49	6.43	-0.37	0.29
			132	22.58	-0.01	-53.13	-262.85	-0.57	0.29
222	Primo Impalcato	44, 46	0	108.26	0.05	-74.51	284.38	1.82	1.16
			66	108.26	0.05	24.32	15.10	1.06	1.16
			132	108.26	0.05	-54.57	-254.18	0.29	1.16
223	Primo Impalcato	45, 47	0	-52.16	0.00	-51.77	261.77	0.64	0.82
			66	-52.16	0.00	32.13	-7.51	0.10	0.82
			132	-52.16	0.00	-61.69	-276.79	-0.44	0.82
224	Primo Impalcato	46, 48	0	32.50	0.00	-63.88	279.03	-0.75	-0.73
			66	32.50	0.00	31.42	9.75	-0.27	-0.73
			132	32.50	0.00	-51.01	-259.53	0.21	-0.73
225	Primo Impalcato	47, 49	0	39.95	0.03	-59.47	276.62	-1.56	2.09
			66	39.95	0.03	34.23	7.34	-2.93	2.09
			132	39.95	0.03	-49.79	-261.94	-4.31	2.09
226	Primo Impalcato	48, 50	0	114.88	-0.05	-50.84	262.90	1.21	-2.26
			66	114.88	-0.05	33.81	-6.38	2.71	-2.26
			132	114.88	-0.05	-59.26	-275.66	4.20	-2.26
227	Primo Impalcato	49, 51	0	-31.39	0.11	-45.76	256.80	-3.51	-3.13
			66	-31.39	0.11	34.87	-12.48	-1.44	-3.13
			132	-31.39	0.11	-62.23	-281.76	0.62	-3.13
228	Primo Impalcato	50, 52	0	36.75	-0.10	-57.83	278.97	3.53	3.61
			66	36.75	-0.10	37.43	9.69	1.15	3.61
			132	36.75	-0.10	-45.04	-259.59	-1.23	3.61
229	Primo Impalcato	51, 53	0	67.74	-0.02	-56.01	271.71	-1.23	-33.11
			66	67.74	-0.02	34.46	2.43	20.63	-33.11
			132	67.74	-0.02	-52.80	-266.85	42.48	-33.11
230	Primo Impalcato	52, 54	0	36.58	0.02	-40.90	258.44	-0.04	33.03
			66	36.58	0.02	40.81	-10.84	-21.84	33.03
			132	36.58	0.02	-55.20	-280.12	-43.64	33.03
231	Primo Impalcato	53, 55	0	11.88	-0.81	-44.38	246.15	46.16	-64.09
			66	11.88	-0.81	29.22	-23.13	88.46	-64.09
			132	11.88	-0.81	-74.90	-292.41	130.76	-64.09
232	Primo Impalcato	54, 56	0	31.81	0.93	-44.52	246.21	-47.28	62.67
			66	31.81	0.93	29.12	-23.07	-88.64	62.67
			132	31.81	0.93	-74.97	-292.35	-130.00	62.67
233	Primo Impalcato	55, 57	0	96.60	-10.41	-66.26	337.74	144.98	203.29
			80	96.60	-10.41	73.33	13.42	-16.63	203.29
			159	96.60	-10.41	-44.92	-310.90	-178.25	203.29
234	Primo Impalcato	56, 70	0	120.70	10.18	-71.86	339.29	-126.54	-177.63
			80	120.70	10.18	68.95	14.97	14.68	-177.63
			159	120.70	10.18	-48.06	-309.36	155.90	-177.63
235	Primo Impalcato	57, 58	0	317.62	0.21	-4.89	284.84	-150.54	-85.19
			83	317.62	0.21	91.13	-53.80	-79.73	-85.19
			166	317.62	0.21	-94.33	-392.44	-8.92	-85.19
236	Primo Impalcato	58, 59	0	278.25	0.23	-90.10	286.19	-11.34	-16.05
			69	278.25	0.23	10.25	4.67	-0.27	-16.05
			138	278.25	0.23	-83.65	-276.85	10.81	-16.05
237	Primo Impalcato	59, 60	0	277.83	0.34	-82.21	295.87	10.21	2.05
			69	277.83	0.34	24.81	14.35	8.79	2.05
			138	277.83	0.34	-62.41	-267.17	7.38	2.05
238	Primo Impalcato	60, 61	0	277.32	0.18	-61.98	275.52	7.16	3.41
			69	277.32	0.18	31.00	-6.00	4.81	3.41
			138	277.32	0.18	-70.26	-287.52	2.45	3.41
239	Primo Impalcato	61, 62	0	330.44	0.08	-70.01	281.95	2.32	1.53

			69	330.44	0.08	27.41	0.43	1.26	1.53
			138	330.44	0.08	-69.42	-281.09	0.21	1.53
240	Primo Impalcato	62, 63	0	259.81	0.04	-69.59	288.23	0.33	0.42
			69	259.81	0.04	32.16	6.71	0.04	0.42
			138	259.81	0.04	-60.33	-274.81	-0.25	0.42
241	Primo Impalcato	63, 64	0	259.78	0.00	-60.51	281.51	-0.23	0.00
			69	259.78	0.00	36.61	-0.01	-0.23	0.00
			138	259.78	0.00	-60.53	-281.53	-0.24	0.00
242	Primo Impalcato	64, 65	0	259.87	-0.03	-60.32	274.65	-0.25	-0.42
			69	259.87	-0.03	32.07	-6.87	0.04	-0.42
			138	259.87	-0.03	-69.80	-288.39	0.34	-0.42
243	Primo Impalcato	65, 66	0	332.61	-0.08	-69.61	281.26	0.21	-1.60
			69	332.61	-0.08	27.34	-0.26	1.32	-1.60
			138	332.61	-0.08	-69.97	-281.78	2.42	-1.60
244	Primo Impalcato	66, 67	0	281.41	-0.19	-70.20	287.43	2.56	-3.61
			69	281.41	-0.19	31.00	5.91	5.05	-3.61
			138	281.41	-0.19	-62.05	-275.61	7.55	-3.61
245	Primo Impalcato	67, 68	0	281.98	-0.35	-62.48	267.28	7.77	-2.18
			69	281.98	-0.35	24.82	-14.24	9.28	-2.18
			138	281.98	-0.35	-82.13	-295.76	10.79	-2.18
246	Primo Impalcato	68, 69	0	282.47	-0.25	-83.55	277.88	11.42	16.78
			69	282.47	-0.25	11.06	-3.64	-0.16	16.78
			138	282.47	-0.25	-88.58	-285.16	-11.74	16.78
247	Primo Impalcato	69, 70	0	324.62	-0.16	-92.71	385.89	-9.20	89.00
			83	324.62	-0.16	87.31	47.25	-83.18	89.00
			166	324.62	-0.16	-14.16	-291.39	-157.15	89.00
248	Primo Impalcato	1	0	-584.11	-12.66	17.61	-5.88	-11.50	-29.15
			188	-584.11	-12.66	6.55	-5.88	43.30	-29.15
			376	-584.11	-12.66	-4.51	-5.88	98.10	-29.15
249	Primo Impalcato	2	0	-897.87	0.34	-56.31	35.43	-1.82	-0.94
			188	-897.87	0.34	10.30	35.43	-0.05	-0.94
			376	-897.87	0.34	76.91	35.43	1.73	-0.94
250	Primo Impalcato	3	0	-821.13	0.34	-16.36	14.14	-0.24	-0.09
			188	-821.13	0.34	10.22	14.14	-0.07	-0.09
			376	-821.13	0.34	36.80	14.14	0.11	-0.09
251	Primo Impalcato	4	0	-750.06	0.14	2.80	2.96	0.37	0.23
			188	-750.06	0.14	8.36	2.96	-0.06	0.23
			376	-750.06	0.14	13.92	2.96	-0.48	0.23
252	Primo Impalcato	5	0	-671.35	0.03	6.82	0.11	0.23	0.17
			188	-671.35	0.03	7.01	0.11	-0.09	0.17
			376	-671.35	0.03	7.21	0.11	-0.40	0.17
253	Primo Impalcato	6	0	-570.68	0.00	5.79	0.30	0.08	0.08
			188	-570.68	0.00	6.35	0.30	-0.06	0.08
			376	-570.68	0.00	6.91	0.30	-0.20	0.08
254	Primo Impalcato	7	0	-556.86	0.00	4.75	0.66	0.17	0.07
			188	-556.86	0.00	5.99	0.66	0.03	0.07
			376	-556.86	0.00	7.24	0.66	-0.10	0.07
255	Primo Impalcato	8	0	-599.53	0.00	4.81	0.55	-0.05	-0.03
			188	-599.53	0.00	5.85	0.55	0.00	-0.03
			376	-599.53	0.00	6.88	0.55	0.06	-0.03
256	Primo Impalcato	9	0	-566.74	0.00	5.83	0.23	-0.28	-0.14
			188	-566.74	0.00	6.25	0.23	-0.02	-0.14
			376	-566.74	0.00	6.68	0.23	0.24	-0.14
257	Primo Impalcato	10	0	-601.73	-0.03	6.63	0.24	-0.23	-0.17
			188	-601.73	-0.03	7.08	0.24	0.08	-0.17

			376	-601.73	-0.03	7.53	0.24	0.40	-0.17
258	Primo Impalcato	11	0	-728.82	-0.14	2.65	3.02	-0.27	-0.20
			188	-728.82	-0.14	8.34	3.02	0.10	-0.20
			376	-728.82	-0.14	14.02	3.02	0.47	-0.20
259	Primo Impalcato	12	0	-820.13	-0.35	-16.85	14.41	0.25	0.10
			188	-820.13	-0.35	10.24	14.41	0.07	0.10
			376	-820.13	-0.35	37.33	14.41	-0.11	0.10
260	Primo Impalcato	13	0	-890.62	-0.34	-56.80	35.66	1.81	0.95
			188	-890.62	-0.34	10.25	35.66	0.03	0.95
			376	-890.62	-0.34	77.30	35.66	-1.75	0.95
261	Primo Impalcato	14	0	-591.91	13.08	19.34	-6.87	19.64	32.17
			188	-591.91	13.08	6.41	-6.87	-40.83	32.17
			376	-591.91	13.08	-6.51	-6.87	-101.30	32.17
262	Primo Impalcato	15	0	-1317.62	-6.66	2.65	-1.28	114.31	161.31
			188	-1317.62	-6.66	0.24	-1.28	-188.94	161.31
			376	-1317.62	-6.66	-2.17	-1.28	-492.20	161.31
263	Primo Impalcato	16	0	-1318.47	6.57	3.77	-1.87	-120.14	-162.28
			188	-1318.47	6.57	0.25	-1.87	184.95	-162.28
			376	-1318.47	6.57	-3.26	-1.87	490.04	-162.28
264	Primo Impalcato	17	0	-1413.00	-1.05	2.90	-1.48	412.82	320.94
			188	-1413.00	-1.05	0.13	-1.48	-190.56	320.94
			376	-1413.00	-1.05	-2.65	-1.48	-793.94	320.94
265	Primo Impalcato	18	0	-1424.15	1.20	4.02	-2.08	-409.40	-319.00
			188	-1424.15	1.20	0.11	-2.08	190.33	-319.00
			376	-1424.15	1.20	-3.80	-2.08	790.05	-319.00
266	Primo Impalcato	19	0	-1460.88	0.27	1.50	-0.77	418.18	320.83
			188	-1460.88	0.27	0.06	-0.77	-184.98	320.83
			376	-1460.88	0.27	-1.38	-0.77	-788.14	320.83
267	Primo Impalcato	20	0	-1464.02	-0.25	2.74	-1.42	-420.06	-321.65
			188	-1464.02	-0.25	0.06	-1.42	184.65	-321.65
			376	-1464.02	-0.25	-2.62	-1.42	789.36	-321.65
268	Primo Impalcato	21	0	-1502.73	0.20	0.00	0.05	394.14	305.80
			188	-1502.73	0.20	0.09	0.05	-180.76	305.80
			376	-1502.73	0.20	0.18	0.05	-755.67	305.80
269	Primo Impalcato	22	0	-1516.19	-0.19	1.43	-0.71	-394.97	-306.12
			188	-1516.19	-0.19	0.09	-0.71	180.55	-306.12
			376	-1516.19	-0.19	-1.25	-0.71	756.06	-306.12
270	Primo Impalcato	23	0	-1573.37	0.04	-1.81	1.04	386.15	301.67
			188	-1573.37	0.04	0.15	1.04	-180.99	301.67
			376	-1573.37	0.04	2.12	1.04	-748.13	301.67
271	Primo Impalcato	24	0	-1568.57	-0.01	-0.01	0.06	-386.81	-301.61
			188	-1568.57	-0.01	0.11	0.06	180.21	-301.61
			376	-1568.57	-0.01	0.23	0.06	747.23	-301.61
272	Primo Impalcato	25	0	-1745.39	0.03	-0.12	0.31	387.30	305.28
			188	-1745.39	0.03	0.45	0.31	-186.62	305.28
			376	-1745.39	0.03	1.03	0.31	-760.54	305.28
273	Primo Impalcato	26	0	-1633.51	0.00	0.70	-0.37	-388.50	-304.40
			188	-1633.51	0.00	0.00	-0.37	183.78	-304.40
			376	-1633.51	0.00	-0.71	-0.37	756.06	-304.40
274	Primo Impalcato	27	0	-1558.63	0.05	1.49	-0.87	-388.37	-302.21
			188	-1558.63	0.05	-0.16	-0.87	179.79	-302.21
			376	-1558.63	0.05	-1.80	-0.87	747.95	-302.21
275	Primo Impalcato	28	0	-1734.32	-0.07	0.21	-0.23	387.63	303.68
			188	-1734.32	-0.07	-0.23	-0.23	-183.28	303.68
			376	-1734.32	-0.07	-0.67	-0.23	-754.19	303.68

276	Primo Impalcato	29	0	-1523.89	0.00	1.32	-0.72	-389.94	-302.19
			188	-1523.89	0.00	-0.03	-0.72	178.17	-302.19
			376	-1523.89	0.00	-1.38	-0.72	746.28	-302.19
277	Primo Impalcato	30	0	-1751.82	-0.04	0.71	-0.35	392.74	304.83
			188	-1751.82	-0.04	0.06	-0.35	-180.34	304.83
			376	-1751.82	-0.04	-0.59	-0.35	-753.42	304.83
278	Primo Impalcato	31	0	-1510.39	0.01	0.54	-0.32	-390.55	-302.17
			188	-1510.39	0.01	-0.06	-0.32	177.52	-302.17
			376	-1510.39	0.01	-0.66	-0.32	745.60	-302.17
279	Primo Impalcato	32	0	-1756.71	-0.02	-0.06	0.06	393.82	304.82
			188	-1756.71	-0.02	0.06	0.06	-179.25	304.82
			376	-1756.71	-0.02	0.17	0.06	-752.31	304.82
280	Primo Impalcato	33	0	-1512.04	-0.03	0.47	-0.26	-390.80	-302.07
			188	-1512.04	-0.03	-0.01	-0.26	177.10	-302.07
			376	-1512.04	-0.03	-0.50	-0.26	744.99	-302.07
281	Primo Impalcato	34	0	-1773.69	-0.02	-0.38	0.24	394.14	304.87
			188	-1773.69	-0.02	0.07	0.24	-179.01	304.87
			376	-1773.69	-0.02	0.52	0.24	-752.16	304.87
282	Primo Impalcato	35	0	-1517.23	0.01	0.06	-0.06	-390.80	-301.95
			188	-1517.23	0.01	-0.05	-0.06	176.87	-301.95
			376	-1517.23	0.01	-0.16	-0.06	744.53	-301.95
283	Primo Impalcato	36	0	-1787.93	-0.02	-0.44	0.26	394.40	304.91
			188	-1787.93	-0.02	0.06	0.26	-178.82	304.91
			376	-1787.93	-0.02	0.56	0.26	-752.04	304.91
284	Primo Impalcato	37	0	-1511.02	-0.03	-0.18	0.08	-390.89	-301.95
			188	-1511.02	-0.03	-0.03	0.08	176.78	-301.95
			376	-1511.02	-0.03	0.11	0.08	744.45	-301.95
285	Primo Impalcato	38	0	-1784.00	-0.03	-0.28	0.17	395.12	304.95
			188	-1784.00	-0.03	0.03	0.17	-178.19	304.95
			376	-1784.00	-0.03	0.34	0.17	-751.50	304.95
286	Primo Impalcato	39	0	-1560.86	0.01	-0.12	0.16	-390.89	-302.19
			188	-1560.86	0.01	0.18	0.16	177.23	-302.19
			376	-1560.86	0.01	0.48	0.16	745.35	-302.19
287	Primo Impalcato	40	0	-1753.23	-0.03	-0.15	0.06	396.49	304.93
			188	-1753.23	-0.03	-0.04	0.06	-176.77	304.93
			376	-1753.23	-0.03	0.06	0.06	-750.03	304.93
288	Primo Impalcato	41	0	-1705.87	-0.03	-0.96	0.55	-393.13	-303.96
			188	-1705.87	-0.03	0.08	0.55	178.31	-303.96
			376	-1705.87	-0.03	1.12	0.55	749.75	-303.96
289	Primo Impalcato	42	0	-1537.10	0.02	-2.23	0.88	394.44	301.60
			188	-1537.10	0.02	-0.59	0.88	-172.57	301.60
			376	-1537.10	0.02	1.06	0.88	-739.59	301.60
290	Primo Impalcato	43	0	-1485.07	0.05	-0.87	0.54	393.61	302.47
			188	-1485.07	0.05	0.14	0.54	-175.03	302.47
			376	-1485.07	0.05	1.16	0.54	-743.68	302.47
291	Primo Impalcato	44	0	-1672.06	-0.03	-0.01	-0.06	-390.87	-304.65
			188	-1672.06	-0.03	-0.13	-0.06	181.87	-304.65
			376	-1672.06	-0.03	-0.25	-0.06	754.61	-304.65
292	Primo Impalcato	45	0	-1554.99	0.03	-1.10	0.61	391.12	301.29
			188	-1554.99	0.03	0.05	0.61	-175.31	301.29
			376	-1554.99	0.03	1.19	0.61	-741.73	301.29
293	Primo Impalcato	46	0	-1568.59	0.03	1.06	-0.65	-388.28	-300.79
			188	-1568.59	0.03	-0.16	-0.65	177.20	-300.79
			376	-1568.59	0.03	-1.39	-0.65	742.68	-300.79
294	Primo	47	0	-1544.83	0.03	-1.46	0.77	389.71	301.40

	Impalcato								
			188	-1544.83	0.03	-0.01	0.77	-176.93	301.40
			376	-1544.83	0.03	1.44	0.77	-743.56	301.40
295	Primo Impalcato	48	0	-1534.04	0.02	0.34	-0.19	-388.95	-300.70
			188	-1534.04	0.02	-0.01	-0.19	176.37	-300.70
			376	-1534.04	0.02	-0.37	-0.19	741.69	-300.70
296	Primo Impalcato	49	0	-1542.17	-0.15	-2.43	1.27	395.59	305.72
			188	-1542.17	-0.15	-0.04	1.27	-179.16	305.72
			376	-1542.17	-0.15	2.34	1.27	-753.91	305.72
297	Primo Impalcato	50	0	-1555.19	0.19	-0.97	0.58	-396.27	-305.45
			188	-1555.19	0.19	0.12	0.58	177.96	-305.45
			376	-1555.19	0.19	1.21	0.58	752.20	-305.45
298	Primo Impalcato	51	0	-1487.06	-0.25	-3.45	1.79	418.77	320.74
			188	-1487.06	-0.25	-0.08	1.79	-184.22	320.74
			376	-1487.06	-0.25	3.30	1.79	-787.22	320.74
299	Primo Impalcato	52	0	-1654.76	0.26	-2.57	1.40	-423.48	-322.56
			188	-1654.76	0.26	0.06	1.40	182.94	-322.56
			376	-1654.76	0.26	2.69	1.40	789.35	-322.56
300	Primo Impalcato	53	0	-1440.95	1.06	-4.46	2.31	413.60	321.28
			188	-1440.95	1.06	-0.12	2.31	-190.40	321.28
			376	-1440.95	1.06	4.21	2.31	-794.41	321.28
301	Primo Impalcato	54	0	-1588.77	-1.12	-4.36	2.18	-416.22	-322.07
			188	-1588.77	-1.12	-0.26	2.18	189.27	-322.07
			376	-1588.77	-1.12	3.84	2.18	794.76	-322.07
302	Primo Impalcato	55	0	-1320.67	6.67	-4.10	2.04	114.40	161.62
			188	-1320.67	6.67	-0.27	2.04	-189.45	161.62
			376	-1320.67	6.67	3.56	2.04	-493.30	161.62
303	Primo Impalcato	56	0	-1360.61	-6.74	-3.92	1.85	-116.99	-160.92
			188	-1360.61	-6.74	-0.44	1.85	185.54	-160.92
			376	-1360.61	-6.74	3.03	1.85	488.08	-160.92
304	Primo Impalcato	57	0	-580.48	12.72	-19.99	7.21	-13.14	-29.88
			188	-580.48	12.72	-6.44	7.21	43.04	-29.88
			376	-580.48	12.72	7.10	7.21	99.21	-29.88
305	Primo Impalcato	58	0	-890.87	-0.33	55.93	-34.90	-1.90	-0.99
			188	-890.87	-0.33	-9.67	-34.90	-0.04	-0.99
			376	-890.87	-0.33	-75.28	-34.90	1.81	-0.99
306	Primo Impalcato	59	0	-816.77	-0.34	16.54	-14.01	-0.28	-0.11
			188	-816.77	-0.34	-9.79	-14.01	-0.07	-0.11
			376	-816.77	-0.34	-36.13	-14.01	0.15	-0.11
307	Primo Impalcato	60	0	-727.98	-0.14	-2.55	-2.85	0.24	0.18
			188	-727.98	-0.14	-7.92	-2.85	-0.10	0.18
			376	-727.98	-0.14	-13.29	-2.85	-0.44	0.18
308	Primo Impalcato	61	0	-603.58	-0.03	-6.37	-0.21	0.19	0.15
			188	-603.58	-0.03	-6.76	-0.21	-0.08	0.15
			376	-603.58	-0.03	-7.15	-0.21	-0.36	0.15
309	Primo Impalcato	62	0	-570.73	0.00	-5.53	-0.24	0.23	0.11
			188	-570.73	0.00	-5.98	-0.24	0.02	0.11
			376	-570.73	0.00	-6.43	-0.24	-0.19	0.11
310	Primo Impalcato	63	0	-618.25	0.00	-4.52	-0.51	0.11	0.04
			188	-618.25	0.00	-5.49	-0.51	0.03	0.04
			376	-618.25	0.00	-6.46	-0.51	-0.04	0.04
311	Primo Impalcato	64	0	-618.50	0.00	-4.53	-0.50	-0.19	-0.08
			188	-618.50	0.00	-5.47	-0.50	-0.03	-0.08
			376	-618.50	0.00	-6.42	-0.50	0.12	-0.08
312	Primo Impalcato	65	0	-571.26	0.00	-5.56	-0.19	-0.30	-0.15

			188	-571.26	0.00	-5.92	-0.19	-0.02	-0.15
			376	-571.26	0.00	-6.28	-0.19	0.26	-0.15
313	Primo Impalcato	66	0	-604.28	0.03	-6.44	-0.12	-0.26	-0.18
			188	-604.28	0.03	-6.67	-0.12	0.08	-0.18
			376	-604.28	0.03	-6.89	-0.12	0.42	-0.18
314	Primo Impalcato	67	0	-728.56	0.14	-2.39	-2.93	-0.31	-0.22
			188	-728.56	0.14	-7.90	-2.93	0.10	-0.22
			376	-728.56	0.14	-13.41	-2.93	0.51	-0.22
315	Primo Impalcato	68	0	-818.59	0.35	17.63	-14.60	0.21	0.07
			188	-818.59	0.35	-9.83	-14.60	0.07	0.07
			376	-818.59	0.35	-37.28	-14.60	-0.07	0.07
316	Primo Impalcato	69	0	-891.07	0.35	59.03	-36.66	1.78	0.93
			188	-891.07	0.35	-9.89	-36.66	0.04	0.93
			376	-891.07	0.35	-78.80	-36.66	-1.71	0.93
317	Primo Impalcato	70	0	-591.37	-13.23	-17.89	6.17	18.17	31.65
			188	-591.37	-13.23	-6.29	6.17	-41.34	31.65
			376	-591.37	-13.23	5.30	6.17	-100.84	31.65
318	Fondazio ne	1, 71	0	-195.90	-0.24	0.00	0.00	0.41	3.01
			102	-195.90	-0.24	0.00	0.00	-2.66	3.01
			204	-195.90	-0.24	0.00	0.00	-5.73	3.01
319	Fondazio ne	1, 92	0	-20.68	-0.01	0.00	0.00	-1.42	-0.46
			103	-20.68	-0.01	0.00	0.00	-0.95	-0.46
			206	-20.68	-0.01	0.00	0.00	-0.48	-0.46
320	Primo Impalcato	92, 2	0	-259.39	-0.08	0.00	0.00	1.27	1.93
			103	-259.39	-0.08	0.00	0.00	-0.72	1.93
			206	-259.39	-0.08	0.00	0.00	-2.70	1.93
321	Fondazio ne	6, 89	0	-152.31	0.00	0.00	0.00	-0.17	-0.01
			100	-152.31	0.00	0.00	0.00	-0.16	-0.01
			200	-152.31	0.00	0.00	0.00	-0.15	-0.01
322	Primo Impalcato	89, 7	0	-138.71	-0.01	0.00	0.00	-0.14	0.01
			100	-138.71	-0.01	0.00	0.00	-0.15	0.01
			200	-138.71	-0.01	0.00	0.00	-0.16	0.01
323	Fondazio ne	9, 90	0	-136.49	0.01	0.00	0.00	-0.13	0.02
			100	-136.49	0.01	0.00	0.00	-0.15	0.02
			200	-136.49	0.01	0.00	0.00	-0.18	0.02
324	Primo Impalcato	90, 10	0	-165.19	-0.01	0.00	0.00	-0.16	0.01
			100	-165.19	-0.01	0.00	0.00	-0.16	0.01
			200	-165.19	-0.01	0.00	0.00	-0.17	0.01
325	Fondazio ne	13, 91	0	-260.42	0.08	0.00	0.00	-2.72	-1.97
			103	-260.42	0.08	0.00	0.00	-0.69	-1.97
			206	-260.42	0.08	0.00	0.00	1.34	-1.97
326	Primo Impalcato	88, 14	0	-213.05	0.24	0.00	0.00	-5.64	-2.94
			102	-213.05	0.24	0.00	0.00	-2.64	-2.94
			204	-213.05	0.24	0.00	0.00	0.36	-2.94
327	Primo Impalcato	91, 14	0	-18.47	0.01	0.00	0.00	-0.51	0.43
			103	-18.47	0.01	0.00	0.00	-0.96	0.43
			206	-18.47	0.01	0.00	0.00	-1.40	0.43
328	Primo Impalcato	71, 15	0	-67.05	-0.34	0.00	0.00	4.13	3.80
			102	-67.05	-0.34	0.00	0.00	0.26	3.80
			204	-67.05	-0.34	0.00	0.00	-3.62	3.80
329	Fondazio ne	16, 88	0	-50.97	0.33	0.00	0.00	-3.63	-3.79
			102	-50.97	0.33	0.00	0.00	0.24	-3.79
			204	-50.97	0.33	0.00	0.00	4.11	-3.79
330	Fondazio ne	17, 72	0	-265.94	0.15	0.00	0.00	-7.70	-3.06
			100	-265.94	0.15	0.00	0.00	-4.65	-3.06

			199	-265.94	0.15	0.00	0.00	-1.60	-3.06
331	Primo Impalcato	87, 18	0	-285.82	-0.14	0.00	0.00	-1.63	3.05
			100	-285.82	-0.14	0.00	0.00	-4.67	3.05
			199	-285.82	-0.14	0.00	0.00	-7.71	3.05
332	Primo Impalcato	72, 19	0	-192.49	-0.16	0.00	0.00	-1.59	2.91
			100	-192.49	-0.16	0.00	0.00	-4.49	2.91
			199	-192.49	-0.16	0.00	0.00	-7.39	2.91
333	Fondazio ne	20, 87	0	-175.16	0.16	0.00	0.00	-7.40	-2.94
			100	-175.16	0.16	0.00	0.00	-4.47	-2.94
			199	-175.16	0.16	0.00	0.00	-1.54	-2.94
334	Fondazio ne	21, 73	0	-228.51	0.15	0.00	0.00	-6.93	-2.68
			100	-228.51	0.15	0.00	0.00	-4.26	-2.68
			199	-228.51	0.15	0.00	0.00	-1.59	-2.68
335	Primo Impalcato	86, 22	0	-254.90	-0.15	0.00	0.00	-1.59	2.69
			100	-254.90	-0.15	0.00	0.00	-4.27	2.69
			199	-254.90	-0.15	0.00	0.00	-6.95	2.69
336	Primo Impalcato	73, 23	0	-262.41	-0.14	0.00	0.00	-1.71	2.62
			100	-262.41	-0.14	0.00	0.00	-4.32	2.62
			199	-262.41	-0.14	0.00	0.00	-6.92	2.62
337	Fondazio ne	24, 86	0	-237.97	0.14	0.00	0.00	-6.90	-2.61
			100	-237.97	0.14	0.00	0.00	-4.30	-2.61
			199	-237.97	0.14	0.00	0.00	-1.70	-2.61
338	Fondazio ne	25, 74	0	-259.93	0.17	0.00	0.00	-6.59	-2.44
			103	-259.93	0.17	0.00	0.00	-4.08	-2.44
			206	-259.93	0.17	0.00	0.00	-1.56	-2.44
339	Primo Impalcato	85, 26	0	-278.82	-0.14	0.00	0.00	-1.65	2.71
			100	-278.82	-0.14	0.00	0.00	-4.34	2.71
			199	-278.82	-0.14	0.00	0.00	-7.04	2.71
340	Fondazio ne	27, 85	0	-231.44	0.15	0.00	0.00	-6.85	-2.61
			100	-231.44	0.15	0.00	0.00	-4.25	-2.61
			199	-231.44	0.15	0.00	0.00	-1.66	-2.61
341	Primo Impalcato	74, 28	0	-256.16	-0.18	0.00	0.00	-1.55	2.37
			103	-256.16	-0.18	0.00	0.00	-4.00	2.37
			206	-256.16	-0.18	0.00	0.00	-6.45	2.37
342	Primo Impalcato	84, 29	0	-258.68	-0.14	0.00	0.00	-1.61	2.66
			100	-258.68	-0.14	0.00	0.00	-4.26	2.66
			199	-258.68	-0.14	0.00	0.00	-6.91	2.66
343	Fondazio ne	31, 84	0	-226.38	0.14	0.00	0.00	-6.89	-2.65
			100	-226.38	0.14	0.00	0.00	-4.25	-2.65
			199	-226.38	0.14	0.00	0.00	-1.61	-2.65
344	Primo Impalcato	83, 33	0	-248.30	-0.14	0.00	0.00	-1.60	2.65
			100	-248.30	-0.14	0.00	0.00	-4.24	2.65
			199	-248.30	-0.14	0.00	0.00	-6.89	2.65
345	Fondazio ne	35, 83	0	-235.67	0.14	0.00	0.00	-6.88	-2.65
			100	-235.67	0.14	0.00	0.00	-4.25	-2.65
			199	-235.67	0.14	0.00	0.00	-1.61	-2.65
346	Primo Impalcato	82, 37	0	-242.03	-0.14	0.00	0.00	-1.60	2.64
			100	-242.03	-0.14	0.00	0.00	-4.24	2.64
			199	-242.03	-0.14	0.00	0.00	-6.87	2.64
347	Fondazio ne	39, 82	0	-248.26	0.14	0.00	0.00	-6.90	-2.66
			100	-248.26	0.14	0.00	0.00	-4.25	-2.66
			199	-248.26	0.14	0.00	0.00	-1.61	-2.66
348	Primo Impalcato	78, 43	0	-227.09	0.14	0.00	0.00	1.57	-2.66
			100	-227.09	0.14	0.00	0.00	4.22	-2.66
			199	-227.09	0.14	0.00	0.00	6.86	-2.66

349	Primo Impalcato	81, 44	0	-276.55	-0.14	0.00	0.00	-1.61	2.72
			100	-276.55	-0.14	0.00	0.00	-4.32	2.72
			199	-276.55	-0.14	0.00	0.00	-7.03	2.72
350	Fondazio ne	45, 78	0	-259.51	-0.14	0.00	0.00	6.87	2.64
			100	-259.51	-0.14	0.00	0.00	4.24	2.64
			199	-259.51	-0.14	0.00	0.00	1.61	2.64
351	Fondazio ne	46, 81	0	-240.55	0.15	0.00	0.00	-6.80	-2.58
			100	-240.55	0.15	0.00	0.00	-4.23	-2.58
			199	-240.55	0.15	0.00	0.00	-1.66	-2.58
352	Primo Impalcato	77, 47	0	-216.92	0.14	0.00	0.00	1.67	-2.59
			100	-216.92	0.14	0.00	0.00	4.25	-2.59
			199	-216.92	0.14	0.00	0.00	6.83	-2.59
353	Primo Impalcato	80, 48	0	-238.75	-0.14	0.00	0.00	-1.68	2.59
			100	-238.75	-0.14	0.00	0.00	-4.26	2.59
			199	-238.75	-0.14	0.00	0.00	-6.83	2.59
354	Fondazio ne	49, 77	0	-276.79	-0.14	0.00	0.00	6.96	2.70
			100	-276.79	-0.14	0.00	0.00	4.27	2.70
			199	-276.79	-0.14	0.00	0.00	1.59	2.70
355	Fondazio ne	50, 80	0	-253.85	0.15	0.00	0.00	-6.93	-2.69
			100	-253.85	0.15	0.00	0.00	-4.24	-2.69
			199	-253.85	0.15	0.00	0.00	-1.56	-2.69
356	Primo Impalcato	76, 51	0	-169.78	0.16	0.00	0.00	1.58	-2.90
			100	-169.78	0.16	0.00	0.00	4.47	-2.90
			199	-169.78	0.16	0.00	0.00	7.36	-2.90
357	Fondazio ne	53, 76	0	-297.85	-0.15	0.00	0.00	7.72	3.07
			100	-297.85	-0.15	0.00	0.00	4.66	3.07
			199	-297.85	-0.15	0.00	0.00	1.60	3.07
358	Primo Impalcato	75, 55	0	-45.14	0.34	0.00	0.00	-4.14	-3.81
			102	-45.14	0.34	0.00	0.00	-0.26	-3.81
			204	-45.14	0.34	0.00	0.00	3.63	-3.81
359	Fondazio ne	56, 79	0	-58.95	-0.33	0.00	0.00	3.58	3.74
			102	-58.95	-0.33	0.00	0.00	-0.24	3.74
			204	-58.95	-0.33	0.00	0.00	-4.06	3.74
360	Fondazio ne	57, 75	0	-218.14	0.24	0.00	0.00	-0.41	-3.02
			102	-218.14	0.24	0.00	0.00	2.67	-3.02
			204	-218.14	0.24	0.00	0.00	5.75	-3.02
361	Fondazio ne	57, 93	0	-16.63	0.01	0.00	0.00	1.34	0.41
			103	-16.63	0.01	0.00	0.00	0.92	0.41
			206	-16.63	0.01	0.00	0.00	0.50	0.41
362	Primo Impalcato	93, 58	0	-261.26	0.08	0.00	0.00	-1.31	-1.92
			103	-261.26	0.08	0.00	0.00	0.67	-1.92
			206	-261.26	0.08	0.00	0.00	2.65	-1.92
363	Fondazio ne	61, 95	0	-163.66	-0.01	0.00	0.00	0.16	0.01
			100	-163.66	-0.01	0.00	0.00	0.16	0.01
			200	-163.66	-0.01	0.00	0.00	0.15	0.01
364	Primo Impalcato	95, 62	0	-139.63	0.01	0.00	0.00	0.17	0.02
			100	-139.63	0.01	0.00	0.00	0.15	0.02
			200	-139.63	0.01	0.00	0.00	0.13	0.02
365	Primo Impalcato	96, 65	0	-136.36	-0.01	0.00	0.00	-0.16	-0.02
			100	-136.36	-0.01	0.00	0.00	-0.15	-0.02
			200	-136.36	-0.01	0.00	0.00	-0.13	-0.02
366	Fondazio ne	66, 96	0	-167.20	0.01	0.00	0.00	-0.16	0.00
			100	-167.20	0.01	0.00	0.00	-0.15	0.00
			200	-167.20	0.01	0.00	0.00	-0.15	0.00
367	Fondazio	69, 94	0	-259.56	-0.08	0.00	0.00	2.78	2.00

	ne								
			103	-259.56	-0.08	0.00	0.00	0.72	2.00
			206	-259.56	-0.08	0.00	0.00	-1.34	2.00
368	Primo Impalcato	79, 70	0	-210.97	-0.24	0.00	0.00	5.61	2.93
			102	-210.97	-0.24	0.00	0.00	2.62	2.93
			204	-210.97	-0.24	0.00	0.00	-0.36	2.93
369	Primo Impalcato	94, 70	0	-19.37	-0.01	0.00	0.00	0.49	-0.48
			103	-19.37	-0.01	0.00	0.00	0.98	-0.48
			206	-19.37	-0.01	0.00	0.00	1.47	-0.48
370	Primo Impalcato	1, 71	0	-67.05	-0.12	0.00	0.00	1.13	-1.59
			102	-67.05	-0.12	0.00	0.00	2.76	-1.59
			204	-67.05	-0.12	0.00	0.00	4.38	-1.59
371	Primo Impalcato	1, 92	0	-259.39	-0.43	0.00	0.00	3.72	1.27
			103	-259.39	-0.43	0.00	0.00	2.41	1.27
			206	-259.39	-0.43	0.00	0.00	1.11	1.27
372	Primo Impalcato	92, 2	0	-20.68	0.11	0.00	0.00	-0.12	-1.12
			103	-20.68	0.11	0.00	0.00	1.03	-1.12
			206	-20.68	0.11	0.00	0.00	2.18	-1.12
373	Primo Impalcato	6, 89	0	-138.71	0.00	0.00	0.00	-0.15	-0.01
			100	-138.71	0.00	0.00	0.00	-0.14	-0.01
			200	-138.71	0.00	0.00	0.00	-0.14	-0.01
374	Primo Impalcato	89, 7	0	-152.31	0.01	0.00	0.00	-0.16	-0.03
			100	-152.31	0.01	0.00	0.00	-0.13	-0.03
			200	-152.31	0.01	0.00	0.00	-0.10	-0.03
375	Primo Impalcato	9, 90	0	-165.19	0.00	0.00	0.00	-0.12	0.02
			100	-165.19	0.00	0.00	0.00	-0.14	0.02
			200	-165.19	0.00	0.00	0.00	-0.17	0.02
376	Primo Impalcato	90, 10	0	-136.49	0.00	0.00	0.00	-0.17	0.03
			100	-136.49	0.00	0.00	0.00	-0.20	0.03
			200	-136.49	0.00	0.00	0.00	-0.24	0.03
377	Primo Impalcato	13, 91	0	-18.47	-0.11	0.00	0.00	2.21	1.14
			103	-18.47	-0.11	0.00	0.00	1.03	1.14
			206	-18.47	-0.11	0.00	0.00	-0.14	1.14
378	Primo Impalcato	88, 14	0	-50.97	0.14	0.00	0.00	4.33	1.49
			102	-50.97	0.14	0.00	0.00	2.81	1.49
			204	-50.97	0.14	0.00	0.00	1.29	1.49
379	Primo Impalcato	91, 14	0	-260.42	0.44	0.00	0.00	1.18	-1.26
			103	-260.42	0.44	0.00	0.00	2.47	-1.26
			206	-260.42	0.44	0.00	0.00	3.77	-1.26
380	Primo Impalcato	71, 15	0	-195.90	-0.22	0.00	0.00	-6.07	-2.38
			102	-195.90	-0.22	0.00	0.00	-3.64	-2.38
			204	-195.90	-0.22	0.00	0.00	-1.22	-2.38
381	Primo Impalcato	16, 88	0	-213.05	0.21	0.00	0.00	-1.16	2.34
			102	-213.05	0.21	0.00	0.00	-3.55	2.34
			204	-213.05	0.21	0.00	0.00	-5.94	2.34
382	Primo Impalcato	17, 72	0	-192.49	-0.06	0.00	0.00	4.59	3.16
			100	-192.49	-0.06	0.00	0.00	1.45	3.16
			199	-192.49	-0.06	0.00	0.00	-1.70	3.16
383	Primo Impalcato	87, 18	0	-175.16	0.07	0.00	0.00	-1.65	-3.16
			100	-175.16	0.07	0.00	0.00	1.49	-3.16
			199	-175.16	0.07	0.00	0.00	4.64	-3.16
384	Primo Impalcato	72, 19	0	-265.94	0.00	0.00	0.00	-1.58	-2.82
			100	-265.94	0.00	0.00	0.00	1.22	-2.82
			199	-265.94	0.00	0.00	0.00	4.03	-2.82
385	Primo Impalcato	20, 87	0	-285.82	0.00	0.00	0.00	4.06	2.84

			100	-285.82	0.00	0.00	0.00	1.23	2.84
			199	-285.82	0.00	0.00	0.00	-1.60	2.84
386	Primo Impalcato	21, 73	0	-262.41	0.05	0.00	0.00	3.56	2.67
			100	-262.41	0.05	0.00	0.00	0.89	2.67
			199	-262.41	0.05	0.00	0.00	-1.77	2.67
387	Primo Impalcato	86, 22	0	-237.97	-0.05	0.00	0.00	-1.76	-2.67
			100	-237.97	-0.05	0.00	0.00	0.90	-2.67
			199	-237.97	-0.05	0.00	0.00	3.56	-2.67
388	Primo Impalcato	73, 23	0	-228.51	-0.03	0.00	0.00	-1.66	-2.62
			100	-228.51	-0.03	0.00	0.00	0.95	-2.62
			199	-228.51	-0.03	0.00	0.00	3.57	-2.62
389	Primo Impalcato	24, 86	0	-254.90	0.03	0.00	0.00	3.56	2.62
			100	-254.90	0.03	0.00	0.00	0.95	2.62
			199	-254.90	0.03	0.00	0.00	-1.66	2.62
390	Primo Impalcato	25, 74	0	-256.16	0.04	0.00	0.00	3.29	2.39
			103	-256.16	0.04	0.00	0.00	0.82	2.39
			206	-256.16	0.04	0.00	0.00	-1.64	2.39
391	Primo Impalcato	85, 26	0	-231.44	-0.04	0.00	0.00	-1.71	-2.64
			100	-231.44	-0.04	0.00	0.00	0.92	-2.64
			199	-231.44	-0.04	0.00	0.00	3.55	-2.64
392	Primo Impalcato	27, 85	0	-278.82	0.03	0.00	0.00	3.61	2.68
			100	-278.82	0.03	0.00	0.00	0.95	2.68
			199	-278.82	0.03	0.00	0.00	-1.72	2.68
393	Primo Impalcato	74, 28	0	-259.93	-0.04	0.00	0.00	-1.66	-2.42
			103	-259.93	-0.04	0.00	0.00	0.84	-2.42
			206	-259.93	-0.04	0.00	0.00	3.34	-2.42
394	Primo Impalcato	84, 29	0	-226.38	-0.03	0.00	0.00	-1.67	-2.65
			100	-226.38	-0.03	0.00	0.00	0.97	-2.65
			199	-226.38	-0.03	0.00	0.00	3.61	-2.65
395	Primo Impalcato	31, 84	0	-258.68	0.03	0.00	0.00	3.62	2.66
			100	-258.68	0.03	0.00	0.00	0.97	2.66
			199	-258.68	0.03	0.00	0.00	-1.68	2.66
396	Primo Impalcato	83, 33	0	-235.67	-0.03	0.00	0.00	-1.67	-2.65
			100	-235.67	-0.03	0.00	0.00	0.97	-2.65
			199	-235.67	-0.03	0.00	0.00	3.61	-2.65
397	Primo Impalcato	35, 83	0	-248.30	0.03	0.00	0.00	3.62	2.65
			100	-248.30	0.03	0.00	0.00	0.98	2.65
			199	-248.30	0.03	0.00	0.00	-1.66	2.65
398	Primo Impalcato	82, 37	0	-248.26	-0.03	0.00	0.00	-1.67	-2.65
			100	-248.26	-0.03	0.00	0.00	0.97	-2.65
			199	-248.26	-0.03	0.00	0.00	3.61	-2.65
399	Primo Impalcato	39, 82	0	-242.03	0.03	0.00	0.00	3.61	2.65
			100	-242.03	0.03	0.00	0.00	0.97	2.65
			199	-242.03	0.03	0.00	0.00	-1.67	2.65
400	Primo Impalcato	78, 43	0	-259.51	0.04	0.00	0.00	1.67	2.66
			100	-259.51	0.04	0.00	0.00	-0.98	2.66
			199	-259.51	0.04	0.00	0.00	-3.63	2.66
401	Primo Impalcato	81, 44	0	-240.55	-0.04	0.00	0.00	-1.70	-2.64
			100	-240.55	-0.04	0.00	0.00	0.93	-2.64
			199	-240.55	-0.04	0.00	0.00	3.56	-2.64
402	Primo Impalcato	45, 78	0	-227.09	-0.03	0.00	0.00	-3.62	-2.64
			100	-227.09	-0.03	0.00	0.00	-1.00	-2.64
			199	-227.09	-0.03	0.00	0.00	1.63	-2.64
403	Primo Impalcato	46, 81	0	-276.55	0.03	0.00	0.00	3.62	2.66
			100	-276.55	0.03	0.00	0.00	0.97	2.66

			199	-276.55	0.03	0.00	0.00	-1.68	2.66
404	Primo Impalcato	77, 47	0	-276.79	0.04	0.00	0.00	1.66	2.64
			100	-276.79	0.04	0.00	0.00	-0.97	2.64
			199	-276.79	0.04	0.00	0.00	-3.59	2.64
405	Primo Impalcato	80, 48	0	-253.85	-0.03	0.00	0.00	-1.63	-2.63
			100	-253.85	-0.03	0.00	0.00	0.98	-2.63
			199	-253.85	-0.03	0.00	0.00	3.60	-2.63
406	Primo Impalcato	49, 77	0	-216.92	-0.05	0.00	0.00	-3.56	-2.65
			100	-216.92	-0.05	0.00	0.00	-0.92	-2.65
			199	-216.92	-0.05	0.00	0.00	1.72	-2.65
407	Primo Impalcato	50, 80	0	-238.75	0.05	0.00	0.00	3.56	2.66
			100	-238.75	0.05	0.00	0.00	0.91	2.66
			199	-238.75	0.05	0.00	0.00	-1.73	2.66
408	Primo Impalcato	76, 51	0	-297.85	0.00	0.00	0.00	1.58	2.82
			100	-297.85	0.00	0.00	0.00	-1.22	2.82
			199	-297.85	0.00	0.00	0.00	-4.03	2.82
409	Primo Impalcato	53, 76	0	-169.78	0.05	0.00	0.00	-4.59	-3.15
			100	-169.78	0.05	0.00	0.00	-1.45	-3.15
			199	-169.78	0.05	0.00	0.00	1.69	-3.15
410	Primo Impalcato	75, 55	0	-218.14	0.22	0.00	0.00	6.08	2.38
			102	-218.14	0.22	0.00	0.00	3.65	2.38
			204	-218.14	0.22	0.00	0.00	1.22	2.38
411	Primo Impalcato	56, 79	0	-210.97	-0.23	0.00	0.00	1.42	-2.18
			102	-210.97	-0.23	0.00	0.00	3.65	-2.18
			204	-210.97	-0.23	0.00	0.00	5.87	-2.18
412	Primo Impalcato	57, 75	0	-45.14	0.12	0.00	0.00	-1.14	1.60
			102	-45.14	0.12	0.00	0.00	-2.76	1.60
			204	-45.14	0.12	0.00	0.00	-4.39	1.60
413	Primo Impalcato	57, 93	0	-261.26	0.43	0.00	0.00	-3.62	-1.20
			103	-261.26	0.43	0.00	0.00	-2.39	-1.20
			206	-261.26	0.43	0.00	0.00	-1.15	-1.20
414	Primo Impalcato	93, 58	0	-16.63	-0.11	0.00	0.00	0.14	1.13
			103	-16.63	-0.11	0.00	0.00	-1.02	1.13
			206	-16.63	-0.11	0.00	0.00	-2.18	1.13
415	Primo Impalcato	61, 95	0	-139.63	0.00	0.00	0.00	0.23	0.03
			100	-139.63	0.00	0.00	0.00	0.19	0.03
			200	-139.63	0.00	0.00	0.00	0.16	0.03
416	Primo Impalcato	95, 62	0	-163.66	0.00	0.00	0.00	0.16	0.02
			100	-163.66	0.00	0.00	0.00	0.14	0.02
			200	-163.66	0.00	0.00	0.00	0.12	0.02
417	Primo Impalcato	96, 65	0	-167.20	0.00	0.00	0.00	-0.16	-0.02
			100	-167.20	0.00	0.00	0.00	-0.14	-0.02
			200	-167.20	0.00	0.00	0.00	-0.12	-0.02
418	Primo Impalcato	66, 96	0	-136.36	0.00	0.00	0.00	-0.23	-0.04
			100	-136.36	0.00	0.00	0.00	-0.19	-0.04
			200	-136.36	0.00	0.00	0.00	-0.16	-0.04
419	Primo Impalcato	69, 94	0	-19.37	0.11	0.00	0.00	-2.28	-1.16
			103	-19.37	0.11	0.00	0.00	-1.09	-1.16
			206	-19.37	0.11	0.00	0.00	0.11	-1.16
420	Primo Impalcato	79, 70	0	-58.95	-0.14	0.00	0.00	-4.24	-1.37
			102	-58.95	-0.14	0.00	0.00	-2.85	-1.37
			204	-58.95	-0.14	0.00	0.00	-1.45	-1.37
421	Primo Impalcato	94, 70	0	-259.56	-0.44	0.00	0.00	-1.18	1.32
			103	-259.56	-0.44	0.00	0.00	-2.53	1.32
			206	-259.56	-0.44	0.00	0.00	-3.89	1.32

422	Copertura	1, 2	0	19.71	-16.84	300.70	-53.51	-8.85	-14.27
			83	19.71	-16.84	224.44	-129.98	3.01	-14.27
			166	19.71	-16.84	84.62	-206.45	14.86	-14.27
423	Copertura	15, 1	0	-25.08	-277.16	704.34	-479.39	15.51	22.67
			80	-25.08	-277.16	323.23	-479.39	-2.51	22.67
			159	-25.08	-277.16	-57.88	-479.39	-20.54	22.67
424	Copertura	2, 3	0	34.28	5.48	85.39	-106.92	14.33	2.19
			69	34.28	5.48	-10.29	-170.40	12.82	2.19
			138	34.28	5.48	-149.76	-233.88	11.31	2.19
425	Copertura	3, 4	0	34.82	6.83	-148.56	19.75	11.04	6.19
			69	34.82	6.83	-156.84	-43.73	6.77	6.19
			138	34.82	6.83	-208.91	-107.21	2.50	6.19
426	Copertura	4, 5	0	35.13	2.57	-208.15	84.05	2.42	4.62
			69	35.13	2.57	-172.05	20.57	-0.76	4.62
			138	35.13	2.57	-179.75	-42.91	-3.95	4.62
427	Copertura	5, 6	0	35.38	0.02	-179.19	78.80	-3.94	2.52
			69	35.38	0.02	-146.71	15.32	-5.67	2.52
			138	35.38	0.02	-158.04	-48.16	-7.41	2.52
428	Copertura	6, 7	0	46.00	-0.45	-157.69	99.56	-7.37	1.06
			69	46.00	-0.45	-110.89	36.08	-8.11	1.06
			138	46.00	-0.45	-107.90	-27.40	-8.84	1.06
429	Copertura	7, 8	0	41.15	-0.02	-107.85	80.68	-8.83	0.08
			69	41.15	-0.02	-74.09	17.20	-8.88	0.08
			138	41.15	-0.02	-84.12	-46.28	-8.93	0.08
430	Copertura	8, 9	0	41.13	0.39	-84.17	12.24	-8.94	-0.91
			69	41.13	0.39	-97.62	-51.24	-8.31	-0.91
			138	41.13	0.39	-154.88	-114.72	-7.68	-0.91
431	Copertura	9, 10	0	45.75	-0.08	-155.04	3.31	-7.71	-2.34
			69	45.75	-0.08	-174.66	-60.17	-6.10	-2.34
			138	45.75	-0.08	-238.08	-123.65	-4.49	-2.34
432	Copertura	10, 11	0	31.50	-2.64	-238.61	66.90	-4.49	-4.47
			69	31.50	-2.64	-214.34	3.42	-1.40	-4.47
			138	31.50	-2.64	-233.88	-60.06	1.68	-4.47
433	Copertura	11, 12	0	31.15	-6.87	-234.70	125.88	1.76	-6.00
			69	31.15	-6.87	-169.74	62.40	5.90	-6.00
			138	31.15	-6.87	-148.59	-1.08	10.04	-6.00
434	Copertura	12, 13	0	30.61	-5.27	-149.80	245.28	10.31	-1.83
			69	30.61	-5.27	-2.45	181.80	11.57	-1.83
			138	30.61	-5.27	101.09	118.32	12.84	-1.83
435	Copertura	13, 14	0	15.38	16.84	100.34	215.80	13.37	15.13
			83	15.38	16.84	247.94	139.33	0.79	15.13
			166	15.38	16.84	331.97	62.86	-11.78	15.13
436	Copertura	16, 14	0	-26.43	275.47	681.50	-464.55	-44.98	-58.69
			80	-26.43	275.47	312.18	-464.55	1.68	-58.69
			159	-26.43	275.47	-57.13	-464.55	48.33	-58.69
437	Copertura	15, 17	0	-27.18	-27.03	699.19	23.20	-8.32	-11.56
			66	-27.18	-27.03	714.50	23.20	-0.69	-11.56
			132	-27.18	-27.03	729.82	23.20	6.94	-11.56
438	Copertura	16, 18	0	-32.99	28.99	675.84	24.91	17.84	15.03
			66	-32.99	28.99	692.28	24.91	7.92	15.03
			132	-32.99	28.99	708.73	24.91	-2.00	15.03
439	Copertura	17, 19	0	-28.84	-2.68	725.95	-127.30	8.07	5.28
			66	-28.84	-2.68	641.93	-127.30	4.58	5.28
			132	-28.84	-2.68	557.91	-127.30	1.09	5.28
440	Copertura	18, 20	0	-35.90	2.91	704.41	-124.40	-2.88	-1.41
			66	-35.90	2.91	622.31	-124.40	-1.95	-1.41
			132	-35.90	2.91	540.21	-124.40	-1.02	-1.41
441	Copertura	19, 21	0	-29.80	2.10	555.74	-174.90	1.17	1.92
			66	-29.80	2.10	440.30	-174.90	-0.09	1.92
			132	-29.80	2.10	324.87	-174.90	-1.36	1.92
442	Copertura	20, 22	0	-37.13	-2.23	538.54	-154.73	-0.68	-0.22
			66	-37.13	-2.23	436.42	-154.73	-0.53	-0.22
			132	-37.13	-2.23	334.30	-154.73	-0.39	-0.22
443	Copertura	21, 23	0	-30.13	0.99	324.16	-181.09	-1.24	0.14
			66	-30.13	0.99	204.64	-181.09	-1.34	0.14
			132	-30.13	0.99	85.12	-181.09	-1.43	0.14
444	Copertura	22, 24	0	-36.34	-1.04	334.85	-157.51	0.11	0.93
			66	-36.34	-1.04	230.89	-157.51	-0.51	0.93
			132	-36.34	-1.04	126.93	-157.51	-1.12	0.93
445	Copertura	23, 25	0	-30.01	0.17	85.27	-122.31	-1.27	0.06
			66	-30.01	0.17	4.55	-122.31	-1.31	0.06
			132	-30.01	0.17	-76.18	-122.31	-1.35	0.06

446	Copertura	24, 26	0	-35.64	-0.11	128.08	-111.48	-0.84	0.72
			66	-35.64	-0.11	54.50	-111.48	-1.31	0.72
			132	-35.64	-0.11	-19.08	-111.48	-1.78	0.72
447	Copertura	25, 28	0	-30.34	-0.32	-76.70	-5.36	-1.30	0.00
			85	-30.34	-0.32	-81.25	-5.36	-1.29	0.00
			170	-30.34	-0.32	-85.81	-5.36	-1.29	0.00
448	Copertura	26, 27	0	-28.44	0.43	-11.64	-27.67	-1.69	-0.06
			66	-28.44	0.43	-29.90	-27.67	-1.65	-0.06
			132	-28.44	0.43	-48.16	-27.67	-1.60	-0.06
449	Copertura	27, 29	0	-35.06	0.58	-38.16	21.35	-1.66	-0.53
			66	-35.06	0.58	-24.07	21.35	-1.31	-0.53
			132	-35.06	0.58	-9.98	21.35	-0.96	-0.53
450	Copertura	28, 30	0	-30.68	-0.53	-102.85	72.99	-1.22	-0.15
			73	-30.68	-0.53	-49.57	72.99	-1.11	-0.15
			146	-30.68	-0.53	3.71	72.99	-1.00	-0.15
451	Copertura	29, 31	0	-35.42	0.30	11.83	12.21	-0.99	-0.28
			66	-35.42	0.30	19.88	12.21	-0.80	-0.28
			132	-35.42	0.30	27.94	12.21	-0.62	-0.28
452	Copertura	30, 32	0	-31.30	-0.21	-19.85	58.53	-1.04	-0.39
			69	-31.30	-0.21	20.25	58.53	-0.77	-0.39
			137	-31.30	-0.21	60.34	58.53	-0.51	-0.39
453	Copertura	31, 33	0	-38.53	0.21	49.56	-8.17	-0.74	-0.38
			66	-38.53	0.21	44.17	-8.17	-0.49	-0.38
			132	-38.53	0.21	38.77	-8.17	-0.24	-0.38
454	Copertura	32, 34	0	-31.77	-0.10	34.89	31.03	-0.64	-0.32
			69	-31.77	-0.10	56.30	31.03	-0.42	-0.32
			138	-31.77	-0.10	77.72	31.03	-0.20	-0.32
455	Copertura	33, 35	0	-39.17	0.22	65.31	-25.67	-0.33	-0.35
			66	-39.17	0.22	48.37	-25.67	-0.09	-0.35
			132	-39.17	0.22	31.43	-25.67	0.14	-0.35
456	Copertura	34, 36	0	-32.12	-0.10	49.90	20.84	-0.35	-0.38
			69	-32.12	-0.10	64.28	20.84	-0.09	-0.38
			138	-32.12	-0.10	78.65	20.84	0.17	-0.38
457	Copertura	35, 37	0	-42.14	0.20	58.41	-43.72	0.02	-0.65
			66	-42.14	0.20	29.55	-43.72	0.45	-0.65
			132	-42.14	0.20	0.70	-43.72	0.88	-0.65
458	Copertura	36, 38	0	-32.41	-0.16	48.43	25.04	0.02	-0.52
			69	-32.41	-0.16	65.70	25.04	0.38	-0.52
			138	-32.41	-0.16	82.97	25.04	0.74	-0.52
459	Copertura	37, 39	0	-44.07	0.21	31.18	-43.41	0.85	-0.53
			66	-44.07	0.21	2.52	-43.41	1.19	-0.53
			132	-44.07	0.21	-26.13	-43.41	1.54	-0.53
460	Copertura	38, 40	0	-32.66	-0.23	50.30	22.90	0.66	-0.58
			69	-32.66	-0.23	65.98	22.90	1.06	-0.58
			137	-32.66	-0.23	81.67	22.90	1.46	-0.58
461	Copertura	39, 41	0	-47.04	-0.13	5.22	-40.62	1.65	0.06
			66	-47.04	-0.13	-21.59	-40.62	1.62	0.06
			132	-47.04	-0.13	-48.39	-40.62	1.58	0.06
462	Copertura	40, 42	0	-32.85	0.14	47.02	-18.99	1.51	-0.57
			69	-32.85	0.14	33.91	-18.99	1.90	-0.57
			138	-32.85	0.14	20.81	-18.99	2.30	-0.57
463	Copertura	41, 44	0	-63.39	-1.06	-27.48	-46.09	1.82	0.38
			66	-63.39	-1.06	-57.90	-46.09	1.58	0.38
			132	-63.39	-1.06	-88.32	-46.09	1.33	0.38
464	Copertura	42, 43	0	-32.43	2.47	-15.48	2.84	2.48	0.03
			23	-32.43	2.47	-14.83	2.84	2.47	0.03
			46	-32.43	2.47	-14.17	2.84	2.47	0.03
465	Copertura	43, 45	0	-32.41	0.30	-13.99	63.56	2.53	1.06
			66	-32.41	0.30	27.96	63.56	1.83	1.06
			132	-32.41	0.30	69.91	63.56	1.12	1.06
466	Copertura	44, 46	0	-48.87	-0.25	-74.02	54.06	1.61	0.34
			66	-48.87	-0.25	-38.34	54.06	1.38	0.34
			132	-48.87	-0.25	-2.66	54.06	1.16	0.34
467	Copertura	45, 47	0	-32.31	0.01	70.23	87.27	1.36	1.27
			66	-32.31	0.01	127.83	87.27	0.52	1.27
			132	-32.31	0.01	185.43	87.27	-0.32	1.27
468	Copertura	46, 48	0	-48.44	0.03	-1.78	135.41	1.40	1.06
			66	-48.44	0.03	87.59	135.41	0.70	1.06
			132	-48.44	0.03	176.96	135.41	0.00	1.06
469	Copertura	47, 49	0	-31.99	-0.78	186.24	118.72	-0.02	1.32
			66	-31.99	-0.78	264.60	118.72	-0.89	1.32
			132	-31.99	-0.78	342.95	118.72	-1.77	1.32

470	Copertura	48, 50	0	-46.64	0.76	178.90	165.22	0.30	0.56
			66	-46.64	0.76	287.95	165.22	-0.07	0.56
			132	-46.64	0.76	396.99	165.22	-0.43	0.56
471	Copertura	49, 51	0	-31.27	-2.03	344.66	125.56	-1.35	-0.77
			66	-31.27	-2.03	427.53	125.56	-0.84	-0.77
			132	-31.27	-2.03	510.40	125.56	-0.33	-0.77
472	Copertura	50, 52	0	-44.52	1.99	399.55	173.91	-0.49	1.07
			66	-44.52	1.99	514.33	173.91	-1.20	1.07
			132	-44.52	1.99	629.11	173.91	-1.91	1.07
473	Copertura	51, 53	0	-29.96	2.55	513.48	118.85	0.08	-4.50
			66	-29.96	2.55	591.92	118.85	3.05	-4.50
			132	-29.96	2.55	670.35	118.85	6.02	-4.50
474	Copertura	52, 54	0	-41.42	-2.75	633.70	91.17	-2.07	3.09
			66	-41.42	-2.75	693.87	91.17	-4.11	3.09
			132	-41.42	-2.75	754.04	91.17	-6.15	3.09
475	Copertura	53, 55	0	-28.03	26.64	674.94	-14.11	5.13	13.81
			66	-28.03	26.64	665.63	-14.11	-3.98	13.81
			132	-28.03	26.64	656.32	-14.11	-13.09	13.81
476	Copertura	54, 56	0	-34.95	-27.65	762.06	-59.96	-3.03	-16.39
			66	-34.95	-27.65	722.48	-59.96	7.78	-16.39
			132	-34.95	-27.65	682.91	-59.96	18.60	-16.39
477	Copertura	55, 57	0	-25.79	277.74	661.78	-453.46	-19.58	-26.57
			80	-25.79	277.74	301.28	-453.46	1.54	-26.57
			159	-25.79	277.74	-59.22	-453.46	22.66	-26.57
478	Copertura	56, 70	0	-27.51	-276.96	693.09	-474.92	27.03	38.28
			80	-27.51	-276.96	315.53	-474.92	-3.40	38.28
			159	-27.51	-276.96	-62.02	-474.92	-33.84	38.28
479	Copertura	57, 58	0	14.50	17.29	300.79	-51.01	10.89	14.91
			83	14.50	17.29	226.60	-127.48	-1.51	14.91
			166	14.50	17.29	88.85	-203.96	-13.90	14.91
480	Copertura	58, 59	0	29.58	-5.17	89.59	-113.70	-13.37	-1.82
			69	29.58	-5.17	-10.77	-177.18	-12.12	-1.82
			138	29.58	-5.17	-154.92	-240.66	-10.86	-1.82
481	Copertura	59, 60	0	30.11	-6.74	-153.74	3.40	-10.60	-5.91
			69	30.11	-6.74	-173.30	-60.08	-6.53	-5.91
			138	30.11	-6.74	-236.66	-123.56	-2.45	-5.91
482	Copertura	60, 61	0	30.45	-2.57	-235.87	61.73	-2.37	-4.41
			69	30.45	-2.57	-215.18	-1.75	0.67	-4.41
			138	30.45	-2.57	-238.29	-65.23	3.72	-4.41
483	Copertura	61, 62	0	44.75	-0.05	-237.80	127.74	3.72	-2.34
			69	44.75	-0.05	-171.56	64.26	5.33	-2.34
			138	44.75	-0.05	-149.11	0.78	6.95	-2.34
484	Copertura	62, 63	0	39.42	0.43	-148.97	128.05	6.91	-0.99
			69	39.42	0.43	-82.52	64.57	7.59	-0.99
			138	39.42	0.43	-59.87	1.09	8.27	-0.99
485	Copertura	63, 64	0	39.40	0.02	-59.88	63.02	8.26	-0.06
			69	39.40	0.02	-38.30	-0.46	8.30	-0.06
			138	39.40	0.02	-60.52	-63.94	8.34	-0.06
486	Copertura	64, 65	0	39.40	-0.38	-60.55	-1.62	8.35	0.87
			69	39.40	-0.38	-83.57	-65.10	7.75	0.87
			138	39.40	-0.38	-150.39	-128.58	7.15	0.87
487	Copertura	65, 66	0	43.97	0.12	-150.58	-2.80	7.18	2.24
			69	43.97	0.12	-174.41	-66.28	5.63	2.24
			138	43.97	0.12	-242.04	-129.76	4.08	2.24
488	Copertura	66, 67	0	28.82	2.76	-242.58	66.11	4.08	4.36
			69	28.82	2.76	-218.87	2.63	1.08	4.36
			138	28.82	2.76	-238.96	-60.85	-1.93	4.36
489	Copertura	67, 68	0	28.46	7.13	-239.80	124.81	-2.01	5.85
			69	28.46	7.13	-175.58	61.33	-6.05	5.85
			138	28.46	7.13	-155.16	-2.15	-10.09	5.85
490	Copertura	68, 69	0	27.90	5.47	-156.40	242.80	-10.36	1.49
			69	27.90	5.47	-10.77	179.32	-11.40	1.49
			138	27.90	5.47	91.06	115.84	-12.43	1.49
491	Copertura	69, 70	0	12.05	-18.33	90.34	209.41	-12.98	-16.36
			83	12.05	-18.33	232.63	132.94	0.62	-16.36
			166	12.05	-18.33	311.35	56.47	14.22	-16.36
492	Copertura	1	0	-325.64	10.77	22.45	-10.58	-22.06	-3.69
			220	-325.64	10.77	-0.83	-10.58	-13.94	-3.69
			440	-325.64	10.77	-24.10	-10.58	-5.81	-3.69
493	Copertura	2	0	-137.78	-0.29	26.05	-17.56	-1.76	-0.90
			220	-137.78	-0.29	-12.57	-17.56	0.23	-0.90
			440	-137.78	-0.29	-51.19	-17.56	2.22	-0.90

494	Copertura	3	0	-253.62	-0.26	1.35	-4.00	-1.20	-0.54
			220	-253.62	-0.26	-7.45	-4.00	0.00	-0.54
			440	-253.62	-0.26	-16.26	-4.00	1.19	-0.54
495	Copertura	4	0	-191.27	-0.08	-4.27	1.57	-0.77	-0.31
			220	-191.27	-0.08	-0.81	1.57	-0.08	-0.31
			440	-191.27	-0.08	2.65	1.57	0.61	-0.31
496	Copertura	5	0	-121.71	0.02	-2.54	2.10	-0.57	-0.24
			220	-121.71	0.02	2.08	2.10	-0.03	-0.24
			440	-121.71	0.02	6.71	2.10	0.51	-0.24
497	Copertura	6	0	-114.37	0.03	-0.50	1.42	-0.36	-0.16
			220	-114.37	0.03	2.63	1.42	0.00	-0.16
			440	-114.37	0.03	5.76	1.42	0.35	-0.16
498	Copertura	7	0	-92.63	0.01	0.42	0.97	-0.05	-0.01
			220	-92.63	0.01	2.56	0.97	-0.04	-0.01
			440	-92.63	0.01	4.70	0.97	-0.02	-0.01
499	Copertura	8	0	-58.52	-0.01	0.41	0.99	0.05	0.02
			220	-58.52	-0.01	2.59	0.99	0.00	0.02
			440	-58.52	-0.01	4.77	0.99	-0.04	0.02
500	Copertura	9	0	-103.15	-0.03	-0.46	1.41	0.16	0.05
			220	-103.15	-0.03	2.63	1.41	0.05	0.05
			440	-103.15	-0.03	5.72	1.41	-0.06	0.05
501	Copertura	10	0	-145.83	-0.02	-2.50	2.07	0.52	0.22
			220	-145.83	-0.02	2.05	2.07	0.03	0.22
			440	-145.83	-0.02	6.59	2.07	-0.47	0.22
502	Copertura	11	0	-185.94	0.08	-4.24	1.53	0.82	0.35
			220	-185.94	0.08	-0.87	1.53	0.06	0.35
			440	-185.94	0.08	2.49	1.53	-0.70	0.35
503	Copertura	12	0	-246.36	0.27	1.61	-4.17	1.21	0.54
			220	-246.36	0.27	-7.57	-4.17	0.01	0.54
			440	-246.36	0.27	-16.74	-4.17	-1.19	0.54
504	Copertura	13	0	-137.58	0.28	26.66	-17.82	1.76	0.90
			220	-137.58	0.28	-12.55	-17.82	-0.22	0.90
			440	-137.58	0.28	-51.76	-17.82	-2.19	0.90
505	Copertura	57	0	-304.93	-10.85	-23.29	10.86	-21.54	-3.38
			220	-304.93	-10.85	0.60	10.86	-14.09	-3.38
			440	-304.93	-10.85	24.49	10.86	-6.65	-3.38
506	Copertura	58	0	-129.93	0.28	-26.42	17.57	-1.76	-0.90
			220	-129.93	0.28	12.24	17.57	0.23	-0.90
			440	-129.93	0.28	50.89	17.57	2.21	-0.90
507	Copertura	59	0	-244.05	0.26	-1.57	4.09	-1.18	-0.53
			220	-244.05	0.26	7.43	4.09	-0.01	-0.53
			440	-244.05	0.26	16.43	4.09	1.16	-0.53
508	Copertura	60	0	-185.29	0.08	4.17	-1.49	-0.78	-0.33
			220	-185.29	0.08	0.89	-1.49	-0.05	-0.33
			440	-185.29	0.08	-2.40	-1.49	0.68	-0.33
509	Copertura	61	0	-148.05	-0.02	2.46	-2.00	-0.49	-0.21
			220	-148.05	-0.02	-1.94	-2.00	-0.02	-0.21
			440	-148.05	-0.02	-6.34	-2.00	0.44	-0.21
510	Copertura	62	0	-110.13	-0.03	0.46	-1.34	-0.14	-0.05
			220	-110.13	-0.03	-2.49	-1.34	-0.04	-0.05
			440	-110.13	-0.03	-5.44	-1.34	0.06	-0.05
511	Copertura	63	0	-61.93	-0.01	-0.40	-0.93	0.01	0.02
			220	-61.93	-0.01	-2.45	-0.93	-0.03	0.02
			440	-61.93	-0.01	-4.49	-0.93	-0.07	0.02
512	Copertura	64	0	-62.32	0.01	-0.40	-0.93	0.03	0.00
			220	-62.32	0.01	-2.45	-0.93	0.03	0.00
			440	-62.32	0.01	-4.50	-0.93	0.02	0.00
513	Copertura	65	0	-111.01	0.03	0.49	-1.35	0.19	0.07
			220	-111.01	0.03	-2.49	-1.35	0.04	0.07
			440	-111.01	0.03	-5.47	-1.35	-0.10	0.07
514	Copertura	66	0	-148.31	0.01	2.58	-2.04	0.54	0.24
			220	-148.31	0.01	-1.91	-2.04	0.02	0.24
			440	-148.31	0.01	-6.40	-2.04	-0.50	0.24
515	Copertura	67	0	-185.66	-0.08	4.36	-1.50	0.84	0.36
			220	-185.66	-0.08	1.07	-1.50	0.05	0.36
			440	-185.66	-0.08	-2.23	-1.50	-0.73	0.36
516	Copertura	68	0	-244.95	-0.28	-1.65	4.36	1.24	0.56
			220	-244.95	-0.28	7.94	4.36	0.01	0.56
			440	-244.95	-0.28	17.53	4.36	-1.22	0.56
517	Copertura	69	0	-135.44	-0.30	-27.81	18.59	1.80	0.92
			220	-135.44	-0.30	13.08	18.59	-0.22	0.92
			440	-135.44	-0.30	53.97	18.59	-2.23	0.92

518	Primo Impalcato	1, 74	0	40.89	0.34	0.00	0.00	4.00	1.39
			118	40.89	0.34	0.00	0.00	2.37	1.39
			235	40.89	0.34	0.00	0.00	0.74	1.39
519	Copertura	74, 2	0	-107.16	-0.11	0.00	0.00	0.68	-0.58
			118	-107.16	-0.11	0.00	0.00	1.36	-0.58
			235	-107.16	-0.11	0.00	0.00	2.05	-0.58
520	Primo Impalcato	6, 71	0	-16.20	0.01	0.00	0.00	-0.12	-0.04
			115	-16.20	0.01	0.00	0.00	-0.08	-0.04
			231	-16.20	0.01	0.00	0.00	-0.04	-0.04
521	Copertura	71, 7	0	-34.94	0.00	0.00	0.00	-0.10	0.01
			115	-34.94	0.00	0.00	0.00	-0.11	0.01
			231	-34.94	0.00	0.00	0.00	-0.12	0.01
522	Primo Impalcato	9, 72	0	-46.88	0.00	0.00	0.00	-0.18	-0.03
			115	-46.88	0.00	0.00	0.00	-0.14	-0.03
			231	-46.88	0.00	0.00	0.00	-0.11	-0.03
523	Copertura	72, 10	0	-15.59	0.00	0.00	0.00	-0.03	0.06
			115	-15.59	0.00	0.00	0.00	-0.09	0.06
			231	-15.59	0.00	0.00	0.00	-0.16	0.06
524	Copertura	73, 13	0	-106.99	0.11	0.00	0.00	-0.62	0.62
			118	-106.99	0.11	0.00	0.00	-1.35	0.62
			235	-106.99	0.11	0.00	0.00	-2.09	0.62
525	Primo Impalcato	14, 73	0	42.86	-0.35	0.00	0.00	-3.98	-1.35
			118	42.86	-0.35	0.00	0.00	-2.39	-1.35
			235	42.86	-0.35	0.00	0.00	-0.81	-1.35
526	Primo Impalcato	57, 75	0	42.41	-0.34	0.00	0.00	-4.02	-1.40
			118	42.41	-0.34	0.00	0.00	-2.38	-1.40
			235	42.41	-0.34	0.00	0.00	-0.73	-1.40
527	Copertura	75, 58	0	-104.24	0.10	0.00	0.00	-0.66	0.58
			118	-104.24	0.10	0.00	0.00	-1.35	0.58
			235	-104.24	0.10	0.00	0.00	-2.03	0.58
528	Copertura	77, 61	0	-17.95	0.00	0.00	0.00	-0.02	0.06
			115	-17.95	0.00	0.00	0.00	-0.09	0.06
			231	-17.95	0.00	0.00	0.00	-0.15	0.06
529	Primo Impalcato	62, 77	0	-47.08	0.00	0.00	0.00	-0.17	-0.03
			115	-47.08	0.00	0.00	0.00	-0.14	-0.03
			231	-47.08	0.00	0.00	0.00	-0.10	-0.03
530	Primo Impalcato	65, 78	0	-49.84	0.00	0.00	0.00	0.17	0.03
			115	-49.84	0.00	0.00	0.00	0.14	0.03
			231	-49.84	0.00	0.00	0.00	0.10	0.03
531	Copertura	78, 66	0	-15.48	0.00	0.00	0.00	0.02	-0.06
			115	-15.48	0.00	0.00	0.00	0.09	-0.06
			231	-15.48	0.00	0.00	0.00	0.16	-0.06
532	Primo Impalcato	69, 76	0	-109.35	-0.11	0.00	0.00	-2.16	-0.63
			118	-109.35	-0.11	0.00	0.00	-1.42	-0.63
			235	-109.35	-0.11	0.00	0.00	-0.68	-0.63
533	Copertura	76, 70	0	44.75	0.36	0.00	0.00	-0.77	1.44
			118	44.75	0.36	0.00	0.00	-2.47	1.44
			235	44.75	0.36	0.00	0.00	-4.17	1.44
534	Copertura	1, 74	0	-107.16	0.02	0.00	0.00	-2.51	-1.24
			118	-107.16	0.02	0.00	0.00	-1.05	-1.24
			235	-107.16	0.02	0.00	0.00	0.40	-1.24
535	Copertura	74, 2	0	40.89	0.06	0.00	0.00	0.86	0.73
			118	40.89	0.06	0.00	0.00	0.00	0.73
			235	40.89	0.06	0.00	0.00	-0.86	0.73
536	Copertura	6, 71	0	-34.94	0.00	0.00	0.00	-0.02	0.03
			115	-34.94	0.00	0.00	0.00	-0.06	0.03
			231	-34.94	0.00	0.00	0.00	-0.10	0.03
537	Copertura	71, 7	0	-16.20	0.00	0.00	0.00	-0.04	-0.01
			115	-16.20	0.00	0.00	0.00	-0.02	-0.01
			231	-16.20	0.00	0.00	0.00	-0.01	-0.01
538	Copertura	9, 72	0	-15.59	0.00	0.00	0.00	0.01	0.02
			115	-15.59	0.00	0.00	0.00	-0.01	0.02
			231	-15.59	0.00	0.00	0.00	-0.03	0.02
539	Copertura	72, 10	0	-46.88	0.00	0.00	0.00	-0.11	-0.07
			115	-46.88	0.00	0.00	0.00	-0.02	-0.07

			231	-46.88	0.00	0.00	0.00	0.06	-0.07
540	Copertura	73, 13	0	42.86	-0.07	0.00	0.00	-0.93	-0.77
			118	42.86	-0.07	0.00	0.00	-0.02	-0.77
			235	42.86	-0.07	0.00	0.00	0.89	-0.77
541	Copertura	14, 73	0	-106.99	-0.03	0.00	0.00	2.47	1.20
			118	-106.99	-0.03	0.00	0.00	1.06	1.20
			235	-106.99	-0.03	0.00	0.00	-0.35	1.20
542	Copertura	15, 125	0	1133.72	-1.69	-152.69	-90.80	-4.25	-3.53
			75	1133.72	-1.69	-261.29	-198.80	-1.59	-3.53
			150	1133.72	-1.69	-450.90	-306.80	1.06	-3.53
543	Copertura	127, 16	0	1164.99	5.17	-489.60	328.82	6.55	14.63
			75	1164.99	5.17	-283.48	220.82	-4.43	14.63
			150	1164.99	5.17	-158.37	112.82	-15.40	14.63
544	Copertura	17, 129	0	994.89	-0.36	64.33	-2.26	-0.63	-0.61
			75	994.89	-0.36	25.52	-101.26	-0.17	-0.61
			150	994.89	-0.36	-87.55	-200.26	0.29	-0.61
545	Copertura	130, 18	0	994.61	0.38	-88.55	199.79	0.62	0.66
			75	994.61	0.38	24.17	100.79	0.13	0.66
			150	994.61	0.38	62.64	1.79	-0.37	0.66
546	Copertura	19, 135	0	1019.09	-0.05	84.29	-6.36	-0.15	0.07
			75	1019.09	-0.05	42.39	-105.36	-0.20	0.07
			150	1019.09	-0.05	-73.75	-204.36	-0.25	0.07
547	Copertura	134, 20	0	1016.46	0.05	-70.46	202.46	0.29	-0.03
			75	1016.46	0.05	44.27	103.46	0.31	-0.03
			150	1016.46	0.05	84.74	4.46	0.33	-0.03
548	Copertura	21, 136	0	1021.48	0.00	89.46	-19.02	-0.18	0.05
			75	1021.48	0.00	38.07	-118.02	-0.21	0.05
			150	1021.48	0.00	-87.57	-217.02	-0.25	0.05
549	Copertura	138, 22	0	1020.53	-0.06	-86.33	216.34	0.14	-0.17
			75	1020.53	-0.06	38.80	117.34	0.27	-0.17
			150	1020.53	-0.06	89.68	18.34	0.40	-0.17
550	Copertura	23, 141	0	1022.33	0.01	90.71	-24.25	-0.17	-0.01
			75	1022.33	0.01	35.40	-123.25	-0.16	-0.01
			150	1022.33	0.01	-94.16	-222.25	-0.16	-0.01
551	Copertura	142, 24	0	1021.60	-0.06	-93.51	221.66	0.09	-0.09
			75	1021.60	-0.06	35.61	122.66	0.16	-0.09
			150	1021.60	-0.06	90.49	23.66	0.23	-0.09
552	Copertura	25, 145	0	1024.56	0.00	92.22	-26.47	-0.06	-0.01
			75	1024.56	0.00	35.24	-125.47	-0.05	-0.01
			150	1024.56	0.00	-95.99	-224.47	-0.04	-0.01
553	Copertura	146, 26	0	1022.24	-0.24	-94.00	222.57	-0.17	-0.19
			75	1022.24	-0.24	35.81	123.57	-0.03	-0.19
			150	1022.24	-0.24	91.36	24.57	0.11	-0.19
554	Copertura	150, 27	0	1020.75	-0.47	-93.53	220.54	-0.33	-0.22
			75	1020.75	-0.47	34.76	121.54	-0.17	-0.22
			150	1020.75	-0.47	88.79	22.54	0.00	-0.22
555	Copertura	28, 149	0	1021.88	-0.72	88.84	-23.47	-0.10	-0.45
			75	1021.88	-0.72	34.11	-122.47	0.23	-0.45
			150	1021.88	-0.72	-94.87	-221.47	0.57	-0.45
556	Copertura	154, 29	0	1018.10	-0.90	-91.92	216.64	-0.79	-0.56
			75	1018.10	-0.90	33.44	117.64	-0.37	-0.56
			150	1018.10	-0.90	84.54	18.64	0.05	-0.56
557	Copertura	30, 153	0	1017.47	-0.97	83.97	-18.09	-0.04	-0.58
			75	1017.47	-0.97	33.28	-117.09	0.40	-0.58
			150	1017.47	-0.97	-91.66	-216.09	0.83	-0.58
558	Copertura	158, 31	0	1017.26	-0.92	-91.00	215.74	-0.84	-0.53
			75	1017.26	-0.92	33.68	116.74	-0.44	-0.53
			150	1017.26	-0.92	84.11	17.74	-0.04	-0.53
559	Copertura	32, 157	0	1016.33	-1.04	83.16	-16.93	0.03	-0.61
			75	1016.33	-1.04	33.34	-115.93	0.49	-0.61
			150	1016.33	-1.04	-90.73	-214.93	0.94	-0.61
560	Copertura	162, 33	0	1016.18	-1.10	-90.68	214.71	-1.02	-0.68
			75	1016.18	-1.10	33.23	115.71	-0.52	-0.68
			150	1016.18	-1.10	82.89	16.71	-0.01	-0.68
561	Copertura	34, 161	0	1016.61	-1.13	82.89	-17.06	0.04	-0.66
			75	1016.61	-1.13	32.97	-116.06	0.54	-0.66
			150	1016.61	-1.13	-91.21	-215.06	1.04	-0.66
562	Copertura	166, 35	0	1015.62	-1.13	-90.45	214.19	-1.03	-0.67
			75	1015.62	-1.13	33.06	115.19	-0.53	-0.67
			150	1015.62	-1.13	82.32	16.19	-0.03	-0.67
563	Copertura	36, 165	0	1016.77	-1.23	82.40	-17.13	0.02	-0.73
			75	1016.77	-1.23	32.43	-116.13	0.57	-0.73

			150	1016.77	-1.23	-91.79	-215.13	1.11	-0.73
564	Copertura	170, 37	0	1015.50	-1.27	-90.82	213.89	-1.10	-0.78
			75	1015.50	-1.27	32.48	114.89	-0.52	-0.78
			150	1015.50	-1.27	81.52	15.89	0.07	-0.78
565	Copertura	38, 169	0	1015.90	-1.33	81.20	-16.20	-0.05	-0.80
			75	1015.90	-1.33	31.93	-115.20	0.55	-0.80
			150	1015.90	-1.33	-91.59	-214.20	1.15	-0.80
566	Copertura	175, 39	0	1016.01	-1.32	-91.20	213.63	-1.04	-0.83
			75	1016.01	-1.32	31.90	114.63	-0.41	-0.83
			150	1016.01	-1.32	80.75	15.63	0.21	-0.83
567	Copertura	40, 173	0	1013.87	-1.41	78.80	-13.77	-0.19	-0.87
			75	1013.87	-1.41	31.35	-112.77	0.47	-0.87
			150	1013.87	-1.41	-90.36	-211.77	1.12	-0.87
568	Copertura	178, 41	0	1017.72	-1.03	-93.56	215.99	-0.59	-0.59
			75	1017.72	-1.03	31.30	116.99	-0.15	-0.59
			150	1017.72	-1.03	81.91	17.99	0.29	-0.59
569	Copertura	42, 177	0	1014.03	-1.49	77.82	-14.89	-0.35	-0.90
			75	1014.03	-1.49	29.53	-113.89	0.33	-0.90
			150	1014.03	-1.49	-93.01	-212.89	1.01	-0.90
570	Copertura	43, 181	0	1020.07	0.04	92.28	-20.88	-0.09	0.00
			75	1020.07	0.04	39.49	-119.88	-0.08	0.00
			150	1020.07	0.04	-87.54	-218.88	-0.08	0.00
571	Copertura	182, 44	0	1022.58	-0.46	-90.56	220.78	-0.38	-0.45
			75	1022.58	-0.46	37.90	121.78	-0.05	-0.45
			150	1022.58	-0.46	92.12	22.78	0.29	-0.45
572	Copertura	45, 185	0	1020.17	0.02	89.46	-20.66	-0.24	-0.02
			75	1020.17	0.02	36.84	-119.66	-0.22	-0.02
			150	1020.17	0.02	-90.03	-218.66	-0.21	-0.02
573	Copertura	186, 46	0	1022.12	-0.03	-91.15	220.34	0.17	-0.04
			75	1022.12	-0.03	36.97	121.34	0.20	-0.04
			150	1022.12	-0.03	90.85	22.34	0.23	-0.04
574	Copertura	47, 189	0	1021.29	0.04	90.09	-22.11	-0.30	-0.03
			75	1021.29	0.04	36.38	-121.11	-0.28	-0.03
			150	1021.29	0.04	-91.58	-220.11	-0.27	-0.03
575	Copertura	190, 48	0	1019.18	-0.06	-89.36	218.44	0.18	-0.08
			75	1019.18	-0.06	37.35	119.44	0.24	-0.08
			150	1019.18	-0.06	89.80	20.44	0.30	-0.08
576	Copertura	49, 193	0	1022.52	0.04	90.07	-19.28	-0.36	-0.10
			75	1022.52	0.04	38.48	-118.28	-0.28	-0.10
			150	1022.52	0.04	-87.35	-217.28	-0.21	-0.10
577	Copertura	195, 50	0	1019.06	-0.03	-83.40	214.64	0.22	0.09
			75	1019.06	-0.03	40.46	115.64	0.15	0.09
			150	1019.06	-0.03	90.07	16.64	0.08	0.09
578	Copertura	51, 197	0	1020.84	0.08	85.69	-7.61	-0.33	-0.12
			75	1020.84	0.08	42.86	-106.61	-0.24	-0.12
			150	1020.84	0.08	-74.22	-205.61	-0.15	-0.12
579	Copertura	199, 52	0	1014.31	-0.11	-68.66	200.22	0.07	0.07
			75	1014.31	-0.11	44.38	101.22	0.01	0.07
			150	1014.31	-0.11	83.18	2.22	-0.04	0.07
580	Copertura	53, 201	0	994.22	0.41	65.17	-2.75	0.39	0.58
			75	994.22	0.41	25.98	-101.75	-0.05	0.58
			150	994.22	0.41	-87.46	-200.75	-0.48	0.58
581	Copertura	202, 54	0	991.91	-0.86	-85.72	198.84	-1.01	-1.83
			75	991.91	-0.86	26.28	99.84	0.37	-1.83
			150	991.91	-0.86	64.04	0.84	1.75	-1.83
582	Copertura	55, 205	0	1142.36	1.51	-152.99	-92.62	3.57	3.52
			75	1142.36	1.51	-262.96	-200.62	0.93	3.52
			150	1142.36	1.51	-453.92	-308.62	-1.71	3.52
583	Copertura	206, 56	0	1159.14	-1.89	-472.87	321.11	-1.77	-4.46
			75	1159.14	-1.89	-272.53	213.11	1.58	-4.46
			150	1159.14	-1.89	-153.20	105.11	4.93	-4.46
584	Copertura	57, 75	0	-104.24	-0.02	0.00	0.00	2.56	1.25
			118	-104.24	-0.02	0.00	0.00	1.08	1.25
			235	-104.24	-0.02	0.00	0.00	-0.39	1.25
585	Copertura	75, 58	0	42.41	-0.07	0.00	0.00	-0.85	-0.73
			118	42.41	-0.07	0.00	0.00	0.01	-0.73
			235	42.41	-0.07	0.00	0.00	0.86	-0.73
586	Copertura	77, 61	0	-47.08	0.00	0.00	0.00	-0.10	-0.07
			115	-47.08	0.00	0.00	0.00	-0.02	-0.07
			231	-47.08	0.00	0.00	0.00	0.06	-0.07
587	Copertura	62, 77	0	-17.95	0.00	0.00	0.00	0.01	0.02
			115	-17.95	0.00	0.00	0.00	-0.01	0.02

			231	-17.95	0.00	0.00	0.00	-0.02	0.02
588	Copertura	65, 78	0	-15.48	0.00	0.00	0.00	-0.01	-0.02
			115	-15.48	0.00	0.00	0.00	0.01	-0.02
			231	-15.48	0.00	0.00	0.00	0.02	-0.02
589	Copertura	78, 66	0	-49.84	0.00	0.00	0.00	0.10	0.07
			115	-49.84	0.00	0.00	0.00	0.02	0.07
			231	-49.84	0.00	0.00	0.00	-0.07	0.07
590	Copertura	69, 76	0	44.75	0.07	0.00	0.00	0.89	0.76
			118	44.75	0.07	0.00	0.00	0.00	0.76
			235	44.75	0.07	0.00	0.00	-0.89	0.76
591	Copertura	76, 70	0	-109.35	0.03	0.00	0.00	-0.40	-1.32
			118	-109.35	0.03	0.00	0.00	1.15	-1.32
			235	-109.35	0.03	0.00	0.00	2.69	-1.32
592	Copertura	79, 81	0	-2.34	1.29	-10.40	12.71	43.03	50.36
			80	-2.34	1.29	-0.29	12.71	3.00	50.36
			159	-2.34	1.29	9.82	12.71	-37.04	50.36
593	Copertura	80, 82	0	2.53	0.31	-3.16	4.73	-15.12	-5.95
			66	2.53	0.31	-0.04	4.73	-11.19	-5.95
			132	2.53	0.31	3.09	4.73	-7.26	-5.95
594	Copertura	83, 84	0	-0.94	-0.02	-1.03	1.35	-0.39	-0.64
			66	-0.94	-0.02	-0.14	1.35	0.03	-0.64
			132	-0.94	-0.02	0.75	1.35	0.46	-0.64
595	Copertura	85, 86	0	-6.54	0.00	-0.24	0.86	0.07	0.05
			66	-6.54	0.00	0.33	0.86	0.04	0.05
			132	-6.54	0.00	0.90	0.86	0.01	0.05
596	Copertura	87, 88	0	-12.45	0.00	-3.97	6.82	-0.07	0.01
			66	-12.45	0.00	0.54	6.82	-0.08	0.01
			132	-12.45	0.00	5.04	6.82	-0.08	0.01
597	Copertura	89, 90	0	-5.19	0.00	-7.10	11.07	-0.07	-0.02
			66	-5.19	0.00	0.20	11.07	-0.06	-0.02
			132	-5.19	0.00	7.51	11.07	-0.04	-0.02
598	Copertura	91, 92	0	-3.30	0.00	-8.24	12.68	-0.06	-0.02
			66	-3.30	0.00	0.13	12.68	-0.04	-0.02
			132	-3.30	0.00	8.49	12.68	-0.02	-0.02
599	Copertura	93, 94	0	11.89	0.00	-7.26	10.05	-0.06	-0.02
			66	11.89	0.00	-0.63	10.05	-0.05	-0.02
			132	11.89	0.00	6.00	10.05	-0.04	-0.02
600	Copertura	95, 96	0	19.20	0.00	-3.64	4.72	0.10	0.00
			66	19.20	0.00	-0.52	4.72	0.10	0.00
			132	19.20	0.00	2.59	4.72	0.10	0.00
601	Copertura	97, 106	0	2.06	0.00	0.58	-0.92	0.25	-0.03
			66	2.06	0.00	-0.02	-0.92	0.26	-0.03
			132	2.06	0.00	-0.63	-0.92	0.28	-0.03
602	Copertura	98, 99	0	0.46	0.03	-2.92	4.15	-2.49	-1.52
			66	0.46	0.03	-0.19	4.15	-1.49	-1.52
			132	0.46	0.03	2.55	4.15	-0.49	-1.52
603	Copertura	100, 101	0	-1.21	-0.02	0.73	-1.39	0.12	-0.01
			66	-1.21	-0.02	-0.19	-1.39	0.13	-0.01
			132	-1.21	-0.02	-1.11	-1.39	0.13	-0.01
604	Copertura	102, 103	0	-12.11	0.00	0.88	-0.75	0.02	0.00
			66	-12.11	0.00	0.38	-0.75	0.02	0.00
			132	-12.11	0.00	-0.12	-0.75	0.02	0.00
605	Copertura	104, 105	0	-3.55	0.00	-1.34	1.83	-0.11	-0.14
			66	-3.55	0.00	-0.14	1.83	-0.02	-0.14
			132	-3.55	0.00	1.07	1.83	0.07	-0.14
606	Copertura	107, 108	0	-1.93	-0.01	3.59	-5.71	-1.05	1.91
			66	-1.93	-0.01	-0.17	-5.71	-2.30	1.91
			132	-1.93	-0.01	-3.94	-5.71	-3.56	1.91
607	Copertura	109, 110	0	-13.73	1.14	6.08	-8.02	-26.35	-40.22
			80	-13.73	1.14	-0.29	-8.02	5.63	-40.22
			159	-13.73	1.14	-6.67	-8.02	37.61	-40.22
608	Copertura	111, 112	0	-2.80	0.13	-1.66	2.25	-0.12	-0.17
			66	-2.80	0.13	-0.18	2.25	-0.01	-0.17
			132	-2.80	0.13	1.31	2.25	0.10	-0.17
609	Copertura	113, 114	0	-0.12	0.00	-1.43	2.47	-0.11	-0.19
			66	-0.12	0.00	0.20	2.47	0.02	-0.19
			132	-0.12	0.00	1.82	2.47	0.15	-0.19
610	Copertura	115, 116	0	27.43	0.00	-0.95	0.27	-0.15	-0.22
			66	27.43	0.00	-0.78	0.27	0.00	-0.22
			132	27.43	0.00	-0.60	0.27	0.14	-0.22
611	Copertura	117, 118	0	2.29	0.00	1.10	-1.37	0.01	-0.04
			66	2.29	0.00	0.19	-1.37	0.04	-0.04

			132	2.29	0.00	-0.72	-1.37	0.06	-0.04
612	Copertura	119, 120	0	-0.42	0.05	2.77	-4.52	0.35	0.63
			66	-0.42	0.05	-0.21	-4.52	-0.06	0.63
			132	-0.42	0.05	-3.20	-4.52	-0.48	0.63
613	Copertura	121, 122	0	-1.45	-0.67	8.16	-13.03	-4.31	2.06
			66	-1.45	-0.67	-0.44	-13.03	-5.67	2.06
			132	-1.45	-0.67	-9.04	-13.03	-7.03	2.06
614	Copertura	124, 125	0	-2086.39	0.20	-106.39	71.25	4.99	3.44
			99	-2086.39	0.20	-35.68	71.25	1.58	3.44
			198	-2086.39	0.20	35.03	71.25	-1.84	3.44
615	Copertura	125, 127	0	-396.28	-0.34	-415.87	1113.48	-0.20	-0.09
			775	-396.28	-0.34	3889.07	-2.52	0.53	-0.09
			1550	-396.28	-0.34	-454.99	-1118.52	1.27	-0.09
616	Copertura	126, 127	0	-2127.75	-0.70	-106.76	71.22	-21.64	-14.73
			99	-2127.75	-0.70	-36.07	71.22	-7.03	-14.73
			198	-2127.75	-0.70	34.61	71.22	7.59	-14.73
617	Copertura	128, 129	0	-1787.49	0.06	-99.76	69.48	0.70	0.59
			99	-1787.49	0.06	-30.80	69.48	0.11	0.59
			198	-1787.49	0.06	38.15	69.48	-0.48	0.59
618	Copertura	129, 130	0	-310.40	0.00	-49.40	1022.93	-0.04	-0.02
			775	-310.40	0.00	3914.20	-0.07	0.12	-0.02
			1550	-310.40	0.00	-50.44	-1023.07	0.28	-0.02
619	Copertura	131, 130	0	-1787.07	-0.06	-99.68	69.42	-0.84	-0.68
			99	-1787.07	-0.06	-30.79	69.42	-0.17	-0.68
			198	-1787.07	-0.06	38.10	69.42	0.50	-0.68
620	Copertura	132, 135	0	-1793.37	0.01	-100.46	70.19	-0.27	-0.10
			99	-1793.37	0.01	-30.79	70.19	-0.17	-0.10
			198	-1793.37	0.01	38.87	70.19	-0.07	-0.10
621	Copertura	133, 134	0	-1789.86	-0.01	-100.34	70.15	0.04	-0.01
			99	-1789.86	-0.01	-30.72	70.15	0.05	-0.01
			198	-1789.86	-0.01	38.91	70.15	0.06	-0.01
622	Copertura	135, 134	0	-290.17	0.00	-34.88	1023.22	-0.29	-0.04
			775	-290.17	0.00	3930.91	0.22	-0.02	-0.04
			1550	-290.17	0.00	-31.55	-1022.78	0.25	-0.04
623	Copertura	137, 136	0	-1812.08	0.00	-101.03	70.56	-0.17	-0.08
			99	-1812.08	0.00	-31.00	70.56	-0.09	-0.08
			198	-1812.08	0.00	39.02	70.56	-0.01	-0.08
624	Copertura	136, 138	0	-301.68	0.01	-48.55	1023.08	-0.26	-0.03
			775	-301.68	0.01	3916.20	0.08	-0.02	-0.03
			1550	-301.68	0.01	-47.30	-1022.92	0.21	-0.03
625	Copertura	139, 138	0	-1810.81	0.00	-100.99	70.54	0.19	0.14
			99	-1810.81	0.00	-30.98	70.54	0.04	0.14
			198	-1810.81	0.00	39.03	70.54	-0.10	0.14
626	Copertura	140, 141	0	-1819.82	0.00	-101.21	70.72	-0.03	-0.02
			99	-1819.82	0.00	-31.03	70.72	-0.01	-0.02
			198	-1819.82	0.00	39.15	70.72	0.00	-0.02
627	Copertura	141, 142	0	-306.57	0.01	-55.01	1023.04	-0.16	-0.02
			775	-306.57	0.01	3909.43	0.04	0.00	-0.02
			1550	-306.57	0.01	-54.39	-1022.96	0.16	-0.02
628	Copertura	143, 142	0	-1818.83	0.01	-101.19	70.69	0.05	0.07
			99	-1818.83	0.01	-31.03	70.69	-0.02	0.07
			198	-1818.83	0.01	39.12	70.69	-0.10	0.07
629	Copertura	144, 145	0	-1823.17	0.00	-101.34	70.86	-0.03	0.00
			99	-1823.17	0.00	-31.01	70.86	-0.03	0.00
			198	-1823.17	0.00	39.31	70.86	-0.03	0.00
630	Copertura	145, 146	0	-306.78	0.02	-56.68	1023.12	-0.07	-0.01
			775	-306.78	0.02	3908.40	0.12	0.01	-0.01
			1550	-306.78	0.02	-54.78	-1022.88	0.08	-0.01
631	Copertura	147, 146	0	-1820.01	0.03	-101.23	70.76	0.00	0.18
			99	-1820.01	0.03	-31.01	70.76	-0.18	0.18
			198	-1820.01	0.03	39.22	70.76	-0.36	0.18
632	Copertura	148, 149	0	-1819.00	0.06	-101.28	70.79	0.12	0.45
			99	-1819.00	0.06	-31.03	70.79	-0.33	0.45
			198	-1819.00	0.06	39.22	70.79	-0.78	0.45
633	Copertura	149, 150	0	-306.36	-0.17	-55.65	1023.34	0.02	0.00
			775	-306.36	-0.17	3911.10	0.08	-0.01	0.00
			1550	-306.36	-0.17	-54.39	-1023.18	-0.03	0.00
634	Copertura	151, 150	0	-1817.43	0.03	-101.20	70.70	0.02	0.23
			99	-1817.43	0.03	-31.03	70.70	-0.20	0.23
			198	-1817.43	0.03	39.14	70.70	-0.43	0.23
635	Copertura	152, 153	0	-1811.21	0.08	-101.10	70.58	0.11	0.59
			99	-1811.21	0.08	-31.06	70.58	-0.47	0.59

			198	-1811.21	0.08	38.99	70.58	-1.06	0.59
636	Copertura	153, 154	0	-305.02	-0.21	-52.67	1023.47	0.08	0.01
			775	-305.02	-0.21	3915.08	-0.01	-0.01	0.01
			1551	-305.02	-0.21	-52.90	-1023.50	-0.09	0.01
637	Copertura	155, 154	0	-1812.07	0.06	-101.14	70.61	0.16	0.57
			99	-1812.07	0.06	-31.06	70.61	-0.41	0.57
			198	-1812.07	0.06	39.02	70.61	-0.98	0.57
638	Copertura	156, 157	0	-1809.60	0.08	-101.10	70.57	0.11	0.63
			99	-1809.60	0.08	-31.06	70.57	-0.51	0.63
			198	-1809.60	0.08	38.98	70.57	-1.13	0.63
639	Copertura	157, 158	0	-304.94	-0.24	-51.76	1023.56	0.14	0.02
			775	-304.94	-0.24	3916.74	-0.02	-0.01	0.02
			1551	-304.94	-0.24	-52.00	-1023.59	-0.16	0.02
640	Copertura	159, 158	0	-1810.85	0.07	-101.13	70.60	0.14	0.55
			99	-1810.85	0.07	-31.06	70.60	-0.41	0.55
			198	-1810.85	0.07	39.00	70.60	-0.96	0.55
641	Copertura	160, 161	0	-1810.00	0.09	-101.17	70.64	0.13	0.69
			99	-1810.00	0.09	-31.06	70.64	-0.55	0.69
			198	-1810.00	0.09	39.04	70.64	-1.24	0.69
642	Copertura	161, 162	0	-304.92	-0.25	-52.16	1023.74	0.17	0.02
			776	-304.92	-0.25	3917.70	0.03	-0.01	0.02
			1551	-304.92	-0.25	-51.66	-1023.68	-0.18	0.02
643	Copertura	163, 162	0	-1809.39	0.08	-101.13	70.61	0.20	0.70
			99	-1809.39	0.08	-31.06	70.61	-0.50	0.70
			198	-1809.39	0.08	39.02	70.61	-1.19	0.70
644	Copertura	164, 165	0	-1810.31	0.10	-101.24	70.70	0.15	0.75
			99	-1810.31	0.10	-31.07	70.70	-0.60	0.75
			198	-1810.31	0.10	39.10	70.70	-1.34	0.75
645	Copertura	165, 166	0	-304.96	-0.28	-52.69	1023.93	0.16	0.02
			776	-304.96	-0.28	3918.65	0.08	-0.01	0.02
			1551	-304.96	-0.28	-51.43	-1023.77	-0.18	0.02
646	Copertura	167, 166	0	-1808.72	0.09	-101.15	70.62	0.17	0.69
			99	-1808.72	0.09	-31.06	70.62	-0.51	0.69
			198	-1808.72	0.09	39.03	70.62	-1.20	0.69
647	Copertura	168, 169	0	-1809.06	0.10	-101.26	70.72	0.18	0.82
			99	-1809.06	0.10	-31.08	70.72	-0.64	0.82
			198	-1809.06	0.10	39.11	70.72	-1.45	0.82
648	Copertura	169, 170	0	-304.87	-0.30	-52.49	1024.05	0.12	0.02
			776	-304.87	-0.30	3919.80	0.05	-0.01	0.02
			1552	-304.87	-0.30	-51.73	-1023.95	-0.13	0.02
649	Copertura	171, 170	0	-1808.49	0.10	-101.19	70.67	0.22	0.80
			99	-1808.49	0.10	-31.05	70.67	-0.58	0.80
			198	-1808.49	0.10	39.09	70.67	-1.37	0.80
650	Copertura	172, 173	0	-1805.51	0.10	-101.20	70.64	0.20	0.88
			99	-1805.51	0.10	-31.09	70.64	-0.67	0.88
			198	-1805.51	0.10	39.01	70.64	-1.54	0.88
651	Copertura	173, 175	0	-304.27	-0.32	-51.35	1024.09	0.02	0.00
			776	-304.27	-0.32	3921.26	-0.05	-0.01	0.00
			1552	-304.27	-0.32	-52.08	-1024.19	-0.03	0.00
652	Copertura	174, 175	0	-1808.41	0.09	-101.25	70.71	0.25	0.84
			99	-1808.41	0.09	-31.06	70.71	-0.58	0.84
			198	-1808.41	0.09	39.12	70.71	-1.41	0.84
653	Copertura	176, 177	0	-1807.39	0.10	-101.25	70.73	0.19	0.89
			99	-1807.39	0.10	-31.05	70.73	-0.70	0.89
			198	-1807.39	0.10	39.15	70.73	-1.58	0.89
654	Copertura	177, 178	0	-305.47	-0.38	-53.87	1024.28	-0.12	-0.01
			776	-305.47	-0.38	3920.17	-0.04	-0.03	-0.01
			1552	-305.47	-0.38	-54.49	-1024.36	0.07	-0.01
655	Copertura	179, 178	0	-1812.26	0.06	-101.29	70.72	0.22	0.58
			99	-1812.26	0.06	-31.11	70.72	-0.35	0.58
			198	-1812.26	0.06	39.08	70.72	-0.92	0.58
656	Copertura	180, 181	0	-1814.36	0.00	-101.09	70.67	-0.03	-0.01
			99	-1814.36	0.00	-30.95	70.67	-0.02	-0.01
			198	-1814.36	0.00	39.19	70.67	-0.01	-0.01
657	Copertura	181, 182	0	-304.74	0.05	-48.35	1022.81	-0.09	-0.01
			775	-304.74	0.05	3914.31	-0.19	0.02	-0.01
			1550	-304.74	0.05	-51.28	-1023.19	0.13	-0.01
658	Copertura	183, 182	0	-1817.76	0.05	-101.17	70.75	0.14	0.43
			99	-1817.76	0.05	-30.95	70.75	-0.29	0.43
			198	-1817.76	0.05	39.27	70.75	-0.72	0.43
659	Copertura	184, 185	0	-1814.32	0.00	-101.05	70.58	0.00	0.00
			99	-1814.32	0.00	-30.99	70.58	0.00	0.00

			198	-1814.32	0.00	39.06	70.58	0.00	0.00
660	Copertura	185, 186	0	-304.66	0.01	-50.97	1022.94	-0.21	-0.03
			775	-304.66	0.01	3912.66	-0.06	0.00	-0.03
			1550	-304.66	0.01	-51.96	-1023.06	0.21	-0.03
661	Copertura	187, 186	0	-1816.98	0.01	-101.10	70.67	-0.03	0.01
			99	-1816.98	0.01	-30.95	70.67	-0.05	0.01
			198	-1816.98	0.01	39.19	70.67	-0.06	0.01
662	Copertura	188, 189	0	-1816.78	-0.01	-101.14	70.65	0.01	-0.01
			99	-1816.78	-0.01	-31.02	70.65	0.02	-0.01
			198	-1816.78	-0.01	39.10	70.65	0.02	-0.01
663	Copertura	189, 190	0	-305.35	0.02	-52.48	1023.14	-0.25	-0.03
			775	-305.35	0.02	3912.74	0.14	0.00	-0.03
			1550	-305.35	0.02	-50.30	-1022.86	0.26	-0.03
664	Copertura	191, 190	0	-1813.90	0.01	-101.00	70.56	-0.02	0.05
			99	-1813.90	0.01	-30.97	70.56	-0.07	0.05
			198	-1813.90	0.01	39.06	70.56	-0.11	0.05
665	Copertura	192, 193	0	-1812.68	-0.01	-101.07	70.60	0.18	0.07
			99	-1812.68	-0.01	-31.00	70.60	0.10	0.07
			198	-1812.68	-0.01	39.07	70.60	0.03	0.07
666	Copertura	193, 195	0	-301.06	0.01	-48.28	1023.25	-0.19	-0.03
			775	-301.06	0.01	3917.81	0.25	0.03	-0.03
			1550	-301.06	0.01	-44.35	-1022.75	0.25	-0.03
667	Copertura	194, 195	0	-1808.00	0.00	-100.88	70.49	-0.29	-0.12
			99	-1808.00	0.00	-30.92	70.49	-0.17	-0.12
			198	-1808.00	0.00	39.05	70.49	-0.05	-0.12
668	Copertura	196, 197	0	-1795.35	-0.02	-100.54	70.29	0.29	0.10
			99	-1795.35	-0.02	-30.77	70.29	0.19	0.10
			198	-1795.35	-0.02	38.99	70.29	0.08	0.10
669	Copertura	197, 199	0	-289.84	0.01	-35.23	1023.34	-0.11	-0.02
			775	-289.84	0.01	3931.55	0.34	0.03	-0.02
			1550	-289.84	0.01	-29.92	-1022.66	0.17	-0.02
670	Copertura	198, 199	0	-1786.44	0.02	-100.18	69.99	-0.34	-0.09
			99	-1786.44	0.02	-30.72	69.99	-0.25	-0.09
			198	-1786.44	0.02	38.74	69.99	-0.16	-0.09
671	Copertura	200, 201	0	-1788.46	-0.07	-99.81	69.53	-0.67	-0.58
			99	-1788.46	-0.07	-30.80	69.53	-0.09	-0.58
			198	-1788.46	-0.07	38.21	69.53	0.48	-0.58
672	Copertura	201, 202	0	-311.76	0.04	-49.25	1023.11	-0.16	0.00
			775	-311.76	0.04	3915.71	0.11	-0.16	0.00
			1550	-311.76	0.04	-47.58	-1022.89	-0.16	0.00
673	Copertura	203, 202	0	-1785.32	0.13	-99.69	69.44	2.41	1.83
			99	-1785.32	0.13	-30.77	69.44	0.59	1.83
			198	-1785.32	0.13	38.15	69.44	-1.23	1.83
674	Copertura	204, 205	0	-2090.98	-0.22	-106.61	71.40	-5.04	-3.55
			99	-2090.98	-0.22	-35.75	71.40	-1.52	-3.55
			198	-2090.98	-0.22	35.11	71.40	2.00	-3.55
675	Copertura	205, 206	0	-391.01	0.03	-418.81	1114.78	-0.34	-0.03
			775	-391.01	0.03	3896.23	-1.22	-0.14	-0.03
			1550	-391.01	0.03	-437.74	-1117.22	0.05	-0.03
676	Copertura	207, 206	0	-2113.45	0.26	-107.17	71.69	6.17	4.44
			99	-2113.45	0.26	-36.02	71.69	1.77	4.44
			198	-2113.45	0.26	35.13	71.69	-2.64	4.44
677	Copertura	79	0	-314.31	7.38	8.89	-13.68	-13.57	-14.95
			125	-314.31	7.38	-8.20	-13.68	5.12	-14.95
			250	-314.31	7.38	-25.30	-13.68	23.81	-14.95
678	Copertura	124	0	-873.30	6.85	2.22	-2.00	1438.29	430.51
			155	-873.30	6.85	-0.88	-2.00	770.99	430.51
			310	-873.30	6.85	-3.99	-2.00	103.70	430.51
679	Copertura	80	0	-886.99	-6.64	-0.57	-1.95	-482.37	-413.69
			45	-886.99	-6.64	-1.45	-1.95	-296.21	-413.69
			90	-886.99	-6.64	-2.33	-1.95	-110.05	-413.69
680	Copertura	128	0	-1070.43	1.06	1.73	-1.64	1326.33	293.55
			155	-1070.43	1.06	-0.81	-1.64	871.33	293.55
			310	-1070.43	1.06	-3.36	-1.64	416.32	293.55
681	Copertura	82	0	-1071.09	3.58	0.69	-4.83	-667.33	-298.39
			43	-1071.09	3.58	-1.37	-4.83	-540.05	-298.39
			85	-1071.09	3.58	-3.43	-4.83	-412.77	-298.39
682	Copertura	132	0	-1173.62	-0.27	0.97	-0.93	1331.82	293.54
			155	-1173.62	-0.27	-0.47	-0.93	876.83	293.54
			310	-1173.62	-0.27	-1.91	-0.93	421.85	293.54
683	Copertura	83	0	-1187.65	0.13	-0.01	-2.67	-673.08	-292.24
			43	-1187.65	0.13	-1.14	-2.67	-548.42	-292.24

			85	-1187.65	0.13	-2.28	-2.67	-423.76	-292.24
684	Copertura	137	0	-1214.89	-0.19	0.34	-0.30	1338.30	303.45
			155	-1214.89	-0.19	-0.12	-0.30	867.95	303.45
			310	-1214.89	-0.19	-0.58	-0.30	397.60	303.45
685	Copertura	84	0	-1215.40	-0.10	0.14	0.49	-657.30	-303.46
			43	-1215.40	-0.10	0.35	0.49	-527.86	-303.46
			85	-1215.40	-0.10	0.55	0.49	-398.41	-303.46
686	Copertura	140	0	-1279.82	-0.03	0.04	0.14	1340.24	306.65
			155	-1279.82	-0.03	0.26	0.14	864.92	306.65
			310	-1279.82	-0.03	0.48	0.14	389.60	306.65
687	Copertura	85	0	-1269.25	0.04	2.40	-4.64	-651.66	-306.41
			43	-1269.25	0.04	0.42	-4.64	-520.95	-306.41
			85	-1269.25	0.04	-1.56	-4.64	-390.25	-306.41
688	Copertura	144	0	-1338.07	-0.03	0.13	-0.32	1341.46	306.84
			155	-1338.07	-0.03	-0.37	-0.32	865.85	306.84
			310	-1338.07	-0.03	-0.87	-0.32	390.25	306.84
689	Copertura	86	0	-1303.08	0.01	-1.90	1.61	-652.80	-305.95
			43	-1303.08	0.01	-1.21	1.61	-522.30	-305.95
			85	-1303.08	0.01	-0.52	1.61	-391.79	-305.95
690	Copertura	87	0	-1277.77	-0.10	3.88	-13.24	-652.72	-305.83
			43	-1277.77	-0.10	-1.76	-13.24	-522.26	-305.83
			85	-1277.77	-0.10	-7.41	-13.24	-391.80	-305.83
691	Copertura	148	0	-1299.69	0.09	-11.11	5.94	1340.63	306.44
			155	-1299.69	0.09	-1.90	5.94	865.66	306.44
			310	-1299.69	0.09	7.31	5.94	390.68	306.44
692	Copertura	88	0	-1207.36	0.06	-3.89	-0.01	-653.57	-305.01
			43	-1207.36	0.06	-3.90	-0.01	-523.46	-305.01
			85	-1207.36	0.06	-3.91	-0.01	-393.36	-305.01
693	Copertura	152	0	-1207.01	0.06	-15.12	7.94	1338.69	305.13
			155	-1207.01	0.06	-2.82	7.94	865.73	305.13
			310	-1207.01	0.06	9.48	7.94	392.77	305.13
694	Copertura	89	0	-1210.46	-0.08	1.81	-14.13	-654.01	-304.81
			43	-1210.46	-0.08	-4.21	-14.13	-523.99	-304.81
			85	-1210.46	-0.08	-10.24	-14.13	-393.97	-304.81
695	Copertura	156	0	-1194.07	0.04	-16.65	8.91	1338.51	304.74
			155	-1194.07	0.04	-2.84	8.91	866.17	304.74
			310	-1194.07	0.04	10.97	8.91	393.83	304.74
696	Copertura	90	0	-1195.46	0.04	-1.37	-8.52	-654.09	-304.62
			43	-1195.46	0.04	-5.01	-8.52	-524.15	-304.62
			85	-1195.46	0.04	-8.64	-8.52	-394.21	-304.62
697	Copertura	160	0	-1211.54	0.04	-18.53	10.00	1339.02	304.80
			155	-1211.54	0.04	-3.03	10.00	866.58	304.80
			310	-1211.54	0.04	12.46	10.00	394.14	304.80
698	Copertura	91	0	-1214.04	-0.06	1.24	-14.90	-654.09	-304.60
			43	-1214.04	-0.06	-5.11	-14.90	-524.16	-304.60
			85	-1214.04	-0.06	-11.47	-14.90	-394.23	-304.60
699	Copertura	164	0	-1226.13	0.05	-20.42	11.06	1339.56	304.89
			155	-1226.13	0.05	-3.28	11.06	866.98	304.89
			310	-1226.13	0.05	13.86	11.06	394.40	304.89
700	Copertura	92	0	-1212.04	0.04	-0.73	-11.09	-654.16	-304.57
			43	-1212.04	0.04	-5.46	-11.09	-524.24	-304.57
			85	-1212.04	0.04	-10.19	-11.09	-394.32	-304.57
701	Copertura	168	0	-1219.91	0.07	-22.29	12.08	1339.61	304.68
			155	-1219.91	0.07	-3.57	12.08	867.36	304.68
			310	-1219.91	0.07	15.15	12.08	395.10	304.68
702	Copertura	93	0	-1232.57	-0.06	-3.83	-4.09	-654.29	-304.75
			43	-1232.57	-0.06	-5.58	-4.09	-524.29	-304.75
			85	-1232.57	-0.06	-7.33	-4.09	-394.30	-304.75
703	Copertura	172	0	-1180.20	0.08	-23.84	12.95	1338.80	303.98
			155	-1180.20	0.08	-3.76	12.95	867.63	303.98
			310	-1180.20	0.08	16.31	12.95	396.45	303.98
704	Copertura	94	0	-1207.10	0.06	4.02	-15.01	-653.61	-305.26
			43	-1207.10	0.06	-2.38	-15.01	-523.39	-305.26
			85	-1207.10	0.06	-8.78	-15.01	-393.18	-305.26
705	Copertura	176	0	-1244.11	0.04	-25.83	14.62	1338.66	304.54
			155	-1244.11	0.04	-3.16	14.62	866.63	304.54
			310	-1244.11	0.04	19.50	14.62	394.59	304.54
706	Copertura	180	0	-1281.54	-0.05	-0.09	0.03	1338.42	303.71
			155	-1281.54	-0.05	-0.04	0.03	867.67	303.71
			310	-1281.54	-0.05	0.02	0.03	396.93	303.71
707	Copertura	95	0	-1325.79	0.09	-5.07	6.27	-654.28	-304.92
			43	-1325.79	0.09	-2.39	6.27	-524.21	-304.92

			85	-1325.79	0.09	0.28	6.27	-394.14	-304.92
708	Copertura	184	0	-1244.65	-0.01	-0.14	0.13	1338.38	304.45
			155	-1244.65	-0.01	0.06	0.13	866.47	304.45
			310	-1244.65	-0.01	0.26	0.13	394.57	304.45
709	Copertura	96	0	-1296.32	-0.09	5.83	-16.50	-652.25	-305.34
			43	-1296.32	-0.09	-1.20	-16.50	-522.00	-305.34
			85	-1296.32	-0.09	-8.24	-16.50	-391.76	-305.34
710	Copertura	188	0	-1252.59	-0.01	-0.34	0.35	1339.58	305.30
			155	-1252.59	-0.01	0.21	0.35	866.36	305.30
			310	-1252.59	-0.01	0.76	0.35	393.14	305.30
711	Copertura	97	0	-1251.13	0.17	-0.79	1.52	-652.50	-304.86
			43	-1251.13	0.17	-0.14	1.52	-522.46	-304.86
			85	-1251.13	0.17	0.51	1.52	-392.41	-304.86
712	Copertura	192	0	-1228.10	0.18	-0.72	0.75	1338.81	303.15
			155	-1228.10	0.18	0.44	0.75	868.93	303.15
			310	-1228.10	0.18	1.60	0.75	399.04	303.15
713	Copertura	106	0	-1225.83	-0.28	0.78	-0.38	-657.54	-302.23
			43	-1225.83	-0.28	0.62	-0.38	-528.62	-302.23
			85	-1225.83	-0.28	0.46	-0.38	-399.70	-302.23
714	Copertura	196	0	-1214.63	0.28	-1.34	1.33	1332.52	293.57
			155	-1214.63	0.28	0.71	1.33	877.48	293.57
			310	-1214.63	0.28	2.77	1.33	422.44	293.57
715	Copertura	107	0	-1136.73	-0.92	0.24	1.57	-673.44	-293.14
			43	-1136.73	-0.92	0.90	1.57	-548.40	-293.14
			85	-1136.73	-0.92	1.57	1.57	-423.36	-293.14
716	Copertura	200	0	-1088.15	-1.05	-2.03	1.93	1326.84	293.45
			155	-1088.15	-1.05	0.96	1.93	871.98	293.45
			310	-1088.15	-1.05	3.96	1.93	417.13	293.45
717	Copertura	108	0	-1062.44	2.52	0.39	6.95	-664.79	-292.43
			43	-1062.44	2.52	3.35	6.95	-540.05	-292.43
			85	-1062.44	2.52	6.32	6.95	-415.31	-292.43
718	Copertura	204	0	-891.43	-6.87	-2.48	2.27	1441.06	431.39
			155	-891.43	-6.87	1.03	2.27	772.41	431.39
			310	-891.43	-6.87	4.55	2.27	103.76	431.39
719	Copertura	109	0	-923.28	-10.97	3.34	-4.87	-450.68	-403.40
			43	-923.28	-10.97	1.26	-4.87	-278.60	-403.40
			85	-923.28	-10.97	-0.82	-4.87	-106.53	-403.40
720	Copertura	110	0	-324.17	-18.98	9.04	25.03	-4.25	-29.46
			43	-324.17	-18.98	19.72	25.03	8.31	-29.46
			85	-324.17	-18.98	30.39	25.03	20.88	-29.46
721	Copertura	14	0	-301.60	-35.65	20.05	-11.34	54.98	35.40
			95	-301.60	-35.65	9.27	-11.34	21.35	35.40
			190	-301.60	-35.65	-1.50	-11.34	-12.28	35.40
722	Copertura	15	0	546.98	2.94	3.46	1.44	-97.43	-1099.49
			65	546.98	2.94	4.40	1.44	617.23	-1099.49
			130	546.98	2.94	5.33	1.44	1331.90	-1099.49
723	Copertura	16	0	552.46	-11.74	0.49	8.08	88.11	1091.27
			65	552.46	-11.74	5.74	8.08	-621.22	1091.27
			130	552.46	-11.74	11.00	8.08	-1330.55	1091.27
724	Copertura	17	0	152.76	0.49	3.51	-1.05	-88.68	-1011.73
			65	152.76	0.49	2.83	-1.05	568.95	-1011.73
			130	152.76	0.49	2.14	-1.05	1226.57	-1011.73
725	Copertura	18	0	151.11	-0.51	3.94	-2.25	88.72	1011.05
			65	151.11	-0.51	2.47	-2.25	-568.46	1011.05
			130	151.11	-0.51	1.01	-2.25	-1225.64	1011.05
726	Copertura	19	0	53.96	-0.07	2.13	-1.03	-89.07	-1015.72
			65	53.96	-0.07	1.46	-1.03	571.15	-1015.72
			130	53.96	-0.07	0.79	-1.03	1231.37	-1015.72
727	Copertura	20	0	34.80	0.02	1.62	-1.26	89.88	1015.26
			65	34.80	0.02	0.80	-1.26	-570.04	1015.26
			130	34.80	0.02	-0.02	-1.26	-1229.96	1015.26
728	Copertura	21	0	25.22	-0.06	0.72	-0.38	-88.35	-1019.71
			65	25.22	-0.06	0.47	-0.38	574.46	-1019.71
			130	25.22	-0.06	0.23	-0.38	1237.27	-1019.71
729	Copertura	22	0	21.12	0.10	-0.49	0.61	88.49	1019.38
			65	21.12	0.10	-0.09	0.61	-574.11	1019.38
			130	21.12	0.10	0.30	0.61	-1236.71	1019.38
730	Copertura	23	0	-34.53	-0.01	-0.14	0.13	-89.90	-1022.25
			65	-34.53	-0.01	-0.06	0.13	574.56	-1022.25
			130	-34.53	-0.01	0.02	0.13	1239.02	-1022.25
731	Copertura	24	0	-22.37	0.05	-1.08	0.61	89.56	1021.82
			65	-22.37	0.05	-0.68	0.61	-574.63	1021.82

			130	-22.37	0.05	-0.29	0.61	-1238.81	1021.82
732	Copertura	25	0	-90.48	-0.01	0.52	-0.32	-91.73	-1024.50
			65	-90.48	-0.01	0.31	-0.32	574.20	-1024.50
			130	-90.48	-0.01	0.11	-0.32	1240.13	-1024.50
733	Copertura	26	0	-59.25	-0.02	-7.21	7.00	90.82	1023.02
			65	-59.25	-0.02	-2.66	7.00	-574.14	1023.02
			130	-59.25	-0.02	1.90	7.00	-1239.11	1023.02
734	Copertura	27	0	-26.47	-0.06	-11.36	14.13	88.63	1021.01
			65	-26.47	-0.06	-2.17	14.13	-575.03	1021.01
			130	-26.47	-0.06	7.01	14.13	-1238.68	1021.01
735	Copertura	28	0	-54.87	-0.03	18.15	-20.88	-88.62	-1021.54
			65	-54.87	-0.03	4.57	-20.88	575.37	-1021.54
			130	-54.87	-0.03	-9.00	-20.88	1239.37	-1021.54
736	Copertura	29	0	27.78	-0.08	-23.28	27.68	84.81	1017.45
			65	27.78	-0.08	-5.29	27.68	-576.53	1017.45
			130	27.78	-0.08	12.71	27.68	-1237.88	1017.45
737	Copertura	30	0	32.55	-0.07	24.95	-28.63	-84.28	-1016.85
			65	32.55	-0.07	6.34	-28.63	576.67	-1016.85
			130	32.55	-0.07	-12.27	-28.63	1237.62	-1016.85
738	Copertura	31	0	38.12	-0.08	-23.30	27.69	84.18	1016.89
			65	38.12	-0.08	-5.30	27.69	-576.80	1016.89
			130	38.12	-0.08	12.70	27.69	-1237.78	1016.89
739	Copertura	32	0	44.42	-0.10	26.97	-31.15	-83.26	-1015.94
			65	44.42	-0.10	6.72	-31.15	577.10	-1015.94
			130	44.42	-0.10	-13.53	-31.15	1237.46	-1015.94
740	Copertura	33	0	34.21	-0.09	-28.26	33.26	82.87	1015.59
			65	34.21	-0.09	-6.64	33.26	-577.26	1015.59
			130	34.21	-0.09	14.98	33.26	-1237.40	1015.59
741	Copertura	34	0	27.26	-0.11	29.51	-34.29	-82.88	-1015.99
			65	27.26	-0.11	7.22	-34.29	577.52	-1015.99
			130	27.26	-0.11	-15.07	-34.29	1237.91	-1015.99
742	Copertura	35	0	34.23	-0.09	-28.92	34.21	82.32	1015.23
			65	34.23	-0.09	-6.68	34.21	-577.58	1015.23
			130	34.23	-0.09	15.56	34.21	-1237.48	1015.23
743	Copertura	36	0	12.93	-0.13	32.07	-37.45	-82.33	-1015.94
			65	12.93	-0.13	7.72	-37.45	578.03	-1015.94
			130	12.93	-0.13	-16.62	-37.45	1238.39	-1015.94
744	Copertura	37	0	15.59	-0.10	-32.51	38.42	81.50	1014.58
			65	15.59	-0.10	-7.54	38.42	-577.97	1014.58
			130	15.59	-0.10	17.44	38.42	-1237.45	1014.58
745	Copertura	38	0	18.33	-0.13	34.64	-40.60	-81.12	-1015.04
			65	18.33	-0.13	8.24	-40.60	578.66	-1015.04
			130	18.33	-0.13	-18.15	-40.60	1238.43	-1015.04
746	Copertura	39	0	12.83	-0.10	-33.52	40.10	81.07	1014.51
			65	12.83	-0.10	-7.46	40.10	-578.37	1014.51
			130	12.83	-0.10	18.60	40.10	-1237.80	1014.51
747	Copertura	40	0	55.66	-0.14	36.64	-43.12	-79.15	-1012.97
			65	55.66	-0.14	8.61	-43.12	579.28	-1012.97
			130	55.66	-0.14	-19.42	-43.12	1237.70	-1012.97
748	Copertura	41	0	23.46	-0.05	-23.69	30.32	82.81	1016.33
			65	23.46	-0.05	-3.98	30.32	-577.80	1016.33
			130	23.46	-0.05	15.72	30.32	-1238.41	1016.33
749	Copertura	42	0	-6.94	-0.17	38.41	-45.76	-80.14	-1013.58
			65	-6.94	-0.17	8.67	-45.76	578.69	-1013.58
			130	-6.94	-0.17	-21.08	-45.76	1237.52	-1013.58
750	Copertura	43	0	-39.85	-0.02	-0.14	0.03	-90.11	-1021.10
			65	-39.85	-0.02	-0.12	0.03	573.61	-1021.10
			130	-39.85	-0.02	-0.11	0.03	1237.33	-1021.10
751	Copertura	44	0	-77.37	0.00	-13.84	14.07	91.31	1022.62
			65	-77.37	0.00	-4.69	14.07	-573.39	1022.62
			130	-77.37	0.00	4.45	14.07	-1238.09	1022.62
752	Copertura	45	0	-3.05	0.00	-0.30	0.12	-89.17	-1020.38
			65	-3.05	0.00	-0.22	0.12	574.08	-1020.38
			130	-3.05	0.00	-0.13	0.12	1237.33	-1020.38
753	Copertura	46	0	-59.01	0.01	-0.84	0.40	90.57	1021.40
			65	-59.01	0.01	-0.59	0.40	-573.34	1021.40
			130	-59.01	0.01	-0.33	0.40	-1237.25	1021.40
754	Copertura	47	0	-9.33	-0.01	-0.78	0.35	-89.31	-1021.34
			65	-9.33	-0.01	-0.55	0.35	574.56	-1021.34
			130	-9.33	-0.01	-0.33	0.35	1238.44	-1021.34
755	Copertura	48	0	-9.37	0.00	-1.88	1.72	89.07	1019.68
			65	-9.37	0.00	-0.77	1.72	-573.72	1019.68

			130	-9.37	0.00	0.35	1.72	-1236.52	1019.68
756	Copertura	49	0	12.44	0.06	-1.66	0.82	-88.82	-1020.43
			65	12.44	0.06	-1.13	0.82	574.46	-1020.43
			130	12.44	0.06	-0.60	0.82	1237.74	-1020.43
757	Copertura	50	0	7.95	-0.14	-2.54	2.22	88.84	1018.54
			65	7.95	-0.14	-1.09	2.22	-573.21	1018.54
			130	7.95	-0.14	0.35	2.22	-1235.26	1018.54
758	Copertura	51	0	14.32	0.08	-2.99	1.43	-90.27	-1017.12
			65	14.32	0.08	-2.06	1.43	570.85	-1017.12
			130	14.32	0.08	-1.14	1.43	1231.98	-1017.12
759	Copertura	52	0	84.96	-0.11	-4.48	3.17	87.92	1012.29
			65	84.96	-0.11	-2.41	3.17	-570.07	1012.29
			130	84.96	-0.11	-0.35	3.17	-1228.06	1012.29
760	Copertura	53	0	135.71	-0.50	-4.18	1.36	-89.25	-1012.53
			65	135.71	-0.50	-3.30	1.36	568.89	-1012.53
			130	135.71	-0.50	-2.42	1.36	1227.03	-1012.53
761	Copertura	54	0	151.97	1.37	-7.16	4.63	88.94	1011.39
			65	151.97	1.37	-4.15	4.63	-568.46	1011.39
			130	151.97	1.37	-1.14	4.63	-1225.86	1011.39
762	Copertura	55	0	531.97	-2.92	-3.96	-1.28	-98.12	-1101.98
			65	531.97	-2.92	-4.79	-1.28	618.17	-1101.98
			130	531.97	-2.92	-5.62	-1.28	1334.46	-1101.98
763	Copertura	56	0	520.07	3.50	-8.29	2.98	96.11	1104.47
			65	520.07	3.50	-6.36	2.98	-621.80	1104.47
			130	520.07	3.50	-4.42	2.98	-1339.70	1104.47
764	Copertura	70	0	-316.16	18.63	-24.36	11.30	32.81	10.77
			95	-316.16	18.63	-13.63	11.30	22.58	10.77
			190	-316.16	18.63	-2.90	11.30	12.35	10.77
765	Copertura	81	0	-882.18	8.48	3.18	-4.32	-1154.02	-419.64
			80	-882.18	8.48	-0.28	-4.32	-818.31	-419.64
			160	-882.18	8.48	-3.73	-4.32	-482.59	-419.64
766	Copertura	126	0	-894.89	-28.55	-2.65	-6.65	-1437.30	-470.00
			30	-894.89	-28.55	-4.64	-6.65	-1296.30	-470.00
			60	-894.89	-28.55	-6.64	-6.65	-1155.31	-470.00
767	Copertura	98	0	-1075.90	-3.68	1.67	-2.47	-1148.98	-292.44
			82	-1075.90	-3.68	-0.36	-2.47	-908.18	-292.44
			165	-1075.90	-3.68	-2.40	-2.47	-667.38	-292.44
768	Copertura	99	0	-1186.31	0.53	1.81	-1.73	-1155.45	-292.89
			82	-1186.31	0.53	0.38	-1.73	-914.28	-292.89
			165	-1186.31	0.53	-1.04	-1.73	-673.11	-292.89
769	Copertura	100	0	-1216.74	0.36	0.14	-0.45	-1155.98	-302.82
			82	-1216.74	0.36	-0.23	-0.45	-906.63	-302.82
			165	-1216.74	0.36	-0.61	-0.45	-657.28	-302.82
770	Copertura	101	0	-1268.38	-0.04	-0.96	1.89	-1156.20	-306.36
			82	-1268.38	-0.04	0.60	1.89	-903.93	-306.36
			165	-1268.38	-0.04	2.16	1.89	-651.66	-306.36
771	Copertura	102	0	-1303.94	0.01	5.31	-4.92	-1156.74	-306.00
			82	-1303.94	0.01	1.26	-4.92	-904.77	-306.00
			165	-1303.94	0.01	-2.80	-4.92	-652.80	-306.00
772	Copertura	103	0	-1270.94	-0.04	1.22	-0.79	-1156.37	-305.82
			82	-1270.94	-0.04	0.57	-0.79	-904.54	-305.82
			165	-1270.94	-0.04	-0.08	-0.79	-652.71	-305.82
773	Copertura	104	0	-1214.18	-0.03	11.60	-12.47	-1155.89	-305.01
			82	-1214.18	-0.03	1.33	-12.47	-904.73	-305.01
			165	-1214.18	-0.03	-8.93	-12.47	-653.57	-305.01
774	Copertura	105	0	-1199.39	-0.01	9.43	-8.94	-1156.04	-304.84
			82	-1199.39	-0.01	2.07	-8.94	-905.02	-304.84
			165	-1199.39	-0.01	-5.29	-8.94	-654.01	-304.84
775	Copertura	111	0	-1206.53	0.00	12.98	-13.71	-1140.01	-304.60
			80	-1206.53	0.00	2.05	-13.71	-897.05	-304.60
			160	-1206.53	0.00	-8.88	-13.71	-654.10	-304.60
776	Copertura	112	0	-1201.37	-0.01	12.11	-11.60	-1155.76	-304.62
			82	-1201.37	-0.01	2.55	-11.60	-904.92	-304.62
			165	-1201.37	-0.01	-7.00	-11.60	-654.08	-304.62
777	Copertura	113	0	-1224.72	0.02	14.48	-14.39	-1155.71	-304.55
			82	-1224.72	0.02	2.63	-14.39	-904.94	-304.55
			165	-1224.72	0.02	-9.22	-14.39	-654.16	-304.55
778	Copertura	114	0	-1222.52	0.00	15.23	-15.98	-1156.20	-304.77
			82	-1222.52	0.00	2.07	-15.98	-905.24	-304.77
			165	-1222.52	0.00	-11.10	-15.98	-654.29	-304.77
779	Copertura	115	0	-1217.15	0.01	3.15	-3.12	-1156.31	-305.24
			82	-1217.15	0.01	0.59	-3.12	-904.96	-305.24

			165	-1217.15	0.01	-1.98	-3.12	-653.61	-305.24
780	Copertura	116	0	-1321.07	-0.01	12.60	-12.93	-1156.45	-304.92
			82	-1321.07	-0.01	1.95	-12.93	-905.36	-304.92
			165	-1321.07	-0.01	-8.71	-12.93	-654.28	-304.92
781	Copertura	117	0	-1301.04	0.00	-1.21	2.70	-1155.12	-305.34
			82	-1301.04	0.00	1.02	2.70	-903.69	-305.34
			165	-1301.04	0.00	3.24	2.70	-652.26	-305.34
782	Copertura	118	0	-1252.04	-0.07	0.67	-0.53	-1154.61	-304.89
			82	-1252.04	-0.07	0.23	-0.53	-903.55	-304.89
			165	-1252.04	-0.07	-0.21	-0.53	-652.50	-304.89
783	Copertura	131	0	-1071.76	-1.19	0.50	-2.93	-1325.32	-293.96
			30	-1071.76	-1.19	-0.37	-2.93	-1237.14	-293.96
			60	-1071.76	-1.19	-1.25	-2.93	-1148.95	-293.96
784	Copertura	133	0	-1190.45	0.04	0.02	-1.27	-1330.31	-291.37
			30	-1190.45	0.04	-0.36	-1.27	-1242.90	-291.37
			60	-1190.45	0.04	-0.74	-1.27	-1155.49	-291.37
785	Copertura	139	0	-1218.14	0.24	0.42	0.75	-1337.70	-302.83
			30	-1218.14	0.24	0.65	0.75	-1246.85	-302.83
			60	-1218.14	0.24	0.88	0.75	-1156.00	-302.83
786	Copertura	143	0	-1266.99	0.10	-0.26	0.69	-1340.00	-306.35
			30	-1266.99	0.10	-0.06	0.69	-1248.09	-306.35
			60	-1266.99	0.10	0.15	0.69	-1156.19	-306.35
787	Copertura	147	0	-1304.69	0.00	1.87	7.19	-1340.34	-306.00
			30	-1304.69	0.00	4.03	7.19	-1248.54	-306.00
			60	-1304.69	0.00	6.19	7.19	-1156.74	-306.00
788	Copertura	151	0	-1270.19	-0.02	9.08	-12.90	-1339.86	-305.82
			30	-1270.19	-0.02	5.21	-12.90	-1248.12	-305.82
			60	-1270.19	-0.02	1.34	-12.90	-1156.37	-305.82
789	Copertura	155	0	-1212.36	0.08	15.60	-8.92	-1338.98	-305.15
			30	-1212.36	0.08	12.93	-8.92	-1247.43	-305.15
			60	-1212.36	0.08	10.25	-8.92	-1155.89	-305.15
790	Copertura	159	0	-1201.21	0.07	15.85	-12.48	-1338.86	-304.70
			30	-1201.21	0.07	12.10	-12.48	-1247.45	-304.70
			60	-1201.21	0.07	8.36	-12.48	-1156.04	-304.70
791	Copertura	119	0	-1224.92	0.00	-1.36	1.68	-1155.24	-302.21
			82	-1224.92	0.00	0.03	1.68	-906.39	-302.21
			165	-1224.92	0.00	1.41	1.68	-657.55	-302.21
792	Copertura	120	0	-1142.44	0.13	-1.94	3.50	-1153.07	-291.23
			82	-1142.44	0.13	0.95	3.50	-913.26	-291.23
			165	-1142.44	0.13	3.83	3.50	-673.45	-291.23
793	Copertura	121	0	-1056.73	-1.05	-3.94	5.02	-1149.52	-294.34
			82	-1056.73	-1.05	0.20	5.02	-907.15	-294.34
			165	-1056.73	-1.05	4.33	5.02	-664.78	-294.34
794	Copertura	122	0	-931.30	15.37	-5.17	8.86	-1180.13	-443.62
			82	-931.30	15.37	2.12	8.86	-814.84	-443.62
			165	-931.30	15.37	9.42	8.86	-449.54	-443.62
795	Copertura	123	0	-316.16	18.63	-2.90	11.30	12.35	10.77
			82	-316.16	18.63	6.41	11.30	3.48	10.77
			165	-316.16	18.63	15.71	11.30	-5.39	10.77
796	Copertura	163	0	-1204.18	0.12	18.49	-11.00	-1338.47	-304.77
			33	-1204.18	0.12	14.91	-11.00	-1239.17	-304.77
			65	-1204.18	0.12	11.32	-11.00	-1139.87	-304.77
797	Copertura	167	0	-1203.72	0.09	19.38	-14.31	-1338.56	-304.45
			30	-1203.72	0.09	15.09	-14.31	-1247.22	-304.45
			60	-1203.72	0.09	10.80	-14.31	-1155.88	-304.45
798	Copertura	171	0	-1222.26	0.13	21.60	-14.27	-1338.56	-304.74
			30	-1222.26	0.13	17.32	-14.27	-1247.13	-304.74
			60	-1222.26	0.13	13.04	-14.27	-1155.71	-304.74
799	Copertura	174	0	-1224.99	0.15	23.07	-16.11	-1338.95	-304.57
			30	-1224.99	0.15	18.24	-16.11	-1247.57	-304.57
			60	-1224.99	0.15	13.40	-16.11	-1156.20	-304.57
800	Copertura	179	0	-1216.89	0.16	20.53	-30.55	-1339.59	-305.46
			30	-1216.89	0.16	11.36	-30.55	-1247.95	-305.46
			60	-1216.89	0.16	2.20	-30.55	-1156.31	-305.46
801	Copertura	183	0	-1321.34	0.14	4.50	14.50	-1339.26	-304.70
			30	-1321.34	0.14	8.85	14.50	-1247.85	-304.70
			60	-1321.34	0.14	13.20	14.50	-1156.44	-304.70
802	Copertura	187	0	-1302.41	-0.01	-0.36	0.41	-1338.35	-305.38
			30	-1302.41	-0.01	-0.23	0.41	-1246.73	-305.38
			60	-1302.41	-0.01	-0.11	0.41	-1155.12	-305.38
803	Copertura	191	0	-1250.67	-0.01	0.33	1.76	-1337.52	-304.85
			30	-1250.67	-0.01	0.86	1.76	-1246.06	-304.85

			60	-1250.67	-0.01	1.38	1.76	-1154.61	-304.85
804	Copertura	194	0	-1229.44	-0.36	0.15	2.10	-1336.14	-301.58
			30	-1229.44	-0.36	0.78	2.10	-1245.67	-301.58
			60	-1229.44	-0.36	1.41	2.10	-1155.20	-301.58
805	Copertura	198	0	-1137.92	-0.35	-0.59	3.08	-1328.24	-291.86
			30	-1137.92	-0.35	0.33	3.08	-1240.68	-291.86
			60	-1137.92	-0.35	1.26	3.08	-1153.12	-291.86
806	Copertura	203	0	-1069.76	3.27	0.35	6.46	-1325.55	-292.28
			30	-1069.76	3.27	2.29	6.46	-1237.87	-292.28
			60	-1069.76	3.27	4.22	6.46	-1150.18	-292.28
807	Copertura	207	0	-918.27	8.34	-0.58	7.42	-1446.87	-445.68
			30	-918.27	8.34	1.64	7.42	-1313.17	-445.68
			60	-918.27	8.34	3.87	7.42	-1179.46	-445.68

1.1.2.2 Piastre SLU

Tabella 4.I

Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	3.061	1.031	-0.564	-858.722	-258.020	-118.174	7.462	5.066
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	3.274	1.979	-0.970	-827.263	-268.968	282.368	11.135	-6.586
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	3.257	1.963	0.877	-772.690	-250.467	-280.185	8.012	6.601

1.1.3 Risultati Condizioni (Carichi d'Esercizio).

1.1.3.1 Sollecitazioni SLU

Tabella 5.I

Sollecitazioni									
Asta	Imp.	Fili	X [cm]	N [daN]	Mt [daNm]	Mxz [daNm]	Txz [daN]	Mxy [daNm]	Txy [daN]
1	Fondazione	1, 2	0	-9.50	17.62	19.48	-188.57	1.05	-1.45
			42	-9.57	17.63	-34.54	-72.34	1.59	-1.17
			83	-9.65	17.63	-41.25	39.28	2.04	-0.99
2	Fondazione	1, 2	0	-11.64	15.69	-31.36	-79.95	2.03	-0.90
			42	-11.72	15.70	-41.96	28.42	2.38	-0.80
			83	-11.82	15.70	-7.95	134.99	2.70	-0.77
3	Fondazione	1, 15	0	26.71	3.04	12.72	-140.93	4.67	8.48
			40	26.40	3.04	-20.10	-23.05	1.31	8.38
			80	26.10	3.04	-4.34	103.60	-1.99	8.20
4	Fondazione	1, 15	0	26.35	73.83	-16.96	-30.06	-2.00	-7.86
			40	26.07	73.84	-2.16	105.88	1.18	-8.12

			80	25.80	73.84	68.59	251.41	4.47	-8.46
5	Fondazio ne	2, 3	0	-15.69	7.09	0.96	-114.04	2.30	2.89
			35	-15.77	7.09	-23.23	-26.44	1.30	2.88
			69	-15.86	7.10	-17.33	60.49	0.31	2.85
6	Fondazio ne	2, 3	0	-7.29	10.89	-8.28	-62.12	0.31	-0.75
			35	-7.38	10.89	-14.74	24.56	0.57	-0.80
			69	-7.48	10.90	8.71	111.29	0.86	-0.87
7	Fondazio ne	3, 4	0	-0.84	7.85	14.37	-110.30	0.76	0.80
			35	-0.94	7.85	-8.67	-23.41	0.49	0.72
			69	-1.04	7.86	-1.72	63.66	0.26	0.62
8	Fondazio ne	3, 4	0	4.68	6.05	2.92	-66.95	0.26	0.02
			35	4.58	6.05	-5.10	20.43	0.27	-0.08
			69	4.49	6.06	17.10	108.20	0.32	-0.19
9	Fondazio ne	4, 5	0	9.12	5.51	21.16	-114.22	0.28	0.21
			35	9.03	5.52	-3.04	-26.13	0.23	0.09
			69	8.94	5.52	3.19	62.17	0.22	-0.04
10	Fondazio ne	4, 5	0	12.45	2.81	5.91	-71.34	0.22	0.26
			35	12.36	2.82	-3.42	17.20	0.15	0.13
			69	12.28	2.82	17.85	106.00	0.13	-0.01
11	Fondazio ne	5, 6	0	14.78	3.21	19.30	-111.03	0.13	0.03
			35	14.70	3.21	-3.64	-22.05	0.15	-0.11
			69	14.63	3.22	4.13	67.02	0.21	-0.26
12	Fondazio ne	5, 6	0	16.08	0.96	4.98	-66.64	0.21	0.33
			35	16.01	0.96	-2.62	22.54	0.12	0.19
			69	15.96	0.97	20.57	111.85	0.08	0.04
13	Fondazio ne	6, 7	0	23.61	2.50	21.12	-114.93	0.08	0.20
			35	23.56	2.50	-3.11	-25.60	0.03	0.05
			69	23.52	2.51	3.46	63.63	0.04	-0.10
14	Fondazio ne	6, 7	0	24.24	0.57	4.43	-70.07	0.04	0.11
			35	24.21	0.58	-4.36	19.08	0.03	-0.04
			69	24.19	0.58	17.61	108.22	0.07	-0.19
15	Fondazio ne	7, 8	0	18.45	1.07	20.21	-118.73	0.09	0.03
			35	18.44	1.07	-5.38	-29.70	0.10	-0.12
			69	18.43	1.08	-0.30	59.15	0.17	-0.28
16	Fondazio ne	7, 8	0	18.69	-1.08	1.54	-72.55	0.17	0.22
			35	18.69	-1.08	-8.17	16.21	0.12	0.07
			69	18.70	-1.07	12.73	104.99	0.13	-0.08
17	Fondazio ne	8, 9	0	18.23	-1.25	13.45	-105.41	0.12	0.10
			35	18.25	-1.24	-7.60	-16.59	0.11	-0.05
			69	18.27	-1.24	2.00	72.27	0.15	-0.20
18	Fondazio ne	8, 9	0	17.04	-3.11	0.78	-60.43	0.16	0.19
			35	17.07	-3.10	-4.72	28.57	0.11	0.05
			69	17.10	-3.10	20.51	117.79	0.12	-0.09
19	Fondazio ne	9, 10	0	21.38	-1.27	17.92	-104.92	0.09	0.15
			35	21.43	-1.27	-2.88	-15.57	0.07	0.01
			69	21.48	-1.26	7.16	73.80	0.08	-0.12
20	Fondazio ne	9, 10	0	19.52	-3.54	3.65	-60.18	0.09	0.14
			35	19.58	-3.53	-1.70	29.23	0.06	0.01
			69	19.65	-3.53	23.81	118.70	0.08	-0.12
21	Fondazio ne	10, 11	0	9.53	-2.63	22.27	-110.54	0.10	-0.18
			35	9.60	-2.62	-0.46	-21.18	0.18	-0.30
			69	9.68	-2.62	7.59	67.91	0.30	-0.41
22	Fondazio ne	10, 11	0	6.62	-5.09	4.27	-64.98	0.30	0.10
			35	6.70	-5.09	-2.84	23.81	0.29	-0.01
			69	6.79	-5.08	20.64	112.34	0.31	-0.11

23	Fondazio ne	11, 12	0	2.26	-5.67	17.01	-107.87	0.34	0.21
			35	2.35	-5.67	-5.01	-19.73	0.29	0.12
			69	2.44	-5.66	3.30	67.96	0.26	0.04
24	Fondazio ne	11, 12	0	-3.42	-7.09	-2.12	-63.53	0.26	-0.81
			35	-3.34	-7.08	-8.99	23.78	0.55	-0.88
			69	-3.25	-7.08	14.22	110.85	0.87	-0.93
25	Fondazio ne	12, 13	0	-10.40	-11.08	7.63	-112.46	0.97	0.96
			35	-10.32	-11.08	-16.19	-25.60	0.65	0.92
			69	-10.24	-11.07	-10.07	61.18	0.33	0.91
26	Fondazio ne	12, 13	0	-18.90	-8.63	-18.46	-61.60	0.34	-2.84
			35	-18.83	-8.62	-24.73	25.44	1.32	-2.83
			69	-18.76	-8.62	-0.86	113.18	2.29	-2.80
27	Fondazio ne	13, 14	0	-12.98	-16.62	-11.44	-133.14	2.69	0.36
			42	-12.90	-16.62	-44.63	-26.30	2.53	0.45
			83	-12.84	-16.61	-33.05	82.56	2.31	0.61
28	Fondazio ne	13, 14	0	-11.78	-18.52	-38.36	-44.53	2.32	1.26
			42	-11.73	-18.52	-33.68	67.84	1.75	1.51
			83	-11.67	-18.51	18.67	185.05	1.05	1.87
29	Fondazio ne	14, 16	0	30.50	-4.64	15.09	-150.45	-4.86	-8.22
			40	30.11	-4.64	-21.31	-31.65	-1.60	-8.14
			80	29.74	-4.64	-8.81	95.69	1.61	-7.98
30	Fondazio ne	14, 16	0	27.91	-69.04	-14.02	-42.62	1.62	7.19
			40	27.55	-69.04	-4.09	93.84	-1.28	7.44
			80	27.21	-69.04	61.96	239.73	-4.31	7.77
31	Fondazio ne	15, 17	0	34.10	-0.68	42.89	-151.47	6.78	20.55
			33	33.88	-0.68	13.84	-23.85	0.05	20.22
			66	33.68	-0.67	27.84	109.40	-6.56	19.85
32	Fondazio ne	15, 17	0	30.95	113.24	0.02	28.90	-6.57	-24.77
			33	30.76	113.24	32.32	167.53	1.67	-25.18
			66	30.58	113.25	111.21	311.19	10.06	-25.64
33	Fondazio ne	16, 18	0	35.10	-0.87	40.23	-144.90	-6.57	-19.76
			33	34.83	-0.88	13.40	-17.02	-0.10	-19.43
			66	34.57	-0.88	29.71	116.51	6.25	-19.07
34	Fondazio ne	16, 18	0	33.48	-108.98	4.35	12.33	6.26	23.64
			33	33.23	-108.98	31.24	151.22	-1.61	24.05
			66	32.99	-108.99	104.80	295.11	-9.62	24.51
35	Fondazio ne	17, 19	0	49.11	-41.07	85.16	-245.43	11.84	31.35
			33	48.95	-41.07	28.46	-97.82	1.58	30.86
			66	48.80	-41.06	20.98	52.79	-8.52	30.36
36	Fondazio ne	17, 19	0	42.12	88.54	4.05	-20.63	-8.53	-28.94
			33	41.99	88.54	22.47	132.60	1.11	-29.45
			66	41.88	88.55	91.87	288.20	10.91	-29.99
37	Fondazio ne	18, 20	0	49.12	36.29	84.03	-241.97	-11.46	-30.41
			33	48.89	36.29	28.52	-94.11	-1.51	-29.92
			66	48.69	36.28	22.32	56.79	8.28	-29.41
38	Fondazio ne	18, 20	0	44.44	-92.46	5.93	-36.39	8.29	28.64
			33	44.25	-92.47	19.22	117.17	-1.25	29.16
			66	44.08	-92.47	83.59	273.15	-10.96	29.72
39	Fondazio ne	19, 21	0	28.72	-52.50	74.50	-259.97	9.69	28.70
			33	28.62	-52.49	14.63	-102.85	0.31	28.15
			66	28.53	-52.48	6.75	55.09	-8.89	27.61
40	Fondazio ne	19, 21	0	23.31	79.94	-2.22	-31.37	-8.89	-26.95
			33	23.23	79.94	13.59	127.24	0.09	-27.49
			66	23.15	79.95	81.85	286.41	9.25	-28.06
41	Fondazio	20, 22	0	29.45	50.03	70.62	-255.11	-9.75	-28.84

	ne								
			33	29.29	50.02	12.44	-97.48	-0.33	-28.27
			66	29.14	50.02	6.45	61.17	8.91	-27.71
42	Fondazio ne	20, 22	0	24.20	-81.79	-4.90	-29.51	8.91	26.71
			33	24.06	-81.79	11.69	130.04	0.00	27.28
			66	23.93	-81.80	81.08	290.41	-9.10	27.87
43	Fondazio ne	21, 23	0	34.17	-59.75	75.55	-277.86	10.26	28.99
			33	34.10	-59.75	10.13	-118.82	0.79	28.42
			66	34.05	-59.74	-2.93	39.45	-8.49	27.86
44	Fondazio ne	21, 23	0	29.11	68.30	-6.33	-30.41	-8.49	-28.38
			33	29.07	68.31	9.64	127.05	0.96	-28.94
			66	29.04	68.32	77.45	283.67	10.61	-29.50
45	Fondazio ne	22, 24	0	35.41	55.52	72.43	-277.16	-10.11	-28.64
			33	35.29	55.51	7.48	-116.63	-0.76	-28.04
			66	35.18	55.50	-4.55	43.47	8.40	-27.46
46	Fondazio ne	22, 24	0	30.34	-71.63	-11.03	-40.38	8.40	27.74
			33	30.24	-71.64	2.02	119.30	-0.85	28.32
			66	30.16	-71.65	67.71	278.64	-10.30	28.92
47	Fondazio ne	23, 25	0	2.95	-80.92	82.18	-333.50	9.51	26.77
			33	2.92	-80.92	-2.21	-178.35	0.77	26.21
			66	2.90	-80.91	-35.74	-25.22	-7.80	25.68
48	Fondazio ne	23, 25	0	-5.88	25.05	-25.66	-81.31	-7.79	-16.97
			33	-5.90	25.06	-27.46	70.11	-2.11	-17.48
			66	-5.93	25.06	20.50	220.36	3.75	-18.00
49	Fondazio ne	24, 26	0	6.17	66.11	64.26	-308.27	-9.21	-26.19
			33	6.10	66.11	-11.26	-149.74	-0.67	-25.59
			66	6.02	66.10	-34.66	7.65	7.68	-25.02
50	Fondazio ne	24, 26	0	-1.32	-42.74	-35.71	-61.20	7.68	16.10
			33	-1.39	-42.74	-30.03	95.47	2.27	16.66
			66	-1.47	-42.75	27.32	252.02	-3.32	17.22
51	Fondazio ne	25, 26	0	47.84	10.26	-117.40	-86.27	-0.90	-1.13
			49	47.09	10.26	-128.71	35.44	-0.36	-1.09
			97	46.38	10.26	-85.54	138.81	0.16	-1.06
52	Fondazio ne	25, 26	0	46.85	4.52	-79.12	-56.99	0.16	0.31
			49	46.18	4.52	-84.11	34.35	0.00	0.33
			97	45.54	4.52	-46.54	118.63	-0.16	0.34
53	Fondazio ne	25, 26	0	50.07	0.98	-32.92	-60.33	-0.16	-0.19
			49	49.47	0.98	-42.37	20.71	-0.07	-0.19
			97	48.91	0.98	-12.65	100.99	0.03	-0.20
54	Fondazio ne	25, 26	0	52.85	0.02	-3.39	-68.50	0.02	-0.01
			49	52.33	0.01	-16.93	12.71	0.04	-0.04
			97	51.85	0.01	9.47	95.72	0.06	-0.08
55	Fondazio ne	25, 26	0	54.67	-0.08	14.73	-81.17	0.06	0.01
			49	54.23	-0.08	-4.05	4.01	0.06	-0.03
			97	53.83	-0.08	19.14	91.31	0.09	-0.09
56	Fondazio ne	25, 26	0	55.68	0.04	20.55	-89.10	0.09	0.05
			49	55.33	0.04	-1.12	0.08	0.08	-0.01
			97	55.02	0.04	21.00	90.81	0.11	-0.09
57	Fondazio ne	25, 26	0	56.16	0.06	20.84	-93.35	0.10	0.08
			49	55.90	0.05	-2.21	-1.43	0.09	-0.01
			97	55.68	0.05	19.69	91.37	0.11	-0.10
58	Fondazio ne	25, 26	0	56.37	0.14	18.87	-94.59	0.11	0.11
			49	56.20	0.14	-4.43	-1.19	0.08	0.01
			97	56.06	0.14	17.83	92.60	0.10	-0.08
59	Fondazio ne	25, 26	0	56.49	0.57	17.10	-94.13	0.10	0.06

			49	56.40	0.57	-5.83	-0.11	0.09	-0.04
			97	56.36	0.57	17.04	94.03	0.14	-0.14
60	Fondazio ne	25, 26	0	56.75	-1.82	16.49	-94.40	0.14	0.15
			49	56.75	-1.82	-6.53	-0.23	0.09	0.05
			97	56.80	-1.82	16.25	93.88	0.09	-0.05
61	Fondazio ne	25, 26	0	56.89	0.56	15.54	-92.47	0.09	0.08
			49	56.98	0.56	-6.61	1.54	0.08	-0.02
			97	57.11	0.56	16.96	95.39	0.11	-0.12
62	Fondazio ne	25, 26	0	57.10	0.12	17.83	-91.63	0.11	0.09
			49	57.27	0.12	-4.00	1.99	0.09	0.00
			97	57.50	0.12	19.63	95.20	0.11	-0.08
63	Fondazio ne	25, 26	0	57.20	0.07	20.19	-90.69	0.11	0.07
			49	57.47	0.07	-1.44	1.88	0.09	0.00
			97	57.78	0.07	21.75	93.48	0.11	-0.07
64	Fondazio ne	25, 26	0	57.04	-0.05	21.61	-90.30	0.11	0.07
			49	57.40	-0.05	-0.38	-0.02	0.09	0.02
			97	57.80	-0.05	21.16	88.53	0.10	-0.03
65	Fondazio ne	25, 26	0	56.34	-0.04	18.68	-91.55	0.10	0.06
			49	56.79	-0.04	-4.84	-5.09	0.08	0.03
			97	57.28	-0.04	13.17	79.09	0.07	0.01
66	Fondazio ne	25, 26	0	54.82	0.20	7.30	-96.36	0.07	0.04
			49	55.35	0.20	-19.69	-14.46	0.06	0.04
			97	55.93	0.20	-7.29	65.67	0.04	0.04
67	Fondazio ne	25, 26	0	52.33	0.93	-18.82	-105.92	0.04	0.18
			49	52.95	0.93	-51.17	-26.49	-0.05	0.20
			97	53.62	0.93	-44.64	54.35	-0.16	0.24
68	Fondazio ne	25, 26	0	48.38	1.58	-59.35	-111.94	-0.16	-0.54
			49	49.09	1.58	-93.49	-26.62	0.10	-0.49
			97	49.83	1.58	-84.13	67.61	0.32	-0.42
69	Fondazio ne	25, 26	0	49.49	2.01	-97.82	-145.31	0.32	0.87
			49	50.27	2.01	-143.01	-36.71	-0.12	0.96
			97	51.09	2.01	-130.45	93.29	-0.61	1.06
70	Fondazio ne	25, 28	0	11.03	-49.40	34.88	-293.25	5.91	17.06
			43	11.00	-49.39	-48.89	-101.27	-1.19	16.40
			85	10.97	-49.38	-51.34	89.69	-8.03	15.75
71	Fondazio ne	25, 28	0	12.73	68.73	-49.43	-50.30	-8.03	-20.65
			43	12.71	68.73	-30.09	141.64	0.89	-21.32
			85	12.70	68.74	71.34	336.18	10.10	-22.03
72	Fondazio ne	26, 27	0	14.65	37.61	24.69	-249.48	-5.03	-19.25
			33	14.58	37.61	-31.79	-92.89	1.23	-18.68
			66	14.51	37.60	-36.57	63.92	7.30	-18.11
73	Fondazio ne	26, 27	0	17.41	-71.86	-38.87	-8.47	7.31	25.84
			33	17.35	-71.87	-15.67	149.19	-1.32	26.43
			66	17.29	-71.87	59.77	308.20	-10.14	27.04
74	Fondazio ne	27, 29	0	1.21	63.57	59.39	-273.26	-9.07	-27.70
			33	1.16	63.56	-4.38	-113.15	-0.04	-27.08
			66	1.11	63.55	-15.19	47.70	8.80	-26.47
75	Fondazio ne	27, 29	0	1.77	-63.76	-15.20	-40.86	8.80	25.65
			33	1.72	-63.77	-2.01	120.94	0.24	26.27
			66	1.68	-63.78	64.76	283.86	-8.54	26.90
76	Fondazio ne	28, 30	0	-4.92	-60.34	70.14	-291.10	8.86	25.68
			37	-4.93	-60.34	-5.32	-122.19	-0.40	25.06
			73	-4.94	-60.33	-18.93	47.83	-9.43	24.45
77	Fondazio ne	28, 30	0	-1.85	71.24	-21.18	-45.47	-9.43	-25.43
			37	-1.87	71.24	-6.54	125.98	-0.04	-26.04

			73	-1.88	71.25	71.01	299.24	9.58	-26.68
78	Fondazio ne	29, 31	0	17.43	67.45	67.32	-288.06	-9.61	-28.08
			33	17.38	67.45	-0.74	-124.44	-0.45	-27.44
			66	17.34	67.44	-14.77	39.43	8.51	-26.82
79	Fondazio ne	29, 31	0	17.92	-61.92	-14.27	-53.54	8.51	26.81
			33	17.88	-61.93	-4.85	110.73	-0.44	27.43
			66	17.86	-61.94	58.89	275.61	-9.60	28.08
80	Fondazio ne	30, 32	0	1.16	-61.40	68.72	-287.91	9.59	27.92
			34	1.15	-61.39	-1.87	-124.18	0.13	27.31
			69	1.14	-61.39	-16.28	40.13	-9.12	26.71
81	Fondazio ne	30, 32	0	1.20	72.52	-18.52	-37.85	-9.12	-26.69
			34	1.20	72.53	-3.24	127.26	0.12	-27.29
			69	1.19	72.53	68.78	293.41	9.58	-27.91
82	Fondazio ne	31, 33	0	-0.61	66.63	62.10	-285.42	-8.51	-26.89
			33	-0.63	66.63	-4.84	-120.29	0.25	-26.25
			66	-0.65	66.62	-17.30	44.72	8.81	-25.62
83	Fondazio ne	31, 33	0	0.88	-62.70	-18.17	-51.03	8.81	25.28
			33	0.86	-62.71	-7.77	114.08	0.37	25.91
			66	0.84	-62.72	57.17	279.57	-8.29	26.55
84	Fondazio ne	32, 34	0	2.42	-65.34	67.45	-296.74	9.58	27.99
			35	2.41	-65.33	-5.96	-128.83	0.03	27.36
			69	2.40	-65.32	-21.43	39.19	-9.30	26.75
85	Fondazio ne	32, 34	0	1.65	67.18	-22.44	-38.24	-9.30	-26.42
			35	1.64	67.19	-6.60	130.18	-0.08	-27.04
			69	1.64	67.20	67.47	299.32	9.36	-27.67
86	Fondazio ne	33, 35	0	14.49	64.98	60.03	-283.31	-9.36	-27.60
			33	14.46	64.97	-6.14	-117.78	-0.35	-26.95
			66	14.45	64.97	-17.73	47.47	8.44	-26.32
87	Fondazio ne	33, 35	0	16.57	-63.53	-19.81	-49.17	8.44	26.54
			33	16.56	-63.54	-8.78	116.03	-0.43	27.17
			66	16.56	-63.54	56.80	281.47	-9.50	27.81
88	Fondazio ne	34, 36	0	2.79	-61.28	60.72	-288.84	9.37	27.41
			35	2.79	-61.27	-9.70	-119.40	0.02	26.77
			69	2.78	-61.27	-21.68	49.96	-9.10	26.14
89	Fondazio ne	34, 36	0	2.53	71.47	-24.01	-43.56	-9.10	-26.01
			35	2.53	71.48	-9.79	126.08	-0.02	-26.64
			69	2.52	71.49	63.07	296.37	9.28	-27.29
90	Fondazio ne	35, 37	0	-2.59	63.31	58.92	-278.63	-8.42	-26.75
			33	-2.59	63.30	-5.73	-113.26	0.31	-26.11
			66	-2.59	63.29	-15.87	51.71	8.82	-25.49
91	Fondazio ne	35, 37	0	-0.12	-65.46	-18.96	-43.76	8.82	25.41
			33	-0.12	-65.46	-6.20	121.04	0.33	26.03
			66	-0.12	-65.47	60.94	285.91	-8.36	26.67
92	Fondazio ne	36, 38	0	4.03	-56.54	57.82	-287.35	9.29	27.32
			35	4.03	-56.53	-11.89	-116.77	-0.02	26.66
			69	4.03	-56.52	-22.76	53.78	-9.11	26.02
93	Fondazio ne	36, 38	0	2.84	77.53	-27.87	-39.33	-9.11	-25.76
			35	2.84	77.53	-11.98	131.60	-0.11	-26.40
			69	2.85	77.54	63.02	303.32	9.11	-27.06
94	Fondazio ne	37, 39	0	14.14	62.20	61.76	-276.78	-9.44	-27.81
			33	14.13	62.19	-2.40	-112.19	-0.37	-27.18
			66	14.14	62.18	-12.36	51.72	8.50	-26.56
95	Fondazio ne	37, 39	0	16.04	-66.40	-15.65	-39.76	8.50	26.94
			33	16.05	-66.41	-1.80	123.64	-0.49	27.56
			66	16.07	-66.41	65.91	286.69	-9.69	28.19

96	Fondazio ne	38, 40	0	6.47	-47.40	51.75	-278.94	9.14	26.88
			34	6.48	-47.39	-14.52	-107.99	0.04	26.22
			69	6.48	-47.38	-22.21	63.18	-8.82	25.57
97	Fondazio ne	38, 40	0	3.78	87.04	-32.02	-32.89	-8.82	-25.14
			34	3.79	87.05	-13.89	138.94	-0.10	-25.79
			69	3.80	87.06	63.28	311.88	8.85	-26.46
98	Fondazio ne	39, 41	0	-2.26	63.96	66.17	-287.70	-8.62	-27.00
			33	-2.24	63.95	-1.96	-125.42	0.18	-26.38
			66	-2.22	63.94	-16.75	35.66	8.79	-25.78
99	Fondazio ne	39, 41	0	-1.28	-63.47	-18.51	-52.87	8.79	27.12
			33	-1.26	-63.47	-9.52	107.20	-0.26	27.72
			66	-1.25	-63.48	52.16	266.52	-9.50	28.32
100	Fondazio ne	40, 42	0	8.85	-37.77	47.89	-272.32	8.87	27.43
			35	8.87	-37.76	-15.88	-97.28	-0.47	26.75
			69	8.89	-37.76	-19.17	78.39	-9.59	26.09
101	Fondazio ne	40, 42	0	9.78	101.09	-37.88	7.89	-9.59	-27.17
			35	9.80	101.10	-4.72	184.64	-0.10	-27.84
			69	9.82	101.11	89.68	362.86	9.62	-28.53
102	Fondazio ne	41, 44	0	-4.85	68.34	52.58	-298.16	-9.50	-26.56
			33	-4.84	68.33	-19.66	-139.82	-0.84	-25.96
			66	-4.82	68.33	-39.84	17.37	7.64	-25.39
103	Fondazio ne	41, 44	0	-9.20	-40.41	-40.12	-51.51	7.63	16.27
			33	-9.18	-40.42	-31.27	105.09	2.17	16.82
			66	-9.18	-40.42	29.25	261.75	-3.47	17.38
104	Fondazio ne	42, 43	0	14.64	-38.26	66.83	-150.45	9.61	24.52
			23	14.66	-38.25	45.94	-31.11	4.03	24.05
			46	14.68	-38.25	52.51	88.28	-1.45	23.58
105	Fondazio ne	43, 44	0	72.16	12.28	-149.91	-133.61	-4.07	-5.26
			49	71.21	12.27	-177.50	13.78	-1.49	-5.30
			97	70.32	12.27	-140.69	132.72	1.10	-5.34
106	Fondazio ne	43, 44	0	66.92	0.63	-118.12	-56.93	1.10	1.20
			49	66.08	0.63	-120.78	42.67	0.52	1.16
			97	65.30	0.63	-78.18	130.20	-0.03	1.12
107	Fondazio ne	43, 44	0	64.16	-2.20	-56.63	-51.09	-0.03	-0.06
			49	63.43	-2.20	-61.42	30.08	0.01	-0.08
			97	62.74	-2.20	-27.47	108.68	0.05	-0.10
108	Fondazio ne	43, 44	0	64.09	0.45	-13.22	-63.13	0.06	0.08
			49	63.46	0.45	-24.72	15.51	0.02	0.08
			97	62.87	0.45	2.37	95.62	-0.02	0.08
109	Fondazio ne	43, 44	0	63.89	0.06	10.52	-76.38	-0.02	0.02
			49	63.36	0.06	-6.61	5.96	-0.03	0.03
			97	62.87	0.06	16.91	90.69	-0.05	0.05
110	Fondazio ne	43, 44	0	63.66	-0.16	20.37	-86.46	-0.05	-0.01
			49	63.22	-0.16	-0.53	0.55	-0.05	0.02
			97	62.84	-0.16	21.38	89.50	-0.07	0.06
111	Fondazio ne	43, 44	0	63.26	-0.19	21.95	-92.26	-0.07	-0.04
			49	62.92	-0.19	-0.92	-1.76	-0.06	0.01
			97	62.64	-0.19	20.55	89.90	-0.08	0.06
112	Fondazio ne	43, 44	0	62.74	-0.20	20.12	-94.49	-0.08	-0.05
			49	62.50	-0.20	-3.35	-2.00	-0.07	0.01
			97	62.31	-0.20	18.34	91.03	-0.09	0.07
113	Fondazio ne	43, 44	0	62.17	-0.38	17.90	-95.09	-0.08	-0.07
			49	62.03	-0.38	-5.64	-1.71	-0.07	0.00
			97	61.94	-0.38	16.32	91.87	-0.09	0.07
114	Fondazio	43, 44	0	61.59	0.81	16.72	-93.29	-0.08	-0.07

	ne								
			49	61.54	0.81	-5.88	0.40	-0.07	0.01
			97	61.55	0.81	17.12	94.11	-0.09	0.08
115	Fondazio ne	43, 44	0	61.08	-0.39	16.49	-92.73	-0.09	-0.08
			49	61.14	-0.39	-5.86	0.90	-0.07	-0.01
			97	61.24	-0.39	17.31	94.35	-0.08	0.07
116	Fondazio ne	43, 44	0	60.51	0.02	18.05	-91.63	-0.09	-0.07
			49	60.66	0.02	-3.89	1.53	-0.07	0.00
			97	60.86	0.02	19.40	94.21	-0.09	0.07
117	Fondazio ne	43, 44	0	59.82	0.13	20.13	-90.52	-0.09	-0.08
			49	60.06	0.13	-1.56	1.46	-0.07	-0.01
			97	60.35	0.13	21.27	92.41	-0.08	0.06
118	Fondazio ne	43, 44	0	58.85	0.28	21.22	-90.02	-0.08	-0.07
			49	59.19	0.28	-0.80	-0.44	-0.06	-0.01
			97	59.57	0.28	20.36	87.39	-0.07	0.04
119	Fondazio ne	43, 44	0	57.43	0.37	18.18	-91.00	-0.07	-0.07
			49	57.86	0.37	-5.24	-5.25	-0.05	-0.02
			97	58.33	0.37	12.53	78.23	-0.05	0.02
120	Fondazio ne	43, 44	0	55.38	0.52	6.55	-95.13	-0.05	-0.10
			49	55.90	0.52	-19.99	-13.86	-0.01	-0.07
			97	56.47	0.52	-7.43	65.72	0.02	-0.05
121	Fondazio ne	43, 44	0	52.79	0.52	-19.13	-104.41	0.02	0.13
			49	53.40	0.52	-50.86	-25.41	-0.05	0.15
			97	54.05	0.52	-43.89	55.08	-0.12	0.15
122	Fondazio ne	43, 44	0	49.58	0.70	-59.69	-112.86	-0.12	-0.83
			49	50.27	0.70	-94.33	-27.81	0.28	-0.84
			97	51.00	0.70	-85.61	66.26	0.69	-0.85
123	Fondazio ne	43, 44	0	49.64	0.48	-99.79	-140.47	0.69	0.85
			49	50.40	0.48	-142.62	-31.86	0.28	0.84
			97	51.21	0.48	-127.66	98.34	-0.12	0.82
124	Fondazio ne	43, 45	0	25.89	-68.61	84.04	-377.88	3.67	18.40
			33	25.92	-68.60	-12.46	-207.11	-2.29	17.75
			66	25.97	-68.59	-52.78	-37.30	-8.05	17.12
125	Fondazio ne	43, 45	0	25.09	50.23	-24.20	-49.00	-8.05	-26.54
			33	25.15	50.24	-12.43	120.34	0.82	-27.18
			66	25.21	50.25	55.20	289.63	9.89	-27.83
126	Fondazio ne	44, 46	0	11.24	36.66	28.47	-260.84	-4.68	-18.74
			33	11.25	36.66	-31.73	-103.98	1.41	-18.18
			66	11.26	36.65	-40.12	53.25	7.32	-17.63
127	Fondazio ne	44, 46	0	17.42	-78.58	-48.35	26.16	7.32	25.81
			33	17.43	-78.59	-13.65	184.42	-1.29	26.38
			66	17.46	-78.60	73.53	344.26	-10.09	26.97
128	Fondazio ne	45, 47	0	10.36	-88.91	67.22	-324.10	8.79	27.76
			33	10.43	-88.90	-11.85	-155.12	-0.26	27.11
			66	10.50	-88.89	-35.26	13.24	-9.10	26.48
129	Fondazio ne	45, 47	0	13.46	44.96	-18.40	-43.04	-9.10	-26.36
			33	13.54	44.97	-4.88	125.08	-0.30	-26.99
			66	13.63	44.97	64.13	293.23	8.71	-27.63
130	Fondazio ne	46, 48	0	3.76	71.46	70.79	-293.76	-9.03	-27.01
			33	3.79	71.45	0.40	-132.73	-0.21	-26.42
			66	3.82	71.44	-16.74	29.02	8.41	-25.83
131	Fondazio ne	46, 48	0	10.38	-60.18	-11.73	-38.54	8.41	24.59
			33	10.41	-60.19	2.35	124.07	0.20	25.17
			66	10.45	-60.19	70.25	287.65	-8.21	25.77
132	Fondazio ne	47, 49	0	33.18	-81.01	68.41	-298.55	9.77	28.33

			33	33.27	-81.00	-2.42	-130.76	0.52	27.69
			66	33.37	-80.99	-18.02	36.23	-8.51	27.07
133	Fondazio ne	47, 49	0	38.11	50.35	-8.32	-52.59	-8.51	-27.53
			33	38.23	50.35	1.77	113.79	0.68	-28.15
			66	38.36	50.36	66.68	279.66	10.07	-28.77
134	Fondazio ne	48, 50	0	28.94	78.06	77.82	-298.03	-9.29	-27.33
			33	28.98	78.06	6.53	-134.00	-0.37	-26.73
			66	29.04	78.05	-10.65	29.90	8.36	-26.14
135	Fondazio ne	48, 50	0	35.90	-55.28	-6.13	-41.21	8.35	27.60
			33	35.97	-55.29	7.29	122.60	-0.85	28.19
			66	36.04	-55.30	74.75	286.33	-10.25	28.78
136	Fondazio ne	49, 51	0	23.53	-85.20	79.42	-302.87	9.04	28.00
			33	23.67	-85.19	6.68	-138.02	-0.10	27.39
			66	23.82	-85.18	-11.91	25.23	-9.04	26.80
137	Fondazio ne	49, 51	0	30.01	48.81	-0.05	-61.14	-9.04	-27.89
			33	30.17	48.82	6.46	100.54	0.26	-28.46
			66	30.34	48.83	66.07	260.65	9.75	-29.05
138	Fondazio ne	50, 52	0	20.15	85.40	86.23	-306.60	-9.24	-28.41
			33	20.24	85.40	11.98	-143.56	0.04	-27.82
			66	20.34	85.39	-8.70	18.08	9.12	-27.25
139	Fondazio ne	50, 52	0	27.57	-50.39	1.90	-53.37	9.12	28.95
			33	27.67	-50.40	10.74	106.84	-0.52	29.51
			66	27.78	-50.41	72.21	265.55	-10.35	30.07
140	Fondazio ne	51, 53	0	43.66	-94.79	81.43	-278.86	10.96	29.94
			33	43.85	-94.78	15.51	-120.88	1.17	29.37
			66	44.05	-94.78	1.26	34.28	-8.43	28.83
141	Fondazio ne	51, 53	0	49.76	36.12	17.89	-51.83	-8.43	-29.88
			33	49.98	36.13	25.94	100.33	1.52	-30.39
			66	50.22	36.14	83.67	249.18	11.63	-30.89
142	Fondazio ne	52, 54	0	30.40	96.04	88.33	-291.60	-10.42	-29.53
			33	30.52	96.03	17.99	-135.04	-0.77	-28.98
			66	30.65	96.03	-1.16	18.61	8.71	-28.46
143	Fondazio ne	52, 54	0	35.32	-37.16	15.98	-61.52	8.70	29.51
			33	35.47	-37.17	20.58	89.03	-1.12	30.01
			66	35.63	-37.17	74.32	236.24	-11.10	30.50
144	Fondazio ne	53, 55	0	32.13	-111.49	106.11	-301.57	9.84	25.06
			33	32.38	-111.48	30.54	-156.94	1.65	24.59
			66	32.64	-111.48	1.85	-17.56	-6.39	24.17
145	Fondazio ne	53, 55	0	34.57	-2.02	28.17	-116.32	-6.38	-19.28
			33	34.85	-2.02	11.97	17.47	0.05	-19.65
			66	35.13	-2.02	38.96	145.43	6.59	-19.99
146	Fondazio ne	54, 56	0	36.02	109.57	97.96	-291.77	-10.47	-25.97
			33	36.19	109.57	25.38	-148.70	-1.97	-25.50
			66	36.37	109.56	-0.80	-10.67	6.37	-25.09
147	Fondazio ne	54, 56	0	36.59	-1.69	24.50	-102.41	6.36	19.35
			33	36.79	-1.69	12.71	30.31	-0.09	19.72
			66	37.00	-1.70	43.82	157.48	-6.65	20.06
148	Fondazio ne	55, 57	0	26.73	-70.75	61.78	-240.76	4.28	7.77
			40	27.09	-70.74	-4.70	-95.00	1.26	7.43
			80	27.46	-70.74	-15.16	41.09	-1.64	7.18
149	Fondazio ne	55, 57	0	29.66	-5.39	-8.89	-96.21	-1.63	-7.96
			40	30.05	-5.38	-21.71	30.55	1.57	-8.12
			80	30.46	-5.38	14.10	148.58	4.82	-8.20
150	Fondazio ne	56, 70	0	27.65	69.61	65.88	-246.07	-4.31	-7.91
			40	27.92	69.60	-2.82	-100.93	-1.24	-7.56

			80	28.21	69.60	-15.70	34.83	1.71	-7.29
151	Fondazio ne	56, 70	0	29.27	4.21	-8.77	-96.19	1.70	7.98
			40	29.57	4.21	-21.59	30.49	-1.51	8.16
			80	29.89	4.21	14.23	148.68	-4.78	8.26
152	Fondazio ne	57, 58	0	-11.44	-17.71	17.20	-181.94	-0.92	2.06
			42	-11.49	-17.72	-34.05	-65.62	-1.69	1.68
			83	-11.55	-17.72	-37.98	45.92	-2.33	1.42
153	Fondazio ne	57, 58	0	-12.93	-15.67	-33.14	-81.04	-2.32	0.60
			42	-12.99	-15.68	-44.25	27.04	-2.53	0.42
			83	-13.06	-15.68	-10.90	133.17	-2.68	0.33
154	Fondazio ne	58, 59	0	-19.09	-8.13	-1.02	-111.94	-2.29	-2.72
			35	-19.15	-8.14	-24.57	-24.77	-1.34	-2.76
			69	-19.22	-8.14	-18.17	61.72	-0.39	-2.77
155	Fondazio ne	58, 59	0	-10.75	-10.05	-10.27	-61.36	-0.38	0.86
			35	-10.82	-10.05	-16.55	24.89	-0.68	0.87
			69	-10.90	-10.06	6.95	111.25	-0.99	0.90
156	Fondazio ne	59, 60	0	-3.71	-5.38	13.88	-111.94	-0.88	-0.94
			35	-3.80	-5.38	-9.79	-25.35	-0.57	-0.89
			69	-3.88	-5.39	-3.55	61.53	-0.27	-0.82
157	Fondazio ne	59, 60	0	2.29	-4.10	1.58	-63.23	-0.27	0.07
			35	2.21	-4.10	-5.17	24.09	-0.31	0.15
			69	2.12	-4.11	18.30	111.94	-0.38	0.24
158	Fondazio ne	60, 61	0	7.22	-6.42	19.74	-108.50	-0.34	-0.21
			35	7.14	-6.43	-2.45	-20.19	-0.29	-0.11
			69	7.06	-6.43	5.88	68.48	-0.27	0.00
159	Fondazio ne	60, 61	0	9.82	-2.37	7.00	-65.57	-0.27	-0.25
			35	9.75	-2.37	-0.26	23.45	-0.20	-0.13
			69	9.67	-2.38	23.25	112.79	-0.18	-0.01
160	Fondazio ne	61, 62	0	19.49	-3.75	25.07	-117.86	-0.16	-0.21
			35	19.42	-3.76	-0.14	-28.36	-0.11	-0.08
			69	19.36	-3.76	5.52	61.10	-0.10	0.05
161	Fondazio ne	61, 62	0	21.51	-2.11	7.32	-71.70	-0.10	-0.18
			35	21.46	-2.11	-1.98	17.72	-0.07	-0.04
			69	21.42	-2.12	19.56	107.08	-0.08	0.11
162	Fondazio ne	62, 63	0	17.27	-3.62	21.35	-117.84	-0.11	-0.03
			35	17.24	-3.63	-3.90	-28.66	-0.12	0.12
			69	17.21	-3.63	1.56	60.24	-0.19	0.27
163	Fondazio ne	62, 63	0	18.69	-1.38	3.09	-74.24	-0.19	-0.27
			35	18.67	-1.39	-7.22	14.43	-0.12	-0.11
			69	18.66	-1.39	13.04	102.97	-0.11	0.05
164	Fondazio ne	63, 64	0	19.44	-1.41	13.91	-108.78	-0.11	-0.13
			35	19.44	-1.42	-8.36	-20.38	-0.10	0.03
			69	19.44	-1.42	-0.16	67.89	-0.14	0.19
165	Fondazio ne	63, 64	0	19.65	1.38	-0.17	-67.97	-0.14	-0.20
			35	19.66	1.37	-8.40	20.30	-0.09	-0.04
			69	19.67	1.37	13.84	108.68	-0.11	0.12
166	Fondazio ne	64, 65	0	19.30	1.38	13.05	-103.18	-0.10	-0.05
			35	19.32	1.37	-7.28	-14.66	-0.11	0.10
			69	19.35	1.37	2.94	74.00	-0.18	0.26
167	Fondazio ne	64, 65	0	18.29	3.72	1.42	-60.48	-0.18	-0.28
			35	18.33	3.71	-4.13	28.40	-0.11	-0.12
			69	18.37	3.71	21.03	117.56	-0.09	0.03
168	Fondazio ne	65, 66	0	22.72	2.32	19.29	-107.12	-0.06	-0.13
			35	22.78	2.32	-2.26	-17.78	-0.04	0.02
			69	22.84	2.31	7.01	71.64	-0.08	0.17

169	Fondazio ne	65, 66	0	21.11	4.16	5.14	-60.91	-0.08	-0.11
			35	21.18	4.16	-0.45	28.57	-0.07	0.04
			69	21.26	4.15	24.83	118.10	-0.10	0.18
170	Fondazio ne	66, 67	0	11.46	2.36	22.91	-112.04	-0.12	0.06
			35	11.54	2.36	-0.33	-22.63	-0.17	0.20
			69	11.63	2.35	7.23	66.49	-0.26	0.34
171	Fondazio ne	66, 67	0	8.60	4.66	4.97	-66.77	-0.26	-0.10
			35	8.69	4.66	-2.75	22.03	-0.25	0.03
			69	8.79	4.65	20.10	110.52	-0.28	0.16
172	Fondazio ne	67, 68	0	4.33	5.21	16.82	-108.04	-0.32	-0.24
			35	4.43	5.20	-5.26	-19.95	-0.26	-0.12
			69	4.53	5.20	2.96	67.66	-0.23	-0.01
173	Fondazio ne	67, 68	0	-1.25	6.73	-1.62	-65.00	-0.24	0.76
			35	-1.15	6.73	-9.01	22.22	-0.52	0.86
			69	-1.05	6.72	13.64	109.17	-0.83	0.95
174	Fondazio ne	68, 69	0	-8.30	10.89	7.40	-111.92	-0.94	-0.96
			35	-8.19	10.89	-16.27	-25.19	-0.62	-0.89
			69	-8.10	10.88	-10.04	61.44	-0.32	-0.84
175	Fondazio ne	68, 69	0	-16.46	8.47	-17.63	-62.52	-0.33	2.68
			35	-16.37	8.47	-24.24	24.36	-1.26	2.71
			69	-16.28	8.47	-0.78	111.91	-2.20	2.72
176	Fondazio ne	69, 70	0	-11.91	17.00	-10.59	-132.67	-2.62	-0.40
			42	-11.81	17.00	-43.65	-26.10	-2.45	-0.43
			83	-11.72	16.99	-32.06	82.42	-2.25	-0.52
177	Fondazio ne	69, 70	0	-11.46	18.19	-38.47	-44.38	-2.26	-1.08
			42	-11.38	18.19	-33.82	67.54	-1.78	-1.26
			83	-11.30	18.18	18.29	184.19	-1.20	-1.54
178	Primo Impalcato	1, 2	0	108.02	0.02	7.90	-7.19	59.75	33.25
			83	108.02	0.02	1.93	-7.19	32.11	33.25
			166	108.02	0.02	-4.04	-7.19	4.47	33.25
179	Primo Impalcato	1, 15	0	18.37	4.42	-18.02	18.24	-71.48	-80.11
			80	18.37	4.42	-3.53	18.24	-7.79	-80.11
			159	18.37	4.42	10.97	18.24	55.90	-80.11
180	Primo Impalcato	2, 3	0	89.31	-0.03	-3.72	1.67	5.44	6.67
			69	89.31	-0.03	-2.57	1.67	0.84	6.67
			138	89.31	-0.03	-1.42	1.67	-3.75	6.67
181	Primo Impalcato	3, 4	0	89.14	-0.05	-1.39	1.29	-3.53	-0.70
			69	89.14	-0.05	-0.51	1.29	-3.05	-0.70
			138	89.14	-0.05	0.38	1.29	-2.57	-0.70
182	Primo Impalcato	4, 5	0	89.00	0.00	0.37	-0.14	-2.47	-1.32
			69	89.00	0.00	0.27	-0.14	-1.57	-1.32
			138	89.00	0.00	0.18	-0.14	-0.66	-1.32
183	Primo Impalcato	5, 6	0	88.89	0.02	0.21	-0.34	-0.64	-0.57
			69	88.89	0.02	-0.03	-0.34	-0.25	-0.57
			138	88.89	0.02	-0.26	-0.34	0.15	-0.57
184	Primo Impalcato	6, 7	0	106.28	0.01	-0.22	0.27	0.13	-0.13
			69	106.28	0.01	-0.03	0.27	0.22	-0.13
			138	106.28	0.01	0.16	0.27	0.31	-0.13
185	Primo Impalcato	7, 8	0	86.49	0.00	0.20	-0.73	0.32	0.00
			69	86.49	0.00	-0.30	-0.73	0.32	0.00
			138	86.49	0.00	-0.80	-0.73	0.31	0.00
186	Primo Impalcato	8, 9	0	86.51	-0.02	-0.79	0.66	0.32	0.14
			69	86.51	-0.02	-0.33	0.66	0.22	0.14
			138	86.51	-0.02	0.12	0.66	0.13	0.14
187	Primo	9, 10	0	108.12	-0.02	0.10	0.06	0.13	0.58

	Impalcato								
			69	108.12	-0.02	0.14	0.06	-0.27	0.58
			138	108.12	-0.02	0.19	0.06	-0.68	0.58
188	Primo Impalcato	10, 11	0	91.95	0.00	0.18	0.06	-0.70	1.32
			69	91.95	0.00	0.23	0.06	-1.61	1.32
			138	91.95	0.00	0.27	0.06	-2.52	1.32
189	Primo Impalcato	11, 12	0	92.11	0.05	0.31	-1.29	-2.62	0.64
			69	92.11	0.05	-0.58	-1.29	-3.06	0.64
			138	92.11	0.05	-1.47	-1.29	-3.50	0.64
190	Primo Impalcato	12, 13	0	92.29	0.03	-1.48	-1.32	-3.74	-6.89
			69	92.29	0.03	-2.39	-1.32	1.02	-6.89
			138	92.29	0.03	-3.30	-1.32	5.77	-6.89
191	Primo Impalcato	13, 14	0	111.10	-0.02	-3.59	4.66	4.79	-33.90
			83	111.10	-0.02	0.28	4.66	32.98	-33.90
			166	111.10	-0.02	4.15	4.66	61.16	-33.90
192	Primo Impalcato	14, 16	0	16.22	-4.31	-18.78	18.72	65.53	74.52
			80	16.22	-4.31	-3.90	18.72	6.29	74.52
			159	16.22	-4.31	10.98	18.72	-52.96	74.52
193	Primo Impalcato	15, 17	0	-22.38	0.79	3.30	7.58	49.66	20.35
			66	-22.38	0.79	8.30	7.58	36.23	20.35
			132	-22.38	0.79	13.30	7.58	22.80	20.35
194	Primo Impalcato	16, 18	0	-24.35	-0.86	1.56	9.53	-47.48	-19.45
			66	-24.35	-0.86	7.85	9.53	-34.64	-19.45
			132	-24.35	-0.86	14.15	9.53	-21.80	-19.45
195	Primo Impalcato	17, 19	0	-6.52	0.08	8.63	-2.02	20.84	15.08
			66	-6.52	0.08	7.29	-2.02	10.89	15.08
			132	-6.52	0.08	5.95	-2.02	0.94	15.08
196	Primo Impalcato	18, 20	0	-10.31	-0.09	9.46	-3.53	-22.29	-16.02
			66	-10.31	-0.09	7.13	-3.53	-11.72	-16.02
			132	-10.31	-0.09	4.80	-3.53	-1.15	-16.02
197	Primo Impalcato	19, 21	0	-34.46	-0.04	4.12	-0.41	1.67	2.22
			66	-34.46	-0.04	3.84	-0.41	0.20	2.22
			132	-34.46	-0.04	3.57	-0.41	-1.27	2.22
198	Primo Impalcato	20, 22	0	-39.83	0.03	1.82	2.22	-1.79	-2.31
			66	-39.83	0.03	3.28	2.22	-0.26	-2.31
			132	-39.83	0.03	4.75	2.22	1.26	-2.31
199	Primo Impalcato	21, 23	0	-3.54	-0.02	3.40	-0.07	-1.61	-0.83
			66	-3.54	-0.02	3.36	-0.07	-1.06	-0.83
			132	-3.54	-0.02	3.32	-0.07	-0.52	-0.83
200	Primo Impalcato	22, 24	0	-13.88	0.02	4.66	-2.13	1.70	0.81
			66	-13.88	0.02	3.25	-2.13	1.17	0.81
			132	-13.88	0.02	1.84	-2.13	0.63	0.81
201	Primo Impalcato	23, 25	0	-25.28	0.02	4.48	-6.90	0.02	0.06
			66	-25.28	0.02	-0.07	-6.90	-0.02	0.06
			132	-25.28	0.02	-4.62	-6.90	-0.06	0.06
202	Primo Impalcato	24, 26	0	-37.27	-0.01	0.86	-2.48	0.11	0.09
			66	-37.27	-0.01	-0.77	-2.48	0.05	0.09
			132	-37.27	-0.01	-2.41	-2.48	-0.01	0.09
203	Primo Impalcato	25, 28	0	11.45	-0.01	-3.53	-0.33	-0.62	-0.16
			85	11.45	-0.01	-3.82	-0.33	-0.48	-0.16
			170	11.45	-0.01	-4.10	-0.33	-0.35	-0.16
204	Primo Impalcato	26, 27	0	-12.40	0.01	-2.60	2.63	0.49	0.37
			66	-12.40	0.01	-0.87	2.63	0.24	0.37
			132	-12.40	0.01	0.86	2.63	0.00	0.37
205	Primo Impalcato	27, 29	0	-36.27	0.00	-3.26	4.36	-0.46	-0.08

			66	-36.27	0.00	-0.38	4.36	-0.41	-0.08
			132	-36.27	0.00	2.49	4.36	-0.36	-0.08
206	Primo Impalcato	28, 30	0	-23.33	-0.01	-1.08	1.34	0.19	0.03
			73	-23.33	-0.01	-0.10	1.34	0.16	0.03
			146	-23.33	-0.01	0.88	1.34	0.14	0.03
207	Primo Impalcato	29, 31	0	-12.59	0.00	0.34	1.78	0.12	-0.07
			66	-12.59	0.00	1.52	1.78	0.16	-0.07
			132	-12.59	0.00	2.70	1.78	0.21	-0.07
208	Primo Impalcato	30, 32	0	-27.24	0.00	5.25	-5.45	0.10	0.04
			69	-27.24	0.00	1.51	-5.45	0.08	0.04
			137	-27.24	0.00	-2.22	-5.45	0.05	0.04
209	Primo Impalcato	31, 33	0	-33.64	0.01	-2.53	3.63	-0.27	-0.05
			66	-33.64	0.01	-0.13	3.63	-0.24	-0.05
			132	-33.64	0.01	2.26	3.63	-0.21	-0.05
210	Primo Impalcato	32, 34	0	-31.45	0.01	3.12	-4.23	0.03	0.06
			69	-31.45	0.01	0.20	-4.23	-0.02	0.06
			138	-31.45	0.01	-2.71	-4.23	-0.06	0.06
211	Primo Impalcato	33, 35	0	-5.18	0.01	-1.87	4.02	0.27	-0.01
			66	-5.18	0.01	0.79	4.02	0.28	-0.01
			132	-5.18	0.01	3.44	4.02	0.29	-0.01
212	Primo Impalcato	34, 36	0	-36.12	0.01	3.32	-4.76	-0.08	0.01
			69	-36.12	0.01	0.03	-4.76	-0.09	0.01
			138	-36.12	0.01	-3.25	-4.76	-0.10	0.01
213	Primo Impalcato	35, 37	0	-24.67	0.01	-2.25	3.79	-0.19	-0.03
			66	-24.67	0.01	0.25	3.79	-0.18	-0.03
			132	-24.67	0.01	2.75	3.79	-0.16	-0.03
214	Primo Impalcato	36, 38	0	-41.29	0.00	3.37	-5.26	-0.14	-0.01
			69	-41.29	0.00	-0.26	-5.26	-0.13	-0.01
			138	-41.29	0.00	-3.89	-5.26	-0.13	-0.01
215	Primo Impalcato	37, 39	0	6.39	0.01	-1.94	1.65	0.33	0.02
			66	6.39	0.01	-0.85	1.65	0.32	0.02
			132	6.39	0.01	0.23	1.65	0.31	0.02
216	Primo Impalcato	38, 40	0	-47.00	-0.01	3.22	-5.40	-0.19	-0.23
			69	-47.00	-0.01	-0.48	-5.40	-0.03	-0.23
			137	-47.00	-0.01	-4.18	-5.40	0.12	-0.23
217	Primo Impalcato	39, 41	0	-17.88	0.01	-3.30	7.13	-0.16	0.16
			66	-17.88	0.01	1.41	7.13	-0.27	0.16
			132	-17.88	0.01	6.12	7.13	-0.37	0.16
218	Primo Impalcato	40, 42	0	-53.21	-0.02	3.20	-0.78	0.05	-0.62
			69	-53.21	-0.02	2.66	-0.78	0.48	-0.62
			138	-53.21	-0.02	2.12	-0.78	0.91	-0.62
219	Primo Impalcato	41, 44	0	-10.85	-0.02	2.16	-5.03	-0.40	-0.44
			66	-10.85	-0.02	-1.15	-5.03	-0.11	-0.44
			132	-10.85	-0.02	-4.47	-5.03	0.17	-0.44
220	Primo Impalcato	42, 43	0	-59.90	0.06	10.82	-29.28	0.89	0.71
			23	-59.90	0.06	4.09	-29.28	0.73	0.71
			46	-59.90	0.06	-2.65	-29.28	0.57	0.71
221	Primo Impalcato	43, 45	0	-29.81	0.00	-1.75	1.31	0.08	0.19
			66	-29.81	0.00	-0.89	1.31	-0.04	0.19
			132	-29.81	0.00	-0.03	1.31	-0.16	0.19
222	Primo Impalcato	44, 46	0	11.87	0.02	-4.98	4.68	0.64	0.45
			66	11.87	0.02	-1.89	4.68	0.34	0.45
			132	11.87	0.02	1.20	4.68	0.05	0.45
223	Primo Impalcato	45, 47	0	-55.47	0.01	0.62	-0.17	0.38	0.56
			66	-55.47	0.01	0.51	-0.17	0.01	0.56

			132	-55.47	0.01	0.39	-0.17	-0.36	0.56
224	Primo Impalcato	46, 48	0	-13.46	-0.01	-2.86	5.51	-0.43	-0.51
			66	-13.46	-0.01	0.78	5.51	-0.09	-0.51
			132	-13.46	-0.01	4.41	5.51	0.24	-0.51
225	Primo Impalcato	47, 49	0	-26.16	0.02	1.27	2.23	-0.85	0.73
			66	-26.16	0.02	2.75	2.23	-1.33	0.73
			132	-26.16	0.02	4.22	2.23	-1.82	0.73
226	Primo Impalcato	48, 50	0	11.78	-0.03	4.03	-2.44	0.67	-0.86
			66	11.78	-0.03	2.42	-2.44	1.24	-0.86
			132	11.78	-0.03	0.81	-2.44	1.80	-0.86
227	Primo Impalcato	49, 51	0	-50.49	0.03	6.15	-4.50	-1.46	-2.32
			66	-50.49	0.03	3.18	-4.50	0.07	-2.32
			132	-50.49	0.03	0.21	-4.50	1.60	-2.32
228	Primo Impalcato	50, 52	0	-16.14	-0.03	1.86	4.22	1.51	2.64
			66	-16.14	-0.03	4.64	4.22	-0.24	2.64
			132	-16.14	-0.03	7.42	4.22	-1.99	2.64
229	Primo Impalcato	51, 53	0	-17.68	-0.08	3.50	4.27	0.88	-15.00
			66	-17.68	-0.08	6.32	4.27	10.78	-15.00
			132	-17.68	-0.08	9.13	4.27	20.69	-15.00
230	Primo Impalcato	52, 54	0	-16.23	0.09	9.36	-1.90	-1.42	14.84
			66	-16.23	0.09	8.11	-1.90	-11.21	14.84
			132	-16.23	0.09	6.86	-1.90	-21.01	14.84
231	Primo Impalcato	53, 55	0	-30.17	-0.78	14.90	-10.13	22.63	-20.60
			66	-30.17	-0.78	8.22	-10.13	36.23	-20.60
			132	-30.17	-0.78	1.53	-10.13	49.82	-20.60
232	Primo Impalcato	54, 56	0	-20.48	0.82	14.36	-11.23	-22.78	20.51
			66	-20.48	0.82	6.95	-11.23	-36.31	20.51
			132	-20.48	0.82	-0.46	-11.23	-49.85	20.51
233	Primo Impalcato	55, 57	0	14.32	-4.42	10.23	-18.79	56.07	80.23
			80	14.32	-4.42	-4.71	-18.79	-7.71	80.23
			159	14.32	-4.42	-19.65	-18.79	-71.50	80.23
234	Primo Impalcato	56, 70	0	17.49	4.33	9.58	-16.64	-48.63	-69.75
			80	17.49	4.33	-3.65	-16.64	6.83	-69.75
			159	17.49	4.33	-16.88	-16.64	62.28	-69.75
235	Primo Impalcato	57, 58	0	108.61	0.01	8.37	-7.64	-59.72	-33.20
			83	108.61	0.01	2.02	-7.64	-32.13	-33.20
			166	108.61	0.01	-4.33	-7.64	-4.53	-33.20
236	Primo Impalcato	58, 59	0	90.83	0.02	-4.01	1.76	-5.50	-6.65
			69	90.83	0.02	-2.80	1.76	-0.90	-6.65
			138	90.83	0.02	-1.58	1.76	3.69	-6.65
237	Primo Impalcato	59, 60	0	90.66	0.04	-1.58	1.39	3.46	0.65
			69	90.66	0.04	-0.62	1.39	3.01	0.65
			138	90.66	0.04	0.34	1.39	2.56	0.65
238	Primo Impalcato	60, 61	0	90.52	0.00	0.29	-0.02	2.47	1.31
			69	90.52	0.00	0.28	-0.02	1.57	1.31
			138	90.52	0.00	0.26	-0.02	0.66	1.31
239	Primo Impalcato	61, 62	0	107.49	-0.02	0.26	0.02	0.65	0.57
			69	107.49	-0.02	0.27	0.02	0.25	0.57
			138	107.49	-0.02	0.29	0.02	-0.14	0.57
240	Primo Impalcato	62, 63	0	86.33	-0.02	0.33	-0.64	-0.15	0.14
			69	86.33	-0.02	-0.11	-0.64	-0.24	0.14
			138	86.33	-0.02	-0.55	-0.64	-0.33	0.14
241	Primo Impalcato	63, 64	0	86.33	0.00	-0.52	-0.01	-0.33	0.00
			69	86.33	0.00	-0.53	-0.01	-0.33	0.00
			138	86.33	0.00	-0.53	-0.01	-0.33	0.00

242	Primo Impalcato	64, 65	0	86.35	0.02	-0.56	0.61	-0.34	-0.14
			69	86.35	0.02	-0.14	0.61	-0.24	-0.14
			138	86.35	0.02	0.29	0.61	-0.14	-0.14
243	Primo Impalcato	65, 66	0	108.33	0.02	0.25	-0.02	-0.14	-0.61
			69	108.33	0.02	0.23	-0.02	0.28	-0.61
			138	108.33	0.02	0.22	-0.02	0.70	-0.61
244	Primo Impalcato	66, 67	0	92.05	0.00	0.22	0.02	0.72	-1.37
			69	92.05	0.00	0.24	0.02	1.66	-1.37
			138	92.05	0.00	0.26	0.02	2.61	-1.37
245	Primo Impalcato	67, 68	0	92.22	-0.05	0.30	-1.30	2.71	-0.72
			69	92.22	-0.05	-0.60	-1.30	3.21	-0.72
			138	92.22	-0.05	-1.49	-1.30	3.70	-0.72
246	Primo Impalcato	68, 69	0	92.40	-0.03	-1.50	-1.31	3.94	6.97
			69	92.40	-0.03	-2.41	-1.31	-0.87	6.97
			138	92.40	-0.03	-3.31	-1.31	-5.68	6.97
247	Primo Impalcato	69, 70	0	111.35	-0.01	-3.60	4.88	-4.66	34.79
			83	111.35	-0.01	0.46	4.88	-33.58	34.79
			166	111.35	-0.01	4.52	4.88	-62.50	34.79
248	Primo Impalcato	1	0	-240.30	-5.47	7.70	-4.04	-7.59	-6.27
			188	-240.30	-5.47	0.11	-4.04	4.20	-6.27
			376	-240.30	-5.47	-7.47	-4.04	16.00	-6.27
249	Primo Impalcato	2	0	-156.10	0.08	-24.12	12.67	-0.01	0.00
			188	-156.10	0.08	-0.29	12.67	-0.01	0.00
			376	-156.10	0.08	23.53	12.67	-0.01	0.00
250	Primo Impalcato	3	0	-143.04	0.10	-9.79	4.81	0.15	0.08
			188	-143.04	0.10	-0.74	4.81	-0.01	0.08
			376	-143.04	0.10	8.31	4.81	-0.17	0.08
251	Primo Impalcato	4	0	-131.50	0.03	-2.15	0.45	0.14	0.08
			188	-131.50	0.03	-1.30	0.45	-0.01	0.08
			376	-131.50	0.03	-0.46	0.45	-0.16	0.08
252	Primo Impalcato	5	0	-120.86	0.00	-0.33	-0.57	0.08	0.05
			188	-120.86	0.00	-1.41	-0.57	-0.01	0.05
			376	-120.86	0.00	-2.49	-0.57	-0.10	0.05
253	Primo Impalcato	6	0	-112.59	-0.01	-0.47	-0.44	0.04	0.02
			188	-112.59	-0.01	-1.29	-0.44	0.00	0.02
			376	-112.59	-0.01	-2.12	-0.44	-0.05	0.02
254	Primo Impalcato	7	0	-111.55	0.00	-0.74	-0.25	-0.01	-0.01
			188	-111.55	0.00	-1.22	-0.25	0.00	-0.01
			376	-111.55	0.00	-1.70	-0.25	0.01	-0.01
255	Primo Impalcato	8	0	-111.66	0.00	-0.74	-0.26	-0.02	-0.01
			188	-111.66	0.00	-1.23	-0.26	0.00	-0.01
			376	-111.66	0.00	-1.72	-0.26	0.02	-0.01
256	Primo Impalcato	9	0	-111.98	0.01	-0.49	-0.43	-0.04	-0.02
			188	-111.98	0.01	-1.31	-0.43	0.00	-0.02
			376	-111.98	0.01	-2.12	-0.43	0.04	-0.02
257	Primo Impalcato	10	0	-115.74	0.00	-0.36	-0.57	-0.10	-0.06
			188	-115.74	0.00	-1.42	-0.57	0.01	-0.06
			376	-115.74	0.00	-2.48	-0.57	0.12	-0.06
258	Primo Impalcato	11	0	-127.29	-0.03	-2.24	0.48	-0.17	-0.10
			188	-127.29	-0.03	-1.33	0.48	0.01	-0.10
			376	-127.29	-0.03	-0.42	0.48	0.19	-0.10
259	Primo Impalcato	12	0	-141.74	-0.10	-10.01	4.91	-0.17	-0.10
			188	-141.74	-0.10	-0.78	4.91	0.01	-0.10
			376	-141.74	-0.10	8.45	4.91	0.20	-0.10
260	Primo	13	0	-155.32	-0.08	-24.36	12.80	-0.01	-0.01

	Impalcato								
			188	-155.32	-0.08	-0.31	12.80	0.01	-0.01
			376	-155.32	-0.08	23.75	12.80	0.03	-0.01
261	Primo Impalcato	14	0	-244.29	5.65	8.66	-4.56	10.96	7.66
			188	-244.29	5.65	0.08	-4.56	-3.43	7.66
			376	-244.29	5.65	-8.49	-4.56	-17.82	7.66
262	Primo Impalcato	15	0	-311.83	-2.92	3.59	-1.82	55.07	79.71
			188	-311.83	-2.92	0.18	-1.82	-94.79	79.71
			376	-311.83	-2.92	-3.24	-1.82	-244.65	79.71
263	Primo Impalcato	16	0	-311.61	2.88	4.05	-2.07	-57.44	-80.06
			188	-311.61	2.88	0.17	-2.07	93.07	-80.06
			376	-311.61	2.88	-3.72	-2.07	243.58	-80.06
264	Primo Impalcato	17	0	-393.73	-0.62	2.01	-1.02	173.01	148.41
			188	-393.73	-0.62	0.09	-1.02	-106.01	148.41
			376	-393.73	-0.62	-1.84	-1.02	-385.02	148.41
265	Primo Impalcato	18	0	-397.12	0.68	2.55	-1.31	-171.86	-147.70
			188	-397.12	0.68	0.09	-1.31	105.83	-147.70
			376	-397.12	0.68	-2.37	-1.31	383.51	-147.70
266	Primo Impalcato	19	0	-434.46	0.07	0.52	-0.24	183.34	153.84
			188	-434.46	0.07	0.06	-0.24	-105.88	153.84
			376	-434.46	0.07	-0.40	-0.24	-395.11	153.84
267	Primo Impalcato	20	0	-436.37	-0.06	1.10	-0.56	-184.14	-154.13
			188	-436.37	-0.06	0.05	-0.56	105.63	-154.13
			376	-436.37	-0.06	-0.99	-0.56	395.40	-154.13
268	Primo Impalcato	21	0	-473.29	0.08	-0.30	0.20	174.21	148.07
			188	-473.29	0.08	0.07	0.20	-104.17	148.07
			376	-473.29	0.08	0.45	0.20	-382.55	148.07
269	Primo Impalcato	22	0	-481.19	-0.08	0.40	-0.17	-174.62	-148.21
			188	-481.19	-0.08	0.08	-0.17	104.01	-148.21
			376	-481.19	-0.08	-0.24	-0.17	382.64	-148.21
270	Primo Impalcato	23	0	-521.17	0.02	-1.03	0.59	170.38	145.65
			188	-521.17	0.02	0.08	0.59	-103.45	145.65
			376	-521.17	0.02	1.19	0.59	-377.28	145.65
271	Primo Impalcato	24	0	-519.72	0.00	-0.24	0.15	-170.81	-145.74
			188	-519.72	0.00	0.05	0.15	103.18	-145.74
			376	-519.72	0.00	0.34	0.15	377.18	-145.74
272	Primo Impalcato	25	0	-561.32	0.01	-0.90	0.50	170.77	147.05
			188	-561.32	0.01	0.04	0.50	-105.68	147.05
			376	-561.32	0.01	0.98	0.50	-382.12	147.05
273	Primo Impalcato	26	0	-543.49	0.00	0.08	-0.05	-171.36	-146.56
			188	-543.49	0.00	0.00	-0.05	104.18	-146.56
			376	-543.49	0.00	-0.09	-0.05	379.73	-146.56
274	Primo Impalcato	27	0	-515.71	0.02	0.43	-0.27	-171.23	-145.76
			188	-515.71	0.02	-0.07	-0.27	102.80	-145.76
			376	-515.71	0.02	-0.58	-0.27	376.83	-145.76
275	Primo Impalcato	28	0	-548.87	-0.02	0.24	-0.14	170.75	146.51
			188	-548.87	-0.02	-0.01	-0.14	-104.68	146.51
			376	-548.87	-0.02	-0.27	-0.14	-380.12	146.51
276	Primo Impalcato	29	0	-496.32	-0.01	0.45	-0.25	-171.69	-145.96
			188	-496.32	-0.01	-0.02	-0.25	102.72	-145.96
			376	-496.32	-0.01	-0.49	-0.25	377.13	-145.96
277	Primo Impalcato	30	0	-558.42	-0.01	0.22	-0.10	172.86	147.34
			188	-558.42	-0.01	0.03	-0.10	-104.13	147.34
			376	-558.42	-0.01	-0.17	-0.10	-381.13	147.34
278	Primo Impalcato	31	0	-487.97	0.00	0.17	-0.11	-171.67	-146.01

			188	-487.97	0.00	-0.03	-0.11	102.83	-146.01
			376	-487.97	0.00	-0.23	-0.11	377.33	-146.01
279	Primo Impalcato	32	0	-558.11	-0.01	-0.07	0.05	173.03	147.26
			188	-558.11	-0.01	0.02	0.05	-103.82	147.26
			376	-558.11	-0.01	0.10	0.05	-380.67	147.26
280	Primo Impalcato	33	0	-486.80	-0.02	0.19	-0.10	-171.62	-145.97
			188	-486.80	-0.02	-0.01	-0.10	102.80	-145.97
			376	-486.80	-0.02	-0.20	-0.10	377.22	-145.97
281	Primo Impalcato	34	0	-563.64	-0.01	-0.11	0.08	173.14	147.38
			188	-563.64	-0.01	0.03	0.08	-103.94	147.38
			376	-563.64	-0.01	0.18	0.08	-381.01	147.38
282	Primo Impalcato	35	0	-488.28	0.00	0.06	-0.05	-171.59	-145.89
			188	-488.28	0.00	-0.02	-0.05	102.69	-145.89
			376	-488.28	0.00	-0.11	-0.05	376.97	-145.89
283	Primo Impalcato	36	0	-572.00	-0.02	-0.07	0.05	173.29	147.35
			188	-572.00	-0.02	0.03	0.05	-103.73	147.35
			376	-572.00	-0.02	0.13	0.05	-380.75	147.35
284	Primo Impalcato	37	0	-485.96	-0.01	0.01	-0.01	-171.75	-145.85
			188	-485.96	-0.01	-0.01	-0.01	102.44	-145.85
			376	-485.96	-0.01	-0.04	-0.01	376.64	-145.85
285	Primo Impalcato	38	0	-576.32	-0.02	0.05	-0.01	173.89	147.32
			188	-576.32	-0.02	0.03	-0.01	-103.07	147.32
			376	-576.32	-0.02	0.00	-0.01	-380.03	147.32
286	Primo Impalcato	39	0	-505.51	0.01	0.04	0.02	-172.05	-145.88
			188	-505.51	0.01	0.07	0.02	102.20	-145.88
			376	-505.51	0.01	0.10	0.02	376.45	-145.88
287	Primo Impalcato	40	0	-572.98	-0.03	0.25	-0.12	174.79	147.01
			188	-572.98	-0.03	0.01	-0.12	-101.60	147.01
			376	-572.98	-0.03	-0.22	-0.12	-377.98	147.01
288	Primo Impalcato	41	0	-559.52	-0.01	-0.19	0.12	-173.37	-146.48
			188	-559.52	-0.01	0.04	0.12	102.02	-146.48
			376	-559.52	-0.01	0.26	0.12	377.40	-146.48
289	Primo Impalcato	42	0	-535.41	0.01	-0.08	0.00	174.14	145.25
			188	-535.41	0.01	-0.09	0.00	-98.92	145.25
			376	-535.41	0.01	-0.09	0.00	-371.99	145.25
290	Primo Impalcato	43	0	-521.88	0.02	-0.50	0.26	173.68	145.69
			188	-521.88	0.02	-0.02	0.26	-100.22	145.69
			376	-521.88	0.02	0.47	0.26	-374.12	145.69
291	Primo Impalcato	44	0	-554.92	-0.01	0.22	-0.14	-172.40	-146.65
			188	-554.92	-0.01	-0.04	-0.14	103.30	-146.65
			376	-554.92	-0.01	-0.29	-0.14	379.01	-146.65
292	Primo Impalcato	45	0	-523.00	0.02	-0.29	0.15	172.44	145.35
			188	-523.00	0.02	-0.01	0.15	-100.83	145.35
			376	-523.00	0.02	0.28	0.15	-374.09	145.35
293	Primo Impalcato	46	0	-520.13	0.01	0.67	-0.39	-171.18	-145.08
			188	-520.13	0.01	-0.07	-0.39	101.56	-145.08
			376	-520.13	0.01	-0.80	-0.39	374.31	-145.08
294	Primo Impalcato	47	0	-513.07	0.02	-0.31	0.16	171.89	145.94
			188	-513.07	0.02	-0.02	0.16	-102.48	145.94
			376	-513.07	0.02	0.27	0.16	-376.84	145.94
295	Primo Impalcato	48	0	-505.60	0.00	0.43	-0.24	-171.50	-145.54
			188	-505.60	0.00	-0.02	-0.24	102.11	-145.54
			376	-505.60	0.00	-0.48	-0.24	375.73	-145.54
296	Primo Impalcato	49	0	-494.20	-0.07	-0.79	0.39	174.63	148.11
			188	-494.20	-0.07	-0.06	0.39	-103.81	148.11

			376	-494.20	-0.07	0.68	0.39	-382.25	148.11
297	Primo Impalcato	50	0	-492.41	0.08	-0.14	0.07	-175.00	-148.09
			188	-492.41	0.08	0.00	0.07	103.41	-148.09
			376	-492.41	0.08	0.14	0.07	381.81	-148.09
298	Primo Impalcato	51	0	-448.14	-0.06	-1.39	0.71	183.47	153.78
			188	-448.14	-0.06	-0.06	0.71	-105.64	153.78
			376	-448.14	-0.06	1.26	0.71	-394.76	153.78
299	Primo Impalcato	52	0	-496.07	0.07	-1.06	0.55	-185.44	-154.58
			188	-496.07	0.07	-0.03	0.55	105.17	-154.58
			376	-496.07	0.07	1.00	0.55	395.77	-154.58
300	Primo Impalcato	53	0	-406.00	0.62	-2.67	1.37	173.41	148.64
			188	-406.00	0.62	-0.09	1.37	-106.04	148.64
			376	-406.00	0.62	2.49	1.37	-385.49	148.64
301	Primo Impalcato	54	0	-442.89	-0.64	-2.58	1.30	-174.89	-149.12
			188	-442.89	-0.64	-0.13	1.30	105.46	-149.12
			376	-442.89	-0.64	2.32	1.30	385.80	-149.12
302	Primo Impalcato	55	0	-312.04	2.92	-4.21	2.14	55.07	79.78
			188	-312.04	2.92	-0.19	2.14	-94.92	79.78
			376	-312.04	2.92	3.83	2.14	-244.90	79.78
303	Primo Impalcato	56	0	-326.45	-2.95	-3.91	1.97	-55.92	-79.49
			188	-326.45	-2.95	-0.20	1.97	93.52	-79.49
			376	-326.45	-2.95	3.51	1.97	242.96	-79.49
304	Primo Impalcato	57	0	-237.12	5.49	-8.67	4.58	-8.24	-6.67
			188	-237.12	5.49	-0.06	4.58	4.30	-6.67
			376	-237.12	5.49	8.54	4.58	16.84	-6.67
305	Primo Impalcato	58	0	-154.51	-0.08	24.08	-12.50	-0.02	-0.01
			188	-154.51	-0.08	0.58	-12.50	-0.01	-0.01
			376	-154.51	-0.08	-22.92	-12.50	0.00	-0.01
306	Primo Impalcato	59	0	-140.51	-0.10	9.87	-4.72	0.15	0.09
			188	-140.51	-0.10	0.99	-4.72	-0.01	0.09
			376	-140.51	-0.10	-7.88	-4.72	-0.18	0.09
307	Primo Impalcato	60	0	-126.94	-0.03	2.28	-0.44	0.16	0.09
			188	-126.94	-0.03	1.45	-0.44	-0.01	0.09
			376	-126.94	-0.03	0.61	-0.44	-0.18	0.09
308	Primo Impalcato	61	0	-115.93	0.00	0.45	0.58	0.09	0.05
			188	-115.93	0.00	1.54	0.58	-0.01	0.05
			376	-115.93	0.00	2.62	0.58	-0.10	0.05
309	Primo Impalcato	62	0	-113.85	0.01	0.59	0.45	0.01	0.01
			188	-113.85	0.01	1.43	0.45	0.00	0.01
			376	-113.85	0.01	2.28	0.45	-0.01	0.01
310	Primo Impalcato	63	0	-115.18	0.00	0.85	0.28	-0.02	-0.01
			188	-115.18	0.00	1.38	0.28	0.00	-0.01
			376	-115.18	0.00	1.91	0.28	0.02	-0.01
311	Primo Impalcato	64	0	-115.30	0.00	0.84	0.29	-0.01	0.00
			188	-115.30	0.00	1.38	0.29	0.00	0.00
			376	-115.30	0.00	1.93	0.29	0.01	0.00
312	Primo Impalcato	65	0	-114.20	-0.01	0.57	0.47	-0.04	-0.02
			188	-114.20	-0.01	1.45	0.47	0.00	-0.02
			376	-114.20	-0.01	2.33	0.47	0.03	-0.02
313	Primo Impalcato	66	0	-116.32	0.00	0.43	0.60	-0.11	-0.06
			188	-116.32	0.00	1.55	0.60	0.01	-0.06
			376	-116.32	0.00	2.67	0.60	0.12	-0.06
314	Primo Impalcato	67	0	-127.21	0.03	2.32	-0.45	-0.18	-0.10
			188	-127.21	0.03	1.47	-0.45	0.01	-0.10
			376	-127.21	0.03	0.62	-0.45	0.20	-0.10

315	Primo Impalcato	68	0	-140.87	0.11	10.32	-5.00	-0.18	-0.10
			188	-140.87	0.11	0.92	-5.00	0.01	-0.10
			376	-140.87	0.11	-8.47	-5.00	0.20	-0.10
316	Primo Impalcato	69	0	-153.88	0.09	25.31	-13.24	-0.02	-0.01
			188	-153.88	0.09	0.42	-13.24	0.01	-0.01
			376	-153.88	0.09	-24.48	-13.24	0.04	-0.01
317	Primo Impalcato	70	0	-242.87	-5.71	-8.43	4.39	10.26	7.29
			188	-242.87	-5.71	-0.19	4.39	-3.45	7.29
			376	-242.87	-5.71	8.06	4.39	-17.15	7.29
318	Fondazio ne	1, 71	0	-104.66	-0.09	0.00	0.00	0.07	1.29
			102	-104.66	-0.09	0.00	0.00	-1.25	1.29
			204	-104.66	-0.09	0.00	0.00	-2.57	1.29
319	Fondazio ne	1, 92	0	-17.14	-0.02	0.00	0.00	-0.48	-0.14
			103	-17.14	-0.02	0.00	0.00	-0.33	-0.14
			206	-17.14	-0.02	0.00	0.00	-0.19	-0.14
320	Primo Impalcato	92, 2	0	-45.21	-0.03	0.00	0.00	0.68	0.74
			103	-45.21	-0.03	0.00	0.00	-0.08	0.74
			206	-45.21	-0.03	0.00	0.00	-0.84	0.74
321	Fondazio ne	6, 89	0	-29.20	0.00	0.00	0.00	0.04	0.01
			100	-29.20	0.00	0.00	0.00	0.03	0.01
			200	-29.20	0.00	0.00	0.00	0.02	0.01
322	Primo Impalcato	89, 7	0	-27.73	0.00	0.00	0.00	0.04	0.00
			100	-27.73	0.00	0.00	0.00	0.04	0.00
			200	-27.73	0.00	0.00	0.00	0.04	0.00
323	Fondazio ne	9, 90	0	-25.33	0.00	0.00	0.00	0.06	0.01
			100	-25.33	0.00	0.00	0.00	0.05	0.01
			200	-25.33	0.00	0.00	0.00	0.04	0.01
324	Primo Impalcato	90, 10	0	-32.52	0.00	0.00	0.00	0.02	-0.02
			100	-32.52	0.00	0.00	0.00	0.04	-0.02
			200	-32.52	0.00	0.00	0.00	0.06	-0.02
325	Fondazio ne	13, 91	0	-45.58	0.03	0.00	0.00	-0.85	-0.76
			103	-45.58	0.03	0.00	0.00	-0.07	-0.76
			206	-45.58	0.03	0.00	0.00	0.72	-0.76
326	Primo Impalcato	88, 14	0	-112.89	0.09	0.00	0.00	-2.53	-1.26
			102	-112.89	0.09	0.00	0.00	-1.24	-1.26
			204	-112.89	0.09	0.00	0.00	0.05	-1.26
327	Primo Impalcato	91, 14	0	-16.92	0.02	0.00	0.00	-0.21	0.13
			103	-16.92	0.02	0.00	0.00	-0.34	0.13
			206	-16.92	0.02	0.00	0.00	-0.47	0.13
328	Primo Impalcato	71, 15	0	30.95	-0.15	0.00	0.00	1.67	1.74
			102	30.95	-0.15	0.00	0.00	-0.11	1.74
			204	30.95	-0.15	0.00	0.00	-1.89	1.74
329	Fondazio ne	16, 88	0	38.72	0.15	0.00	0.00	-1.89	-1.74
			102	38.72	0.15	0.00	0.00	-0.12	-1.74
			204	38.72	0.15	0.00	0.00	1.66	-1.74
330	Fondazio ne	17, 72	0	-85.59	0.07	0.00	0.00	-3.73	-1.38
			100	-85.59	0.07	0.00	0.00	-2.36	-1.38
			199	-85.59	0.07	0.00	0.00	-0.98	-1.38
331	Primo Impalcato	87, 18	0	-94.85	-0.07	0.00	0.00	-0.99	1.38
			100	-94.85	-0.07	0.00	0.00	-2.36	1.38
			199	-94.85	-0.07	0.00	0.00	-3.74	1.38
332	Primo Impalcato	72, 19	0	-47.15	-0.08	0.00	0.00	-0.84	1.45
			100	-47.15	-0.08	0.00	0.00	-2.28	1.45
			199	-47.15	-0.08	0.00	0.00	-3.72	1.45
333	Fondazio	20, 87	0	-38.81	0.09	0.00	0.00	-3.72	-1.46

	ne								
			100	-38.81	0.09	0.00	0.00	-2.27	-1.46
			199	-38.81	0.09	0.00	0.00	-0.81	-1.46
334	Fondazio ne	21, 73	0	-67.34	0.08	0.00	0.00	-3.52	-1.31
			100	-67.34	0.08	0.00	0.00	-2.22	-1.31
			199	-67.34	0.08	0.00	0.00	-0.92	-1.31
335	Primo Impalcato	86, 22	0	-79.90	-0.08	0.00	0.00	-0.92	1.31
			100	-79.90	-0.08	0.00	0.00	-2.23	1.31
			199	-79.90	-0.08	0.00	0.00	-3.53	1.31
336	Primo Impalcato	73, 23	0	-92.02	-0.07	0.00	0.00	-0.98	1.26
			100	-92.02	-0.07	0.00	0.00	-2.23	1.26
			199	-92.02	-0.07	0.00	0.00	-3.48	1.26
337	Fondazio ne	24, 86	0	-80.70	0.07	0.00	0.00	-3.47	-1.25
			100	-80.70	0.07	0.00	0.00	-2.22	-1.25
			199	-80.70	0.07	0.00	0.00	-0.97	-1.25
338	Fondazio ne	25, 74	0	-77.40	0.09	0.00	0.00	-3.31	-1.17
			103	-77.40	0.09	0.00	0.00	-2.10	-1.17
			206	-77.40	0.09	0.00	0.00	-0.89	-1.17
339	Primo Impalcato	85, 26	0	-91.31	-0.07	0.00	0.00	-0.94	1.30
			100	-91.31	-0.07	0.00	0.00	-2.23	1.30
			199	-91.31	-0.07	0.00	0.00	-3.53	1.30
340	Fondazio ne	27, 85	0	-78.63	0.08	0.00	0.00	-3.46	-1.26
			100	-78.63	0.08	0.00	0.00	-2.20	-1.26
			199	-78.63	0.08	0.00	0.00	-0.94	-1.26
341	Primo Impalcato	74, 28	0	-88.12	-0.09	0.00	0.00	-0.89	1.15
			103	-88.12	-0.09	0.00	0.00	-2.07	1.15
			206	-88.12	-0.09	0.00	0.00	-3.26	1.15
342	Primo Impalcato	84, 29	0	-84.64	-0.07	0.00	0.00	-0.93	1.28
			100	-84.64	-0.07	0.00	0.00	-2.21	1.28
			199	-84.64	-0.07	0.00	0.00	-3.48	1.28
343	Fondazio ne	31, 84	0	-73.30	0.07	0.00	0.00	-3.49	-1.28
			100	-73.30	0.07	0.00	0.00	-2.21	-1.28
			199	-73.30	0.07	0.00	0.00	-0.94	-1.28
344	Primo Impalcato	83, 33	0	-81.18	-0.07	0.00	0.00	-0.93	1.28
			100	-81.18	-0.07	0.00	0.00	-2.21	1.28
			199	-81.18	-0.07	0.00	0.00	-3.49	1.28
345	Fondazio ne	35, 83	0	-75.14	0.07	0.00	0.00	-3.48	-1.28
			100	-75.14	0.07	0.00	0.00	-2.21	-1.28
			199	-75.14	0.07	0.00	0.00	-0.94	-1.28
346	Primo Impalcato	82, 37	0	-79.72	-0.07	0.00	0.00	-0.93	1.28
			100	-79.72	-0.07	0.00	0.00	-2.21	1.28
			199	-79.72	-0.07	0.00	0.00	-3.48	1.28
347	Fondazio ne	39, 82	0	-79.00	0.07	0.00	0.00	-3.48	-1.28
			100	-79.00	0.07	0.00	0.00	-2.20	-1.28
			199	-79.00	0.07	0.00	0.00	-0.93	-1.28
348	Primo Impalcato	78, 43	0	-77.46	0.07	0.00	0.00	0.90	-1.28
			100	-77.46	0.07	0.00	0.00	2.18	-1.28
			199	-77.46	0.07	0.00	0.00	3.45	-1.28
349	Primo Impalcato	81, 44	0	-96.27	-0.07	0.00	0.00	-0.92	1.31
			100	-96.27	-0.07	0.00	0.00	-2.22	1.31
			199	-96.27	-0.07	0.00	0.00	-3.52	1.31
350	Fondazio ne	45, 78	0	-90.51	-0.07	0.00	0.00	3.47	1.28
			100	-90.51	-0.07	0.00	0.00	2.20	1.28
			199	-90.51	-0.07	0.00	0.00	0.92	1.28
351	Fondazio ne	46, 81	0	-75.73	0.07	0.00	0.00	-3.44	-1.25

			100	-75.73	0.07	0.00	0.00	-2.19	-1.25
			199	-75.73	0.07	0.00	0.00	-0.94	-1.25
352	Primo Impalcato	77, 47	0	-72.99	0.07	0.00	0.00	0.96	-1.25
			100	-72.99	0.07	0.00	0.00	2.21	-1.25
			199	-72.99	0.07	0.00	0.00	3.46	-1.25
353	Primo Impalcato	80, 48	0	-81.94	-0.07	0.00	0.00	-0.97	1.25
			100	-81.94	-0.07	0.00	0.00	-2.21	1.25
			199	-81.94	-0.07	0.00	0.00	-3.46	1.25
354	Fondazio ne	49, 77	0	-88.85	-0.07	0.00	0.00	3.53	1.31
			100	-88.85	-0.07	0.00	0.00	2.23	1.31
			199	-88.85	-0.07	0.00	0.00	0.92	1.31
355	Fondazio ne	50, 80	0	-77.68	0.08	0.00	0.00	-3.52	-1.31
			100	-77.68	0.08	0.00	0.00	-2.22	-1.31
			199	-77.68	0.08	0.00	0.00	-0.91	-1.31
356	Primo Impalcato	76, 51	0	-37.41	0.08	0.00	0.00	0.83	-1.44
			100	-37.41	0.08	0.00	0.00	2.27	-1.44
			199	-37.41	0.08	0.00	0.00	3.71	-1.44
357	Fondazio ne	53, 76	0	-99.70	-0.07	0.00	0.00	3.74	1.39
			100	-99.70	-0.07	0.00	0.00	2.36	1.39
			199	-99.70	-0.07	0.00	0.00	0.98	1.39
358	Primo Impalcato	75, 55	0	40.46	0.15	0.00	0.00	-1.67	-1.75
			102	40.46	0.15	0.00	0.00	0.11	-1.75
			204	40.46	0.15	0.00	0.00	1.89	-1.75
359	Fondazio ne	56, 79	0	34.33	-0.15	0.00	0.00	1.88	1.72
			102	34.33	-0.15	0.00	0.00	0.12	1.72
			204	34.33	-0.15	0.00	0.00	-1.64	1.72
360	Fondazio ne	57, 75	0	-113.96	0.09	0.00	0.00	-0.07	-1.30
			102	-113.96	0.09	0.00	0.00	1.25	-1.30
			204	-113.96	0.09	0.00	0.00	2.58	-1.30
361	Fondazio ne	57, 93	0	-15.90	0.02	0.00	0.00	0.45	0.12
			103	-15.90	0.02	0.00	0.00	0.32	0.12
			206	-15.90	0.02	0.00	0.00	0.20	0.12
362	Primo Impalcato	93, 58	0	-45.69	0.03	0.00	0.00	-0.70	-0.74
			103	-45.69	0.03	0.00	0.00	0.06	-0.74
			206	-45.69	0.03	0.00	0.00	0.83	-0.74
363	Fondazio ne	61, 95	0	-31.72	0.00	0.00	0.00	-0.06	-0.02
			100	-31.72	0.00	0.00	0.00	-0.04	-0.02
			200	-31.72	0.00	0.00	0.00	-0.02	-0.02
364	Primo Impalcato	95, 62	0	-26.68	0.00	0.00	0.00	-0.04	0.01
			100	-26.68	0.00	0.00	0.00	-0.05	0.01
			200	-26.68	0.00	0.00	0.00	-0.06	0.01
365	Primo Impalcato	96, 65	0	-25.59	0.00	0.00	0.00	0.05	-0.01
			100	-25.59	0.00	0.00	0.00	0.05	-0.01
			200	-25.59	0.00	0.00	0.00	0.06	-0.01
366	Fondazio ne	66, 96	0	-32.98	0.00	0.00	0.00	0.06	0.02
			100	-32.98	0.00	0.00	0.00	0.04	0.02
			200	-32.98	0.00	0.00	0.00	0.02	0.02
367	Fondazio ne	69, 94	0	-44.81	-0.03	0.00	0.00	0.88	0.78
			103	-44.81	-0.03	0.00	0.00	0.08	0.78
			206	-44.81	-0.03	0.00	0.00	-0.72	0.78
368	Primo Impalcato	79, 70	0	-110.58	-0.09	0.00	0.00	2.52	1.26
			102	-110.58	-0.09	0.00	0.00	1.24	1.26
			204	-110.58	-0.09	0.00	0.00	-0.05	1.26
369	Primo Impalcato	94, 70	0	-17.17	-0.02	0.00	0.00	0.20	-0.14
			103	-17.17	-0.02	0.00	0.00	0.35	-0.14

			206	-17.17	-0.02	0.00	0.00	0.49	-0.14
370	Primo Impalcato	1, 71	0	30.95	-0.06	0.00	0.00	0.56	-0.58
			102	30.95	-0.06	0.00	0.00	1.15	-0.58
			204	30.95	-0.06	0.00	0.00	1.75	-0.58
371	Primo Impalcato	1, 92	0	-45.21	-0.17	0.00	0.00	1.50	0.42
			103	-45.21	-0.17	0.00	0.00	1.06	0.42
			206	-45.21	-0.17	0.00	0.00	0.63	0.42
372	Primo Impalcato	92, 2	0	-17.14	0.04	0.00	0.00	-0.05	-0.46
			103	-17.14	0.04	0.00	0.00	0.43	-0.46
			206	-17.14	0.04	0.00	0.00	0.90	-0.46
373	Primo Impalcato	6, 89	0	-27.73	0.00	0.00	0.00	0.02	-0.01
			100	-27.73	0.00	0.00	0.00	0.03	-0.01
			200	-27.73	0.00	0.00	0.00	0.04	-0.01
374	Primo Impalcato	89, 7	0	-29.20	0.00	0.00	0.00	0.02	0.00
			100	-29.20	0.00	0.00	0.00	0.02	0.00
			200	-29.20	0.00	0.00	0.00	0.02	0.00
375	Primo Impalcato	9, 90	0	-32.52	0.00	0.00	0.00	0.00	-0.01
			100	-32.52	0.00	0.00	0.00	0.01	-0.01
			200	-32.52	0.00	0.00	0.00	0.02	-0.01
376	Primo Impalcato	90, 10	0	-25.33	0.00	0.00	0.00	0.04	0.02
			100	-25.33	0.00	0.00	0.00	0.02	0.02
			200	-25.33	0.00	0.00	0.00	0.01	0.02
377	Primo Impalcato	13, 91	0	-16.92	-0.04	0.00	0.00	0.91	0.48
			103	-16.92	-0.04	0.00	0.00	0.42	0.48
			206	-16.92	-0.04	0.00	0.00	-0.06	0.48
378	Primo Impalcato	88, 14	0	38.72	0.07	0.00	0.00	1.73	0.54
			102	38.72	0.07	0.00	0.00	1.18	0.54
			204	38.72	0.07	0.00	0.00	0.63	0.54
379	Primo Impalcato	91, 14	0	-45.58	0.18	0.00	0.00	0.66	-0.41
			103	-45.58	0.18	0.00	0.00	1.09	-0.41
			206	-45.58	0.18	0.00	0.00	1.51	-0.41
380	Primo Impalcato	71, 15	0	-104.66	-0.10	0.00	0.00	-2.69	-1.03
			102	-104.66	-0.10	0.00	0.00	-1.64	-1.03
			204	-104.66	-0.10	0.00	0.00	-0.59	-1.03
381	Primo Impalcato	16, 88	0	-112.89	0.10	0.00	0.00	-0.57	1.01
			102	-112.89	0.10	0.00	0.00	-1.60	1.01
			204	-112.89	0.10	0.00	0.00	-2.64	1.01
382	Primo Impalcato	17, 72	0	-47.15	-0.04	0.00	0.00	2.02	1.46
			100	-47.15	-0.04	0.00	0.00	0.57	1.46
			199	-47.15	-0.04	0.00	0.00	-0.89	1.46
383	Primo Impalcato	87, 18	0	-38.81	0.04	0.00	0.00	-0.87	-1.46
			100	-38.81	0.04	0.00	0.00	0.59	-1.46
			199	-38.81	0.04	0.00	0.00	2.05	-1.46
384	Primo Impalcato	72, 19	0	-85.59	0.00	0.00	0.00	-0.96	-1.37
			100	-85.59	0.00	0.00	0.00	0.40	-1.37
			199	-85.59	0.00	0.00	0.00	1.76	-1.37
385	Primo Impalcato	20, 87	0	-94.85	0.00	0.00	0.00	1.77	1.37
			100	-94.85	0.00	0.00	0.00	0.40	1.37
			199	-94.85	0.00	0.00	0.00	-0.97	1.37
386	Primo Impalcato	21, 73	0	-92.02	0.02	0.00	0.00	1.57	1.29
			100	-92.02	0.02	0.00	0.00	0.28	1.29
			199	-92.02	0.02	0.00	0.00	-1.01	1.29
387	Primo Impalcato	86, 22	0	-80.70	-0.02	0.00	0.00	-1.00	-1.29
			100	-80.70	-0.02	0.00	0.00	0.29	-1.29
			199	-80.70	-0.02	0.00	0.00	1.57	-1.29

388	Primo Impalcato	73, 23	0	-67.34	-0.01	0.00	0.00	-0.95	-1.27
			100	-67.34	-0.01	0.00	0.00	0.31	-1.27
			199	-67.34	-0.01	0.00	0.00	1.58	-1.27
389	Primo Impalcato	24, 86	0	-79.90	0.01	0.00	0.00	1.58	1.27
			100	-79.90	0.01	0.00	0.00	0.31	1.27
			199	-79.90	0.01	0.00	0.00	-0.96	1.27
390	Primo Impalcato	25, 74	0	-88.12	0.01	0.00	0.00	1.46	1.16
			103	-88.12	0.01	0.00	0.00	0.26	1.16
			206	-88.12	0.01	0.00	0.00	-0.93	1.16
391	Primo Impalcato	85, 26	0	-78.63	-0.01	0.00	0.00	-0.97	-1.28
			100	-78.63	-0.01	0.00	0.00	0.30	-1.28
			199	-78.63	-0.01	0.00	0.00	1.57	-1.28
392	Primo Impalcato	27, 85	0	-91.31	0.01	0.00	0.00	1.59	1.29
			100	-91.31	0.01	0.00	0.00	0.31	1.29
			199	-91.31	0.01	0.00	0.00	-0.97	1.29
393	Primo Impalcato	74, 28	0	-77.40	-0.01	0.00	0.00	-0.93	-1.17
			103	-77.40	-0.01	0.00	0.00	0.27	-1.17
			206	-77.40	-0.01	0.00	0.00	1.47	-1.17
394	Primo Impalcato	84, 29	0	-73.30	-0.01	0.00	0.00	-0.97	-1.28
			100	-73.30	-0.01	0.00	0.00	0.31	-1.28
			199	-73.30	-0.01	0.00	0.00	1.59	-1.28
395	Primo Impalcato	31, 84	0	-84.64	0.01	0.00	0.00	1.59	1.28
			100	-84.64	0.01	0.00	0.00	0.31	1.28
			199	-84.64	0.01	0.00	0.00	-0.96	1.28
396	Primo Impalcato	83, 33	0	-75.14	-0.01	0.00	0.00	-0.97	-1.28
			100	-75.14	-0.01	0.00	0.00	0.31	-1.28
			199	-75.14	-0.01	0.00	0.00	1.58	-1.28
397	Primo Impalcato	35, 83	0	-81.18	0.01	0.00	0.00	1.59	1.28
			100	-81.18	0.01	0.00	0.00	0.31	1.28
			199	-81.18	0.01	0.00	0.00	-0.96	1.28
398	Primo Impalcato	82, 37	0	-79.00	-0.01	0.00	0.00	-0.96	-1.28
			100	-79.00	-0.01	0.00	0.00	0.31	-1.28
			199	-79.00	-0.01	0.00	0.00	1.58	-1.28
399	Primo Impalcato	39, 82	0	-79.72	0.01	0.00	0.00	1.59	1.28
			100	-79.72	0.01	0.00	0.00	0.31	1.28
			199	-79.72	0.01	0.00	0.00	-0.96	1.28
400	Primo Impalcato	78, 43	0	-90.51	0.01	0.00	0.00	0.95	1.29
			100	-90.51	0.01	0.00	0.00	-0.33	1.29
			199	-90.51	0.01	0.00	0.00	-1.61	1.29
401	Primo Impalcato	81, 44	0	-75.73	-0.01	0.00	0.00	-0.97	-1.28
			100	-75.73	-0.01	0.00	0.00	0.30	-1.28
			199	-75.73	-0.01	0.00	0.00	1.57	-1.28
402	Primo Impalcato	45, 78	0	-77.46	-0.01	0.00	0.00	-1.60	-1.27
			100	-77.46	-0.01	0.00	0.00	-0.33	-1.27
			199	-77.46	-0.01	0.00	0.00	0.93	-1.27
403	Primo Impalcato	46, 81	0	-96.27	0.01	0.00	0.00	1.60	1.28
			100	-96.27	0.01	0.00	0.00	0.32	1.28
			199	-96.27	0.01	0.00	0.00	-0.96	1.28
404	Primo Impalcato	77, 47	0	-88.85	0.01	0.00	0.00	0.96	1.28
			100	-88.85	0.01	0.00	0.00	-0.31	1.28
			199	-88.85	0.01	0.00	0.00	-1.58	1.28
405	Primo Impalcato	80, 48	0	-77.68	-0.01	0.00	0.00	-0.95	-1.27
			100	-77.68	-0.01	0.00	0.00	0.32	-1.27
			199	-77.68	-0.01	0.00	0.00	1.59	-1.27
406	Primo	49, 77	0	-72.99	-0.02	0.00	0.00	-1.57	-1.28

	Impalcato								
			100	-72.99	-0.02	0.00	0.00	-0.29	-1.28
			199	-72.99	-0.02	0.00	0.00	0.99	-1.28
407	Primo Impalcato	50, 80	0	-81.94	0.02	0.00	0.00	1.57	1.29
			100	-81.94	0.02	0.00	0.00	0.29	1.29
			199	-81.94	0.02	0.00	0.00	-0.99	1.29
408	Primo Impalcato	76, 51	0	-99.70	0.00	0.00	0.00	0.96	1.37
			100	-99.70	0.00	0.00	0.00	-0.40	1.37
			199	-99.70	0.00	0.00	0.00	-1.76	1.37
409	Primo Impalcato	53, 76	0	-37.41	0.04	0.00	0.00	-2.03	-1.46
			100	-37.41	0.04	0.00	0.00	-0.57	-1.46
			199	-37.41	0.04	0.00	0.00	0.89	-1.46
410	Primo Impalcato	75, 55	0	-113.96	0.10	0.00	0.00	2.70	1.03
			102	-113.96	0.10	0.00	0.00	1.64	1.03
			204	-113.96	0.10	0.00	0.00	0.59	1.03
411	Primo Impalcato	56, 79	0	-110.58	-0.11	0.00	0.00	0.68	-0.95
			102	-110.58	-0.11	0.00	0.00	1.64	-0.95
			204	-110.58	-0.11	0.00	0.00	2.61	-0.95
412	Primo Impalcato	57, 75	0	40.46	0.06	0.00	0.00	-0.56	0.58
			102	40.46	0.06	0.00	0.00	-1.16	0.58
			204	40.46	0.06	0.00	0.00	-1.75	0.58
413	Primo Impalcato	57, 93	0	-45.69	0.17	0.00	0.00	-1.46	-0.40
			103	-45.69	0.17	0.00	0.00	-1.05	-0.40
			206	-45.69	0.17	0.00	0.00	-0.65	-0.40
414	Primo Impalcato	93, 58	0	-15.90	-0.04	0.00	0.00	0.06	0.47
			103	-15.90	-0.04	0.00	0.00	-0.42	0.47
			206	-15.90	-0.04	0.00	0.00	-0.91	0.47
415	Primo Impalcato	61, 95	0	-26.68	0.00	0.00	0.00	-0.01	0.02
			100	-26.68	0.00	0.00	0.00	-0.03	0.02
			200	-26.68	0.00	0.00	0.00	-0.05	0.02
416	Primo Impalcato	95, 62	0	-31.72	0.00	0.00	0.00	-0.02	-0.01
			100	-31.72	0.00	0.00	0.00	-0.01	-0.01
			200	-31.72	0.00	0.00	0.00	0.00	-0.01
417	Primo Impalcato	96, 65	0	-32.98	0.00	0.00	0.00	0.02	0.01
			100	-32.98	0.00	0.00	0.00	0.01	0.01
			200	-32.98	0.00	0.00	0.00	0.00	0.01
418	Primo Impalcato	66, 96	0	-25.59	0.00	0.00	0.00	0.01	-0.02
			100	-25.59	0.00	0.00	0.00	0.03	-0.02
			200	-25.59	0.00	0.00	0.00	0.05	-0.02
419	Primo Impalcato	69, 94	0	-17.17	0.04	0.00	0.00	-0.95	-0.49
			103	-17.17	0.04	0.00	0.00	-0.45	-0.49
			206	-17.17	0.04	0.00	0.00	0.05	-0.49
420	Primo Impalcato	79, 70	0	34.33	-0.07	0.00	0.00	-1.69	-0.49
			102	34.33	-0.07	0.00	0.00	-1.19	-0.49
			204	34.33	-0.07	0.00	0.00	-0.69	-0.49
421	Primo Impalcato	94, 70	0	-44.81	-0.18	0.00	0.00	-0.66	0.43
			103	-44.81	-0.18	0.00	0.00	-1.10	0.43
			206	-44.81	-0.18	0.00	0.00	-1.54	0.43
422	Copertura	1, 2	0	-3.39	-8.32	122.54	38.39	-19.13	-11.86
			83	-3.39	-8.32	122.67	-38.08	-9.27	-11.86
			166	-3.39	-8.32	59.24	-114.55	0.58	-11.86
423	Copertura	15, 1	0	-16.27	-117.08	324.02	-220.97	7.07	19.61
			80	-16.27	-117.08	148.35	-220.97	-8.52	19.61
			159	-16.27	-117.08	-27.32	-220.97	-24.10	19.61
424	Copertura	2, 3	0	-10.66	1.72	58.94	31.10	0.37	-2.65
			69	-10.66	1.72	58.50	-32.38	2.20	-2.65
			138	-10.66	1.72	14.26	-95.86	4.03	-2.65
425	Copertura	3, 4	0	-10.58	3.16	14.44	47.56	3.91	-0.11

			69	-10.58	3.16	25.36	-15.92	3.98	-0.11
			138	-10.58	3.16	-7.53	-79.40	4.05	-0.11
426	Copertura	4, 5	0	-10.52	1.72	-7.38	53.52	4.00	0.07
			69	-10.52	1.72	7.65	-9.96	3.95	0.07
			138	-10.52	1.72	-21.12	-73.44	3.91	0.07
427	Copertura	5, 6	0	-10.46	0.63	-20.98	47.63	3.89	-0.10
			69	-10.46	0.63	-10.02	-15.85	3.96	-0.10
			138	-10.46	0.63	-42.86	-79.33	4.03	-0.10
428	Copertura	6, 7	0	-0.70	0.17	-42.77	64.49	4.02	-0.10
			69	-0.70	0.17	-20.17	1.01	4.08	-0.10
			138	-0.70	0.17	-41.38	-62.47	4.15	-0.10
429	Copertura	7, 8	0	-8.58	-0.02	-41.34	71.67	4.15	0.03
			69	-8.58	-0.02	-13.79	8.19	4.14	0.03
			138	-8.58	-0.02	-30.04	-55.29	4.12	0.03
430	Copertura	8, 9	0	-8.59	-0.20	-30.05	54.98	4.12	0.15
			69	-8.59	-0.20	-14.02	-8.50	4.01	0.15
			138	-8.59	-0.20	-41.78	-71.98	3.91	0.15
431	Copertura	9, 10	0	-1.06	-0.65	-41.85	62.20	3.92	0.16
			69	-1.06	-0.65	-20.83	-1.28	3.81	0.16
			138	-1.06	-0.65	-43.62	-64.76	3.70	0.16
432	Copertura	10, 11	0	-11.47	-1.77	-43.74	83.69	3.74	-0.01
			69	-11.47	-1.77	-7.89	20.21	3.74	-0.01
			138	-11.47	-1.77	-15.85	-43.27	3.75	-0.01
433	Copertura	11, 12	0	-11.54	-3.19	-16.01	85.36	3.81	0.19
			69	-11.54	-3.19	20.99	21.88	3.67	0.19
			138	-11.54	-3.19	14.19	-41.60	3.54	0.19
434	Copertura	12, 13	0	-11.62	-1.64	14.01	100.18	3.67	2.81
			69	-11.62	-1.64	61.23	36.70	1.73	2.81
			138	-11.62	-1.64	64.66	-26.78	-0.21	2.81
435	Copertura	13, 14	0	-4.76	8.35	64.96	119.11	0.00	12.20
			83	-4.76	8.35	132.19	42.64	-10.14	12.20
			166	-4.76	8.35	135.85	-33.83	-20.28	12.20
436	Copertura	16, 14	0	-19.02	116.40	310.70	-213.66	-19.24	-34.52
			80	-19.02	116.40	140.84	-213.66	8.21	-34.52
			159	-19.02	116.40	-29.02	-213.66	35.65	-34.52
437	Copertura	15, 17	0	-18.15	-22.30	319.87	78.36	-3.87	-4.15
			66	-18.15	-22.30	371.59	78.36	-1.13	-4.15
			132	-18.15	-22.30	423.31	78.36	1.61	-4.15
438	Copertura	16, 18	0	-22.23	23.06	307.18	77.39	7.60	5.25
			66	-22.23	23.06	358.25	77.39	4.13	5.25
			132	-22.23	23.06	409.33	77.39	0.66	5.25
439	Copertura	17, 19	0	-19.42	-2.69	420.44	-42.72	2.28	1.27
			66	-19.42	-2.69	392.24	-42.72	1.45	1.27
			132	-19.42	-2.69	364.05	-42.72	0.61	1.27
440	Copertura	18, 20	0	-24.54	2.79	405.82	-43.56	-0.01	0.31
			66	-24.54	2.79	377.07	-43.56	-0.21	0.31
			132	-24.54	2.79	348.32	-43.56	-0.41	0.31
441	Copertura	19, 21	0	-20.09	0.68	362.48	-98.16	0.69	0.92
			66	-20.09	0.68	297.70	-98.16	0.09	0.92
			132	-20.09	0.68	232.91	-98.16	-0.52	0.92
442	Copertura	20, 22	0	-26.40	-0.74	346.08	-89.58	-0.42	-0.13
			66	-26.40	-0.74	286.96	-89.58	-0.33	-0.13
			132	-26.40	-0.74	227.84	-89.58	-0.25	-0.13
443	Copertura	21, 23	0	-20.35	0.42	232.32	-107.38	-0.46	0.17
			66	-20.35	0.42	161.45	-107.38	-0.57	0.17
			132	-20.35	0.42	90.58	-107.38	-0.69	0.17
444	Copertura	22, 24	0	-26.35	-0.45	227.56	-95.63	-0.03	0.38
			66	-26.35	-0.45	164.45	-95.63	-0.28	0.38
			132	-26.35	-0.45	101.33	-95.63	-0.53	0.38
445	Copertura	23, 25	0	-20.33	0.08	90.59	-84.81	-0.61	0.05
			66	-20.33	0.08	34.61	-84.81	-0.64	0.05
			132	-20.33	0.08	-21.36	-84.81	-0.67	0.05
446	Copertura	24, 26	0	-26.37	-0.07	101.47	-69.79	-0.40	0.38
			66	-26.37	-0.07	55.41	-69.79	-0.65	0.38
			132	-26.37	-0.07	9.35	-69.79	-0.90	0.38
447	Copertura	25, 28	0	-20.27	-0.10	-21.25	-18.79	-0.65	0.02
			85	-20.27	-0.10	-37.22	-18.79	-0.67	0.02
			170	-20.27	-0.10	-53.19	-18.79	-0.69	0.02
448	Copertura	26, 27	0	-22.98	0.13	12.79	-25.28	-0.85	0.01
			66	-22.98	0.13	-3.89	-25.28	-0.86	0.01
			132	-22.98	0.13	-20.58	-25.28	-0.87	0.01
449	Copertura	27, 29	0	-26.19	0.19	-15.97	2.49	-0.90	-0.26

			66	-26.19	0.19	-14.32	2.49	-0.73	-0.26
			132	-26.19	0.19	-12.68	2.49	-0.56	-0.26
450	Copertura	28, 30	0	-20.53	-0.18	-61.27	29.92	-0.68	-0.08
			73	-20.53	-0.18	-39.43	29.92	-0.62	-0.08
			146	-20.53	-0.18	-17.59	29.92	-0.57	-0.08
451	Copertura	29, 31	0	-26.23	0.08	-2.33	3.90	-0.58	-0.15
			66	-26.23	0.08	0.25	3.90	-0.48	-0.15
			132	-26.23	0.08	2.82	3.90	-0.38	-0.15
452	Copertura	30, 32	0	-20.86	-0.05	-28.62	26.16	-0.62	-0.22
			69	-20.86	-0.05	-10.70	26.16	-0.47	-0.22
			137	-20.86	-0.05	7.22	26.16	-0.32	-0.22
453	Copertura	31, 33	0	-27.69	0.07	12.98	-3.43	-0.46	-0.24
			66	-27.69	0.07	10.71	-3.43	-0.31	-0.24
			132	-27.69	0.07	8.44	-3.43	-0.15	-0.24
454	Copertura	32, 34	0	-21.13	-0.01	-4.75	14.08	-0.42	-0.21
			69	-21.13	-0.01	4.97	14.08	-0.27	-0.21
			138	-21.13	-0.01	14.68	14.08	-0.13	-0.21
455	Copertura	33, 35	0	-27.86	0.09	21.03	-10.98	-0.23	-0.24
			66	-27.86	0.09	13.79	-10.98	-0.07	-0.24
			132	-27.86	0.09	6.54	-10.98	0.09	-0.24
456	Copertura	34, 36	0	-21.39	-0.03	1.54	9.26	-0.24	-0.25
			69	-21.39	-0.03	7.93	9.26	-0.07	-0.25
			138	-21.39	-0.03	14.32	9.26	0.10	-0.25
457	Copertura	35, 37	0	-29.25	0.11	19.22	-19.64	-0.01	-0.39
			66	-29.25	0.11	6.26	-19.64	0.25	-0.39
			132	-29.25	0.11	-6.70	-19.64	0.51	-0.39
458	Copertura	36, 38	0	-21.64	-0.08	-0.01	12.75	-0.01	-0.32
			69	-21.64	-0.08	8.79	12.75	0.21	-0.32
			138	-21.64	-0.08	17.59	12.75	0.43	-0.32
459	Copertura	37, 39	0	-29.98	0.14	7.76	-21.08	0.45	-0.32
			66	-29.98	0.14	-6.15	-21.08	0.66	-0.32
			132	-29.98	0.14	-20.07	-21.08	0.87	-0.32
460	Copertura	38, 40	0	-21.89	-0.13	2.08	20.22	0.36	-0.33
			69	-21.89	-0.13	15.93	20.22	0.58	-0.33
			137	-21.89	-0.13	29.78	20.22	0.81	-0.33
461	Copertura	39, 41	0	-31.34	0.02	-5.31	-18.34	0.88	-0.05
			66	-31.34	0.02	-17.41	-18.34	0.92	-0.05
			132	-31.34	0.02	-29.51	-18.34	0.95	-0.05
462	Copertura	40, 42	0	-22.15	0.00	13.30	19.63	0.81	-0.29
			69	-22.15	0.00	26.84	19.63	1.01	-0.29
			138	-22.15	0.00	40.39	19.63	1.21	-0.29
463	Copertura	41, 44	0	-38.87	-0.35	-19.55	-11.15	1.04	0.31
			66	-38.87	-0.35	-26.91	-11.15	0.83	0.31
			132	-38.87	-0.35	-34.27	-11.15	0.63	0.31
464	Copertura	42, 43	0	-22.28	0.85	22.92	14.64	1.28	-0.07
			23	-22.28	0.85	26.29	14.64	1.30	-0.07
			46	-22.28	0.85	29.66	14.64	1.32	-0.07
465	Copertura	43, 45	0	-22.14	0.17	29.94	22.45	1.34	0.61
			66	-22.14	0.17	44.76	22.45	0.94	0.61
			132	-22.14	0.17	59.58	22.45	0.54	0.61
466	Copertura	44, 46	0	-32.07	-0.14	-27.53	34.53	0.74	0.14
			66	-32.07	-0.14	-4.74	34.53	0.64	0.14
			132	-32.07	-0.14	18.05	34.53	0.55	0.14
467	Copertura	45, 47	0	-21.99	0.03	59.92	51.05	0.64	0.59
			66	-21.99	0.03	93.62	51.05	0.24	0.59
			132	-21.99	0.03	127.31	51.05	-0.15	0.59
468	Copertura	46, 48	0	-31.67	-0.01	18.65	78.75	0.66	0.49
			66	-31.67	-0.01	70.63	78.75	0.34	0.49
			132	-31.67	-0.01	122.60	78.75	0.02	0.49
469	Copertura	47, 49	0	-21.73	-0.34	127.96	76.52	-0.02	0.51
			66	-21.73	-0.34	178.46	76.52	-0.36	0.51
			132	-21.73	-0.34	228.96	76.52	-0.69	0.51
470	Copertura	48, 50	0	-30.70	0.33	123.75	96.54	0.16	0.32
			66	-30.70	0.33	187.47	96.54	-0.06	0.32
			132	-30.70	0.33	251.18	96.54	-0.27	0.32
471	Copertura	49, 51	0	-21.20	-0.68	230.23	77.23	-0.51	-0.42
			66	-21.20	-0.68	281.20	77.23	-0.23	-0.42
			132	-21.20	-0.68	332.17	77.23	0.04	-0.42
472	Copertura	50, 52	0	-29.12	0.65	253.07	93.15	-0.27	0.48
			66	-29.12	0.65	314.55	93.15	-0.59	0.48
			132	-29.12	0.65	376.03	93.15	-0.91	0.48
473	Copertura	51, 53	0	-20.28	2.64	334.34	41.57	0.19	-1.01

			66	-20.28	2.64	361.77	41.57	0.86	-1.01
			132	-20.28	2.64	389.20	41.57	1.53	-1.01
474	Copertura	52, 54	0	-27.13	-2.80	379.04	27.30	-0.92	0.36
			66	-27.13	-2.80	397.06	27.30	-1.16	0.36
			132	-27.13	-2.80	415.08	27.30	-1.39	0.36
475	Copertura	53, 55	0	-18.82	22.07	392.58	-71.65	0.95	5.27
			66	-18.82	22.07	345.30	-71.65	-2.52	5.27
			132	-18.82	22.07	298.01	-71.65	-6.00	5.27
476	Copertura	54, 56	0	-23.23	-22.33	419.91	-84.81	0.91	-4.76
			66	-23.23	-22.33	363.94	-84.81	4.05	-4.76
			132	-23.23	-22.33	307.96	-84.81	7.19	-4.76
477	Copertura	55, 57	0	-16.79	117.33	302.47	-208.10	-8.90	-21.30
			80	-16.79	117.33	137.04	-208.10	8.03	-21.30
			159	-16.79	117.33	-28.40	-208.10	24.96	-21.30
478	Copertura	56, 70	0	-18.68	-117.08	314.03	-216.93	11.73	26.00
			80	-18.68	-117.08	141.57	-216.93	-8.94	26.00
			159	-18.68	-117.08	-30.89	-216.93	-29.61	26.00
479	Copertura	57, 58	0	-5.58	8.60	122.63	39.08	19.94	12.16
			83	-5.58	8.60	123.33	-37.39	9.84	12.16
			166	-5.58	8.60	60.47	-113.86	-0.27	12.16
480	Copertura	58, 59	0	-12.65	-1.61	60.15	29.09	-0.05	2.80
			69	-12.65	-1.61	58.32	-34.39	-1.99	2.80
			138	-12.65	-1.61	12.69	-97.87	-3.92	2.80
481	Copertura	59, 60	0	-12.58	-3.14	12.86	43.00	-3.79	0.22
			69	-12.58	-3.14	20.63	-20.48	-3.94	0.22
			138	-12.58	-3.14	-15.41	-83.96	-4.09	0.22
482	Copertura	60, 61	0	-12.52	-1.74	-15.27	44.39	-4.03	0.00
			69	-12.52	-1.74	-6.54	-19.09	-4.03	0.00
			138	-12.52	-1.74	-41.61	-82.57	-4.04	0.00
483	Copertura	61, 62	0	-2.27	-0.64	-41.51	65.81	-4.00	0.15
			69	-2.27	-0.64	-18.01	2.33	-4.10	0.15
			138	-2.27	-0.64	-38.30	-61.15	-4.20	0.15
484	Copertura	62, 63	0	-10.12	-0.18	-38.25	75.70	-4.20	0.12
			69	-10.12	-0.18	-7.91	12.22	-4.28	0.12
			138	-10.12	-0.18	-21.38	-51.26	-4.36	0.12
485	Copertura	63, 64	0	-10.11	0.01	-21.37	63.29	-4.36	-0.03
			69	-10.11	0.01	0.40	-0.19	-4.34	-0.03
			138	-10.11	0.01	-21.64	-63.67	-4.32	-0.03
486	Copertura	64, 65	0	-10.13	0.19	-21.67	51.01	-4.32	-0.17
			69	-10.13	0.19	-8.37	-12.47	-4.20	-0.17
			138	-10.13	0.19	-38.87	-75.95	-4.08	-0.17
487	Copertura	65, 66	0	-2.59	0.66	-38.95	60.31	-4.09	-0.20
			69	-2.59	0.66	-19.24	-3.17	-3.95	-0.20
			138	-2.59	0.66	-43.33	-66.65	-3.82	-0.20
488	Copertura	66, 67	0	-13.20	1.82	-43.45	83.18	-3.86	-0.04
			69	-13.20	1.82	-7.96	19.70	-3.83	-0.04
			138	-13.20	1.82	-16.27	-43.78	-3.81	-0.04
489	Copertura	67, 68	0	-13.27	3.29	-16.43	84.75	-3.87	-0.24
			69	-13.27	3.29	20.15	21.27	-3.71	-0.24
			138	-13.27	3.29	12.92	-42.21	-3.54	-0.24
490	Copertura	68, 69	0	-13.36	1.74	12.73	98.67	-3.67	-2.94
			69	-13.36	1.74	58.91	35.19	-1.65	-2.94
			138	-13.36	1.74	61.30	-28.29	0.38	-2.94
491	Copertura	69, 70	0	-6.56	-8.94	61.62	115.76	0.16	-12.75
			83	-6.56	-8.94	126.06	39.29	10.75	-12.75
			166	-6.56	-8.94	126.94	-37.18	21.35	-12.75
492	Copertura	1	0	-224.16	4.54	11.28	-4.78	-4.77	-2.27
			220	-224.16	4.54	0.75	-4.78	0.22	-2.27
			440	-224.16	4.54	-9.77	-4.78	5.21	-2.27
493	Copertura	2	0	-127.72	-0.11	12.89	-8.34	-0.22	-0.12
			220	-127.72	-0.11	-5.45	-8.34	0.04	-0.12
			440	-127.72	-0.11	-23.79	-8.34	0.29	-0.12
494	Copertura	3	0	-143.42	-0.13	1.44	-2.55	-0.18	-0.08
			220	-143.42	-0.13	-4.16	-2.55	0.00	-0.08
			440	-143.42	-0.13	-9.77	-2.55	0.17	-0.08
495	Copertura	4	0	-132.93	-0.06	-1.44	-0.17	-0.15	-0.06
			220	-132.93	-0.06	-1.82	-0.17	-0.01	-0.06
			440	-132.93	-0.06	-2.20	-0.17	0.13	-0.06
496	Copertura	5	0	-121.06	-0.02	-1.09	0.17	-0.13	-0.06
			220	-121.06	-0.02	-0.72	0.17	-0.01	-0.06
			440	-121.06	-0.02	-0.35	0.17	0.11	-0.06
497	Copertura	6	0	-112.83	-0.01	-0.45	-0.01	-0.09	-0.04

			220	-112.83	-0.01	-0.46	-0.01	-0.01	-0.04
			440	-112.83	-0.01	-0.47	-0.01	0.08	-0.04
498	Copertura	7	0	-108.97	0.00	-0.18	-0.12	-0.03	-0.02
			220	-108.97	0.00	-0.45	-0.12	0.00	-0.02
			440	-108.97	0.00	-0.72	-0.12	0.03	-0.02
499	Copertura	8	0	-110.27	0.00	-0.18	-0.12	0.02	0.01
			220	-110.27	0.00	-0.45	-0.12	0.00	0.01
			440	-110.27	0.00	-0.73	-0.12	-0.01	0.01
500	Copertura	9	0	-110.08	0.01	-0.46	0.00	0.07	0.03
			220	-110.08	0.01	-0.46	0.00	0.00	0.03
			440	-110.08	0.01	-0.47	0.00	-0.07	0.03
501	Copertura	10	0	-115.43	0.02	-1.07	0.15	0.12	0.05
			220	-115.43	0.02	-0.73	0.15	0.01	0.05
			440	-115.43	0.02	-0.40	0.15	-0.10	0.05
502	Copertura	11	0	-128.63	0.06	-1.42	-0.20	0.16	0.06
			220	-128.63	0.06	-1.85	-0.20	0.01	0.06
			440	-128.63	0.06	-2.29	-0.20	-0.13	0.06
503	Copertura	12	0	-141.78	0.13	1.55	-2.62	0.19	0.08
			220	-141.78	0.13	-4.22	-2.62	0.00	0.08
			440	-141.78	0.13	-9.99	-2.62	-0.18	0.08
504	Copertura	13	0	-129.08	0.11	13.14	-8.45	0.23	0.12
			220	-129.08	0.11	-5.46	-8.45	-0.03	0.12
			440	-129.08	0.11	-24.05	-8.45	-0.29	0.12
505	Copertura	57	0	-213.12	-4.57	-12.04	5.08	-4.59	-2.18
			220	-213.12	-4.57	-0.86	5.08	0.21	-2.18
			440	-213.12	-4.57	10.32	5.08	5.02	-2.18
506	Copertura	58	0	-125.59	0.11	-13.12	8.39	-0.22	-0.11
			220	-125.59	0.11	5.33	8.39	0.04	-0.11
			440	-125.59	0.11	23.78	8.39	0.29	-0.11
507	Copertura	59	0	-140.87	0.13	-1.53	2.59	-0.17	-0.07
			220	-140.87	0.13	4.16	2.59	0.00	-0.07
			440	-140.87	0.13	9.84	2.59	0.16	-0.07
508	Copertura	60	0	-128.35	0.06	1.40	0.21	-0.14	-0.06
			220	-128.35	0.06	1.86	0.21	-0.01	-0.06
			440	-128.35	0.06	2.33	0.21	0.11	-0.06
509	Copertura	61	0	-115.83	0.02	1.06	-0.13	-0.10	-0.04
			220	-115.83	0.02	0.77	-0.13	-0.01	-0.04
			440	-115.83	0.02	0.48	-0.13	0.09	-0.04
510	Copertura	62	0	-111.74	0.01	0.46	0.03	-0.05	-0.02
			220	-111.74	0.01	0.51	0.03	0.00	-0.02
			440	-111.74	0.01	0.57	0.03	0.06	-0.02
511	Copertura	63	0	-114.55	0.00	0.18	0.15	-0.01	-0.01
			220	-114.55	0.00	0.51	0.15	0.00	-0.01
			440	-114.55	0.00	0.83	0.15	0.02	-0.01
512	Copertura	64	0	-114.69	0.00	0.18	0.15	0.03	0.02
			220	-114.69	0.00	0.50	0.15	0.00	0.02
			440	-114.69	0.00	0.82	0.15	-0.04	0.02
513	Copertura	65	0	-112.10	-0.01	0.47	0.02	0.07	0.03
			220	-112.10	-0.01	0.51	0.02	0.00	0.03
			440	-112.10	-0.01	0.55	0.02	-0.08	0.03
514	Copertura	66	0	-116.15	-0.02	1.10	-0.15	0.12	0.05
			220	-116.15	-0.02	0.78	-0.15	0.01	0.05
			440	-116.15	-0.02	0.46	-0.15	-0.11	0.05
515	Copertura	67	0	-128.53	-0.06	1.48	0.20	0.16	0.07
			220	-128.53	-0.06	1.93	0.20	0.01	0.07
			440	-128.53	-0.06	2.37	0.20	-0.13	0.07
516	Copertura	68	0	-140.88	-0.13	-1.56	2.70	0.19	0.09
			220	-140.88	-0.13	4.37	2.70	0.00	0.09
			440	-140.88	-0.13	10.30	2.70	-0.18	0.09
517	Copertura	69	0	-127.47	-0.12	-13.63	8.79	0.23	0.12
			220	-127.47	-0.12	5.70	8.79	-0.03	0.12
			440	-127.47	-0.12	25.03	8.79	-0.30	0.12
518	Primo Impalcato	1, 74	0	-19.17	0.14	0.00	0.00	1.59	0.54
			118	-19.17	0.14	0.00	0.00	0.95	0.54
			235	-19.17	0.14	0.00	0.00	0.31	0.54
519	Copertura	74, 2	0	-37.63	-0.04	0.00	0.00	0.22	-0.31
			118	-37.63	-0.04	0.00	0.00	0.58	-0.31
			235	-37.63	-0.04	0.00	0.00	0.95	-0.31
520	Primo Impalcato	6, 71	0	-26.39	0.00	0.00	0.00	0.01	0.00
			115	-26.39	0.00	0.00	0.00	0.01	0.00

			231	-26.39	0.00	0.00	0.00	0.01	0.00
521	Copertura	71, 7	0	-32.48	0.00	0.00	0.00	0.01	0.00
			115	-32.48	0.00	0.00	0.00	0.02	0.00
			231	-32.48	0.00	0.00	0.00	0.02	0.00
522	Primo Impalcato	9, 72	0	-34.61	0.00	0.00	0.00	0.01	0.00
			115	-34.61	0.00	0.00	0.00	0.02	0.00
			231	-34.61	0.00	0.00	0.00	0.02	0.00
523	Copertura	72, 10	0	-25.25	0.00	0.00	0.00	0.01	0.01
			115	-25.25	0.00	0.00	0.00	0.00	0.01
			231	-25.25	0.00	0.00	0.00	-0.01	0.01
524	Copertura	73, 13	0	-38.20	0.04	0.00	0.00	-0.20	0.33
			118	-38.20	0.04	0.00	0.00	-0.58	0.33
			235	-38.20	0.04	0.00	0.00	-0.97	0.33
525	Primo Impalcato	14, 73	0	-17.97	-0.14	0.00	0.00	-1.58	-0.53
			118	-17.97	-0.14	0.00	0.00	-0.96	-0.53
			235	-17.97	-0.14	0.00	0.00	-0.34	-0.53
526	Primo Impalcato	57, 75	0	-18.56	-0.14	0.00	0.00	-1.61	-0.56
			118	-18.56	-0.14	0.00	0.00	-0.96	-0.56
			235	-18.56	-0.14	0.00	0.00	-0.30	-0.56
527	Copertura	75, 58	0	-36.41	0.04	0.00	0.00	-0.22	0.31
			118	-36.41	0.04	0.00	0.00	-0.58	0.31
			235	-36.41	0.04	0.00	0.00	-0.95	0.31
528	Copertura	77, 61	0	-26.32	0.00	0.00	0.00	0.01	0.01
			115	-26.32	0.00	0.00	0.00	0.00	0.01
			231	-26.32	0.00	0.00	0.00	-0.01	0.01
529	Primo Impalcato	62, 77	0	-34.11	0.00	0.00	0.00	0.02	0.00
			115	-34.11	0.00	0.00	0.00	0.02	0.00
			231	-34.11	0.00	0.00	0.00	0.02	0.00
530	Primo Impalcato	65, 78	0	-35.30	0.00	0.00	0.00	-0.02	0.00
			115	-35.30	0.00	0.00	0.00	-0.02	0.00
			231	-35.30	0.00	0.00	0.00	-0.02	0.00
531	Copertura	78, 66	0	-25.31	0.00	0.00	0.00	-0.01	-0.01
			115	-25.31	0.00	0.00	0.00	0.00	-0.01
			231	-25.31	0.00	0.00	0.00	0.01	-0.01
532	Primo Impalcato	69, 76	0	-38.39	-0.04	0.00	0.00	-0.99	-0.32
			118	-38.39	-0.04	0.00	0.00	-0.61	-0.32
			235	-38.39	-0.04	0.00	0.00	-0.23	-0.32
533	Copertura	76, 70	0	-17.72	0.14	0.00	0.00	-0.32	0.58
			118	-17.72	0.14	0.00	0.00	-1.00	0.58
			235	-17.72	0.14	0.00	0.00	-1.69	0.58
534	Copertura	1, 74	0	-37.63	0.02	0.00	0.00	-1.18	-0.56
			118	-37.63	0.02	0.00	0.00	-0.53	-0.56
			235	-37.63	0.02	0.00	0.00	0.12	-0.56
535	Copertura	74, 2	0	-19.17	0.03	0.00	0.00	0.34	0.30
			118	-19.17	0.03	0.00	0.00	-0.01	0.30
			235	-19.17	0.03	0.00	0.00	-0.36	0.30
536	Copertura	6, 71	0	-32.48	0.00	0.00	0.00	0.02	0.00
			115	-32.48	0.00	0.00	0.00	0.02	0.00
			231	-32.48	0.00	0.00	0.00	0.01	0.00
537	Copertura	71, 7	0	-26.39	0.00	0.00	0.00	0.01	0.00
			115	-26.39	0.00	0.00	0.00	0.01	0.00
			231	-26.39	0.00	0.00	0.00	0.01	0.00
538	Copertura	9, 72	0	-25.25	0.00	0.00	0.00	0.00	0.00
			115	-25.25	0.00	0.00	0.00	0.01	0.00
			231	-25.25	0.00	0.00	0.00	0.01	0.00
539	Copertura	72, 10	0	-34.61	0.00	0.00	0.00	0.02	-0.01
			115	-34.61	0.00	0.00	0.00	0.04	-0.01
			231	-34.61	0.00	0.00	0.00	0.06	-0.01
540	Copertura	73, 13	0	-17.97	-0.03	0.00	0.00	-0.37	-0.31
			118	-17.97	-0.03	0.00	0.00	0.00	-0.31
			235	-17.97	-0.03	0.00	0.00	0.37	-0.31
541	Copertura	14, 73	0	-38.20	-0.02	0.00	0.00	1.17	0.54
			118	-38.20	-0.02	0.00	0.00	0.54	0.54
			235	-38.20	-0.02	0.00	0.00	-0.10	0.54
542	Copertura	15, 125	0	492.15	-0.82	-53.11	-41.94	-1.89	-1.58
			75	492.15	-0.82	-101.67	-87.55	-0.70	-1.58
			150	492.15	-0.82	-184.43	-133.15	0.48	-1.58

543	Copertura	127, 16	0	504.66	2.26	-199.98	141.94	2.80	6.27
			75	504.66	2.26	-110.63	96.33	-1.90	6.27
			150	504.66	2.26	-55.48	50.72	-6.61	6.27
544	Copertura	17, 129	0	468.37	-0.24	20.56	-9.80	-0.38	-0.37
			75	468.37	-0.24	-4.09	-55.93	-0.10	-0.37
			150	468.37	-0.24	-63.34	-102.07	0.18	-0.37
545	Copertura	130, 18	0	468.69	0.28	-64.25	102.21	0.37	0.46
			75	468.69	0.28	-4.89	56.07	0.02	0.46
			150	468.69	0.28	19.86	9.94	-0.32	0.46
546	Copertura	19, 135	0	476.89	-0.06	37.12	-10.80	-0.09	0.00
			75	476.89	-0.06	11.72	-56.93	-0.09	0.00
			150	476.89	-0.06	-48.28	-103.06	-0.08	0.00
547	Copertura	134, 20	0	476.08	0.10	-47.19	102.50	0.22	0.11
			75	476.08	0.10	12.38	56.36	0.14	0.11
			150	476.08	0.10	37.35	10.23	0.06	0.11
548	Copertura	21, 136	0	479.77	-0.01	41.17	-16.73	-0.08	0.02
			75	479.77	-0.01	11.32	-62.86	-0.09	0.02
			150	479.77	-0.01	-53.12	-108.99	-0.11	0.02
549	Copertura	138, 22	0	479.53	0.00	-52.74	108.84	0.08	-0.07
			75	479.53	0.00	11.59	62.70	0.13	-0.07
			150	479.53	0.00	41.31	16.57	0.18	-0.07
550	Copertura	23, 141	0	480.28	0.00	41.95	-19.14	-0.08	-0.01
			75	480.28	0.00	10.30	-65.27	-0.08	-0.01
			150	480.28	0.00	-55.96	-111.41	-0.07	-0.01
551	Copertura	142, 24	0	480.33	-0.02	-55.88	111.48	0.05	-0.03
			75	480.33	-0.02	10.42	65.34	0.08	-0.03
			150	480.33	-0.02	42.13	19.21	0.10	-0.03
552	Copertura	25, 145	0	481.65	0.01	43.12	-20.64	-0.03	0.00
			75	481.65	0.01	10.34	-66.77	-0.03	0.00
			150	481.65	0.01	-57.03	-112.90	-0.03	0.00
553	Copertura	146, 26	0	480.45	-0.11	-56.10	111.90	-0.09	-0.09
			75	480.45	-0.11	10.52	65.76	-0.02	-0.09
			150	480.45	-0.11	42.54	19.63	0.05	-0.09
554	Copertura	150, 27	0	479.64	-0.22	-55.95	111.00	-0.17	-0.11
			75	479.64	-0.22	10.00	64.87	-0.09	-0.11
			150	479.64	-0.22	41.36	18.75	-0.01	-0.11
555	Copertura	28, 149	0	480.49	-0.34	41.57	-19.45	-0.03	-0.21
			75	480.49	-0.34	9.68	-65.58	0.12	-0.21
			150	480.49	-0.34	-56.80	-111.70	0.28	-0.21
556	Copertura	154, 29	0	478.48	-0.42	-55.53	109.40	-0.40	-0.27
			75	478.48	-0.42	9.23	63.28	-0.19	-0.27
			150	478.48	-0.42	39.40	17.17	0.01	-0.27
557	Copertura	30, 153	0	478.27	-0.45	39.08	-16.97	0.01	-0.27
			75	478.27	-0.45	9.06	-63.08	0.21	-0.27
			150	478.27	-0.45	-55.55	-109.20	0.41	-0.27
558	Copertura	158, 31	0	478.03	-0.43	-55.35	109.08	-0.42	-0.25
			75	478.03	-0.43	9.16	62.97	-0.24	-0.25
			150	478.03	-0.43	39.10	16.85	-0.05	-0.25
559	Copertura	32, 157	0	477.72	-0.48	38.62	-16.56	0.05	-0.28
			75	477.72	-0.48	8.90	-62.67	0.26	-0.28
			150	477.72	-0.48	-55.39	-108.78	0.47	-0.28
560	Copertura	162, 33	0	477.46	-0.52	-55.30	108.61	-0.52	-0.32
			75	477.46	-0.52	8.86	62.50	-0.28	-0.32
			150	477.46	-0.52	38.45	16.40	-0.04	-0.32
561	Copertura	34, 161	0	477.80	-0.53	38.45	-16.67	0.06	-0.31
			75	477.80	-0.53	8.66	-62.77	0.29	-0.31
			150	477.80	-0.53	-55.71	-108.88	0.52	-0.31
562	Copertura	166, 35	0	477.13	-0.53	-55.17	108.33	-0.52	-0.31
			75	477.13	-0.53	8.79	62.23	-0.29	-0.31
			150	477.13	-0.53	38.18	16.13	-0.05	-0.31
563	Copertura	36, 165	0	477.83	-0.58	38.25	-16.70	0.05	-0.34
			75	477.83	-0.58	8.44	-62.80	0.31	-0.34
			150	477.83	-0.58	-55.95	-108.90	0.56	-0.34
564	Copertura	170, 37	0	476.93	-0.60	-55.15	108.01	-0.55	-0.36
			75	476.93	-0.60	8.58	61.92	-0.28	-0.36
			150	476.93	-0.60	37.73	15.82	-0.01	-0.36
565	Copertura	38, 169	0	477.42	-0.63	37.87	-16.24	0.01	-0.38
			75	477.42	-0.63	8.40	-62.33	0.30	-0.38
			150	477.42	-0.63	-55.63	-108.43	0.58	-0.38
566	Copertura	175, 39	0	477.10	-0.61	-55.01	107.75	-0.51	-0.38
			75	477.10	-0.61	8.52	61.66	-0.22	-0.38
			150	477.10	-0.61	37.48	15.57	0.06	-0.38

567	Copertura	40, 173	0	476.50	-0.67	37.04	-15.09	-0.06	-0.42
			75	476.50	-0.67	8.44	-61.18	0.25	-0.42
			150	476.50	-0.67	-54.72	-107.27	0.56	-0.42
568	Copertura	178, 41	0	478.19	-0.48	-55.80	108.81	-0.29	-0.27
			75	478.19	-0.48	8.53	62.73	-0.09	-0.27
			150	478.19	-0.48	38.29	16.64	0.11	-0.27
569	Copertura	42, 177	0	475.44	-0.71	35.70	-14.31	-0.15	-0.43
			75	475.44	-0.71	7.69	-60.39	0.18	-0.43
			150	475.44	-0.71	-54.88	-106.47	0.50	-0.43
570	Copertura	43, 181	0	478.54	0.03	41.98	-17.18	-0.03	0.00
			75	478.54	0.03	11.80	-63.31	-0.03	0.00
			150	478.54	0.03	-52.98	-109.44	-0.03	0.00
571	Copertura	182, 44	0	480.23	-0.22	-54.44	110.83	-0.19	-0.20
			75	480.23	-0.22	11.38	64.69	-0.03	-0.20
			150	480.23	-0.22	42.60	18.56	0.12	-0.20
572	Copertura	45, 185	0	480.05	0.02	42.05	-18.33	-0.10	0.00
			75	480.05	0.02	11.01	-64.46	-0.10	0.00
			150	480.05	0.02	-54.63	-110.59	-0.10	0.00
573	Copertura	186, 46	0	480.43	-0.02	-54.82	110.92	0.06	-0.03
			75	480.43	-0.02	11.07	64.79	0.08	-0.03
			150	480.43	-0.02	42.36	18.66	0.10	-0.03
574	Copertura	47, 189	0	480.48	0.03	42.17	-18.92	-0.14	-0.01
			75	480.48	0.03	10.68	-65.06	-0.13	-0.01
			150	480.48	0.03	-55.41	-111.19	-0.13	-0.01
575	Copertura	190, 48	0	479.22	-0.04	-54.22	110.16	0.07	-0.04
			75	479.22	-0.04	11.11	64.03	0.10	-0.04
			150	479.22	-0.04	41.83	17.90	0.13	-0.04
576	Copertura	49, 193	0	480.55	0.04	41.57	-17.23	-0.17	-0.04
			75	480.55	0.04	11.35	-63.36	-0.14	-0.04
			150	480.55	0.04	-53.47	-109.49	-0.11	-0.04
577	Copertura	195, 50	0	478.77	-0.04	-51.56	108.12	0.07	0.01
			75	478.77	-0.04	12.23	61.98	0.06	0.01
			150	478.77	-0.04	41.42	15.85	0.05	0.01
578	Copertura	51, 197	0	477.91	0.08	37.76	-11.56	-0.14	-0.02
			75	477.91	0.08	11.79	-57.69	-0.12	-0.02
			150	477.91	0.08	-48.77	-103.82	-0.11	-0.02
579	Copertura	199, 52	0	475.16	-0.10	-46.44	101.55	-0.01	-0.01
			75	475.16	-0.10	12.42	55.42	0.00	-0.01
			150	475.16	-0.10	36.69	9.29	0.01	-0.01
580	Copertura	53, 201	0	467.80	0.28	20.99	-10.00	0.27	0.35
			75	467.80	0.28	-3.81	-56.13	0.01	0.35
			150	467.80	0.28	-63.20	-102.26	-0.26	0.35
581	Copertura	202, 54	0	468.32	-0.59	-64.07	102.57	-0.68	-1.32
			75	468.32	-0.59	-4.44	56.44	0.31	-1.32
			150	468.32	-0.59	20.59	10.31	1.30	-1.32
582	Copertura	55, 205	0	496.11	0.76	-53.31	-42.79	1.60	1.57
			75	496.11	0.76	-102.51	-88.40	0.43	1.57
			150	496.11	0.76	-185.92	-134.01	-0.75	1.57
583	Copertura	206, 56	0	501.50	-1.04	-192.02	138.04	-0.99	-2.42
			75	501.50	-1.04	-105.60	92.43	0.83	-2.42
			150	501.50	-1.04	-53.38	46.82	2.65	-2.42
584	Copertura	57, 75	0	-36.41	-0.02	0.00	0.00	1.22	0.57
			118	-36.41	-0.02	0.00	0.00	0.55	0.57
			235	-36.41	-0.02	0.00	0.00	-0.12	0.57
585	Copertura	75, 58	0	-18.56	-0.03	0.00	0.00	-0.34	-0.29
			118	-18.56	-0.03	0.00	0.00	0.01	-0.29
			235	-18.56	-0.03	0.00	0.00	0.36	-0.29
586	Copertura	77, 61	0	-34.11	0.00	0.00	0.00	0.02	-0.01
			115	-34.11	0.00	0.00	0.00	0.04	-0.01
			231	-34.11	0.00	0.00	0.00	0.06	-0.01
587	Copertura	62, 77	0	-26.32	0.00	0.00	0.00	0.00	0.00
			115	-26.32	0.00	0.00	0.00	0.01	0.00
			231	-26.32	0.00	0.00	0.00	0.01	0.00
588	Copertura	65, 78	0	-25.31	0.00	0.00	0.00	0.00	0.00
			115	-25.31	0.00	0.00	0.00	-0.01	0.00
			231	-25.31	0.00	0.00	0.00	-0.01	0.00
589	Copertura	78, 66	0	-35.30	0.00	0.00	0.00	-0.02	0.01
			115	-35.30	0.00	0.00	0.00	-0.04	0.01
			231	-35.30	0.00	0.00	0.00	-0.06	0.01
590	Copertura	69, 76	0	-17.72	0.03	0.00	0.00	0.37	0.31
			118	-17.72	0.03	0.00	0.00	0.01	0.31
			235	-17.72	0.03	0.00	0.00	-0.36	0.31

591	Copertura	76, 70	0	-38.39	0.02	0.00	0.00	-0.13	-0.59
			118	-38.39	0.02	0.00	0.00	0.57	-0.59
			235	-38.39	0.02	0.00	0.00	1.27	-0.59
592	Copertura	79, 81	0	1.55	0.55	-6.15	7.69	17.98	20.97
			80	1.55	0.55	-0.03	7.69	1.31	20.97
			159	1.55	0.55	6.08	7.69	-15.36	20.97
593	Copertura	80, 82	0	-0.48	0.06	-3.65	5.23	-5.43	-1.21
			66	-0.48	0.06	-0.19	5.23	-4.63	-1.21
			132	-0.48	0.06	3.26	5.23	-3.83	-1.21
594	Copertura	83, 84	0	-1.41	-0.01	-0.87	1.17	-0.28	-0.32
			66	-1.41	-0.01	-0.09	1.17	-0.07	-0.32
			132	-1.41	-0.01	0.68	1.17	0.15	-0.32
595	Copertura	85, 86	0	-3.73	0.00	-0.28	0.62	0.03	0.02
			66	-3.73	0.00	0.13	0.62	0.01	0.02
			132	-3.73	0.00	0.54	0.62	-0.01	0.02
596	Copertura	87, 88	0	-6.40	0.00	-1.89	3.23	-0.04	0.00
			66	-6.40	0.00	0.24	3.23	-0.04	0.00
			132	-6.40	0.00	2.37	3.23	-0.03	0.00
597	Copertura	89, 90	0	-2.98	0.00	-3.40	5.27	-0.03	-0.01
			66	-2.98	0.00	0.08	5.27	-0.02	-0.01
			132	-2.98	0.00	3.56	5.27	-0.01	-0.01
598	Copertura	91, 92	0	-2.07	0.00	-3.94	6.04	-0.02	-0.01
			66	-2.07	0.00	0.05	6.04	-0.01	-0.01
			132	-2.07	0.00	4.04	6.04	0.00	-0.01
599	Copertura	93, 94	0	5.29	0.00	-3.41	4.71	-0.02	0.00
			66	5.29	0.00	-0.30	4.71	-0.02	0.00
			132	5.29	0.00	2.81	4.71	-0.02	0.00
600	Copertura	95, 96	0	8.16	0.00	-1.68	2.12	0.03	-0.01
			66	8.16	0.00	-0.29	2.12	0.03	-0.01
			132	8.16	0.00	1.11	2.12	0.03	-0.01
601	Copertura	97, 106	0	0.12	0.00	0.46	-0.78	0.12	0.01
			66	0.12	0.00	-0.05	-0.78	0.12	0.01
			132	0.12	0.00	-0.57	-0.78	0.11	0.01
602	Copertura	98, 99	0	-0.83	0.03	-2.82	3.94	-1.14	-0.55
			66	-0.83	0.03	-0.22	3.94	-0.78	-0.55
			132	-0.83	0.03	2.38	3.94	-0.42	-0.55
603	Copertura	100, 101	0	-0.84	-0.01	-0.11	-0.03	0.03	-0.02
			66	-0.84	-0.01	-0.13	-0.03	0.05	-0.02
			132	-0.84	-0.01	-0.15	-0.03	0.06	-0.02
604	Copertura	102, 103	0	-5.99	0.00	0.30	-0.22	-0.01	-0.01
			66	-5.99	0.00	0.15	-0.22	0.00	-0.01
			132	-5.99	0.00	0.00	-0.22	0.01	-0.01
605	Copertura	104, 105	0	-1.87	0.00	-0.68	0.91	-0.06	-0.07
			66	-1.87	0.00	-0.08	0.91	-0.01	-0.07
			132	-1.87	0.00	0.52	0.91	0.04	-0.07
606	Copertura	107, 108	0	-1.94	-0.01	2.44	-3.96	-0.68	0.94
			66	-1.94	-0.01	-0.17	-3.96	-1.30	0.94
			132	-1.94	-0.01	-2.78	-3.96	-1.92	0.94
607	Copertura	109, 110	0	2.24	0.48	4.54	-5.70	-10.53	-16.42
			80	2.24	0.48	0.00	-5.70	2.52	-16.42
			159	2.24	0.48	-4.53	-5.70	15.58	-16.42
608	Copertura	111, 112	0	-1.54	0.06	-0.84	1.13	-0.06	-0.08
			66	-1.54	0.06	-0.10	1.13	0.00	-0.08
			132	-1.54	0.06	0.64	1.13	0.05	-0.08
609	Copertura	113, 114	0	-0.29	0.00	-0.72	1.19	-0.05	-0.09
			66	-0.29	0.00	0.07	1.19	0.01	-0.09
			132	-0.29	0.00	0.86	1.19	0.07	-0.09
610	Copertura	115, 116	0	12.73	0.00	-0.51	0.18	-0.06	-0.08
			66	12.73	0.00	-0.39	0.18	-0.01	-0.08
			132	12.73	0.00	-0.27	0.18	0.05	-0.08
611	Copertura	117, 118	0	0.82	0.00	0.67	-0.93	0.00	-0.02
			66	0.82	0.00	0.06	-0.93	0.02	-0.02
			132	0.82	0.00	-0.56	-0.93	0.03	-0.02
612	Copertura	119, 120	0	-0.60	0.02	1.92	-3.16	0.12	0.30
			66	-0.60	0.02	-0.16	-3.16	-0.08	0.30
			132	-0.60	0.02	-2.25	-3.16	-0.27	0.30
613	Copertura	121, 122	0	-0.29	-0.31	5.52	-8.65	-3.19	-1.28
			66	-0.29	-0.31	-0.18	-8.65	-2.34	-1.28
			132	-0.29	-0.31	-5.89	-8.65	-1.49	-1.28
614	Copertura	124, 125	0	-886.09	0.11	-45.45	30.56	2.14	1.54
			99	-886.09	0.11	-15.12	30.56	0.62	1.54
			198	-886.09	0.11	15.22	30.56	-0.91	1.54

615	Copertura	125, 127	0	-157.45	-0.14	-169.21	470.27	-0.14	-0.04
			775	-157.45	-0.14	1649.15	-1.01	0.18	-0.04
			1550	-157.45	-0.14	-184.94	-472.30	0.51	-0.04
616	Copertura	126, 127	0	-902.63	-0.31	-45.58	30.54	-9.22	-6.31
			99	-902.63	-0.31	-15.27	30.54	-2.96	-6.31
			198	-902.63	-0.31	15.04	30.54	3.31	-6.31
617	Copertura	128, 129	0	-846.32	0.04	-46.70	32.32	0.40	0.36
			99	-846.32	0.04	-14.62	32.32	0.04	0.36
			198	-846.32	0.04	17.45	32.32	-0.31	0.36
618	Copertura	129, 130	0	-150.02	0.00	-45.89	476.64	-0.03	-0.01
			775	-150.02	0.00	1800.86	-0.06	0.04	-0.01
			1550	-150.02	0.00	-46.81	-476.76	0.11	-0.01
619	Copertura	131, 130	0	-846.74	-0.05	-46.69	32.30	-0.55	-0.47
			99	-846.74	-0.05	-14.63	32.30	-0.09	-0.47
			198	-846.74	-0.05	17.43	32.30	0.38	-0.47
620	Copertura	132, 135	0	-847.45	0.01	-47.17	32.84	-0.10	-0.01
			99	-847.45	0.01	-14.58	32.84	-0.09	-0.01
			198	-847.45	0.01	18.01	32.84	-0.07	-0.01
621	Copertura	133, 134	0	-846.37	-0.02	-47.14	32.83	-0.10	-0.12
			99	-846.37	-0.02	-14.55	32.83	0.02	-0.12
			198	-846.37	-0.02	18.03	32.83	0.14	-0.12
622	Copertura	135, 134	0	-142.01	0.00	-30.27	476.77	-0.13	-0.02
			775	-142.01	0.00	1817.50	0.07	0.00	-0.02
			1550	-142.01	0.00	-29.16	-476.63	0.12	-0.02
623	Copertura	137, 136	0	-856.16	0.00	-47.47	33.07	-0.08	-0.03
			99	-856.16	0.00	-14.65	33.07	-0.05	-0.03
			198	-856.16	0.00	18.17	33.07	-0.02	-0.03
624	Copertura	136, 138	0	-145.56	0.00	-34.95	476.73	-0.12	-0.01
			775	-145.56	0.00	1812.46	0.03	-0.01	-0.01
			1550	-145.56	0.00	-34.56	-476.68	0.10	-0.01
625	Copertura	139, 138	0	-855.84	0.00	-47.46	33.07	0.09	0.05
			99	-855.84	0.00	-14.64	33.07	0.04	0.05
			198	-855.84	0.00	18.18	33.07	-0.02	0.05
626	Copertura	140, 141	0	-859.73	0.00	-47.56	33.15	-0.01	0.00
			99	-859.73	0.00	-14.66	33.15	-0.01	0.00
			198	-859.73	0.00	18.24	33.15	0.00	0.00
627	Copertura	141, 142	0	-147.69	0.00	-37.72	476.71	-0.07	-0.01
			775	-147.69	0.00	1809.54	0.01	0.00	-0.01
			1550	-147.69	0.00	-37.63	-476.70	0.07	-0.01
628	Copertura	143, 142	0	-859.80	0.00	-47.57	33.16	0.02	0.02
			99	-859.80	0.00	-14.66	33.16	0.00	0.02
			198	-859.80	0.00	18.26	33.16	-0.03	0.02
629	Copertura	144, 145	0	-861.97	0.00	-47.63	33.25	-0.01	0.00
			99	-861.97	0.00	-14.64	33.25	0.00	0.00
			198	-861.97	0.00	18.36	33.25	0.00	0.00
630	Copertura	145, 146	0	-147.96	0.01	-38.67	476.76	-0.03	0.00
			775	-147.96	0.01	1808.98	0.06	0.00	0.00
			1550	-147.96	0.01	-37.80	-476.64	0.03	0.00
631	Copertura	147, 146	0	-860.34	0.01	-47.58	33.19	0.01	0.09
			99	-860.34	0.01	-14.64	33.19	-0.08	0.09
			198	-860.34	0.01	18.30	33.19	-0.17	0.09
632	Copertura	148, 149	0	-860.20	0.03	-47.61	33.22	0.05	0.21
			99	-860.20	0.03	-14.65	33.22	-0.16	0.21
			198	-860.20	0.03	18.32	33.22	-0.37	0.21
633	Copertura	149, 150	0	-147.80	-0.08	-38.48	476.77	0.02	0.00
			775	-147.80	-0.08	1809.67	0.05	0.00	0.00
			1550	-147.80	-0.08	-37.69	-476.67	-0.03	0.00
634	Copertura	151, 150	0	-859.03	0.01	-47.56	33.16	0.02	0.11
			99	-859.03	0.01	-14.65	33.16	-0.09	0.11
			198	-859.03	0.01	18.26	33.16	-0.20	0.11
635	Copertura	152, 153	0	-856.46	0.04	-47.53	33.11	0.05	0.28
			99	-856.46	0.04	-14.67	33.11	-0.22	0.28
			198	-856.46	0.04	18.19	33.11	-0.50	0.28
636	Copertura	153, 154	0	-147.26	-0.09	-37.36	476.74	0.06	0.01
			775	-147.26	-0.09	1810.88	0.00	0.00	0.01
			1551	-147.26	-0.09	-37.33	-476.73	-0.06	0.01
637	Copertura	155, 154	0	-856.74	0.03	-47.54	33.12	0.09	0.28
			99	-856.74	0.03	-14.67	33.12	-0.19	0.28
			198	-856.74	0.03	18.20	33.12	-0.47	0.28
638	Copertura	156, 157	0	-855.85	0.04	-47.53	33.10	0.05	0.29
			99	-855.85	0.04	-14.68	33.10	-0.24	0.29
			198	-855.85	0.04	18.17	33.10	-0.53	0.29

639	Copertura	157, 158	0	-147.36	-0.11	-37.22	476.75	0.09	0.01
			775	-147.36	-0.11	1811.24	0.00	0.00	0.01
			1551	-147.36	-0.11	-37.17	-476.74	-0.10	0.01
640	Copertura	159, 158	0	-856.27	0.03	-47.54	33.11	0.07	0.26
			99	-856.27	0.03	-14.68	33.11	-0.19	0.26
			198	-856.27	0.03	18.18	33.11	-0.45	0.26
641	Copertura	160, 161	0	-856.00	0.04	-47.56	33.13	0.06	0.32
			99	-856.00	0.04	-14.68	33.13	-0.26	0.32
			198	-856.00	0.04	18.20	33.13	-0.58	0.32
642	Copertura	161, 162	0	-147.38	-0.12	-37.51	476.78	0.11	0.01
			776	-147.38	-0.12	1811.39	0.03	0.00	0.01
			1551	-147.38	-0.12	-37.12	-476.73	-0.12	0.01
643	Copertura	163, 162	0	-855.54	0.04	-47.53	33.11	0.10	0.33
			99	-855.54	0.04	-14.67	33.11	-0.23	0.33
			198	-855.54	0.04	18.19	33.11	-0.57	0.33
644	Copertura	164, 165	0	-856.05	0.05	-47.59	33.16	0.07	0.36
			99	-856.05	0.05	-14.68	33.16	-0.28	0.36
			198	-856.05	0.05	18.23	33.16	-0.63	0.36
645	Copertura	165, 166	0	-147.36	-0.13	-37.72	476.81	0.11	0.02
			776	-147.36	-0.13	1811.65	0.05	0.00	0.02
			1551	-147.36	-0.13	-36.98	-476.72	-0.12	0.02
646	Copertura	167, 166	0	-855.09	0.04	-47.53	33.11	0.09	0.33
			99	-855.09	0.04	-14.67	33.11	-0.24	0.33
			198	-855.09	0.04	18.19	33.11	-0.56	0.33
647	Copertura	168, 169	0	-855.31	0.05	-47.59	33.17	0.09	0.39
			99	-855.31	0.05	-14.67	33.17	-0.30	0.39
			198	-855.31	0.05	18.25	33.17	-0.69	0.39
648	Copertura	169, 170	0	-147.21	-0.14	-37.39	476.81	0.09	0.01
			776	-147.21	-0.14	1812.16	0.03	0.00	0.01
			1552	-147.21	-0.14	-36.94	-476.75	-0.10	0.01
649	Copertura	171, 170	0	-854.63	0.04	-47.54	33.13	0.10	0.38
			99	-854.63	0.04	-14.67	33.13	-0.27	0.38
			198	-854.63	0.04	18.21	33.13	-0.65	0.38
650	Copertura	172, 173	0	-853.51	0.05	-47.55	33.14	0.10	0.42
			99	-853.51	0.05	-14.66	33.14	-0.32	0.42
			198	-853.51	0.05	18.23	33.14	-0.74	0.42
651	Copertura	173, 175	0	-146.79	-0.15	-36.50	476.77	0.04	0.01
			776	-146.79	-0.15	1812.97	-0.02	0.00	0.01
			1552	-146.79	-0.15	-36.78	-476.81	-0.04	0.01
652	Copertura	174, 175	0	-854.31	0.04	-47.56	33.14	0.11	0.39
			99	-854.31	0.04	-14.66	33.14	-0.27	0.39
			198	-854.31	0.04	18.23	33.14	-0.66	0.39
653	Copertura	176, 177	0	-852.30	0.05	-47.51	33.10	0.09	0.43
			99	-852.30	0.05	-14.66	33.10	-0.34	0.43
			198	-852.30	0.05	18.20	33.10	-0.76	0.43
654	Copertura	177, 178	0	-146.95	-0.17	-36.68	476.74	-0.04	0.00
			776	-146.95	-0.17	1812.86	-0.06	-0.01	0.00
			1552	-146.95	-0.17	-37.57	-476.86	0.02	0.00
655	Copertura	179, 178	0	-855.99	0.03	-47.57	33.15	0.10	0.27
			99	-855.99	0.03	-14.67	33.15	-0.17	0.27
			198	-855.99	0.03	18.23	33.15	-0.44	0.27
656	Copertura	180, 181	0	-856.65	0.00	-47.48	33.10	-0.01	-0.01
			99	-856.65	0.00	-14.63	33.10	0.00	-0.01
			198	-856.65	0.00	18.22	33.10	0.01	-0.01
657	Copertura	181, 182	0	-147.14	0.02	-34.77	476.61	-0.03	-0.01
			775	-147.14	0.02	1811.76	-0.09	0.01	-0.01
			1550	-147.14	0.02	-36.13	-476.79	0.05	-0.01
658	Copertura	183, 182	0	-858.94	0.02	-47.54	33.17	0.05	0.20
			99	-858.94	0.02	-14.62	33.17	-0.14	0.20
			198	-858.94	0.02	18.31	33.17	-0.33	0.20
659	Copertura	184, 185	0	-858.47	0.00	-47.52	33.14	0.00	-0.01
			99	-858.47	0.00	-14.63	33.14	0.01	-0.01
			198	-858.47	0.00	18.26	33.14	0.01	-0.01
660	Copertura	185, 186	0	-146.98	0.01	-36.37	476.69	-0.09	-0.01
			775	-146.98	0.01	1810.76	-0.01	0.00	-0.01
			1550	-146.98	0.01	-36.53	-476.71	0.09	-0.01
661	Copertura	187, 186	0	-858.99	0.00	-47.52	33.15	-0.01	0.01
			99	-858.99	0.00	-14.62	33.15	-0.02	0.01
			198	-858.99	0.00	18.29	33.15	-0.04	0.01
662	Copertura	188, 189	0	-859.48	-0.01	-47.57	33.16	0.01	-0.01
			99	-859.48	-0.01	-14.65	33.16	0.02	-0.01
			198	-859.48	-0.01	18.26	33.16	0.03	-0.01

663	Copertura	189, 190	0	-147.30	0.01	-37.15	476.78	-0.11	-0.01
			775	-147.30	0.01	1810.64	0.07	0.00	-0.01
			1550	-147.30	0.01	-35.99	-476.63	0.12	-0.01
664	Copertura	191, 190	0	-857.76	0.01	-47.49	33.11	-0.01	0.03
			99	-857.76	0.01	-14.63	33.11	-0.04	0.03
			198	-857.76	0.01	18.23	33.11	-0.07	0.03
665	Copertura	192, 193	0	-857.03	-0.01	-47.51	33.11	0.09	0.03
			99	-857.03	-0.01	-14.65	33.11	0.07	0.03
			198	-857.03	-0.01	18.21	33.11	0.04	0.03
666	Copertura	193, 195	0	-145.41	0.01	-35.26	476.82	-0.08	-0.01
			775	-145.41	0.01	1812.90	0.12	0.01	-0.01
			1550	-145.41	0.01	-33.37	-476.58	0.11	-0.01
667	Copertura	194, 195	0	-854.62	0.01	-47.42	33.05	-0.12	-0.02
			99	-854.62	0.01	-14.62	33.05	-0.09	-0.02
			198	-854.62	0.01	18.19	33.05	-0.07	-0.02
668	Copertura	196, 197	0	-848.66	-0.02	-47.22	32.89	0.12	0.01
			99	-848.66	-0.02	-14.58	32.89	0.10	0.01
			198	-848.66	-0.02	18.07	32.89	0.09	0.01
669	Copertura	197, 199	0	-141.87	0.01	-30.70	476.84	-0.05	-0.01
			775	-141.87	0.01	1817.62	0.14	0.01	-0.01
			1550	-141.87	0.01	-28.48	-476.56	0.08	-0.01
670	Copertura	198, 199	0	-844.90	0.02	-47.06	32.76	-0.12	0.01
			99	-844.90	0.02	-14.55	32.76	-0.13	0.01
			198	-844.90	0.02	17.97	32.76	-0.13	0.01
671	Copertura	200, 201	0	-846.61	-0.05	-46.72	32.34	-0.37	-0.35
			99	-846.61	-0.05	-14.62	32.34	-0.03	-0.35
			198	-846.61	-0.05	17.48	32.34	0.32	-0.35
672	Copertura	201, 202	0	-150.79	0.03	-45.73	476.64	-0.05	0.00
			775	-150.79	0.03	1801.05	-0.06	-0.07	0.00
			1550	-150.79	0.03	-46.61	-476.76	-0.09	0.00
673	Copertura	203, 202	0	-847.28	0.09	-46.69	32.32	1.78	1.33
			99	-847.28	0.09	-14.62	32.32	0.46	1.33
			198	-847.28	0.09	17.46	32.32	-0.86	1.33
674	Copertura	204, 205	0	-888.27	-0.11	-45.55	30.63	-2.15	-1.58
			99	-888.27	-0.11	-15.15	30.63	-0.59	-1.58
			198	-888.27	-0.11	15.25	30.63	0.98	-1.58
675	Copertura	205, 206	0	-155.08	0.03	-170.66	470.89	-0.09	-0.01
			775	-155.08	0.03	1652.51	-0.39	-0.03	-0.01
			1550	-155.08	0.03	-176.76	-471.68	0.02	-0.01
676	Copertura	207, 206	0	-895.49	0.15	-45.75	30.74	3.34	2.42
			99	-895.49	0.15	-15.25	30.74	0.94	2.42
			198	-895.49	0.15	15.26	30.74	-1.46	2.42
677	Copertura	79	0	-219.45	3.04	4.54	-5.73	-11.46	-5.37
			125	-219.45	3.04	-2.63	-5.73	-4.75	-5.37
			250	-219.45	3.04	-9.80	-5.73	1.96	-5.37
678	Copertura	124	0	-418.88	3.00	1.62	-1.84	612.68	181.21
			155	-418.88	3.00	-1.23	-1.84	331.81	181.21
			310	-418.88	3.00	-4.08	-1.84	50.94	181.21
679	Copertura	80	0	-424.76	-2.28	-0.45	-5.46	-211.05	-175.05
			45	-424.76	-2.28	-2.91	-5.46	-132.28	-175.05
			90	-424.76	-2.28	-5.37	-5.46	-53.51	-175.05
680	Copertura	128	0	-447.82	0.63	1.23	-1.26	622.45	144.60
			155	-447.82	0.63	-0.71	-1.26	398.32	144.60
			310	-447.82	0.63	-2.66	-1.26	174.19	144.60
681	Copertura	82	0	-446.81	1.89	-0.02	-2.49	-297.32	-145.73
			43	-446.81	1.89	-1.08	-2.49	-235.16	-145.73
			85	-446.81	1.89	-2.14	-2.49	-173.00	-145.73
682	Copertura	132	0	-513.60	-0.07	0.71	-0.66	626.19	142.36
			155	-513.60	-0.07	-0.30	-0.66	405.54	142.36
			310	-513.60	-0.07	-1.32	-0.66	184.88	142.36
683	Copertura	83	0	-520.11	-0.01	0.21	-2.46	-306.67	-141.80
			43	-520.11	-0.01	-0.83	-2.46	-246.18	-141.80
			85	-520.11	-0.01	-1.88	-2.46	-185.69	-141.80
684	Copertura	137	0	-559.76	-0.08	0.28	-0.24	629.29	146.32
			155	-559.76	-0.08	-0.10	-0.24	402.50	146.32
			310	-559.76	-0.08	-0.47	-0.24	175.72	146.32
685	Copertura	84	0	-561.69	-0.01	-0.21	0.60	-301.00	-146.37
			43	-561.69	-0.01	0.05	0.60	-238.56	-146.37
			85	-561.69	-0.01	0.30	0.60	-176.12	-146.37
686	Copertura	140	0	-591.54	-0.01	0.04	0.03	630.14	147.82
			155	-591.54	-0.01	0.08	0.03	401.03	147.82
			310	-591.54	-0.01	0.13	0.03	171.91	147.82

687	Copertura	85	0	-595.45	0.01	1.27	-2.92	-298.37	-147.74
			43	-595.45	0.01	0.03	-2.92	-235.36	-147.74
			85	-595.45	0.01	-1.21	-2.92	-172.34	-147.74
688	Copertura	144	0	-635.04	-0.01	-0.02	0.06	630.82	147.98
			155	-635.04	-0.01	0.08	0.06	401.45	147.98
			310	-635.04	-0.01	0.18	0.06	172.08	147.98
689	Copertura	86	0	-612.57	0.01	-1.07	1.12	-298.70	-147.56
			43	-612.57	0.01	-0.59	1.12	-235.76	-147.56
			85	-612.57	0.01	-0.11	1.12	-172.82	-147.56
690	Copertura	87	0	-600.13	-0.04	1.98	-6.64	-298.59	-147.50
			43	-600.13	-0.04	-0.86	-6.64	-235.67	-147.50
			85	-600.13	-0.04	-3.69	-6.64	-172.75	-147.50
691	Copertura	148	0	-617.72	0.03	-5.30	2.76	630.49	147.87
			155	-617.72	0.03	-1.02	2.76	401.30	147.87
			310	-617.72	0.03	3.27	2.76	172.10	147.87
692	Copertura	88	0	-568.06	0.03	-2.00	0.35	-298.80	-147.24
			43	-568.06	0.03	-1.85	0.35	-236.00	-147.24
			85	-568.06	0.03	-1.70	0.35	-173.19	-147.24
693	Copertura	152	0	-565.21	0.02	-7.20	3.80	629.64	147.34
			155	-565.21	0.02	-1.31	3.80	401.25	147.34
			310	-565.21	0.02	4.59	3.80	172.87	147.34
694	Copertura	89	0	-565.99	-0.03	1.00	-7.10	-298.80	-147.26
			43	-565.99	-0.03	-2.03	-7.10	-235.98	-147.26
			85	-565.99	-0.03	-5.06	-7.10	-173.16	-147.26
695	Copertura	156	0	-556.89	0.02	-7.91	4.25	629.62	147.28
			155	-556.89	0.02	-1.32	4.25	401.33	147.28
			310	-556.89	0.02	5.28	4.25	173.04	147.28
696	Copertura	90	0	-557.31	0.01	-0.81	-3.67	-298.71	-147.21
			43	-557.31	0.01	-2.37	-3.67	-235.91	-147.21
			85	-557.31	0.01	-3.94	-3.67	-173.12	-147.21
697	Copertura	160	0	-564.18	0.02	-8.78	4.74	629.85	147.33
			155	-564.18	0.02	-1.43	4.74	401.49	147.33
			310	-564.18	0.02	5.93	4.74	173.13	147.33
698	Copertura	91	0	-565.12	-0.03	0.73	-7.45	-298.66	-147.19
			43	-565.12	-0.03	-2.45	-7.45	-235.88	-147.19
			85	-565.12	-0.03	-5.63	-7.45	-173.09	-147.19
699	Copertura	164	0	-572.50	0.03	-9.65	5.23	630.03	147.34
			155	-572.50	0.03	-1.54	5.23	401.66	147.34
			310	-572.50	0.03	6.56	5.23	173.29	147.34
700	Copertura	92	0	-562.64	0.01	-0.50	-4.91	-298.74	-147.08
			43	-562.64	0.01	-2.59	-4.91	-236.00	-147.08
			85	-562.64	0.01	-4.68	-4.91	-173.26	-147.08
701	Copertura	168	0	-576.46	0.04	-10.51	5.70	629.88	147.10
			155	-576.46	0.04	-1.68	5.70	401.88	147.10
			310	-576.46	0.04	7.16	5.70	173.88	147.10
702	Copertura	93	0	-575.25	-0.03	-1.69	-2.12	-298.97	-147.01
			43	-575.25	-0.03	-2.59	-2.12	-236.26	-147.01
			85	-575.25	-0.03	-3.49	-2.12	-173.55	-147.01
703	Copertura	172	0	-568.36	0.05	-11.22	6.08	629.28	146.62
			155	-568.36	0.05	-1.80	6.08	402.02	146.62
			310	-568.36	0.05	7.63	6.08	174.77	146.62
704	Copertura	94	0	-571.68	0.02	1.76	-6.91	-298.88	-147.08
			43	-571.68	0.02	-1.19	-6.91	-236.14	-147.08
			85	-571.68	0.02	-4.14	-6.91	-173.40	-147.08
705	Copertura	176	0	-563.91	0.02	-12.13	6.69	628.62	146.58
			155	-563.91	0.02	-1.75	6.69	401.43	146.58
			310	-563.91	0.02	8.62	6.69	174.23	146.58
706	Copertura	180	0	-576.69	-0.02	-0.07	0.15	629.17	146.46
			155	-576.69	-0.02	0.16	0.15	402.15	146.46
			310	-576.69	-0.02	0.39	0.15	175.14	146.46
707	Copertura	95	0	-616.67	0.03	-2.20	2.24	-299.30	-147.05
			43	-616.67	0.03	-1.24	2.24	-236.58	-147.05
			85	-616.67	0.03	-0.29	2.24	-173.85	-147.05
708	Copertura	184	0	-597.56	-0.01	-0.13	0.16	629.65	147.00
			155	-597.56	-0.01	0.11	0.16	401.80	147.00
			310	-597.56	-0.01	0.36	0.16	173.96	147.00
709	Copertura	96	0	-610.14	-0.03	2.54	-6.96	-298.40	-147.31
			43	-610.14	-0.03	-0.42	-6.96	-235.56	-147.31
			85	-610.14	-0.03	-3.39	-6.96	-172.72	-147.31
710	Copertura	188	0	-594.50	-0.01	-0.28	0.27	630.28	147.38
			155	-594.50	-0.01	0.15	0.27	401.84	147.38
			310	-594.50	-0.01	0.57	0.27	173.39	147.38

711	Copertura	97	0	-586.84	0.09	-0.15	0.25	-298.57	-147.16
			43	-586.84	0.09	-0.05	0.25	-235.80	-147.16
			85	-586.84	0.09	0.06	0.25	-173.02	-147.16
712	Copertura	192	0	-569.80	0.08	-0.55	0.55	629.79	146.34
			155	-569.80	0.08	0.29	0.55	402.96	146.34
			310	-569.80	0.08	1.14	0.55	176.14	146.34
713	Copertura	106	0	-563.07	-0.12	0.19	0.84	-300.93	-145.87
			43	-563.07	-0.12	0.55	0.84	-238.71	-145.87
			85	-563.07	-0.12	0.91	0.84	-176.49	-145.87
714	Copertura	196	0	-533.45	0.08	-0.96	0.92	626.65	142.46
			155	-533.45	0.08	0.47	0.92	405.83	142.46
			310	-533.45	0.08	1.90	0.92	185.01	142.46
715	Copertura	107	0	-502.18	-0.50	0.33	0.64	-306.79	-142.38
			43	-502.18	-0.50	0.60	0.64	-246.05	-142.38
			85	-502.18	-0.50	0.87	0.64	-185.32	-142.38
716	Copertura	200	0	-455.69	-0.62	-1.44	1.46	622.59	144.51
			155	-455.69	-0.62	0.83	1.46	398.60	144.51
			310	-455.69	-0.62	3.10	1.46	174.61	144.51
717	Copertura	108	0	-452.22	1.13	0.18	5.55	-296.54	-143.45
			43	-452.22	1.13	2.55	5.55	-235.35	-143.45
			85	-452.22	1.13	4.92	5.55	-174.16	-143.45
718	Copertura	204	0	-425.66	-3.01	-1.80	2.03	614.02	181.64
			155	-425.66	-3.01	1.34	2.03	332.47	181.64
			310	-425.66	-3.01	4.49	2.03	50.93	181.64
719	Copertura	109	0	-433.71	-4.53	0.09	7.08	-197.46	-170.70
			43	-433.71	-4.53	3.11	7.08	-124.64	-170.70
			85	-433.71	-4.53	6.13	7.08	-51.83	-170.70
720	Copertura	110	0	-223.90	-7.78	4.42	4.21	-8.78	-11.24
			43	-223.90	-7.78	6.22	4.21	-3.98	-11.24
			85	-223.90	-7.78	8.01	4.21	0.81	-11.24
721	Copertura	14	0	-211.76	-14.94	12.24	-7.29	18.73	15.60
			95	-211.76	-14.94	5.31	-7.29	3.91	15.60
			190	-211.76	-14.94	-1.61	-7.29	-10.91	15.60
722	Copertura	15	0	184.54	1.31	3.33	-0.30	-41.67	-468.39
			65	184.54	1.31	3.13	-0.30	262.78	-468.39
			130	184.54	1.31	2.94	-0.30	567.23	-468.39
723	Copertura	16	0	187.00	-5.04	1.26	3.07	37.85	464.88
			65	187.00	-5.04	3.26	3.07	-264.32	464.88
			130	187.00	-5.04	5.25	3.07	-566.49	464.88
724	Copertura	17	0	130.89	0.30	2.63	-0.90	-40.17	-473.79
			65	130.89	0.30	2.05	-0.90	267.79	-473.79
			130	130.89	0.30	1.46	-0.90	575.75	-473.79
725	Copertura	18	0	130.89	-0.35	3.23	-1.85	40.14	473.64
			65	130.89	-0.35	2.02	-1.85	-267.73	473.64
			130	130.89	-0.35	0.82	-1.85	-575.59	473.64
726	Copertura	19	0	66.23	0.00	1.51	-0.67	-40.49	-476.54
			65	66.23	0.00	1.07	-0.67	269.27	-476.54
			130	66.23	0.00	0.64	-0.67	579.02	-476.54
727	Copertura	20	0	56.25	-0.06	2.14	-1.75	40.88	476.51
			65	56.25	-0.06	1.00	-1.75	-268.85	476.51
			130	56.25	-0.06	-0.14	-1.75	-578.58	476.51
728	Copertura	21	0	25.96	-0.02	0.58	-0.27	-40.90	-479.02
			65	25.96	-0.02	0.40	-0.27	270.46	-479.02
			130	25.96	-0.02	0.23	-0.27	581.82	-479.02
729	Copertura	22	0	22.62	0.04	0.28	-0.02	41.02	479.02
			65	22.62	0.04	0.26	-0.02	-270.34	479.02
			130	22.62	0.04	0.25	-0.02	-581.70	479.02
730	Copertura	23	0	-3.43	0.00	-0.01	0.03	-41.62	-480.16
			65	-3.43	0.00	0.01	0.03	270.48	-480.16
			130	-3.43	0.00	0.03	0.03	582.59	-480.16
731	Copertura	24	0	-6.63	0.02	-0.13	-0.05	41.75	480.33
			65	-6.63	0.02	-0.16	-0.05	-270.47	480.33
			130	-6.63	0.02	-0.19	-0.05	-582.68	480.33
732	Copertura	25	0	-45.39	-0.01	-0.10	0.06	-42.93	-481.63
			65	-45.39	-0.01	-0.06	0.06	270.13	-481.63
			130	-45.39	-0.01	-0.02	0.06	583.19	-481.63
733	Copertura	26	0	-24.88	-0.01	-3.33	3.29	42.34	480.82
			65	-24.88	-0.01	-1.19	3.29	-270.19	480.82
			130	-24.88	-0.01	0.95	3.29	-582.72	480.82
734	Copertura	27	0	-9.02	-0.02	-5.24	6.54	41.30	479.82
			65	-9.02	-0.02	-0.99	6.54	-270.58	479.82
			130	-9.02	-0.02	3.26	6.54	-582.46	479.82

735	Copertura	28	0	-29.25	-0.02	8.60	-9.93	-41.49	-480.29
			65	-29.25	-0.02	2.14	-9.93	270.70	-480.29
			130	-29.25	-0.02	-4.31	-9.93	582.89	-480.29
736	Copertura	29	0	15.76	-0.04	-11.04	13.13	39.50	478.19
			65	15.76	-0.04	-2.50	13.13	-271.32	478.19
			130	15.76	-0.04	6.03	13.13	-582.15	478.19
737	Copertura	30	0	20.72	-0.04	11.68	-13.50	-39.21	-477.95
			65	20.72	-0.04	2.91	-13.50	271.46	-477.95
			130	20.72	-0.04	-5.86	-13.50	582.13	-477.95
738	Copertura	31	0	24.18	-0.04	-10.93	13.00	39.11	477.90
			65	24.18	-0.04	-2.48	13.00	-271.52	477.90
			130	24.18	-0.04	5.97	13.00	-582.16	477.90
739	Copertura	32	0	28.65	-0.05	12.67	-14.70	-38.64	-477.50
			65	28.65	-0.05	3.12	-14.70	271.73	-477.50
			130	28.65	-0.05	-6.44	-14.70	582.11	-477.50
740	Copertura	33	0	23.94	-0.04	-13.38	15.77	38.42	477.20
			65	23.94	-0.04	-3.13	15.77	-271.76	477.20
			130	23.94	-0.04	7.12	15.77	-581.94	477.20
741	Copertura	34	0	21.48	-0.06	13.92	-16.21	-38.43	-477.50
			65	21.48	-0.06	3.39	-16.21	271.95	-477.50
			130	21.48	-0.06	-7.15	-16.21	582.32	-477.50
742	Copertura	35	0	24.79	-0.05	-13.57	16.08	38.15	476.96
			65	24.79	-0.05	-3.12	16.08	-271.88	476.96
			130	24.79	-0.05	7.33	16.08	-581.90	476.96
743	Copertura	36	0	13.21	-0.06	15.17	-17.72	-38.20	-477.44
			65	13.21	-0.06	3.66	-17.72	272.14	-477.44
			130	13.21	-0.06	-7.86	-17.72	582.47	-477.44
744	Copertura	37	0	17.27	-0.05	-15.40	18.22	37.69	476.48
			65	17.27	-0.05	-3.55	18.22	-272.02	476.48
			130	17.27	-0.05	8.29	18.22	-581.74	476.48
745	Copertura	38	0	8.77	-0.06	16.42	-19.21	-37.81	-477.03
			65	8.77	-0.06	3.93	-19.21	272.26	-477.03
			130	8.77	-0.06	-8.56	-19.21	582.33	-477.03
746	Copertura	39	0	12.83	-0.05	-15.76	18.86	37.60	476.40
			65	12.83	-0.05	-3.50	18.86	-272.06	476.40
			130	12.83	-0.05	8.76	18.86	-581.72	476.40
747	Copertura	40	0	15.67	-0.06	17.41	-20.43	-37.17	-476.11
			65	15.67	-0.06	4.13	-20.43	272.30	-476.11
			130	15.67	-0.06	-9.14	-20.43	581.77	-476.11
748	Copertura	41	0	9.45	-0.03	-11.26	14.41	38.64	477.32
			65	9.45	-0.03	-1.89	14.41	-271.62	477.32
			130	9.45	-0.03	7.48	14.41	-581.88	477.32
749	Copertura	42	0	19.31	-0.08	18.41	-21.78	-36.55	-475.16
			65	19.31	-0.08	4.26	-21.78	272.31	-475.16
			130	19.31	-0.08	-9.90	-21.78	581.17	-475.16
750	Copertura	43	0	9.36	-0.01	-0.26	0.14	-41.30	-479.22
			65	9.36	-0.01	-0.17	0.14	270.20	-479.22
			130	9.36	-0.01	-0.08	0.14	581.69	-479.22
751	Copertura	44	0	-27.12	-0.01	-6.52	6.60	42.39	480.39
			65	-27.12	-0.01	-2.23	6.60	-269.87	480.39
			130	-27.12	-0.01	2.06	6.60	-582.13	480.39
752	Copertura	45	0	-10.28	-0.01	-0.33	0.15	-41.91	-480.03
			65	-10.28	-0.01	-0.23	0.15	270.11	-480.03
			130	-10.28	-0.01	-0.13	0.15	582.13	-480.03
753	Copertura	46	0	-25.56	0.01	-0.59	0.37	42.24	480.09
			65	-25.56	0.01	-0.34	0.37	-269.82	480.09
			130	-25.56	0.01	-0.10	0.37	-581.87	480.09
754	Copertura	47	0	-6.54	-0.01	-0.61	0.27	-41.80	-480.40
			65	-6.54	-0.01	-0.44	0.27	270.46	-480.40
			130	-6.54	-0.01	-0.27	0.27	582.71	-480.40
755	Copertura	48	0	0.11	0.00	-1.11	0.92	41.49	479.38
			65	0.11	0.00	-0.51	0.92	-270.11	479.38
			130	0.11	0.00	0.09	0.92	-581.71	479.38
756	Copertura	49	0	16.52	0.02	-1.23	0.57	-41.23	-479.62
			65	16.52	0.02	-0.85	0.57	270.52	-479.62
			130	16.52	0.02	-0.48	0.57	582.28	-479.62
757	Copertura	50	0	19.24	-0.05	-1.85	1.59	41.10	478.61
			65	19.24	-0.05	-0.81	1.59	-269.99	478.61
			130	19.24	-0.05	0.22	1.59	-581.09	478.61
758	Copertura	51	0	47.22	0.00	-2.09	0.94	-41.07	-477.31
			65	47.22	0.00	-1.48	0.94	269.18	-477.31
			130	47.22	0.00	-0.87	0.94	579.43	-477.31

759	Copertura	52	0	75.13	-0.02	-2.91	1.98	40.14	475.28
			65	75.13	-0.02	-1.63	1.98	-268.80	475.28
			130	75.13	-0.02	-0.34	1.98	-577.73	475.28
760	Copertura	53	0	123.21	-0.30	-3.10	1.12	-40.42	-474.08
			65	123.21	-0.30	-2.38	1.12	267.73	-474.08
			130	123.21	-0.30	-1.65	1.12	575.88	-474.08
761	Copertura	54	0	122.42	1.00	-4.24	2.57	40.12	473.44
			65	122.42	1.00	-2.57	2.57	-267.62	473.44
			130	122.42	1.00	-0.89	2.57	-575.35	473.44
762	Copertura	55	0	179.24	-1.30	-3.71	0.45	-41.95	-469.55
			65	179.24	-1.30	-3.42	0.45	263.26	-469.55
			130	179.24	-1.30	-3.13	0.45	568.46	-469.55
763	Copertura	56	0	178.94	1.89	-5.03	2.13	41.37	470.74
			65	178.94	1.89	-3.64	2.13	-264.61	470.74
			130	178.94	1.89	-2.26	2.13	-570.59	470.74
764	Copertura	70	0	-218.19	7.80	-13.91	6.45	9.12	5.18
			95	-218.19	7.80	-7.79	6.45	4.20	5.18
			190	-218.19	7.80	-1.66	6.45	-0.72	5.18
765	Copertura	81	0	-419.55	3.15	3.58	-4.80	-493.19	-176.25
			80	-419.55	3.15	-0.26	-4.80	-352.19	-176.25
			160	-419.55	3.15	-4.10	-4.80	-211.18	-176.25
766	Copertura	126	0	-427.24	-12.21	-0.55	-3.24	-612.07	-197.22
			30	-427.24	-12.21	-1.52	-3.24	-552.90	-197.22
			60	-427.24	-12.21	-2.50	-3.24	-493.74	-197.22
767	Copertura	98	0	-452.02	-1.94	1.91	-3.15	-535.27	-144.53
			82	-452.02	-1.94	-0.68	-3.15	-416.26	-144.53
			165	-452.02	-1.94	-3.28	-3.15	-297.25	-144.53
768	Copertura	99	0	-518.94	0.27	1.07	-1.04	-540.74	-142.13
			82	-518.94	0.27	0.21	-1.04	-423.71	-142.13
			165	-518.94	0.27	-0.65	-1.04	-306.67	-142.13
769	Copertura	100	0	-562.86	0.14	0.44	-0.81	-541.52	-146.05
			82	-562.86	0.14	-0.22	-0.81	-421.25	-146.05
			165	-562.86	0.14	-0.89	-0.81	-300.99	-146.05
770	Copertura	101	0	-594.83	-0.02	-0.35	0.81	-541.64	-147.71
			82	-594.83	-0.02	0.32	0.81	-420.01	-147.71
			165	-594.83	-0.02	0.99	0.81	-298.38	-147.71
771	Copertura	102	0	-613.20	0.00	2.67	-2.60	-541.75	-147.58
			82	-613.20	0.00	0.53	-2.60	-420.22	-147.58
			165	-613.20	0.00	-1.61	-2.60	-298.70	-147.58
772	Copertura	103	0	-596.91	-0.01	0.50	-0.25	-541.51	-147.51
			82	-596.91	-0.01	0.29	-0.25	-420.05	-147.51
			165	-596.91	-0.01	0.09	-0.25	-298.59	-147.51
773	Copertura	104	0	-571.28	0.00	5.59	-6.04	-541.28	-147.24
			82	-571.28	0.00	0.61	-6.04	-420.04	-147.24
			165	-571.28	0.00	-4.37	-6.04	-298.80	-147.24
774	Copertura	105	0	-560.72	0.00	4.38	-4.12	-541.34	-147.28
			82	-560.72	0.00	0.99	-4.12	-420.07	-147.28
			165	-560.72	0.00	-2.40	-4.12	-298.80	-147.28
775	Copertura	111	0	-562.58	0.00	6.25	-6.66	-533.53	-147.20
			80	-562.58	0.00	0.94	-6.66	-416.12	-147.20
			160	-562.58	0.00	-4.37	-6.66	-298.71	-147.20
776	Copertura	112	0	-559.07	-0.01	5.65	-5.38	-541.08	-147.20
			82	-559.07	-0.01	1.22	-5.38	-419.87	-147.20
			165	-559.07	-0.01	-3.21	-5.38	-298.66	-147.20
777	Copertura	113	0	-568.68	0.01	6.96	-6.98	-540.94	-147.07
			82	-568.68	0.01	1.21	-6.98	-419.84	-147.07
			165	-568.68	0.01	-4.53	-6.98	-298.74	-147.07
778	Copertura	114	0	-570.54	-0.01	7.10	-7.41	-541.08	-147.01
			82	-570.54	-0.01	1.00	-7.41	-420.02	-147.01
			165	-570.54	-0.01	-5.10	-7.41	-298.97	-147.01
779	Copertura	115	0	-576.39	0.00	1.63	-1.63	-541.11	-147.08
			82	-576.39	0.00	0.29	-1.63	-420.00	-147.08
			165	-576.39	0.00	-1.05	-1.63	-298.88	-147.08
780	Copertura	116	0	-614.55	0.01	5.88	-5.93	-541.48	-147.05
			82	-614.55	0.01	1.00	-5.93	-420.39	-147.05
			165	-614.55	0.01	-3.88	-5.93	-299.30	-147.05
781	Copertura	117	0	-612.26	0.01	-0.55	1.21	-541.00	-147.31
			82	-612.26	0.01	0.44	1.21	-419.70	-147.31
			165	-612.26	0.01	1.43	1.21	-298.40	-147.31
782	Copertura	118	0	-587.62	-0.03	0.09	0.13	-540.92	-147.16
			82	-587.62	-0.03	0.20	0.13	-419.74	-147.16
			165	-587.62	-0.03	0.30	0.13	-298.57	-147.16

783	Copertura	131	0	-448.08	-0.80	0.49	-2.32	-622.28	-145.07
			30	-448.08	-0.80	-0.21	-2.32	-578.76	-145.07
			60	-448.08	-0.80	-0.90	-2.32	-535.24	-145.07
784	Copertura	133	0	-522.88	-0.15	-0.19	-1.88	-625.72	-141.58
			30	-522.88	-0.15	-0.76	-1.88	-583.24	-141.58
			60	-522.88	-0.15	-1.32	-1.88	-540.77	-141.58
785	Copertura	139	0	-562.89	0.10	0.31	0.03	-629.17	-146.07
			30	-562.89	0.10	0.32	0.03	-585.35	-146.07
			60	-562.89	0.10	0.33	0.03	-541.53	-146.07
786	Copertura	143	0	-594.80	0.04	-0.18	-0.03	-630.25	-147.69
			30	-594.80	0.04	-0.19	-0.03	-585.94	-147.69
			60	-594.80	0.04	-0.20	-0.03	-541.63	-147.69
787	Copertura	147	0	-613.42	0.01	0.94	3.38	-630.30	-147.59
			30	-613.42	0.01	1.96	3.38	-586.02	-147.59
			60	-613.42	0.01	2.97	3.38	-541.75	-147.59
788	Copertura	151	0	-596.69	0.00	4.24	-6.23	-630.01	-147.50
			30	-596.69	0.00	2.37	-6.23	-585.76	-147.50
			60	-596.69	0.00	0.50	-6.23	-541.51	-147.50
789	Copertura	155	0	-570.37	0.05	7.40	-4.17	-629.67	-147.31
			30	-570.37	0.05	6.15	-4.17	-585.47	-147.31
			60	-570.37	0.05	4.90	-4.17	-541.28	-147.31
790	Copertura	159	0	-561.63	0.04	7.46	-5.99	-629.67	-147.20
			30	-561.63	0.04	5.66	-5.99	-585.51	-147.20
			60	-561.63	0.04	3.86	-5.99	-541.35	-147.20
791	Copertura	119	0	-562.29	-0.01	-0.84	0.97	-541.17	-145.88
			82	-562.29	-0.01	-0.04	0.97	-421.05	-145.88
			165	-562.29	-0.01	0.75	0.97	-300.93	-145.88
792	Copertura	120	0	-506.14	0.17	-1.49	2.58	-539.73	-141.44
			82	-506.14	0.17	0.64	2.58	-423.26	-141.44
			165	-506.14	0.17	2.77	2.58	-306.79	-141.44
793	Copertura	121	0	-448.27	-0.78	-2.98	3.61	-534.33	-144.39
			82	-448.27	-0.78	-0.01	3.61	-415.43	-144.39
			165	-448.27	-0.78	2.96	3.61	-296.54	-144.39
794	Copertura	122	0	-439.42	6.00	-3.34	4.84	-505.14	-187.12
			82	-439.42	6.00	0.64	4.84	-351.06	-187.12
			165	-439.42	6.00	4.63	4.84	-196.98	-187.12
795	Copertura	123	0	-218.19	7.80	-1.66	6.45	-0.72	5.18
			82	-218.19	7.80	3.64	6.45	-4.99	5.18
			165	-218.19	7.80	8.95	6.45	-9.26	5.18
796	Copertura	163	0	-561.40	0.06	8.77	-5.16	-629.45	-147.29
			33	-561.40	0.06	7.09	-5.16	-581.46	-147.29
			65	-561.40	0.06	5.40	-5.16	-533.47	-147.29
797	Copertura	167	0	-560.26	0.05	9.13	-6.87	-629.40	-147.11
			30	-560.26	0.05	7.07	-6.87	-585.27	-147.11
			60	-560.26	0.05	5.00	-6.87	-541.14	-147.11
798	Copertura	171	0	-567.49	0.05	10.25	-6.68	-629.24	-147.16
			30	-567.49	0.05	8.25	-6.68	-585.09	-147.16
			60	-567.49	0.05	6.24	-6.68	-540.94	-147.16
799	Copertura	174	0	-571.73	0.06	10.86	-7.70	-629.23	-146.92
			30	-571.73	0.06	8.55	-7.70	-585.15	-146.92
			60	-571.73	0.06	6.24	-7.70	-541.08	-146.92
800	Copertura	179	0	-576.21	0.06	9.73	-14.35	-629.41	-147.16
			30	-576.21	0.06	5.42	-14.35	-585.26	-147.16
			60	-576.21	0.06	1.12	-14.35	-541.11	-147.16
801	Copertura	183	0	-614.73	0.05	2.08	6.80	-629.66	-146.97
			30	-614.73	0.05	4.12	6.80	-585.57	-146.97
			60	-614.73	0.05	6.15	6.80	-541.48	-146.97
802	Copertura	187	0	-613.20	0.00	-0.11	0.39	-629.39	-147.33
			30	-613.20	0.00	0.00	0.39	-585.19	-147.33
			60	-613.20	0.00	0.12	0.39	-541.00	-147.33
803	Copertura	191	0	-586.68	0.00	0.08	0.95	-629.20	-147.14
			30	-586.68	0.00	0.37	0.95	-585.06	-147.14
			60	-586.68	0.00	0.65	0.95	-540.92	-147.14
804	Copertura	194	0	-565.45	-0.13	0.14	1.57	-628.50	-145.58
			30	-565.45	-0.13	0.61	1.57	-584.83	-145.58
			60	-565.45	-0.13	1.08	1.57	-541.16	-145.58
805	Copertura	198	0	-502.98	-0.10	-0.43	1.99	-624.80	-141.74
			30	-502.98	-0.10	0.16	1.99	-582.27	-141.74
			60	-502.98	-0.10	0.76	1.99	-539.75	-141.74
806	Copertura	203	0	-456.91	2.40	0.20	3.90	-622.04	-145.67
			30	-456.91	2.40	1.37	3.90	-578.34	-145.67
			60	-456.91	2.40	2.54	3.90	-534.64	-145.67

807	Copertura	207	0	-430.77	4.51	-0.18	4.55	-616.34	-185.84
			30	-430.77	4.51	1.18	4.55	-560.59	-185.84
			60	-430.77	4.51	2.55	4.55	-504.84	-185.84

1.1.3.2 Piastre SLU

Tabella 6.I

Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	1.511	0.435	-0.295	-339.107	-99.326	-52.853	-3.505	-1.728
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	1.571	0.924	0.413	-366.041	91.755	-65.481	4.449	-1.674
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	1.512	0.924	0.384	-322.686	95.246	67.662	-4.075	-1.614

1.1.4 Risultati Condizioni (Delta Termico).

1.1.4.1 Sollecitazioni SLU

Tabella 7.I

Sollecitazioni									
Asta	Imp.	Fili	X [cm]	N [daN]	Mt [daNm]	Mxz [daNm]	Txz [daN]	Mxy [daNm]	Txy [daN]
1	Fondazione	1, 2	0	0.00	0.00	0.00	0.00	0.00	0.00
			42	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
2	Fondazione	1, 2	0	0.00	0.00	0.00	0.00	0.00	0.00
			42	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
3	Fondazione	1, 15	0	0.00	0.00	0.00	0.00	0.00	0.00
			40	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
4	Fondazione	1, 15	0	0.00	0.00	0.00	0.00	0.00	0.00
			40	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
5	Fondazione	2, 3	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
6	Fondazione	2, 3	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
7	Fondazione	3, 4	0	0.00	0.00	0.00	0.00	0.00	0.00

	ne								
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
8	Fondazio ne	3, 4	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
9	Fondazio ne	4, 5	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
10	Fondazio ne	4, 5	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
11	Fondazio ne	5, 6	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
12	Fondazio ne	5, 6	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
13	Fondazio ne	6, 7	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
14	Fondazio ne	6, 7	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
15	Fondazio ne	7, 8	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
16	Fondazio ne	7, 8	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
17	Fondazio ne	8, 9	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
18	Fondazio ne	8, 9	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
19	Fondazio ne	9, 10	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
20	Fondazio ne	9, 10	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
21	Fondazio ne	10, 11	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
22	Fondazio ne	10, 11	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
23	Fondazio ne	11, 12	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
24	Fondazio ne	11, 12	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
25	Fondazio ne	12, 13	0	0.00	0.00	0.00	0.00	0.00	0.00

			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
26	Fondazio ne	12, 13	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
27	Fondazio ne	13, 14	0	0.00	0.00	0.00	0.00	0.00	0.00
			42	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
28	Fondazio ne	13, 14	0	0.00	0.00	0.00	0.00	0.00	0.00
			42	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
29	Fondazio ne	14, 16	0	0.00	0.00	0.00	0.00	0.00	0.00
			40	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
30	Fondazio ne	14, 16	0	0.00	0.00	0.00	0.00	0.00	0.00
			40	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
31	Fondazio ne	15, 17	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
32	Fondazio ne	15, 17	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
33	Fondazio ne	16, 18	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
34	Fondazio ne	16, 18	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
35	Fondazio ne	17, 19	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
36	Fondazio ne	17, 19	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
37	Fondazio ne	18, 20	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
38	Fondazio ne	18, 20	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
39	Fondazio ne	19, 21	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
40	Fondazio ne	19, 21	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
41	Fondazio ne	20, 22	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
42	Fondazio ne	20, 22	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
43	Fondazio ne	21, 23	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00

			66	0.00	0.00	0.00	0.00	0.00	0.00
44	Fondazio ne	21, 23	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
45	Fondazio ne	22, 24	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
46	Fondazio ne	22, 24	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
47	Fondazio ne	23, 25	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
48	Fondazio ne	23, 25	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
49	Fondazio ne	24, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
50	Fondazio ne	24, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
51	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
52	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
53	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
54	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
55	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
56	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
57	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
58	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
59	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
60	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
61	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00

62	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
63	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
64	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
65	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
66	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
67	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
68	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
69	Fondazio ne	25, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
70	Fondazio ne	25, 28	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
71	Fondazio ne	25, 28	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
72	Fondazio ne	26, 27	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
73	Fondazio ne	26, 27	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
74	Fondazio ne	27, 29	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
75	Fondazio ne	27, 29	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
76	Fondazio ne	28, 30	0	0.00	0.00	0.00	0.00	0.00	0.00
			37	0.00	0.00	0.00	0.00	0.00	0.00
			73	0.00	0.00	0.00	0.00	0.00	0.00
77	Fondazio ne	28, 30	0	0.00	0.00	0.00	0.00	0.00	0.00
			37	0.00	0.00	0.00	0.00	0.00	0.00
			73	0.00	0.00	0.00	0.00	0.00	0.00
78	Fondazio ne	29, 31	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
79	Fondazio ne	29, 31	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
80	Fondazio	30, 32	0	0.00	0.00	0.00	0.00	0.00	0.00

	ne								
			34	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
81	Fondazio ne	30, 32	0	0.00	0.00	0.00	0.00	0.00	0.00
			34	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
82	Fondazio ne	31, 33	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
83	Fondazio ne	31, 33	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
84	Fondazio ne	32, 34	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
85	Fondazio ne	32, 34	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
86	Fondazio ne	33, 35	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
87	Fondazio ne	33, 35	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
88	Fondazio ne	34, 36	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
89	Fondazio ne	34, 36	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
90	Fondazio ne	35, 37	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
91	Fondazio ne	35, 37	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
92	Fondazio ne	36, 38	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
93	Fondazio ne	36, 38	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
94	Fondazio ne	37, 39	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
95	Fondazio ne	37, 39	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
96	Fondazio ne	38, 40	0	0.00	0.00	0.00	0.00	0.00	0.00
			34	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
97	Fondazio ne	38, 40	0	0.00	0.00	0.00	0.00	0.00	0.00
			34	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
98	Fondazio ne	39, 41	0	0.00	0.00	0.00	0.00	0.00	0.00

			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
99	Fondazio ne	39, 41	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
100	Fondazio ne	40, 42	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
101	Fondazio ne	40, 42	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
102	Fondazio ne	41, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
103	Fondazio ne	41, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
104	Fondazio ne	42, 43	0	0.00	0.00	0.00	0.00	0.00	0.00
			23	0.00	0.00	0.00	0.00	0.00	0.00
			46	0.00	0.00	0.00	0.00	0.00	0.00
105	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
106	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
107	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
108	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
109	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
110	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
111	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
112	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
113	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
114	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
115	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
116	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00

			97	0.00	0.00	0.00	0.00	0.00	0.00
117	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
118	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
119	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
120	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
121	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
122	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
123	Fondazio ne	43, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			49	0.00	0.00	0.00	0.00	0.00	0.00
			97	0.00	0.00	0.00	0.00	0.00	0.00
124	Fondazio ne	43, 45	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
125	Fondazio ne	43, 45	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
126	Fondazio ne	44, 46	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
127	Fondazio ne	44, 46	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
128	Fondazio ne	45, 47	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
129	Fondazio ne	45, 47	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
130	Fondazio ne	46, 48	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
131	Fondazio ne	46, 48	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
132	Fondazio ne	47, 49	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
133	Fondazio ne	47, 49	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
134	Fondazio ne	48, 50	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00

135	Fondazio ne	48, 50	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
136	Fondazio ne	49, 51	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
137	Fondazio ne	49, 51	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
138	Fondazio ne	50, 52	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
139	Fondazio ne	50, 52	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
140	Fondazio ne	51, 53	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
141	Fondazio ne	51, 53	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
142	Fondazio ne	52, 54	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
143	Fondazio ne	52, 54	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
144	Fondazio ne	53, 55	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
145	Fondazio ne	53, 55	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
146	Fondazio ne	54, 56	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
147	Fondazio ne	54, 56	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
148	Fondazio ne	55, 57	0	0.00	0.00	0.00	0.00	0.00	0.00
			40	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
149	Fondazio ne	55, 57	0	0.00	0.00	0.00	0.00	0.00	0.00
			40	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
150	Fondazio ne	56, 70	0	0.00	0.00	0.00	0.00	0.00	0.00
			40	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
151	Fondazio ne	56, 70	0	0.00	0.00	0.00	0.00	0.00	0.00
			40	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
152	Fondazio ne	57, 58	0	0.00	0.00	0.00	0.00	0.00	0.00
			42	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
153	Fondazio	57, 58	0	0.00	0.00	0.00	0.00	0.00	0.00

	ne								
			42	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
154	Fondazio ne	58, 59	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
155	Fondazio ne	58, 59	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
156	Fondazio ne	59, 60	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
157	Fondazio ne	59, 60	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
158	Fondazio ne	60, 61	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
159	Fondazio ne	60, 61	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
160	Fondazio ne	61, 62	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
161	Fondazio ne	61, 62	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
162	Fondazio ne	62, 63	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
163	Fondazio ne	62, 63	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
164	Fondazio ne	63, 64	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
165	Fondazio ne	63, 64	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
166	Fondazio ne	64, 65	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
167	Fondazio ne	64, 65	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
168	Fondazio ne	65, 66	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
169	Fondazio ne	65, 66	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
170	Fondazio ne	66, 67	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
171	Fondazio ne	66, 67	0	0.00	0.00	0.00	0.00	0.00	0.00

			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
172	Fondazio ne	67, 68	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
173	Fondazio ne	67, 68	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
174	Fondazio ne	68, 69	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
175	Fondazio ne	68, 69	0	0.00	0.00	0.00	0.00	0.00	0.00
			35	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
176	Fondazio ne	69, 70	0	0.00	0.00	0.00	0.00	0.00	0.00
			42	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
177	Fondazio ne	69, 70	0	0.00	0.00	0.00	0.00	0.00	0.00
			42	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
178	Primo Impalcato	1, 2	0	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
			166	0.00	0.00	0.00	0.00	0.00	0.00
179	Primo Impalcato	1, 15	0	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
			159	0.00	0.00	0.00	0.00	0.00	0.00
180	Primo Impalcato	2, 3	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
181	Primo Impalcato	3, 4	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
182	Primo Impalcato	4, 5	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
183	Primo Impalcato	5, 6	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
184	Primo Impalcato	6, 7	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
185	Primo Impalcato	7, 8	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
186	Primo Impalcato	8, 9	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
187	Primo Impalcato	9, 10	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
188	Primo Impalcato	10, 11	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
189	Primo Impalcato	11, 12	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00

			138	0.00	0.00	0.00	0.00	0.00	0.00
190	Primo Impalcato	12, 13	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
191	Primo Impalcato	13, 14	0	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
			166	0.00	0.00	0.00	0.00	0.00	0.00
192	Primo Impalcato	14, 16	0	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
			159	0.00	0.00	0.00	0.00	0.00	0.00
193	Primo Impalcato	15, 17	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
194	Primo Impalcato	16, 18	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
195	Primo Impalcato	17, 19	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
196	Primo Impalcato	18, 20	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
197	Primo Impalcato	19, 21	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
198	Primo Impalcato	20, 22	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
199	Primo Impalcato	21, 23	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
200	Primo Impalcato	22, 24	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
201	Primo Impalcato	23, 25	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
202	Primo Impalcato	24, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
203	Primo Impalcato	25, 28	0	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
			170	0.00	0.00	0.00	0.00	0.00	0.00
204	Primo Impalcato	26, 27	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
205	Primo Impalcato	27, 29	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
206	Primo Impalcato	28, 30	0	0.00	0.00	0.00	0.00	0.00	0.00
			73	0.00	0.00	0.00	0.00	0.00	0.00
			146	0.00	0.00	0.00	0.00	0.00	0.00
207	Primo Impalcato	29, 31	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00

208	Primo Impalcato	30, 32	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			137	0.00	0.00	0.00	0.00	0.00	0.00
209	Primo Impalcato	31, 33	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
210	Primo Impalcato	32, 34	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
211	Primo Impalcato	33, 35	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
212	Primo Impalcato	34, 36	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
213	Primo Impalcato	35, 37	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
214	Primo Impalcato	36, 38	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
215	Primo Impalcato	37, 39	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
216	Primo Impalcato	38, 40	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			137	0.00	0.00	0.00	0.00	0.00	0.00
217	Primo Impalcato	39, 41	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
218	Primo Impalcato	40, 42	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
219	Primo Impalcato	41, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
220	Primo Impalcato	42, 43	0	0.00	0.00	0.00	0.00	0.00	0.00
			23	0.00	0.00	0.00	0.00	0.00	0.00
			46	0.00	0.00	0.00	0.00	0.00	0.00
221	Primo Impalcato	43, 45	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
222	Primo Impalcato	44, 46	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
223	Primo Impalcato	45, 47	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
224	Primo Impalcato	46, 48	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
225	Primo Impalcato	47, 49	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
226	Primo	48, 50	0	0.00	0.00	0.00	0.00	0.00	0.00

	Impalcato								
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
227	Primo Impalcato	49, 51	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
228	Primo Impalcato	50, 52	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
229	Primo Impalcato	51, 53	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
230	Primo Impalcato	52, 54	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
231	Primo Impalcato	53, 55	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
232	Primo Impalcato	54, 56	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
233	Primo Impalcato	55, 57	0	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
			159	0.00	0.00	0.00	0.00	0.00	0.00
234	Primo Impalcato	56, 70	0	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
			159	0.00	0.00	0.00	0.00	0.00	0.00
235	Primo Impalcato	57, 58	0	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
			166	0.00	0.00	0.00	0.00	0.00	0.00
236	Primo Impalcato	58, 59	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
237	Primo Impalcato	59, 60	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
238	Primo Impalcato	60, 61	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
239	Primo Impalcato	61, 62	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
240	Primo Impalcato	62, 63	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
241	Primo Impalcato	63, 64	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
242	Primo Impalcato	64, 65	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
243	Primo Impalcato	65, 66	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
244	Primo Impalcato	66, 67	0	0.00	0.00	0.00	0.00	0.00	0.00

			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
245	Primo Impalcato	67, 68	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
246	Primo Impalcato	68, 69	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
247	Primo Impalcato	69, 70	0	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
			166	0.00	0.00	0.00	0.00	0.00	0.00
248	Primo Impalcato	1	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
249	Primo Impalcato	2	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
250	Primo Impalcato	3	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
251	Primo Impalcato	4	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
252	Primo Impalcato	5	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
253	Primo Impalcato	6	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
254	Primo Impalcato	7	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
255	Primo Impalcato	8	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
256	Primo Impalcato	9	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
257	Primo Impalcato	10	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
258	Primo Impalcato	11	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
259	Primo Impalcato	12	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
260	Primo Impalcato	13	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
261	Primo Impalcato	14	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
262	Primo Impalcato	15	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00

			376	0.00	0.00	0.00	0.00	0.00	0.00
263	Primo Impalcato	16	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
264	Primo Impalcato	17	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
265	Primo Impalcato	18	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
266	Primo Impalcato	19	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
267	Primo Impalcato	20	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
268	Primo Impalcato	21	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
269	Primo Impalcato	22	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
270	Primo Impalcato	23	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
271	Primo Impalcato	24	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
272	Primo Impalcato	25	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
273	Primo Impalcato	26	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
274	Primo Impalcato	27	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
275	Primo Impalcato	28	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
276	Primo Impalcato	29	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
277	Primo Impalcato	30	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
278	Primo Impalcato	31	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
279	Primo Impalcato	32	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
280	Primo Impalcato	33	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00

281	Primo Impalcato	34	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
282	Primo Impalcato	35	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
283	Primo Impalcato	36	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
284	Primo Impalcato	37	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
285	Primo Impalcato	38	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
286	Primo Impalcato	39	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
287	Primo Impalcato	40	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
288	Primo Impalcato	41	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
289	Primo Impalcato	42	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
290	Primo Impalcato	43	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
291	Primo Impalcato	44	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
292	Primo Impalcato	45	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
293	Primo Impalcato	46	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
294	Primo Impalcato	47	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
295	Primo Impalcato	48	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
296	Primo Impalcato	49	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
297	Primo Impalcato	50	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
298	Primo Impalcato	51	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
299	Primo	52	0	0.00	0.00	0.00	0.00	0.00	0.00

	Impalcato								
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
300	Primo Impalcato	53	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
301	Primo Impalcato	54	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
302	Primo Impalcato	55	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
303	Primo Impalcato	56	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
304	Primo Impalcato	57	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
305	Primo Impalcato	58	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
306	Primo Impalcato	59	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
307	Primo Impalcato	60	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
308	Primo Impalcato	61	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
309	Primo Impalcato	62	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
310	Primo Impalcato	63	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
311	Primo Impalcato	64	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
312	Primo Impalcato	65	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
313	Primo Impalcato	66	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
314	Primo Impalcato	67	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
315	Primo Impalcato	68	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
316	Primo Impalcato	69	0	0.00	0.00	0.00	0.00	0.00	0.00
			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
317	Primo Impalcato	70	0	0.00	0.00	0.00	0.00	0.00	0.00

			188	0.00	0.00	0.00	0.00	0.00	0.00
			376	0.00	0.00	0.00	0.00	0.00	0.00
318	Fondazio ne	1, 71	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
319	Fondazio ne	1, 92	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
320	Primo Impalcato	92, 2	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
321	Fondazio ne	6, 89	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
322	Primo Impalcato	89, 7	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
323	Fondazio ne	9, 90	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
324	Primo Impalcato	90, 10	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
325	Fondazio ne	13, 91	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
326	Primo Impalcato	88, 14	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
327	Primo Impalcato	91, 14	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
328	Primo Impalcato	71, 15	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
329	Fondazio ne	16, 88	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
330	Fondazio ne	17, 72	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
331	Primo Impalcato	87, 18	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
332	Primo Impalcato	72, 19	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
333	Fondazio ne	20, 87	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
334	Fondazio ne	21, 73	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
335	Primo Impalcato	86, 22	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00

			199	0.00	0.00	0.00	0.00	0.00	0.00
336	Primo Impalcato	73, 23	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
337	Fondazio ne	24, 86	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
338	Fondazio ne	25, 74	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
339	Primo Impalcato	85, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
340	Fondazio ne	27, 85	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
341	Primo Impalcato	74, 28	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
342	Primo Impalcato	84, 29	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
343	Fondazio ne	31, 84	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
344	Primo Impalcato	83, 33	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
345	Fondazio ne	35, 83	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
346	Primo Impalcato	82, 37	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
347	Fondazio ne	39, 82	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
348	Primo Impalcato	78, 43	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
349	Primo Impalcato	81, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
350	Fondazio ne	45, 78	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
351	Fondazio ne	46, 81	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
352	Primo Impalcato	77, 47	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
353	Primo Impalcato	80, 48	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00

354	Fondazio ne	49, 77	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
355	Fondazio ne	50, 80	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
356	Primo Impalcato	76, 51	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
357	Fondazio ne	53, 76	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
358	Primo Impalcato	75, 55	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
359	Fondazio ne	56, 79	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
360	Fondazio ne	57, 75	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
361	Fondazio ne	57, 93	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
362	Primo Impalcato	93, 58	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
363	Fondazio ne	61, 95	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
364	Primo Impalcato	95, 62	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
365	Primo Impalcato	96, 65	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
366	Fondazio ne	66, 96	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
367	Fondazio ne	69, 94	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
368	Primo Impalcato	79, 70	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
369	Primo Impalcato	94, 70	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
370	Primo Impalcato	1, 71	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
371	Primo Impalcato	1, 92	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
372	Primo	92, 2	0	0.00	0.00	0.00	0.00	0.00	0.00

	Impalcato								
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
373	Primo Impalcato	6, 89	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
374	Primo Impalcato	89, 7	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
375	Primo Impalcato	9, 90	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
376	Primo Impalcato	90, 10	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
377	Primo Impalcato	13, 91	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
378	Primo Impalcato	88, 14	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
379	Primo Impalcato	91, 14	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
380	Primo Impalcato	71, 15	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
381	Primo Impalcato	16, 88	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
382	Primo Impalcato	17, 72	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
383	Primo Impalcato	87, 18	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
384	Primo Impalcato	72, 19	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
385	Primo Impalcato	20, 87	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
386	Primo Impalcato	21, 73	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
387	Primo Impalcato	86, 22	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
388	Primo Impalcato	73, 23	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
389	Primo Impalcato	24, 86	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
390	Primo Impalcato	25, 74	0	0.00	0.00	0.00	0.00	0.00	0.00

			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
391	Primo Impalcato	85, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
392	Primo Impalcato	27, 85	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
393	Primo Impalcato	74, 28	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
394	Primo Impalcato	84, 29	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
395	Primo Impalcato	31, 84	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
396	Primo Impalcato	83, 33	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
397	Primo Impalcato	35, 83	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
398	Primo Impalcato	82, 37	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
399	Primo Impalcato	39, 82	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
400	Primo Impalcato	78, 43	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
401	Primo Impalcato	81, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
402	Primo Impalcato	45, 78	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
403	Primo Impalcato	46, 81	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
404	Primo Impalcato	77, 47	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
405	Primo Impalcato	80, 48	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
406	Primo Impalcato	49, 77	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
407	Primo Impalcato	50, 80	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
408	Primo Impalcato	76, 51	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00

			199	0.00	0.00	0.00	0.00	0.00	0.00
409	Primo Impalcato	53, 76	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			199	0.00	0.00	0.00	0.00	0.00	0.00
410	Primo Impalcato	75, 55	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
411	Primo Impalcato	56, 79	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
412	Primo Impalcato	57, 75	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
413	Primo Impalcato	57, 93	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
414	Primo Impalcato	93, 58	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
415	Primo Impalcato	61, 95	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
416	Primo Impalcato	95, 62	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
417	Primo Impalcato	96, 65	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
418	Primo Impalcato	66, 96	0	0.00	0.00	0.00	0.00	0.00	0.00
			100	0.00	0.00	0.00	0.00	0.00	0.00
			200	0.00	0.00	0.00	0.00	0.00	0.00
419	Primo Impalcato	69, 94	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
420	Primo Impalcato	79, 70	0	0.00	0.00	0.00	0.00	0.00	0.00
			102	0.00	0.00	0.00	0.00	0.00	0.00
			204	0.00	0.00	0.00	0.00	0.00	0.00
421	Primo Impalcato	94, 70	0	0.00	0.00	0.00	0.00	0.00	0.00
			103	0.00	0.00	0.00	0.00	0.00	0.00
			206	0.00	0.00	0.00	0.00	0.00	0.00
422	Copertura	1, 2	0	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
			166	0.00	0.00	0.00	0.00	0.00	0.00
423	Copertura	15, 1	0	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
			159	0.00	0.00	0.00	0.00	0.00	0.00
424	Copertura	2, 3	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
425	Copertura	3, 4	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
426	Copertura	4, 5	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
427	Copertura	5, 6	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
428	Copertura	6, 7	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00

			138	0.00	0.00	0.00	0.00	0.00	0.00
429	Copertura	7, 8	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
430	Copertura	8, 9	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
431	Copertura	9, 10	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
432	Copertura	10, 11	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
433	Copertura	11, 12	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
434	Copertura	12, 13	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
435	Copertura	13, 14	0	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
			166	0.00	0.00	0.00	0.00	0.00	0.00
436	Copertura	16, 14	0	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
			159	0.00	0.00	0.00	0.00	0.00	0.00
437	Copertura	15, 17	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
438	Copertura	16, 18	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
439	Copertura	17, 19	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
440	Copertura	18, 20	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
441	Copertura	19, 21	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
442	Copertura	20, 22	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
443	Copertura	21, 23	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
444	Copertura	22, 24	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
445	Copertura	23, 25	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
446	Copertura	24, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
447	Copertura	25, 28	0	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
			170	0.00	0.00	0.00	0.00	0.00	0.00
448	Copertura	26, 27	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
449	Copertura	27, 29	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
450	Copertura	28, 30	0	0.00	0.00	0.00	0.00	0.00	0.00
			73	0.00	0.00	0.00	0.00	0.00	0.00
			146	0.00	0.00	0.00	0.00	0.00	0.00
451	Copertura	29, 31	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
452	Copertura	30, 32	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00

			137	0.00	0.00	0.00	0.00	0.00	0.00
453	Copertura	31, 33	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
454	Copertura	32, 34	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
455	Copertura	33, 35	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
456	Copertura	34, 36	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
457	Copertura	35, 37	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
458	Copertura	36, 38	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
459	Copertura	37, 39	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
460	Copertura	38, 40	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			137	0.00	0.00	0.00	0.00	0.00	0.00
461	Copertura	39, 41	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
462	Copertura	40, 42	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
463	Copertura	41, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
464	Copertura	42, 43	0	0.00	0.00	0.00	0.00	0.00	0.00
			23	0.00	0.00	0.00	0.00	0.00	0.00
			46	0.00	0.00	0.00	0.00	0.00	0.00
465	Copertura	43, 45	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
466	Copertura	44, 46	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
467	Copertura	45, 47	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
468	Copertura	46, 48	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
469	Copertura	47, 49	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
470	Copertura	48, 50	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
471	Copertura	49, 51	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
472	Copertura	50, 52	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
473	Copertura	51, 53	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
474	Copertura	52, 54	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
475	Copertura	53, 55	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
476	Copertura	54, 56	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00

			132	0.00	0.00	0.00	0.00	0.00	0.00
477	Copertura	55, 57	0	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
			159	0.00	0.00	0.00	0.00	0.00	0.00
478	Copertura	56, 70	0	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
			159	0.00	0.00	0.00	0.00	0.00	0.00
479	Copertura	57, 58	0	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
			166	0.00	0.00	0.00	0.00	0.00	0.00
480	Copertura	58, 59	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
481	Copertura	59, 60	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
482	Copertura	60, 61	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
483	Copertura	61, 62	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
484	Copertura	62, 63	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
485	Copertura	63, 64	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
486	Copertura	64, 65	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
487	Copertura	65, 66	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
488	Copertura	66, 67	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
489	Copertura	67, 68	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
490	Copertura	68, 69	0	0.00	0.00	0.00	0.00	0.00	0.00
			69	0.00	0.00	0.00	0.00	0.00	0.00
			138	0.00	0.00	0.00	0.00	0.00	0.00
491	Copertura	69, 70	0	0.00	0.00	0.00	0.00	0.00	0.00
			83	0.00	0.00	0.00	0.00	0.00	0.00
			166	0.00	0.00	0.00	0.00	0.00	0.00
492	Copertura	1	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
493	Copertura	2	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
494	Copertura	3	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
495	Copertura	4	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
496	Copertura	5	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
497	Copertura	6	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
498	Copertura	7	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
499	Copertura	8	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
500	Copertura	9	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00

			440	0.00	0.00	0.00	0.00	0.00	0.00
501	Copertura	10	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
502	Copertura	11	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
503	Copertura	12	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
504	Copertura	13	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
505	Copertura	57	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
506	Copertura	58	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
507	Copertura	59	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
508	Copertura	60	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
509	Copertura	61	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
510	Copertura	62	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
511	Copertura	63	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
512	Copertura	64	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
513	Copertura	65	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
514	Copertura	66	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
515	Copertura	67	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
516	Copertura	68	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
517	Copertura	69	0	0.00	0.00	0.00	0.00	0.00	0.00
			220	0.00	0.00	0.00	0.00	0.00	0.00
			440	0.00	0.00	0.00	0.00	0.00	0.00
518	Primo Impalcato	1, 74	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
519	Copertura	74, 2	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
520	Primo Impalcato	6, 71	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00
521	Copertura	71, 7	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00
522	Primo Impalcato	9, 72	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00
523	Copertura	72, 10	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00

524	Copertura	73, 13	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
525	Primo Impalcato	14, 73	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
526	Primo Impalcato	57, 75	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
527	Copertura	75, 58	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
528	Copertura	77, 61	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00
529	Primo Impalcato	62, 77	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00
530	Primo Impalcato	65, 78	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00
531	Copertura	78, 66	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00
532	Primo Impalcato	69, 76	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
533	Copertura	76, 70	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
534	Copertura	1, 74	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
535	Copertura	74, 2	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
536	Copertura	6, 71	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00
537	Copertura	71, 7	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00
538	Copertura	9, 72	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00
539	Copertura	72, 10	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00
540	Copertura	73, 13	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
541	Copertura	14, 73	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
542	Copertura	15, 125	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
543	Copertura	127, 16	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
544	Copertura	17, 129	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
545	Copertura	130, 18	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
546	Copertura	19, 135	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00

			150	0.00	0.00	0.00	0.00	0.00	0.00
547	Copertura	134, 20	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
548	Copertura	21, 136	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
549	Copertura	138, 22	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
550	Copertura	23, 141	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
551	Copertura	142, 24	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
552	Copertura	25, 145	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
553	Copertura	146, 26	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
554	Copertura	150, 27	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
555	Copertura	28, 149	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
556	Copertura	154, 29	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
557	Copertura	30, 153	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
558	Copertura	158, 31	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
559	Copertura	32, 157	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
560	Copertura	162, 33	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
561	Copertura	34, 161	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
562	Copertura	166, 35	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
563	Copertura	36, 165	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
564	Copertura	170, 37	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
565	Copertura	38, 169	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
566	Copertura	175, 39	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
567	Copertura	40, 173	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
568	Copertura	178, 41	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
569	Copertura	42, 177	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
570	Copertura	43, 181	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00

			150	0.00	0.00	0.00	0.00	0.00	0.00
571	Copertura	182, 44	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
572	Copertura	45, 185	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
573	Copertura	186, 46	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
574	Copertura	47, 189	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
575	Copertura	190, 48	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
576	Copertura	49, 193	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
577	Copertura	195, 50	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
578	Copertura	51, 197	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
579	Copertura	199, 52	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
580	Copertura	53, 201	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
581	Copertura	202, 54	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
582	Copertura	55, 205	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
583	Copertura	206, 56	0	0.00	0.00	0.00	0.00	0.00	0.00
			75	0.00	0.00	0.00	0.00	0.00	0.00
			150	0.00	0.00	0.00	0.00	0.00	0.00
584	Copertura	57, 75	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
585	Copertura	75, 58	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
586	Copertura	77, 61	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00
587	Copertura	62, 77	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00
588	Copertura	65, 78	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00
589	Copertura	78, 66	0	0.00	0.00	0.00	0.00	0.00	0.00
			115	0.00	0.00	0.00	0.00	0.00	0.00
			231	0.00	0.00	0.00	0.00	0.00	0.00
590	Copertura	69, 76	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
591	Copertura	76, 70	0	0.00	0.00	0.00	0.00	0.00	0.00
			118	0.00	0.00	0.00	0.00	0.00	0.00
			235	0.00	0.00	0.00	0.00	0.00	0.00
592	Copertura	79, 81	0	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
			159	0.00	0.00	0.00	0.00	0.00	0.00
593	Copertura	80, 82	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
594	Copertura	83, 84	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00

			132	0.00	0.00	0.00	0.00	0.00	0.00
595	Copertura	85, 86	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
596	Copertura	87, 88	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
597	Copertura	89, 90	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
598	Copertura	91, 92	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
599	Copertura	93, 94	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
600	Copertura	95, 96	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
601	Copertura	97, 106	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
602	Copertura	98, 99	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
603	Copertura	100, 101	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
604	Copertura	102, 103	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
605	Copertura	104, 105	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
606	Copertura	107, 108	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
607	Copertura	109, 110	0	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
			159	0.00	0.00	0.00	0.00	0.00	0.00
608	Copertura	111, 112	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
609	Copertura	113, 114	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
610	Copertura	115, 116	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
611	Copertura	117, 118	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
612	Copertura	119, 120	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
613	Copertura	121, 122	0	0.00	0.00	0.00	0.00	0.00	0.00
			66	0.00	0.00	0.00	0.00	0.00	0.00
			132	0.00	0.00	0.00	0.00	0.00	0.00
614	Copertura	124, 125	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
615	Copertura	125, 127	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00
			1550	0.00	0.00	0.00	0.00	0.00	0.00
616	Copertura	126, 127	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
617	Copertura	128, 129	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
618	Copertura	129, 130	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00

			1550	0.00	0.00	0.00	0.00	0.00	0.00
619	Copertura	131, 130	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
620	Copertura	132, 135	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
621	Copertura	133, 134	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
622	Copertura	135, 134	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00
			1550	0.00	0.00	0.00	0.00	0.00	0.00
623	Copertura	137, 136	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
624	Copertura	136, 138	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00
			1550	0.00	0.00	0.00	0.00	0.00	0.00
625	Copertura	139, 138	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
626	Copertura	140, 141	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
627	Copertura	141, 142	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00
			1550	0.00	0.00	0.00	0.00	0.00	0.00
628	Copertura	143, 142	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
629	Copertura	144, 145	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
630	Copertura	145, 146	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00
			1550	0.00	0.00	0.00	0.00	0.00	0.00
631	Copertura	147, 146	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
632	Copertura	148, 149	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
633	Copertura	149, 150	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00
			1550	0.00	0.00	0.00	0.00	0.00	0.00
634	Copertura	151, 150	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
635	Copertura	152, 153	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
636	Copertura	153, 154	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00
			1551	0.00	0.00	0.00	0.00	0.00	0.00
637	Copertura	155, 154	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
638	Copertura	156, 157	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
639	Copertura	157, 158	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00
			1551	0.00	0.00	0.00	0.00	0.00	0.00
640	Copertura	159, 158	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
641	Copertura	160, 161	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
642	Copertura	161, 162	0	0.00	0.00	0.00	0.00	0.00	0.00
			776	0.00	0.00	0.00	0.00	0.00	0.00

			1551	0.00	0.00	0.00	0.00	0.00	0.00
643	Copertura	163, 162	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
644	Copertura	164, 165	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
645	Copertura	165, 166	0	0.00	0.00	0.00	0.00	0.00	0.00
			776	0.00	0.00	0.00	0.00	0.00	0.00
			1551	0.00	0.00	0.00	0.00	0.00	0.00
646	Copertura	167, 166	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
647	Copertura	168, 169	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
648	Copertura	169, 170	0	0.00	0.00	0.00	0.00	0.00	0.00
			776	0.00	0.00	0.00	0.00	0.00	0.00
			1552	0.00	0.00	0.00	0.00	0.00	0.00
649	Copertura	171, 170	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
650	Copertura	172, 173	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
651	Copertura	173, 175	0	0.00	0.00	0.00	0.00	0.00	0.00
			776	0.00	0.00	0.00	0.00	0.00	0.00
			1552	0.00	0.00	0.00	0.00	0.00	0.00
652	Copertura	174, 175	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
653	Copertura	176, 177	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
654	Copertura	177, 178	0	0.00	0.00	0.00	0.00	0.00	0.00
			776	0.00	0.00	0.00	0.00	0.00	0.00
			1552	0.00	0.00	0.00	0.00	0.00	0.00
655	Copertura	179, 178	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
656	Copertura	180, 181	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
657	Copertura	181, 182	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00
			1550	0.00	0.00	0.00	0.00	0.00	0.00
658	Copertura	183, 182	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
659	Copertura	184, 185	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
660	Copertura	185, 186	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00
			1550	0.00	0.00	0.00	0.00	0.00	0.00
661	Copertura	187, 186	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
662	Copertura	188, 189	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
663	Copertura	189, 190	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00
			1550	0.00	0.00	0.00	0.00	0.00	0.00
664	Copertura	191, 190	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
665	Copertura	192, 193	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
666	Copertura	193, 195	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00

			1550	0.00	0.00	0.00	0.00	0.00	0.00
667	Copertura	194, 195	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
668	Copertura	196, 197	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
669	Copertura	197, 199	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00
			1550	0.00	0.00	0.00	0.00	0.00	0.00
670	Copertura	198, 199	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
671	Copertura	200, 201	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
672	Copertura	201, 202	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00
			1550	0.00	0.00	0.00	0.00	0.00	0.00
673	Copertura	203, 202	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
674	Copertura	204, 205	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
675	Copertura	205, 206	0	0.00	0.00	0.00	0.00	0.00	0.00
			775	0.00	0.00	0.00	0.00	0.00	0.00
			1550	0.00	0.00	0.00	0.00	0.00	0.00
676	Copertura	207, 206	0	0.00	0.00	0.00	0.00	0.00	0.00
			99	0.00	0.00	0.00	0.00	0.00	0.00
			198	0.00	0.00	0.00	0.00	0.00	0.00
677	Copertura	79	0	0.00	0.00	0.00	0.00	0.00	0.00
			125	0.00	0.00	0.00	0.00	0.00	0.00
			250	0.00	0.00	0.00	0.00	0.00	0.00
678	Copertura	124	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
679	Copertura	80	0	0.00	0.00	0.00	0.00	0.00	0.00
			45	0.00	0.00	0.00	0.00	0.00	0.00
			90	0.00	0.00	0.00	0.00	0.00	0.00
680	Copertura	128	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
681	Copertura	82	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
682	Copertura	132	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
683	Copertura	83	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
684	Copertura	137	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
685	Copertura	84	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
686	Copertura	140	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
687	Copertura	85	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
688	Copertura	144	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
689	Copertura	86	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
690	Copertura	87	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00

			85	0.00	0.00	0.00	0.00	0.00	0.00
691	Copertura	148	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
692	Copertura	88	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
693	Copertura	152	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
694	Copertura	89	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
695	Copertura	156	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
696	Copertura	90	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
697	Copertura	160	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
698	Copertura	91	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
699	Copertura	164	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
700	Copertura	92	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
701	Copertura	168	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
702	Copertura	93	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
703	Copertura	172	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
704	Copertura	94	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
705	Copertura	176	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
706	Copertura	180	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
707	Copertura	95	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
708	Copertura	184	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
709	Copertura	96	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
710	Copertura	188	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
711	Copertura	97	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
712	Copertura	192	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00
			310	0.00	0.00	0.00	0.00	0.00	0.00
713	Copertura	106	0	0.00	0.00	0.00	0.00	0.00	0.00
			43	0.00	0.00	0.00	0.00	0.00	0.00
			85	0.00	0.00	0.00	0.00	0.00	0.00
714	Copertura	196	0	0.00	0.00	0.00	0.00	0.00	0.00
			155	0.00	0.00	0.00	0.00	0.00	0.00

			130	0.00	0.00	0.00	0.00	0.00	0.00
763	Copertura	56	0	0.00	0.00	0.00	0.00	0.00	0.00
			65	0.00	0.00	0.00	0.00	0.00	0.00
			130	0.00	0.00	0.00	0.00	0.00	0.00
764	Copertura	70	0	0.00	0.00	0.00	0.00	0.00	0.00
			95	0.00	0.00	0.00	0.00	0.00	0.00
			190	0.00	0.00	0.00	0.00	0.00	0.00
765	Copertura	81	0	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
			160	0.00	0.00	0.00	0.00	0.00	0.00
766	Copertura	126	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
767	Copertura	98	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
768	Copertura	99	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
769	Copertura	100	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
770	Copertura	101	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
771	Copertura	102	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
772	Copertura	103	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
773	Copertura	104	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
774	Copertura	105	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
775	Copertura	111	0	0.00	0.00	0.00	0.00	0.00	0.00
			80	0.00	0.00	0.00	0.00	0.00	0.00
			160	0.00	0.00	0.00	0.00	0.00	0.00
776	Copertura	112	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
777	Copertura	113	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
778	Copertura	114	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
779	Copertura	115	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
780	Copertura	116	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
781	Copertura	117	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
782	Copertura	118	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
783	Copertura	131	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
784	Copertura	133	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
785	Copertura	139	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
786	Copertura	143	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00

			60	0.00	0.00	0.00	0.00	0.00	0.00
787	Copertura	147	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
788	Copertura	151	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
789	Copertura	155	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
790	Copertura	159	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
791	Copertura	119	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
792	Copertura	120	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
793	Copertura	121	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
794	Copertura	122	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
795	Copertura	123	0	0.00	0.00	0.00	0.00	0.00	0.00
			82	0.00	0.00	0.00	0.00	0.00	0.00
			165	0.00	0.00	0.00	0.00	0.00	0.00
796	Copertura	163	0	0.00	0.00	0.00	0.00	0.00	0.00
			33	0.00	0.00	0.00	0.00	0.00	0.00
			65	0.00	0.00	0.00	0.00	0.00	0.00
797	Copertura	167	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
798	Copertura	171	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
799	Copertura	174	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
800	Copertura	179	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
801	Copertura	183	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
802	Copertura	187	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
803	Copertura	191	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
804	Copertura	194	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
805	Copertura	198	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
806	Copertura	203	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00
807	Copertura	207	0	0.00	0.00	0.00	0.00	0.00	0.00
			30	0.00	0.00	0.00	0.00	0.00	0.00
			60	0.00	0.00	0.00	0.00	0.00	0.00

1.1.4.2 Piastre SLU

Tabella 8.I

Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
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1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

1.1.5 Risultati Condizioni (Torsione Accidentale X).

1.1.5.1 Sollecitazioni SLV

Tabella 9.I

Sollecitazioni									
Asta	Imp.	Fili	X [cm]	N [daN]	Mt [daNm]	Mxz [daNm]	Txz [daN]	Mxy [daNm]	Txy [daN]
1	Fondazione	1, 2	0	-128.39	-32.38	79.88	91.80	0.44	-11.45
			42	-119.52	-32.38	110.33	67.80	3.77	-4.67
			83	-110.72	-32.38	136.06	68.35	4.38	1.66
2	Fondazione	1, 2	0	-93.22	-36.09	114.28	127.73	4.32	-5.72
			42	-84.48	-36.10	169.30	148.54	5.45	0.21
			83	-75.79	-36.10	236.33	184.40	4.20	5.76
3	Fondazione	1, 15	0	68.04	56.87	-53.68	104.13	-8.06	-32.92
			40	61.82	56.86	-18.49	65.87	3.30	-24.27
			80	55.64	56.85	0.63	23.43	11.30	-16.05
4	Fondazione	1, 15	0	49.03	-22.97	-25.03	-42.19	11.24	9.07
			40	42.88	-22.98	-49.63	-88.38	6.07	16.90
			80	36.75	-22.99	-93.19	-137.27	-2.16	24.41
5	Fondazione	2, 3	0	-181.41	17.77	247.67	-258.00	3.91	-1.30
			35	-174.02	17.77	163.35	-221.60	3.67	2.66
			69	-166.70	17.76	92.03	-183.25	2.10	6.41
6	Fondazione	2, 3	0	-139.14	4.62	98.01	-117.72	2.06	0.29
			35	-131.88	4.61	62.49	-80.06	1.34	3.85
			69	-124.66	4.61	39.61	-44.74	-0.57	7.21
7	Fondazione	3, 4	0	-113.02	48.56	68.43	-122.16	-0.73	-7.10
			35	-105.86	48.56	30.46	-90.29	1.16	-3.92
			69	-98.73	48.56	2.78	-62.75	1.99	-0.92
8	Fondazione	3, 4	0	-84.54	7.12	20.88	-57.86	1.96	1.54
			35	-77.45	7.12	3.58	-35.06	0.94	4.36
			69	-70.39	7.12	-6.70	-17.19	-1.03	7.00
9	Fondazione	4, 5	0	-62.21	51.23	21.49	-80.51	-0.90	-5.92
			35	-55.18	51.23	-5.32	-67.60	0.71	-3.44
			69	-48.17	51.23	-28.54	-59.72	1.49	-1.13

10	Fondazio ne	4, 5	0	-33.56	11.27	-8.87	-55.10	1.46	1.64
			35	-26.56	11.27	-28.60	-51.97	0.52	3.78
			69	-19.58	11.27	-48.00	-53.13	-1.13	5.77
11	Fondazio ne	5, 6	0	-6.19	43.26	-20.58	-61.28	-0.92	-3.60
			35	0.79	43.26	-43.84	-66.05	0.00	-1.77
			69	7.77	43.26	-69.27	-73.68	0.32	-0.11
12	Fondazio ne	5, 6	0	34.81	-12.67	-58.82	-121.36	0.28	0.01
			35	41.79	-12.67	-103.67	-130.71	0.02	1.50
			69	48.80	-12.67	-151.81	-140.08	-0.74	2.84
13	Fondazio ne	6, 7	0	-40.87	-21.40	-155.74	262.47	-1.19	-4.09
			35	-33.86	-21.40	-67.89	255.58	0.01	-2.91
			69	-26.87	-21.40	18.34	253.32	0.83	-1.90
14	Fondazio ne	6, 7	0	12.57	-46.71	-7.42	261.15	0.80	1.42
			35	19.56	-46.71	81.64	264.11	0.16	2.27
			69	26.56	-46.72	172.52	271.44	-0.75	2.95
15	Fondazio ne	7, 8	0	-62.21	26.31	173.55	-192.45	0.15	-2.12
			35	-55.22	26.31	107.34	-183.20	0.79	-1.60
			69	-48.26	26.31	44.26	-174.77	1.27	-1.23
16	Fondazio ne	7, 8	0	-16.48	28.01	64.75	-120.25	1.24	2.67
			35	-9.53	28.01	22.99	-114.26	0.28	2.88
			69	-2.58	28.01	-17.24	-111.54	-0.73	2.94
17	Fondazio ne	8, 9	0	20.28	46.85	21.46	-118.80	-0.32	-0.15
			35	27.24	46.85	-20.94	-119.55	-0.26	-0.24
			69	34.20	46.85	-64.19	-123.65	-0.14	-0.49
18	Fondazio ne	8, 9	0	68.55	10.85	-41.58	-165.44	-0.16	2.36
			35	75.54	10.85	-101.14	-172.07	-0.92	1.96
			69	82.55	10.85	-163.23	-179.70	-1.50	1.40
19	Fondazio ne	9, 10	0	-12.84	-24.81	-165.37	265.36	-1.29	-2.18
			35	-5.81	-24.81	-76.36	259.31	-0.42	-2.91
			69	1.21	-24.81	11.19	257.17	0.74	-3.80
20	Fondazio ne	9, 10	0	44.48	-38.57	-10.86	244.66	0.70	3.15
			35	51.52	-38.58	72.43	247.16	-0.21	2.10
			69	58.58	-38.58	157.31	253.62	-0.73	0.87
21	Fondazio ne	10, 11	0	-32.22	5.52	160.16	-145.23	-0.26	0.14
			35	-25.16	5.52	110.04	-137.07	-0.07	-1.25
			69	-18.11	5.52	62.65	-129.81	0.62	-2.81
22	Fondazio ne	10, 11	0	11.35	34.33	73.36	-75.22	0.59	2.55
			35	18.40	34.33	46.88	-70.69	0.00	0.82
			69	25.46	34.33	21.32	-70.09	0.04	-1.07
23	Fondazio ne	11, 12	0	41.10	34.08	53.16	-96.99	0.44	4.11
			35	48.17	34.08	17.72	-101.12	-0.63	2.05
			69	55.26	34.08	-20.05	-110.59	-0.96	-0.18
24	Fondazio ne	11, 12	0	73.99	45.50	4.56	-104.69	-0.99	1.37
			35	81.11	45.50	-35.38	-119.54	-1.05	-1.03
			69	88.25	45.50	-81.34	-139.40	-0.26	-3.60
25	Fondazio ne	12, 13	0	104.76	23.10	-49.67	-90.81	-0.03	5.38
			35	111.94	23.10	-86.44	-114.59	-1.42	2.62
			69	119.17	23.10	-131.90	-140.83	-1.82	-0.32
26	Fondazio ne	12, 13	0	150.84	9.86	-120.66	-192.01	-1.85	4.58
			35	158.12	9.87	-192.97	-218.50	-2.90	1.45
			69	165.46	9.87	-274.02	-241.98	-2.83	-1.88
27	Fondazio ne	13, 14	0	61.57	-45.39	-272.57	180.99	-2.61	7.10
			42	70.24	-45.38	-203.34	163.12	-4.58	2.32
			83	78.94	-45.38	-137.85	164.21	-4.50	-2.79
28	Fondazio	13, 14	0	113.47	-56.31	-164.38	99.99	-4.55	3.75

	ne								
			42	122.24	-56.31	-120.10	126.32	-4.99	-1.74
			83	131.07	-56.31	-58.76	182.84	-3.05	-7.66
29	Fondazio ne	14, 16	0	-62.06	80.69	82.72	-220.95	-7.73	-31.91
			40	-56.67	80.68	7.50	-152.59	3.23	-23.33
			80	-51.31	80.66	-41.16	-87.43	10.87	-15.18
30	Fondazio ne	14, 16	0	-51.02	10.37	0.92	-22.79	10.81	7.95
			40	-45.69	10.36	3.25	39.45	6.09	15.73
			80	-40.38	10.35	29.78	98.88	-1.66	23.19
31	Fondazio ne	15, 17	0	107.63	80.08	-131.87	249.85	-2.55	-19.20
			33	102.57	80.07	-55.20	208.80	2.78	-13.20
			66	97.54	80.06	8.08	168.88	6.18	-7.42
32	Fondazio ne	15, 17	0	64.90	-30.84	-17.51	144.14	6.15	9.57
			33	59.91	-30.85	24.69	105.85	2.06	15.16
			66	54.93	-30.86	54.51	69.07	-3.84	20.57
33	Fondazio ne	16, 18	0	-98.35	82.75	74.25	-202.24	-2.36	-18.21
			33	-93.97	82.74	14.43	-155.43	2.66	-12.25
			66	-89.63	82.73	-30.40	-111.53	5.75	-6.49
34	Fondazio ne	16, 18	0	-69.34	-22.02	-5.61	-94.83	5.70	8.59
			33	-65.02	-22.03	-30.91	-53.77	1.94	14.16
			66	-60.73	-22.04	-43.08	-15.16	-3.63	19.56
35	Fondazio ne	17, 19	0	95.04	61.13	31.72	0.04	-5.51	-22.36
			33	90.09	61.12	26.79	-35.86	1.00	-17.13
			66	85.17	61.11	10.06	-71.46	5.81	-12.08
36	Fondazio ne	17, 19	0	53.98	-56.23	10.02	-86.99	5.78	12.79
			33	49.09	-56.23	-23.58	-122.61	0.75	17.67
			66	44.21	-56.24	-68.93	-158.12	-5.87	22.38
37	Fondazio ne	18, 20	0	-83.52	67.53	-20.86	-33.42	-5.45	-22.03
			33	-79.25	67.52	-26.63	3.34	0.96	-16.81
			66	-75.02	67.51	-20.50	38.74	5.67	-11.77
38	Fondazio ne	18, 20	0	-56.09	-49.06	-15.23	47.25	5.63	12.72
			33	-51.88	-49.07	5.23	81.70	0.62	17.59
			66	-47.69	-49.08	36.92	115.29	-5.96	22.30
39	Fondazio ne	19, 21	0	88.17	77.28	-82.88	181.40	-5.13	-20.83
			33	83.32	77.28	-27.80	146.78	0.99	-16.28
			66	78.50	77.27	16.12	113.91	5.64	-11.92
40	Fondazio ne	19, 21	0	50.95	-38.53	1.78	99.35	5.60	12.40
			33	46.15	-38.54	30.37	68.39	0.81	16.60
			66	41.37	-38.54	49.01	39.00	-5.34	20.65
41	Fondazio ne	20, 22	0	-76.05	77.37	53.26	-136.84	-5.23	-20.98
			33	-71.87	77.36	12.65	-104.46	0.94	-16.44
			66	-67.73	77.35	-17.53	-73.78	5.64	-12.06
42	Fondazio ne	20, 22	0	-50.84	-38.19	-4.86	-62.51	5.60	12.45
			33	-46.72	-38.20	-21.49	-33.52	0.79	16.66
			66	-42.61	-38.20	-28.78	-5.94	-5.38	20.72
43	Fondazio ne	21, 23	0	82.40	68.14	28.32	-1.23	-6.04	-20.77
			33	77.64	68.13	24.16	-29.68	0.16	-16.87
			66	72.92	68.13	10.68	-57.70	5.11	-13.15
44	Fondazio ne	21, 23	0	45.50	-41.40	6.18	-77.42	5.08	13.65
			33	40.79	-41.41	-23.04	-105.32	-0.02	17.21
			66	36.10	-41.41	-61.43	-132.95	-6.26	20.62
45	Fondazio ne	22, 24	0	-67.73	73.00	-11.92	-21.42	-6.09	-21.05
			33	-63.64	72.99	-15.40	5.14	0.21	-17.15
			66	-59.58	72.98	-10.24	30.98	5.24	-13.41
46	Fondazio ne	22, 24	0	-44.01	-35.29	-2.95	39.57	5.21	13.77

			33	-39.96	-35.30	13.49	64.89	0.06	17.36
			66	-35.93	-35.31	38.20	89.62	-6.23	20.79
47	Fondazio ne	23, 25	0	85.63	93.40	-90.80	207.32	-4.64	-16.20
			33	80.96	93.39	-25.89	180.72	0.16	-12.94
			66	76.31	93.39	30.54	156.02	3.92	-9.86
48	Fondazio ne	23, 25	0	52.88	9.68	4.97	145.56	3.88	11.29
			33	48.27	9.67	50.12	122.79	-0.33	14.21
			66	43.67	9.67	88.01	101.39	-5.48	16.98
49	Fondazio ne	24, 26	0	-65.38	86.71	58.50	-137.20	-4.59	-16.43
			33	-61.37	86.70	16.37	-113.52	0.28	-13.15
			66	-57.37	86.70	-18.20	-91.45	4.10	-10.04
50	Fondazio ne	24, 26	0	-45.30	3.04	0.42	-82.66	4.07	9.66
			33	-41.32	3.04	-24.24	-62.24	0.39	12.62
			66	-37.36	3.04	-42.40	-43.20	-4.24	15.42
51	Fondazio ne	25, 26	0	-26.56	-9.61	106.53	-26.18	-7.40	-16.23
			49	-22.60	-9.61	86.82	-48.85	-1.12	-9.64
			97	-18.66	-9.61	59.51	-58.24	2.06	-3.47
52	Fondazio ne	25, 26	0	-20.64	-4.57	65.92	-23.45	1.92	-3.35
			49	-16.72	-4.57	53.33	-23.83	2.13	2.43
			97	-12.81	-4.57	42.05	-18.60	-0.38	7.84
53	Fondazio ne	25, 26	0	-14.36	2.59	36.66	-21.74	-0.48	-5.31
			49	-10.46	2.59	27.20	-13.59	0.86	-0.26
			97	-6.57	2.59	22.04	-4.38	-0.17	4.43
54	Fondazio ne	25, 26	0	-10.54	2.88	16.31	-17.70	-0.26	-4.43
			49	-6.66	2.88	9.12	-8.77	0.82	-0.08
			97	-2.78	2.88	6.04	-0.90	-0.13	3.92
55	Fondazio ne	25, 26	0	-7.45	2.42	2.24	-8.83	-0.22	-3.71
			49	-3.57	2.42	-1.20	-2.40	0.68	-0.03
			97	0.30	2.42	-1.88	2.53	-0.13	3.31
56	Fondazio ne	25, 26	0	-5.38	1.59	-3.38	-2.62	-0.22	-3.09
			49	-1.51	1.59	-4.51	0.93	0.54	-0.07
			97	2.36	1.59	-4.22	3.29	-0.10	2.63
57	Fondazio ne	25, 26	0	-3.97	0.79	-4.42	0.86	-0.18	-2.44
			49	-0.10	0.79	-4.39	2.32	0.41	-0.06
			97	3.77	0.79	-3.82	3.10	-0.07	2.01
58	Fondazio ne	25, 26	0	-2.98	0.25	-3.45	2.28	-0.16	-1.82
			49	0.89	0.25	-3.01	2.64	0.28	-0.06
			97	4.76	0.25	-2.47	2.75	-0.05	1.40
59	Fondazio ne	25, 26	0	-2.26	-0.02	-1.95	2.48	-0.14	-1.25
			49	1.61	-0.02	-1.51	2.51	0.18	-0.10
			97	5.49	-0.02	-1.06	2.54	0.01	0.74
60	Fondazio ne	25, 26	0	-0.89	-0.06	-0.44	2.31	-0.11	-0.59
			49	2.98	-0.06	-0.07	2.43	0.03	-0.05
			97	6.86	-0.06	0.39	2.65	-0.01	0.18
61	Fondazio ne	25, 26	0	-0.46	0.04	0.92	2.27	-0.11	-0.04
			49	3.42	0.04	1.32	2.58	-0.09	-0.11
			97	7.30	0.04	1.89	2.92	0.05	-0.49
62	Fondazio ne	25, 26	0	0.47	0.37	2.39	2.52	-0.04	0.62
			49	4.35	0.37	2.91	2.80	-0.19	-0.06
			97	8.24	0.37	3.52	2.86	0.07	-1.05
63	Fondazio ne	25, 26	0	1.71	0.88	3.92	3.04	-0.01	1.24
			49	5.61	0.88	4.56	2.70	-0.31	-0.06
			97	9.50	0.88	4.89	1.72	0.10	-1.67
64	Fondazio ne	25, 26	0	3.32	1.45	4.84	3.30	0.02	1.86
			49	7.22	1.45	5.26	1.41	-0.43	-0.07

			97	11.13	1.45	4.47	-1.68	0.14	-2.31
65	Fondazio ne	25, 26	0	5.30	1.73	3.24	2.70	0.07	2.47
			49	9.21	1.73	2.72	-1.87	-0.53	-0.09
			97	13.14	1.73	-0.42	-8.10	0.20	-2.98
66	Fondazio ne	25, 26	0	7.77	1.14	-3.76	-0.08	0.13	3.14
			49	11.70	1.14	-6.45	-8.01	-0.63	-0.07
			97	15.63	1.14	-13.37	-17.40	0.26	-3.62
67	Fondazio ne	25, 26	0	10.72	-1.22	-20.30	-7.18	0.18	3.56
			49	14.67	-1.22	-27.06	-17.40	-0.62	-0.33
			97	18.63	-1.22	-38.75	-27.17	0.55	-4.55
68	Fondazio ne	25, 26	0	13.85	-7.41	-46.28	-5.97	0.47	5.77
			49	17.83	-7.41	-51.93	-13.37	-1.24	1.20
			97	21.81	-7.41	-60.07	-15.67	-0.64	-3.72
69	Fondazio ne	25, 26	0	20.13	-12.44	-65.05	-56.76	-0.72	-0.30
			49	24.14	-12.44	-92.43	-50.67	0.70	-5.59
			97	28.16	-12.44	-113.93	-31.67	4.78	-11.24
70	Fondazio ne	25, 28	0	98.54	29.39	45.73	-8.77	1.88	-3.98
			43	92.65	29.39	37.41	-36.04	2.85	-0.65
			85	86.82	29.38	17.27	-64.56	2.47	2.43
71	Fondazio ne	25, 28	0	55.11	-36.76	14.93	-78.50	2.43	5.09
			43	49.32	-36.76	-23.73	-109.30	-0.35	7.94
			85	43.56	-36.77	-75.97	-142.22	-4.29	10.56
72	Fondazio ne	26, 27	0	-56.77	40.72	-15.19	-4.25	0.74	-6.34
			33	-52.82	40.71	-14.36	13.91	2.39	-3.68
			66	-48.90	40.71	-7.63	31.53	3.19	-1.17
73	Fondazio ne	26, 27	0	-31.11	-24.94	-2.64	42.41	3.15	9.64
			33	-27.20	-24.94	13.43	59.66	-0.42	12.01
			66	-23.31	-24.94	35.13	76.47	-4.76	14.25
74	Fondazio ne	27, 29	0	-48.34	61.38	52.75	-109.74	-3.01	-11.13
			33	-44.46	61.38	18.42	-93.83	0.31	-9.04
			66	-40.59	61.37	-10.88	-79.34	2.97	-7.08
75	Fondazio ne	27, 29	0	-23.79	0.52	5.18	-75.97	2.93	7.28
			33	-19.94	0.52	-18.49	-63.02	0.23	9.09
			66	-16.08	0.51	-38.11	-51.45	-3.05	10.77
76	Fondazio ne	28, 30	0	115.60	54.61	-97.26	148.52	-2.55	-10.52
			37	110.69	54.60	-47.31	119.92	0.90	-8.45
			73	105.83	54.60	-7.60	92.65	3.64	-6.56
77	Fondazio ne	28, 30	0	84.91	6.03	-23.60	60.91	3.61	7.31
			37	80.09	6.03	-5.08	35.71	0.62	9.03
			73	75.31	6.03	4.67	12.89	-2.97	10.60
78	Fondazio ne	29, 31	0	-41.52	46.08	-18.72	10.11	-2.37	-8.37
			33	-37.68	46.07	-14.37	20.74	0.14	-6.83
			66	-33.86	46.07	-6.63	30.76	2.15	-5.43
79	Fondazio ne	29, 31	0	-17.01	2.56	1.43	32.63	2.12	5.54
			33	-13.19	2.56	13.03	42.21	0.08	6.79
			66	-9.38	2.56	27.70	51.24	-2.35	7.92
80	Fondazio ne	30, 32	0	68.51	56.58	-27.63	80.21	-1.91	-7.07
			34	64.05	56.58	-2.62	61.04	0.28	-5.75
			69	59.61	56.58	16.22	44.21	2.05	-4.58
81	Fondazio ne	30, 32	0	50.30	14.73	-3.72	41.88	2.02	5.02
			34	45.89	14.72	8.95	27.34	0.12	6.05
			69	41.50	14.72	17.01	14.96	-2.11	6.95
82	Fondazio ne	31, 33	0	-35.44	45.49	48.11	-95.24	-0.99	-4.46
			33	-31.64	45.49	17.29	-87.15	0.32	-3.48
			66	-27.84	45.49	-11.09	-80.48	1.32	-2.63

83	Fondazio ne	31, 33	0	-11.25	20.96	6.13	-76.90	1.29	3.34
			33	-7.46	20.96	-19.12	-71.76	0.06	4.05
			66	-3.68	20.96	-42.90	-67.99	-1.37	4.63
84	Fondazio ne	32, 34	0	40.30	44.81	-16.05	54.19	-1.08	-3.95
			35	35.89	44.81	1.67	43.75	0.15	-3.19
			69	31.49	44.81	16.14	35.37	1.14	-2.57
85	Fondazio ne	32, 34	0	23.95	22.32	-3.23	31.33	1.12	2.89
			35	19.56	22.32	7.29	24.90	0.03	3.36
			69	15.18	22.31	15.91	20.30	-1.19	3.70
86	Fondazio ne	33, 35	0	-29.48	27.80	-23.54	26.53	-0.48	-1.95
			33	-25.70	27.80	-15.05	29.41	0.09	-1.50
			66	-21.93	27.80	-5.69	31.78	0.53	-1.20
87	Fondazio ne	33, 35	0	-5.28	19.59	2.58	32.14	0.50	1.35
			33	-1.52	19.59	12.77	34.16	0.02	1.52
			66	2.24	19.59	23.57	35.71	-0.50	1.56
88	Fondazio ne	34, 36	0	16.24	34.85	-13.94	32.95	-0.20	-0.85
			35	11.87	34.85	-2.25	30.05	0.05	-0.65
			69	7.50	34.85	8.74	28.91	0.26	-0.60
89	Fondazio ne	34, 36	0	1.67	31.63	-8.00	29.09	0.23	0.87
			35	-2.70	31.63	2.96	29.69	-0.06	0.79
			69	-7.06	31.63	14.43	32.05	-0.30	0.56
90	Fondazio ne	35, 37	0	-23.58	26.76	43.20	-77.99	0.50	1.33
			33	-19.82	26.76	16.86	-77.26	0.08	1.23
			66	-16.07	26.76	-9.43	-77.79	-0.29	0.99
91	Fondazio ne	35, 37	0	-0.18	36.78	6.67	-76.31	-0.33	-0.42
			33	3.56	36.78	-19.54	-78.24	-0.13	-0.79
			66	7.31	36.78	-46.60	-81.38	0.21	-1.29
92	Fondazio ne	36, 38	0	-6.49	26.98	-14.79	18.98	0.67	2.29
			35	-10.86	26.98	-6.72	23.00	-0.06	1.92
			69	-15.23	26.98	3.04	28.82	-0.64	1.42
93	Fondazio ne	36, 38	0	-21.43	42.70	-14.42	31.69	-0.68	-1.05
			35	-25.81	42.70	-1.34	39.39	-0.21	-1.70
			69	-30.20	42.70	14.74	49.08	0.51	-2.49
94	Fondazio ne	37, 39	0	-19.43	7.94	-29.13	48.56	1.39	4.50
			33	-15.69	7.94	-14.48	44.70	0.01	3.86
			66	-11.94	7.94	-1.16	40.53	-1.14	3.09
95	Fondazio ne	37, 39	0	3.27	34.44	6.16	38.81	-1.17	-3.19
			33	7.01	34.44	17.51	34.46	0.02	-4.09
			66	10.76	34.44	27.36	29.72	1.54	-5.14
96	Fondazio ne	38, 40	0	-29.85	22.39	-16.51	12.52	1.50	5.35
			34	-34.23	22.39	-9.43	24.09	-0.18	4.43
			69	-38.61	22.39	1.98	37.77	-1.52	3.36
97	Fondazio ne	38, 40	0	-46.43	56.26	-18.11	43.70	-1.55	-2.90
			34	-50.83	56.27	0.40	59.63	-0.36	-4.11
			69	-55.25	56.27	24.77	77.90	1.28	-5.46
98	Fondazio ne	39, 41	0	-16.61	6.86	44.83	-49.89	2.28	7.35
			33	-12.87	6.86	26.74	-55.43	0.05	6.17
			66	-9.13	6.86	6.60	-62.35	-1.78	4.86
99	Fondazio ne	39, 41	0	3.38	56.43	22.51	-51.56	-1.81	-4.96
			33	7.12	56.43	3.37	-60.20	0.06	-6.40
			66	10.86	56.44	-18.93	-70.76	2.43	-7.98
100	Fondazio ne	40, 42	0	-56.81	17.33	-11.07	19.08	2.33	8.81
			35	-61.29	17.33	-0.09	39.75	-0.46	7.31
			69	-65.78	17.33	18.41	62.71	-2.70	5.66
101	Fondazio	40, 42	0	-78.75	69.52	-5.31	85.34	-2.72	-4.69

	ne								
			35	-83.28	69.53	29.31	110.46	-0.80	-6.49
			69	-87.84	69.53	72.94	137.43	1.77	-8.45
102	Fondazio ne	41, 44	0	19.36	-0.06	4.90	-18.55	3.41	10.96
			33	23.10	-0.06	-3.97	-30.96	0.07	9.25
			66	26.85	-0.06	-17.23	-45.18	-2.68	7.41
103	Fondazio ne	41, 44	0	39.85	45.90	-2.56	-65.13	-2.71	0.07
			33	43.62	45.90	-27.38	-81.00	-2.42	-1.90
			66	47.40	45.91	-57.68	-98.22	-1.45	-4.01
104	Fondazio ne	42, 43	0	-93.95	-3.02	40.36	40.23	2.91	18.18
			23	-97.01	-3.02	52.36	58.78	-1.11	16.79
			46	-100.08	-3.02	68.64	77.44	-4.81	15.32
105	Fondazio ne	43, 44	0	29.07	-0.06	-86.68	-28.68	-7.28	-15.43
			49	25.92	-0.07	-91.98	1.19	-1.32	-9.08
			97	22.78	-0.07	-86.75	15.55	1.62	-3.09
106	Fondazio ne	43, 44	0	18.54	-0.57	-71.86	18.25	1.53	-3.24
			49	15.42	-0.57	-61.07	22.06	1.72	2.37
			97	12.32	-0.57	-50.19	19.27	-0.73	7.64
107	Fondazio ne	43, 44	0	12.20	1.89	-38.82	21.24	-0.82	-5.47
			49	9.11	1.89	-29.30	14.92	0.63	-0.54
			97	6.01	1.89	-23.28	7.14	-0.24	4.06
108	Fondazio ne	43, 44	0	7.11	2.66	-16.22	15.72	-0.38	-4.29
			49	4.02	2.66	-9.87	7.90	0.66	-0.03
			97	0.94	2.66	-7.16	0.84	-0.30	3.91
109	Fondazio ne	43, 44	0	4.55	2.60	-3.06	8.66	-0.40	-3.77
			49	1.47	2.59	0.29	2.81	0.54	-0.16
			97	-1.61	2.59	1.12	-1.72	-0.20	3.14
110	Fondazio ne	43, 44	0	2.65	1.85	2.77	2.80	-0.29	-3.08
			49	-0.43	1.85	3.90	-0.48	0.47	-0.10
			97	-3.51	1.85	3.70	-2.69	-0.14	2.56
111	Fondazio ne	43, 44	0	1.32	1.02	3.95	-0.51	-0.23	-2.45
			49	-1.76	1.02	3.96	-1.87	0.38	-0.09
			97	-4.84	1.02	3.46	-2.61	-0.09	1.95
112	Fondazio ne	43, 44	0	0.41	0.40	3.15	-1.88	-0.18	-1.83
			49	-2.67	0.40	2.76	-2.20	0.28	-0.09
			97	-5.76	0.40	2.28	-2.29	-0.04	1.34
113	Fondazio ne	43, 44	0	-0.22	0.06	1.83	-2.13	-0.13	-1.20
			49	-3.30	0.06	1.41	-2.12	0.17	-0.07
			97	-6.39	0.06	1.00	-2.11	-0.01	0.76
114	Fondazio ne	43, 44	0	-0.56	-0.06	0.55	-2.03	-0.10	-0.65
			49	-3.65	-0.06	0.17	-2.07	0.07	-0.11
			97	-6.74	-0.06	-0.24	-2.20	0.06	0.12
115	Fondazio ne	43, 44	0	-1.37	0.08	-0.67	-1.87	-0.05	-0.01
			49	-4.47	0.08	-1.01	-2.09	-0.04	-0.08
			97	-7.57	0.08	-1.47	-2.34	0.07	-0.44
116	Fondazio ne	43, 44	0	-1.87	0.38	-1.90	-2.04	-0.01	0.58
			49	-4.98	0.38	-2.33	-2.25	-0.14	-0.08
			97	-8.09	0.38	-2.83	-2.31	0.12	-1.04
117	Fondazio ne	43, 44	0	-2.59	0.88	-3.18	-2.37	0.03	1.18
			49	-5.70	0.88	-3.67	-2.13	-0.25	-0.08
			97	-8.82	0.88	-3.93	-1.38	0.16	-1.65
118	Fondazio ne	43, 44	0	-3.51	1.45	-3.86	-2.61	0.08	1.78
			49	-6.64	1.45	-4.19	-1.15	-0.34	-0.09
			97	-9.77	1.45	-3.58	1.26	0.22	-2.27
119	Fondazio ne	43, 44	0	-4.63	1.77	-2.43	-2.20	0.13	2.37

			49	-7.76	1.77	-2.06	1.37	-0.43	-0.11
			97	-10.90	1.77	0.37	6.26	0.29	-2.91
120	Fondazio ne	43, 44	0	-5.89	1.10	3.52	-0.27	0.20	3.04
			49	-9.04	1.10	5.48	5.95	-0.53	-0.07
			97	-12.19	1.10	10.76	13.28	0.32	-3.50
121	Fondazio ne	43, 44	0	-7.23	-1.01	17.46	5.40	0.23	3.33
			49	-10.39	-1.01	22.64	13.32	-0.49	-0.42
			97	-13.56	-1.01	31.62	20.77	0.69	-4.49
122	Fondazio ne	43, 44	0	-9.02	-4.61	41.90	9.56	0.59	5.65
			49	-12.20	-4.61	48.62	14.88	-1.11	1.25
			97	-15.39	-4.61	56.93	15.61	-0.58	-3.48
123	Fondazio ne	43, 44	0	-14.49	-11.99	67.19	19.60	-0.70	0.41
			49	-17.69	-11.99	76.07	12.59	0.32	-4.67
			97	-20.91	-11.99	78.86	-6.15	3.90	-10.09
124	Fondazio ne	43, 45	0	-56.68	-23.11	51.85	-138.51	4.20	14.48
			33	-61.12	-23.10	11.40	-112.21	-0.22	12.26
			66	-65.58	-23.10	-20.54	-86.92	-3.88	9.90
125	Fondazio ne	43, 45	0	-90.57	57.56	-12.67	-75.31	-3.91	-10.24
			33	-95.06	57.57	-32.59	-50.98	-0.12	-12.75
			66	-99.58	57.57	-44.58	-27.19	4.53	-15.42
126	Fondazio ne	44, 46	0	21.65	-2.36	-30.00	64.30	4.06	13.68
			33	25.45	-2.35	-12.49	46.38	-0.08	11.42
			66	29.25	-2.35	-0.94	28.18	-3.46	9.02
127	Fondazio ne	44, 46	0	43.37	70.60	11.75	16.13	-3.49	-9.27
			33	47.18	70.61	13.28	-2.27	-0.01	-11.82
			66	51.01	70.61	8.69	-21.04	4.33	-14.52
128	Fondazio ne	45, 47	0	-45.31	-20.83	-70.50	72.18	4.79	17.23
			33	-49.86	-20.82	-41.84	96.18	-0.43	14.42
			66	-54.42	-20.82	-5.08	121.28	-4.71	11.46
129	Fondazio ne	45, 47	0	-81.95	74.66	-24.10	138.24	-4.74	-10.59
			33	-86.54	74.67	26.80	164.93	-0.73	-13.70
			66	-91.16	74.67	86.76	193.10	4.32	-16.97
130	Fondazio ne	46, 48	0	17.02	-20.17	36.08	-46.26	4.57	15.86
			33	20.86	-20.17	16.86	-65.69	-0.20	13.01
			66	24.72	-20.16	-8.93	-86.15	-4.00	10.01
131	Fondazio ne	46, 48	0	39.91	76.95	13.22	-85.85	-4.03	-8.78
			33	43.77	76.96	-19.42	-107.48	-0.62	-11.92
			66	47.65	76.96	-59.38	-130.17	3.85	-15.22
132	Fondazio ne	47, 49	0	-44.51	-44.57	60.03	-136.72	5.94	20.26
			33	-49.16	-44.56	20.60	-107.90	-0.19	16.83
			66	-53.82	-44.55	-9.33	-79.16	-5.15	13.25
133	Fondazio ne	47, 49	0	-80.06	62.15	-9.51	-70.08	-5.19	-12.89
			33	-84.75	62.15	-26.99	-41.53	-0.33	-16.62
			66	-89.47	62.16	-35.03	-12.83	5.79	-20.51
134	Fondazio ne	48, 50	0	15.33	-44.38	-42.03	98.43	5.48	19.05
			33	19.22	-44.37	-14.14	75.29	-0.24	15.61
			66	23.12	-44.36	6.11	52.19	-4.80	12.01
135	Fondazio ne	48, 50	0	37.03	65.80	12.25	39.13	-4.83	-12.63
			33	40.94	65.80	20.58	16.13	-0.05	-16.37
			66	44.86	65.81	21.31	-7.05	5.99	-20.28
136	Fondazio ne	49, 51	0	-47.97	-40.20	-52.55	41.08	5.14	20.27
			33	-52.71	-40.20	-33.22	70.51	-0.89	16.22
			66	-57.47	-40.19	-3.96	101.38	-5.55	12.02
137	Fondazio ne	49, 51	0	-85.01	74.50	-17.17	115.02	-5.59	-11.56
			33	-89.80	74.50	27.08	147.69	-1.06	-15.92

			66	-94.62	74.51	82.41	182.03	4.94	-20.46
138	Fondazio ne	50, 52	0	14.84	-44.27	35.86	4.84	5.37	20.04
			33	18.77	-44.27	32.77	-18.93	-0.58	15.98
			66	22.71	-44.26	21.66	-43.87	-5.16	11.78
139	Fondazio ne	50, 52	0	33.10	80.16	34.74	-46.65	-5.19	-12.29
			33	37.05	80.17	14.22	-73.28	-0.42	-16.64
			66	41.01	80.17	-15.43	-101.99	5.81	-21.16
140	Fondazio ne	51, 53	0	-49.79	-59.03	66.30	-156.08	5.70	22.12
			33	-54.63	-59.02	21.56	-120.92	-0.83	17.42
			66	-59.50	-59.01	-11.56	-85.67	-5.78	12.55
141	Fondazio ne	51, 53	0	-89.40	57.63	-9.68	-74.53	-5.82	-11.96
			33	-94.29	57.64	-27.49	-39.31	-1.04	-17.00
			66	-99.22	57.65	-33.63	-3.78	5.42	-22.22
142	Fondazio ne	52, 54	0	46.52	-37.28	7.12	39.88	5.59	21.58
			33	50.50	-37.27	14.46	8.99	-0.77	16.91
			66	54.49	-37.26	11.21	-24.24	-5.56	12.09
143	Fondazio ne	52, 54	0	63.45	81.02	27.76	-39.25	-5.59	-10.96
			33	67.47	81.03	8.17	-75.09	-1.16	-15.94
			66	71.52	81.04	-23.72	-113.82	4.95	-21.09
144	Fondazio ne	53, 55	0	-58.96	-29.54	-54.86	67.96	3.76	20.60
			33	-63.92	-29.54	-25.47	104.39	-2.15	15.19
			66	-68.90	-29.53	16.20	142.37	-6.24	9.60
145	Fondazio ne	53, 55	0	-99.35	75.84	-4.39	160.79	-6.29	-8.03
			33	-104.36	75.85	56.17	200.45	-2.69	-13.81
			66	-109.41	75.85	130.04	241.26	2.85	-19.80
146	Fondazio ne	54, 56	0	78.36	-20.21	5.86	20.63	4.10	20.42
			33	82.43	-20.20	5.07	-20.95	-1.76	15.11
			66	86.53	-20.19	-9.92	-65.44	-5.85	9.63
147	Fondazio ne	54, 56	0	101.77	80.19	15.62	-102.13	-5.88	-6.64
			33	105.91	80.20	-26.65	-149.55	-2.77	-12.29
			66	110.08	80.21	-85.04	-199.71	2.25	-18.15
148	Fondazio ne	55, 57	0	-38.46	-20.90	91.54	-135.14	2.43	25.16
			40	-44.57	-20.89	48.77	-86.52	-6.09	17.66
			80	-50.71	-20.88	24.87	-40.51	-11.57	9.84
149	Fondazio ne	55, 57	0	-62.11	49.84	1.99	20.89	-11.63	-16.19
			40	-68.28	49.85	20.07	63.22	-3.58	-24.40
			80	-74.48	49.86	54.18	101.38	7.83	-33.04
150	Fondazio ne	56, 70	0	45.08	5.20	-42.36	118.73	1.50	22.55
			40	50.14	5.21	-8.61	55.77	-6.02	15.24
			80	55.23	5.22	-0.31	-9.20	-10.58	7.62
151	Fondazio ne	56, 70	0	54.54	77.34	36.38	-77.51	-10.64	-14.79
			40	59.66	77.36	-8.69	-144.50	-3.18	-22.77
			80	64.81	77.37	-80.85	-213.72	7.52	-31.16
152	Fondazio ne	57, 58	0	130.82	-29.69	-84.21	-78.10	0.10	-12.58
			42	121.96	-29.69	-108.92	-53.67	3.90	-5.82
			83	113.16	-29.70	-128.51	-52.74	5.00	0.49
153	Fondazio ne	57, 58	0	88.05	-31.07	-117.52	-118.68	4.94	-4.70
			42	79.31	-31.08	-168.31	-137.05	5.65	1.21
			83	70.62	-31.08	-229.89	-169.52	3.98	6.74
154	Fondazio ne	58, 59	0	181.12	20.61	-240.04	240.97	3.71	-1.72
			35	173.73	20.61	-161.01	208.02	3.61	2.22
			69	166.41	20.61	-93.72	173.63	2.20	5.96
155	Fondazio ne	58, 59	0	136.35	4.48	-105.01	126.03	2.16	0.29
			35	129.08	4.47	-65.87	92.84	1.44	3.83
			69	121.87	4.47	-37.72	62.57	-0.46	7.18

156	Fondazio ne	59, 60	0	106.48	52.99	-66.74	139.43	-0.68	-6.88
			35	99.31	52.99	-21.86	113.22	1.14	-3.71
			69	92.18	52.98	14.79	91.83	1.91	-0.73
157	Fondazio ne	59, 60	0	74.76	8.11	-6.64	88.11	1.88	1.91
			35	67.67	8.10	22.20	71.71	0.73	4.71
			69	60.60	8.10	46.21	60.06	-1.36	7.35
158	Fondazio ne	60, 61	0	45.21	45.28	21.33	85.36	-1.26	-5.49
			35	38.16	45.28	50.78	77.84	0.20	-3.03
			69	31.12	45.28	78.23	73.62	0.85	-0.74
159	Fondazio ne	60, 61	0	7.00	-20.43	68.11	116.49	0.81	0.15
			35	-0.02	-20.43	109.28	114.28	0.39	2.27
			69	-7.05	-20.43	149.79	112.22	-0.73	4.23
160	Fondazio ne	61, 62	0	78.31	-20.87	156.44	-241.08	-1.42	-5.61
			35	71.30	-20.87	74.01	-245.54	0.20	-3.82
			69	64.31	-20.88	-10.71	-254.62	1.24	-2.21
161	Fondazio ne	61, 62	0	28.30	-55.03	17.56	-262.49	1.20	1.57
			35	21.33	-55.04	-73.94	-276.94	0.41	3.02
			69	14.38	-55.04	-171.28	-296.08	-0.86	4.30
162	Fondazio ne	62, 63	0	104.58	23.99	-168.58	179.35	0.18	-3.27
			35	97.65	23.99	-109.00	157.87	1.11	-2.15
			69	90.75	23.99	-56.84	136.74	1.68	-1.18
163	Fondazio ne	62, 63	0	63.94	21.17	-70.92	75.73	1.64	2.30
			35	57.08	21.17	-46.78	56.71	0.71	3.11
			69	50.23	21.16	-28.67	40.98	-0.48	3.76
164	Fondazio ne	63, 64	0	34.90	57.02	-62.31	118.12	-0.09	-1.48
			35	28.08	57.02	-22.33	106.53	0.32	-0.97
			69	21.26	57.01	14.47	99.81	0.59	-0.61
165	Fondazio ne	63, 64	0	2.84	35.19	-13.19	97.80	0.56	1.96
			35	-3.97	35.19	21.47	96.13	-0.16	2.18
			69	-10.78	35.19	56.41	99.32	-0.93	2.25
166	Fondazio ne	64, 65	0	-26.08	44.72	22.26	61.18	-0.48	0.12
			35	-32.90	44.72	45.90	68.57	-0.52	0.05
			69	-39.73	44.72	72.69	79.37	-0.50	-0.18
167	Fondazio ne	64, 65	0	-66.83	4.36	57.61	136.67	-0.53	0.71
			35	-73.69	4.36	108.33	149.69	-0.72	0.33
			69	-80.57	4.36	163.70	163.17	-0.74	-0.20
168	Fondazio ne	65, 66	0	10.45	-30.28	165.05	-275.65	-0.51	0.07
			35	3.55	-30.28	73.39	-264.35	-0.42	-0.62
			69	-3.34	-30.28	-15.11	-257.52	-0.07	-1.47
169	Fondazio ne	65, 66	0	-39.99	-37.07	10.71	-254.39	-0.10	0.71
			35	-46.89	-37.07	-75.23	-252.73	-0.18	-0.30
			69	-53.82	-37.07	-161.41	-255.48	0.12	-1.47
170	Fondazio ne	66, 67	0	33.25	5.30	-157.33	136.49	0.59	1.81
			35	26.32	5.30	-109.68	131.60	0.20	0.47
			69	19.40	5.30	-63.70	127.19	0.29	-1.03
171	Fondazio ne	66, 67	0	-6.94	32.68	-74.84	75.70	0.25	1.78
			35	-13.85	32.68	-47.80	73.61	-0.08	0.12
			69	-20.77	32.68	-20.89	75.04	0.19	-1.70
172	Fondazio ne	67, 68	0	-35.32	32.54	-50.21	88.18	0.58	4.07
			35	-42.25	32.54	-17.55	93.95	-0.48	2.09
			69	-49.20	32.54	17.94	104.63	-0.84	-0.05
173	Fondazio ne	67, 68	0	-67.41	44.71	-4.51	101.39	-0.87	1.24
			35	-74.38	44.71	34.42	117.07	-0.91	-1.06
			69	-81.38	44.72	79.58	137.35	-0.12	-3.53
174	Fondazio	68, 69	0	-97.52	23.00	50.02	85.42	0.10	5.62

	ne								
			35	-104.56	23.00	84.92	109.26	-1.39	2.99
			69	-111.63	23.00	128.47	135.21	-1.94	0.18
175	Fondazio ne	68, 69	0	-142.10	10.29	118.18	186.00	-1.98	3.57
			35	-149.22	10.29	188.28	211.89	-2.70	0.58
			69	-156.41	10.29	266.89	234.56	-2.36	-2.61
176	Fondazio ne	69, 70	0	-59.94	-42.17	262.34	-167.42	-2.11	8.06
			42	-68.42	-42.17	198.49	-150.63	-4.52	3.49
			83	-76.94	-42.17	137.95	-152.69	-4.96	-1.41
177	Fondazio ne	69, 70	0	-111.17	-51.37	163.23	-97.05	-5.02	2.65
			42	-119.74	-51.37	119.96	-124.13	-5.04	-2.62
			83	-128.38	-51.37	59.39	-181.16	-2.79	-8.28
178	Primo Impalcato	1, 2	0	-24.64	-6.90	256.92	-111.32	34.68	47.51
			83	-24.64	-6.90	164.39	-111.32	-4.82	47.51
			166	-24.64	-6.90	71.85	-111.32	-44.31	47.51
179	Primo Impalcato	1, 15	0	88.96	-3.29	-377.88	312.53	-29.80	-11.67
			80	88.96	-3.29	-129.42	312.53	-20.52	-11.67
			159	88.96	-3.29	119.03	312.53	-11.25	-11.67
180	Primo Impalcato	2, 3	0	1.48	-0.30	95.09	-103.75	-41.18	-14.73
			69	1.48	-0.30	23.50	-103.75	-31.01	-14.73
			138	1.48	-0.30	-48.09	-103.75	-20.84	-14.73
181	Primo Impalcato	3, 4	0	2.75	0.25	-21.01	9.88	-20.69	-11.37
			69	2.75	0.25	-14.19	9.88	-12.84	-11.37
			138	2.75	0.25	-7.38	9.88	-5.00	-11.37
182	Primo Impalcato	4, 5	0	3.84	0.69	18.73	9.94	-5.10	-2.55
			69	3.84	0.69	25.59	9.94	-3.34	-2.55
			138	3.84	0.69	32.46	9.94	-1.59	-2.55
183	Primo Impalcato	5, 6	0	4.98	1.16	60.94	-172.42	-1.55	0.86
			69	4.98	1.16	-58.03	-172.42	-2.14	0.86
			138	4.98	1.16	-177.00	-172.42	-2.73	0.86
184	Primo Impalcato	6, 7	0	12.21	1.65	-154.47	223.40	-3.12	0.77
			69	12.21	1.65	-0.32	223.40	-3.65	0.77
			138	12.21	1.65	153.83	223.40	-4.18	0.77
185	Primo Impalcato	7, 8	0	18.37	2.09	176.34	-138.50	-3.27	-0.54
			69	18.37	2.09	80.77	-138.50	-2.90	-0.54
			138	18.37	2.09	-14.80	-138.50	-2.53	-0.54
186	Primo Impalcato	8, 9	0	19.70	2.33	15.72	-139.23	-2.02	-0.82
			69	19.70	2.33	-80.35	-139.23	-1.45	-0.82
			138	19.70	2.33	-176.42	-139.23	-0.89	-0.82
187	Primo Impalcato	9, 10	0	21.41	2.36	-153.83	222.60	-0.63	-0.49
			69	21.41	2.36	-0.23	222.60	-0.29	-0.49
			138	21.41	2.36	153.36	222.60	0.05	-0.49
188	Primo Impalcato	10, 11	0	35.90	2.19	175.94	-173.19	0.52	-1.85
			69	35.90	2.19	56.44	-173.19	1.79	-1.85
			138	35.90	2.19	-63.06	-173.19	3.07	-1.85
189	Primo Impalcato	11, 12	0	37.16	1.73	-34.71	38.80	3.36	-6.08
			69	37.16	1.73	-7.94	38.80	7.56	-6.08
			138	37.16	1.73	18.84	38.80	11.75	-6.08
190	Primo Impalcato	12, 13	0	38.46	1.05	46.25	-103.40	12.01	-8.96
			69	38.46	1.05	-25.10	-103.40	18.19	-8.96
			138	38.46	1.05	-96.45	-103.40	24.37	-8.96
191	Primo Impalcato	13, 14	0	48.16	-2.72	-72.76	-100.30	25.29	12.99
			83	48.16	-2.72	-156.13	-100.30	14.49	12.99
			166	48.16	-2.72	-239.50	-100.30	3.70	12.99
192	Primo Impalcato	14, 16	0	21.98	-3.13	162.05	-138.32	4.90	9.17

			80	21.98	-3.13	52.09	-138.32	-2.39	9.17
			159	21.98	-3.13	-57.88	-138.32	-9.68	9.17
193	Primo Impalcato	15, 17	0	42.77	-1.62	-57.61	136.76	-10.34	-2.25
			66	42.77	-1.62	32.65	136.76	-8.86	-2.25
			132	42.77	-1.62	122.92	136.76	-7.38	-2.25
194	Primo Impalcato	16, 18	0	43.24	-1.71	18.70	-60.57	-8.90	0.44
			66	43.24	-1.71	-21.28	-60.57	-9.19	0.44
			132	43.24	-1.71	-61.26	-60.57	-9.48	0.44
195	Primo Impalcato	17, 19	0	8.43	-0.78	-45.53	63.24	-6.89	1.31
			66	8.43	-0.78	-3.79	63.24	-7.75	1.31
			132	8.43	-0.78	37.95	63.24	-8.62	1.31
196	Primo Impalcato	18, 20	0	36.49	-0.81	13.00	-17.58	-10.38	-0.78
			66	36.49	-0.81	1.40	-17.58	-9.86	-0.78
			132	36.49	-0.81	-10.21	-17.58	-9.35	-0.78
197	Primo Impalcato	19, 21	0	-20.49	0.03	-131.57	198.03	-8.15	-0.05
			66	-20.49	0.03	-0.87	198.03	-8.11	-0.05
			132	-20.49	0.03	129.83	198.03	-8.08	-0.05
198	Primo Impalcato	20, 22	0	36.38	0.03	58.60	-89.59	-8.82	-1.00
			66	36.38	0.03	-0.53	-89.59	-8.16	-1.00
			132	36.38	0.03	-59.65	-89.59	-7.49	-1.00
199	Primo Impalcato	21, 23	0	-57.84	0.77	-39.89	59.87	-7.61	-1.75
			66	-57.84	0.77	-0.37	59.87	-6.45	-1.75
			132	-57.84	0.77	39.15	59.87	-5.30	-1.75
200	Primo Impalcato	22, 24	0	40.95	0.76	8.64	-13.52	-8.05	-1.83
			66	40.95	0.76	-0.29	-13.52	-6.84	-1.83
			132	40.95	0.76	-9.21	-13.52	-5.63	-1.83
201	Primo Impalcato	23, 25	0	-88.33	1.21	-130.60	200.13	-4.96	-2.29
			66	-88.33	1.21	1.49	200.13	-3.44	-2.29
			132	-88.33	1.21	133.58	200.13	-1.93	-2.29
202	Primo Impalcato	24, 26	0	42.46	1.24	58.68	-89.22	-5.24	-1.58
			66	42.46	1.24	-0.20	-89.22	-4.19	-1.58
			132	42.46	1.24	-59.09	-89.22	-3.15	-1.58
203	Primo Impalcato	25, 28	0	-168.98	1.50	-35.58	48.38	-1.59	-0.25
			85	-168.98	1.50	5.54	48.38	-1.37	-0.25
			170	-168.98	1.50	46.66	48.38	-1.16	-0.25
204	Primo Impalcato	26, 27	0	47.30	1.61	8.36	-12.91	-3.30	-2.00
			66	47.30	1.61	-0.16	-12.91	-1.98	-2.00
			132	47.30	1.61	-8.69	-12.91	-0.65	-2.00
205	Primo Impalcato	27, 29	0	49.78	1.65	58.95	-89.19	-0.48	-0.75
			66	49.78	1.65	0.09	-89.19	0.01	-0.75
			132	49.78	1.65	-58.77	-89.19	0.51	-0.75
206	Primo Impalcato	28, 30	0	-243.58	1.58	-121.80	149.43	-0.76	-0.24
			73	-243.58	1.58	-12.71	149.43	-0.59	-0.24
			146	-243.58	1.58	96.37	149.43	-0.42	-0.24
207	Primo Impalcato	29, 31	0	55.64	1.60	8.31	-13.20	0.70	-0.24
			66	55.64	1.60	-0.40	-13.20	0.86	-0.24
			132	55.64	1.60	-9.12	-13.20	1.02	-0.24
208	Primo Impalcato	30, 32	0	-181.83	1.57	-76.55	118.16	0.36	-0.06
			69	-181.83	1.57	4.39	118.16	0.40	-0.06
			137	-181.83	1.57	85.33	118.16	0.44	-0.06
209	Primo Impalcato	31, 33	0	56.08	1.51	60.08	-90.73	1.10	0.62
			66	56.08	1.51	0.20	-90.73	0.70	0.62
			132	56.08	1.51	-59.68	-90.73	0.29	0.62
210	Primo Impalcato	32, 34	0	-120.37	1.49	-86.16	124.56	1.22	0.78
			69	-120.37	1.49	-0.22	124.56	0.68	0.78

			138	-120.37	1.49	85.73	124.56	0.14	0.78
211	Primo Impalcato	33, 35	0	62.86	1.48	7.88	-12.35	0.48	0.32
			66	62.86	1.48	-0.27	-12.35	0.27	0.32
			132	62.86	1.48	-8.42	-12.35	0.06	0.32
212	Primo Impalcato	34, 36	0	-59.22	1.45	-85.52	123.89	0.94	0.95
			69	-59.22	1.45	-0.04	123.89	0.29	0.95
			138	-59.22	1.45	85.44	123.89	-0.36	0.95
213	Primo Impalcato	35, 37	0	65.22	1.46	59.73	-89.75	0.21	0.68
			66	65.22	1.46	0.50	-89.75	-0.24	0.68
			132	65.22	1.46	-58.74	-89.75	-0.69	0.68
214	Primo Impalcato	36, 38	0	1.55	1.44	-85.44	123.97	0.44	1.09
			69	1.55	1.44	0.10	123.97	-0.31	1.09
			138	1.55	1.44	85.64	123.97	-1.06	1.09
215	Primo Impalcato	37, 39	0	74.75	1.53	7.27	-15.68	-0.58	-0.43
			66	74.75	1.53	-3.07	-15.68	-0.30	-0.43
			132	74.75	1.53	-13.42	-15.68	-0.02	-0.43
216	Primo Impalcato	38, 40	0	61.90	1.49	-84.77	118.03	-0.29	1.01
			69	61.90	1.49	-3.91	118.03	-0.98	1.01
			137	61.90	1.49	76.94	118.03	-1.67	1.01
217	Primo Impalcato	39, 41	0	81.51	1.53	53.42	-66.53	0.15	-0.30
			66	81.51	1.53	9.50	-66.53	0.35	-0.30
			132	81.51	1.53	-34.41	-66.53	0.55	-0.30
218	Primo Impalcato	40, 42	0	121.71	1.55	-93.95	145.26	-0.99	0.48
			69	121.71	1.55	6.28	145.26	-1.31	0.48
			138	121.71	1.55	106.50	145.26	-1.64	0.48
219	Primo Impalcato	41, 44	0	25.64	1.45	37.44	-71.60	1.01	1.28
			66	25.64	1.45	-9.82	-71.60	0.16	1.28
			132	25.64	1.45	-57.08	-71.60	-0.69	1.28
220	Primo Impalcato	42, 43	0	181.41	2.01	-61.66	353.13	-1.09	-5.97
			23	181.41	2.01	19.56	353.13	0.28	-5.97
			46	181.41	2.01	100.78	353.13	1.65	-5.97
221	Primo Impalcato	43, 45	0	144.02	1.54	-66.55	85.73	1.86	-0.97
			66	144.02	1.54	-9.97	85.73	2.50	-0.97
			132	144.02	1.54	46.62	85.73	3.14	-0.97
222	Primo Impalcato	44, 46	0	31.32	1.47	10.35	-11.43	-0.53	-1.75
			66	31.32	1.47	2.80	-11.43	0.63	-1.75
			132	31.32	1.47	-4.75	-11.43	1.78	-1.75
223	Primo Impalcato	45, 47	0	107.40	1.28	-123.50	191.71	3.46	-1.09
			66	107.40	1.28	3.02	191.71	4.18	-1.09
			132	107.40	1.28	129.55	191.71	4.90	-1.09
224	Primo Impalcato	46, 48	0	37.22	1.28	64.36	-97.60	2.05	-2.30
			66	37.22	1.28	-0.06	-97.60	3.56	-2.30
			132	37.22	1.28	-64.47	-97.60	5.08	-2.30
225	Primo Impalcato	47, 49	0	74.34	0.83	-39.91	59.43	5.24	-1.60
			66	74.34	0.83	-0.69	59.43	6.30	-1.60
			132	74.34	0.83	38.53	59.43	7.36	-1.60
226	Primo Impalcato	48, 50	0	40.15	0.83	4.46	-9.69	4.76	-1.78
			66	40.15	0.83	-1.93	-9.69	5.94	-1.78
			132	40.15	0.83	-8.32	-9.69	7.11	-1.78
227	Primo Impalcato	49, 51	0	34.99	0.10	-131.22	199.79	7.83	-0.36
			66	34.99	0.10	0.64	199.79	8.07	-0.36
			132	34.99	0.10	132.51	199.79	8.31	-0.36
228	Primo Impalcato	50, 52	0	50.11	0.11	58.75	-77.47	7.67	-1.77
			66	50.11	0.11	7.63	-77.47	8.84	-1.77
			132	50.11	0.11	-43.50	-77.47	10.01	-1.77

229	Primo Impalcato	51, 53	0	3.12	-0.73	-37.15	61.71	8.77	1.16
			66	3.12	-0.73	3.58	61.71	8.01	1.16
			132	3.12	-0.73	44.31	61.71	7.24	1.16
230	Primo Impalcato	52, 54	0	-5.38	-0.79	27.61	-41.67	9.14	-0.85
			66	-5.38	-0.79	0.11	-41.67	9.70	-0.85
			132	-5.38	-0.79	-27.40	-41.67	10.26	-0.85
231	Primo Impalcato	53, 55	0	-34.28	-1.60	-124.35	138.80	7.72	-2.43
			66	-34.28	-1.60	-32.74	138.80	9.33	-2.43
			132	-34.28	-1.60	58.87	138.80	10.94	-2.43
232	Primo Impalcato	54, 56	0	-58.99	-1.69	43.46	-51.06	10.68	0.47
			66	-58.99	-1.69	9.76	-51.06	10.38	0.47
			132	-58.99	-1.69	-23.93	-51.06	10.07	0.47
233	Primo Impalcato	55, 57	0	-83.97	-3.34	-118.03	312.03	11.85	-11.74
			80	-83.97	-3.34	130.04	312.03	21.18	-11.74
			159	-83.97	-3.34	378.11	312.03	30.52	-11.74
234	Primo Impalcato	56, 70	0	-43.58	-3.15	56.07	-121.51	9.08	8.85
			80	-43.58	-3.15	-40.53	-121.51	2.05	8.85
			159	-43.58	-3.15	-137.13	-121.51	-4.99	8.85
235	Primo Impalcato	57, 58	0	25.11	-7.09	-253.26	111.16	35.15	47.21
			83	25.11	-7.09	-160.87	111.16	-4.09	47.21
			166	25.11	-7.09	-68.47	111.16	-43.33	47.21
236	Primo Impalcato	58, 59	0	-3.32	-0.58	-91.17	98.73	-40.26	-13.92
			69	-3.32	-0.58	-23.04	98.73	-30.65	-13.92
			138	-3.32	-0.58	45.08	98.73	-21.05	-13.92
237	Primo Impalcato	59, 60	0	-4.63	0.03	18.60	-38.10	-20.95	-10.71
			69	-4.63	0.03	-7.69	-38.10	-13.56	-10.71
			138	-4.63	0.03	-33.98	-38.10	-6.17	-10.71
238	Primo Impalcato	60, 61	0	-5.85	0.67	-61.38	166.97	-6.30	-2.20
			69	-5.85	0.67	53.83	166.97	-4.78	-2.20
			138	-5.85	0.67	169.04	166.97	-3.27	-2.20
239	Primo Impalcato	61, 62	0	-19.57	1.34	147.10	-214.30	-3.92	0.69
			69	-19.57	1.34	-0.76	-214.30	-4.40	0.69
			138	-19.57	1.34	-148.63	-214.30	-4.88	0.69
240	Primo Impalcato	62, 63	0	-18.64	1.93	-170.69	164.36	-3.94	-0.29
			69	-18.64	1.93	-57.28	164.36	-3.74	-0.29
			138	-18.64	1.93	56.12	164.36	-3.54	-0.29
241	Primo Impalcato	63, 64	0	-19.79	2.27	28.13	-41.10	-3.07	-1.10
			69	-19.79	2.27	-0.23	-41.10	-2.31	-1.10
			138	-19.79	2.27	-28.59	-41.10	-1.55	-1.10
242	Primo Impalcato	64, 65	0	-20.94	2.47	-56.63	165.10	-1.02	-0.66
			69	-20.94	2.47	57.29	165.10	-0.56	-0.66
			138	-20.94	2.47	171.22	165.10	-0.11	-0.66
243	Primo Impalcato	65, 66	0	-20.76	2.42	149.08	-215.35	0.15	-0.26
			69	-20.76	2.42	0.49	-215.35	0.33	-0.26
			138	-20.76	2.42	-148.10	-215.35	0.51	-0.26
244	Primo Impalcato	66, 67	0	-34.84	2.21	-170.17	168.02	1.00	-1.63
			69	-34.84	2.21	-54.24	168.02	2.13	-1.63
			138	-34.84	2.21	61.70	168.02	3.25	-1.63
245	Primo Impalcato	67, 68	0	-36.08	1.72	34.08	-37.75	3.55	-5.82
			69	-36.08	1.72	8.04	-37.75	7.56	-5.82
			138	-36.08	1.72	-18.01	-37.75	11.58	-5.82
246	Primo Impalcato	68, 69	0	-37.36	1.02	-44.68	100.32	11.82	-8.82
			69	-37.36	1.02	24.55	100.32	17.91	-8.82
			138	-37.36	1.02	93.77	100.32	23.99	-8.82
247	Primo	69, 70	0	-48.16	-2.88	70.77	97.88	24.87	12.05

	Impalcato								
			83	-48.16	-2.88	152.13	97.88	14.85	12.05
			166	-48.16	-2.88	233.49	97.88	4.84	12.05
248	Primo Impalcato	1	0	135.91	6.68	-7.24	-2.59	-60.51	-67.70
			188	135.91	6.68	-12.11	-2.59	66.75	-67.70
			376	135.91	6.68	-16.98	-2.59	194.02	-67.70
249	Primo Impalcato	2	0	-314.36	0.84	-97.75	8.99	-11.97	-6.30
			188	-314.36	0.84	-80.85	8.99	-0.12	-6.30
			376	-314.36	0.84	-63.95	8.99	11.73	-6.30
250	Primo Impalcato	3	0	-38.56	0.13	-46.43	-19.67	-13.72	-7.23
			188	-38.56	0.13	-83.40	-19.67	-0.14	-7.23
			376	-38.56	0.13	-120.38	-19.67	13.45	-7.23
251	Primo Impalcato	4	0	-38.32	-0.16	-42.98	-20.89	-13.10	-7.01
			188	-38.32	-0.16	-82.26	-20.89	0.08	-7.01
			376	-38.32	-0.16	-121.54	-20.89	13.27	-7.01
252	Primo Impalcato	5	0	43.91	-0.23	-47.20	-16.28	-14.32	-7.47
			188	43.91	-0.23	-77.80	-16.28	-0.28	-7.47
			376	43.91	-0.23	-108.41	-16.28	13.76	-7.47
253	Primo Impalcato	6	0	305.95	-0.28	-45.32	-12.81	-11.02	-6.01
			188	305.95	-0.28	-69.41	-12.81	0.28	-6.01
			376	305.95	-0.28	-93.50	-12.81	11.57	-6.01
254	Primo Impalcato	7	0	-326.62	-0.37	-39.74	-8.61	-11.04	-6.03
			188	-326.62	-0.37	-55.92	-8.61	0.30	-6.03
			376	-326.62	-0.37	-72.11	-8.61	11.64	-6.03
255	Primo Impalcato	8	0	20.00	-0.43	-28.03	-6.76	-15.47	-7.92
			188	20.00	-0.43	-40.74	-6.76	-0.57	-7.92
			376	20.00	-0.43	-53.46	-6.76	14.33	-7.92
256	Primo Impalcato	9	0	366.69	-0.46	-15.42	-4.42	-11.10	-6.06
			188	366.69	-0.46	-23.73	-4.42	0.30	-6.06
			376	366.69	-0.46	-32.04	-4.42	11.70	-6.06
257	Primo Impalcato	10	0	-281.92	-0.47	-7.87	1.55	-11.09	-6.06
			188	-281.92	-0.47	-4.95	1.55	0.30	-6.06
			376	-281.92	-0.47	-2.03	1.55	11.69	-6.06
258	Primo Impalcato	11	0	-65.63	-0.43	-0.71	6.35	-14.35	-7.51
			188	-65.63	-0.43	11.23	6.35	-0.22	-7.51
			376	-65.63	-0.43	23.17	6.35	13.90	-7.51
259	Primo Impalcato	12	0	55.55	-0.26	6.10	9.18	-13.91	-7.32
			188	55.55	-0.26	23.36	9.18	-0.15	-7.32
			376	55.55	-0.26	40.61	9.18	13.61	-7.32
260	Primo Impalcato	13	0	360.70	0.16	28.99	1.03	-11.96	-6.27
			188	360.70	0.16	30.92	1.03	-0.17	-6.27
			376	360.70	0.16	32.85	1.03	11.62	-6.27
261	Primo Impalcato	14	0	-382.94	3.80	-10.63	8.05	-67.87	-70.65
			188	-382.94	3.80	4.51	8.05	64.95	-70.65
			376	-382.94	3.80	19.64	8.05	197.78	-70.65
262	Primo Impalcato	15	0	234.01	1.27	20.12	-10.36	-10.77	-72.30
			188	234.01	1.27	0.64	-10.36	125.16	-72.30
			376	234.01	1.27	-18.84	-10.36	261.09	-72.30
263	Primo Impalcato	16	0	-183.47	1.43	-13.31	6.84	7.59	-61.01
			188	-183.47	1.43	-0.44	6.84	122.28	-61.01
			376	-183.47	1.43	12.42	6.84	236.97	-61.01
264	Primo Impalcato	17	0	-35.85	0.70	15.63	-8.66	-1.55	-84.58
			188	-35.85	0.70	-0.65	-8.66	157.47	-84.58
			376	-35.85	0.70	-16.93	-8.66	316.48	-84.58
265	Primo Impalcato	18	0	-21.99	0.85	-10.23	5.59	3.64	-81.44

			188	-21.99	0.85	0.28	5.59	156.75	-81.44
			376	-21.99	0.85	10.79	5.59	309.87	-81.44
266	Primo Impalcato	19	0	136.27	0.21	16.17	-8.88	4.21	-89.46
			188	136.27	0.21	-0.52	-8.88	172.40	-89.46
			376	136.27	0.21	-17.21	-8.88	340.60	-89.46
267	Primo Impalcato	20	0	-97.71	0.22	-10.36	5.60	3.53	-89.95
			188	-97.71	0.22	0.17	5.60	172.64	-89.95
			376	-97.71	0.22	10.71	5.60	341.75	-89.95
268	Primo Impalcato	21	0	7.87	-0.30	16.34	-8.95	4.80	-89.53
			188	7.87	-0.30	-0.49	-8.95	173.12	-89.53
			376	7.87	-0.30	-17.32	-8.95	341.45	-89.53
269	Primo Impalcato	22	0	-11.07	-0.30	-10.30	5.57	4.15	-90.04
			188	-11.07	-0.30	0.17	5.57	173.41	-90.04
			376	-11.07	-0.30	10.65	5.57	342.68	-90.04
270	Primo Impalcato	23	0	130.60	-0.71	16.48	-9.03	4.22	-82.58
			188	130.60	-0.71	-0.48	-9.03	159.47	-82.58
			376	130.60	-0.71	-17.45	-9.03	314.71	-82.58
271	Primo Impalcato	24	0	-69.13	-0.73	-10.32	5.59	4.02	-83.09
			188	-69.13	-0.73	0.18	5.59	160.22	-83.09
			376	-69.13	-0.73	10.69	5.59	316.43	-83.09
272	Primo Impalcato	25	0	-7.38	-0.93	16.24	-8.88	1.08	-73.84
			188	-7.38	-0.93	-0.46	-8.88	139.91	-73.84
			376	-7.38	-0.93	-17.17	-8.88	278.73	-73.84
273	Primo Impalcato	26	0	6.32	-1.00	-10.32	5.58	3.66	-72.33
			188	6.32	-1.00	0.17	5.58	139.64	-72.33
			376	6.32	-1.00	10.66	5.58	275.62	-72.33
274	Primo Impalcato	27	0	-53.41	-1.12	-10.36	5.61	3.21	-56.65
			188	-53.41	-1.12	0.18	5.61	109.70	-56.65
			376	-53.41	-1.12	10.73	5.61	216.20	-56.65
275	Primo Impalcato	28	0	123.72	-1.05	15.40	-8.55	0.25	-54.59
			188	123.72	-1.05	-0.68	-8.55	102.88	-54.59
			376	123.72	-1.05	-16.76	-8.55	205.51	-54.59
276	Primo Impalcato	29	0	22.39	-1.12	-10.45	5.66	2.19	-41.59
			188	22.39	-1.12	0.18	5.66	80.38	-41.59
			376	22.39	-1.12	10.82	5.66	158.58	-41.59
277	Primo Impalcato	30	0	32.67	-1.09	18.18	-9.87	-2.48	-39.56
			188	32.67	-1.09	-0.38	-9.87	71.89	-39.56
			376	32.67	-1.09	-18.95	-9.87	146.27	-39.56
278	Primo Impalcato	31	0	-45.55	-1.07	-10.46	5.67	2.46	-26.15
			188	-45.55	-1.07	0.20	5.67	51.62	-26.15
			376	-45.55	-1.07	10.85	5.67	100.78	-26.15
279	Primo Impalcato	32	0	16.01	-1.06	17.73	-9.71	-3.71	-25.12
			188	16.01	-1.06	-0.53	-9.71	43.52	-25.12
			376	16.01	-1.06	-18.79	-9.71	90.75	-25.12
280	Primo Impalcato	33	0	28.75	-1.02	-10.55	5.71	1.93	-12.33
			188	28.75	-1.02	0.19	5.71	25.11	-12.33
			376	28.75	-1.02	10.92	5.71	48.29	-12.33
281	Primo Impalcato	34	0	7.71	-1.02	17.86	-9.76	-3.84	-10.69
			188	7.71	-1.02	-0.49	-9.76	16.25	-10.69
			376	7.71	-1.02	-18.85	-9.76	36.35	-10.69
282	Primo Impalcato	35	0	-39.07	-1.01	-10.57	5.73	1.98	1.79
			188	-39.07	-1.01	0.19	5.73	-1.39	1.79
			376	-39.07	-1.01	10.95	5.73	-4.76	1.79
283	Primo Impalcato	36	0	-12.87	-1.00	17.93	-9.80	-4.43	3.05
			188	-12.87	-1.00	-0.49	-9.80	-10.16	3.05

			376	-12.87	-1.00	-18.91	-9.80	-15.89	3.05
284	Primo Impalcato	37	0	43.39	-1.02	-10.71	5.78	1.66	15.29
			188	43.39	-1.02	0.16	5.78	-27.08	15.29
			376	43.39	-1.02	11.03	5.78	-55.82	15.29
285	Primo Impalcato	38	0	-25.01	-1.02	17.96	-9.83	-4.94	16.72
			188	-25.01	-1.02	-0.52	-9.83	-36.38	16.72
			376	-25.01	-1.02	-19.00	-9.83	-67.81	16.72
286	Primo Impalcato	39	0	-33.81	-1.04	-10.37	5.67	1.01	29.59
			188	-33.81	-1.04	0.28	5.67	-54.62	29.59
			376	-33.81	-1.04	10.93	5.67	-110.24	29.59
287	Primo Impalcato	40	0	-40.91	-1.08	18.52	-10.06	-4.88	30.96
			188	-40.91	-1.08	-0.40	-10.06	-63.08	30.96
			376	-40.91	-1.08	-19.32	-10.06	-121.28	30.96
288	Primo Impalcato	41	0	10.59	-1.02	-12.04	6.42	-1.49	42.57
			188	10.59	-1.02	0.04	6.42	-81.51	42.57
			376	10.59	-1.02	12.11	6.42	-161.54	42.57
289	Primo Impalcato	42	0	-121.42	-1.17	17.18	-9.42	-0.13	48.20
			188	-121.42	-1.17	-0.52	-9.42	-90.75	48.20
			376	-121.42	-1.17	-18.23	-9.42	-181.37	48.20
290	Primo Impalcato	43	0	-31.52	-1.16	15.87	-8.78	-6.67	51.82
			188	-31.52	-1.16	-0.64	-8.78	-104.09	51.82
			376	-31.52	-1.16	-17.15	-8.78	-201.52	51.82
291	Primo Impalcato	44	0	68.00	-1.01	-10.42	5.69	-0.11	57.14
			188	68.00	-1.01	0.28	5.69	-107.53	57.14
			376	68.00	-1.01	10.98	5.69	-214.95	57.14
292	Primo Impalcato	45	0	30.98	-1.00	17.24	-9.36	-1.89	69.31
			188	30.98	-1.00	-0.35	-9.36	-132.19	69.31
			376	30.98	-1.00	-17.93	-9.36	-262.49	69.31
293	Primo Impalcato	46	0	-28.48	-0.97	-10.85	5.86	-2.33	69.62
			188	-28.48	-0.97	0.17	5.86	-133.21	69.62
			376	-28.48	-0.97	11.20	5.86	-264.10	69.62
294	Primo Impalcato	47	0	-126.14	-0.74	16.75	-9.18	-2.76	80.84
			188	-126.14	-0.74	-0.50	-9.18	-154.73	80.84
			376	-126.14	-0.74	-17.75	-9.18	-306.70	80.84
295	Primo Impalcato	48	0	77.27	-0.74	-10.85	5.86	-4.08	80.63
			188	77.27	-0.74	0.16	5.86	-155.67	80.63
			376	77.27	-0.74	11.17	5.86	-307.26	80.63
296	Primo Impalcato	49	0	-2.85	-0.34	16.78	-9.18	-4.15	88.13
			188	-2.85	-0.34	-0.48	-9.18	-169.84	88.13
			376	-2.85	-0.34	-17.74	-9.18	-335.52	88.13
297	Primo Impalcato	50	0	-0.14	-0.37	-10.64	5.79	-3.76	88.79
			188	-0.14	-0.37	0.24	5.79	-170.68	88.79
			376	-0.14	-0.37	11.13	5.79	-337.61	88.79
298	Primo Impalcato	51	0	-138.75	0.17	16.65	-9.13	-4.28	88.46
			188	-138.75	0.17	-0.51	-9.13	-170.57	88.46
			376	-138.75	0.17	-17.68	-9.13	-336.87	88.46
299	Primo Impalcato	52	0	61.79	0.19	-12.10	6.50	-3.27	89.53
			188	61.79	0.19	0.12	6.50	-171.59	89.53
			376	61.79	0.19	12.33	6.50	-339.91	89.53
300	Primo Impalcato	53	0	35.12	0.68	16.14	-8.93	1.46	84.17
			188	35.12	0.68	-0.65	-8.93	-156.79	84.17
			376	35.12	0.68	-17.43	-8.93	-315.03	84.17
301	Primo Impalcato	54	0	63.48	0.81	-12.22	6.60	-2.65	81.12
			188	63.48	0.81	0.18	6.60	-155.15	81.12
			376	63.48	0.81	12.58	6.60	-307.65	81.12

302	Primo Impalcato	55	0	-242.43	1.28	20.63	-10.63	10.45	71.98
			188	-242.43	1.28	0.65	-10.63	-124.87	71.98
			376	-242.43	1.28	-19.34	-10.63	-260.19	71.98
303	Primo Impalcato	56	0	186.62	1.47	-13.36	6.97	-8.67	59.83
			188	186.62	1.47	-0.26	6.97	-121.16	59.83
			376	186.62	1.47	12.84	6.97	-233.65	59.83
304	Primo Impalcato	57	0	-136.84	6.82	-6.23	-3.15	60.03	66.60
			188	-136.84	6.82	-12.16	-3.15	-65.17	66.60
			376	-136.84	6.82	-18.09	-3.15	-190.37	66.60
305	Primo Impalcato	58	0	295.00	0.88	-98.26	8.24	11.72	6.18
			188	295.00	0.88	-82.77	8.24	0.10	6.18
			376	295.00	0.88	-67.28	8.24	-11.52	6.18
306	Primo Impalcato	59	0	51.29	0.18	-49.36	-20.31	13.46	7.10
			188	51.29	0.18	-87.53	-20.31	0.11	7.10
			376	51.29	0.18	-125.71	-20.31	-13.23	7.10
307	Primo Impalcato	60	0	-47.83	-0.13	-46.91	-21.94	13.86	7.26
			188	-47.83	-0.13	-88.15	-21.94	0.21	7.26
			376	-47.83	-0.13	-129.39	-21.94	-13.44	7.26
308	Primo Impalcato	61	0	-258.78	-0.23	-50.67	-17.40	10.75	5.87
			188	-258.78	-0.23	-83.38	-17.40	-0.28	5.87
			376	-258.78	-0.23	-116.10	-17.40	-11.31	5.87
309	Primo Impalcato	62	0	346.52	-0.33	-49.51	-12.05	10.80	5.89
			188	346.52	-0.33	-72.16	-12.05	-0.27	5.89
			376	346.52	-0.33	-94.81	-12.05	-11.34	5.89
310	Primo Impalcato	63	0	106.51	-0.42	-39.97	-9.63	14.10	7.36
			188	106.51	-0.42	-58.08	-9.63	0.26	7.36
			376	106.51	-0.42	-76.19	-9.63	-13.57	7.36
311	Primo Impalcato	64	0	-104.46	-0.47	-28.19	-7.35	14.12	7.37
			188	-104.46	-0.47	-42.00	-7.35	0.26	7.37
			376	-104.46	-0.47	-55.82	-7.35	-13.59	7.37
312	Primo Impalcato	65	0	-345.19	-0.49	-15.54	-4.40	10.85	5.92
			188	-345.19	-0.49	-23.81	-4.40	-0.27	5.92
			376	-345.19	-0.49	-32.07	-4.40	-11.39	5.92
313	Primo Impalcato	66	0	263.82	-0.48	-7.75	1.75	10.83	5.91
			188	263.82	-0.48	-4.46	1.75	-0.28	5.91
			376	263.82	-0.48	-1.17	1.75	-11.40	5.91
314	Primo Impalcato	67	0	50.37	-0.43	-0.34	6.50	13.98	7.32
			188	50.37	-0.43	11.88	6.50	0.22	7.32
			376	50.37	-0.43	24.11	6.50	-13.55	7.32
315	Primo Impalcato	68	0	-61.20	-0.26	6.28	9.39	13.54	7.13
			188	-61.20	-0.26	23.94	9.39	0.14	7.13
			376	-61.20	-0.26	41.61	9.39	-13.27	7.13
316	Primo Impalcato	69	0	-349.09	0.15	27.95	1.75	11.64	6.11
			188	-349.09	0.15	31.25	1.75	0.16	6.11
			376	-349.09	0.15	34.54	1.75	-11.32	6.11
317	Primo Impalcato	70	0	381.90	3.84	-15.74	10.29	66.48	68.86
			188	381.90	3.84	3.60	10.29	-62.98	68.86
			376	381.90	3.84	22.95	10.29	-192.45	68.86
318	Fondazione	1, 71	0	-275.86	0.00	0.00	0.00	1.58	0.02
			102	-275.86	0.00	0.00	0.00	1.56	0.02
			204	-275.86	0.00	0.00	0.00	1.54	0.02
319	Fondazione	1, 92	0	439.37	0.03	0.00	0.00	0.56	-0.94
			103	439.37	0.03	0.00	0.00	1.53	-0.94
			206	439.37	0.03	0.00	0.00	2.50	-0.94
320	Primo	92, 2	0	-504.47	0.13	0.00	0.00	-0.33	-1.05

	Impalcato								
			103	-504.47	0.13	0.00	0.00	0.75	-1.05
			206	-504.47	0.13	0.00	0.00	1.82	-1.05
321	Fondazio ne	6, 89	0	511.83	-0.09	0.00	0.00	2.30	0.63
			100	511.83	-0.09	0.00	0.00	1.66	0.63
			200	511.83	-0.09	0.00	0.00	1.03	0.63
322	Primo Impalcato	89, 7	0	-517.05	0.03	0.00	0.00	1.91	0.09
			100	-517.05	0.03	0.00	0.00	1.82	0.09
			200	-517.05	0.03	0.00	0.00	1.73	0.09
323	Fondazio ne	9, 90	0	530.02	-0.05	0.00	0.00	0.79	0.54
			100	530.02	-0.05	0.00	0.00	0.25	0.54
			200	530.02	-0.05	0.00	0.00	-0.30	0.54
324	Primo Impalcato	90, 10	0	-507.09	-0.03	0.00	0.00	0.97	0.47
			100	-507.09	-0.03	0.00	0.00	0.50	0.47
			200	-507.09	-0.03	0.00	0.00	0.03	0.47
325	Fondazio ne	13, 91	0	488.49	0.06	0.00	0.00	-1.16	-0.63
			103	488.49	0.06	0.00	0.00	-0.51	-0.63
			206	488.49	0.06	0.00	0.00	0.13	-0.63
326	Primo Impalcato	88, 14	0	188.51	-0.01	0.00	0.00	-1.50	-0.13
			102	188.51	-0.01	0.00	0.00	-1.36	-0.13
			204	188.51	-0.01	0.00	0.00	-1.23	-0.13
327	Primo Impalcato	91, 14	0	-438.15	0.00	0.00	0.00	-0.77	0.07
			103	-438.15	0.00	0.00	0.00	-0.85	0.07
			206	-438.15	0.00	0.00	0.00	-0.92	0.07
328	Primo Impalcato	71, 15	0	329.29	0.11	0.00	0.00	-0.31	-1.42
			102	329.29	0.11	0.00	0.00	1.13	-1.42
			204	329.29	0.11	0.00	0.00	2.58	-1.42
329	Fondazio ne	16, 88	0	-258.62	0.09	0.00	0.00	-2.20	-1.10
			102	-258.62	0.09	0.00	0.00	-1.07	-1.10
			204	-258.62	0.09	0.00	0.00	0.06	-1.10
330	Fondazio ne	17, 72	0	-273.78	-0.06	0.00	0.00	3.01	0.67
			100	-273.78	-0.06	0.00	0.00	2.35	0.67
			199	-273.78	-0.06	0.00	0.00	1.68	0.67
331	Primo Impalcato	87, 18	0	166.33	-0.06	0.00	0.00	-1.71	0.63
			100	166.33	-0.06	0.00	0.00	-2.34	0.63
			199	166.33	-0.06	0.00	0.00	-2.98	0.63
332	Primo Impalcato	72, 19	0	290.21	0.09	0.00	0.00	1.26	-0.99
			100	290.21	0.09	0.00	0.00	2.25	-0.99
			199	290.21	0.09	0.00	0.00	3.23	-0.99
333	Fondazio ne	20, 87	0	-184.95	0.09	0.00	0.00	-3.26	-1.03
			100	-184.95	0.09	0.00	0.00	-2.24	-1.03
			199	-184.95	0.09	0.00	0.00	-1.21	-1.03
334	Fondazio ne	21, 73	0	-277.82	-0.09	0.00	0.00	3.20	0.98
			100	-277.82	-0.09	0.00	0.00	2.23	0.98
			199	-277.82	-0.09	0.00	0.00	1.25	0.98
335	Primo Impalcato	86, 22	0	168.43	-0.09	0.00	0.00	-1.25	0.98
			100	168.43	-0.09	0.00	0.00	-2.23	0.98
			199	168.43	-0.09	0.00	0.00	-3.21	0.98
336	Primo Impalcato	73, 23	0	299.01	0.06	0.00	0.00	1.73	-0.64
			100	299.01	0.06	0.00	0.00	2.37	-0.64
			199	299.01	0.06	0.00	0.00	3.01	-0.64
337	Fondazio ne	24, 86	0	-180.59	0.06	0.00	0.00	-3.03	-0.65
			100	-180.59	0.06	0.00	0.00	-2.39	-0.65
			199	-180.59	0.06	0.00	0.00	-1.74	-0.65
338	Fondazio ne	25, 74	0	-332.66	-0.10	0.00	0.00	2.39	0.93

			103	-332.66	-0.10	0.00	0.00	1.44	0.93
			206	-332.66	-0.10	0.00	0.00	0.48	0.93
339	Primo Impalcato	85, 26	0	171.47	-0.09	0.00	0.00	-0.63	0.95
			100	171.47	-0.09	0.00	0.00	-1.58	0.95
			199	171.47	-0.09	0.00	0.00	-2.53	0.95
340	Fondazio ne	27, 85	0	-178.18	0.02	0.00	0.00	-2.06	-0.21
			100	-178.18	0.02	0.00	0.00	-1.85	-0.21
			199	-178.18	0.02	0.00	0.00	-1.64	-0.21
341	Primo Impalcato	74, 28	0	345.15	0.04	0.00	0.00	1.57	-0.13
			103	345.15	0.04	0.00	0.00	1.70	-0.13
			206	345.15	0.04	0.00	0.00	1.83	-0.13
342	Primo Impalcato	84, 29	0	175.73	-0.07	0.00	0.00	-0.10	0.65
			100	175.73	-0.07	0.00	0.00	-0.75	0.65
			199	175.73	-0.07	0.00	0.00	-1.40	0.65
343	Fondazio ne	31, 84	0	-178.40	-0.01	0.00	0.00	-0.98	0.07
			100	-178.40	-0.01	0.00	0.00	-1.05	0.07
			199	-178.40	-0.01	0.00	0.00	-1.12	0.07
344	Primo Impalcato	83, 33	0	178.39	-0.04	0.00	0.00	0.36	0.37
			100	178.39	-0.04	0.00	0.00	-0.02	0.37
			199	178.39	-0.04	0.00	0.00	-0.39	0.37
345	Fondazio ne	35, 83	0	-178.84	-0.03	0.00	0.00	-0.01	0.29
			100	-178.84	-0.03	0.00	0.00	-0.29	0.29
			199	-178.84	-0.03	0.00	0.00	-0.58	0.29
346	Primo Impalcato	82, 37	0	180.69	-0.01	0.00	0.00	0.85	0.14
			100	180.69	-0.01	0.00	0.00	0.71	0.14
			199	180.69	-0.01	0.00	0.00	0.56	0.14
347	Fondazio ne	39, 82	0	-177.69	-0.05	0.00	0.00	0.96	0.53
			100	-177.69	-0.05	0.00	0.00	0.43	0.53
			199	-177.69	-0.05	0.00	0.00	-0.10	0.53
348	Primo Impalcato	78, 43	0	-294.66	0.02	0.00	0.00	1.59	-0.18
			100	-294.66	0.02	0.00	0.00	1.77	-0.18
			199	-294.66	0.02	0.00	0.00	1.95	-0.18
349	Primo Impalcato	81, 44	0	184.03	0.02	0.00	0.00	1.56	-0.25
			100	184.03	0.02	0.00	0.00	1.81	-0.25
			199	184.03	0.02	0.00	0.00	2.06	-0.25
350	Fondazio ne	45, 78	0	297.23	-0.09	0.00	0.00	2.40	0.92
			100	297.23	-0.09	0.00	0.00	1.48	0.92
			199	297.23	-0.09	0.00	0.00	0.56	0.92
351	Fondazio ne	46, 81	0	-176.99	-0.09	0.00	0.00	2.39	0.87
			100	-176.99	-0.09	0.00	0.00	1.52	0.87
			199	-176.99	-0.09	0.00	0.00	0.65	0.87
352	Primo Impalcato	77, 47	0	-303.79	0.06	0.00	0.00	1.71	-0.61
			100	-303.79	0.06	0.00	0.00	2.32	-0.61
			199	-303.79	0.06	0.00	0.00	2.93	-0.61
353	Primo Impalcato	80, 48	0	187.53	0.06	0.00	0.00	1.73	-0.60
			100	187.53	0.06	0.00	0.00	2.33	-0.60
			199	187.53	0.06	0.00	0.00	2.93	-0.60
354	Fondazio ne	49, 77	0	284.43	-0.09	0.00	0.00	3.15	0.98
			100	284.43	-0.09	0.00	0.00	2.18	0.98
			199	284.43	-0.09	0.00	0.00	1.20	0.98
355	Fondazio ne	50, 80	0	-174.30	-0.09	0.00	0.00	3.16	0.98
			100	-174.30	-0.09	0.00	0.00	2.18	0.98
			199	-174.30	-0.09	0.00	0.00	1.20	0.98
356	Primo Impalcato	76, 51	0	-298.19	0.09	0.00	0.00	1.27	-0.97
			100	-298.19	0.09	0.00	0.00	2.23	-0.97

			199	-298.19	0.09	0.00	0.00	3.20	-0.97
357	Fondazio ne	53, 76	0	281.47	-0.06	0.00	0.00	3.00	0.68
			100	281.47	-0.06	0.00	0.00	2.33	0.68
			199	281.47	-0.06	0.00	0.00	1.66	0.68
358	Primo Impalcato	75, 55	0	-338.55	0.11	0.00	0.00	-0.34	-1.43
			102	-338.55	0.11	0.00	0.00	1.12	-1.43
			204	-338.55	0.11	0.00	0.00	2.58	-1.43
359	Fondazio ne	56, 79	0	270.18	0.09	0.00	0.00	-2.16	-1.09
			102	270.18	0.09	0.00	0.00	-1.04	-1.09
			204	270.18	0.09	0.00	0.00	0.07	-1.09
360	Fondazio ne	57, 75	0	283.86	0.00	0.00	0.00	1.58	0.02
			102	283.86	0.00	0.00	0.00	1.56	0.02
			204	283.86	0.00	0.00	0.00	1.54	0.02
361	Fondazio ne	57, 93	0	-433.53	0.03	0.00	0.00	0.57	-0.97
			103	-433.53	0.03	0.00	0.00	1.57	-0.97
			206	-433.53	0.03	0.00	0.00	2.56	-0.97
362	Primo Impalcato	93, 58	0	493.68	0.13	0.00	0.00	-0.34	-1.08
			103	493.68	0.13	0.00	0.00	0.78	-1.08
			206	493.68	0.13	0.00	0.00	1.89	-1.08
363	Fondazio ne	61, 95	0	-491.41	-0.10	0.00	0.00	2.84	0.71
			100	-491.41	-0.10	0.00	0.00	2.13	0.71
			200	-491.41	-0.10	0.00	0.00	1.42	0.71
364	Primo Impalcato	95, 62	0	514.31	0.05	0.00	0.00	2.23	-0.03
			100	514.31	0.05	0.00	0.00	2.26	-0.03
			200	514.31	0.05	0.00	0.00	2.29	-0.03
365	Primo Impalcato	96, 65	0	-517.09	-0.05	0.00	0.00	0.31	0.55
			100	-517.09	-0.05	0.00	0.00	-0.23	0.55
			200	-517.09	-0.05	0.00	0.00	-0.78	0.55
366	Fondazio ne	66, 96	0	495.08	-0.03	0.00	0.00	0.00	0.49
			100	495.08	-0.03	0.00	0.00	-0.50	0.49
			200	495.08	-0.03	0.00	0.00	-0.99	0.49
367	Fondazio ne	69, 94	0	-474.06	0.05	0.00	0.00	-1.22	-0.65
			103	-474.06	0.05	0.00	0.00	-0.56	-0.65
			206	-474.06	0.05	0.00	0.00	0.11	-0.65
368	Primo Impalcato	79, 70	0	-200.28	-0.01	0.00	0.00	-1.50	-0.15
			102	-200.28	-0.01	0.00	0.00	-1.35	-0.15
			204	-200.28	-0.01	0.00	0.00	-1.20	-0.15
369	Primo Impalcato	94, 70	0	426.52	-0.01	0.00	0.00	-0.71	0.14
			103	426.52	-0.01	0.00	0.00	-0.86	0.14
			206	426.52	-0.01	0.00	0.00	-1.01	0.14
370	Primo Impalcato	1, 71	0	329.29	0.19	0.00	0.00	-2.60	-1.18
			102	329.29	0.19	0.00	0.00	-1.40	-1.18
			204	329.29	0.19	0.00	0.00	-0.19	-1.18
371	Primo Impalcato	1, 92	0	-504.47	0.16	0.00	0.00	-1.98	-0.82
			103	-504.47	0.16	0.00	0.00	-1.14	-0.82
			206	-504.47	0.16	0.00	0.00	-0.29	-0.82
372	Primo Impalcato	92, 2	0	439.37	0.03	0.00	0.00	2.45	-0.72
			103	439.37	0.03	0.00	0.00	3.18	-0.72
			206	439.37	0.03	0.00	0.00	3.92	-0.72
373	Primo Impalcato	6, 89	0	-517.05	0.00	0.00	0.00	1.65	-0.09
			100	-517.05	0.00	0.00	0.00	1.74	-0.09
			200	-517.05	0.00	0.00	0.00	1.84	-0.09
374	Primo Impalcato	89, 7	0	511.83	-0.11	0.00	0.00	1.11	0.45
			100	511.83	-0.11	0.00	0.00	0.65	0.45
			200	511.83	-0.11	0.00	0.00	0.20	0.45

375	Primo Impalcato	9, 90	0	-507.09	-0.06	0.00	0.00	1.28	0.20
			100	-507.09	-0.06	0.00	0.00	1.08	0.20
			200	-507.09	-0.06	0.00	0.00	0.88	0.20
376	Primo Impalcato	90, 10	0	530.02	-0.09	0.00	0.00	-0.20	0.27
			100	530.02	-0.09	0.00	0.00	-0.47	0.27
			200	530.02	-0.09	0.00	0.00	-0.74	0.27
377	Primo Impalcato	13, 91	0	-438.15	-0.02	0.00	0.00	-0.88	-0.08
			103	-438.15	-0.02	0.00	0.00	-0.80	-0.08
			206	-438.15	-0.02	0.00	0.00	-0.73	-0.08
378	Primo Impalcato	88, 14	0	-258.62	0.09	0.00	0.00	-0.03	-0.84
			102	-258.62	0.09	0.00	0.00	0.83	-0.84
			204	-258.62	0.09	0.00	0.00	1.68	-0.84
379	Primo Impalcato	91, 14	0	488.49	0.10	0.00	0.00	0.12	-0.78
			103	488.49	0.10	0.00	0.00	0.92	-0.78
			206	488.49	0.10	0.00	0.00	1.72	-0.78
380	Primo Impalcato	71, 15	0	-275.86	0.03	0.00	0.00	1.39	0.26
			102	-275.86	0.03	0.00	0.00	1.13	0.26
			204	-275.86	0.03	0.00	0.00	0.86	0.26
381	Primo Impalcato	16, 88	0	188.51	0.05	0.00	0.00	-1.16	0.14
			102	188.51	0.05	0.00	0.00	-1.30	0.14
			204	188.51	0.05	0.00	0.00	-1.44	0.14
382	Primo Impalcato	17, 72	0	290.21	0.07	0.00	0.00	-0.47	-0.89
			100	290.21	0.07	0.00	0.00	0.42	-0.89
			199	290.21	0.07	0.00	0.00	1.31	-0.89
383	Primo Impalcato	87, 18	0	-184.95	0.08	0.00	0.00	-1.26	-0.89
			100	-184.95	0.08	0.00	0.00	-0.37	-0.89
			199	-184.95	0.08	0.00	0.00	0.51	-0.89
384	Primo Impalcato	72, 19	0	-273.78	-0.02	0.00	0.00	1.66	0.76
			100	-273.78	-0.02	0.00	0.00	0.91	0.76
			199	-273.78	-0.02	0.00	0.00	0.15	0.76
385	Primo Impalcato	20, 87	0	166.33	-0.03	0.00	0.00	-0.13	0.78
			100	166.33	-0.03	0.00	0.00	-0.91	0.78
			199	166.33	-0.03	0.00	0.00	-1.68	0.78
386	Primo Impalcato	21, 73	0	299.01	0.02	0.00	0.00	0.18	-0.77
			100	299.01	0.02	0.00	0.00	0.95	-0.77
			199	299.01	0.02	0.00	0.00	1.72	-0.77
387	Primo Impalcato	86, 22	0	-180.59	0.02	0.00	0.00	-1.72	-0.78
			100	-180.59	0.02	0.00	0.00	-0.94	-0.78
			199	-180.59	0.02	0.00	0.00	-0.16	-0.78
388	Primo Impalcato	73, 23	0	-277.82	-0.07	0.00	0.00	1.29	0.84
			100	-277.82	-0.07	0.00	0.00	0.45	0.84
			199	-277.82	-0.07	0.00	0.00	-0.39	0.84
389	Primo Impalcato	24, 86	0	168.43	-0.07	0.00	0.00	0.39	0.85
			100	168.43	-0.07	0.00	0.00	-0.45	0.85
			199	168.43	-0.07	0.00	0.00	-1.29	0.85
390	Primo Impalcato	25, 74	0	345.15	-0.02	0.00	0.00	0.65	-0.44
			103	345.15	-0.02	0.00	0.00	1.10	-0.44
			206	345.15	-0.02	0.00	0.00	1.55	-0.44
391	Primo Impalcato	85, 26	0	-178.18	-0.03	0.00	0.00	-1.59	-0.50
			100	-178.18	-0.03	0.00	0.00	-1.09	-0.50
			199	-178.18	-0.03	0.00	0.00	-0.59	-0.50
392	Primo Impalcato	27, 85	0	171.47	-0.08	0.00	0.00	0.62	0.67
			100	171.47	-0.08	0.00	0.00	-0.04	0.67
			199	171.47	-0.08	0.00	0.00	-0.70	0.67
393	Primo	74, 28	0	-332.66	-0.07	0.00	0.00	0.54	0.62

	Impalcato								
			103	-332.66	-0.07	0.00	0.00	-0.10	0.62
			206	-332.66	-0.07	0.00	0.00	-0.74	0.62
394	Primo Impalcato	84, 29	0	-178.40	-0.05	0.00	0.00	-1.06	-0.20
			100	-178.40	-0.05	0.00	0.00	-0.86	-0.20
			199	-178.40	-0.05	0.00	0.00	-0.66	-0.20
395	Primo Impalcato	31, 84	0	175.73	-0.07	0.00	0.00	0.58	0.38
			100	175.73	-0.07	0.00	0.00	0.20	0.38
			199	175.73	-0.07	0.00	0.00	-0.18	0.38
396	Primo Impalcato	83, 33	0	-178.84	-0.05	0.00	0.00	-0.52	0.04
			100	-178.84	-0.05	0.00	0.00	-0.56	0.04
			199	-178.84	-0.05	0.00	0.00	-0.60	0.04
397	Primo Impalcato	35, 83	0	178.39	-0.06	0.00	0.00	0.55	0.13
			100	178.39	-0.06	0.00	0.00	0.42	0.13
			199	178.39	-0.06	0.00	0.00	0.29	0.13
398	Primo Impalcato	82, 37	0	-177.69	-0.06	0.00	0.00	-0.03	0.28
			100	-177.69	-0.06	0.00	0.00	-0.32	0.28
			199	-177.69	-0.06	0.00	0.00	-0.60	0.28
399	Primo Impalcato	39, 82	0	180.69	-0.05	0.00	0.00	0.58	-0.11
			100	180.69	-0.05	0.00	0.00	0.69	-0.11
			199	180.69	-0.05	0.00	0.00	0.80	-0.11
400	Primo Impalcato	78, 43	0	297.23	-0.08	0.00	0.00	0.63	0.61
			100	297.23	-0.08	0.00	0.00	0.02	0.61
			199	297.23	-0.08	0.00	0.00	-0.59	0.61
401	Primo Impalcato	81, 44	0	-176.99	-0.07	0.00	0.00	0.71	0.64
			100	-176.99	-0.07	0.00	0.00	0.07	0.64
			199	-176.99	-0.07	0.00	0.00	-0.57	0.64
402	Primo Impalcato	45, 78	0	-294.66	-0.03	0.00	0.00	0.56	-0.49
			100	-294.66	-0.03	0.00	0.00	1.05	-0.49
			199	-294.66	-0.03	0.00	0.00	1.54	-0.49
403	Primo Impalcato	46, 81	0	184.03	-0.03	0.00	0.00	0.55	-0.48
			100	184.03	-0.03	0.00	0.00	1.03	-0.48
			199	184.03	-0.03	0.00	0.00	1.51	-0.48
404	Primo Impalcato	77, 47	0	284.43	-0.07	0.00	0.00	1.25	0.84
			100	284.43	-0.07	0.00	0.00	0.41	0.84
			199	284.43	-0.07	0.00	0.00	-0.42	0.84
405	Primo Impalcato	80, 48	0	-174.30	-0.07	0.00	0.00	1.24	0.83
			100	-174.30	-0.07	0.00	0.00	0.42	0.83
			199	-174.30	-0.07	0.00	0.00	-0.40	0.83
406	Primo Impalcato	49, 77	0	-303.79	0.02	0.00	0.00	0.20	-0.75
			100	-303.79	0.02	0.00	0.00	0.95	-0.75
			199	-303.79	0.02	0.00	0.00	1.69	-0.75
407	Primo Impalcato	50, 80	0	187.53	0.01	0.00	0.00	0.21	-0.76
			100	187.53	0.01	0.00	0.00	0.96	-0.76
			199	187.53	0.01	0.00	0.00	1.71	-0.76
408	Primo Impalcato	76, 51	0	281.47	-0.03	0.00	0.00	1.64	0.76
			100	281.47	-0.03	0.00	0.00	0.88	0.76
			199	281.47	-0.03	0.00	0.00	0.12	0.76
409	Primo Impalcato	53, 76	0	-298.19	0.07	0.00	0.00	-0.46	-0.89
			100	-298.19	0.07	0.00	0.00	0.42	-0.89
			199	-298.19	0.07	0.00	0.00	1.30	-0.89
410	Primo Impalcato	75, 55	0	283.86	0.03	0.00	0.00	1.39	0.26
			102	283.86	0.03	0.00	0.00	1.13	0.26
			204	283.86	0.03	0.00	0.00	0.87	0.26
411	Primo Impalcato	56, 79	0	-200.28	0.06	0.00	0.00	-1.20	0.12

			102	-200.28	0.06	0.00	0.00	-1.32	0.12
			204	-200.28	0.06	0.00	0.00	-1.44	0.12
412	Primo Impalcato	57, 75	0	-338.55	0.19	0.00	0.00	-2.64	-1.19
			102	-338.55	0.19	0.00	0.00	-1.43	-1.19
			204	-338.55	0.19	0.00	0.00	-0.22	-1.19
413	Primo Impalcato	57, 93	0	493.68	0.16	0.00	0.00	-2.07	-0.87
			103	493.68	0.16	0.00	0.00	-1.18	-0.87
			206	493.68	0.16	0.00	0.00	-0.29	-0.87
414	Primo Impalcato	93, 58	0	-433.53	0.04	0.00	0.00	2.50	-0.75
			103	-433.53	0.04	0.00	0.00	3.27	-0.75
			206	-433.53	0.04	0.00	0.00	4.04	-0.75
415	Primo Impalcato	61, 95	0	514.31	0.02	0.00	0.00	1.65	-0.26
			100	514.31	0.02	0.00	0.00	1.91	-0.26
			200	514.31	0.02	0.00	0.00	2.17	-0.26
416	Primo Impalcato	95, 62	0	-491.41	-0.11	0.00	0.00	1.48	0.48
			100	-491.41	-0.11	0.00	0.00	1.00	0.48
			200	-491.41	-0.11	0.00	0.00	0.52	0.48
417	Primo Impalcato	96, 65	0	495.08	-0.07	0.00	0.00	-0.89	0.22
			100	495.08	-0.07	0.00	0.00	-1.11	0.22
			200	495.08	-0.07	0.00	0.00	-1.32	0.22
418	Primo Impalcato	66, 96	0	-517.09	-0.09	0.00	0.00	0.75	0.27
			100	-517.09	-0.09	0.00	0.00	0.48	0.27
			200	-517.09	-0.09	0.00	0.00	0.21	0.27
419	Primo Impalcato	69, 94	0	426.52	-0.02	0.00	0.00	-0.92	-0.13
			103	426.52	-0.02	0.00	0.00	-0.79	-0.13
			206	426.52	-0.02	0.00	0.00	-0.66	-0.13
420	Primo Impalcato	79, 70	0	270.18	0.09	0.00	0.00	-0.01	-0.83
			102	270.18	0.09	0.00	0.00	0.83	-0.83
			204	270.18	0.09	0.00	0.00	1.68	-0.83
421	Primo Impalcato	94, 70	0	-474.06	0.10	0.00	0.00	0.08	-0.92
			103	-474.06	0.10	0.00	0.00	1.02	-0.92
			206	-474.06	0.10	0.00	0.00	1.96	-0.92
422	Copertura	1, 2	0	7.99	-81.05	339.11	649.32	-91.47	37.05
			83	7.99	-81.05	878.84	649.32	-122.27	37.05
			166	7.99	-81.05	1418.56	649.32	-153.06	37.05
423	Copertura	15, 1	0	8.12	-6.71	-351.52	-82.29	65.41	101.30
			80	8.12	-6.71	-416.94	-82.29	-15.13	101.30
			159	8.12	-6.71	-482.36	-82.29	-95.67	101.30
424	Copertura	2, 3	0	71.29	-31.26	1423.58	-356.36	-154.09	-17.00
			69	71.29	-31.26	1177.69	-356.36	-142.36	-17.00
			138	71.29	-31.26	931.80	-356.36	-130.63	-17.00
425	Copertura	3, 4	0	72.25	-6.49	944.64	-431.43	-130.65	-3.85
			69	72.25	-6.49	646.95	-431.43	-128.00	-3.85
			138	72.25	-6.49	349.26	-431.43	-125.35	-3.85
426	Copertura	4, 5	0	73.22	3.20	362.31	-393.18	-125.40	5.57
			69	73.22	3.20	91.02	-393.18	-129.24	5.57
			138	73.22	3.20	-180.27	-393.18	-133.08	5.57
427	Copertura	5, 6	0	74.12	12.19	-166.59	-254.73	-133.36	16.04
			69	74.12	12.19	-342.35	-254.73	-144.42	16.04
			138	74.12	12.19	-518.11	-254.73	-155.49	16.04
428	Copertura	6, 7	0	107.03	20.59	-505.95	620.64	-156.14	-21.14
			69	107.03	20.59	-77.71	620.64	-141.55	-21.14
			138	107.03	20.59	350.53	620.64	-126.96	-21.14
429	Copertura	7, 8	0	132.29	27.23	362.62	-263.08	-128.20	-49.49
			69	132.29	27.23	181.10	-263.08	-94.05	-49.49
			138	132.29	27.23	-0.43	-263.08	-59.90	-49.49
430	Copertura	8, 9	0	132.92	29.97	13.56	-282.35	-60.84	-43.41
			69	132.92	29.97	-181.26	-282.35	-30.89	-43.41
			138	132.92	29.97	-376.09	-282.35	-0.94	-43.41
431	Copertura	9, 10	0	149.41	28.52	-363.98	557.29	-2.33	-50.42
			69	149.41	28.52	20.55	557.29	32.45	-50.42
			138	149.41	28.52	405.07	557.29	67.24	-50.42
432	Copertura	10, 11	0	166.36	23.73	417.19	-354.69	66.02	-46.21

			69	166.36	23.73	172.46	-354.69	97.91	-46.21
			138	166.36	23.73	-72.27	-354.69	129.79	-46.21
433	Copertura	11, 12	0	166.98	14.18	-58.79	-501.05	129.07	-47.66
			69	166.98	14.18	-404.52	-501.05	161.95	-47.66
			138	166.98	14.18	-750.25	-501.05	194.84	-47.66
434	Copertura	12, 13	0	167.61	-6.78	-737.26	-414.39	194.32	-52.82
			69	167.61	-6.78	-1023.19	-414.39	230.77	-52.82
			138	167.61	-6.78	-1309.13	-414.39	267.21	-52.82
435	Copertura	13, 14	0	192.50	-12.39	-1299.96	604.56	265.87	-22.43
			83	192.50	-12.39	-797.43	604.56	284.52	-22.43
			166	192.50	-12.39	-294.91	604.56	303.17	-22.43
436	Copertura	16, 14	0	13.48	-5.96	66.12	77.79	96.41	250.92
			80	13.48	-5.96	127.97	77.79	-103.07	250.92
			159	13.48	-5.96	189.81	77.79	-302.56	250.92
437	Copertura	15, 17	0	55.72	-3.70	-509.02	309.64	-84.37	55.07
			66	55.72	-3.70	-304.66	309.64	-120.72	55.07
			132	55.72	-3.70	-100.30	309.64	-157.07	55.07
438	Copertura	16, 18	0	-16.74	-1.94	134.59	-178.85	-82.87	72.30
			66	-16.74	-1.94	16.55	-178.85	-130.59	72.30
			132	-16.74	-1.94	-101.50	-178.85	-178.31	72.30
439	Copertura	17, 19	0	94.21	-1.73	-256.40	184.31	-178.84	-13.47
			66	94.21	-1.73	-134.75	184.31	-169.94	-13.47
			132	94.21	-1.73	-13.11	184.31	-161.05	-13.47
440	Copertura	18, 20	0	-31.92	-1.09	-20.85	-36.37	-172.96	-1.48
			66	-31.92	-1.09	-44.86	-36.37	-171.99	-1.48
			132	-31.92	-1.09	-68.86	-36.37	-171.02	-1.48
441	Copertura	19, 21	0	124.70	0.06	-169.70	214.40	-192.85	-52.26
			66	124.70	0.06	-28.20	214.40	-158.36	-52.26
			132	124.70	0.06	113.30	214.40	-123.87	-52.26
442	Copertura	20, 22	0	-48.16	0.09	10.96	-101.26	-183.92	-40.21
			66	-48.16	0.09	-55.87	-101.26	-157.38	-40.21
			132	-48.16	0.09	-122.70	-101.26	-130.84	-40.21
443	Copertura	21, 23	0	145.97	1.40	-43.26	105.57	-163.16	-65.93
			66	145.97	1.40	26.41	105.57	-119.65	-65.93
			132	145.97	1.40	96.09	105.57	-76.14	-65.93
444	Copertura	22, 24	0	-63.52	1.47	-42.63	-4.09	-156.66	-57.72
			66	-63.52	1.47	-45.33	-4.09	-118.56	-57.72
			132	-63.52	1.47	-48.03	-4.09	-80.47	-57.72
445	Copertura	23, 25	0	155.70	2.27	-60.34	136.20	-117.44	-70.28
			66	155.70	2.27	29.55	136.20	-71.06	-70.28
			132	155.70	2.27	119.44	136.20	-24.67	-70.28
446	Copertura	24, 26	0	-77.02	1.92	31.70	-93.38	-117.15	-56.16
			66	-77.02	1.92	-29.93	-93.38	-80.09	-56.16
			132	-77.02	1.92	-91.56	-93.38	-43.02	-56.16
447	Copertura	25, 28	0	153.21	2.51	-36.71	15.08	-62.75	-38.02
			85	153.21	2.51	-23.90	15.08	-30.43	-38.02
			170	153.21	2.51	-11.08	15.08	1.88	-38.02
448	Copertura	26, 27	0	-85.18	3.05	-11.45	-6.94	-82.93	-68.39
			66	-85.18	3.05	-16.03	-6.94	-37.79	-68.39
			132	-85.18	3.05	-20.61	-6.94	7.34	-68.39
449	Copertura	27, 29	0	-82.97	2.68	60.13	-101.04	-28.32	-43.39
			66	-82.97	2.68	-6.55	-101.04	0.31	-43.39
			132	-82.97	2.68	-73.24	-101.04	28.95	-43.39
450	Copertura	28, 30	0	128.85	2.81	-164.67	119.69	-22.99	-27.25
			73	128.85	2.81	-77.30	119.69	-3.10	-27.25
			146	128.85	2.81	10.07	119.69	16.79	-27.25
451	Copertura	29, 31	0	-69.98	2.95	7.59	-15.20	2.41	-18.11
			66	-69.98	2.95	-2.44	-15.20	14.37	-18.11
			132	-69.98	2.95	-12.48	-15.20	26.32	-18.11
452	Copertura	30, 32	0	90.85	2.65	-144.66	137.44	1.91	-13.65
			69	90.85	2.65	-50.52	137.44	11.26	-13.65
			137	90.85	2.65	43.63	137.44	20.61	-13.65
453	Copertura	31, 33	0	-46.81	2.49	68.71	-104.12	10.23	-4.03
			66	-46.81	2.49	-0.01	-104.12	12.89	-4.03
			132	-46.81	2.49	-68.73	-104.12	15.55	-4.03
454	Copertura	32, 34	0	45.86	2.64	-111.62	127.00	12.68	0.19
			69	45.86	2.64	-23.98	127.00	12.55	0.19
			138	45.86	2.64	63.65	127.00	12.42	0.19
455	Copertura	33, 35	0	-18.66	2.73	8.89	-13.35	8.65	6.22
			66	-18.66	2.73	0.07	-13.35	4.54	6.22
			132	-18.66	2.73	-8.74	-13.35	0.44	6.22
456	Copertura	34, 36	0	-2.32	2.44	-92.47	125.52	8.41	5.53

			69	-2.32	2.44	-5.87	125.52	4.59	5.53
			138	-2.32	2.44	80.74	125.52	0.78	5.53
457	Copertura	35, 37	0	17.95	2.42	74.49	-100.23	-2.47	5.03
			66	17.95	2.42	8.33	-100.23	-5.79	5.03
			132	17.95	2.42	-57.82	-100.23	-9.10	5.03
458	Copertura	36, 38	0	-49.91	2.58	-76.42	137.25	-3.15	2.50
			69	-49.91	2.58	18.28	137.25	-4.88	2.50
			138	-49.91	2.58	112.98	137.25	-6.60	2.50
459	Copertura	37, 39	0	50.24	2.93	20.10	-6.78	-15.15	-8.35
			66	50.24	2.93	15.62	-6.78	-9.64	-8.35
			132	50.24	2.93	11.15	-6.78	-4.12	-8.35
460	Copertura	38, 40	0	-94.08	2.41	-45.37	160.94	-13.85	-4.70
			69	-94.08	2.41	64.87	160.94	-10.63	-4.70
			137	-94.08	2.41	175.12	160.94	-7.41	-4.70
461	Copertura	39, 41	0	80.58	2.83	89.47	-113.18	-16.96	-35.15
			66	80.58	2.83	14.77	-113.18	6.24	-35.15
			132	80.58	2.83	-59.93	-113.18	29.44	-35.15
462	Copertura	40, 42	0	-133.20	2.39	15.18	160.57	-20.19	-14.62
			69	-133.20	2.39	125.98	160.57	-10.10	-14.62
			138	-133.20	2.39	236.77	160.57	-0.01	-14.62
463	Copertura	41, 44	0	105.18	1.95	17.41	-63.09	11.67	9.05
			66	105.18	1.95	-24.22	-63.09	5.69	9.05
			132	105.18	1.95	-65.86	-63.09	-0.28	9.05
464	Copertura	42, 43	0	-162.06	5.51	75.70	53.61	-18.78	-104.15
			23	-162.06	5.51	88.03	53.61	5.17	-104.15
			46	-162.06	5.51	100.36	53.61	29.13	-104.15
465	Copertura	43, 45	0	-177.17	2.48	-54.72	45.92	-1.62	-49.15
			66	-177.17	2.48	-24.41	45.92	30.82	-49.15
			132	-177.17	2.48	5.90	45.92	63.26	-49.15
466	Copertura	44, 46	0	101.89	2.68	11.39	-35.23	-36.17	-72.78
			66	101.89	2.68	-11.87	-35.23	11.87	-72.78
			132	101.89	2.68	-35.12	-35.23	59.90	-72.78
467	Copertura	45, 47	0	-178.37	2.05	-149.98	154.24	24.31	-66.85
			66	-178.37	2.05	-48.19	154.24	68.43	-66.85
			132	-178.37	2.05	53.61	154.24	112.55	-66.85
468	Copertura	46, 48	0	93.21	2.44	42.97	-24.96	20.10	-69.54
			66	93.21	2.44	26.49	-24.96	66.00	-69.54
			132	93.21	2.44	10.02	-24.96	111.90	-69.54
469	Copertura	47, 49	0	-167.20	1.65	-102.31	105.92	69.79	-70.58
			66	-167.20	1.65	-32.41	105.92	116.37	-70.58
			132	-167.20	1.65	37.50	105.92	162.95	-70.58
470	Copertura	48, 50	0	79.85	1.34	88.39	-24.22	75.71	-62.24
			66	79.85	1.34	72.41	-24.22	116.78	-62.24
			132	79.85	1.34	56.43	-24.22	157.86	-62.24
471	Copertura	49, 51	0	-144.93	0.16	-118.70	212.90	122.12	-56.52
			66	-144.93	0.16	21.82	212.90	159.43	-56.52
			132	-144.93	0.16	162.33	212.90	196.73	-56.52
472	Copertura	50, 52	0	64.31	0.32	135.49	-53.39	129.61	-43.19
			66	64.31	0.32	100.26	-53.39	158.11	-43.19
			132	64.31	0.32	65.02	-53.39	186.61	-43.19
473	Copertura	51, 53	0	-113.64	-1.54	6.12	181.68	163.50	-17.04
			66	-113.64	-1.54	126.03	181.68	174.74	-17.04
			132	-113.64	-1.54	245.93	181.68	185.99	-17.04
474	Copertura	52, 54	0	48.43	-1.11	144.63	-143.59	174.58	-5.44
			66	48.43	-1.11	49.86	-143.59	178.17	-5.44
			132	48.43	-1.11	-44.91	-143.59	181.76	-5.44
475	Copertura	53, 55	0	-74.62	-3.67	90.10	312.01	163.53	50.99
			66	-74.62	-3.67	296.02	312.01	129.87	50.99
			132	-74.62	-3.67	501.95	312.01	96.22	50.99
476	Copertura	54, 56	0	32.32	-1.97	34.06	-123.48	184.98	65.21
			66	32.32	-1.97	-47.43	-123.48	141.94	65.21
			132	32.32	-1.97	-128.93	-123.48	98.90	65.21
477	Copertura	55, 57	0	-27.01	-7.14	344.74	88.49	77.59	79.23
			80	-27.01	-7.14	415.09	88.49	14.61	79.23
			159	-27.01	-7.14	485.44	88.49	-48.37	79.23
478	Copertura	56, 70	0	15.10	-5.69	-49.26	-79.61	114.51	265.09
			80	15.10	-5.69	-112.55	-79.61	-96.24	265.09
			159	15.10	-5.69	-175.84	-79.61	-306.99	265.09
479	Copertura	57, 58	0	-27.12	-85.08	-334.65	-603.80	-43.74	60.21
			83	-27.12	-85.08	-836.54	-603.80	-93.79	60.21
			166	-27.12	-85.08	-1338.43	-603.80	-143.84	60.21
480	Copertura	58, 59	0	-85.21	-33.78	-1343.07	400.44	-144.63	1.77

			69	-85.21	-33.78	-1066.76	400.44	-145.86	1.77
			138	-85.21	-33.78	-790.45	400.44	-147.08	1.77
481	Copertura	59, 60	0	-85.88	-8.55	-802.92	485.98	-147.00	15.62
			69	-85.88	-8.55	-467.60	485.98	-157.78	15.62
			138	-85.88	-8.55	-132.27	485.98	-168.55	15.62
482	Copertura	60, 61	0	-86.85	2.98	-145.29	328.74	-168.55	26.31
			69	-86.85	2.98	81.55	328.74	-186.71	26.31
			138	-86.85	2.98	308.38	328.74	-204.86	26.31
483	Copertura	61, 62	0	-126.62	14.19	296.59	-582.12	-205.12	-19.65
			69	-126.62	14.19	-105.07	-582.12	-191.56	-19.65
			138	-126.62	14.19	-506.73	-582.12	-178.00	-19.65
484	Copertura	62, 63	0	-155.69	23.90	-518.63	222.12	-179.08	-55.45
			69	-155.69	23.90	-365.36	222.12	-140.82	-55.45
			138	-155.69	23.90	-212.10	222.12	-102.56	-55.45
485	Copertura	63, 64	0	-156.25	29.54	-225.53	321.07	-103.45	-46.46
			69	-156.25	29.54	-3.99	321.07	-71.40	-46.46
			138	-156.25	29.54	217.54	321.07	-39.34	-46.46
486	Copertura	64, 65	0	-156.76	31.54	204.10	219.32	-40.34	-40.48
			69	-156.76	31.54	355.43	219.32	-12.41	-40.48
			138	-156.76	31.54	506.77	219.32	15.52	-40.48
487	Copertura	65, 66	0	-170.36	29.46	494.84	-591.60	14.06	-47.58
			69	-170.36	29.46	86.64	-591.60	46.89	-47.58
			138	-170.36	29.46	-321.56	-591.60	79.72	-47.58
488	Copertura	66, 67	0	-184.51	24.13	-333.41	318.43	78.48	-43.51
			69	-184.51	24.13	-113.69	318.43	108.50	-43.51
			138	-184.51	24.13	106.03	318.43	138.53	-43.51
489	Copertura	67, 68	0	-185.02	14.11	92.91	473.84	137.80	-45.16
			69	-185.02	14.11	419.86	473.84	168.96	-45.16
			138	-185.02	14.11	746.81	473.84	200.12	-45.16
490	Copertura	68, 69	0	-185.56	-7.04	734.20	396.97	199.62	-50.42
			69	-185.56	-7.04	1008.11	396.97	234.41	-50.42
			138	-185.56	-7.04	1282.02	396.97	269.20	-50.42
491	Copertura	69, 70	0	-210.80	-13.05	1273.20	-592.63	267.91	-22.55
			83	-210.80	-13.05	780.60	-592.63	286.65	-22.55
			166	-210.80	-13.05	287.99	-592.63	305.39	-22.55
492	Copertura	1	0	-320.96	-0.70	369.55	-163.48	-326.78	-117.28
			220	-320.96	-0.70	9.89	-163.48	-68.77	-117.28
			440	-320.96	-0.70	-349.77	-163.48	189.25	-117.28
493	Copertura	2	0	505.71	-0.31	124.57	-53.45	-11.38	-5.28
			220	505.71	-0.31	6.99	-53.45	0.24	-5.28
			440	505.71	-0.31	-110.59	-53.45	11.87	-5.28
494	Copertura	3	0	75.07	-0.02	24.77	-16.30	-12.84	-5.95
			220	75.07	-0.02	-11.10	-16.30	0.26	-5.95
			440	75.07	-0.02	-46.97	-16.30	13.36	-5.95
495	Copertura	4	0	-38.25	-0.05	9.69	-12.07	-13.05	-5.92
			220	-38.25	-0.05	-16.87	-12.07	-0.02	-5.92
			440	-38.25	-0.05	-43.42	-12.07	13.01	-5.92
496	Copertura	5	0	-138.45	-0.27	8.99	-12.87	-13.69	-6.33
			220	-138.45	-0.27	-19.34	-12.87	0.24	-6.33
			440	-138.45	-0.27	-47.66	-12.87	14.16	-6.33
497	Copertura	6	0	-330.57	-0.55	8.57	-12.55	-12.16	-5.38
			220	-330.57	-0.55	-19.05	-12.55	-0.32	-5.38
			440	-330.57	-0.55	-46.67	-12.55	11.51	-5.38
498	Copertura	7	0	336.77	-0.79	5.68	-10.13	-12.09	-5.35
			220	336.77	-0.79	-16.62	-10.13	-0.31	-5.35
			440	336.77	-0.79	-38.91	-10.13	11.47	-5.35
499	Copertura	8	0	19.27	-0.94	2.74	-7.05	-13.99	-6.60
			220	19.27	-0.94	-12.77	-7.05	0.53	-6.60
			440	19.27	-0.94	-28.27	-7.05	15.05	-6.60
500	Copertura	9	0	-301.38	-0.98	-0.55	-3.73	-12.10	-5.36
			220	-301.38	-0.98	-8.76	-3.73	-0.31	-5.36
			440	-301.38	-0.98	-16.97	-3.73	11.49	-5.36
501	Copertura	10	0	358.11	-0.90	-5.42	-0.18	-12.12	-5.37
			220	358.11	-0.90	-5.82	-0.18	-0.31	-5.37
			440	358.11	-0.90	-6.23	-0.18	11.49	-5.37
502	Copertura	11	0	146.37	-0.72	-9.55	2.11	-13.48	-6.25
			220	146.37	-0.72	-4.90	2.11	0.26	-6.25
			440	146.37	-0.72	-0.25	2.11	14.01	-6.25
503	Copertura	12	0	-86.66	-0.51	-20.95	6.30	-12.98	-6.02
			220	-86.66	-0.51	-7.08	6.30	0.26	-6.02
			440	-86.66	-0.51	6.78	6.30	13.50	-6.02
504	Copertura	13	0	-484.61	-0.36	-73.65	25.18	-11.62	-5.37

			220	-484.61	-0.36	-18.26	25.18	0.19	-5.37
			440	-484.61	-0.36	37.13	25.18	12.00	-5.37
505	Copertura	57	0	294.07	-0.27	368.83	-163.12	321.68	115.38
			220	294.07	-0.27	9.97	-163.12	67.85	115.38
			440	294.07	-0.27	-348.89	-163.12	-185.98	115.38
506	Copertura	58	0	-512.16	-0.19	121.97	-52.95	11.11	5.16
			220	-512.16	-0.19	5.48	-52.95	-0.24	5.16
			440	-512.16	-0.19	-111.01	-52.95	-11.59	5.16
507	Copertura	59	0	-85.54	0.08	25.23	-17.09	12.47	5.79
			220	-85.54	0.08	-12.37	-17.09	-0.28	5.79
			440	-85.54	0.08	-49.96	-17.09	-13.02	5.79
508	Copertura	60	0	157.24	0.00	11.53	-13.43	13.02	6.04
			220	157.24	0.00	-18.01	-13.43	-0.26	6.04
			440	157.24	0.00	-47.55	-13.43	-13.55	6.04
509	Copertura	61	0	366.07	-0.32	11.04	-14.32	11.79	5.22
			220	366.07	-0.32	-20.45	-14.32	0.30	5.22
			440	366.07	-0.32	-51.95	-14.32	-11.19	5.22
510	Copertura	62	0	-280.93	-0.65	8.78	-13.12	11.89	5.26
			220	-280.93	-0.65	-20.09	-13.12	0.32	5.26
			440	-280.93	-0.65	-48.97	-13.12	-11.26	5.26
511	Copertura	63	0	-98.95	-0.89	5.64	-10.44	13.43	6.21
			220	-98.95	-0.89	-17.33	-10.44	-0.23	6.21
			440	-98.95	-0.89	-40.31	-10.44	-13.90	6.21
512	Copertura	64	0	101.75	-1.00	2.00	-6.91	13.45	6.22
			220	101.75	-1.00	-13.19	-6.91	-0.23	6.22
			440	101.75	-1.00	-28.39	-6.91	-13.91	6.22
513	Copertura	65	0	285.62	-1.02	-1.12	-3.63	11.92	5.28
			220	285.62	-1.02	-9.10	-3.63	0.32	5.28
			440	285.62	-1.02	-17.07	-3.63	-11.29	5.28
514	Copertura	66	0	-363.54	-0.92	-5.96	-0.02	11.85	5.25
			220	-363.54	-0.92	-5.99	-0.02	0.30	5.25
			440	-363.54	-0.92	-6.03	-0.02	-11.24	5.25
515	Copertura	67	0	-155.41	-0.73	-10.02	2.31	13.12	6.08
			220	-155.41	-0.73	-4.93	2.31	-0.26	6.08
			440	-155.41	-0.73	0.15	2.31	-13.64	6.08
516	Copertura	68	0	76.87	-0.50	-21.14	6.39	12.61	5.85
			220	76.87	-0.50	-7.08	6.39	-0.26	5.85
			440	76.87	-0.50	6.98	6.39	-13.12	5.85
517	Copertura	69	0	470.73	-0.33	-72.63	24.74	11.26	5.21
			220	470.73	-0.33	-18.21	24.74	-0.19	5.21
			440	470.73	-0.33	36.22	24.74	-11.65	5.21
518	Primo Impalcato	1, 74	0	534.47	-0.20	0.00	0.00	13.64	7.56
			118	534.47	-0.20	0.00	0.00	4.75	7.56
			235	534.47	-0.20	0.00	0.00	-4.14	7.56
519	Copertura	74, 2	0	-438.99	0.09	0.00	0.00	3.29	0.86
			118	-438.99	0.09	0.00	0.00	2.27	0.86
			235	-438.99	0.09	0.00	0.00	1.26	0.86
520	Primo Impalcato	6, 71	0	573.23	-0.12	0.00	0.00	0.69	0.44
			115	573.23	-0.12	0.00	0.00	0.17	0.44
			231	573.23	-0.12	0.00	0.00	-0.34	0.44
521	Copertura	71, 7	0	-570.97	-0.05	0.00	0.00	1.04	-0.23
			115	-570.97	-0.05	0.00	0.00	1.31	-0.23
			231	-570.97	-0.05	0.00	0.00	1.57	-0.23
522	Primo Impalcato	9, 72	0	580.46	-0.13	0.00	0.00	-0.40	0.16
			115	580.46	-0.13	0.00	0.00	-0.59	0.16
			231	580.46	-0.13	0.00	0.00	-0.78	0.16
523	Copertura	72, 10	0	-564.11	-0.11	0.00	0.00	1.16	0.11
			115	-564.11	-0.11	0.00	0.00	1.03	0.11
			231	-564.11	-0.11	0.00	0.00	0.90	0.11
524	Copertura	73, 13	0	478.57	0.07	0.00	0.00	0.67	0.13
			118	478.57	0.07	0.00	0.00	0.52	0.13
			235	478.57	0.07	0.00	0.00	0.37	0.13
525	Primo Impalcato	14, 73	0	-571.22	-0.11	0.00	0.00	4.93	2.89
			118	-571.22	-0.11	0.00	0.00	1.54	2.89
			235	-571.22	-0.11	0.00	0.00	-1.86	2.89
526	Primo Impalcato	57, 75	0	-526.03	-0.19	0.00	0.00	13.65	7.50
			118	-526.03	-0.19	0.00	0.00	4.83	7.50
			235	-526.03	-0.19	0.00	0.00	-3.98	7.50

527	Copertura	75, 58	0	425.70	0.10	0.00	0.00	3.21	0.86
			118	425.70	0.10	0.00	0.00	2.20	0.86
			235	425.70	0.10	0.00	0.00	1.18	0.86
528	Copertura	77, 61	0	-548.44	-0.10	0.00	0.00	0.10	0.46
			115	-548.44	-0.10	0.00	0.00	-0.43	0.46
			231	-548.44	-0.10	0.00	0.00	-0.96	0.46
529	Primo Impalcato	62, 77	0	570.95	-0.02	0.00	0.00	-1.75	-0.38
			115	570.95	-0.02	0.00	0.00	-1.31	-0.38
			231	570.95	-0.02	0.00	0.00	-0.87	-0.38
530	Primo Impalcato	65, 78	0	-572.74	-0.13	0.00	0.00	-0.42	0.16
			115	-572.74	-0.13	0.00	0.00	-0.61	0.16
			231	-572.74	-0.13	0.00	0.00	-0.79	0.16
531	Copertura	78, 66	0	550.54	-0.12	0.00	0.00	1.21	0.13
			115	550.54	-0.12	0.00	0.00	1.06	0.13
			231	550.54	-0.12	0.00	0.00	0.91	0.13
532	Primo Impalcato	69, 76	0	-461.98	0.08	0.00	0.00	-0.30	0.15
			118	-461.98	0.08	0.00	0.00	-0.48	0.15
			235	-461.98	0.08	0.00	0.00	-0.66	0.15
533	Copertura	76, 70	0	554.67	-0.11	0.00	0.00	1.83	2.91
			118	554.67	-0.11	0.00	0.00	-1.58	2.91
			235	554.67	-0.11	0.00	0.00	-5.00	2.91
534	Copertura	1, 74	0	-438.99	-0.20	0.00	0.00	-14.40	-7.51
			118	-438.99	-0.20	0.00	0.00	-5.57	-7.51
			235	-438.99	-0.20	0.00	0.00	3.27	-7.51
535	Copertura	74, 2	0	534.47	0.00	0.00	0.00	-3.93	-0.81
			118	534.47	0.00	0.00	0.00	-2.98	-0.81
			235	534.47	0.00	0.00	0.00	-2.02	-0.81
536	Copertura	6, 71	0	-570.97	-0.04	0.00	0.00	0.19	-0.36
			115	-570.97	-0.04	0.00	0.00	0.61	-0.36
			231	-570.97	-0.04	0.00	0.00	1.02	-0.36
537	Copertura	71, 7	0	573.23	-0.14	0.00	0.00	-0.33	0.31
			115	573.23	-0.14	0.00	0.00	-0.69	0.31
			231	573.23	-0.14	0.00	0.00	-1.05	0.31
538	Copertura	9, 72	0	-564.11	-0.13	0.00	0.00	0.97	-0.08
			115	-564.11	-0.13	0.00	0.00	1.07	-0.08
			231	-564.11	-0.13	0.00	0.00	1.16	-0.08
539	Copertura	72, 10	0	580.46	-0.12	0.00	0.00	-0.76	-0.03
			115	580.46	-0.12	0.00	0.00	-0.73	-0.03
			231	580.46	-0.12	0.00	0.00	-0.69	-0.03
540	Copertura	73, 13	0	-571.22	-0.09	0.00	0.00	-1.75	0.33
			118	-571.22	-0.09	0.00	0.00	-2.14	0.33
			235	-571.22	-0.09	0.00	0.00	-2.53	0.33
541	Copertura	14, 73	0	478.57	-0.01	0.00	0.00	-5.12	-2.43
			118	478.57	-0.01	0.00	0.00	-2.26	-2.43
			235	478.57	-0.01	0.00	0.00	0.60	-2.43
542	Copertura	15, 125	0	-170.82	-7.56	-12.81	167.40	21.15	55.92
			75	-170.82	-7.56	112.74	167.40	-20.79	55.92
			150	-170.82	-7.56	238.29	167.40	-62.72	55.92
543	Copertura	127, 16	0	68.65	-3.37	-255.14	181.90	62.85	33.24
			75	68.65	-3.37	-118.72	181.90	37.92	33.24
			150	68.65	-3.37	17.70	181.90	12.99	33.24
544	Copertura	17, 129	0	-185.82	-7.19	-26.12	220.64	23.74	49.98
			75	-185.82	-7.19	139.36	220.64	-13.75	49.98
			150	-185.82	-7.19	304.85	220.64	-51.23	49.98
545	Copertura	130, 18	0	208.48	-3.78	-309.49	223.01	50.87	31.02
			75	208.48	-3.78	-142.23	223.01	27.60	31.02
			150	208.48	-3.78	25.03	223.01	4.34	31.02
546	Copertura	19, 135	0	-220.84	-6.78	-22.68	238.90	33.28	46.70
			75	-220.84	-6.78	156.49	238.90	-1.75	46.70
			150	-220.84	-6.78	335.66	238.90	-36.77	46.70
547	Copertura	134, 20	0	244.92	-3.04	-335.88	237.62	37.32	33.36
			75	244.92	-3.04	-157.66	237.62	12.30	33.36
			150	244.92	-3.04	20.55	237.62	-12.71	33.36
548	Copertura	21, 136	0	-240.60	-6.35	-25.91	242.26	40.36	42.18
			75	-240.60	-6.35	155.79	242.26	8.73	42.18
			150	-240.60	-6.35	337.49	242.26	-22.91	42.18
549	Copertura	138, 22	0	260.47	-2.98	-337.67	241.83	23.74	33.15
			75	260.47	-2.98	-156.29	241.83	-1.12	33.15
			150	260.47	-2.98	25.09	241.83	-25.99	33.15
550	Copertura	23, 141	0	-220.56	-6.06	-19.76	219.02	42.12	35.94

			75	-220.56	-6.06	144.50	219.02	15.16	35.94
			150	-220.56	-6.06	308.76	219.02	-11.80	35.94
551	Copertura	142, 24	0	247.63	-2.46	-308.20	217.01	13.63	33.11
			75	247.63	-2.46	-145.44	217.01	-11.20	33.11
			150	247.63	-2.46	17.32	217.01	-36.03	33.11
552	Copertura	25, 145	0	-226.68	-5.85	-20.34	192.08	38.79	28.48
			75	-226.68	-5.85	123.73	192.08	17.43	28.48
			150	-226.68	-5.85	267.79	192.08	-3.93	28.48
553	Copertura	146, 26	0	200.69	-2.44	-269.70	193.28	5.91	30.27
			75	200.69	-2.44	-124.74	193.28	-16.79	30.27
			150	200.69	-2.44	20.23	193.28	-39.49	30.27
554	Copertura	150, 27	0	174.49	-2.27	-205.99	136.76	0.24	23.54
			75	174.49	-2.27	-103.42	136.76	-17.41	23.54
			150	174.49	-2.27	-0.85	136.76	-35.06	23.54
555	Copertura	28, 149	0	-170.48	-5.65	-34.89	160.77	25.71	15.43
			75	-170.48	-5.65	85.69	160.77	14.13	15.43
			150	-170.48	-5.65	206.27	160.77	2.56	15.43
556	Copertura	154, 29	0	130.42	-2.25	-151.52	98.92	-2.19	15.88
			75	130.42	-2.25	-77.34	98.92	-14.10	15.88
			150	130.42	-2.25	-3.15	98.92	-26.01	15.88
557	Copertura	30, 153	0	-140.93	-5.68	-42.38	128.12	15.86	7.09
			75	-140.93	-5.68	53.71	128.12	10.55	7.09
			150	-140.93	-5.68	149.81	128.12	5.23	7.09
558	Copertura	158, 31	0	72.00	-2.30	-93.62	53.59	-3.14	8.41
			75	72.00	-2.30	-53.42	53.59	-9.45	8.41
			150	72.00	-2.30	-13.23	53.59	-15.76	8.41
559	Copertura	32, 157	0	-105.84	-5.72	-43.01	91.81	9.03	2.05
			75	-105.84	-5.72	25.85	91.81	7.49	2.05
			150	-105.84	-5.72	94.71	91.81	5.95	2.05
560	Copertura	162, 33	0	32.46	-2.20	-44.64	21.70	-3.56	2.07
			75	32.46	-2.20	-28.37	21.70	-5.11	2.07
			150	32.46	-2.20	-12.10	21.70	-6.67	2.07
561	Copertura	34, 161	0	-64.67	-5.77	-43.34	57.93	5.18	-0.56
			75	-64.67	-5.77	0.10	57.93	5.61	-0.56
			150	-64.67	-5.77	43.55	57.93	6.03	-0.56
562	Copertura	166, 35	0	-23.52	-2.36	8.80	-21.31	-3.92	-0.82
			75	-23.52	-2.36	-7.18	-21.31	-3.31	-0.82
			150	-23.52	-2.36	-23.17	-21.31	-2.69	-0.82
563	Copertura	36, 165	0	-24.00	-5.80	-44.14	24.58	5.11	-0.52
			75	-24.00	-5.80	-25.70	24.58	5.50	-0.52
			150	-24.00	-5.80	-7.27	24.58	5.89	-0.52
564	Copertura	170, 37	0	-68.49	-2.20	56.13	-51.43	-3.55	1.52
			75	-68.49	-2.20	17.56	-51.43	-4.69	1.52
			150	-68.49	-2.20	-21.02	-51.43	-5.84	1.52
565	Copertura	38, 169	0	12.08	-5.82	-44.45	-8.34	8.37	1.81
			75	12.08	-5.82	-50.70	-8.34	7.01	1.81
			150	12.08	-5.82	-56.95	-8.34	5.66	1.81
566	Copertura	175, 39	0	-126.59	-2.16	111.91	-95.66	-2.99	6.33
			75	-126.59	-2.16	40.16	-95.66	-7.74	6.33
			150	-126.59	-2.16	-31.58	-95.66	-12.49	6.33
567	Copertura	40, 173	0	47.98	-5.85	-45.49	-41.80	13.81	5.66
			75	47.98	-5.85	-76.84	-41.80	9.56	5.66
			150	47.98	-5.85	-108.19	-41.80	5.31	5.66
568	Copertura	178, 41	0	-92.49	-2.12	163.77	-131.84	-1.57	10.52
			75	-92.49	-2.12	64.89	-131.84	-9.46	10.52
			150	-92.49	-2.12	-33.99	-131.84	-17.35	10.52
569	Copertura	42, 177	0	156.66	-5.85	-53.22	-69.20	19.71	10.18
			75	156.66	-5.85	-105.12	-69.20	12.07	10.18
			150	156.66	-5.85	-157.01	-69.20	4.43	10.18
570	Copertura	43, 181	0	91.93	-5.75	16.55	-148.53	31.53	20.66
			75	91.93	-5.75	-94.85	-148.53	16.04	20.66
			150	91.93	-5.75	-206.25	-148.53	0.54	20.66
571	Copertura	182, 44	0	-240.02	-2.21	203.83	-142.57	2.84	25.43
			75	-240.02	-2.21	96.90	-142.57	-16.23	25.43
			150	-240.02	-2.21	-10.02	-142.57	-35.30	25.43
572	Copertura	45, 185	0	205.50	-5.84	19.68	-184.90	39.65	28.87
			75	205.50	-5.84	-118.99	-184.90	18.00	28.87
			150	205.50	-5.84	-257.66	-184.90	-3.66	28.87
573	Copertura	186, 46	0	-199.93	-2.25	256.51	-181.93	6.02	30.09
			75	-199.93	-2.25	120.06	-181.93	-16.55	30.09
			150	-199.93	-2.25	-16.39	-181.93	-39.12	30.09
574	Copertura	47, 189	0	222.92	-6.00	18.22	-211.98	43.53	36.36

			75	222.92	-6.00	-140.76	-211.98	16.26	36.36
			150	222.92	-6.00	-299.75	-211.98	-11.01	36.36
575	Copertura	190, 48	0	-234.19	-2.56	301.98	-214.48	12.50	32.29
			75	-234.19	-2.56	141.12	-214.48	-11.72	32.29
			150	-234.19	-2.56	-19.74	-214.48	-35.94	32.29
576	Copertura	49, 193	0	236.22	-6.32	25.61	-237.69	41.84	42.54
			75	236.22	-6.32	-152.65	-237.69	9.94	42.54
			150	236.22	-6.32	-330.92	-237.69	-21.97	42.54
577	Copertura	195, 50	0	-252.46	-2.64	330.45	-235.41	23.08	33.87
			75	-252.46	-2.64	153.89	-235.41	-2.32	33.87
			150	-252.46	-2.64	-22.67	-235.41	-27.73	33.87
578	Copertura	51, 197	0	218.04	-6.72	22.37	-236.54	34.67	46.98
			75	218.04	-6.72	-155.03	-236.54	-0.57	46.98
			150	218.04	-6.72	-332.44	-236.54	-35.80	46.98
579	Copertura	199, 52	0	-247.56	-3.34	334.03	-239.42	35.88	32.33
			75	-247.56	-3.34	154.47	-239.42	11.63	32.33
			150	-247.56	-3.34	-25.10	-239.42	-12.62	32.33
580	Copertura	53, 201	0	185.14	-7.19	26.26	-219.51	24.41	50.11
			75	185.14	-7.19	-138.38	-219.51	-13.17	50.11
			150	185.14	-7.19	-303.01	-219.51	-50.75	50.11
581	Copertura	202, 54	0	-203.10	-3.38	305.97	-217.22	50.82	31.86
			75	-203.10	-3.38	143.06	-217.22	26.93	31.86
			150	-203.10	-3.38	-19.85	-217.22	3.03	31.86
582	Copertura	55, 205	0	187.33	-7.52	12.86	-166.51	20.81	55.81
			75	187.33	-7.52	-112.02	-166.51	-21.04	55.81
			150	187.33	-7.52	-236.90	-166.51	-62.90	55.81
583	Copertura	206, 56	0	-52.36	-3.95	252.92	-182.09	62.44	31.94
			75	-52.36	-3.95	116.35	-182.09	38.49	31.94
			150	-52.36	-3.95	-20.21	-182.09	14.53	31.94
584	Copertura	57, 75	0	425.70	-0.20	0.00	0.00	-14.42	-7.49
			118	425.70	-0.20	0.00	0.00	-5.61	-7.49
			235	425.70	-0.20	0.00	0.00	3.19	-7.49
585	Copertura	75, 58	0	-526.03	0.02	0.00	0.00	-3.77	-0.85
			118	-526.03	0.02	0.00	0.00	-2.77	-0.85
			235	-526.03	0.02	0.00	0.00	-1.77	-0.85
586	Copertura	77, 61	0	570.95	0.00	0.00	0.00	-0.86	-0.45
			115	570.95	0.00	0.00	0.00	-0.34	-0.45
			231	570.95	0.00	0.00	0.00	0.18	-0.45
587	Copertura	62, 77	0	-548.44	-0.12	0.00	0.00	1.01	0.39
			115	-548.44	-0.12	0.00	0.00	0.56	0.39
			231	-548.44	-0.12	0.00	0.00	0.11	0.39
588	Copertura	65, 78	0	550.54	-0.14	0.00	0.00	1.04	-0.07
			115	550.54	-0.14	0.00	0.00	1.12	-0.07
			231	550.54	-0.14	0.00	0.00	1.20	-0.07
589	Copertura	78, 66	0	-572.74	-0.12	0.00	0.00	-0.77	-0.04
			115	-572.74	-0.12	0.00	0.00	-0.73	-0.04
			231	-572.74	-0.12	0.00	0.00	-0.69	-0.04
590	Copertura	69, 76	0	554.67	-0.09	0.00	0.00	2.49	0.32
			118	554.67	-0.09	0.00	0.00	2.11	0.32
			235	554.67	-0.09	0.00	0.00	1.72	0.32
591	Copertura	76, 70	0	-461.98	-0.01	0.00	0.00	-0.59	-2.43
			118	-461.98	-0.01	0.00	0.00	2.27	-2.43
			235	-461.98	-0.01	0.00	0.00	5.12	-2.43
592	Copertura	79, 81	0	-27.01	-0.02	70.20	-87.29	4.89	4.92
			80	-27.01	-0.02	0.80	-87.29	0.98	4.92
			159	-27.01	-0.02	-68.59	-87.29	-2.94	4.92
593	Copertura	80, 82	0	-17.31	-0.24	56.89	-85.08	-1.03	0.88
			66	-17.31	-0.24	0.70	-85.08	-1.61	0.88
			132	-17.31	-0.24	-55.48	-85.08	-2.19	0.88
594	Copertura	83, 84	0	-0.54	0.00	52.18	-78.91	-1.62	-0.15
			66	-0.54	0.00	0.10	-78.91	-1.52	-0.15
			132	-0.54	0.00	-51.98	-78.91	-1.42	-0.15
595	Copertura	85, 86	0	-0.41	0.18	51.47	-77.84	-1.16	-0.56
			66	-0.41	0.18	0.09	-77.84	-0.79	-0.56
			132	-0.41	0.18	-51.28	-77.84	-0.42	-0.56
596	Copertura	87, 88	0	0.52	0.24	51.08	-77.31	-0.37	-0.57
			66	0.52	0.24	0.05	-77.31	0.00	-0.57
			132	0.52	0.24	-50.97	-77.31	0.37	-0.57
597	Copertura	89, 90	0	5.33	0.22	51.44	-78.12	-0.05	-0.25
			66	5.33	0.22	-0.12	-78.12	0.12	-0.25
			132	5.33	0.22	-51.68	-78.12	0.28	-0.25
598	Copertura	91, 92	0	6.51	0.22	50.45	-76.75	-0.20	-0.23

			66	6.51	0.22	-0.20	-76.75	-0.05	-0.23
			132	6.51	0.22	-50.85	-76.75	0.10	-0.23
599	Copertura	93, 94	0	-1.37	0.23	51.47	-78.11	-0.22	-0.43
			66	-1.37	0.23	-0.09	-78.11	0.06	-0.43
			132	-1.37	0.23	-51.64	-78.11	0.35	-0.43
600	Copertura	95, 96	0	-1.68	0.22	50.26	-76.09	-0.33	-0.70
			66	-1.68	0.22	0.04	-76.09	0.13	-0.70
			132	-1.68	0.22	-50.18	-76.09	0.59	-0.70
601	Copertura	97, 106	0	1.64	0.12	50.00	-75.68	0.76	-0.55
			66	1.64	0.12	0.05	-75.68	1.12	-0.55
			132	1.64	0.12	-49.90	-75.68	1.49	-0.55
602	Copertura	98, 99	0	-1.56	-0.08	74.98	-113.74	-1.35	0.71
			66	-1.56	-0.08	-0.09	-113.74	-1.82	0.71
			132	-1.56	-0.08	-75.15	-113.74	-2.29	0.71
603	Copertura	100, 101	0	-0.15	0.07	75.08	-113.69	-1.86	-0.91
			66	-0.15	0.07	0.04	-113.69	-1.26	-0.91
			132	-0.15	0.07	-74.99	-113.69	-0.66	-0.91
604	Copertura	102, 103	0	-1.33	0.14	74.70	-113.02	-1.49	-1.60
			66	-1.33	0.14	0.11	-113.02	-0.43	-1.60
			132	-1.33	0.14	-74.49	-113.02	0.62	-1.60
605	Copertura	104, 105	0	1.35	0.15	74.20	-112.34	-0.45	-0.84
			66	1.35	0.15	0.06	-112.34	0.10	-0.84
			132	1.35	0.15	-74.08	-112.34	0.66	-0.84
606	Copertura	107, 108	0	1.83	-0.12	51.58	-78.29	1.91	0.22
			66	1.83	-0.12	-0.09	-78.29	1.76	0.22
			132	1.83	-0.12	-51.76	-78.29	1.61	0.22
607	Copertura	109, 110	0	12.27	-0.33	46.12	-57.99	2.79	4.17
			80	12.27	-0.33	0.02	-57.99	-0.53	4.17
			159	12.27	-0.33	-46.08	-57.99	-3.85	4.17
608	Copertura	111, 112	0	12.23	0.14	74.31	-112.44	-0.18	-0.27
			66	12.23	0.14	0.05	-112.44	0.00	-0.27
			132	12.23	0.14	-74.22	-112.44	0.18	-0.27
609	Copertura	113, 114	0	1.91	0.14	74.44	-112.74	-0.36	-0.46
			66	1.91	0.14	0.04	-112.74	-0.05	-0.46
			132	1.91	0.14	-74.37	-112.74	0.25	-0.46
610	Copertura	115, 116	0	-2.21	0.14	74.93	-113.21	-0.18	-0.51
			66	-2.21	0.14	0.21	-113.21	0.16	-0.51
			132	-2.21	0.14	-74.51	-113.21	0.50	-0.51
611	Copertura	117, 118	0	0.26	0.12	74.30	-112.59	-0.17	-1.32
			66	0.26	0.12	-0.01	-112.59	0.70	-1.32
			132	0.26	0.12	-74.32	-112.59	1.57	-1.32
612	Copertura	119, 120	0	-0.09	0.01	74.74	-113.38	1.48	-0.26
			66	-0.09	0.01	-0.09	-113.38	1.66	-0.26
			132	-0.09	0.01	-74.92	-113.38	1.83	-0.26
613	Copertura	121, 122	0	3.03	-0.14	75.26	-113.69	2.84	1.69
			66	3.03	-0.14	0.22	-113.69	1.72	1.69
			132	3.03	-0.14	-74.82	-113.69	0.60	1.69
614	Copertura	124, 125	0	294.16	1.32	14.00	-8.28	-3.08	4.31
			99	294.16	1.32	5.78	-8.28	-7.35	4.31
			198	294.16	1.32	-2.44	-8.28	-11.63	4.31
615	Copertura	125, 127	0	-38.48	1.06	235.85	-31.51	-70.65	-8.93
			775	-38.48	1.06	-8.39	-31.51	-1.47	-8.93
			1550	-38.48	1.06	-252.62	-31.51	67.71	-8.93
616	Copertura	126, 127	0	-316.15	0.17	-14.16	8.40	-1.89	2.36
			99	-316.15	0.17	-5.82	8.40	-4.23	2.36
			198	-316.15	0.17	2.52	8.40	-6.57	2.36
617	Copertura	128, 129	0	384.06	1.37	17.70	-10.90	-3.21	3.92
			99	384.06	1.37	6.88	-10.90	-7.10	3.92
			198	384.06	1.37	-3.93	-10.90	-11.00	3.92
618	Copertura	129, 130	0	29.81	1.04	300.91	-39.12	-58.65	-7.39
			775	29.81	1.04	-2.30	-39.12	-1.34	-7.39
			1550	29.81	1.04	-305.52	-39.12	55.96	-7.39
619	Copertura	131, 130	0	-387.57	0.31	-17.84	10.99	-0.07	3.50
			99	-387.57	0.31	-6.93	10.99	-3.54	3.50
			198	-387.57	0.31	3.97	10.99	-7.01	3.50
620	Copertura	132, 135	0	416.70	1.45	19.28	-11.67	-3.53	3.31
			99	416.70	1.45	7.71	-11.67	-6.82	3.31
			198	416.70	1.45	-3.87	-11.67	-10.10	3.31
621	Copertura	133, 134	0	-414.80	0.37	-19.27	11.62	-1.34	2.16
			99	-414.80	0.37	-7.74	11.62	-3.48	2.16
			198	-414.80	0.37	3.79	11.62	-5.62	2.16
622	Copertura	135, 134	0	32.12	0.93	331.79	-42.83	-43.46	-5.47

			775	32.12	0.93	-0.15	-42.83	-1.06	-5.47
			1550	32.12	0.93	-332.08	-42.83	41.33	-5.47
623	Copertura	137, 136	0	421.80	1.52	19.47	-11.94	-3.81	2.76
			99	421.80	1.52	7.62	-11.94	-6.55	2.76
			198	421.80	1.52	-4.24	-11.94	-9.30	2.76
624	Copertura	136, 138	0	28.70	0.88	333.25	-43.01	-28.94	-3.64
			775	28.70	0.88	-0.10	-43.01	-0.76	-3.64
			1550	28.70	0.88	-333.44	-43.01	27.42	-3.64
625	Copertura	139, 138	0	-421.14	0.51	-19.49	11.95	0.21	2.78
			99	-421.14	0.51	-7.64	11.95	-2.55	2.78
			198	-421.14	0.51	4.22	11.95	-5.31	2.78
626	Copertura	140, 141	0	382.11	1.56	17.74	-10.73	-4.09	2.31
			99	382.11	1.56	7.09	-10.73	-6.39	2.31
			198	382.11	1.56	-3.56	-10.73	-8.68	2.31
627	Copertura	141, 142	0	31.45	0.81	305.20	-39.35	-17.33	-2.19
			775	31.45	0.81	0.23	-39.35	-0.38	-2.19
			1550	31.45	0.81	-304.75	-39.35	16.57	-2.19
628	Copertura	143, 142	0	-379.11	0.54	-17.75	10.68	-0.70	1.84
			99	-379.11	0.54	-7.15	10.68	-2.53	1.84
			198	-379.11	0.54	3.45	10.68	-4.35	1.84
629	Copertura	144, 145	0	334.49	1.58	15.56	-9.60	-4.38	1.98
			99	334.49	1.58	6.03	-9.60	-6.35	1.98
			198	334.49	1.58	-3.50	-9.60	-8.31	1.98
630	Copertura	145, 146	0	0.42	0.79	264.29	-34.23	-9.18	-1.15
			775	0.42	0.79	-1.02	-34.23	-0.24	-1.15
			1550	0.42	0.79	-266.34	-34.23	8.71	-1.15
631	Copertura	147, 146	0	-336.42	0.61	-15.51	9.51	0.02	2.14
			99	-336.42	0.61	-6.07	9.51	-2.10	2.14
			198	-336.42	0.61	3.37	9.51	-4.22	2.14
632	Copertura	148, 149	0	276.41	1.55	13.08	-7.96	-4.85	1.58
			99	276.41	1.55	5.18	-7.96	-6.42	1.58
			198	276.41	1.55	-2.72	-7.96	-7.99	1.58
633	Copertura	149, 150	0	24.79	0.75	203.55	-26.28	-2.47	-0.34
			775	24.79	0.75	-0.15	-26.28	0.17	-0.34
			1550	24.79	0.75	-203.84	-26.28	2.80	-0.34
634	Copertura	151, 150	0	-240.94	0.61	-11.61	6.93	-0.50	1.72
			99	-240.94	0.61	-4.73	6.93	-2.21	1.72
			198	-240.94	0.61	2.15	6.93	-3.92	1.72
635	Copertura	152, 153	0	217.41	1.54	10.36	-6.47	-5.10	1.48
			99	217.41	1.54	3.94	-6.47	-6.57	1.48
			198	217.41	1.54	-2.48	-6.47	-8.04	1.48
636	Copertura	153, 154	0	16.06	0.75	147.33	-19.15	0.16	-0.01
			775	16.06	0.75	-1.16	-19.15	0.27	-0.01
			1551	16.06	0.75	-149.65	-19.15	0.37	-0.01
637	Copertura	155, 154	0	-174.30	0.59	-8.40	5.18	-0.82	1.55
			99	-174.30	0.59	-3.26	5.18	-2.36	1.55
			198	-174.30	0.59	1.88	5.18	-3.90	1.55
638	Copertura	156, 157	0	153.01	1.52	7.39	-4.72	-5.22	1.46
			99	153.01	1.52	2.71	-4.72	-6.67	1.46
			198	153.01	1.52	-1.97	-4.72	-8.12	1.46
639	Copertura	157, 158	0	5.91	0.75	92.73	-11.97	0.81	0.08
			775	5.91	0.75	-0.06	-11.97	0.16	0.08
			1551	5.91	0.75	-92.86	-11.97	-0.48	0.08
640	Copertura	159, 158	0	-96.79	0.56	-4.94	2.87	-0.99	1.52
			99	-96.79	0.56	-2.09	2.87	-2.50	1.52
			198	-96.79	0.56	0.76	2.87	-4.01	1.52
641	Copertura	160, 161	0	93.43	1.51	4.61	-3.04	-5.27	1.48
			99	93.43	1.51	1.60	-3.04	-6.74	1.48
			198	93.43	1.51	-1.42	-3.04	-8.21	1.48
642	Copertura	161, 162	0	3.85	0.75	42.13	-5.56	0.82	0.12
			776	3.85	0.75	-0.97	-5.56	-0.08	0.12
			1551	3.85	0.75	-44.07	-5.56	-0.97	0.12
643	Copertura	163, 162	0	-40.05	0.53	-2.12	1.36	-1.48	1.21
			99	-40.05	0.53	-0.78	1.36	-2.68	1.21
			198	-40.05	0.53	0.57	1.36	-3.88	1.21
644	Copertura	164, 165	0	34.33	1.52	1.87	-1.38	-5.25	1.52
			99	34.33	1.52	0.50	-1.38	-6.76	1.52
			198	34.33	1.52	-0.87	-1.38	-8.27	1.52
645	Copertura	165, 166	0	1.05	0.76	-8.13	1.06	0.64	0.11
			776	1.05	0.76	0.08	1.06	-0.25	0.11
			1551	1.05	0.76	8.30	1.06	-1.13	0.11
646	Copertura	167, 166	0	33.23	0.53	1.09	-0.80	-1.49	1.34

			99	33.23	0.53	0.29	-0.80	-2.83	1.34
			198	33.23	0.53	-0.51	-0.80	-4.16	1.34
647	Copertura	168, 169	0	-23.54	1.53	-0.81	0.25	-5.18	1.56
			99	-23.54	1.53	-0.57	0.25	-6.73	1.56
			198	-23.54	1.53	-0.33	0.25	-8.28	1.56
648	Copertura	169, 170	0	-5.09	0.75	-57.28	7.27	0.40	0.09
			776	-5.09	0.75	-0.91	7.27	-0.27	0.09
			1552	-5.09	0.75	55.46	7.27	-0.95	0.09
649	Copertura	171, 170	0	87.03	0.52	3.80	-2.25	-1.40	1.26
			99	87.03	0.52	1.57	-2.25	-2.65	1.26
			198	87.03	0.52	-0.67	-2.25	-3.90	1.26
650	Copertura	172, 173	0	-83.09	1.55	-3.61	1.90	-5.04	1.64
			99	-83.09	1.55	-1.72	1.90	-6.66	1.64
			198	-83.09	1.55	0.16	1.90	-8.29	1.64
651	Copertura	173, 175	0	-11.67	0.75	-108.03	14.06	0.06	0.03
			776	-11.67	0.75	1.03	14.06	-0.20	0.03
			1552	-11.67	0.75	110.08	14.06	-0.45	0.03
652	Copertura	174, 175	0	162.30	0.54	7.15	-4.52	-1.30	1.27
			99	162.30	0.54	2.66	-4.52	-2.56	1.27
			198	162.30	0.54	-1.83	-4.52	-3.82	1.27
653	Copertura	176, 177	0	-133.05	1.56	-6.28	3.40	-4.86	1.73
			99	-133.05	1.56	-2.91	3.40	-6.57	1.73
			198	-133.05	1.56	0.47	3.40	-8.29	1.73
654	Copertura	177, 178	0	62.92	0.76	-156.55	20.51	-0.81	-0.11
			776	62.92	0.76	2.61	20.51	0.05	-0.11
			1552	62.92	0.76	161.78	20.51	0.92	-0.11
655	Copertura	179, 178	0	225.68	0.54	9.96	-6.02	-1.19	1.30
			99	225.68	0.54	3.98	-6.02	-2.48	1.30
			198	225.68	0.54	-2.00	-6.02	-3.77	1.30
656	Copertura	180, 181	0	-258.48	1.56	-11.79	7.13	-4.57	1.80
			99	-258.48	1.56	-4.71	7.13	-6.35	1.80
			198	-258.48	1.56	2.37	7.13	-8.14	1.80
657	Copertura	181, 182	0	-87.55	0.76	-203.88	26.15	-4.58	-0.64
			775	-87.55	0.76	-1.25	26.15	0.40	-0.64
			1550	-87.55	0.76	201.39	26.15	5.38	-0.64
658	Copertura	183, 182	0	249.26	0.58	11.91	-7.23	-0.50	1.69
			99	249.26	0.58	4.73	-7.23	-2.18	1.69
			198	249.26	0.58	-2.44	-7.23	-3.86	1.69
659	Copertura	184, 185	0	-321.73	1.58	-14.92	9.19	-4.33	1.98
			99	-321.73	1.58	-5.80	9.19	-6.30	1.98
			198	-321.73	1.58	3.32	9.19	-8.27	1.98
660	Copertura	185, 186	0	-12.24	0.77	-254.34	32.76	-8.88	-1.13
			775	-12.24	0.77	-0.43	32.76	-0.13	-1.13
			1550	-12.24	0.77	253.48	32.76	8.62	-1.13
661	Copertura	187, 186	0	317.44	0.58	14.82	-8.99	-0.50	1.74
			99	317.44	0.58	5.89	-8.99	-2.22	1.74
			198	317.44	0.58	-3.03	-8.99	-3.95	1.74
662	Copertura	188, 189	0	-370.24	1.56	-17.24	10.41	-4.08	2.28
			99	-370.24	1.56	-6.91	10.41	-6.34	2.28
			198	-370.24	1.56	3.43	10.41	-8.60	2.28
663	Copertura	189, 190	0	-20.43	0.81	-296.32	38.37	-16.48	-2.07
			775	-20.43	0.81	1.05	38.37	-0.47	-2.07
			1550	-20.43	0.81	298.42	38.37	15.54	-2.07
664	Copertura	191, 190	0	373.91	0.56	17.36	-10.54	0.10	2.32
			99	373.91	0.56	6.90	-10.54	-2.20	2.32
			198	373.91	0.56	-3.56	-10.54	-4.50	2.32
665	Copertura	192, 193	0	-413.74	1.52	-19.11	11.73	-3.81	2.71
			99	-413.74	1.52	-7.47	11.73	-6.50	2.71
			198	-413.74	1.52	4.16	11.73	-9.19	2.71
666	Copertura	193, 195	0	-27.34	0.84	-326.75	42.14	-27.92	-3.50
			775	-27.34	0.84	-0.14	42.14	-0.76	-3.50
			1550	-27.34	0.84	326.47	42.14	26.39	-3.50
667	Copertura	194, 195	0	410.40	0.47	19.06	-11.61	-0.99	1.91
			99	410.40	0.47	7.54	-11.61	-2.89	1.91
			198	410.40	0.47	-3.98	-11.61	-4.78	1.91
668	Copertura	196, 197	0	-412.70	1.45	-19.10	11.55	-3.52	3.28
			99	-412.70	1.45	-7.63	11.55	-6.77	3.28
			198	-412.70	1.45	3.83	11.55	-10.03	3.28
669	Copertura	197, 199	0	-32.27	0.94	-328.61	42.48	-42.43	-5.33
			775	-32.27	0.94	0.63	42.48	-1.12	-5.33
			1550	-32.27	0.94	329.86	42.48	40.18	-5.33
670	Copertura	198, 199	0	416.79	0.42	19.29	-11.82	0.18	3.14

			99	416.79	0.42	7.56	-11.82	-2.94	3.14
			198	416.79	0.42	-4.17	-11.82	-6.06	3.14
671	Copertura	200, 201	0	-381.91	1.37	-17.60	10.84	-3.21	3.88
			99	-381.91	1.37	-6.84	10.84	-7.07	3.88
			198	-381.91	1.37	3.93	10.84	-10.92	3.88
672	Copertura	201, 202	0	-29.33	1.00	-299.09	38.81	-58.11	-7.33
			775	-29.33	1.00	1.69	38.81	-1.32	-7.33
			1550	-29.33	1.00	302.47	38.81	55.48	-7.33
673	Copertura	203, 202	0	378.73	0.26	17.48	-10.57	-1.59	2.42
			99	378.73	0.26	6.99	-10.57	-3.99	2.42
			198	378.73	0.26	-3.50	-10.57	-6.39	2.42
674	Copertura	204, 205	0	-292.43	1.32	-13.97	8.28	-3.07	4.33
			99	-292.43	1.32	-5.76	8.28	-7.36	4.33
			198	-292.43	1.32	2.46	8.28	-11.65	4.33
675	Copertura	205, 206	0	55.71	1.11	-234.44	31.27	-70.85	-8.96
			775	55.71	1.11	7.89	31.27	-1.44	-8.96
			1550	55.71	1.11	250.22	31.27	67.96	-8.96
676	Copertura	207, 206	0	315.95	0.21	14.19	-8.51	-0.56	3.49
			99	315.95	0.21	5.75	-8.51	-4.02	3.49
			198	315.95	0.21	-2.70	-8.51	-7.49	3.49
677	Copertura	79	0	321.96	2.48	-43.80	69.35	-96.95	-105.24
			125	321.96	2.48	42.88	69.35	34.60	-105.24
			250	321.96	2.48	129.57	69.35	166.15	-105.24
678	Copertura	124	0	-195.83	0.72	65.47	-71.61	-204.05	-63.14
			155	-195.83	0.72	-45.53	-71.61	-106.18	-63.14
			310	-195.83	0.72	-156.52	-71.61	-8.31	-63.14
679	Copertura	80	0	67.90	1.14	10.16	59.00	-52.83	-69.87
			45	67.90	1.14	36.71	59.00	-21.39	-69.87
			90	67.90	1.14	63.26	59.00	10.05	-69.87
680	Copertura	128	0	164.45	0.44	65.56	-70.44	-255.08	-81.92
			155	164.45	0.44	-43.63	-70.44	-128.10	-81.92
			310	164.45	0.44	-152.82	-70.44	-1.13	-81.92
681	Copertura	82	0	-153.51	1.99	1.23	73.61	-67.19	-83.55
			43	-153.51	1.99	32.63	73.61	-31.55	-83.55
			85	-153.51	1.99	64.03	73.61	4.09	-83.55
682	Copertura	132	0	12.74	-0.23	65.67	-70.65	-278.76	-91.59
			155	12.74	-0.23	-43.84	-70.65	-136.79	-91.59
			310	12.74	-0.23	-153.35	-70.65	5.17	-91.59
683	Copertura	83	0	-12.78	-0.29	6.57	60.81	-73.10	-90.95
			43	-12.78	-0.29	32.51	60.81	-34.30	-90.95
			85	-12.78	-0.29	58.45	60.81	4.49	-90.95
684	Copertura	137	0	151.84	-0.81	65.61	-70.64	-279.50	-92.00
			155	151.84	-0.81	-43.88	-70.64	-136.90	-92.00
			310	151.84	-0.81	-153.38	-70.64	5.71	-92.00
685	Copertura	84	0	-105.39	0.22	6.10	60.82	-73.15	-91.65
			43	-105.39	0.22	32.04	60.82	-34.05	-91.65
			85	-105.39	0.22	57.99	60.82	5.04	-91.65
686	Copertura	140	0	8.72	-1.25	65.50	-70.57	-255.95	-83.96
			155	8.72	-1.25	-43.88	-70.57	-125.81	-83.96
			310	8.72	-1.25	-153.27	-70.57	4.33	-83.96
687	Copertura	85	0	14.09	-1.33	6.50	59.86	-67.25	-83.69
			43	14.09	-1.33	32.03	59.86	-31.55	-83.69
			85	14.09	-1.33	57.57	59.86	4.15	-83.69
688	Copertura	144	0	155.36	-1.56	65.39	-70.42	-221.98	-72.24
			155	155.36	-1.56	-43.76	-70.42	-110.01	-72.24
			310	155.36	-1.56	-152.92	-70.42	1.96	-72.24
689	Copertura	86	0	-85.49	-1.07	6.15	59.76	-57.91	-73.25
			43	-85.49	-1.07	31.64	59.76	-26.67	-73.25
			85	-85.49	-1.07	57.13	59.76	4.58	-73.25
690	Copertura	87	0	32.11	-1.58	6.15	59.93	-45.14	-56.06
			43	32.11	-1.58	31.71	59.93	-21.22	-56.06
			85	32.11	-1.58	57.28	59.93	2.69	-56.06
691	Copertura	148	0	-78.34	-1.82	67.04	-71.00	-171.43	-55.20
			155	-78.34	-1.82	-43.01	-71.00	-85.88	-55.20
			310	-78.34	-1.82	-153.06	-71.00	-0.32	-55.20
692	Copertura	88	0	-69.96	-1.58	6.40	58.89	-32.48	-41.28
			43	-69.96	-1.58	31.52	58.89	-14.87	-41.28
			85	-69.96	-1.58	56.64	58.89	2.74	-41.28
693	Copertura	152	0	1.40	-1.86	67.31	-71.63	-124.60	-39.39
			155	1.40	-1.86	-43.71	-71.63	-63.55	-39.39
			310	1.40	-1.86	-154.74	-71.63	-2.50	-39.39
694	Copertura	89	0	42.73	-1.41	4.62	63.44	-20.06	-25.67

			43	42.73	-1.41	31.68	63.44	-9.11	-25.67
			85	42.73	-1.41	58.74	63.44	1.84	-25.67
695	Copertura	156	0	22.40	-1.84	66.87	-71.18	-79.04	-24.28
			155	22.40	-1.84	-43.45	-71.18	-41.41	-24.28
			310	22.40	-1.84	-153.77	-71.18	-3.78	-24.28
696	Copertura	90	0	-61.62	-1.47	7.38	58.17	-8.29	-12.58
			43	-61.62	-1.47	32.19	58.17	-2.92	-12.58
			85	-61.62	-1.47	57.01	58.17	2.44	-12.58
697	Copertura	160	0	7.04	-1.81	66.41	-70.90	-36.53	-10.53
			155	7.04	-1.81	-43.49	-70.90	-20.21	-10.53
			310	7.04	-1.81	-153.39	-70.90	-3.89	-10.53
698	Copertura	91	0	51.86	-1.39	4.30	62.46	3.19	2.02
			43	51.86	-1.39	30.94	62.46	2.33	2.02
			85	51.86	-1.39	57.58	62.46	1.47	2.02
699	Copertura	164	0	-12.79	-1.80	65.82	-70.57	5.46	3.19
			155	-12.79	-1.80	-43.56	-70.57	0.51	3.19
			310	-12.79	-1.80	-152.95	-70.57	-4.44	3.19
700	Copertura	92	0	-50.19	-1.39	8.28	55.11	14.61	14.47
			43	-50.19	-1.39	31.79	55.11	8.44	14.47
			85	-50.19	-1.39	55.30	55.11	2.27	14.47
701	Copertura	168	0	-30.95	-1.79	65.11	-70.18	46.70	16.64
			155	-30.95	-1.79	-43.67	-70.18	20.90	16.64
			310	-30.95	-1.79	-152.44	-70.18	-4.89	16.64
702	Copertura	93	0	85.82	-1.46	6.33	58.76	25.91	29.82
			43	85.82	-1.46	31.40	58.76	13.19	29.82
			85	85.82	-1.46	56.46	58.76	0.47	29.82
703	Copertura	172	0	-13.69	-1.77	64.26	-69.88	89.49	30.42
			155	-13.69	-1.77	-44.05	-69.88	42.33	30.42
			310	-13.69	-1.77	-152.37	-69.88	-4.83	30.42
704	Copertura	94	0	5.52	-1.48	6.67	62.29	36.10	44.15
			43	5.52	-1.48	33.24	62.29	17.27	44.15
			85	5.52	-1.48	59.81	62.29	-1.56	44.15
705	Copertura	176	0	86.45	-1.72	63.28	-69.12	129.75	41.75
			155	86.45	-1.72	-43.85	-69.12	65.04	41.75
			310	86.45	-1.72	-150.98	-69.12	0.33	41.75
706	Copertura	180	0	-18.46	-1.64	65.05	-69.84	171.46	57.44
			155	-18.46	-1.64	-43.21	-69.84	82.43	57.44
			310	-18.46	-1.64	-151.46	-69.84	-6.60	57.44
707	Copertura	95	0	-38.83	-1.42	6.97	58.64	47.12	54.74
			43	-38.83	-1.42	31.99	58.64	23.77	54.74
			85	-38.83	-1.42	57.00	58.64	0.42	54.74
708	Copertura	184	0	-141.08	-1.54	65.20	-70.35	213.34	69.68
			155	-141.08	-1.54	-43.84	-70.35	105.34	69.68
			310	-141.08	-1.54	-152.88	-70.35	-2.66	69.68
709	Copertura	96	0	58.99	-1.45	6.28	60.92	56.31	69.55
			43	58.99	-1.45	32.27	60.92	26.64	69.55
			85	58.99	-1.45	58.25	60.92	-3.03	69.55
710	Copertura	188	0	9.95	-1.29	65.31	-70.33	248.76	81.16
			155	9.95	-1.29	-43.70	-70.33	122.96	81.16
			310	9.95	-1.29	-152.71	-70.33	-2.84	81.16
711	Copertura	97	0	0.71	-0.62	6.34	60.66	65.76	81.98
			43	0.71	-0.62	32.21	60.66	30.79	81.98
			85	0.71	-0.62	58.09	60.66	-4.18	81.98
712	Copertura	192	0	-149.12	-0.86	65.44	-70.46	274.30	90.12
			155	-149.12	-0.86	-43.77	-70.46	134.61	90.12
			310	-149.12	-0.86	-152.97	-70.46	-5.07	90.12
713	Copertura	106	0	109.02	-0.98	6.99	57.96	71.72	89.55
			43	109.02	-0.98	31.71	57.96	33.52	89.55
			85	109.02	-0.98	56.44	57.96	-4.68	89.55
714	Copertura	196	0	-11.26	-0.27	65.52	-70.49	276.07	90.74
			155	-11.26	-0.27	-43.74	-70.49	135.42	90.74
			310	-11.26	-0.27	-153.00	-70.49	-5.23	90.74
715	Copertura	107	0	97.59	1.06	6.14	61.99	73.00	90.46
			43	97.59	1.06	32.58	61.99	34.41	90.46
			85	97.59	1.06	59.02	61.99	-4.17	90.46
716	Copertura	200	0	-169.14	0.42	65.43	-70.31	253.53	81.46
			155	-169.14	0.42	-43.55	-70.31	127.26	81.46
			310	-169.14	0.42	-152.52	-70.31	1.00	81.46
717	Copertura	108	0	54.10	0.39	7.27	60.20	66.78	82.43
			43	54.10	0.39	32.95	60.20	31.61	82.43
			85	54.10	0.39	58.63	60.20	-3.55	82.43
718	Copertura	204	0	192.24	0.73	65.37	-71.50	203.01	62.93

			155	192.24	0.73	-45.45	-71.50	105.47	62.93
			310	192.24	0.73	-156.27	-71.50	7.93	62.93
719	Copertura	109	0	-68.30	2.97	7.29	69.57	47.08	68.33
			43	-68.30	2.97	36.97	69.57	17.93	68.33
			85	-68.30	2.97	66.64	69.57	-11.22	68.33
720	Copertura	110	0	-298.07	3.64	52.01	55.55	-72.91	103.84
			43	-298.07	3.64	75.71	55.55	-117.20	103.84
			85	-298.07	3.64	99.40	55.55	-161.49	103.84
721	Copertura	14	0	234.67	-2.40	-156.69	96.36	-287.59	-100.32
			95	234.67	-2.40	-65.15	96.36	-192.28	-100.32
			190	234.67	-2.40	26.39	96.36	-96.98	-100.32
722	Copertura	15	0	-394.74	2.19	149.95	-67.30	9.80	153.73
			65	-394.74	2.19	106.20	-67.30	-90.12	153.73
			130	-394.74	2.19	62.46	-67.30	-190.05	153.73
723	Copertura	16	0	282.96	0.55	-65.10	43.92	13.68	159.49
			65	282.96	0.55	-36.55	43.92	-89.99	159.49
			130	282.96	0.55	-8.00	43.92	-193.67	159.49
724	Copertura	17	0	-95.31	1.98	148.90	-66.52	24.15	201.17
			65	-95.31	1.98	105.66	-66.52	-106.61	201.17
			130	-95.31	1.98	62.42	-66.52	-237.37	201.17
725	Copertura	18	0	80.53	1.01	-76.86	57.39	24.18	201.97
			65	80.53	1.01	-39.56	57.39	-107.10	201.97
			130	80.53	1.01	-2.26	57.39	-238.38	201.97
726	Copertura	19	0	-268.99	1.49	149.80	-67.34	20.90	215.67
			65	-268.99	1.49	106.03	-67.34	-119.29	215.67
			130	-268.99	1.49	62.26	-67.34	-259.47	215.67
727	Copertura	20	0	302.50	-0.19	-76.78	57.63	19.37	214.03
			65	302.50	-0.19	-39.32	57.63	-119.75	214.03
			130	302.50	-0.19	-1.86	57.63	-258.87	214.03
728	Copertura	21	0	-133.43	1.07	150.21	-67.88	24.57	218.92
			65	-133.43	1.07	106.09	-67.88	-117.73	218.92
			130	-133.43	1.07	61.97	-67.88	-260.03	218.92
729	Copertura	22	0	144.67	0.16	-77.09	57.65	23.70	218.02
			65	144.67	0.16	-39.62	57.65	-118.01	218.02
			130	144.67	0.16	-2.14	57.65	-259.72	218.02
730	Copertura	23	0	-249.65	0.82	150.37	-68.26	18.89	197.77
			65	-249.65	0.82	106.00	-68.26	-109.66	197.77
			130	-249.65	0.82	61.64	-68.26	-238.21	197.77
731	Copertura	24	0	306.30	-0.65	-77.27	58.28	16.87	196.16
			65	306.30	-0.65	-39.39	58.28	-110.63	196.16
			130	306.30	-0.65	-1.50	58.28	-238.13	196.16
732	Copertura	25	0	-70.96	0.71	150.30	-68.44	20.09	174.24
			65	-70.96	0.71	105.82	-68.44	-93.17	174.24
			130	-70.96	0.71	61.33	-68.44	-206.42	174.24
733	Copertura	26	0	106.85	-0.42	-77.68	58.54	19.10	173.71
			65	106.85	-0.42	-39.62	58.54	-93.81	173.71
			130	106.85	-0.42	-1.57	58.54	-206.73	173.71
734	Copertura	27	0	230.86	-0.60	-78.45	60.01	-0.44	122.50
			65	230.86	-0.60	-39.44	60.01	-80.07	122.50
			130	230.86	-0.60	-0.44	60.01	-159.69	122.50
735	Copertura	28	0	-265.38	0.83	147.22	-65.23	34.47	148.39
			65	-265.38	0.83	104.82	-65.23	-61.99	148.39
			130	-265.38	0.83	62.42	-65.23	-158.44	148.39
736	Copertura	29	0	13.08	-0.52	-78.50	60.11	-3.35	86.76
			65	13.08	-0.52	-39.43	60.11	-59.75	86.76
			130	13.08	-0.52	-0.35	60.11	-116.14	86.76
737	Copertura	30	0	-145.87	0.98	147.87	-65.65	42.37	120.56
			65	-145.87	0.98	105.19	-65.65	-36.00	120.56
			130	-145.87	0.98	62.52	-65.65	-114.36	120.56
738	Copertura	31	0	142.51	-0.32	-78.48	60.13	-12.69	46.19
			65	142.51	-0.32	-39.40	60.13	-42.72	46.19
			130	142.51	-0.32	-0.31	60.13	-72.75	46.19
739	Copertura	32	0	-81.37	1.10	148.20	-66.25	42.82	88.17
			65	-81.37	1.10	105.14	-66.25	-14.49	88.17
			130	-81.37	1.10	62.08	-66.25	-71.80	88.17
740	Copertura	33	0	-69.07	-0.24	-75.00	55.46	-12.25	16.80
			65	-69.07	-0.24	-38.95	55.46	-23.17	16.80
			130	-69.07	-0.24	-2.90	55.46	-34.08	16.80
741	Copertura	34	0	-56.44	1.18	148.88	-67.09	43.31	57.99
			65	-56.44	1.18	105.27	-67.09	5.62	57.99
			130	-56.44	1.18	61.66	-67.09	-32.07	57.99
742	Copertura	35	0	65.56	-0.22	-80.00	61.52	-22.76	-22.45

			65	65.56	-0.22	-40.01	61.52	-8.16	-22.45
			130	65.56	-0.22	-0.02	61.52	6.43	-22.45
743	Copertura	36	0	-36.32	1.18	149.73	-68.12	43.75	28.15
			65	-36.32	1.18	105.45	-68.12	25.45	28.15
			130	-36.32	1.18	61.17	-68.12	7.15	28.15
744	Copertura	37	0	-144.88	-0.21	-74.87	55.85	-21.42	-49.96
			65	-144.88	-0.21	-38.57	55.85	11.05	-49.96
			130	-144.88	-0.21	-2.26	55.85	43.53	-49.96
745	Copertura	38	0	-15.35	1.12	150.74	-69.33	44.35	-1.04
			65	-15.35	1.12	105.67	-69.33	45.02	-1.04
			130	-15.35	1.12	60.60	-69.33	45.70	-1.04
746	Copertura	39	0	10.73	-0.35	-74.80	55.60	-31.35	-89.67
			65	10.73	-0.35	-38.66	55.60	26.94	-89.67
			130	10.73	-0.35	-2.52	55.60	85.22	-89.67
747	Copertura	40	0	42.17	1.03	152.13	-70.90	45.21	-31.14
			65	42.17	1.03	106.04	-70.90	65.45	-31.14
			130	42.17	1.03	59.95	-70.90	85.69	-31.14
748	Copertura	41	0	-181.94	-0.41	-73.64	54.10	-32.98	-122.29
			65	-181.94	-0.41	-38.48	54.10	46.51	-122.29
			130	-181.94	-0.41	-3.32	54.10	125.99	-122.29
749	Copertura	42	0	176.16	0.93	152.75	-71.95	49.77	-56.54
			65	176.16	0.93	105.98	-71.95	86.52	-56.54
			130	176.16	0.93	59.21	-71.95	123.27	-56.54
750	Copertura	43	0	156.21	0.78	149.33	-68.04	-13.52	-133.22
			65	156.21	0.78	105.10	-68.04	73.08	-133.22
			130	156.21	0.78	60.87	-68.04	159.67	-133.22
751	Copertura	44	0	-170.42	-0.59	-75.04	56.42	-10.75	-129.07
			65	-170.42	-0.59	-38.37	56.42	73.14	-129.07
			130	-170.42	-0.59	-1.69	56.42	157.04	-129.07
752	Copertura	45	0	76.58	0.71	150.05	-68.36	-19.25	-167.44
			65	76.58	0.71	105.61	-68.36	89.59	-167.44
			130	76.58	0.71	61.17	-68.36	198.42	-167.44
753	Copertura	46	0	-192.21	-0.69	-75.83	57.24	-16.15	-165.07
			65	-192.21	-0.69	-38.63	57.24	91.15	-165.07
			130	-192.21	-0.69	-1.42	57.24	198.44	-165.07
754	Copertura	47	0	260.29	0.77	149.92	-68.05	-17.82	-191.80
			65	260.29	0.77	105.69	-68.05	106.85	-191.80
			130	260.29	0.77	61.46	-68.05	231.52	-191.80
755	Copertura	48	0	-215.22	-0.25	-75.81	56.96	-18.64	-192.91
			65	-215.22	-0.25	-38.78	56.96	106.75	-192.91
			130	-215.22	-0.25	-1.76	56.96	232.14	-192.91
756	Copertura	49	0	130.71	1.02	149.87	-67.75	-24.13	-214.86
			65	130.71	1.02	105.84	-67.75	115.53	-214.86
			130	130.71	1.02	61.80	-67.75	255.19	-214.86
757	Copertura	50	0	-206.24	-0.53	-76.43	57.78	-21.65	-212.68
			65	-206.24	-0.53	-38.87	57.78	116.60	-212.68
			130	-206.24	-0.53	-1.32	57.78	254.84	-212.68
758	Copertura	51	0	267.76	1.43	149.50	-67.21	-20.67	-213.57
			65	267.76	1.43	105.81	-67.21	118.15	-213.57
			130	267.76	1.43	62.12	-67.21	256.97	-213.57
759	Copertura	52	0	-149.22	0.58	-76.28	56.93	-23.67	-216.28
			65	-149.22	0.58	-39.28	56.93	116.91	-216.28
			130	-149.22	0.58	-2.28	56.93	257.49	-216.28
760	Copertura	53	0	89.18	1.95	148.64	-66.42	-24.13	-200.04
			65	89.18	1.95	105.47	-66.42	105.90	-200.04
			130	89.18	1.95	62.29	-66.42	235.93	-200.04
761	Copertura	54	0	-237.33	0.19	-75.59	56.58	-18.99	-195.38
			65	-237.33	0.19	-38.81	56.58	108.01	-195.38
			130	-237.33	0.19	-2.03	56.58	235.01	-195.38
762	Copertura	55	0	390.02	2.19	149.69	-67.17	-9.39	-152.63
			65	390.02	2.19	106.03	-67.17	89.82	-152.63
			130	390.02	2.19	62.37	-67.17	189.03	-152.63
763	Copertura	56	0	-225.95	1.08	-75.72	56.85	-16.50	-162.37
			65	-225.95	1.08	-38.77	56.85	89.05	-162.37
			130	-225.95	1.08	-1.82	56.85	194.59	-162.37
764	Copertura	70	0	-240.08	-0.21	-142.43	67.81	280.92	99.66
			95	-240.08	-0.21	-78.01	67.81	186.24	99.66
			190	-240.08	-0.21	-13.59	67.81	91.56	99.66
765	Copertura	81	0	-17.74	2.16	-50.20	73.28	-163.50	-68.99
			80	-17.74	2.16	8.43	73.28	-108.31	-68.99
			160	-17.74	2.16	67.05	73.28	-53.11	-68.99
766	Copertura	126	0	69.55	-0.77	-9.37	46.27	-207.83	-73.91

			30	69.55	-0.77	4.51	46.27	-185.65	-73.91
			60	69.55	-0.77	18.40	46.27	-163.48	-73.91
767	Copertura	98	0	-67.87	-0.19	-40.98	59.32	-205.91	-84.43
			82	-67.87	-0.19	7.87	59.32	-136.39	-84.43
			165	-67.87	-0.19	56.72	59.32	-66.87	-84.43
768	Copertura	99	0	-91.68	1.33	-42.30	61.35	-223.13	-91.10
			82	-91.68	1.33	8.22	61.35	-148.11	-91.10
			165	-91.68	1.33	58.74	61.35	-73.10	-91.10
769	Copertura	100	0	-26.49	-1.20	-41.20	60.29	-223.84	-91.50
			82	-26.49	-1.20	8.44	60.29	-148.49	-91.50
			165	-26.49	-1.20	58.08	60.29	-73.15	-91.50
770	Copertura	101	0	-63.75	-0.17	-41.30	60.27	-205.81	-84.25
			82	-63.75	-0.17	8.33	60.27	-136.44	-84.25
			165	-63.75	-0.17	57.96	60.27	-67.07	-84.25
771	Copertura	102	0	-7.65	-1.49	-40.31	59.35	-177.81	-72.69
			82	-7.65	-1.49	8.56	59.35	-117.95	-72.69
			165	-7.65	-1.49	57.43	59.35	-58.10	-72.69
772	Copertura	103	0	-45.20	-1.21	-40.62	59.41	-138.15	-56.63
			82	-45.20	-1.21	8.30	59.41	-91.52	-56.63
			165	-45.20	-1.21	57.22	59.41	-44.89	-56.63
773	Copertura	104	0	7.35	-1.21	-40.47	59.41	-99.78	-40.72
			82	7.35	-1.21	8.45	59.41	-66.25	-40.72
			165	7.35	-1.21	57.37	59.41	-32.72	-40.72
774	Copertura	105	0	-35.39	-1.36	-39.64	58.11	-62.53	-25.92
			82	-35.39	-1.36	8.21	58.11	-41.18	-25.92
			165	-35.39	-1.36	56.06	58.11	-19.84	-25.92
775	Copertura	111	0	16.50	-1.18	-42.24	63.50	-28.18	-12.33
			80	16.50	-1.18	8.41	63.50	-18.35	-12.33
			160	16.50	-1.18	59.06	63.50	-8.51	-12.33
776	Copertura	112	0	-24.89	-1.19	-37.39	55.95	6.36	1.79
			82	-24.89	-1.19	8.68	55.95	4.88	1.79
			165	-24.89	-1.19	54.75	55.95	3.40	1.79
777	Copertura	113	0	26.56	-1.29	-42.34	61.62	38.59	14.69
			82	26.56	-1.29	8.40	61.62	26.49	14.69
			165	26.56	-1.29	59.14	61.62	14.39	14.69
778	Copertura	114	0	7.71	-1.24	-41.23	60.13	74.54	29.39
			82	7.71	-1.24	8.28	60.13	50.34	29.39
			165	7.71	-1.24	57.80	60.13	26.14	29.39
779	Copertura	115	0	83.63	-1.13	-42.02	60.92	109.30	44.58
			82	83.63	-1.13	8.14	60.92	72.59	44.58
			165	83.63	-1.13	58.31	60.92	35.88	44.58
780	Copertura	116	0	-114.92	-1.09	-42.10	60.32	136.35	54.05
			82	-114.92	-1.09	7.57	60.32	91.85	54.05
			165	-114.92	-1.09	57.24	60.32	47.34	54.05
781	Copertura	117	0	135.08	-0.86	-41.10	59.24	171.78	70.25
			82	135.08	-0.86	7.68	59.24	113.93	70.25
			165	135.08	-0.86	56.46	59.24	56.08	70.25
782	Copertura	118	0	-74.96	-1.38	-40.87	59.02	199.98	81.43
			82	-74.96	-1.38	7.73	59.02	132.93	81.43
			165	-74.96	-1.38	56.33	59.02	65.88	81.43
783	Copertura	131	0	-181.61	1.16	-2.53	60.89	-256.22	-83.72
			30	-181.61	1.16	15.73	60.89	-231.11	-83.72
			60	-181.61	1.16	34.00	60.89	-205.99	-83.72
784	Copertura	133	0	22.05	-0.96	-3.02	59.79	-278.14	-91.82
			30	22.05	-0.96	14.92	59.79	-250.60	-91.82
			60	22.05	-0.96	32.85	59.79	-223.05	-91.82
785	Copertura	139	0	-140.18	0.66	-2.39	60.44	-279.21	-92.41
			30	-140.18	0.66	15.74	60.44	-251.49	-92.41
			60	-140.18	0.66	33.87	60.44	-223.77	-92.41
786	Copertura	143	0	49.94	-0.83	-2.37	60.12	-255.88	-83.34
			30	49.94	-0.83	15.66	60.12	-230.88	-83.34
			60	49.94	-0.83	33.70	60.12	-205.88	-83.34
787	Copertura	147	0	-120.67	0.00	-2.02	60.68	-222.24	-74.29
			30	-120.67	0.00	16.18	60.68	-199.95	-74.29
			60	-120.67	0.00	34.39	60.68	-177.66	-74.29
788	Copertura	151	0	67.83	-0.58	-0.98	58.09	-171.31	-55.03
			30	67.83	-0.58	16.44	58.09	-154.80	-55.03
			60	67.83	-0.58	33.87	58.09	-138.30	-55.03
789	Copertura	155	0	-104.99	-0.75	-1.10	58.05	-124.57	-41.56
			30	-104.99	-0.75	16.32	58.05	-112.10	-41.56
			60	-104.99	-0.75	33.74	58.05	-99.63	-41.56
790	Copertura	159	0	76.95	-0.70	-1.23	59.46	-77.72	-25.08

			30	76.95	-0.70	16.61	59.46	-70.20	-25.08
			60	76.95	-0.70	34.44	59.46	-62.67	-25.08
791	Copertura	119	0	184.70	0.50	-41.25	59.59	219.99	90.11
			82	184.70	0.50	7.82	59.59	145.79	90.11
			165	184.70	0.50	56.89	59.59	71.60	90.11
792	Copertura	120	0	19.30	-0.84	-41.36	60.16	222.23	90.68
			82	19.30	-0.84	8.18	60.16	147.55	90.68
			165	19.30	-0.84	57.72	60.16	72.88	90.68
793	Copertura	121	0	132.39	2.00	-43.13	62.03	202.28	82.21
			82	132.39	2.00	7.95	62.03	134.59	82.21
			165	132.39	2.00	59.03	62.03	66.89	82.21
794	Copertura	122	0	-126.29	0.19	-40.96	57.30	166.16	72.51
			82	-126.29	0.19	6.23	57.30	106.45	72.51
			165	-126.29	0.19	53.42	57.30	46.75	72.51
795	Copertura	123	0	-240.08	-0.21	-13.59	67.81	91.56	99.66
			82	-240.08	-0.21	42.25	67.81	9.49	99.66
			165	-240.08	-0.21	98.09	67.81	-72.58	99.66
796	Copertura	163	0	-96.33	-1.01	-4.20	55.67	-36.25	-12.60
			33	-96.33	-1.01	13.93	55.67	-32.14	-12.60
			65	-96.33	-1.01	32.07	55.67	-28.04	-12.60
797	Copertura	167	0	87.93	-1.00	-1.44	63.78	7.47	2.07
			30	87.93	-1.00	17.69	63.78	6.85	2.07
			60	87.93	-1.00	36.83	63.78	6.23	2.07
798	Copertura	171	0	-86.18	-0.93	-3.73	59.71	47.27	14.23
			30	-86.18	-0.93	14.19	59.71	43.00	14.23
			60	-86.18	-0.93	32.10	59.71	38.73	14.23
799	Copertura	174	0	120.45	-0.98	-4.09	62.04	92.31	29.85
			30	120.45	-0.98	14.52	62.04	83.36	29.85
			60	120.45	-0.98	33.14	62.04	74.40	29.85
800	Copertura	179	0	-29.58	-0.96	-4.97	63.13	135.89	44.07
			30	-29.58	-0.96	13.97	63.13	122.67	44.07
			60	-29.58	-0.96	32.91	63.13	109.44	44.07
801	Copertura	183	0	-1.70	-0.59	-2.46	58.11	168.94	54.56
			30	-1.70	-0.59	14.97	58.11	152.58	54.56
			60	-1.70	-0.59	32.41	58.11	136.21	54.56
802	Copertura	187	0	22.49	-0.69	-2.19	58.98	213.26	68.93
			30	22.49	-0.69	15.51	58.98	192.58	68.93
			60	22.49	-0.69	33.20	58.98	171.90	68.93
803	Copertura	191	0	37.63	0.19	-2.12	59.28	249.51	82.75
			30	37.63	0.19	15.67	59.28	224.68	82.75
			60	37.63	0.19	33.45	59.28	199.86	82.75
804	Copertura	194	0	71.32	-0.98	-2.32	59.68	273.90	89.84
			30	71.32	-0.98	15.58	59.68	246.95	89.84
			60	71.32	-0.98	33.49	59.68	220.00	89.84
805	Copertura	198	0	132.68	0.99	-2.47	60.07	276.78	90.95
			30	132.68	0.99	15.55	60.07	249.50	90.95
			60	132.68	0.99	33.56	60.07	222.22	90.95
806	Copertura	203	0	18.70	-0.84	-3.27	59.00	252.48	83.90
			30	18.70	-0.84	14.43	59.00	227.31	83.90
			60	18.70	-0.84	32.13	59.00	202.14	83.90
807	Copertura	207	0	-12.59	0.79	-2.34	60.34	208.78	70.81
			30	-12.59	0.79	15.76	60.34	187.54	70.81
			60	-12.59	0.79	33.86	60.34	166.29	70.81

1.1.5.2 Piastre SLV

Tabella 10.I

Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	0.394	-1.588	0.715	-163.104	81.881	56.963	2.092	1.912
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61,	2.539	1.547	-1.354	313.242	120.453	138.258	4.598	-3.767

		62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44								
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	-2.633	1.323	-1.759	-329.630	105.916	160.480	5.117	-3.898

1.1.6 Risultati Condizioni (Torsione Accidentale Y).

1.1.6.1 Sollecitazioni SLV

Tabella 11.I

Sollecitazioni									
Asta	Imp.	Fili	X [cm]	N [daN]	Mt [daNm]	Mxz [daNm]	Txz [daN]	Mxy [daNm]	Txy [daN]
1	Fondazione	1, 2	0	-80.30	-20.25	49.96	57.41	0.27	-7.16
			42	-74.75	-20.25	69.00	42.40	2.36	-2.92
			83	-69.25	-20.25	85.09	42.75	2.74	1.04
2	Fondazione	1, 2	0	-58.30	-22.57	71.47	79.88	2.70	-3.57
			42	-52.83	-22.58	105.89	92.90	3.41	0.13
			83	-47.40	-22.58	147.81	115.33	2.62	3.61
3	Fondazione	1, 15	0	42.55	35.57	-33.57	65.12	-5.04	-20.59
			40	38.66	35.56	-11.57	41.20	2.06	-15.18
			80	34.80	35.56	0.39	14.65	7.06	-10.04
4	Fondazione	1, 15	0	30.67	-14.37	-15.65	-26.39	7.03	5.67
			40	26.82	-14.37	-31.04	-55.28	3.79	10.57
			80	22.98	-14.38	-58.28	-85.85	-1.35	15.26
5	Fondazione	2, 3	0	-113.46	11.11	154.90	-161.36	2.45	-0.81
			35	-108.84	11.11	102.16	-138.59	2.29	1.67
			69	-104.26	11.11	57.56	-114.61	1.31	4.01
6	Fondazione	2, 3	0	-87.02	2.89	61.30	-73.62	1.29	0.18
			35	-82.48	2.88	39.08	-50.07	0.84	2.41
			69	-77.97	2.88	24.77	-27.98	-0.36	4.51
7	Fondazione	3, 4	0	-70.69	30.37	42.80	-76.40	-0.46	-4.44
			35	-66.21	30.37	19.05	-56.47	0.73	-2.45
			69	-61.75	30.37	1.74	-39.25	1.24	-0.58
8	Fondazione	3, 4	0	-52.87	4.45	13.06	-36.19	1.22	0.96
			35	-48.44	4.45	2.24	-21.93	0.59	2.72
			69	-44.03	4.45	-4.19	-10.75	-0.64	4.38
9	Fondazione	4, 5	0	-38.91	32.04	13.44	-50.35	-0.56	-3.70
			35	-34.51	32.04	-3.33	-42.28	0.44	-2.15
			69	-30.13	32.04	-17.85	-37.35	0.93	-0.71
10	Fondazione	4, 5	0	-20.99	7.05	-5.55	-34.46	0.91	1.02
			35	-16.61	7.05	-17.89	-32.50	0.33	2.37
			69	-12.25	7.05	-30.02	-33.23	-0.71	3.61
11	Fondazione	5, 6	0	-3.87	27.06	-12.87	-38.33	-0.58	-2.25
			35	0.49	27.06	-27.42	-41.31	0.00	-1.11
			69	4.86	27.06	-43.32	-46.08	0.20	-0.07
12	Fondazione	5, 6	0	21.77	-7.93	-36.79	-75.90	0.18	0.00
			35	26.14	-7.93	-64.84	-81.75	0.01	0.94
			69	30.52	-7.93	-94.95	-87.61	-0.46	1.78

13	Fondazio ne	6, 7	0	-25.56	-13.39	-97.41	164.16	-0.75	-2.56
			35	-21.18	-13.39	-42.46	159.85	0.00	-1.82
			69	-16.81	-13.39	11.47	158.43	0.52	-1.19
14	Fondazio ne	6, 7	0	7.86	-29.21	-4.64	163.33	0.50	0.89
			35	12.23	-29.22	51.06	165.18	0.10	1.42
			69	16.61	-29.22	107.90	169.76	-0.47	1.85
15	Fondazio ne	7, 8	0	-38.91	16.46	108.54	-120.36	0.09	-1.33
			35	-34.54	16.45	67.14	-114.58	0.49	-1.00
			69	-30.18	16.45	27.68	-109.30	0.80	-0.77
16	Fondazio ne	7, 8	0	-10.31	17.52	40.50	-75.21	0.78	1.67
			35	-5.96	17.52	14.38	-71.46	0.18	1.80
			69	-1.61	17.52	-10.78	-69.76	-0.45	1.84
17	Fondazio ne	8, 9	0	12.69	29.30	13.42	-74.30	-0.20	-0.09
			35	17.04	29.30	-13.10	-74.77	-0.16	-0.15
			69	21.39	29.30	-40.15	-77.33	-0.09	-0.31
18	Fondazio ne	8, 9	0	42.87	6.79	-26.00	-103.47	-0.10	1.48
			35	47.24	6.79	-63.25	-107.62	-0.57	1.23
			69	51.63	6.79	-102.09	-112.39	-0.94	0.87
19	Fondazio ne	9, 10	0	-8.03	-15.52	-103.42	165.96	-0.81	-1.37
			35	-3.64	-15.52	-47.76	162.18	-0.26	-1.82
			69	0.76	-15.52	7.00	160.84	0.46	-2.38
20	Fondazio ne	9, 10	0	27.82	-24.13	-6.80	153.02	0.44	1.97
			35	32.22	-24.13	45.30	154.58	-0.13	1.31
			69	36.63	-24.13	98.39	158.62	-0.46	0.55
21	Fondazio ne	10, 11	0	-20.15	3.45	100.17	-90.83	-0.16	0.09
			35	-15.73	3.45	68.82	-85.72	-0.04	-0.78
			69	-11.33	3.45	39.18	-81.19	0.39	-1.76
22	Fondazio ne	10, 11	0	7.10	21.47	45.88	-47.04	0.37	1.59
			35	11.51	21.47	29.32	-44.21	0.00	0.51
			69	15.92	21.47	13.33	-43.84	0.03	-0.67
23	Fondazio ne	11, 12	0	25.70	21.31	33.25	-60.66	0.28	2.57
			35	30.13	21.31	11.08	-63.25	-0.39	1.28
			69	34.56	21.31	-12.54	-69.16	-0.60	-0.11
24	Fondazio ne	11, 12	0	46.28	28.46	2.85	-65.47	-0.62	0.86
			35	50.72	28.46	-22.13	-74.76	-0.66	-0.64
			69	55.19	28.46	-50.87	-87.18	-0.16	-2.25
25	Fondazio ne	12, 13	0	65.52	14.45	-31.06	-56.79	-0.02	3.36
			35	70.01	14.45	-54.06	-71.67	-0.89	1.64
			69	74.53	14.45	-82.49	-88.08	-1.14	-0.20
26	Fondazio ne	12, 13	0	94.34	6.17	-75.47	-120.09	-1.16	2.87
			35	98.89	6.17	-120.69	-136.65	-1.81	0.91
			69	103.49	6.17	-171.38	-151.34	-1.77	-1.17
27	Fondazio ne	13, 14	0	38.51	-28.39	-170.47	113.20	-1.64	4.44
			42	43.93	-28.38	-127.17	102.02	-2.87	1.45
			83	49.37	-28.38	-86.22	102.70	-2.81	-1.75
28	Fondazio ne	13, 14	0	70.97	-35.22	-102.80	62.53	-2.85	2.35
			42	76.45	-35.22	-75.11	79.00	-3.12	-1.09
			83	81.97	-35.22	-36.75	114.35	-1.91	-4.79
29	Fondazio ne	14, 16	0	-38.81	50.47	51.74	-138.19	-4.84	-19.95
			40	-35.44	50.46	4.69	-95.43	2.02	-14.59
			80	-32.09	50.45	-25.74	-54.68	6.80	-9.49
30	Fondazio ne	14, 16	0	-31.91	6.49	0.57	-14.26	6.76	4.97
			40	-28.58	6.48	2.03	24.67	3.81	9.84
			80	-25.26	6.47	18.63	61.84	-1.04	14.50
31	Fondazio	15, 17	0	67.32	50.08	-82.48	156.26	-1.60	-12.01

	ne								
			33	64.15	50.08	-34.52	130.59	1.74	-8.26
			66	61.01	50.07	5.05	105.62	3.87	-4.64
32	Fondazio ne	15, 17	0	40.59	-19.29	-10.95	90.15	3.84	5.98
			33	37.47	-19.29	15.44	66.20	1.29	9.48
			66	34.36	-19.30	34.09	43.20	-2.40	12.87
33	Fondazio ne	16, 18	0	-61.51	51.75	46.44	-126.49	-1.48	-11.39
			33	-58.77	51.75	9.03	-97.21	1.66	-7.66
			66	-56.06	51.74	-19.01	-69.75	3.59	-4.06
34	Fondazio ne	16, 18	0	-43.37	-13.77	-3.51	-59.31	3.57	5.37
			33	-40.67	-13.78	-19.33	-33.63	1.21	8.86
			66	-37.98	-13.78	-26.94	-9.48	-2.27	12.23
35	Fondazio ne	17, 19	0	59.44	38.23	19.84	0.03	-3.45	-13.98
			33	56.34	38.22	16.75	-22.43	0.62	-10.71
			66	53.27	38.22	6.29	-44.69	3.63	-7.55
36	Fondazio ne	17, 19	0	33.76	-35.16	6.27	-54.41	3.61	8.00
			33	30.70	-35.17	-14.75	-76.68	0.47	11.05
			66	27.65	-35.17	-43.11	-98.89	-3.67	14.00
37	Fondazio ne	18, 20	0	-52.24	42.23	-13.05	-20.90	-3.41	-13.78
			33	-49.57	42.23	-16.66	2.09	0.60	-10.51
			66	-46.92	42.22	-12.82	24.23	3.55	-7.36
38	Fondazio ne	18, 20	0	-35.08	-30.69	-9.52	29.55	3.52	7.95
			33	-32.45	-30.69	3.27	51.09	0.39	11.00
			66	-29.82	-30.69	23.09	72.10	-3.73	13.95
39	Fondazio ne	19, 21	0	55.15	48.33	-51.84	113.45	-3.21	-13.03
			33	52.11	48.33	-17.39	91.80	0.62	-10.18
			66	49.10	48.33	10.08	71.24	3.53	-7.45
40	Fondazio ne	19, 21	0	31.86	-24.10	1.12	62.14	3.50	7.75
			33	28.87	-24.10	18.99	42.77	0.51	10.38
			66	25.88	-24.11	30.65	24.39	-3.34	12.92
41	Fondazio ne	20, 22	0	-47.56	48.39	33.31	-85.58	-3.27	-13.12
			33	-44.95	48.38	7.91	-65.33	0.59	-10.28
			66	-42.36	48.38	-10.97	-46.14	3.53	-7.55
42	Fondazio ne	20, 22	0	-31.80	-23.88	-3.04	-39.10	3.50	7.78
			33	-29.22	-23.89	-13.44	-20.96	0.50	10.42
			66	-26.65	-23.89	-18.00	-3.72	-3.36	12.96
43	Fondazio ne	21, 23	0	51.54	42.62	17.71	-0.77	-3.78	-12.99
			33	48.56	42.61	15.11	-18.56	0.10	-10.55
			66	45.60	42.61	6.68	-36.09	3.20	-8.22
44	Fondazio ne	21, 23	0	28.46	-25.89	3.86	-48.42	3.18	8.53
			33	25.51	-25.90	-14.41	-65.87	-0.01	10.76
			66	22.58	-25.90	-38.42	-83.15	-3.92	12.90
45	Fondazio ne	22, 24	0	-42.36	45.65	-7.46	-13.39	-3.81	-13.17
			33	-39.80	45.65	-9.63	3.22	0.13	-10.72
			66	-37.26	45.65	-6.40	19.37	3.28	-8.39
46	Fondazio ne	22, 24	0	-27.52	-22.07	-1.84	24.75	3.26	8.61
			33	-24.99	-22.08	8.44	40.58	0.04	10.85
			66	-22.47	-22.08	23.89	56.05	-3.90	13.00
47	Fondazio ne	23, 25	0	53.55	58.41	-56.79	129.66	-2.90	-10.13
			33	50.63	58.41	-16.19	113.03	0.10	-8.10
			66	47.73	58.41	19.10	97.58	2.45	-6.17
48	Fondazio ne	23, 25	0	33.08	6.05	3.11	91.04	2.43	7.06
			33	30.19	6.05	31.35	76.80	-0.21	8.89
			66	27.31	6.05	55.04	63.41	-3.43	10.62
49	Fondazio ne	24, 26	0	-40.89	54.23	36.59	-85.81	-2.87	-10.28

			33	-38.38	54.23	10.24	-71.00	0.18	-8.22
			66	-35.88	54.22	-11.38	-57.20	2.57	-6.28
50	Fondazio ne	24, 26	0	-28.33	1.90	0.26	-51.70	2.54	6.04
			33	-25.84	1.90	-15.16	-38.93	0.24	7.89
			66	-23.37	1.90	-26.52	-27.02	-2.65	9.65
51	Fondazio ne	25, 26	0	-16.61	-6.01	66.62	-16.37	-4.63	-10.15
			49	-14.13	-6.01	54.30	-30.55	-0.70	-6.03
			97	-11.67	-6.01	37.22	-36.42	1.29	-2.17
52	Fondazio ne	25, 26	0	-12.91	-2.86	41.23	-14.66	1.20	-2.09
			49	-10.46	-2.86	33.35	-14.90	1.33	1.52
			97	-8.01	-2.86	26.30	-11.64	-0.24	4.90
53	Fondazio ne	25, 26	0	-8.98	1.62	22.93	-13.60	-0.30	-3.32
			49	-6.54	1.62	17.01	-8.50	0.54	-0.17
			97	-4.11	1.62	13.78	-2.74	-0.11	2.77
54	Fondazio ne	25, 26	0	-6.59	1.80	10.20	-11.07	-0.16	-2.77
			49	-4.16	1.80	5.70	-5.49	0.51	-0.05
			97	-1.74	1.80	3.78	-0.56	-0.08	2.45
55	Fondazio ne	25, 26	0	-4.66	1.52	1.40	-5.52	-0.13	-2.32
			49	-2.23	1.52	-0.75	-1.50	0.43	-0.02
			97	0.19	1.52	-1.18	1.58	-0.08	2.07
56	Fondazio ne	25, 26	0	-3.37	1.00	-2.11	-1.64	-0.14	-1.93
			49	-0.94	1.00	-2.82	0.58	0.34	-0.04
			97	1.48	1.00	-2.64	2.06	-0.06	1.65
57	Fondazio ne	25, 26	0	-2.48	0.49	-2.76	0.54	-0.11	-1.53
			49	-0.06	0.49	-2.74	1.45	0.26	-0.04
			97	2.36	0.49	-2.39	1.94	-0.05	1.26
58	Fondazio ne	25, 26	0	-1.86	0.16	-2.16	1.43	-0.10	-1.14
			49	0.56	0.16	-1.88	1.65	0.18	-0.04
			97	2.98	0.16	-1.54	1.72	-0.03	0.87
59	Fondazio ne	25, 26	0	-1.41	-0.01	-1.22	1.55	-0.09	-0.78
			49	1.01	-0.01	-0.95	1.57	0.11	-0.06
			97	3.43	-0.01	-0.66	1.59	0.00	0.46
60	Fondazio ne	25, 26	0	-0.56	-0.04	-0.27	1.44	-0.07	-0.37
			49	1.86	-0.04	-0.04	1.52	0.02	-0.03
			97	4.29	-0.04	0.24	1.66	-0.01	0.11
61	Fondazio ne	25, 26	0	-0.29	0.02	0.58	1.42	-0.07	-0.02
			49	2.14	0.02	0.83	1.62	-0.05	-0.07
			97	4.57	0.02	1.18	1.83	0.03	-0.30
62	Fondazio ne	25, 26	0	0.29	0.23	1.49	1.58	-0.02	0.39
			49	2.72	0.23	1.82	1.75	-0.12	-0.04
			97	5.15	0.23	2.20	1.79	0.04	-0.66
63	Fondazio ne	25, 26	0	1.07	0.55	2.45	1.90	-0.01	0.78
			49	3.51	0.55	2.85	1.69	-0.19	-0.03
			97	5.94	0.55	3.06	1.08	0.06	-1.04
64	Fondazio ne	25, 26	0	2.07	0.91	3.03	2.07	0.01	1.16
			49	4.51	0.91	3.29	0.88	-0.27	-0.04
			97	6.96	0.91	2.79	-1.05	0.09	-1.44
65	Fondazio ne	25, 26	0	3.32	1.08	2.02	1.69	0.04	1.55
			49	5.76	1.08	1.70	-1.17	-0.33	-0.06
			97	8.22	1.08	-0.26	-5.07	0.13	-1.86
66	Fondazio ne	25, 26	0	4.86	0.71	-2.35	-0.05	0.08	1.96
			49	7.32	0.71	-4.03	-5.01	-0.39	-0.05
			97	9.78	0.71	-8.36	-10.88	0.16	-2.26
67	Fondazio ne	25, 26	0	6.70	-0.76	-12.69	-4.49	0.11	2.23
			49	9.17	-0.76	-16.92	-10.88	-0.39	-0.20

			97	11.65	-0.76	-24.24	-16.99	0.34	-2.85
68	Fondazio ne	25, 26	0	8.66	-4.64	-28.94	-3.73	0.29	3.61
			49	11.15	-4.64	-32.48	-8.36	-0.77	0.75
			97	13.64	-4.64	-37.57	-9.80	-0.40	-2.33
69	Fondazio ne	25, 26	0	12.59	-7.78	-40.68	-35.50	-0.45	-0.19
			49	15.09	-7.78	-57.81	-31.69	0.43	-3.50
			97	17.61	-7.78	-71.25	-19.81	2.99	-7.03
70	Fondazio ne	25, 28	0	61.63	18.38	28.60	-5.49	1.18	-2.49
			43	57.95	18.38	23.39	-22.54	1.78	-0.41
			85	54.30	18.37	10.80	-40.38	1.54	1.52
71	Fondazio ne	25, 28	0	34.47	-22.99	9.34	-49.09	1.52	3.18
			43	30.85	-22.99	-14.84	-68.36	-0.22	4.96
			85	27.24	-23.00	-47.51	-88.95	-2.68	6.61
72	Fondazio ne	26, 27	0	-35.50	25.47	-9.50	-2.66	0.46	-3.96
			33	-33.04	25.46	-8.98	8.70	1.49	-2.30
			66	-30.58	25.46	-4.77	19.72	1.99	-0.73
73	Fondazio ne	26, 27	0	-19.46	-15.60	-1.65	26.52	1.97	6.03
			33	-17.01	-15.60	8.40	37.31	-0.27	7.51
			66	-14.58	-15.60	21.97	47.82	-2.98	8.91
74	Fondazio ne	27, 29	0	-30.24	38.39	32.99	-68.64	-1.89	-6.96
			33	-27.81	38.39	11.52	-58.68	0.19	-5.65
			66	-25.39	38.38	-6.80	-49.62	1.85	-4.43
75	Fondazio ne	27, 29	0	-14.88	0.33	3.24	-47.52	1.83	4.55
			33	-12.47	0.32	-11.56	-39.42	0.14	5.68
			66	-10.06	0.32	-23.83	-32.18	-1.91	6.73
76	Fondazio ne	28, 30	0	72.30	34.15	-60.83	92.89	-1.60	-6.58
			37	69.23	34.15	-29.59	75.00	0.56	-5.29
			73	66.19	34.15	-4.76	57.95	2.27	-4.10
77	Fondazio ne	28, 30	0	53.10	3.77	-14.76	38.09	2.26	4.57
			37	50.09	3.77	-3.18	22.34	0.39	5.65
			73	47.10	3.77	2.92	8.06	-1.86	6.63
78	Fondazio ne	29, 31	0	-25.97	28.82	-11.71	6.32	-1.48	-5.23
			33	-23.57	28.82	-8.99	12.97	0.09	-4.27
			66	-21.17	28.81	-4.14	19.24	1.35	-3.40
79	Fondazio ne	29, 31	0	-10.64	1.60	0.89	20.41	1.33	3.46
			33	-8.25	1.60	8.15	26.40	0.05	4.25
			66	-5.87	1.60	17.33	32.05	-1.47	4.95
80	Fondazio ne	30, 32	0	42.85	35.39	-17.28	50.17	-1.19	-4.42
			34	40.06	35.39	-1.64	38.17	0.18	-3.60
			69	37.28	35.38	10.14	27.65	1.28	-2.86
81	Fondazio ne	30, 32	0	31.46	9.21	-2.32	26.19	1.26	3.14
			34	28.70	9.21	5.60	17.10	0.07	3.78
			69	25.95	9.21	10.64	9.36	-1.32	4.35
82	Fondazio ne	31, 33	0	-22.17	28.45	30.09	-59.57	-0.62	-2.79
			33	-19.79	28.45	10.81	-54.51	0.20	-2.17
			66	-17.41	28.45	-6.93	-50.33	0.83	-1.64
83	Fondazio ne	31, 33	0	-7.03	13.11	3.83	-48.10	0.80	2.09
			33	-4.67	13.11	-11.96	-44.88	0.04	2.53
			66	-2.30	13.11	-26.83	-42.52	-0.86	2.89
84	Fondazio ne	32, 34	0	25.20	28.03	-10.04	33.89	-0.67	-2.47
			35	22.44	28.03	1.04	27.36	0.09	-2.00
			69	19.69	28.03	10.09	22.12	0.71	-1.61
85	Fondazio ne	32, 34	0	14.98	13.96	-2.02	19.60	0.70	1.81
			35	12.24	13.96	4.56	15.57	0.02	2.10
			69	9.50	13.96	9.95	12.70	-0.74	2.32

86	Fondazio ne	33, 35	0	-18.44	17.39	-14.72	16.59	-0.30	-1.22
			33	-16.07	17.39	-9.41	18.40	0.06	-0.94
			66	-13.72	17.39	-3.56	19.88	0.33	-0.75
87	Fondazio ne	33, 35	0	-3.30	12.25	1.61	20.10	0.31	0.85
			33	-0.95	12.25	7.99	21.37	0.01	0.95
			66	1.40	12.25	14.74	22.34	-0.31	0.98
88	Fondazio ne	34, 36	0	10.16	21.80	-8.72	20.61	-0.13	-0.53
			35	7.42	21.80	-1.41	18.79	0.03	-0.41
			69	4.69	21.80	5.46	18.08	0.16	-0.37
89	Fondazio ne	34, 36	0	1.04	19.78	-5.00	18.19	0.14	0.54
			35	-1.69	19.78	1.85	18.57	-0.04	0.49
			69	-4.42	19.78	9.03	20.04	-0.19	0.35
90	Fondazio ne	35, 37	0	-14.75	16.74	27.02	-48.77	0.32	0.83
			33	-12.40	16.74	10.55	-48.32	0.05	0.77
			66	-10.05	16.74	-5.90	-48.65	-0.18	0.62
91	Fondazio ne	35, 37	0	-0.12	23.00	4.17	-47.73	-0.21	-0.26
			33	2.23	23.00	-12.22	-48.93	-0.08	-0.49
			66	4.57	23.01	-29.14	-50.90	0.13	-0.81
92	Fondazio ne	36, 38	0	-4.06	16.87	-9.25	11.87	0.42	1.43
			35	-6.79	16.87	-4.20	14.39	-0.04	1.20
			69	-9.53	16.87	1.90	18.02	-0.40	0.89
93	Fondazio ne	36, 38	0	-13.40	26.71	-9.02	19.82	-0.42	-0.66
			35	-16.14	26.71	-0.84	24.64	-0.13	-1.06
			69	-18.89	26.71	9.22	30.70	0.32	-1.56
94	Fondazio ne	37, 39	0	-12.15	4.96	-18.22	30.37	0.87	2.81
			33	-9.81	4.96	-9.05	27.96	0.01	2.41
			66	-7.47	4.96	-0.72	25.35	-0.71	1.93
95	Fondazio ne	37, 39	0	2.05	21.54	3.85	24.27	-0.73	-1.99
			33	4.39	21.54	10.95	21.55	0.01	-2.56
			66	6.73	21.54	17.11	18.59	0.97	-3.21
96	Fondazio ne	38, 40	0	-18.67	14.00	-10.33	7.83	0.94	3.35
			34	-21.41	14.00	-5.90	15.06	-0.11	2.77
			69	-24.15	14.01	1.24	23.62	-0.95	2.10
97	Fondazio ne	38, 40	0	-29.04	35.19	-11.32	27.33	-0.97	-1.82
			34	-31.79	35.19	0.25	37.29	-0.22	-2.57
			69	-34.56	35.19	15.49	48.72	0.80	-3.41
98	Fondazio ne	39, 41	0	-10.39	4.29	28.04	-31.20	1.43	4.60
			33	-8.05	4.29	16.72	-34.67	0.03	3.86
			66	-5.71	4.29	4.13	-39.00	-1.11	3.04
99	Fondazio ne	39, 41	0	2.11	35.29	14.08	-32.25	-1.13	-3.10
			33	4.45	35.30	2.11	-37.65	0.04	-4.00
			66	6.79	35.30	-11.84	-44.26	1.52	-4.99
100	Fondazio ne	40, 42	0	-35.53	10.84	-6.92	11.93	1.46	5.51
			35	-38.33	10.84	-0.06	24.86	-0.28	4.57
			69	-41.14	10.84	11.52	39.22	-1.69	3.54
101	Fondazio ne	40, 42	0	-49.25	43.48	-3.32	53.37	-1.70	-2.93
			35	-52.08	43.48	18.33	69.09	-0.50	-4.06
			69	-54.94	43.49	45.62	85.95	1.11	-5.28
102	Fondazio ne	41, 44	0	12.11	-0.04	3.06	-11.60	2.13	6.86
			33	14.45	-0.04	-2.48	-19.36	0.05	5.79
			66	16.79	-0.03	-10.78	-28.26	-1.68	4.64
103	Fondazio ne	41, 44	0	24.92	28.71	-1.60	-40.73	-1.70	0.04
			33	27.28	28.71	-17.12	-50.66	-1.51	-1.19
			66	29.64	28.71	-36.07	-61.43	-0.90	-2.51
104	Fondazio	42, 43	0	-58.76	-1.89	25.24	25.16	1.82	11.37

	ne								
			23	-60.67	-1.89	32.74	36.76	-0.70	10.50
			46	-62.60	-1.89	42.93	48.44	-3.01	9.58
105	Fondazio ne	43, 44	0	18.18	-0.04	-54.21	-17.94	-4.55	-9.65
			49	16.21	-0.04	-57.53	0.75	-0.83	-5.68
			97	14.25	-0.04	-54.25	9.72	1.01	-1.93
106	Fondazio ne	43, 44	0	11.60	-0.36	-44.94	11.41	0.95	-2.03
			49	9.65	-0.36	-38.20	13.80	1.08	1.48
			97	7.70	-0.36	-31.39	12.05	-0.46	4.78
107	Fondazio ne	43, 44	0	7.63	1.18	-24.28	13.28	-0.51	-3.42
			49	5.69	1.18	-18.32	9.33	0.39	-0.33
			97	3.76	1.18	-14.56	4.47	-0.15	2.54
108	Fondazio ne	43, 44	0	4.45	1.66	-10.14	9.83	-0.24	-2.68
			49	2.52	1.66	-6.17	4.94	0.41	-0.02
			97	0.59	1.66	-4.48	0.53	-0.19	2.45
109	Fondazio ne	43, 44	0	2.85	1.62	-1.91	5.42	-0.25	-2.36
			49	0.92	1.62	0.18	1.76	0.34	-0.10
			97	-1.01	1.62	0.70	-1.08	-0.12	1.96
110	Fondazio ne	43, 44	0	1.66	1.16	1.73	1.75	-0.18	-1.93
			49	-0.27	1.16	2.44	-0.30	0.29	-0.06
			97	-2.19	1.16	2.32	-1.68	-0.09	1.60
111	Fondazio ne	43, 44	0	0.83	0.63	2.47	-0.32	-0.14	-1.53
			49	-1.10	0.63	2.47	-1.17	0.24	-0.06
			97	-3.03	0.63	2.16	-1.63	-0.06	1.22
112	Fondazio ne	43, 44	0	0.26	0.25	1.97	-1.17	-0.11	-1.14
			49	-1.67	0.25	1.73	-1.38	0.17	-0.06
			97	-3.60	0.25	1.42	-1.43	-0.02	0.84
113	Fondazio ne	43, 44	0	-0.14	0.04	1.14	-1.34	-0.08	-0.75
			49	-2.07	0.04	0.88	-1.33	0.11	-0.04
			97	-4.00	0.04	0.62	-1.32	-0.01	0.48
114	Fondazio ne	43, 44	0	-0.35	-0.04	0.34	-1.27	-0.06	-0.40
			49	-2.28	-0.04	0.11	-1.30	0.04	-0.07
			97	-4.22	-0.04	-0.15	-1.38	0.04	0.08
115	Fondazio ne	43, 44	0	-0.86	0.05	-0.42	-1.17	-0.03	-0.01
			49	-2.80	0.05	-0.63	-1.31	-0.03	-0.05
			97	-4.74	0.05	-0.92	-1.46	0.05	-0.28
116	Fondazio ne	43, 44	0	-1.17	0.24	-1.19	-1.28	-0.01	0.36
			49	-3.11	0.24	-1.46	-1.41	-0.09	-0.05
			97	-5.06	0.24	-1.77	-1.45	0.07	-0.65
117	Fondazio ne	43, 44	0	-1.62	0.55	-1.99	-1.48	0.02	0.74
			49	-3.57	0.55	-2.30	-1.33	-0.15	-0.05
			97	-5.52	0.55	-2.46	-0.87	0.10	-1.03
118	Fondazio ne	43, 44	0	-2.20	0.91	-2.42	-1.63	0.05	1.11
			49	-4.15	0.91	-2.62	-0.72	-0.21	-0.06
			97	-6.11	0.91	-2.24	0.79	0.14	-1.42
119	Fondazio ne	43, 44	0	-2.89	1.11	-1.52	-1.38	0.08	1.48
			49	-4.85	1.11	-1.29	0.86	-0.27	-0.07
			97	-6.82	1.11	0.23	3.91	0.18	-1.82
120	Fondazio ne	43, 44	0	-3.69	0.69	2.20	-0.17	0.13	1.90
			49	-5.65	0.69	3.43	3.72	-0.33	-0.05
			97	-7.63	0.69	6.73	8.31	0.20	-2.19
121	Fondazio ne	43, 44	0	-4.52	-0.63	10.92	3.38	0.14	2.08
			49	-6.50	-0.63	14.16	8.33	-0.31	-0.26
			97	-8.48	-0.63	19.78	12.99	0.43	-2.81
122	Fondazio ne	43, 44	0	-5.64	-2.88	26.20	5.98	0.37	3.53

			49	-7.63	-2.88	30.41	9.31	-0.69	0.78
			97	-9.62	-2.88	35.60	9.76	-0.36	-2.18
123	Fondazio ne	43, 44	0	-9.06	-7.50	42.02	12.26	-0.44	0.26
			49	-11.07	-7.50	47.57	7.88	0.20	-2.92
			97	-13.08	-7.50	49.32	-3.84	2.44	-6.31
124	Fondazio ne	43, 45	0	-35.45	-14.45	32.43	-86.63	2.63	9.06
			33	-38.22	-14.45	7.13	-70.18	-0.14	7.67
			66	-41.01	-14.45	-12.84	-54.36	-2.43	6.19
125	Fondazio ne	43, 45	0	-56.65	36.00	-7.93	-47.10	-2.45	-6.41
			33	-59.45	36.00	-20.38	-31.89	-0.07	-7.98
			66	-62.28	36.01	-27.88	-17.00	2.83	-9.64
126	Fondazio ne	44, 46	0	13.54	-1.47	-18.76	40.21	2.54	8.56
			33	15.91	-1.47	-7.81	29.01	-0.05	7.14
			66	18.29	-1.47	-0.59	17.62	-2.16	5.64
127	Fondazio ne	44, 46	0	27.12	44.16	7.35	10.09	-2.18	-5.80
			33	29.51	44.16	8.31	-1.42	-0.01	-7.39
			66	31.91	44.16	5.43	-13.16	2.71	-9.08
128	Fondazio ne	45, 47	0	-28.34	-13.03	-44.10	45.14	3.00	10.78
			33	-31.18	-13.02	-26.17	60.15	-0.27	9.02
			66	-34.04	-13.02	-3.18	75.85	-2.94	7.17
129	Fondazio ne	45, 47	0	-51.25	46.69	-15.07	86.46	-2.96	-6.62
			33	-54.12	46.70	16.76	103.15	-0.46	-8.57
			66	-57.01	46.70	54.26	120.77	2.70	-10.62
130	Fondazio ne	46, 48	0	10.64	-12.62	22.56	-28.93	2.86	9.92
			33	13.05	-12.61	10.55	-41.08	-0.13	8.13
			66	15.46	-12.61	-5.59	-53.88	-2.50	6.26
131	Fondazio ne	46, 48	0	24.96	48.13	8.27	-53.69	-2.52	-5.49
			33	27.38	48.13	-12.14	-67.22	-0.39	-7.46
			66	29.80	48.13	-37.14	-81.41	2.41	-9.52
132	Fondazio ne	47, 49	0	-27.84	-27.87	37.55	-85.50	3.71	12.67
			33	-30.75	-27.87	12.88	-67.48	-0.12	10.52
			66	-33.66	-27.86	-5.84	-49.51	-3.22	8.29
133	Fondazio ne	47, 49	0	-50.07	38.87	-5.95	-43.83	-3.25	-8.06
			33	-53.01	38.87	-16.88	-25.97	-0.21	-10.39
			66	-55.96	38.88	-21.91	-8.02	3.62	-12.83
134	Fondazio ne	48, 50	0	9.59	-27.75	-26.29	61.56	3.43	11.92
			33	12.02	-27.75	-8.85	47.09	-0.15	9.76
			66	14.46	-27.75	3.82	32.64	-3.00	7.51
135	Fondazio ne	48, 50	0	23.16	41.15	7.66	24.47	-3.02	-7.90
			33	25.60	41.15	12.87	10.09	-0.03	-10.24
			66	28.06	41.16	13.33	-4.41	3.75	-12.68
136	Fondazio ne	49, 51	0	-30.00	-25.14	-32.87	25.69	3.21	12.68
			33	-32.97	-25.14	-20.78	44.10	-0.55	10.14
			66	-35.95	-25.14	-2.48	63.40	-3.47	7.52
137	Fondazio ne	49, 51	0	-53.17	46.59	-10.74	71.94	-3.50	-7.23
			33	-56.16	46.60	16.94	92.37	-0.66	-9.96
			66	-59.18	46.60	51.54	113.84	3.09	-12.80
138	Fondazio ne	50, 52	0	9.28	-27.69	22.43	3.03	3.36	12.53
			33	11.74	-27.69	20.50	-11.84	-0.36	10.00
			66	14.21	-27.68	13.55	-27.44	-3.23	7.37
139	Fondazio ne	50, 52	0	20.70	50.13	21.73	-29.18	-3.25	-7.69
			33	23.17	50.14	8.90	-45.83	-0.26	-10.41
			66	25.65	50.14	-9.65	-63.79	3.63	-13.23
140	Fondazio ne	51, 53	0	-31.14	-36.92	41.47	-97.62	3.57	13.84
			33	-34.17	-36.91	13.48	-75.62	-0.52	10.89

			66	-37.21	-36.91	-7.23	-53.58	-3.61	7.85
141	Fondazio ne	51, 53	0	-55.91	36.05	-6.05	-46.62	-3.64	-7.48
			33	-58.97	36.05	-17.19	-24.59	-0.65	-10.63
			66	-62.05	36.06	-21.03	-2.36	3.39	-13.90
142	Fondazio ne	52, 54	0	29.09	-23.31	4.46	24.94	3.49	13.50
			33	31.58	-23.31	9.04	5.62	-0.48	10.58
			66	34.08	-23.31	7.01	-15.16	-3.48	7.56
143	Fondazio ne	52, 54	0	39.69	50.67	17.36	-24.55	-3.50	-6.86
			33	42.20	50.68	5.11	-46.96	-0.72	-9.97
			66	44.73	50.68	-14.84	-71.18	3.09	-13.19
144	Fondazio ne	53, 55	0	-36.88	-18.48	-34.31	42.50	2.35	12.88
			33	-39.98	-18.47	-15.93	65.29	-1.34	9.50
			66	-43.09	-18.47	10.13	89.04	-3.90	6.01
145	Fondazio ne	53, 55	0	-62.14	47.43	-2.75	100.56	-3.93	-5.02
			33	-65.27	47.44	35.13	125.36	-1.68	-8.64
			66	-68.42	47.44	81.33	150.89	1.78	-12.38
146	Fondazio ne	54, 56	0	49.01	-12.64	3.66	12.90	2.57	12.77
			33	51.55	-12.63	3.17	-13.10	-1.10	9.45
			66	54.12	-12.63	-6.20	-40.93	-3.66	6.02
147	Fondazio ne	54, 56	0	63.65	50.15	9.77	-63.87	-3.68	-4.15
			33	66.24	50.16	-16.67	-93.53	-1.73	-7.69
			66	68.85	50.16	-53.18	-124.90	1.41	-11.35
148	Fondazio ne	55, 57	0	-24.05	-13.07	57.25	-84.52	1.52	15.74
			40	-27.88	-13.06	30.50	-54.11	-3.81	11.05
			80	-31.71	-13.06	15.55	-25.34	-7.23	6.15
149	Fondazio ne	55, 57	0	-38.85	31.17	1.24	13.06	-7.27	-10.13
			40	-42.70	31.18	12.55	39.54	-2.24	-15.26
			80	-46.58	31.18	33.88	63.40	4.89	-20.67
150	Fondazio ne	56, 70	0	28.19	3.25	-26.49	74.25	0.94	14.10
			40	31.36	3.26	-5.39	34.88	-3.77	9.53
			80	34.54	3.27	-0.20	-5.76	-6.62	4.77
151	Fondazio ne	56, 70	0	34.11	48.37	22.75	-48.48	-6.65	-9.25
			40	37.31	48.38	-5.44	-90.37	-1.99	-14.24
			80	40.53	48.39	-50.57	-133.67	4.70	-19.49
152	Fondazio ne	57, 58	0	81.82	-18.57	-52.67	-48.85	0.06	-7.87
			42	76.28	-18.57	-68.12	-33.57	2.44	-3.64
			83	70.78	-18.57	-80.37	-32.99	3.12	0.31
153	Fondazio ne	57, 58	0	55.07	-19.43	-73.50	-74.22	3.09	-2.94
			42	49.60	-19.44	-105.26	-85.71	3.53	0.75
			83	44.17	-19.44	-143.78	-106.02	2.49	4.22
154	Fondazio ne	58, 59	0	113.28	12.89	-150.13	150.71	2.32	-1.08
			35	108.65	12.89	-100.70	130.10	2.26	1.39
			69	104.07	12.89	-58.61	108.59	1.37	3.73
155	Fondazio ne	58, 59	0	85.27	2.80	-65.68	78.82	1.35	0.18
			35	80.73	2.80	-41.20	58.06	0.90	2.39
			69	76.22	2.80	-23.59	39.13	-0.29	4.49
156	Fondazio ne	59, 60	0	66.59	33.14	-41.74	87.21	-0.42	-4.30
			35	62.11	33.14	-13.67	70.81	0.72	-2.32
			69	57.65	33.14	9.25	57.43	1.19	-0.46
157	Fondazio ne	59, 60	0	46.76	5.07	-4.15	55.11	1.17	1.19
			35	42.32	5.07	13.89	44.85	0.46	2.95
			69	37.90	5.07	28.90	37.56	-0.85	4.60
158	Fondazio ne	60, 61	0	28.27	28.32	13.34	53.39	-0.79	-3.44
			35	23.87	28.32	31.76	48.68	0.13	-1.89
			69	19.47	28.32	48.92	46.04	0.53	-0.46

159	Fondazio ne	60, 61	0	4.38	-12.78	42.59	72.85	0.51	0.09
			35	-0.01	-12.78	68.35	71.47	0.24	1.42
			69	-4.41	-12.78	93.68	70.19	-0.46	2.64
160	Fondazio ne	61, 62	0	48.98	-13.05	97.84	-150.78	-0.89	-3.51
			35	44.59	-13.06	46.29	-153.56	0.13	-2.39
			69	40.22	-13.06	-6.70	-159.25	0.77	-1.38
161	Fondazio ne	61, 62	0	17.70	-34.42	10.98	-164.17	0.75	0.98
			35	13.34	-34.42	-46.24	-173.20	0.25	1.89
			69	8.99	-34.42	-107.12	-185.18	-0.54	2.69
162	Fondazio ne	62, 63	0	65.41	15.00	-105.44	112.17	0.11	-2.04
			35	61.07	15.00	-68.17	98.73	0.69	-1.34
			69	56.76	15.00	-35.55	85.52	1.05	-0.74
163	Fondazio ne	62, 63	0	39.99	13.24	-44.35	47.36	1.03	1.44
			35	35.70	13.24	-29.26	35.47	0.44	1.94
			69	31.42	13.24	-17.93	25.63	-0.30	2.35
164	Fondazio ne	63, 64	0	21.83	35.66	-38.97	73.87	-0.06	-0.93
			35	17.56	35.66	-13.97	66.63	0.20	-0.61
			69	13.30	35.66	9.05	62.42	0.37	-0.38
165	Fondazio ne	63, 64	0	1.77	22.01	-8.25	61.17	0.35	1.23
			35	-2.48	22.01	13.43	60.12	-0.10	1.36
			69	-6.75	22.01	35.28	62.12	-0.58	1.41
166	Fondazio ne	64, 65	0	-16.31	27.97	13.92	38.26	-0.30	0.08
			35	-20.58	27.97	28.70	42.89	-0.32	0.03
			69	-24.85	27.97	45.46	49.64	-0.31	-0.11
167	Fondazio ne	64, 65	0	-41.80	2.73	36.03	85.48	-0.33	0.44
			35	-46.08	2.73	67.75	93.62	-0.45	0.21
			69	-50.39	2.73	102.38	102.05	-0.47	-0.12
168	Fondazio ne	65, 66	0	6.53	-18.94	103.23	-172.40	-0.32	0.05
			35	2.22	-18.94	45.90	-165.33	-0.26	-0.38
			69	-2.09	-18.94	-9.45	-161.06	-0.04	-0.92
169	Fondazio ne	65, 66	0	-25.01	-23.19	6.70	-159.10	-0.06	0.44
			35	-29.33	-23.19	-47.05	-158.06	-0.11	-0.19
			69	-33.66	-23.19	-100.95	-159.78	0.08	-0.92
170	Fondazio ne	66, 67	0	20.79	3.32	-98.40	85.36	0.37	1.13
			35	16.46	3.32	-68.59	82.30	0.12	0.29
			69	12.14	3.32	-39.84	79.55	0.18	-0.64
171	Fondazio ne	66, 67	0	-4.34	20.44	-46.81	47.35	0.16	1.11
			35	-8.66	20.44	-29.89	46.03	-0.05	0.08
			69	-12.99	20.44	-13.07	46.93	0.12	-1.06
172	Fondazio ne	67, 68	0	-22.09	20.35	-31.41	55.15	0.37	2.54
			35	-26.43	20.35	-10.98	58.76	-0.30	1.31
			69	-30.77	20.35	11.22	65.44	-0.52	-0.03
173	Fondazio ne	67, 68	0	-42.16	27.96	-2.82	63.41	-0.55	0.77
			35	-46.52	27.97	21.53	73.22	-0.57	-0.66
			69	-50.90	27.97	49.77	85.90	-0.08	-2.21
174	Fondazio ne	68, 69	0	-60.99	14.38	31.28	53.42	0.06	3.52
			35	-65.39	14.38	53.11	68.33	-0.87	1.87
			69	-69.82	14.39	80.35	84.56	-1.21	0.11
175	Fondazio ne	68, 69	0	-88.87	6.43	73.91	116.33	-1.24	2.23
			35	-93.33	6.43	117.76	132.52	-1.69	0.36
			69	-97.82	6.44	166.92	146.70	-1.47	-1.63
176	Fondazio ne	69, 70	0	-37.49	-26.38	164.08	-104.71	-1.32	5.04
			42	-42.79	-26.37	124.14	-94.21	-2.83	2.18
			83	-48.12	-26.37	86.28	-95.49	-3.10	-0.88
177	Fondazio	69, 70	0	-69.53	-32.13	102.08	-60.70	-3.14	1.66

	ne								
			42	-74.89	-32.13	75.03	-77.63	-3.15	-1.64
			83	-80.29	-32.13	37.14	-113.30	-1.74	-5.18
178	Primo Impalcato	1, 2	0	-15.41	-4.31	160.68	-69.62	21.69	29.71
			83	-15.41	-4.31	102.81	-69.62	-3.01	29.71
			166	-15.41	-4.31	44.94	-69.62	-27.71	29.71
179	Primo Impalcato	1, 15	0	55.64	-2.06	-236.34	195.46	-18.64	-7.30
			80	55.64	-2.06	-80.94	195.46	-12.84	-7.30
			159	55.64	-2.06	74.45	195.46	-7.03	-7.30
180	Primo Impalcato	2, 3	0	0.93	-0.19	59.47	-64.89	-25.75	-9.22
			69	0.93	-0.19	14.69	-64.89	-19.39	-9.22
			138	0.93	-0.19	-30.08	-64.89	-13.04	-9.22
181	Primo Impalcato	3, 4	0	1.72	0.15	-13.14	6.18	-12.94	-7.11
			69	1.72	0.15	-8.88	6.18	-8.03	-7.11
			138	1.72	0.15	-4.61	6.18	-3.12	-7.11
182	Primo Impalcato	4, 5	0	2.40	0.43	11.72	6.22	-3.19	-1.59
			69	2.40	0.43	16.01	6.22	-2.09	-1.59
			138	2.40	0.43	20.30	6.22	-0.99	-1.59
183	Primo Impalcato	5, 6	0	3.11	0.72	38.11	-107.84	-0.97	0.54
			69	3.11	0.72	-36.29	-107.84	-1.34	0.54
			138	3.11	0.72	-110.70	-107.84	-1.71	0.54
184	Primo Impalcato	6, 7	0	7.64	1.03	-96.61	139.72	-1.95	0.48
			69	7.64	1.03	-0.20	139.72	-2.28	0.48
			138	7.64	1.03	96.21	139.72	-2.61	0.48
185	Primo Impalcato	7, 8	0	11.49	1.31	110.29	-86.62	-2.04	-0.34
			69	11.49	1.31	50.52	-86.62	-1.81	-0.34
			138	11.49	1.31	-9.25	-86.62	-1.58	-0.34
186	Primo Impalcato	8, 9	0	12.32	1.46	9.83	-87.08	-1.26	-0.51
			69	12.32	1.46	-50.25	-87.08	-0.91	-0.51
			138	12.32	1.46	-110.34	-87.08	-0.56	-0.51
187	Primo Impalcato	9, 10	0	13.39	1.47	-96.21	139.22	-0.39	-0.31
			69	13.39	1.47	-0.15	139.22	-0.18	-0.31
			138	13.39	1.47	95.92	139.22	0.03	-0.31
188	Primo Impalcato	10, 11	0	22.45	1.37	110.04	-108.32	0.33	-1.15
			69	22.45	1.37	35.30	-108.32	1.12	-1.15
			138	22.45	1.37	-39.44	-108.32	1.92	-1.15
189	Primo Impalcato	11, 12	0	23.24	1.08	-21.71	24.27	2.10	-3.80
			69	23.24	1.08	-4.96	24.27	4.73	-3.80
			138	23.24	1.08	11.78	24.27	7.35	-3.80
190	Primo Impalcato	12, 13	0	24.05	0.66	28.93	-64.67	7.51	-5.60
			69	24.05	0.66	-15.70	-64.67	11.38	-5.60
			138	24.05	0.66	-60.32	-64.67	15.24	-5.60
191	Primo Impalcato	13, 14	0	30.12	-1.70	-45.50	-62.73	15.82	8.12
			83	30.12	-1.70	-97.65	-62.73	9.07	8.12
			166	30.12	-1.70	-149.79	-62.73	2.31	8.12
192	Primo Impalcato	14, 16	0	13.75	-1.95	101.35	-86.51	3.06	5.74
			80	13.75	-1.95	32.58	-86.51	-1.50	5.74
			159	13.75	-1.95	-36.20	-86.51	-6.06	5.74
193	Primo Impalcato	15, 17	0	26.75	-1.01	-36.03	85.54	-6.47	-1.41
			66	26.75	-1.01	20.42	85.54	-5.54	-1.41
			132	26.75	-1.01	76.88	85.54	-4.61	-1.41
194	Primo Impalcato	16, 18	0	27.04	-1.07	11.69	-37.88	-5.56	0.28
			66	27.04	-1.07	-13.31	-37.88	-5.75	0.28
			132	27.04	-1.07	-38.31	-37.88	-5.93	0.28
195	Primo Impalcato	17, 19	0	5.27	-0.49	-28.47	39.55	-4.31	0.82

			66	5.27	-0.49	-2.37	39.55	-4.85	0.82
			132	5.27	-0.49	23.74	39.55	-5.39	0.82
196	Primo Impalcato	18, 20	0	22.82	-0.50	8.13	-10.99	-6.49	-0.49
			66	22.82	-0.50	0.87	-10.99	-6.17	-0.49
			132	22.82	-0.50	-6.38	-10.99	-5.85	-0.49
197	Primo Impalcato	19, 21	0	-12.81	0.02	-82.29	123.86	-5.09	-0.03
			66	-12.81	0.02	-0.54	123.86	-5.07	-0.03
			132	-12.81	0.02	81.20	123.86	-5.05	-0.03
198	Primo Impalcato	20, 22	0	22.75	0.02	36.65	-56.03	-5.51	-0.63
			66	22.75	0.02	-0.33	-56.03	-5.10	-0.63
			132	22.75	0.02	-37.31	-56.03	-4.69	-0.63
199	Primo Impalcato	21, 23	0	-36.18	0.48	-24.95	37.45	-4.76	-1.09
			66	-36.18	0.48	-0.23	37.45	-4.04	-1.09
			132	-36.18	0.48	24.48	37.45	-3.31	-1.09
200	Primo Impalcato	22, 24	0	25.61	0.48	5.40	-8.46	-5.03	-1.14
			66	25.61	0.48	-0.18	-8.46	-4.28	-1.14
			132	25.61	0.48	-5.76	-8.46	-3.52	-1.14
201	Primo Impalcato	23, 25	0	-55.24	0.76	-81.68	125.17	-3.10	-1.43
			66	-55.24	0.76	0.93	125.17	-2.15	-1.43
			132	-55.24	0.76	83.54	125.17	-1.21	-1.43
202	Primo Impalcato	24, 26	0	26.56	0.78	36.70	-55.80	-3.28	-0.99
			66	26.56	0.78	-0.13	-55.80	-2.62	-0.99
			132	26.56	0.78	-36.96	-55.80	-1.97	-0.99
203	Primo Impalcato	25, 28	0	-105.68	0.94	-22.25	30.26	-0.99	-0.16
			85	-105.68	0.94	3.46	30.26	-0.86	-0.16
			170	-105.68	0.94	29.18	30.26	-0.73	-0.16
204	Primo Impalcato	26, 27	0	29.58	1.00	5.23	-8.08	-2.06	-1.25
			66	29.58	1.00	-0.10	-8.08	-1.24	-1.25
			132	29.58	1.00	-5.43	-8.08	-0.41	-1.25
205	Primo Impalcato	27, 29	0	31.13	1.03	36.87	-55.78	-0.30	-0.47
			66	31.13	1.03	0.06	-55.78	0.01	-0.47
			132	31.13	1.03	-36.76	-55.78	0.32	-0.47
206	Primo Impalcato	28, 30	0	-152.34	0.99	-76.18	93.46	-0.48	-0.15
			73	-152.34	0.99	-7.95	93.46	-0.37	-0.15
			146	-152.34	0.99	60.27	93.46	-0.26	-0.15
207	Primo Impalcato	29, 31	0	34.80	1.00	5.20	-8.26	0.44	-0.15
			66	34.80	1.00	-0.25	-8.26	0.54	-0.15
			132	34.80	1.00	-5.70	-8.26	0.64	-0.15
208	Primo Impalcato	30, 32	0	-113.72	0.98	-47.87	73.90	0.22	-0.04
			69	-113.72	0.98	2.75	73.90	0.25	-0.04
			137	-113.72	0.98	53.37	73.90	0.28	-0.04
209	Primo Impalcato	31, 33	0	35.07	0.95	37.58	-56.74	0.69	0.39
			66	35.07	0.95	0.13	-56.74	0.44	0.39
			132	35.07	0.95	-37.32	-56.74	0.18	0.39
210	Primo Impalcato	32, 34	0	-75.28	0.93	-53.89	77.90	0.77	0.49
			69	-75.28	0.93	-0.14	77.90	0.43	0.49
			138	-75.28	0.93	53.61	77.90	0.09	0.49
211	Primo Impalcato	33, 35	0	39.32	0.93	4.93	-7.72	0.30	0.20
			66	39.32	0.93	-0.17	-7.72	0.17	0.20
			132	39.32	0.93	-5.27	-7.72	0.04	0.20
212	Primo Impalcato	34, 36	0	-37.04	0.91	-53.49	77.48	0.59	0.59
			69	-37.04	0.91	-0.03	77.48	0.18	0.59
			138	-37.04	0.91	53.44	77.48	-0.23	0.59
213	Primo Impalcato	35, 37	0	40.79	0.92	37.36	-56.13	0.13	0.43
			66	40.79	0.92	0.31	-56.13	-0.15	0.43

			132	40.79	0.92	-36.73	-56.13	-0.43	0.43
214	Primo Impalcato	36, 38	0	0.97	0.90	-53.44	77.54	0.27	0.68
			69	0.97	0.90	0.06	77.54	-0.20	0.68
			138	0.97	0.90	53.56	77.54	-0.67	0.68
215	Primo Impalcato	37, 39	0	46.75	0.95	4.55	-9.80	-0.37	-0.27
			66	46.75	0.95	-1.92	-9.80	-0.19	-0.27
			132	46.75	0.95	-8.39	-9.80	-0.01	-0.27
216	Primo Impalcato	38, 40	0	38.71	0.93	-53.01	73.82	-0.18	0.63
			69	38.71	0.93	-2.45	73.82	-0.61	0.63
			137	38.71	0.93	48.12	73.82	-1.05	0.63
217	Primo Impalcato	39, 41	0	50.98	0.96	33.41	-41.61	0.10	-0.19
			66	50.98	0.96	5.94	-41.61	0.22	-0.19
			132	50.98	0.96	-21.52	-41.61	0.34	-0.19
218	Primo Impalcato	40, 42	0	76.12	0.97	-58.76	90.85	-0.62	0.30
			69	76.12	0.97	3.93	90.85	-0.82	0.30
			138	76.12	0.97	66.61	90.85	-1.03	0.30
219	Primo Impalcato	41, 44	0	16.03	0.91	23.41	-44.78	0.63	0.80
			66	16.03	0.91	-6.14	-44.78	0.10	0.80
			132	16.03	0.91	-35.70	-44.78	-0.43	0.80
220	Primo Impalcato	42, 43	0	113.46	1.26	-38.56	220.85	-0.68	-3.74
			23	113.46	1.26	12.23	220.85	0.17	-3.74
			46	113.46	1.26	63.03	220.85	1.03	-3.74
221	Primo Impalcato	43, 45	0	90.07	0.96	-41.62	53.62	1.16	-0.61
			66	90.07	0.96	-6.23	53.62	1.56	-0.61
			132	90.07	0.96	29.16	53.62	1.96	-0.61
222	Primo Impalcato	44, 46	0	19.59	0.92	6.47	-7.15	-0.33	-1.10
			66	19.59	0.92	1.75	-7.15	0.39	-1.10
			132	19.59	0.92	-2.97	-7.15	1.11	-1.10
223	Primo Impalcato	45, 47	0	67.17	0.80	-77.24	119.90	2.16	-0.68
			66	67.17	0.80	1.89	119.90	2.61	-0.68
			132	67.17	0.80	81.02	119.90	3.06	-0.68
224	Primo Impalcato	46, 48	0	23.28	0.80	40.25	-61.04	1.28	-1.44
			66	23.28	0.80	-0.04	-61.04	2.23	-1.44
			132	23.28	0.80	-40.32	-61.04	3.18	-1.44
225	Primo Impalcato	47, 49	0	46.49	0.52	-24.96	37.17	3.28	-1.00
			66	46.49	0.52	-0.43	37.17	3.94	-1.00
			132	46.49	0.52	24.10	37.17	4.60	-1.00
226	Primo Impalcato	48, 50	0	25.11	0.52	2.79	-6.06	2.98	-1.11
			66	25.11	0.52	-1.21	-6.06	3.71	-1.11
			132	25.11	0.52	-5.21	-6.06	4.45	-1.11
227	Primo Impalcato	49, 51	0	21.88	0.06	-82.07	124.96	4.90	-0.23
			66	21.88	0.06	0.40	124.96	5.05	-0.23
			132	21.88	0.06	82.87	124.96	5.20	-0.23
228	Primo Impalcato	50, 52	0	31.34	0.07	36.75	-48.45	4.80	-1.11
			66	31.34	0.07	4.77	-48.45	5.53	-1.11
			132	31.34	0.07	-27.21	-48.45	6.26	-1.11
229	Primo Impalcato	51, 53	0	1.95	-0.46	-23.23	38.60	5.49	0.73
			66	1.95	-0.46	2.24	38.60	5.01	0.73
			132	1.95	-0.46	27.71	38.60	4.53	0.73
230	Primo Impalcato	52, 54	0	-3.37	-0.49	17.27	-26.06	5.72	-0.53
			66	-3.37	-0.49	0.07	-26.06	6.07	-0.53
			132	-3.37	-0.49	-17.14	-26.06	6.42	-0.53
231	Primo Impalcato	53, 55	0	-21.44	-1.00	-77.77	86.81	4.83	-1.52
			66	-21.44	-1.00	-20.48	86.81	5.83	-1.52
			132	-21.44	-1.00	36.82	86.81	6.84	-1.52

232	Primo Impalcato	54, 56	0	-36.89	-1.06	27.18	-31.93	6.68	0.29
			66	-36.89	-1.06	6.11	-31.93	6.49	0.29
			132	-36.89	-1.06	-14.97	-31.93	6.30	0.29
233	Primo Impalcato	55, 57	0	-52.52	-2.09	-73.82	195.15	7.41	-7.34
			80	-52.52	-2.09	81.33	195.15	13.25	-7.34
			159	-52.52	-2.09	236.48	195.15	19.08	-7.34
234	Primo Impalcato	56, 70	0	-27.26	-1.97	35.07	-75.99	5.68	5.53
			80	-27.26	-1.97	-25.35	-75.99	1.28	5.53
			159	-27.26	-1.97	-85.76	-75.99	-3.12	5.53
235	Primo Impalcato	57, 58	0	15.71	-4.44	-158.40	69.52	21.98	29.53
			83	15.71	-4.44	-100.61	69.52	-2.56	29.53
			166	15.71	-4.44	-42.82	69.52	-27.10	29.53
236	Primo Impalcato	58, 59	0	-2.08	-0.36	-57.02	61.75	-25.18	-8.71
			69	-2.08	-0.36	-14.41	61.75	-19.17	-8.71
			138	-2.08	-0.36	28.20	61.75	-13.16	-8.71
237	Primo Impalcato	59, 60	0	-2.89	0.02	11.63	-23.83	-13.10	-6.70
			69	-2.89	0.02	-4.81	-23.83	-8.48	-6.70
			138	-2.89	0.02	-21.25	-23.83	-3.86	-6.70
238	Primo Impalcato	60, 61	0	-3.66	0.42	-38.39	104.43	-3.94	-1.37
			69	-3.66	0.42	33.66	104.43	-2.99	-1.37
			138	-3.66	0.42	105.72	104.43	-2.04	-1.37
239	Primo Impalcato	61, 62	0	-12.24	0.84	92.00	-134.03	-2.45	0.43
			69	-12.24	0.84	-0.48	-134.03	-2.75	0.43
			138	-12.24	0.84	-92.95	-134.03	-3.05	0.43
240	Primo Impalcato	62, 63	0	-11.66	1.21	-106.75	102.79	-2.46	-0.18
			69	-11.66	1.21	-35.83	102.79	-2.34	-0.18
			138	-11.66	1.21	35.10	102.79	-2.21	-0.18
241	Primo Impalcato	63, 64	0	-12.38	1.42	17.59	-25.71	-1.92	-0.69
			69	-12.38	1.42	-0.14	-25.71	-1.44	-0.69
			138	-12.38	1.42	-17.88	-25.71	-0.97	-0.69
242	Primo Impalcato	64, 65	0	-13.10	1.55	-35.42	103.26	-0.64	-0.41
			69	-13.10	1.55	35.83	103.26	-0.35	-0.41
			138	-13.10	1.55	107.08	103.26	-0.07	-0.41
243	Primo Impalcato	65, 66	0	-12.99	1.52	93.24	-134.68	0.10	-0.16
			69	-12.99	1.52	0.31	-134.68	0.21	-0.16
			138	-12.99	1.52	-92.63	-134.68	0.32	-0.16
244	Primo Impalcato	66, 67	0	-21.79	1.38	-106.43	105.09	0.63	-1.02
			69	-21.79	1.38	-33.92	105.09	1.33	-1.02
			138	-21.79	1.38	38.59	105.09	2.03	-1.02
245	Primo Impalcato	67, 68	0	-22.56	1.07	21.32	-23.61	2.22	-3.64
			69	-22.56	1.07	5.03	-23.61	4.73	-3.64
			138	-22.56	1.07	-11.27	-23.61	7.24	-3.64
246	Primo Impalcato	68, 69	0	-23.37	0.64	-27.94	62.74	7.39	-5.52
			69	-23.37	0.64	15.35	62.74	11.20	-5.52
			138	-23.37	0.64	58.65	62.74	15.01	-5.52
247	Primo Impalcato	69, 70	0	-30.12	-1.80	44.26	61.22	15.55	7.53
			83	-30.12	-1.80	95.14	61.22	9.29	7.53
			166	-30.12	-1.80	146.03	61.22	3.03	7.53
248	Primo Impalcato	1	0	85.00	4.18	-4.53	-1.62	-37.85	-42.34
			188	85.00	4.18	-7.58	-1.62	41.75	-42.34
			376	85.00	4.18	-10.62	-1.62	121.35	-42.34
249	Primo Impalcato	2	0	-196.61	0.53	-61.13	5.62	-7.49	-3.94
			188	-196.61	0.53	-50.56	5.62	-0.07	-3.94
			376	-196.61	0.53	-39.99	5.62	7.34	-3.94
250	Primo	3	0	-24.12	0.08	-29.04	-12.30	-8.58	-4.52

	Impalcato								
			188	-24.12	0.08	-52.16	-12.30	-0.09	-4.52
			376	-24.12	0.08	-75.29	-12.30	8.41	-4.52
251	Primo Impalcato	4	0	-23.97	-0.10	-26.88	-13.07	-8.19	-4.39
			188	-23.97	-0.10	-51.45	-13.07	0.05	-4.39
			376	-23.97	-0.10	-76.02	-13.07	8.30	-4.39
252	Primo Impalcato	5	0	27.46	-0.15	-29.52	-10.18	-8.96	-4.67
			188	27.46	-0.15	-48.66	-10.18	-0.18	-4.67
			376	27.46	-0.15	-67.80	-10.18	8.61	-4.67
253	Primo Impalcato	6	0	191.35	-0.18	-28.34	-8.01	-6.89	-3.76
			188	191.35	-0.18	-43.41	-8.01	0.17	-3.76
			376	191.35	-0.18	-58.47	-8.01	7.24	-3.76
254	Primo Impalcato	7	0	-204.27	-0.23	-24.85	-5.38	-6.91	-3.77
			188	-204.27	-0.23	-34.98	-5.38	0.19	-3.77
			376	-204.27	-0.23	-45.10	-5.38	7.28	-3.77
255	Primo Impalcato	8	0	12.51	-0.27	-17.53	-4.23	-9.67	-4.96
			188	12.51	-0.27	-25.48	-4.23	-0.36	-4.96
			376	12.51	-0.27	-33.43	-4.23	8.96	-4.96
256	Primo Impalcato	9	0	229.33	-0.29	-9.65	-2.76	-6.94	-3.79
			188	229.33	-0.29	-14.84	-2.76	0.19	-3.79
			376	229.33	-0.29	-20.04	-2.76	7.32	-3.79
257	Primo Impalcato	10	0	-176.32	-0.29	-4.92	0.97	-6.93	-3.79
			188	-176.32	-0.29	-3.10	0.97	0.19	-3.79
			376	-176.32	-0.29	-1.27	0.97	7.31	-3.79
258	Primo Impalcato	11	0	-41.05	-0.27	-0.45	3.97	-8.97	-4.70
			188	-41.05	-0.27	7.02	3.97	-0.14	-4.70
			376	-41.05	-0.27	14.49	3.97	8.69	-4.70
259	Primo Impalcato	12	0	34.74	-0.16	3.82	5.74	-8.70	-4.58
			188	34.74	-0.16	14.61	5.74	-0.09	-4.58
			376	34.74	-0.16	25.40	5.74	8.51	-4.58
260	Primo Impalcato	13	0	225.59	0.10	18.13	0.64	-7.48	-3.92
			188	225.59	0.10	19.34	0.64	-0.11	-3.92
			376	225.59	0.10	20.55	0.64	7.27	-3.92
261	Primo Impalcato	14	0	-239.50	2.38	-6.65	5.03	-42.45	-44.19
			188	-239.50	2.38	2.82	5.03	40.62	-44.19
			376	-239.50	2.38	12.28	5.03	123.70	-44.19
262	Primo Impalcato	15	0	146.35	0.79	12.58	-6.48	-6.73	-45.22
			188	146.35	0.79	0.40	-6.48	78.28	-45.22
			376	146.35	0.79	-11.78	-6.48	163.29	-45.22
263	Primo Impalcato	16	0	-114.75	0.89	-8.32	4.28	4.75	-38.15
			188	-114.75	0.89	-0.28	4.28	76.48	-38.15
			376	-114.75	0.89	7.77	4.28	148.21	-38.15
264	Primo Impalcato	17	0	-22.42	0.44	9.77	-5.42	-0.97	-52.90
			188	-22.42	0.44	-0.41	-5.42	98.48	-52.90
			376	-22.42	0.44	-10.59	-5.42	197.94	-52.90
265	Primo Impalcato	18	0	-13.75	0.53	-6.40	3.50	2.28	-50.94
			188	-13.75	0.53	0.18	3.50	98.04	-50.94
			376	-13.75	0.53	6.75	3.50	193.80	-50.94
266	Primo Impalcato	19	0	85.23	0.13	10.12	-5.55	2.63	-55.95
			188	85.23	0.13	-0.32	-5.55	107.83	-55.95
			376	85.23	0.13	-10.77	-5.55	213.02	-55.95
267	Primo Impalcato	20	0	-61.11	0.14	-6.48	3.50	2.21	-56.26
			188	-61.11	0.14	0.11	3.50	107.97	-56.26
			376	-61.11	0.14	6.70	3.50	213.74	-56.26
268	Primo Impalcato	21	0	4.92	-0.19	10.22	-5.60	3.00	-56.00

			188	4.92	-0.19	-0.31	-5.60	108.27	-56.00
			376	4.92	-0.19	-10.83	-5.60	213.55	-56.00
269	Primo Impalcato	22	0	-6.92	-0.19	-6.44	3.48	2.59	-56.31
			188	-6.92	-0.19	0.11	3.48	108.46	-56.31
			376	-6.92	-0.19	6.66	3.48	214.32	-56.31
270	Primo Impalcato	23	0	81.68	-0.45	10.31	-5.64	2.64	-51.65
			188	81.68	-0.45	-0.30	-5.64	99.73	-51.65
			376	81.68	-0.45	-10.92	-5.64	196.83	-51.65
271	Primo Impalcato	24	0	-43.24	-0.46	-6.46	3.50	2.51	-51.97
			188	-43.24	-0.46	0.12	3.50	100.21	-51.97
			376	-43.24	-0.46	6.69	3.50	197.90	-51.97
272	Primo Impalcato	25	0	-4.62	-0.58	10.16	-5.56	0.68	-46.18
			188	-4.62	-0.58	-0.29	-5.56	87.50	-46.18
			376	-4.62	-0.58	-10.74	-5.56	174.33	-46.18
273	Primo Impalcato	26	0	3.95	-0.62	-6.45	3.49	2.29	-45.24
			188	3.95	-0.62	0.11	3.49	87.33	-45.24
			376	3.95	-0.62	6.67	3.49	172.38	-45.24
274	Primo Impalcato	27	0	-33.40	-0.70	-6.48	3.51	2.00	-35.43
			188	-33.40	-0.70	0.11	3.51	68.61	-35.43
			376	-33.40	-0.70	6.71	3.51	135.22	-35.43
275	Primo Impalcato	28	0	77.38	-0.65	9.63	-5.35	0.15	-34.14
			188	77.38	-0.65	-0.42	-5.35	64.34	-34.14
			376	77.38	-0.65	-10.48	-5.35	128.53	-34.14
276	Primo Impalcato	29	0	14.01	-0.70	-6.53	3.54	1.37	-26.01
			188	14.01	-0.70	0.12	3.54	50.27	-26.01
			376	14.01	-0.70	6.76	3.54	99.18	-26.01
277	Primo Impalcato	30	0	20.43	-0.68	11.37	-6.18	-1.55	-24.74
			188	20.43	-0.68	-0.24	-6.18	44.96	-24.74
			376	20.43	-0.68	-11.85	-6.18	91.48	-24.74
278	Primo Impalcato	31	0	-28.49	-0.67	-6.54	3.55	1.54	-16.35
			188	-28.49	-0.67	0.12	3.55	32.28	-16.35
			376	-28.49	-0.67	6.79	3.55	63.03	-16.35
279	Primo Impalcato	32	0	10.01	-0.66	11.09	-6.07	-2.32	-15.71
			188	10.01	-0.66	-0.33	-6.07	27.22	-15.71
			376	10.01	-0.66	-11.75	-6.07	56.76	-15.71
280	Primo Impalcato	33	0	17.98	-0.64	-6.60	3.57	1.21	-7.71
			188	17.98	-0.64	0.12	3.57	15.70	-7.71
			376	17.98	-0.64	6.83	3.57	30.20	-7.71
281	Primo Impalcato	34	0	4.82	-0.64	11.17	-6.10	-2.40	-6.69
			188	4.82	-0.64	-0.31	-6.10	10.17	-6.69
			376	4.82	-0.64	-11.79	-6.10	22.74	-6.69
282	Primo Impalcato	35	0	-24.43	-0.63	-6.61	3.58	1.24	1.12
			188	-24.43	-0.63	0.12	3.58	-0.87	1.12
			376	-24.43	-0.63	6.85	3.58	-2.97	1.12
283	Primo Impalcato	36	0	-8.05	-0.62	11.22	-6.13	-2.77	1.91
			188	-8.05	-0.62	-0.31	-6.13	-6.35	1.91
			376	-8.05	-0.62	-11.83	-6.13	-9.94	1.91
284	Primo Impalcato	37	0	27.14	-0.64	-6.70	3.62	1.04	9.56
			188	27.14	-0.64	0.10	3.62	-16.94	9.56
			376	27.14	-0.64	6.90	3.62	-34.91	9.56
285	Primo Impalcato	38	0	-15.64	-0.64	11.24	-6.15	-3.09	10.46
			188	-15.64	-0.64	-0.33	-6.15	-22.75	10.46
			376	-15.64	-0.64	-11.89	-6.15	-42.41	10.46
286	Primo Impalcato	39	0	-21.14	-0.65	-6.49	3.54	0.63	18.50
			188	-21.14	-0.65	0.18	3.54	-34.16	18.50

			376	-21.14	-0.65	6.84	3.54	-68.95	18.50
287	Primo Impalcato	40	0	-25.59	-0.68	11.58	-6.29	-3.05	19.36
			188	-25.59	-0.68	-0.25	-6.29	-39.45	19.36
			376	-25.59	-0.68	-12.08	-6.29	-75.85	19.36
288	Primo Impalcato	41	0	6.62	-0.64	-7.53	4.02	-0.93	26.62
			188	6.62	-0.64	0.02	4.02	-50.98	26.62
			376	6.62	-0.64	7.58	4.02	-101.03	26.62
289	Primo Impalcato	42	0	-75.94	-0.73	10.75	-5.89	-0.08	30.15
			188	-75.94	-0.73	-0.33	-5.89	-56.76	30.15
			376	-75.94	-0.73	-11.40	-5.89	-113.43	30.15
290	Primo Impalcato	43	0	-19.71	-0.73	9.92	-5.49	-4.17	32.41
			188	-19.71	-0.73	-0.40	-5.49	-65.10	32.41
			376	-19.71	-0.73	-10.73	-5.49	-126.03	32.41
291	Primo Impalcato	44	0	42.53	-0.63	-6.52	3.56	-0.07	35.74
			188	42.53	-0.63	0.17	3.56	-67.25	35.74
			376	42.53	-0.63	6.87	3.56	-134.43	35.74
292	Primo Impalcato	45	0	19.38	-0.63	10.78	-5.85	-1.18	43.35
			188	19.38	-0.63	-0.22	-5.85	-82.67	43.35
			376	19.38	-0.63	-11.22	-5.85	-164.17	43.35
293	Primo Impalcato	46	0	-17.81	-0.61	-6.79	3.67	-1.46	43.54
			188	-17.81	-0.61	0.11	3.67	-83.31	43.54
			376	-17.81	-0.61	7.00	3.67	-165.17	43.54
294	Primo Impalcato	47	0	-78.89	-0.46	10.48	-5.74	-1.73	50.56
			188	-78.89	-0.46	-0.31	-5.74	-96.77	50.56
			376	-78.89	-0.46	-11.10	-5.74	-191.82	50.56
295	Primo Impalcato	48	0	48.32	-0.47	-6.78	3.66	-2.55	50.43
			188	48.32	-0.47	0.10	3.66	-97.36	50.43
			376	48.32	-0.47	6.98	3.66	-192.17	50.43
296	Primo Impalcato	49	0	-1.78	-0.21	10.49	-5.74	-2.60	55.12
			188	-1.78	-0.21	-0.30	-5.74	-106.22	55.12
			376	-1.78	-0.21	-11.10	-5.74	-209.84	55.12
297	Primo Impalcato	50	0	-0.09	-0.23	-6.66	3.62	-2.35	55.53
			188	-0.09	-0.23	0.15	3.62	-106.75	55.53
			376	-0.09	-0.23	6.96	3.62	-211.15	55.53
298	Primo Impalcato	51	0	-86.78	0.11	10.41	-5.71	-2.67	55.32
			188	-86.78	0.11	-0.32	-5.71	-106.68	55.32
			376	-86.78	0.11	-11.06	-5.71	-210.69	55.32
299	Primo Impalcato	52	0	38.65	0.12	-7.56	4.06	-2.05	56.00
			188	38.65	0.12	0.07	4.06	-107.32	56.00
			376	38.65	0.12	7.71	4.06	-212.59	56.00
300	Primo Impalcato	53	0	21.97	0.43	10.09	-5.58	0.91	52.64
			188	21.97	0.43	-0.41	-5.58	-98.06	52.64
			376	21.97	0.43	-10.90	-5.58	-197.03	52.64
301	Primo Impalcato	54	0	39.70	0.51	-7.65	4.13	-1.66	50.73
			188	39.70	0.51	0.11	4.13	-97.04	50.73
			376	39.70	0.51	7.87	4.13	-192.41	50.73
302	Primo Impalcato	55	0	-151.62	0.80	12.90	-6.65	6.54	45.02
			188	-151.62	0.80	0.40	-6.65	-78.10	45.02
			376	-151.62	0.80	-12.09	-6.65	-162.73	45.02
303	Primo Impalcato	56	0	116.72	0.92	-8.36	4.36	-5.42	37.42
			188	116.72	0.92	-0.16	4.36	-75.78	37.42
			376	116.72	0.92	8.03	4.36	-146.13	37.42
304	Primo Impalcato	57	0	-85.58	4.27	-3.89	-1.97	37.55	41.65
			188	-85.58	4.27	-7.60	-1.97	-40.76	41.65
			376	-85.58	4.27	-11.31	-1.97	-119.06	41.65

305	Primo Impalcato	58	0	184.50	0.55	-61.45	5.15	7.33	3.87
			188	184.50	0.55	-51.76	5.15	0.06	3.87
			376	184.50	0.55	-42.08	5.15	-7.21	3.87
306	Primo Impalcato	59	0	32.08	0.11	-30.87	-12.70	8.42	4.44
			188	32.08	0.11	-54.74	-12.70	0.07	4.44
			376	32.08	0.11	-78.62	-12.70	-8.27	4.44
307	Primo Impalcato	60	0	-29.91	-0.08	-29.34	-13.72	8.67	4.54
			188	-29.91	-0.08	-55.13	-13.72	0.13	4.54
			376	-29.91	-0.08	-80.92	-13.72	-8.41	4.54
308	Primo Impalcato	61	0	-161.85	-0.15	-31.69	-10.88	6.72	3.67
			188	-161.85	-0.15	-52.15	-10.88	-0.18	3.67
			376	-161.85	-0.15	-72.61	-10.88	-7.07	3.67
309	Primo Impalcato	62	0	216.72	-0.21	-30.97	-7.53	6.75	3.68
			188	216.72	-0.21	-45.13	-7.53	-0.17	3.68
			376	216.72	-0.21	-59.30	-7.53	-7.09	3.68
310	Primo Impalcato	63	0	66.61	-0.26	-25.00	-6.02	8.82	4.60
			188	66.61	-0.26	-36.32	-6.02	0.16	4.60
			376	66.61	-0.26	-47.65	-6.02	-8.49	4.60
311	Primo Impalcato	64	0	-65.33	-0.30	-17.63	-4.60	8.83	4.61
			188	-65.33	-0.30	-26.27	-4.60	0.17	4.61
			376	-65.33	-0.30	-34.91	-4.60	-8.50	4.61
312	Primo Impalcato	65	0	-215.89	-0.30	-9.72	-2.75	6.78	3.70
			188	-215.89	-0.30	-14.89	-2.75	-0.17	3.70
			376	-215.89	-0.30	-20.06	-2.75	-7.13	3.70
313	Primo Impalcato	66	0	165.00	-0.30	-4.85	1.09	6.77	3.70
			188	165.00	-0.30	-2.79	1.09	-0.18	3.70
			376	165.00	-0.30	-0.73	1.09	-7.13	3.70
314	Primo Impalcato	67	0	31.50	-0.27	-0.21	4.07	8.74	4.58
			188	31.50	-0.27	7.43	4.07	0.13	4.58
			376	31.50	-0.27	15.08	4.07	-8.47	4.58
315	Primo Impalcato	68	0	-38.28	-0.16	3.93	5.88	8.47	4.46
			188	-38.28	-0.16	14.98	5.88	0.08	4.46
			376	-38.28	-0.16	26.02	5.88	-8.30	4.46
316	Primo Impalcato	69	0	-218.33	0.09	17.48	1.10	7.28	3.82
			188	-218.33	0.09	19.54	1.10	0.10	3.82
			376	-218.33	0.09	21.60	1.10	-7.08	3.82
317	Primo Impalcato	70	0	238.85	2.40	-9.85	6.44	41.58	43.07
			188	238.85	2.40	2.25	6.44	-39.39	43.07
			376	238.85	2.40	14.35	6.44	-120.36	43.07
318	Fondazione	1, 71	0	-172.53	0.00	0.00	0.00	0.99	0.01
			102	-172.53	0.00	0.00	0.00	0.98	0.01
			204	-172.53	0.00	0.00	0.00	0.96	0.01
319	Fondazione	1, 92	0	274.79	0.02	0.00	0.00	0.35	-0.59
			103	274.79	0.02	0.00	0.00	0.95	-0.59
			206	274.79	0.02	0.00	0.00	1.56	-0.59
320	Primo Impalcato	92, 2	0	-315.50	0.08	0.00	0.00	-0.21	-0.65
			103	-315.50	0.08	0.00	0.00	0.47	-0.65
			206	-315.50	0.08	0.00	0.00	1.14	-0.65
321	Fondazione	6, 89	0	320.11	-0.05	0.00	0.00	1.44	0.40
			100	320.11	-0.05	0.00	0.00	1.04	0.40
			200	320.11	-0.05	0.00	0.00	0.64	0.40
322	Primo Impalcato	89, 7	0	-323.38	0.02	0.00	0.00	1.19	0.05
			100	-323.38	0.02	0.00	0.00	1.14	0.05
			200	-323.38	0.02	0.00	0.00	1.08	0.05
323	Fondazione	9, 90	0	331.49	-0.03	0.00	0.00	0.49	0.34

	ne								
			100	331.49	-0.03	0.00	0.00	0.15	0.34
			200	331.49	-0.03	0.00	0.00	-0.18	0.34
324	Primo Impalcato	90, 10	0	-317.15	-0.02	0.00	0.00	0.61	0.29
			100	-317.15	-0.02	0.00	0.00	0.31	0.29
			200	-317.15	-0.02	0.00	0.00	0.02	0.29
325	Fondazio ne	13, 91	0	305.52	0.03	0.00	0.00	-0.72	-0.39
			103	305.52	0.03	0.00	0.00	-0.32	-0.39
			206	305.52	0.03	0.00	0.00	0.08	-0.39
326	Primo Impalcato	88, 14	0	117.90	0.00	0.00	0.00	-0.94	-0.08
			102	117.90	0.00	0.00	0.00	-0.85	-0.08
			204	117.90	0.00	0.00	0.00	-0.77	-0.08
327	Primo Impalcato	91, 14	0	-274.03	0.00	0.00	0.00	-0.48	0.05
			103	-274.03	0.00	0.00	0.00	-0.53	0.05
			206	-274.03	0.00	0.00	0.00	-0.58	0.05
328	Primo Impalcato	71, 15	0	205.94	0.07	0.00	0.00	-0.20	-0.89
			102	205.94	0.07	0.00	0.00	0.71	-0.89
			204	205.94	0.07	0.00	0.00	1.61	-0.89
329	Fondazio ne	16, 88	0	-161.75	0.06	0.00	0.00	-1.38	-0.69
			102	-161.75	0.06	0.00	0.00	-0.67	-0.69
			204	-161.75	0.06	0.00	0.00	0.03	-0.69
330	Fondazio ne	17, 72	0	-171.23	-0.04	0.00	0.00	1.88	0.42
			100	-171.23	-0.04	0.00	0.00	1.47	0.42
			199	-171.23	-0.04	0.00	0.00	1.05	0.42
331	Primo Impalcato	87, 18	0	104.03	-0.04	0.00	0.00	-1.07	0.40
			100	104.03	-0.04	0.00	0.00	-1.47	0.40
			199	104.03	-0.04	0.00	0.00	-1.86	0.40
332	Primo Impalcato	72, 19	0	181.50	0.06	0.00	0.00	0.79	-0.62
			100	181.50	0.06	0.00	0.00	1.41	-0.62
			199	181.50	0.06	0.00	0.00	2.02	-0.62
333	Fondazio ne	20, 87	0	-115.67	0.06	0.00	0.00	-2.04	-0.64
			100	-115.67	0.06	0.00	0.00	-1.40	-0.64
			199	-115.67	0.06	0.00	0.00	-0.76	-0.64
334	Fondazio ne	21, 73	0	-173.76	-0.06	0.00	0.00	2.00	0.61
			100	-173.76	-0.06	0.00	0.00	1.39	0.61
			199	-173.76	-0.06	0.00	0.00	0.78	0.61
335	Primo Impalcato	86, 22	0	105.34	-0.06	0.00	0.00	-0.78	0.61
			100	105.34	-0.06	0.00	0.00	-1.40	0.61
			199	105.34	-0.06	0.00	0.00	-2.01	0.61
336	Primo Impalcato	73, 23	0	187.01	0.04	0.00	0.00	1.08	-0.40
			100	187.01	0.04	0.00	0.00	1.48	-0.40
			199	187.01	0.04	0.00	0.00	1.88	-0.40
337	Fondazio ne	24, 86	0	-112.95	0.04	0.00	0.00	-1.90	-0.41
			100	-112.95	0.04	0.00	0.00	-1.49	-0.41
			199	-112.95	0.04	0.00	0.00	-1.09	-0.41
338	Fondazio ne	25, 74	0	-208.05	-0.06	0.00	0.00	1.50	0.58
			103	-208.05	-0.06	0.00	0.00	0.90	0.58
			206	-208.05	-0.06	0.00	0.00	0.30	0.58
339	Primo Impalcato	85, 26	0	107.24	-0.06	0.00	0.00	-0.39	0.60
			100	107.24	-0.06	0.00	0.00	-0.99	0.60
			199	107.24	-0.06	0.00	0.00	-1.58	0.60
340	Fondazio ne	27, 85	0	-111.44	0.01	0.00	0.00	-1.29	-0.13
			100	-111.44	0.01	0.00	0.00	-1.16	-0.13
			199	-111.44	0.01	0.00	0.00	-1.02	-0.13
341	Primo Impalcato	74, 28	0	215.86	0.02	0.00	0.00	0.98	-0.08

			103	215.86	0.02	0.00	0.00	1.06	-0.08
			206	215.86	0.02	0.00	0.00	1.15	-0.08
342	Primo Impalcato	84, 29	0	109.91	-0.04	0.00	0.00	-0.06	0.41
			100	109.91	-0.04	0.00	0.00	-0.47	0.41
			199	109.91	-0.04	0.00	0.00	-0.87	0.41
343	Fondazio ne	31, 84	0	-111.58	0.00	0.00	0.00	-0.61	0.04
			100	-111.58	0.00	0.00	0.00	-0.66	0.04
			199	-111.58	0.00	0.00	0.00	-0.70	0.04
344	Primo Impalcato	83, 33	0	111.57	-0.02	0.00	0.00	0.22	0.23
			100	111.57	-0.02	0.00	0.00	-0.01	0.23
			199	111.57	-0.02	0.00	0.00	-0.24	0.23
345	Fondazio ne	35, 83	0	-111.85	-0.02	0.00	0.00	-0.01	0.18
			100	-111.85	-0.02	0.00	0.00	-0.18	0.18
			199	-111.85	-0.02	0.00	0.00	-0.36	0.18
346	Primo Impalcato	82, 37	0	113.01	-0.01	0.00	0.00	0.53	0.09
			100	113.01	-0.01	0.00	0.00	0.44	0.09
			199	113.01	-0.01	0.00	0.00	0.35	0.09
347	Fondazio ne	39, 82	0	-111.13	-0.03	0.00	0.00	0.60	0.33
			100	-111.13	-0.03	0.00	0.00	0.27	0.33
			199	-111.13	-0.03	0.00	0.00	-0.06	0.33
348	Primo Impalcato	78, 43	0	-184.29	0.01	0.00	0.00	0.99	-0.11
			100	-184.29	0.01	0.00	0.00	1.10	-0.11
			199	-184.29	0.01	0.00	0.00	1.22	-0.11
349	Primo Impalcato	81, 44	0	115.09	0.01	0.00	0.00	0.97	-0.16
			100	115.09	0.01	0.00	0.00	1.13	-0.16
			199	115.09	0.01	0.00	0.00	1.29	-0.16
350	Fondazio ne	45, 78	0	185.90	-0.06	0.00	0.00	1.50	0.58
			100	185.90	-0.06	0.00	0.00	0.92	0.58
			199	185.90	-0.06	0.00	0.00	0.35	0.58
351	Fondazio ne	46, 81	0	-110.69	-0.06	0.00	0.00	1.49	0.55
			100	-110.69	-0.06	0.00	0.00	0.95	0.55
			199	-110.69	-0.06	0.00	0.00	0.40	0.55
352	Primo Impalcato	77, 47	0	-190.00	0.04	0.00	0.00	1.07	-0.38
			100	-190.00	0.04	0.00	0.00	1.45	-0.38
			199	-190.00	0.04	0.00	0.00	1.83	-0.38
353	Primo Impalcato	80, 48	0	117.29	0.04	0.00	0.00	1.08	-0.38
			100	117.29	0.04	0.00	0.00	1.46	-0.38
			199	117.29	0.04	0.00	0.00	1.83	-0.38
354	Fondazio ne	49, 77	0	177.89	-0.06	0.00	0.00	1.97	0.61
			100	177.89	-0.06	0.00	0.00	1.36	0.61
			199	177.89	-0.06	0.00	0.00	0.75	0.61
355	Fondazio ne	50, 80	0	-109.01	-0.06	0.00	0.00	1.98	0.61
			100	-109.01	-0.06	0.00	0.00	1.36	0.61
			199	-109.01	-0.06	0.00	0.00	0.75	0.61
356	Primo Impalcato	76, 51	0	-186.50	0.06	0.00	0.00	0.79	-0.61
			100	-186.50	0.06	0.00	0.00	1.40	-0.61
			199	-186.50	0.06	0.00	0.00	2.00	-0.61
357	Fondazio ne	53, 76	0	176.04	-0.04	0.00	0.00	1.88	0.42
			100	176.04	-0.04	0.00	0.00	1.46	0.42
			199	176.04	-0.04	0.00	0.00	1.04	0.42
358	Primo Impalcato	75, 55	0	-211.74	0.07	0.00	0.00	-0.21	-0.89
			102	-211.74	0.07	0.00	0.00	0.70	-0.89
			204	-211.74	0.07	0.00	0.00	1.61	-0.89
359	Fondazio ne	56, 79	0	168.98	0.06	0.00	0.00	-1.35	-0.68
			102	168.98	0.06	0.00	0.00	-0.65	-0.68

			204	168.98	0.06	0.00	0.00	0.05	-0.68
360	Fondazio ne	57, 75	0	177.53	0.00	0.00	0.00	0.99	0.01
			102	177.53	0.00	0.00	0.00	0.97	0.01
			204	177.53	0.00	0.00	0.00	0.96	0.01
361	Fondazio ne	57, 93	0	-271.14	0.02	0.00	0.00	0.36	-0.60
			103	-271.14	0.02	0.00	0.00	0.98	-0.60
			206	-271.14	0.02	0.00	0.00	1.60	-0.60
362	Primo Impalcato	93, 58	0	308.76	0.08	0.00	0.00	-0.21	-0.68
			103	308.76	0.08	0.00	0.00	0.49	-0.68
			206	308.76	0.08	0.00	0.00	1.18	-0.68
363	Fondazio ne	61, 95	0	-307.34	-0.06	0.00	0.00	1.78	0.44
			100	-307.34	-0.06	0.00	0.00	1.33	0.44
			200	-307.34	-0.06	0.00	0.00	0.89	0.44
364	Primo Impalcato	95, 62	0	321.66	0.03	0.00	0.00	1.39	-0.02
			100	321.66	0.03	0.00	0.00	1.41	-0.02
			200	321.66	0.03	0.00	0.00	1.43	-0.02
365	Primo Impalcato	96, 65	0	-323.40	-0.03	0.00	0.00	0.20	0.34
			100	-323.40	-0.03	0.00	0.00	-0.15	0.34
			200	-323.40	-0.03	0.00	0.00	-0.49	0.34
366	Fondazio ne	66, 96	0	309.63	-0.02	0.00	0.00	0.00	0.31
			100	309.63	-0.02	0.00	0.00	-0.31	0.31
			200	309.63	-0.02	0.00	0.00	-0.62	0.31
367	Fondazio ne	69, 94	0	-296.49	0.03	0.00	0.00	-0.76	-0.40
			103	-296.49	0.03	0.00	0.00	-0.35	-0.40
			206	-296.49	0.03	0.00	0.00	0.07	-0.40
368	Primo Impalcato	79, 70	0	-125.26	0.00	0.00	0.00	-0.94	-0.09
			102	-125.26	0.00	0.00	0.00	-0.84	-0.09
			204	-125.26	0.00	0.00	0.00	-0.75	-0.09
369	Primo Impalcato	94, 70	0	266.76	0.00	0.00	0.00	-0.45	0.09
			103	266.76	0.00	0.00	0.00	-0.54	0.09
			206	266.76	0.00	0.00	0.00	-0.63	0.09
370	Primo Impalcato	1, 71	0	205.94	0.12	0.00	0.00	-1.63	-0.74
			102	205.94	0.12	0.00	0.00	-0.87	-0.74
			204	205.94	0.12	0.00	0.00	-0.12	-0.74
371	Primo Impalcato	1, 92	0	-315.50	0.10	0.00	0.00	-1.24	-0.51
			103	-315.50	0.10	0.00	0.00	-0.71	-0.51
			206	-315.50	0.10	0.00	0.00	-0.18	-0.51
372	Primo Impalcato	92, 2	0	274.79	0.02	0.00	0.00	1.53	-0.45
			103	274.79	0.02	0.00	0.00	1.99	-0.45
			206	274.79	0.02	0.00	0.00	2.45	-0.45
373	Primo Impalcato	6, 89	0	-323.38	0.00	0.00	0.00	1.03	-0.06
			100	-323.38	0.00	0.00	0.00	1.09	-0.06
			200	-323.38	0.00	0.00	0.00	1.15	-0.06
374	Primo Impalcato	89, 7	0	320.11	-0.07	0.00	0.00	0.69	0.28
			100	320.11	-0.07	0.00	0.00	0.41	0.28
			200	320.11	-0.07	0.00	0.00	0.13	0.28
375	Primo Impalcato	9, 90	0	-317.15	-0.04	0.00	0.00	0.80	0.12
			100	-317.15	-0.04	0.00	0.00	0.67	0.12
			200	-317.15	-0.04	0.00	0.00	0.55	0.12
376	Primo Impalcato	90, 10	0	331.49	-0.05	0.00	0.00	-0.12	0.17
			100	331.49	-0.05	0.00	0.00	-0.29	0.17
			200	331.49	-0.05	0.00	0.00	-0.46	0.17
377	Primo Impalcato	13, 91	0	-274.03	-0.01	0.00	0.00	-0.55	-0.05
			103	-274.03	-0.01	0.00	0.00	-0.50	-0.05
			206	-274.03	-0.01	0.00	0.00	-0.45	-0.05

378	Primo Impalcato	88, 14	0	-161.75	0.06	0.00	0.00	-0.02	-0.52
			102	-161.75	0.06	0.00	0.00	0.52	-0.52
			204	-161.75	0.06	0.00	0.00	1.05	-0.52
379	Primo Impalcato	91, 14	0	305.52	0.06	0.00	0.00	0.07	-0.49
			103	305.52	0.06	0.00	0.00	0.57	-0.49
			206	305.52	0.06	0.00	0.00	1.07	-0.49
380	Primo Impalcato	71, 15	0	-172.53	0.02	0.00	0.00	0.87	0.16
			102	-172.53	0.02	0.00	0.00	0.71	0.16
			204	-172.53	0.02	0.00	0.00	0.54	0.16
381	Primo Impalcato	16, 88	0	117.90	0.03	0.00	0.00	-0.73	0.08
			102	117.90	0.03	0.00	0.00	-0.81	0.08
			204	117.90	0.03	0.00	0.00	-0.90	0.08
382	Primo Impalcato	17, 72	0	181.50	0.05	0.00	0.00	-0.30	-0.56
			100	181.50	0.05	0.00	0.00	0.26	-0.56
			199	181.50	0.05	0.00	0.00	0.82	-0.56
383	Primo Impalcato	87, 18	0	-115.67	0.05	0.00	0.00	-0.79	-0.55
			100	-115.67	0.05	0.00	0.00	-0.23	-0.55
			199	-115.67	0.05	0.00	0.00	0.32	-0.55
384	Primo Impalcato	72, 19	0	-171.23	-0.01	0.00	0.00	1.04	0.48
			100	-171.23	-0.01	0.00	0.00	0.57	0.48
			199	-171.23	-0.01	0.00	0.00	0.09	0.48
385	Primo Impalcato	20, 87	0	104.03	-0.02	0.00	0.00	-0.08	0.49
			100	104.03	-0.02	0.00	0.00	-0.57	0.49
			199	104.03	-0.02	0.00	0.00	-1.05	0.49
386	Primo Impalcato	21, 73	0	187.01	0.01	0.00	0.00	0.11	-0.48
			100	187.01	0.01	0.00	0.00	0.59	-0.48
			199	187.01	0.01	0.00	0.00	1.07	-0.48
387	Primo Impalcato	86, 22	0	-112.95	0.01	0.00	0.00	-1.08	-0.49
			100	-112.95	0.01	0.00	0.00	-0.59	-0.49
			199	-112.95	0.01	0.00	0.00	-0.10	-0.49
388	Primo Impalcato	73, 23	0	-173.76	-0.04	0.00	0.00	0.81	0.53
			100	-173.76	-0.04	0.00	0.00	0.28	0.53
			199	-173.76	-0.04	0.00	0.00	-0.24	0.53
389	Primo Impalcato	24, 86	0	105.34	-0.05	0.00	0.00	0.25	0.53
			100	105.34	-0.05	0.00	0.00	-0.28	0.53
			199	105.34	-0.05	0.00	0.00	-0.81	0.53
390	Primo Impalcato	25, 74	0	215.86	-0.01	0.00	0.00	0.40	-0.27
			103	215.86	-0.01	0.00	0.00	0.69	-0.27
			206	215.86	-0.01	0.00	0.00	0.97	-0.27
391	Primo Impalcato	85, 26	0	-111.44	-0.02	0.00	0.00	-0.99	-0.31
			100	-111.44	-0.02	0.00	0.00	-0.68	-0.31
			199	-111.44	-0.02	0.00	0.00	-0.37	-0.31
392	Primo Impalcato	27, 85	0	107.24	-0.05	0.00	0.00	0.39	0.42
			100	107.24	-0.05	0.00	0.00	-0.03	0.42
			199	107.24	-0.05	0.00	0.00	-0.44	0.42
393	Primo Impalcato	74, 28	0	-208.05	-0.05	0.00	0.00	0.34	0.39
			103	-208.05	-0.05	0.00	0.00	-0.06	0.39
			206	-208.05	-0.05	0.00	0.00	-0.46	0.39
394	Primo Impalcato	84, 29	0	-111.58	-0.03	0.00	0.00	-0.66	-0.13
			100	-111.58	-0.03	0.00	0.00	-0.54	-0.13
			199	-111.58	-0.03	0.00	0.00	-0.41	-0.13
395	Primo Impalcato	31, 84	0	109.91	-0.04	0.00	0.00	0.36	0.24
			100	109.91	-0.04	0.00	0.00	0.13	0.24
			199	109.91	-0.04	0.00	0.00	-0.11	0.24
396	Primo	83, 33	0	-111.85	-0.03	0.00	0.00	-0.32	0.03

	Impalcato								
			100	-111.85	-0.03	0.00	0.00	-0.35	0.03
			199	-111.85	-0.03	0.00	0.00	-0.38	0.03
397	Primo Impalcato	35, 83	0	111.57	-0.03	0.00	0.00	0.35	0.08
			100	111.57	-0.03	0.00	0.00	0.26	0.08
			199	111.57	-0.03	0.00	0.00	0.18	0.08
398	Primo Impalcato	82, 37	0	-111.13	-0.04	0.00	0.00	-0.02	0.18
			100	-111.13	-0.04	0.00	0.00	-0.20	0.18
			199	-111.13	-0.04	0.00	0.00	-0.37	0.18
399	Primo Impalcato	39, 82	0	113.01	-0.03	0.00	0.00	0.36	-0.07
			100	113.01	-0.03	0.00	0.00	0.43	-0.07
			199	113.01	-0.03	0.00	0.00	0.50	-0.07
400	Primo Impalcato	78, 43	0	185.90	-0.05	0.00	0.00	0.39	0.38
			100	185.90	-0.05	0.00	0.00	0.01	0.38
			199	185.90	-0.05	0.00	0.00	-0.37	0.38
401	Primo Impalcato	81, 44	0	-110.69	-0.05	0.00	0.00	0.45	0.40
			100	-110.69	-0.05	0.00	0.00	0.05	0.40
			199	-110.69	-0.05	0.00	0.00	-0.35	0.40
402	Primo Impalcato	45, 78	0	-184.29	-0.02	0.00	0.00	0.35	-0.31
			100	-184.29	-0.02	0.00	0.00	0.65	-0.31
			199	-184.29	-0.02	0.00	0.00	0.96	-0.31
403	Primo Impalcato	46, 81	0	115.09	-0.02	0.00	0.00	0.35	-0.30
			100	115.09	-0.02	0.00	0.00	0.65	-0.30
			199	115.09	-0.02	0.00	0.00	0.95	-0.30
404	Primo Impalcato	77, 47	0	177.89	-0.05	0.00	0.00	0.78	0.52
			100	177.89	-0.05	0.00	0.00	0.26	0.52
			199	177.89	-0.05	0.00	0.00	-0.26	0.52
405	Primo Impalcato	80, 48	0	-109.01	-0.05	0.00	0.00	0.78	0.52
			100	-109.01	-0.05	0.00	0.00	0.26	0.52
			199	-109.01	-0.05	0.00	0.00	-0.25	0.52
406	Primo Impalcato	49, 77	0	-190.00	0.01	0.00	0.00	0.13	-0.47
			100	-190.00	0.01	0.00	0.00	0.59	-0.47
			199	-190.00	0.01	0.00	0.00	1.06	-0.47
407	Primo Impalcato	50, 80	0	117.29	0.01	0.00	0.00	0.13	-0.47
			100	117.29	0.01	0.00	0.00	0.60	-0.47
			199	117.29	0.01	0.00	0.00	1.07	-0.47
408	Primo Impalcato	76, 51	0	176.04	-0.02	0.00	0.00	1.02	0.48
			100	176.04	-0.02	0.00	0.00	0.55	0.48
			199	176.04	-0.02	0.00	0.00	0.08	0.48
409	Primo Impalcato	53, 76	0	-186.50	0.05	0.00	0.00	-0.29	-0.55
			100	-186.50	0.05	0.00	0.00	0.26	-0.55
			199	-186.50	0.05	0.00	0.00	0.82	-0.55
410	Primo Impalcato	75, 55	0	177.53	0.02	0.00	0.00	0.87	0.16
			102	177.53	0.02	0.00	0.00	0.71	0.16
			204	177.53	0.02	0.00	0.00	0.54	0.16
411	Primo Impalcato	56, 79	0	-125.26	0.03	0.00	0.00	-0.75	0.07
			102	-125.26	0.03	0.00	0.00	-0.82	0.07
			204	-125.26	0.03	0.00	0.00	-0.90	0.07
412	Primo Impalcato	57, 75	0	-211.74	0.12	0.00	0.00	-1.65	-0.74
			102	-211.74	0.12	0.00	0.00	-0.89	-0.74
			204	-211.74	0.12	0.00	0.00	-0.13	-0.74
413	Primo Impalcato	57, 93	0	308.76	0.10	0.00	0.00	-1.30	-0.54
			103	308.76	0.10	0.00	0.00	-0.74	-0.54
			206	308.76	0.10	0.00	0.00	-0.18	-0.54
414	Primo Impalcato	93, 58	0	-271.14	0.03	0.00	0.00	1.57	-0.47

			103	-271.14	0.03	0.00	0.00	2.05	-0.47
			206	-271.14	0.03	0.00	0.00	2.53	-0.47
415	Primo Impalcato	61, 95	0	321.66	0.01	0.00	0.00	1.03	-0.16
			100	321.66	0.01	0.00	0.00	1.19	-0.16
			200	321.66	0.01	0.00	0.00	1.36	-0.16
416	Primo Impalcato	95, 62	0	-307.34	-0.07	0.00	0.00	0.93	0.30
			100	-307.34	-0.07	0.00	0.00	0.63	0.30
			200	-307.34	-0.07	0.00	0.00	0.33	0.30
417	Primo Impalcato	96, 65	0	309.63	-0.04	0.00	0.00	-0.56	0.14
			100	309.63	-0.04	0.00	0.00	-0.69	0.14
			200	309.63	-0.04	0.00	0.00	-0.83	0.14
418	Primo Impalcato	66, 96	0	-323.40	-0.05	0.00	0.00	0.47	0.17
			100	-323.40	-0.05	0.00	0.00	0.30	0.17
			200	-323.40	-0.05	0.00	0.00	0.13	0.17
419	Primo Impalcato	69, 94	0	266.76	-0.01	0.00	0.00	-0.58	-0.08
			103	266.76	-0.01	0.00	0.00	-0.50	-0.08
			206	266.76	-0.01	0.00	0.00	-0.41	-0.08
420	Primo Impalcato	79, 70	0	168.98	0.06	0.00	0.00	-0.01	-0.52
			102	168.98	0.06	0.00	0.00	0.52	-0.52
			204	168.98	0.06	0.00	0.00	1.05	-0.52
421	Primo Impalcato	94, 70	0	-296.49	0.06	0.00	0.00	0.05	-0.57
			103	-296.49	0.06	0.00	0.00	0.64	-0.57
			206	-296.49	0.06	0.00	0.00	1.23	-0.57
422	Copertura	1, 2	0	5.00	-50.69	212.09	406.10	-57.21	23.17
			83	5.00	-50.69	549.64	406.10	-76.47	23.17
			166	5.00	-50.69	887.20	406.10	-95.73	23.17
423	Copertura	15, 1	0	5.08	-4.20	-219.85	-51.47	40.91	63.36
			80	5.08	-4.20	-260.76	-51.47	-9.46	63.36
			159	5.08	-4.20	-301.68	-51.47	-59.83	63.36
424	Copertura	2, 3	0	44.59	-19.55	890.34	-222.88	-96.37	-10.63
			69	44.59	-19.55	736.55	-222.88	-89.03	-10.63
			138	44.59	-19.55	582.77	-222.88	-81.70	-10.63
425	Copertura	3, 4	0	45.18	-4.06	590.80	-269.83	-81.71	-2.41
			69	45.18	-4.06	404.62	-269.83	-80.05	-2.41
			138	45.18	-4.06	218.44	-269.83	-78.39	-2.41
426	Copertura	4, 5	0	45.79	2.00	226.60	-245.90	-78.43	3.48
			69	45.79	2.00	56.93	-245.90	-80.83	3.48
			138	45.79	2.00	-112.75	-245.90	-83.23	3.48
427	Copertura	5, 6	0	46.35	7.62	-104.19	-159.31	-83.41	10.03
			69	46.35	7.62	-214.11	-159.31	-90.33	10.03
			138	46.35	7.62	-324.04	-159.31	-97.25	10.03
428	Copertura	6, 7	0	66.94	12.87	-316.43	388.16	-97.65	-13.22
			69	66.94	12.87	-48.60	388.16	-88.53	-13.22
			138	66.94	12.87	219.23	388.16	-79.41	-13.22
429	Copertura	7, 8	0	82.74	17.03	226.79	-164.54	-80.18	-30.95
			69	82.74	17.03	113.26	-164.54	-58.82	-30.95
			138	82.74	17.03	-0.27	-164.54	-37.47	-30.95
430	Copertura	8, 9	0	83.13	18.74	8.48	-176.59	-38.05	-27.15
			69	83.13	18.74	-113.37	-176.59	-19.32	-27.15
			138	83.13	18.74	-235.21	-176.59	-0.59	-27.15
431	Copertura	9, 10	0	93.45	17.84	-227.64	348.54	-1.46	-31.53
			69	93.45	17.84	12.85	348.54	20.30	-31.53
			138	93.45	17.84	253.34	348.54	42.06	-31.53
432	Copertura	10, 11	0	104.05	14.84	260.92	-221.83	41.29	-28.90
			69	104.05	14.84	107.86	-221.83	61.23	-28.90
			138	104.05	14.84	-45.20	-221.83	81.18	-28.90
433	Copertura	11, 12	0	104.44	8.87	-36.77	-313.37	80.72	-29.81
			69	104.44	8.87	-253.00	-313.37	101.29	-29.81
			138	104.44	8.87	-469.22	-313.37	121.86	-29.81
434	Copertura	12, 13	0	104.83	-4.24	-461.10	-259.17	121.53	-33.03
			69	104.83	-4.24	-639.93	-259.17	144.33	-33.03
			138	104.83	-4.24	-818.76	-259.17	167.12	-33.03
435	Copertura	13, 14	0	120.39	-7.75	-813.02	378.11	166.28	-14.03
			83	120.39	-7.75	-498.73	378.11	177.95	-14.03
			166	120.39	-7.75	-184.44	378.11	189.61	-14.03
436	Copertura	16, 14	0	8.43	-3.73	41.35	48.65	60.30	156.93

			80	8.43	-3.73	80.03	48.65	-64.46	156.93
			159	8.43	-3.73	118.71	48.65	-189.23	156.93
437	Copertura	15, 17	0	34.85	-2.31	-318.35	193.65	-52.77	34.44
			66	34.85	-2.31	-190.54	193.65	-75.50	34.44
			132	34.85	-2.31	-62.73	193.65	-98.23	34.44
438	Copertura	16, 18	0	-10.47	-1.21	84.18	-111.86	-51.83	45.22
			66	-10.47	-1.21	10.35	-111.86	-81.68	45.22
			132	-10.47	-1.21	-63.48	-111.86	-111.52	45.22
439	Copertura	17, 19	0	58.92	-1.08	-160.36	115.27	-111.85	-8.42
			66	58.92	-1.08	-84.28	115.27	-106.29	-8.42
			132	58.92	-1.08	-8.20	115.27	-100.73	-8.42
440	Copertura	18, 20	0	-19.96	-0.68	-13.04	-22.75	-108.18	-0.92
			66	-19.96	-0.68	-28.05	-22.75	-107.57	-0.92
			132	-19.96	-0.68	-43.07	-22.75	-106.96	-0.92
441	Copertura	19, 21	0	77.99	0.04	-106.13	134.09	-120.61	-32.68
			66	77.99	0.04	-17.63	134.09	-99.04	-32.68
			132	77.99	0.04	70.86	134.09	-77.47	-32.68
442	Copertura	20, 22	0	-30.12	0.06	6.85	-63.33	-115.03	-25.15
			66	-30.12	0.06	-34.94	-63.33	-98.43	-25.15
			132	-30.12	0.06	-76.74	-63.33	-81.83	-25.15
443	Copertura	21, 23	0	91.29	0.87	-27.06	66.02	-102.04	-41.23
			66	91.29	0.87	16.52	66.02	-74.83	-41.23
			132	91.29	0.87	60.09	66.02	-47.62	-41.23
444	Copertura	22, 24	0	-39.73	0.92	-26.66	-2.56	-97.98	-36.10
			66	-39.73	0.92	-28.35	-2.56	-74.15	-36.10
			132	-39.73	0.92	-30.04	-2.56	-50.33	-36.10
445	Copertura	23, 25	0	97.38	1.42	-37.74	85.18	-73.45	-43.95
			66	97.38	1.42	18.48	85.18	-44.44	-43.95
			132	97.38	1.42	74.70	85.18	-15.43	-43.95
446	Copertura	24, 26	0	-48.17	1.20	19.82	-58.40	-73.27	-35.12
			66	-48.17	1.20	-18.72	-58.40	-50.09	-35.12
			132	-48.17	1.20	-57.26	-58.40	-26.91	-35.12
447	Copertura	25, 28	0	95.82	1.57	-22.96	9.43	-39.24	-23.78
			85	95.82	1.57	-14.95	9.43	-19.03	-23.78
			170	95.82	1.57	-6.93	9.43	1.18	-23.78
448	Copertura	26, 27	0	-53.27	1.91	-7.16	-4.34	-51.87	-42.77
			66	-53.27	1.91	-10.02	-4.34	-23.64	-42.77
			132	-53.27	1.91	-12.89	-4.34	4.59	-42.77
449	Copertura	27, 29	0	-51.89	1.68	37.61	-63.19	-17.71	-27.13
			66	-51.89	1.68	-4.10	-63.19	0.19	-27.13
			132	-51.89	1.68	-45.81	-63.19	18.10	-27.13
450	Copertura	28, 30	0	80.59	1.76	-102.99	74.86	-14.38	-17.04
			73	80.59	1.76	-48.35	74.86	-1.94	-17.04
			146	80.59	1.76	6.30	74.86	10.50	-17.04
451	Copertura	29, 31	0	-43.77	1.85	4.75	-9.51	1.51	-11.32
			66	-43.77	1.85	-1.53	-9.51	8.98	-11.32
			132	-43.77	1.85	-7.80	-9.51	16.46	-11.32
452	Copertura	30, 32	0	56.82	1.66	-90.48	85.96	1.19	-8.54
			69	56.82	1.66	-31.60	85.96	7.04	-8.54
			137	56.82	1.66	27.28	85.96	12.89	-8.54
453	Copertura	31, 33	0	-29.27	1.56	42.97	-65.12	6.40	-2.52
			66	-29.27	1.56	0.00	-65.12	8.06	-2.52
			132	-29.27	1.56	-42.98	-65.12	9.73	-2.52
454	Copertura	32, 34	0	28.68	1.65	-69.81	79.43	7.93	0.12
			69	28.68	1.65	-15.00	79.43	7.85	0.12
			138	28.68	1.65	39.81	79.43	7.77	0.12
455	Copertura	33, 35	0	-11.67	1.71	5.56	-8.35	5.41	3.89
			66	-11.67	1.71	0.05	-8.35	2.84	3.89
			132	-11.67	1.71	-5.47	-8.35	0.27	3.89
456	Copertura	34, 36	0	-1.45	1.53	-57.84	78.50	5.26	3.46
			69	-1.45	1.53	-3.67	78.50	2.87	3.46
			138	-1.45	1.53	50.50	78.50	0.49	3.46
457	Copertura	35, 37	0	11.23	1.52	46.58	-62.69	-1.54	3.14
			66	11.23	1.52	5.21	-62.69	-3.62	3.14
			132	11.23	1.52	-36.16	-62.69	-5.69	3.14
458	Copertura	36, 38	0	-31.21	1.62	-47.80	85.84	-1.97	1.56
			69	-31.21	1.62	11.43	85.84	-3.05	1.56
			138	-31.21	1.62	70.66	85.84	-4.13	1.56
459	Copertura	37, 39	0	31.42	1.84	12.57	-4.24	-9.48	-5.23
			66	31.42	1.84	9.77	-4.24	-6.03	-5.23
			132	31.42	1.84	6.97	-4.24	-2.58	-5.23
460	Copertura	38, 40	0	-58.84	1.51	-28.38	100.66	-8.66	-2.94

			69	-58.84	1.51	40.57	100.66	-6.65	-2.94
			137	-58.84	1.51	109.52	100.66	-4.64	-2.94
461	Copertura	39, 41	0	50.40	1.77	55.95	-70.78	-10.61	-21.98
			66	50.40	1.77	9.24	-70.78	3.90	-21.98
			132	50.40	1.77	-37.48	-70.78	18.41	-21.98
462	Copertura	40, 42	0	-83.31	1.49	9.50	100.42	-12.63	-9.15
			69	-83.31	1.49	78.79	100.42	-6.32	-9.15
			138	-83.31	1.49	148.08	100.42	-0.01	-9.15
463	Copertura	41, 44	0	65.78	1.22	10.89	-39.45	7.30	5.66
			66	65.78	1.22	-15.15	-39.45	3.56	5.66
			132	65.78	1.22	-41.19	-39.45	-0.18	5.66
464	Copertura	42, 43	0	-101.35	3.45	47.35	33.53	-11.75	-65.14
			23	-101.35	3.45	55.06	33.53	3.24	-65.14
			46	-101.35	3.45	62.77	33.53	18.22	-65.14
465	Copertura	43, 45	0	-110.81	1.55	-34.22	28.72	-1.02	-30.74
			66	-110.81	1.55	-15.27	28.72	19.27	-30.74
			132	-110.81	1.55	3.69	28.72	39.56	-30.74
466	Copertura	44, 46	0	63.73	1.68	7.12	-22.04	-22.62	-45.52
			66	63.73	1.68	-7.42	-22.04	7.42	-45.52
			132	63.73	1.68	-21.97	-22.04	37.47	-45.52
467	Copertura	45, 47	0	-111.56	1.28	-93.80	96.46	15.20	-41.81
			66	-111.56	1.28	-30.14	96.46	42.80	-41.81
			132	-111.56	1.28	33.53	96.46	70.39	-41.81
468	Copertura	46, 48	0	58.30	1.52	26.87	-15.61	12.57	-43.49
			66	58.30	1.52	16.57	-15.61	41.28	-43.49
			132	58.30	1.52	6.27	-15.61	69.98	-43.49
469	Copertura	47, 49	0	-104.57	1.03	-63.99	66.25	43.65	-44.14
			66	-104.57	1.03	-20.27	66.25	72.78	-44.14
			132	-104.57	1.03	23.45	66.25	101.91	-44.14
470	Copertura	48, 50	0	49.94	0.84	55.28	-15.15	47.35	-38.93
			66	49.94	0.84	45.29	-15.15	73.04	-38.93
			132	49.94	0.84	35.29	-15.15	98.73	-38.93
471	Copertura	49, 51	0	-90.64	0.10	-74.23	133.15	76.38	-35.35
			66	-90.64	0.10	13.65	133.15	99.71	-35.35
			132	-90.64	0.10	101.53	133.15	123.04	-35.35
472	Copertura	50, 52	0	40.22	0.20	84.74	-33.39	81.06	-27.01
			66	40.22	0.20	62.70	-33.39	98.89	-27.01
			132	40.22	0.20	40.66	-33.39	116.71	-27.01
473	Copertura	51, 53	0	-71.07	-0.96	3.83	113.62	102.25	-10.66
			66	-71.07	-0.96	78.82	113.62	109.29	-10.66
			132	-71.07	-0.96	153.81	113.62	116.32	-10.66
474	Copertura	52, 54	0	30.29	-0.69	90.46	-89.80	109.18	-3.40
			66	30.29	-0.69	31.19	-89.80	111.43	-3.40
			132	30.29	-0.69	-28.08	-89.80	113.67	-3.40
475	Copertura	53, 55	0	-46.67	-2.30	56.35	195.14	102.27	31.89
			66	-46.67	-2.30	185.14	195.14	81.23	31.89
			132	-46.67	-2.30	313.93	195.14	60.18	31.89
476	Copertura	54, 56	0	20.21	-1.23	21.30	-77.23	115.69	40.79
			66	20.21	-1.23	-29.67	-77.23	88.77	40.79
			132	20.21	-1.23	-80.63	-77.23	61.85	40.79
477	Copertura	55, 57	0	-16.89	-4.47	215.61	55.35	48.53	49.55
			80	-16.89	-4.47	259.61	55.35	9.14	49.55
			159	-16.89	-4.47	303.61	55.35	-30.25	49.55
478	Copertura	56, 70	0	9.44	-3.56	-30.81	-49.79	71.62	165.79
			80	9.44	-3.56	-70.39	-49.79	-60.19	165.79
			159	9.44	-3.56	-109.98	-49.79	-192.00	165.79
479	Copertura	57, 58	0	-16.96	-53.21	-209.30	-377.63	-27.35	37.66
			83	-16.96	-53.21	-523.19	-377.63	-58.66	37.66
			166	-16.96	-53.21	-837.09	-377.63	-89.96	37.66
480	Copertura	58, 59	0	-53.29	-21.13	-839.98	250.45	-90.46	1.11
			69	-53.29	-21.13	-667.18	250.45	-91.22	1.11
			138	-53.29	-21.13	-494.37	250.45	-91.99	1.11
481	Copertura	59, 60	0	-53.71	-5.35	-502.17	303.95	-91.94	9.77
			69	-53.71	-5.35	-292.45	303.95	-98.68	9.77
			138	-53.71	-5.35	-82.72	303.95	-105.42	9.77
482	Copertura	60, 61	0	-54.32	1.86	-90.87	205.60	-105.42	16.45
			69	-54.32	1.86	51.00	205.60	-116.77	16.45
			138	-54.32	1.86	192.87	205.60	-128.12	16.45
483	Copertura	61, 62	0	-79.19	8.88	185.49	-364.07	-128.29	-12.29
			69	-79.19	8.88	-65.71	-364.07	-119.81	-12.29
			138	-79.19	8.88	-316.92	-364.07	-111.33	-12.29
484	Copertura	62, 63	0	-97.37	14.95	-324.36	138.92	-112.00	-34.68

			69	-97.37	14.95	-228.51	138.92	-88.07	-34.68
			138	-97.37	14.95	-132.65	138.92	-64.14	-34.68
485	Copertura	63, 64	0	-97.73	18.47	-141.05	200.80	-64.70	-29.05
			69	-97.73	18.47	-2.50	200.80	-44.65	-29.05
			138	-97.73	18.47	136.06	200.80	-24.61	-29.05
486	Copertura	64, 65	0	-98.04	19.73	127.65	137.17	-25.23	-25.32
			69	-98.04	19.73	222.30	137.17	-7.76	-25.32
			138	-98.04	19.73	316.94	137.17	9.71	-25.32
487	Copertura	65, 66	0	-106.55	18.43	309.49	-370.00	8.79	-29.76
			69	-106.55	18.43	54.19	-370.00	29.32	-29.76
			138	-106.55	18.43	-201.11	-370.00	49.86	-29.76
488	Copertura	66, 67	0	-115.39	15.09	-208.52	199.15	49.08	-27.21
			69	-115.39	15.09	-71.11	199.15	67.86	-27.21
			138	-115.39	15.09	66.31	199.15	86.64	-27.21
489	Copertura	67, 68	0	-115.71	8.82	58.11	296.35	86.18	-28.24
			69	-115.71	8.82	262.59	296.35	105.67	-28.24
			138	-115.71	8.82	467.07	296.35	125.16	-28.24
490	Copertura	68, 69	0	-116.05	-4.40	459.19	248.27	124.85	-31.53
			69	-116.05	-4.40	630.50	248.27	146.61	-31.53
			138	-116.05	-4.40	801.80	248.27	168.36	-31.53
491	Copertura	69, 70	0	-131.84	-8.16	796.29	-370.64	167.56	-14.10
			83	-131.84	-8.16	488.20	-370.64	179.28	-14.10
			166	-131.84	-8.16	180.12	-370.64	191.00	-14.10
492	Copertura	1	0	-200.73	-0.44	231.13	-102.25	-204.38	-73.35
			220	-200.73	-0.44	6.19	-102.25	-43.01	-73.35
			440	-200.73	-0.44	-218.75	-102.25	118.36	-73.35
493	Copertura	2	0	316.28	-0.20	77.91	-33.43	-7.12	-3.30
			220	316.28	-0.20	4.37	-33.43	0.15	-3.30
			440	316.28	-0.20	-69.16	-33.43	7.42	-3.30
494	Copertura	3	0	46.95	-0.01	15.49	-10.20	-8.03	-3.72
			220	46.95	-0.01	-6.94	-10.20	0.16	-3.72
			440	46.95	-0.01	-29.38	-10.20	8.36	-3.72
495	Copertura	4	0	-23.92	-0.03	6.06	-7.55	-8.16	-3.70
			220	-23.92	-0.03	-10.55	-7.55	-0.01	-3.70
			440	-23.92	-0.03	-27.16	-7.55	8.14	-3.70
496	Copertura	5	0	-86.59	-0.17	5.62	-8.05	-8.56	-3.96
			220	-86.59	-0.17	-12.09	-8.05	0.15	-3.96
			440	-86.59	-0.17	-29.81	-8.05	8.86	-3.96
497	Copertura	6	0	-206.74	-0.34	5.36	-7.85	-7.60	-3.36
			220	-206.74	-0.34	-11.92	-7.85	-0.20	-3.36
			440	-206.74	-0.34	-29.19	-7.85	7.20	-3.36
498	Copertura	7	0	210.62	-0.49	3.55	-6.34	-7.56	-3.35
			220	210.62	-0.49	-10.39	-6.34	-0.19	-3.35
			440	210.62	-0.49	-24.34	-6.34	7.17	-3.35
499	Copertura	8	0	12.05	-0.59	1.71	-4.41	-8.75	-4.13
			220	12.05	-0.59	-7.98	-4.41	0.33	-4.13
			440	12.05	-0.59	-17.68	-4.41	9.41	-4.13
500	Copertura	9	0	-188.49	-0.61	-0.35	-2.33	-7.57	-3.35
			220	-188.49	-0.61	-5.48	-2.33	-0.19	-3.35
			440	-188.49	-0.61	-10.61	-2.33	7.19	-3.35
501	Copertura	10	0	223.97	-0.56	-3.39	-0.11	-7.58	-3.36
			220	223.97	-0.56	-3.64	-0.11	-0.20	-3.36
			440	223.97	-0.56	-3.89	-0.11	7.19	-3.36
502	Copertura	11	0	91.54	-0.45	-5.97	1.32	-8.43	-3.91
			220	91.54	-0.45	-3.06	1.32	0.17	-3.91
			440	91.54	-0.45	-0.16	1.32	8.76	-3.91
503	Copertura	12	0	-54.20	-0.32	-13.10	3.94	-8.12	-3.77
			220	-54.20	-0.32	-4.43	3.94	0.16	-3.77
			440	-54.20	-0.32	4.24	3.94	8.45	-3.77
504	Copertura	13	0	-303.08	-0.23	-46.06	15.75	-7.27	-3.36
			220	-303.08	-0.23	-11.42	15.75	0.12	-3.36
			440	-303.08	-0.23	23.22	15.75	7.51	-3.36
505	Copertura	57	0	183.92	-0.17	230.68	-102.02	201.19	72.16
			220	183.92	-0.17	6.24	-102.02	42.44	72.16
			440	183.92	-0.17	-218.21	-102.02	-116.32	72.16
506	Copertura	58	0	-320.32	-0.12	76.29	-33.12	6.95	3.23
			220	-320.32	-0.12	3.43	-33.12	-0.15	3.23
			440	-320.32	-0.12	-69.43	-33.12	-7.25	3.23
507	Copertura	59	0	-53.50	0.05	15.78	-10.69	7.80	3.62
			220	-53.50	0.05	-7.73	-10.69	-0.17	3.62
			440	-53.50	0.05	-31.25	-10.69	-8.14	3.62
508	Copertura	60	0	98.34	0.00	7.21	-8.40	8.14	3.78

			220	98.34	0.00	-11.26	-8.40	-0.17	3.78
			440	98.34	0.00	-29.74	-8.40	-8.47	3.78
509	Copertura	61	0	228.95	-0.20	6.90	-8.95	7.37	3.27
			220	228.95	-0.20	-12.79	-8.95	0.19	3.27
			440	228.95	-0.20	-32.49	-8.95	-7.00	3.27
510	Copertura	62	0	-175.70	-0.41	5.49	-8.21	7.44	3.29
			220	-175.70	-0.41	-12.57	-8.21	0.20	3.29
			440	-175.70	-0.41	-30.63	-8.21	-7.04	3.29
511	Copertura	63	0	-61.89	-0.56	3.53	-6.53	8.40	3.88
			220	-61.89	-0.56	-10.84	-6.53	-0.15	3.88
			440	-61.89	-0.56	-25.21	-6.53	-8.69	3.88
512	Copertura	64	0	63.63	-0.63	1.25	-4.32	8.41	3.89
			220	63.63	-0.63	-8.25	-4.32	-0.15	3.89
			440	63.63	-0.63	-17.76	-4.32	-8.70	3.89
513	Copertura	65	0	178.63	-0.64	-0.70	-2.27	7.46	3.30
			220	178.63	-0.64	-5.69	-2.27	0.20	3.30
			440	178.63	-0.64	-10.68	-2.27	-7.06	3.30
514	Copertura	66	0	-227.36	-0.58	-3.73	-0.01	7.41	3.28
			220	-227.36	-0.58	-3.75	-0.01	0.19	3.28
			440	-227.36	-0.58	-3.77	-0.01	-7.03	3.28
515	Copertura	67	0	-97.20	-0.45	-6.27	1.45	8.20	3.80
			220	-97.20	-0.45	-3.09	1.45	-0.16	3.80
			440	-97.20	-0.45	0.09	1.45	-8.53	3.80
516	Copertura	68	0	48.08	-0.31	-13.22	4.00	7.88	3.66
			220	48.08	-0.31	-4.43	4.00	-0.16	3.66
			440	48.08	-0.31	4.37	4.00	-8.21	3.66
517	Copertura	69	0	294.40	-0.21	-45.43	15.47	7.05	3.26
			220	294.40	-0.21	-11.39	15.47	-0.12	3.26
			440	294.40	-0.21	22.65	15.47	-7.29	3.26
518	Primo Impalcato	1, 74	0	334.27	-0.13	0.00	0.00	8.53	4.73
			118	334.27	-0.13	0.00	0.00	2.97	4.73
			235	334.27	-0.13	0.00	0.00	-2.59	4.73
519	Copertura	74, 2	0	-274.55	0.05	0.00	0.00	2.06	0.54
			118	-274.55	0.05	0.00	0.00	1.42	0.54
			235	-274.55	0.05	0.00	0.00	0.79	0.54
520	Primo Impalcato	6, 71	0	358.51	-0.07	0.00	0.00	0.43	0.28
			115	358.51	-0.07	0.00	0.00	0.11	0.28
			231	358.51	-0.07	0.00	0.00	-0.21	0.28
521	Copertura	71, 7	0	-357.10	-0.03	0.00	0.00	0.65	-0.14
			115	-357.10	-0.03	0.00	0.00	0.82	-0.14
			231	-357.10	-0.03	0.00	0.00	0.98	-0.14
522	Primo Impalcato	9, 72	0	363.04	-0.08	0.00	0.00	-0.25	0.10
			115	363.04	-0.08	0.00	0.00	-0.37	0.10
			231	363.04	-0.08	0.00	0.00	-0.49	0.10
523	Copertura	72, 10	0	-352.81	-0.07	0.00	0.00	0.73	0.07
			115	-352.81	-0.07	0.00	0.00	0.64	0.07
			231	-352.81	-0.07	0.00	0.00	0.56	0.07
524	Copertura	73, 13	0	299.31	0.05	0.00	0.00	0.42	0.08
			118	299.31	0.05	0.00	0.00	0.33	0.08
			235	299.31	0.05	0.00	0.00	0.23	0.08
525	Primo Impalcato	14, 73	0	-357.25	-0.07	0.00	0.00	3.09	1.81
			118	-357.25	-0.07	0.00	0.00	0.96	1.81
			235	-357.25	-0.07	0.00	0.00	-1.16	1.81
526	Primo Impalcato	57, 75	0	-328.99	-0.12	0.00	0.00	8.54	4.69
			118	-328.99	-0.12	0.00	0.00	3.02	4.69
			235	-328.99	-0.12	0.00	0.00	-2.49	4.69
527	Copertura	75, 58	0	266.24	0.06	0.00	0.00	2.01	0.54
			118	266.24	0.06	0.00	0.00	1.37	0.54
			235	266.24	0.06	0.00	0.00	0.74	0.54
528	Copertura	77, 61	0	-343.01	-0.06	0.00	0.00	0.06	0.29
			115	-343.01	-0.06	0.00	0.00	-0.27	0.29
			231	-343.01	-0.06	0.00	0.00	-0.60	0.29
529	Primo Impalcato	62, 77	0	357.08	-0.01	0.00	0.00	-1.10	-0.24
			115	357.08	-0.01	0.00	0.00	-0.82	-0.24
			231	357.08	-0.01	0.00	0.00	-0.54	-0.24
530	Primo Impalcato	65, 78	0	-358.20	-0.08	0.00	0.00	-0.26	0.10

			115	-358.20	-0.08	0.00	0.00	-0.38	0.10
			231	-358.20	-0.08	0.00	0.00	-0.49	0.10
531	Copertura	78, 66	0	344.32	-0.07	0.00	0.00	0.75	0.08
			115	344.32	-0.07	0.00	0.00	0.66	0.08
			231	344.32	-0.07	0.00	0.00	0.57	0.08
532	Primo Impalcato	69, 76	0	-288.93	0.05	0.00	0.00	-0.19	0.10
			118	-288.93	0.05	0.00	0.00	-0.30	0.10
			235	-288.93	0.05	0.00	0.00	-0.41	0.10
533	Copertura	76, 70	0	346.90	-0.07	0.00	0.00	1.15	1.82
			118	346.90	-0.07	0.00	0.00	-0.99	1.82
			235	346.90	-0.07	0.00	0.00	-3.13	1.82
534	Copertura	1, 74	0	-274.55	-0.13	0.00	0.00	-9.01	-4.70
			118	-274.55	-0.13	0.00	0.00	-3.48	-4.70
			235	-274.55	-0.13	0.00	0.00	2.04	-4.70
535	Copertura	74, 2	0	334.27	0.00	0.00	0.00	-2.46	-0.51
			118	334.27	0.00	0.00	0.00	-1.86	-0.51
			235	334.27	0.00	0.00	0.00	-1.26	-0.51
536	Copertura	6, 71	0	-357.10	-0.03	0.00	0.00	0.12	-0.23
			115	-357.10	-0.03	0.00	0.00	0.38	-0.23
			231	-357.10	-0.03	0.00	0.00	0.64	-0.23
537	Copertura	71, 7	0	358.51	-0.08	0.00	0.00	-0.21	0.20
			115	358.51	-0.08	0.00	0.00	-0.43	0.20
			231	358.51	-0.08	0.00	0.00	-0.66	0.20
538	Copertura	9, 72	0	-352.81	-0.08	0.00	0.00	0.61	-0.05
			115	-352.81	-0.08	0.00	0.00	0.67	-0.05
			231	-352.81	-0.08	0.00	0.00	0.72	-0.05
539	Copertura	72, 10	0	363.04	-0.07	0.00	0.00	-0.48	-0.02
			115	363.04	-0.07	0.00	0.00	-0.45	-0.02
			231	363.04	-0.07	0.00	0.00	-0.43	-0.02
540	Copertura	73, 13	0	-357.25	-0.06	0.00	0.00	-1.10	0.21
			118	-357.25	-0.06	0.00	0.00	-1.34	0.21
			235	-357.25	-0.06	0.00	0.00	-1.58	0.21
541	Copertura	14, 73	0	299.31	-0.01	0.00	0.00	-3.20	-1.52
			118	299.31	-0.01	0.00	0.00	-1.41	-1.52
			235	299.31	-0.01	0.00	0.00	0.38	-1.52
542	Copertura	15, 125	0	-106.84	-4.73	-8.01	104.70	13.23	34.97
			75	-106.84	-4.73	70.51	104.70	-13.00	34.97
			150	-106.84	-4.73	149.03	104.70	-39.23	34.97
543	Copertura	127, 16	0	42.94	-2.11	-159.57	113.76	39.31	20.79
			75	42.94	-2.11	-74.25	113.76	23.72	20.79
			150	42.94	-2.11	11.07	113.76	8.12	20.79
544	Copertura	17, 129	0	-116.22	-4.50	-16.33	137.99	14.85	31.26
			75	-116.22	-4.50	87.16	137.99	-8.60	31.26
			150	-116.22	-4.50	190.66	137.99	-32.04	31.26
545	Copertura	130, 18	0	130.39	-2.37	-193.56	139.48	31.81	19.40
			75	130.39	-2.37	-88.95	139.48	17.26	19.40
			150	130.39	-2.37	15.65	139.48	2.71	19.40
546	Copertura	19, 135	0	-138.12	-4.24	-14.19	149.41	20.81	29.21
			75	-138.12	-4.24	97.87	149.41	-1.09	29.21
			150	-138.12	-4.24	209.93	149.41	-23.00	29.21
547	Copertura	134, 20	0	153.18	-1.90	-210.06	148.61	23.34	20.86
			75	153.18	-1.90	-98.61	148.61	7.70	20.86
			150	153.18	-1.90	12.85	148.61	-7.95	20.86
548	Copertura	21, 136	0	-150.48	-3.97	-16.20	151.52	25.24	26.38
			75	-150.48	-3.97	97.43	151.52	5.46	26.38
			150	-150.48	-3.97	211.07	151.52	-14.33	26.38
549	Copertura	138, 22	0	162.90	-1.86	-211.18	151.25	14.85	20.73
			75	162.90	-1.86	-97.75	151.25	-0.70	20.73
			150	162.90	-1.86	15.69	151.25	-16.25	20.73
550	Copertura	23, 141	0	-137.95	-3.79	-12.36	136.98	26.34	22.48
			75	-137.95	-3.79	90.37	136.98	9.48	22.48
			150	-137.95	-3.79	193.10	136.98	-7.38	22.48
551	Copertura	142, 24	0	154.87	-1.54	-192.76	135.72	8.52	20.71
			75	154.87	-1.54	-90.96	135.72	-7.00	20.71
			150	154.87	-1.54	10.83	135.72	-22.53	20.71
552	Copertura	25, 145	0	-141.77	-3.66	-12.72	120.13	24.26	17.81
			75	-141.77	-3.66	77.38	120.13	10.90	17.81
			150	-141.77	-3.66	167.48	120.13	-2.46	17.81
553	Copertura	146, 26	0	125.52	-1.52	-168.68	120.88	3.70	18.93
			75	125.52	-1.52	-78.01	120.88	-10.50	18.93
			150	125.52	-1.52	12.65	120.88	-24.70	18.93

554	Copertura	150, 27	0	109.13	-1.42	-128.83	85.53	0.15	14.72
			75	109.13	-1.42	-64.68	85.53	-10.89	14.72
			150	109.13	-1.42	-0.53	85.53	-21.93	14.72
555	Copertura	28, 149	0	-106.62	-3.54	-21.82	100.55	16.08	9.65
			75	-106.62	-3.54	53.59	100.55	8.84	9.65
			150	-106.62	-3.54	129.01	100.55	1.60	9.65
556	Copertura	154, 29	0	81.57	-1.41	-94.77	61.86	-1.37	9.93
			75	81.57	-1.41	-48.37	61.86	-8.82	9.93
			150	81.57	-1.41	-1.97	61.86	-16.27	9.93
557	Copertura	30, 153	0	-88.14	-3.55	-26.51	80.13	9.92	4.43
			75	-88.14	-3.55	33.59	80.13	6.60	4.43
			150	-88.14	-3.55	93.69	80.13	3.27	4.43
558	Copertura	158, 31	0	45.03	-1.44	-58.55	33.52	-1.96	5.26
			75	45.03	-1.44	-33.41	33.52	-5.91	5.26
			150	45.03	-1.44	-8.27	33.52	-9.86	5.26
559	Copertura	32, 157	0	-66.19	-3.58	-26.90	57.42	5.65	1.29
			75	-66.19	-3.58	16.17	57.42	4.69	1.29
			150	-66.19	-3.58	59.23	57.42	3.72	1.29
560	Copertura	162, 33	0	20.30	-1.37	-27.92	13.57	-2.23	1.30
			75	20.30	-1.37	-17.74	13.57	-3.20	1.30
			150	20.30	-1.37	-7.57	13.57	-4.17	1.30
561	Copertura	34, 161	0	-40.45	-3.61	-27.11	36.23	3.24	-0.35
			75	-40.45	-3.61	0.06	36.23	3.51	-0.35
			150	-40.45	-3.61	27.23	36.23	3.77	-0.35
562	Copertura	166, 35	0	-14.71	-1.48	5.51	-13.33	-2.45	-0.52
			75	-14.71	-1.48	-4.49	-13.33	-2.07	-0.52
			150	-14.71	-1.48	-14.49	-13.33	-1.68	-0.52
563	Copertura	36, 165	0	-15.01	-3.63	-27.61	15.38	3.20	-0.33
			75	-15.01	-3.63	-16.08	15.38	3.44	-0.33
			150	-15.01	-3.63	-4.54	15.38	3.68	-0.33
564	Copertura	170, 37	0	-42.83	-1.37	35.10	-32.17	-2.22	0.95
			75	-42.83	-1.37	10.98	-32.17	-2.94	0.95
			150	-42.83	-1.37	-13.15	-32.17	-3.65	0.95
565	Copertura	38, 169	0	7.56	-3.64	-27.80	-5.21	5.23	1.13
			75	7.56	-3.64	-31.71	-5.21	4.39	1.13
			150	7.56	-3.64	-35.62	-5.21	3.54	1.13
566	Copertura	175, 39	0	-79.17	-1.35	69.99	-59.83	-1.87	3.96
			75	-79.17	-1.35	25.12	-59.83	-4.84	3.96
			150	-79.17	-1.35	-19.75	-59.83	-7.81	3.96
567	Copertura	40, 173	0	30.01	-3.66	-28.45	-26.14	8.64	3.54
			75	30.01	-3.66	-48.06	-26.14	5.98	3.54
			150	30.01	-3.66	-67.66	-26.14	3.32	3.54
568	Copertura	178, 41	0	-57.85	-1.33	102.43	-82.46	-0.98	6.58
			75	-57.85	-1.33	40.58	-82.46	-5.92	6.58
			150	-57.85	-1.33	-21.26	-82.46	-10.85	6.58
569	Copertura	42, 177	0	97.98	-3.66	-33.28	-43.28	12.32	6.37
			75	97.98	-3.66	-65.74	-43.28	7.55	6.37
			150	97.98	-3.66	-98.20	-43.28	2.77	6.37
570	Copertura	43, 181	0	57.49	-3.60	10.35	-92.89	19.72	12.92
			75	57.49	-3.60	-59.32	-92.89	10.03	12.92
			150	57.49	-3.60	-128.99	-92.89	0.34	12.92
571	Copertura	182, 44	0	-150.12	-1.38	127.48	-89.17	1.78	15.90
			75	-150.12	-1.38	60.61	-89.17	-10.15	15.90
			150	-150.12	-1.38	-6.27	-89.17	-22.08	15.90
572	Copertura	45, 185	0	128.52	-3.65	12.31	-115.64	24.80	18.06
			75	128.52	-3.65	-74.42	-115.64	11.26	18.06
			150	128.52	-3.65	-161.15	-115.64	-2.29	18.06
573	Copertura	186, 46	0	-125.04	-1.41	160.43	-113.78	3.76	18.82
			75	-125.04	-1.41	75.09	-113.78	-10.35	18.82
			150	-125.04	-1.41	-10.25	-113.78	-24.46	18.82
574	Copertura	47, 189	0	139.42	-3.75	11.39	-132.57	27.22	22.74
			75	139.42	-3.75	-88.04	-132.57	10.17	22.74
			150	139.42	-3.75	-187.47	-132.57	-6.89	22.74
575	Copertura	190, 48	0	-146.47	-1.60	188.87	-134.14	7.82	20.20
			75	-146.47	-1.60	88.26	-134.14	-7.33	20.20
			150	-146.47	-1.60	-12.35	-134.14	-22.47	20.20
576	Copertura	49, 193	0	147.74	-3.95	16.02	-148.65	26.17	26.61
			75	147.74	-3.95	-95.47	-148.65	6.21	26.61
			150	147.74	-3.95	-206.96	-148.65	-13.74	26.61
577	Copertura	195, 50	0	-157.89	-1.65	206.67	-147.23	14.44	21.18
			75	-157.89	-1.65	96.25	-147.23	-1.45	21.18
			150	-157.89	-1.65	-14.18	-147.23	-17.34	21.18

578	Copertura	51, 197	0	136.37	-4.20	13.99	-147.94	21.68	29.38
			75	136.37	-4.20	-96.96	-147.94	-0.35	29.38
			150	136.37	-4.20	-207.91	-147.94	-22.39	29.38
579	Copertura	199, 52	0	-154.83	-2.09	208.91	-149.74	22.44	20.22
			75	-154.83	-2.09	96.61	-149.74	7.27	20.22
			150	-154.83	-2.09	-15.70	-149.74	-7.89	20.22
580	Copertura	53, 201	0	115.79	-4.50	16.42	-137.29	15.27	31.34
			75	115.79	-4.50	-86.54	-137.29	-8.24	31.34
			150	115.79	-4.50	-189.51	-137.29	-31.74	31.34
581	Copertura	202, 54	0	-127.03	-2.11	191.36	-135.85	31.79	19.93
			75	-127.03	-2.11	89.47	-135.85	16.84	19.93
			150	-127.03	-2.11	-12.42	-135.85	1.90	19.93
582	Copertura	55, 205	0	117.16	-4.70	8.04	-104.14	13.02	34.91
			75	117.16	-4.70	-70.06	-104.14	-13.16	34.91
			150	117.16	-4.70	-148.16	-104.14	-39.34	34.91
583	Copertura	206, 56	0	-32.75	-2.47	158.18	-113.88	39.05	19.98
			75	-32.75	-2.47	72.77	-113.88	24.07	19.98
			150	-32.75	-2.47	-12.64	-113.88	9.09	19.98
584	Copertura	57, 75	0	266.24	-0.13	0.00	0.00	-9.02	-4.68
			118	266.24	-0.13	0.00	0.00	-3.51	-4.68
			235	266.24	-0.13	0.00	0.00	2.00	-4.68
585	Copertura	75, 58	0	-328.99	0.01	0.00	0.00	-2.36	-0.53
			118	-328.99	0.01	0.00	0.00	-1.73	-0.53
			235	-328.99	0.01	0.00	0.00	-1.11	-0.53
586	Copertura	77, 61	0	357.08	0.00	0.00	0.00	-0.54	-0.28
			115	357.08	0.00	0.00	0.00	-0.21	-0.28
			231	357.08	0.00	0.00	0.00	0.11	-0.28
587	Copertura	62, 77	0	-343.01	-0.08	0.00	0.00	0.63	0.24
			115	-343.01	-0.08	0.00	0.00	0.35	0.24
			231	-343.01	-0.08	0.00	0.00	0.07	0.24
588	Copertura	65, 78	0	344.32	-0.09	0.00	0.00	0.65	-0.04
			115	344.32	-0.09	0.00	0.00	0.70	-0.04
			231	344.32	-0.09	0.00	0.00	0.75	-0.04
589	Copertura	78, 66	0	-358.20	-0.07	0.00	0.00	-0.48	-0.02
			115	-358.20	-0.07	0.00	0.00	-0.46	-0.02
			231	-358.20	-0.07	0.00	0.00	-0.43	-0.02
590	Copertura	69, 76	0	346.90	-0.05	0.00	0.00	1.55	0.20
			118	346.90	-0.05	0.00	0.00	1.32	0.20
			235	346.90	-0.05	0.00	0.00	1.08	0.20
591	Copertura	76, 70	0	-288.93	-0.01	0.00	0.00	-0.37	-1.52
			118	-288.93	-0.01	0.00	0.00	1.42	-1.52
			235	-288.93	-0.01	0.00	0.00	3.20	-1.52
592	Copertura	79, 81	0	-16.89	-0.01	43.90	-54.59	3.06	3.08
			80	-16.89	-0.01	0.50	-54.59	0.61	3.08
			159	-16.89	-0.01	-42.90	-54.59	-1.84	3.08
593	Copertura	80, 82	0	-10.83	-0.15	35.58	-53.21	-0.64	0.55
			66	-10.83	-0.15	0.44	-53.21	-1.01	0.55
			132	-10.83	-0.15	-34.70	-53.21	-1.37	0.55
594	Copertura	83, 84	0	-0.34	0.00	32.63	-49.35	-1.02	-0.09
			66	-0.34	0.00	0.06	-49.35	-0.95	-0.09
			132	-0.34	0.00	-32.51	-49.35	-0.89	-0.09
595	Copertura	85, 86	0	-0.26	0.11	32.19	-48.68	-0.72	-0.35
			66	-0.26	0.11	0.06	-48.68	-0.49	-0.35
			132	-0.26	0.11	-32.07	-48.68	-0.26	-0.35
596	Copertura	87, 88	0	0.32	0.15	31.94	-48.35	-0.23	-0.35
			66	0.32	0.15	0.03	-48.35	0.00	-0.35
			132	0.32	0.15	-31.88	-48.35	0.23	-0.35
597	Copertura	89, 90	0	3.33	0.14	32.17	-48.86	-0.03	-0.16
			66	3.33	0.14	-0.08	-48.86	0.07	-0.16
			132	3.33	0.14	-32.32	-48.86	0.18	-0.16
598	Copertura	91, 92	0	4.07	0.13	31.56	-48.00	-0.13	-0.14
			66	4.07	0.13	-0.13	-48.00	-0.03	-0.14
			132	4.07	0.13	-31.81	-48.00	0.06	-0.14
599	Copertura	93, 94	0	-0.86	0.14	32.19	-48.85	-0.14	-0.27
			66	-0.86	0.14	-0.05	-48.85	0.04	-0.27
			132	-0.86	0.14	-32.30	-48.85	0.22	-0.27
600	Copertura	95, 96	0	-1.05	0.14	31.44	-47.59	-0.21	-0.44
			66	-1.05	0.14	0.03	-47.59	0.08	-0.44
			132	-1.05	0.14	-31.38	-47.59	0.37	-0.44
601	Copertura	97, 106	0	1.02	0.08	31.27	-47.33	0.47	-0.35
			66	1.02	0.08	0.03	-47.33	0.70	-0.35
			132	1.02	0.08	-31.21	-47.33	0.93	-0.35

602	Copertura	98, 99	0	-0.98	-0.05	46.89	-71.13	-0.85	0.45
			66	-0.98	-0.05	-0.05	-71.13	-1.14	0.45
			132	-0.98	-0.05	-47.00	-71.13	-1.43	0.45
603	Copertura	100, 101	0	-0.09	0.04	46.96	-71.11	-1.16	-0.57
			66	-0.09	0.04	0.03	-71.11	-0.79	-0.57
			132	-0.09	0.04	-46.90	-71.11	-0.41	-0.57
604	Copertura	102, 103	0	-0.83	0.09	46.72	-70.69	-0.93	-1.00
			66	-0.83	0.09	0.07	-70.69	-0.27	-1.00
			132	-0.83	0.09	-46.59	-70.69	0.39	-1.00
605	Copertura	104, 105	0	0.85	0.09	46.41	-70.26	-0.28	-0.53
			66	0.85	0.09	0.04	-70.26	0.06	-0.53
			132	0.85	0.09	-46.33	-70.26	0.41	-0.53
606	Copertura	107, 108	0	1.14	-0.07	32.26	-48.96	1.19	0.14
			66	1.14	-0.07	-0.06	-48.96	1.10	0.14
			132	1.14	-0.07	-32.37	-48.96	1.01	0.14
607	Copertura	109, 110	0	7.67	-0.21	28.85	-36.27	1.74	2.61
			80	7.67	-0.21	0.01	-36.27	-0.33	2.61
			159	7.67	-0.21	-28.82	-36.27	-2.41	2.61
608	Copertura	111, 112	0	7.65	0.09	46.48	-70.32	-0.11	-0.17
			66	7.65	0.09	0.03	-70.32	0.00	-0.17
			132	7.65	0.09	-46.42	-70.32	0.11	-0.17
609	Copertura	113, 114	0	1.19	0.09	46.56	-70.51	-0.22	-0.29
			66	1.19	0.09	0.02	-70.51	-0.03	-0.29
			132	1.19	0.09	-46.51	-70.51	0.16	-0.29
610	Copertura	115, 116	0	-1.38	0.09	46.86	-70.81	-0.11	-0.32
			66	-1.38	0.09	0.13	-70.81	0.10	-0.32
			132	-1.38	0.09	-46.60	-70.81	0.31	-0.32
611	Copertura	117, 118	0	0.16	0.08	46.47	-70.42	-0.11	-0.83
			66	0.16	0.08	-0.01	-70.42	0.44	-0.83
			132	0.16	0.08	-46.48	-70.42	0.98	-0.83
612	Copertura	119, 120	0	-0.06	0.01	46.74	-70.91	0.93	-0.16
			66	-0.06	0.01	-0.06	-70.91	1.04	-0.16
			132	-0.06	0.01	-46.86	-70.91	1.14	-0.16
613	Copertura	121, 122	0	1.90	-0.08	47.07	-71.11	1.77	1.06
			66	1.90	-0.08	0.14	-71.11	1.08	1.06
			132	1.90	-0.08	-46.79	-71.11	0.38	1.06
614	Copertura	124, 125	0	183.98	0.83	8.75	-5.18	-1.92	2.69
			99	183.98	0.83	3.61	-5.18	-4.60	2.69
			198	183.98	0.83	-1.53	-5.18	-7.27	2.69
615	Copertura	125, 127	0	-24.07	0.66	147.50	-19.71	-44.19	-5.58
			775	-24.07	0.66	-5.24	-19.71	-0.92	-5.58
			1550	-24.07	0.66	-157.99	-19.71	42.35	-5.58
616	Copertura	126, 127	0	-197.73	0.10	-8.86	5.26	-1.18	1.48
			99	-197.73	0.10	-3.64	5.26	-2.65	1.48
			198	-197.73	0.10	1.58	5.26	-4.11	1.48
617	Copertura	128, 129	0	240.20	0.85	11.07	-6.82	-2.01	2.45
			99	240.20	0.85	4.31	-6.82	-4.44	2.45
			198	240.20	0.85	-2.46	-6.82	-6.88	2.45
618	Copertura	129, 130	0	18.64	0.65	188.20	-24.47	-36.68	-4.62
			775	18.64	0.65	-1.44	-24.47	-0.84	-4.62
			1550	18.64	0.65	-191.08	-24.47	35.00	-4.62
619	Copertura	131, 130	0	-242.40	0.19	-11.16	6.87	-0.04	2.19
			99	-242.40	0.19	-4.34	6.87	-2.21	2.19
			198	-242.40	0.19	2.48	6.87	-4.39	2.19
620	Copertura	132, 135	0	260.61	0.91	12.06	-7.30	-2.21	2.07
			99	260.61	0.91	4.82	-7.30	-4.26	2.07
			198	260.61	0.91	-2.42	-7.30	-6.32	2.07
621	Copertura	133, 134	0	-259.42	0.23	-12.05	7.27	-0.84	1.35
			99	-259.42	0.23	-4.84	7.27	-2.18	1.35
			198	-259.42	0.23	2.37	7.27	-3.52	1.35
622	Copertura	135, 134	0	20.09	0.58	207.51	-26.79	-27.18	-3.42
			775	20.09	0.58	-0.09	-26.79	-0.66	-3.42
			1550	20.09	0.58	-207.69	-26.79	25.85	-3.42
623	Copertura	137, 136	0	263.80	0.95	12.18	-7.47	-2.38	1.73
			99	263.80	0.95	4.76	-7.47	-4.10	1.73
			198	263.80	0.95	-2.65	-7.47	-5.81	1.73
624	Copertura	136, 138	0	17.95	0.55	208.42	-26.90	-18.10	-2.27
			775	17.95	0.55	-0.06	-26.90	-0.47	-2.27
			1550	17.95	0.55	-208.54	-26.90	17.15	-2.27
625	Copertura	139, 138	0	-263.39	0.32	-12.19	7.47	0.13	1.74
			99	-263.39	0.32	-4.78	7.47	-1.60	1.74
			198	-263.39	0.32	2.64	7.47	-3.32	1.74

626	Copertura	140, 141	0	238.98	0.98	11.09	-6.71	-2.56	1.45
			99	238.98	0.98	4.43	-6.71	-3.99	1.45
			198	238.98	0.98	-2.23	-6.71	-5.43	1.45
627	Copertura	141, 142	0	19.67	0.50	190.88	-24.61	-10.84	-1.37
			775	19.67	0.50	0.14	-24.61	-0.24	-1.37
			1550	19.67	0.50	-190.60	-24.61	10.36	-1.37
628	Copertura	143, 142	0	-237.10	0.34	-11.10	6.68	-0.44	1.15
			99	-237.10	0.34	-4.47	6.68	-1.58	1.15
			198	-237.10	0.34	2.16	6.68	-2.72	1.15
629	Copertura	144, 145	0	209.19	0.99	9.73	-6.00	-2.74	1.24
			99	209.19	0.99	3.77	-6.00	-3.97	1.24
			198	209.19	0.99	-2.19	-6.00	-5.20	1.24
630	Copertura	145, 146	0	0.26	0.49	165.29	-21.41	-5.74	-0.72
			775	0.26	0.49	-0.64	-21.41	-0.15	-0.72
			1550	0.26	0.49	-166.57	-21.41	5.45	-0.72
631	Copertura	147, 146	0	-210.40	0.38	-9.70	5.95	0.01	1.34
			99	-210.40	0.38	-3.80	5.95	-1.31	1.34
			198	-210.40	0.38	2.10	5.95	-2.64	1.34
632	Copertura	148, 149	0	172.87	0.97	8.18	-4.98	-3.03	0.99
			99	172.87	0.97	3.24	-4.98	-4.02	0.99
			198	172.87	0.97	-1.70	-4.98	-5.00	0.99
633	Copertura	149, 150	0	15.50	0.47	127.30	-16.43	-1.54	-0.21
			775	15.50	0.47	-0.09	-16.43	0.11	-0.21
			1550	15.50	0.47	-127.49	-16.43	1.75	-0.21
634	Copertura	151, 150	0	-150.69	0.38	-7.26	4.33	-0.31	1.08
			99	-150.69	0.38	-2.96	4.33	-1.38	1.08
			198	-150.69	0.38	1.34	4.33	-2.45	1.08
635	Copertura	152, 153	0	135.97	0.96	6.48	-4.05	-3.19	0.93
			99	135.97	0.96	2.47	-4.05	-4.11	0.93
			198	135.97	0.96	-1.55	-4.05	-5.03	0.93
636	Copertura	153, 154	0	10.04	0.47	92.14	-11.98	0.10	-0.01
			775	10.04	0.47	-0.73	-11.98	0.17	-0.01
			1551	10.04	0.47	-93.59	-11.98	0.23	-0.01
637	Copertura	155, 154	0	-109.01	0.37	-5.25	3.24	-0.51	0.97
			99	-109.01	0.37	-2.04	3.24	-1.47	0.97
			198	-109.01	0.37	1.17	3.24	-2.44	0.97
638	Copertura	156, 157	0	95.70	0.95	4.62	-2.95	-3.26	0.92
			99	95.70	0.95	1.69	-2.95	-4.17	0.92
			198	95.70	0.95	-1.23	-2.95	-5.08	0.92
639	Copertura	157, 158	0	3.70	0.47	58.00	-7.48	0.51	0.05
			775	3.70	0.47	-0.04	-7.48	0.10	0.05
			1551	3.70	0.47	-58.08	-7.48	-0.30	0.05
640	Copertura	159, 158	0	-60.53	0.35	-3.09	1.80	-0.62	0.95
			99	-60.53	0.35	-1.31	1.80	-1.56	0.95
			198	-60.53	0.35	0.47	1.80	-2.51	0.95
641	Copertura	160, 161	0	58.43	0.95	2.88	-1.90	-3.30	0.92
			99	58.43	0.95	1.00	-1.90	-4.22	0.92
			198	58.43	0.95	-0.89	-1.90	-5.13	0.92
642	Copertura	161, 162	0	2.41	0.47	26.35	-3.48	0.51	0.07
			776	2.41	0.47	-0.61	-3.48	-0.05	0.07
			1551	2.41	0.47	-27.56	-3.48	-0.61	0.07
643	Copertura	163, 162	0	-25.05	0.33	-1.33	0.85	-0.93	0.76
			99	-25.05	0.33	-0.49	0.85	-1.68	0.76
			198	-25.05	0.33	0.36	0.85	-2.43	0.76
644	Copertura	164, 165	0	21.47	0.95	1.17	-0.86	-3.29	0.95
			99	21.47	0.95	0.31	-0.86	-4.23	0.95
			198	21.47	0.95	-0.54	-0.86	-5.17	0.95
645	Copertura	165, 166	0	0.66	0.48	-5.09	0.66	0.40	0.07
			776	0.66	0.48	0.05	0.66	-0.15	0.07
			1551	0.66	0.48	5.19	0.66	-0.71	0.07
646	Copertura	167, 166	0	20.78	0.33	0.68	-0.50	-0.93	0.84
			99	20.78	0.33	0.18	-0.50	-1.77	0.84
			198	20.78	0.33	-0.32	-0.50	-2.60	0.84
647	Copertura	168, 169	0	-14.72	0.95	-0.51	0.15	-3.24	0.98
			99	-14.72	0.95	-0.36	0.15	-4.21	0.98
			198	-14.72	0.95	-0.20	0.15	-5.18	0.98
648	Copertura	169, 170	0	-3.18	0.47	-35.82	4.54	0.25	0.05
			776	-3.18	0.47	-0.57	4.54	-0.17	0.05
			1552	-3.18	0.47	34.69	4.54	-0.59	0.05
649	Copertura	171, 170	0	54.43	0.33	2.38	-1.41	-0.88	0.79
			99	54.43	0.33	0.98	-1.41	-1.66	0.79
			198	54.43	0.33	-0.42	-1.41	-2.44	0.79

650	Copertura	172, 173	0	-51.97	0.97	-2.26	1.19	-3.15	1.02
			99	-51.97	0.97	-1.08	1.19	-4.17	1.02
			198	-51.97	0.97	0.10	1.19	-5.18	1.02
651	Copertura	173, 175	0	-7.30	0.47	-67.56	8.79	0.04	0.02
			776	-7.30	0.47	0.64	8.79	-0.12	0.02
			1552	-7.30	0.47	68.85	8.79	-0.28	0.02
652	Copertura	174, 175	0	101.51	0.34	4.47	-2.83	-0.81	0.79
			99	101.51	0.34	1.67	-2.83	-1.60	0.79
			198	101.51	0.34	-1.14	-2.83	-2.39	0.79
653	Copertura	176, 177	0	-83.21	0.97	-3.93	2.13	-3.04	1.08
			99	-83.21	0.97	-1.82	2.13	-4.11	1.08
			198	-83.21	0.97	0.29	2.13	-5.18	1.08
654	Copertura	177, 178	0	39.35	0.47	-97.91	12.83	-0.51	-0.07
			776	39.35	0.47	1.63	12.83	0.03	-0.07
			1552	39.35	0.47	101.18	12.83	0.57	-0.07
655	Copertura	179, 178	0	141.14	0.34	6.23	-3.77	-0.75	0.81
			99	141.14	0.34	2.49	-3.77	-1.55	0.81
			198	141.14	0.34	-1.25	-3.77	-2.35	0.81
656	Copertura	180, 181	0	-161.66	0.98	-7.37	4.46	-2.86	1.13
			99	-161.66	0.98	-2.95	4.46	-3.97	1.13
			198	-161.66	0.98	1.48	4.46	-5.09	1.13
657	Copertura	181, 182	0	-54.76	0.47	-127.51	16.35	-2.87	-0.40
			775	-54.76	0.47	-0.78	16.35	0.25	-0.40
			1550	-54.76	0.47	125.95	16.35	3.36	-0.40
658	Copertura	183, 182	0	155.89	0.36	7.45	-4.52	-0.31	1.06
			99	155.89	0.36	2.96	-4.52	-1.36	1.06
			198	155.89	0.36	-1.53	-4.52	-2.41	1.06
659	Copertura	184, 185	0	-201.22	0.99	-9.33	5.75	-2.71	1.24
			99	-201.22	0.99	-3.63	5.75	-3.94	1.24
			198	-201.22	0.99	2.08	5.75	-5.17	1.24
660	Copertura	185, 186	0	-7.66	0.48	-159.07	20.49	-5.55	-0.71
			775	-7.66	0.48	-0.27	20.49	-0.08	-0.71
			1550	-7.66	0.48	158.53	20.49	5.39	-0.71
661	Copertura	187, 186	0	198.53	0.36	9.27	-5.62	-0.31	1.09
			99	198.53	0.36	3.69	-5.62	-1.39	1.09
			198	198.53	0.36	-1.90	-5.62	-2.47	1.09
662	Copertura	188, 189	0	-231.55	0.98	-10.78	6.51	-2.55	1.42
			99	-231.55	0.98	-4.32	6.51	-3.96	1.42
			198	-231.55	0.98	2.14	6.51	-5.38	1.42
663	Copertura	189, 190	0	-12.78	0.51	-185.33	24.00	-10.31	-1.29
			775	-12.78	0.51	0.66	24.00	-0.30	-1.29
			1550	-12.78	0.51	186.64	24.00	9.72	-1.29
664	Copertura	191, 190	0	233.85	0.35	10.86	-6.59	0.06	1.45
			99	233.85	0.35	4.32	-6.59	-1.38	1.45
			198	233.85	0.35	-2.22	-6.59	-2.82	1.45
665	Copertura	192, 193	0	-258.76	0.95	-11.95	7.33	-2.38	1.69
			99	-258.76	0.95	-4.67	7.33	-4.06	1.69
			198	-258.76	0.95	2.60	7.33	-5.75	1.69
666	Copertura	193, 195	0	-17.10	0.53	-204.36	26.36	-17.46	-2.19
			775	-17.10	0.53	-0.09	26.36	-0.48	-2.19
			1550	-17.10	0.53	204.18	26.36	16.51	-2.19
667	Copertura	194, 195	0	256.67	0.29	11.92	-7.26	-0.62	1.19
			99	256.67	0.29	4.72	-7.26	-1.81	1.19
			198	256.67	0.29	-2.49	-7.26	-2.99	1.19
668	Copertura	196, 197	0	-258.11	0.91	-11.94	7.22	-2.20	2.05
			99	-258.11	0.91	-4.77	7.22	-4.24	2.05
			198	-258.11	0.91	2.40	7.22	-6.27	2.05
669	Copertura	197, 199	0	-20.19	0.59	-205.52	26.57	-26.53	-3.33
			775	-20.19	0.59	0.39	26.57	-0.70	-3.33
			1550	-20.19	0.59	206.30	26.57	25.13	-3.33
670	Copertura	198, 199	0	260.67	0.26	12.06	-7.39	0.11	1.96
			99	260.67	0.26	4.73	-7.39	-1.84	1.96
			198	260.67	0.26	-2.61	-7.39	-3.79	1.96
671	Copertura	200, 201	0	-238.86	0.85	-11.01	6.78	-2.01	2.43
			99	-238.86	0.85	-4.28	6.78	-4.42	2.43
			198	-238.86	0.85	2.46	6.78	-6.83	2.43
672	Copertura	201, 202	0	-18.35	0.62	-187.05	24.27	-36.34	-4.58
			775	-18.35	0.62	1.06	24.27	-0.82	-4.58
			1550	-18.35	0.62	189.17	24.27	34.70	-4.58
673	Copertura	203, 202	0	236.87	0.16	10.93	-6.61	-0.99	1.51
			99	236.87	0.16	4.37	-6.61	-2.49	1.51
			198	236.87	0.16	-2.19	-6.61	-3.99	1.51

674	Copertura	204, 205	0	-182.89	0.82	-8.74	5.18	-1.92	2.71
			99	-182.89	0.82	-3.60	5.18	-4.60	2.71
			198	-182.89	0.82	1.54	5.18	-7.29	2.71
675	Copertura	205, 206	0	34.84	0.69	-146.63	19.56	-44.31	-5.60
			775	34.84	0.69	4.93	19.56	-0.90	-5.60
			1550	34.84	0.69	156.49	19.56	42.51	-5.60
676	Copertura	207, 206	0	197.60	0.13	8.88	-5.32	-0.35	2.18
			99	197.60	0.13	3.60	-5.32	-2.52	2.18
			198	197.60	0.13	-1.69	-5.32	-4.68	2.18
677	Copertura	79	0	201.36	1.55	-27.40	43.37	-60.64	-65.82
			125	201.36	1.55	26.82	43.37	21.64	-65.82
			250	201.36	1.55	81.04	43.37	103.92	-65.82
678	Copertura	124	0	-122.48	0.45	40.95	-44.79	-127.62	-39.49
			155	-122.48	0.45	-28.47	-44.79	-66.41	-39.49
			310	-122.48	0.45	-97.89	-44.79	-5.20	-39.49
679	Copertura	80	0	42.46	0.71	6.36	36.90	-33.04	-43.70
			45	42.46	0.71	22.96	36.90	-13.38	-43.70
			90	42.46	0.71	39.57	36.90	6.29	-43.70
680	Copertura	128	0	102.85	0.28	41.00	-44.06	-159.53	-51.23
			155	102.85	0.28	-27.29	-44.06	-80.12	-51.23
			310	102.85	0.28	-95.58	-44.06	-0.71	-51.23
681	Copertura	82	0	-96.01	1.25	0.77	46.03	-42.02	-52.26
			43	-96.01	1.25	20.41	46.03	-19.73	-52.26
			85	-96.01	1.25	40.04	46.03	2.56	-52.26
682	Copertura	132	0	7.97	-0.15	41.07	-44.19	-174.34	-57.28
			155	7.97	-0.15	-27.42	-44.19	-85.55	-57.28
			310	7.97	-0.15	-95.91	-44.19	3.23	-57.28
683	Copertura	83	0	-7.99	-0.18	4.11	38.03	-45.72	-56.88
			43	-7.99	-0.18	20.33	38.03	-21.45	-56.88
			85	-7.99	-0.18	36.55	38.03	2.81	-56.88
684	Copertura	137	0	94.96	-0.51	41.04	-44.18	-174.81	-57.54
			155	94.96	-0.51	-27.45	-44.18	-85.62	-57.54
			310	94.96	-0.51	-95.93	-44.18	3.57	-57.54
685	Copertura	84	0	-65.92	0.14	3.81	38.04	-45.75	-57.32
			43	-65.92	0.14	20.04	38.04	-21.30	-57.32
			85	-65.92	0.14	36.27	38.04	3.15	-57.32
686	Copertura	140	0	5.45	-0.78	40.96	-44.14	-160.08	-52.51
			155	5.45	-0.78	-27.45	-44.14	-78.69	-52.51
			310	5.45	-0.78	-95.86	-44.14	2.71	-52.51
687	Copertura	85	0	8.81	-0.83	4.06	37.44	-42.06	-52.34
			43	8.81	-0.83	20.03	37.44	-19.73	-52.34
			85	8.81	-0.83	36.00	37.44	2.59	-52.34
688	Copertura	144	0	97.16	-0.98	40.90	-44.04	-138.83	-45.18
			155	97.16	-0.98	-27.37	-44.04	-68.80	-45.18
			310	97.16	-0.98	-95.64	-44.04	1.22	-45.18
689	Copertura	86	0	-53.47	-0.67	3.85	37.38	-36.22	-45.81
			43	-53.47	-0.67	19.79	37.38	-16.68	-45.81
			85	-53.47	-0.67	35.73	37.38	2.86	-45.81
690	Copertura	87	0	20.08	-0.99	3.84	37.48	-28.23	-35.06
			43	20.08	-0.99	19.83	37.48	-13.27	-35.06
			85	20.08	-0.99	35.82	37.48	1.68	-35.06
691	Copertura	148	0	-48.99	-1.14	41.93	-44.40	-107.22	-34.52
			155	-48.99	-1.14	-26.90	-44.40	-53.71	-34.52
			310	-48.99	-1.14	-95.73	-44.40	-0.20	-34.52
692	Copertura	88	0	-43.75	-0.99	4.00	36.83	-20.31	-25.82
			43	-43.75	-0.99	19.71	36.83	-9.30	-25.82
			85	-43.75	-0.99	35.42	36.83	1.71	-25.82
693	Copertura	152	0	0.88	-1.16	42.10	-44.80	-77.93	-24.63
			155	0.88	-1.16	-27.34	-44.80	-39.74	-24.63
			310	0.88	-1.16	-96.78	-44.80	-1.56	-24.63
694	Copertura	89	0	26.73	-0.88	2.89	39.68	-12.54	-16.06
			43	26.73	-0.88	19.81	39.68	-5.70	-16.06
			85	26.73	-0.88	36.74	39.68	1.15	-16.06
695	Copertura	156	0	14.01	-1.15	41.82	-44.51	-49.43	-15.18
			155	14.01	-1.15	-27.17	-44.51	-25.90	-15.18
			310	14.01	-1.15	-96.17	-44.51	-2.37	-15.18
696	Copertura	90	0	-38.54	-0.92	4.62	36.38	-5.19	-7.87
			43	-38.54	-0.92	20.13	36.38	-1.83	-7.87
			85	-38.54	-0.92	35.65	36.38	1.53	-7.87
697	Copertura	160	0	4.40	-1.13	41.53	-44.35	-22.84	-6.58
			155	4.40	-1.13	-27.20	-44.35	-12.64	-6.58
			310	4.40	-1.13	-95.94	-44.35	-2.43	-6.58

698	Copertura	91	0	32.43	-0.87	2.69	39.06	1.99	1.26
			43	32.43	-0.87	19.35	39.06	1.46	1.26
			85	32.43	-0.87	36.01	39.06	0.92	1.26
699	Copertura	164	0	-8.00	-1.12	41.17	-44.14	3.41	2.00
			155	-8.00	-1.12	-27.25	-44.14	0.32	2.00
			310	-8.00	-1.12	-95.66	-44.14	-2.77	2.00
700	Copertura	92	0	-31.39	-0.87	5.18	34.47	9.14	9.05
			43	-31.39	-0.87	19.88	34.47	5.28	9.05
			85	-31.39	-0.87	34.59	34.47	1.42	9.05
701	Copertura	168	0	-19.36	-1.12	40.72	-43.89	29.20	10.41
			155	-19.36	-1.12	-27.31	-43.89	13.07	10.41
			310	-19.36	-1.12	-95.34	-43.89	-3.06	10.41
702	Copertura	93	0	53.68	-0.91	3.96	36.75	16.21	18.65
			43	53.68	-0.91	19.64	36.75	8.25	18.65
			85	53.68	-0.91	35.31	36.75	0.30	18.65
703	Copertura	172	0	-8.56	-1.11	40.19	-43.71	55.97	19.03
			155	-8.56	-1.11	-27.55	-43.71	26.48	19.03
			310	-8.56	-1.11	-95.30	-43.71	-3.02	19.03
704	Copertura	94	0	3.45	-0.93	4.17	38.96	22.58	27.61
			43	3.45	-0.93	20.79	38.96	10.80	27.61
			85	3.45	-0.93	37.41	38.96	-0.98	27.61
705	Copertura	176	0	54.07	-1.07	39.58	-43.23	81.15	26.11
			155	54.07	-1.07	-27.43	-43.23	40.68	26.11
			310	54.07	-1.07	-94.43	-43.23	0.20	26.11
706	Copertura	180	0	-11.55	-1.03	40.68	-43.68	107.23	35.92
			155	-11.55	-1.03	-27.02	-43.68	51.55	35.92
			310	-11.55	-1.03	-94.73	-43.68	-4.13	35.92
707	Copertura	95	0	-24.28	-0.89	4.36	36.67	29.47	34.24
			43	-24.28	-0.89	20.01	36.67	14.87	34.24
			85	-24.28	-0.89	35.65	36.67	0.26	34.24
708	Copertura	184	0	-88.23	-0.96	40.78	-44.00	133.43	43.58
			155	-88.23	-0.96	-27.42	-44.00	65.88	43.58
			310	-88.23	-0.96	-95.61	-44.00	-1.66	43.58
709	Copertura	96	0	36.89	-0.90	3.93	38.10	35.22	43.50
			43	36.89	-0.90	20.18	38.10	16.66	43.50
			85	36.89	-0.90	36.43	38.10	-1.90	43.50
710	Copertura	188	0	6.22	-0.81	40.85	-43.98	155.58	50.76
			155	6.22	-0.81	-27.33	-43.98	76.90	50.76
			310	6.22	-0.81	-95.51	-43.98	-1.78	50.76
711	Copertura	97	0	0.45	-0.39	3.96	37.94	41.13	51.27
			43	0.45	-0.39	20.15	37.94	19.26	51.27
			85	0.45	-0.39	36.33	37.94	-2.61	51.27
712	Copertura	192	0	-93.26	-0.54	40.93	-44.07	171.55	56.36
			155	-93.26	-0.54	-27.37	-44.07	84.19	56.36
			310	-93.26	-0.54	-95.67	-44.07	-3.17	56.36
713	Copertura	106	0	68.18	-0.61	4.37	36.25	44.86	56.01
			43	68.18	-0.61	19.84	36.25	20.96	56.01
			85	68.18	-0.61	35.30	36.25	-2.93	56.01
714	Copertura	196	0	-7.04	-0.17	40.98	-44.09	172.66	56.75
			155	-7.04	-0.17	-27.36	-44.09	84.69	56.75
			310	-7.04	-0.17	-95.69	-44.09	-3.27	56.75
715	Copertura	107	0	61.03	0.67	3.84	38.77	45.66	56.57
			43	61.03	0.67	20.38	38.77	21.52	56.57
			85	61.03	0.67	36.91	38.77	-2.61	56.57
716	Copertura	200	0	-105.78	0.26	40.92	-43.97	158.56	50.95
			155	-105.78	0.26	-27.23	-43.97	79.59	50.95
			310	-105.78	0.26	-95.39	-43.97	0.62	50.95
717	Copertura	108	0	33.84	0.24	4.55	37.65	41.76	51.55
			43	33.84	0.24	20.61	37.65	19.77	51.55
			85	33.84	0.24	36.67	37.65	-2.22	51.55
718	Copertura	204	0	120.23	0.46	40.89	-44.72	126.96	39.36
			155	120.23	0.46	-28.42	-44.72	65.96	39.36
			310	120.23	0.46	-97.73	-44.72	4.96	39.36
719	Copertura	109	0	-42.72	1.86	4.56	43.51	29.44	42.74
			43	-42.72	1.86	23.12	43.51	11.21	42.74
			85	-42.72	1.86	41.68	43.51	-7.02	42.74
720	Copertura	110	0	-186.42	2.28	32.53	34.74	-45.60	64.94
			43	-186.42	2.28	47.35	34.74	-73.30	64.94
			85	-186.42	2.28	62.17	34.74	-101.00	64.94
721	Copertura	14	0	146.77	-1.50	-98.00	60.26	-179.86	-62.74
			95	146.77	-1.50	-40.74	60.26	-120.26	-62.74
			190	146.77	-1.50	16.51	60.26	-60.65	-62.74

722	Copertura	15	0	-246.88	1.37	93.78	-42.09	6.13	96.15
			65	-246.88	1.37	66.42	-42.09	-56.37	96.15
			130	-246.88	1.37	39.06	-42.09	-118.86	96.15
723	Copertura	16	0	176.97	0.34	-40.71	27.47	8.55	99.75
			65	176.97	0.34	-22.86	27.47	-56.28	99.75
			130	176.97	0.34	-5.01	27.47	-121.12	99.75
724	Copertura	17	0	-59.61	1.24	93.13	-41.60	15.10	125.82
			65	-59.61	1.24	66.08	-41.60	-66.68	125.82
			130	-59.61	1.24	39.04	-41.60	-148.46	125.82
725	Copertura	18	0	50.36	0.63	-48.07	35.89	15.12	126.32
			65	50.36	0.63	-24.74	35.89	-66.98	126.32
			130	50.36	0.63	-1.41	35.89	-149.09	126.32
726	Copertura	19	0	-168.23	0.93	93.69	-42.12	13.07	134.88
			65	-168.23	0.93	66.31	-42.12	-74.60	134.88
			130	-168.23	0.93	38.94	-42.12	-162.28	134.88
727	Copertura	20	0	189.19	-0.12	-48.02	36.04	12.11	133.86
			65	189.19	-0.12	-24.59	36.04	-74.89	133.86
			130	189.19	-0.12	-1.16	36.04	-161.90	133.86
728	Copertura	21	0	-83.45	0.67	93.95	-42.45	15.37	136.92
			65	-83.45	0.67	66.35	-42.45	-73.63	136.92
			130	-83.45	0.67	38.76	-42.45	-162.63	136.92
729	Copertura	22	0	90.48	0.10	-48.21	36.06	14.82	136.35
			65	90.48	0.10	-24.78	36.06	-73.80	136.35
			130	90.48	0.10	-1.34	36.06	-162.43	136.35
730	Copertura	23	0	-156.14	0.51	94.05	-42.69	11.82	123.69
			65	-156.14	0.51	66.30	-42.69	-68.58	123.69
			130	-156.14	0.51	38.55	-42.69	-148.98	123.69
731	Copertura	24	0	191.57	-0.41	-48.33	36.45	10.55	122.68
			65	191.57	-0.41	-24.63	36.45	-69.19	122.68
			130	191.57	-0.41	-0.94	36.45	-148.93	122.68
732	Copertura	25	0	-44.38	0.45	94.00	-42.81	12.57	108.97
			65	-44.38	0.45	66.18	-42.81	-58.27	108.97
			130	-44.38	0.45	38.36	-42.81	-129.10	108.97
733	Copertura	26	0	66.82	-0.26	-48.58	36.61	11.95	108.64
			65	66.82	-0.26	-24.78	36.61	-58.67	108.64
			130	66.82	-0.26	-0.98	36.61	-129.29	108.64
734	Copertura	27	0	144.38	-0.38	-49.07	37.53	-0.28	76.62
			65	144.38	-0.38	-24.67	37.53	-50.08	76.62
			130	144.38	-0.38	-0.27	37.53	-99.88	76.62
735	Copertura	28	0	-165.98	0.52	92.08	-40.80	21.56	92.81
			65	-165.98	0.52	65.56	-40.80	-38.77	92.81
			130	-165.98	0.52	39.04	-40.80	-99.09	92.81
736	Copertura	29	0	8.18	-0.33	-49.09	37.59	-2.10	54.26
			65	8.18	-0.33	-24.66	37.59	-37.37	54.26
			130	8.18	-0.33	-0.22	37.59	-72.64	54.26
737	Copertura	30	0	-91.23	0.62	92.48	-41.06	26.50	75.40
			65	-91.23	0.62	65.79	-41.06	-22.51	75.40
			130	-91.23	0.62	39.10	-41.06	-71.53	75.40
738	Copertura	31	0	89.13	-0.20	-49.09	37.61	-7.94	28.89
			65	89.13	-0.20	-24.64	37.61	-26.72	28.89
			130	89.13	-0.20	-0.20	37.61	-45.50	28.89
739	Copertura	32	0	-50.89	0.69	92.69	-41.43	26.78	55.14
			65	-50.89	0.69	65.76	-41.43	-9.06	55.14
			130	-50.89	0.69	38.83	-41.43	-44.90	55.14
740	Copertura	33	0	-43.20	-0.15	-46.91	34.69	-7.66	10.50
			65	-43.20	-0.15	-24.36	34.69	-14.49	10.50
			130	-43.20	-0.15	-1.82	34.69	-21.32	10.50
741	Copertura	34	0	-35.30	0.74	93.11	-41.96	27.09	36.27
			65	-35.30	0.74	65.84	-41.96	3.52	36.27
			130	-35.30	0.74	38.56	-41.96	-20.06	36.27
742	Copertura	35	0	41.00	-0.14	-50.04	38.48	-14.23	-14.04
			65	41.00	-0.14	-25.03	38.48	-5.11	-14.04
			130	41.00	-0.14	-0.02	38.48	4.02	-14.04
743	Copertura	36	0	-22.71	0.74	93.64	-42.60	27.36	17.61
			65	-22.71	0.74	65.95	-42.60	15.92	17.61
			130	-22.71	0.74	38.26	-42.60	4.47	17.61
744	Copertura	37	0	-90.61	-0.13	-46.83	34.93	-13.40	-31.25
			65	-90.61	-0.13	-24.12	34.93	6.91	-31.25
			130	-90.61	-0.13	-1.42	34.93	27.22	-31.25
745	Copertura	38	0	-9.60	0.70	94.27	-43.36	27.74	-0.65
			65	-9.60	0.70	66.09	-43.36	28.16	-0.65
			130	-9.60	0.70	37.90	-43.36	28.58	-0.65

746	Copertura	39	0	6.71	-0.22	-46.78	34.77	-19.61	-56.08
			65	6.71	-0.22	-24.18	34.77	16.85	-56.08
			130	6.71	-0.22	-1.58	34.77	53.30	-56.08
747	Copertura	40	0	26.37	0.64	95.14	-44.35	28.28	-19.47
			65	26.37	0.64	66.32	-44.35	40.94	-19.47
			130	26.37	0.64	37.50	-44.35	53.59	-19.47
748	Copertura	41	0	-113.79	-0.26	-46.06	33.83	-20.63	-76.48
			65	-113.79	-0.26	-24.07	33.83	29.09	-76.48
			130	-113.79	-0.26	-2.07	33.83	78.80	-76.48
749	Copertura	42	0	110.17	0.58	95.54	-45.00	31.13	-35.36
			65	110.17	0.58	66.28	-45.00	54.11	-35.36
			130	110.17	0.58	37.03	-45.00	77.10	-35.36
750	Copertura	43	0	97.70	0.49	93.39	-42.56	-8.45	-83.32
			65	97.70	0.49	65.73	-42.56	45.70	-83.32
			130	97.70	0.49	38.07	-42.56	99.86	-83.32
751	Copertura	44	0	-106.58	-0.37	-46.93	35.29	-6.73	-80.72
			65	-106.58	-0.37	-23.99	35.29	45.74	-80.72
			130	-106.58	-0.37	-1.06	35.29	98.21	-80.72
752	Copertura	45	0	47.90	0.44	93.84	-42.76	-12.04	-104.72
			65	47.90	0.44	66.05	-42.76	56.03	-104.72
			130	47.90	0.44	38.26	-42.76	124.10	-104.72
753	Copertura	46	0	-120.21	-0.43	-47.43	35.80	-10.10	-103.24
			65	-120.21	-0.43	-24.16	35.80	57.01	-103.24
			130	-120.21	-0.43	-0.89	35.80	124.11	-103.24
754	Copertura	47	0	162.79	0.48	93.77	-42.56	-11.14	-119.96
			65	162.79	0.48	66.10	-42.56	66.83	-119.96
			130	162.79	0.48	38.44	-42.56	144.80	-119.96
755	Copertura	48	0	-134.60	-0.16	-47.41	35.63	-11.66	-120.65
			65	-134.60	-0.16	-24.26	35.63	66.76	-120.65
			130	-134.60	-0.16	-1.10	35.63	145.19	-120.65
756	Copertura	49	0	81.75	0.64	93.73	-42.37	-15.09	-134.38
			65	81.75	0.64	66.19	-42.37	72.26	-134.38
			130	81.75	0.64	38.65	-42.37	159.60	-134.38
757	Copertura	50	0	-128.99	-0.33	-47.80	36.13	-13.54	-133.02
			65	-128.99	-0.33	-24.31	36.13	72.92	-133.02
			130	-128.99	-0.33	-0.82	36.13	159.38	-133.02
758	Copertura	51	0	167.46	0.90	93.50	-42.04	-12.93	-133.57
			65	167.46	0.90	66.17	-42.04	73.89	-133.57
			130	167.46	0.90	38.85	-42.04	160.71	-133.57
759	Copertura	52	0	-93.32	0.36	-47.71	35.60	-14.80	-135.26
			65	-93.32	0.36	-24.57	35.60	73.12	-135.26
			130	-93.32	0.36	-1.42	35.60	161.04	-135.26
760	Copertura	53	0	55.78	1.22	92.96	-41.54	-15.09	-125.11
			65	55.78	1.22	65.96	-41.54	66.23	-125.11
			130	55.78	1.22	38.96	-41.54	147.56	-125.11
761	Copertura	54	0	-148.43	0.12	-47.27	35.39	-11.88	-122.20
			65	-148.43	0.12	-24.27	35.39	67.55	-122.20
			130	-148.43	0.12	-1.27	35.39	146.98	-122.20
762	Copertura	55	0	243.93	1.37	93.62	-42.01	-5.87	-95.46
			65	243.93	1.37	66.31	-42.01	56.18	-95.46
			130	243.93	1.37	39.01	-42.01	118.23	-95.46
763	Copertura	56	0	-141.32	0.67	-47.36	35.55	-10.32	-101.55
			65	-141.32	0.67	-24.25	35.55	55.69	-101.55
			130	-141.32	0.67	-1.14	35.55	121.70	-101.55
764	Copertura	70	0	-150.15	-0.13	-89.08	42.41	175.69	62.33
			95	-150.15	-0.13	-48.79	42.41	116.48	62.33
			190	-150.15	-0.13	-8.50	42.41	57.26	62.33
765	Copertura	81	0	-11.10	1.35	-31.39	45.83	-102.26	-43.15
			80	-11.10	1.35	5.27	45.83	-67.74	-43.15
			160	-11.10	1.35	41.94	45.83	-33.22	-43.15
766	Copertura	126	0	43.50	-0.48	-5.86	28.94	-129.98	-46.23
			30	43.50	-0.48	2.82	28.94	-116.11	-46.23
			60	43.50	-0.48	11.51	28.94	-102.24	-46.23
767	Copertura	98	0	-42.45	-0.12	-25.63	37.10	-128.78	-52.80
			82	-42.45	-0.12	4.92	37.10	-85.30	-52.80
			165	-42.45	-0.12	35.47	37.10	-41.82	-52.80
768	Copertura	99	0	-57.34	0.83	-26.45	38.37	-139.55	-56.98
			82	-57.34	0.83	5.14	38.37	-92.63	-56.98
			165	-57.34	0.83	36.74	38.37	-45.72	-56.98
769	Copertura	100	0	-16.57	-0.75	-25.77	37.70	-139.99	-57.22
			82	-16.57	-0.75	5.28	37.70	-92.87	-57.22
			165	-16.57	-0.75	36.32	37.70	-45.75	-57.22

770	Copertura	101	0	-39.87	-0.11	-25.83	37.69	-128.72	-52.69
			82	-39.87	-0.11	5.21	37.69	-85.33	-52.69
			165	-39.87	-0.11	36.25	37.69	-41.95	-52.69
771	Copertura	102	0	-4.78	-0.93	-25.21	37.12	-111.21	-45.46
			82	-4.78	-0.93	5.35	37.12	-73.77	-45.46
			165	-4.78	-0.93	35.92	37.12	-36.33	-45.46
772	Copertura	103	0	-28.27	-0.75	-25.41	37.16	-86.40	-35.42
			82	-28.27	-0.75	5.19	37.16	-57.24	-35.42
			165	-28.27	-0.75	35.79	37.16	-28.08	-35.42
773	Copertura	104	0	4.60	-0.75	-25.31	37.15	-62.40	-25.47
			82	4.60	-0.75	5.28	37.15	-41.43	-25.47
			165	4.60	-0.75	35.88	37.15	-20.46	-25.47
774	Copertura	105	0	-22.13	-0.85	-24.79	36.34	-39.11	-16.21
			82	-22.13	-0.85	5.13	36.34	-25.76	-16.21
			165	-22.13	-0.85	35.06	36.34	-12.41	-16.21
775	Copertura	111	0	10.32	-0.74	-26.42	39.72	-17.63	-7.71
			80	10.32	-0.74	5.26	39.72	-11.48	-7.71
			160	10.32	-0.74	36.94	39.72	-5.32	-7.71
776	Copertura	112	0	-15.57	-0.75	-23.38	34.99	3.98	1.12
			82	-15.57	-0.75	5.43	34.99	3.05	1.12
			165	-15.57	-0.75	34.24	34.99	2.13	1.12
777	Copertura	113	0	16.61	-0.80	-26.48	38.54	24.13	9.19
			82	16.61	-0.80	5.25	38.54	16.57	9.19
			165	16.61	-0.80	36.99	38.54	9.00	9.19
778	Copertura	114	0	4.82	-0.77	-25.79	37.61	46.62	18.38
			82	4.82	-0.77	5.18	37.61	31.49	18.38
			165	4.82	-0.77	36.15	37.61	16.35	18.38
779	Copertura	115	0	52.31	-0.71	-26.28	38.10	68.36	27.88
			82	52.31	-0.71	5.09	38.10	45.40	27.88
			165	52.31	-0.71	36.47	38.10	22.44	27.88
780	Copertura	116	0	-71.87	-0.68	-26.33	37.73	85.28	33.80
			82	-71.87	-0.68	4.73	37.73	57.44	33.80
			165	-71.87	-0.68	35.80	37.73	29.61	33.80
781	Copertura	117	0	84.48	-0.54	-25.70	37.05	107.43	43.94
			82	84.48	-0.54	4.80	37.05	71.25	43.94
			165	84.48	-0.54	35.31	37.05	35.08	43.94
782	Copertura	118	0	-46.88	-0.86	-25.56	36.92	125.07	50.93
			82	-46.88	-0.86	4.83	36.92	83.14	50.93
			165	-46.88	-0.86	35.23	36.92	41.20	50.93
783	Copertura	131	0	-113.58	0.73	-1.59	38.08	-160.25	-52.36
			30	-113.58	0.73	9.84	38.08	-144.54	-52.36
			60	-113.58	0.73	21.26	38.08	-128.83	-52.36
784	Copertura	133	0	13.79	-0.60	-1.89	37.39	-173.96	-57.42
			30	13.79	-0.60	9.33	37.39	-156.73	-57.42
			60	13.79	-0.60	20.55	37.39	-139.50	-57.42
785	Copertura	139	0	-87.67	0.41	-1.49	37.80	-174.63	-57.79
			30	-87.67	0.41	9.85	37.80	-157.29	-57.79
			60	-87.67	0.41	21.19	37.80	-139.95	-57.79
786	Copertura	143	0	31.23	-0.52	-1.48	37.60	-160.04	-52.12
			30	31.23	-0.52	9.80	37.60	-144.40	-52.12
			60	31.23	-0.52	21.08	37.60	-128.76	-52.12
787	Copertura	147	0	-75.47	0.00	-1.26	37.95	-138.99	-46.46
			30	-75.47	0.00	10.12	37.95	-125.05	-46.46
			60	-75.47	0.00	21.51	37.95	-111.12	-46.46
788	Copertura	151	0	42.42	-0.37	-0.62	36.33	-107.14	-34.42
			30	42.42	-0.37	10.28	36.33	-96.82	-34.42
			60	42.42	-0.37	21.18	36.33	-86.49	-34.42
789	Copertura	155	0	-65.66	-0.47	-0.69	36.31	-77.91	-25.99
			30	-65.66	-0.47	10.21	36.31	-70.11	-25.99
			60	-65.66	-0.47	21.10	36.31	-62.31	-25.99
790	Copertura	159	0	48.13	-0.44	-0.77	37.19	-48.61	-15.69
			30	48.13	-0.44	10.39	37.19	-43.90	-15.69
			60	48.13	-0.44	21.54	37.19	-39.20	-15.69
791	Copertura	119	0	115.51	0.32	-25.80	37.27	137.59	56.35
			82	115.51	0.32	4.89	37.27	91.18	56.35
			165	115.51	0.32	35.58	37.27	44.78	56.35
792	Copertura	120	0	12.07	-0.53	-25.87	37.62	138.98	56.72
			82	12.07	-0.53	5.12	37.62	92.28	56.72
			165	12.07	-0.53	36.10	37.62	45.58	56.72
793	Copertura	121	0	82.80	1.25	-26.97	38.80	126.51	51.41
			82	82.80	1.25	4.97	38.80	84.17	51.41
			165	82.80	1.25	36.92	38.80	41.84	51.41

794	Copertura	122	0	-78.98	0.12	-25.61	35.84	103.92	45.35
			82	-78.98	0.12	3.90	35.84	66.58	45.35
			165	-78.98	0.12	33.41	35.84	29.24	45.35
795	Copertura	123	0	-150.15	-0.13	-8.50	42.41	57.26	62.33
			82	-150.15	-0.13	26.43	42.41	5.94	62.33
			165	-150.15	-0.13	61.35	42.41	-45.39	62.33
796	Copertura	163	0	-60.24	-0.63	-2.63	34.82	-22.67	-7.88
			33	-60.24	-0.63	8.71	34.82	-20.10	-7.88
			65	-60.24	-0.63	20.06	34.82	-17.54	-7.88
797	Copertura	167	0	55.00	-0.63	-0.90	39.89	4.67	1.29
			30	55.00	-0.63	11.07	39.89	4.28	1.29
			60	55.00	-0.63	23.03	39.89	3.89	1.29
798	Copertura	171	0	-53.90	-0.58	-2.33	37.35	29.56	8.90
			30	-53.90	-0.58	8.87	37.35	26.89	8.90
			60	-53.90	-0.58	20.08	37.35	24.22	8.90
799	Copertura	174	0	75.33	-0.61	-2.56	38.80	57.73	18.67
			30	75.33	-0.61	9.08	38.80	52.13	18.67
			60	75.33	-0.61	20.72	38.80	46.53	18.67
800	Copertura	179	0	-18.50	-0.60	-3.11	39.48	84.99	27.56
			30	-18.50	-0.60	8.74	39.48	76.72	27.56
			60	-18.50	-0.60	20.58	39.48	68.45	27.56
801	Copertura	183	0	-1.07	-0.37	-1.54	36.34	105.66	34.12
			30	-1.07	-0.37	9.37	36.34	95.42	34.12
			60	-1.07	-0.37	20.27	36.34	85.19	34.12
802	Copertura	187	0	14.06	-0.43	-1.37	36.89	133.37	43.11
			30	14.06	-0.43	9.70	36.89	120.44	43.11
			60	14.06	-0.43	20.77	36.89	107.51	43.11
803	Copertura	191	0	23.53	0.12	-1.32	37.08	156.05	51.75
			30	23.53	0.12	9.80	37.08	140.52	51.75
			60	23.53	0.12	20.92	37.08	125.00	51.75
804	Copertura	194	0	44.60	-0.61	-1.45	37.33	171.31	56.19
			30	44.60	-0.61	9.75	37.33	154.45	56.19
			60	44.60	-0.61	20.94	37.33	137.59	56.19
805	Copertura	198	0	82.98	0.62	-1.55	37.57	173.11	56.88
			30	82.98	0.62	9.72	37.57	156.04	56.88
			60	82.98	0.62	20.99	37.57	138.98	56.88
806	Copertura	203	0	11.69	-0.53	-2.04	36.90	157.91	52.47
			30	11.69	-0.53	9.03	36.90	142.17	52.47
			60	11.69	-0.53	20.10	36.90	126.42	52.47
807	Copertura	207	0	-7.88	0.50	-1.46	37.74	130.58	44.29
			30	-7.88	0.50	9.86	37.74	117.29	44.29
			60	-7.88	0.50	21.18	37.74	104.00	44.29

1.1.6.2 Piastre SLV

Tabella 12.I

Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	0.246	-0.993	0.447	-102.009	51.211	35.626	1.308	1.196
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	1.588	0.968	-0.847	195.908	75.334	86.470	2.875	-2.356
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13,	-1.647	0.827	-1.100	-206.158	66.242	100.368	3.200	-2.438

		12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2								
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1.1.7 Risultati Condizioni (Sisma X).

1.1.7.1 Sollecitazioni SLV

Tabella 13.I

Sollecitazioni									
Asta	Imp.	Fili	X [cm]	N [daN]	Mt [daNm]	Mxz [daNm]	Txz [daN]	Mxy [daNm]	Txy [daN]
1	Fondazio ne	1, 2	0	-167.36	127.72	339.82	517.84	-18.17	67.39
			42	280.54	127.71	315.69	234.44	-14.79	35.80
			83	481.78	127.70	324.16	223.15	-20.29	-113.76
2	Fondazio ne	1, 2	0	-138.73	91.63	380.44	-190.54	-20.83	-104.37
			42	277.05	91.62	373.32	131.06	-11.97	33.62
			83	485.99	91.61	422.42	-362.86	-15.79	-60.82
3	Fondazio ne	1, 15	0	-89.29	-258.44	171.99	-536.10	-33.32	-223.11
			40	101.39	-258.44	103.16	-330.33	27.61	-105.19
			80	-149.33	-258.45	-120.83	-336.33	-53.34	254.90
4	Fondazio ne	1, 15	0	-155.87	-573.28	195.09	-382.66	-53.36	-222.39
			40	-169.85	-573.30	-73.75	-481.32	16.03	68.82
			80	-210.61	-573.34	-236.35	-844.74	-54.43	261.74
5	Fondazio ne	2, 3	0	231.38	158.52	511.50	-717.10	-15.03	59.05
			35	380.65	158.51	320.85	-577.66	-7.88	-19.38
			69	553.45	158.51	221.58	-446.25	-7.72	-62.05
6	Fondazio ne	2, 3	0	-225.12	142.65	251.46	-492.54	-8.14	-43.87
			35	362.52	142.65	175.98	382.66	-7.46	23.92
			69	532.89	142.65	113.83	345.85	-21.30	-62.68
7	Fondazio ne	3, 4	0	-227.91	86.72	130.11	-329.77	24.11	72.86
			35	346.52	86.72	114.44	-234.45	-6.70	34.57
			69	516.42	86.71	98.22	173.61	4.93	-33.07
8	Fondazio ne	3, 4	0	224.17	-63.88	-94.76	208.91	4.86	33.45
			35	322.80	-63.88	76.93	175.36	-4.31	26.10
			69	491.87	-63.88	55.55	186.12	-16.95	-55.97
9	Fondazio ne	4, 5	0	214.61	103.17	52.36	-184.28	-13.62	41.44
			35	284.71	103.17	64.14	155.23	-5.39	-14.60
			69	452.17	103.17	-86.64	145.29	6.91	-32.08
10	Fondazio ne	4, 5	0	242.08	78.76	-63.95	131.47	7.29	56.24
			35	254.72	78.76	-79.16	139.84	-8.29	30.92
			69	409.85	78.76	-93.07	156.99	16.56	25.65
11	Fondazio ne	5, 6	0	-282.08	132.65	-58.55	233.42	15.95	26.83
			35	243.41	132.65	-84.76	232.20	-7.66	-28.83
			69	382.03	132.65	-130.34	240.60	5.51	-45.92
12	Fondazio ne	5, 6	0	343.94	61.33	-104.80	-295.62	5.93	30.43
			35	252.51	61.33	-176.61	-309.99	-2.22	16.04
			69	373.41	61.33	-259.57	-327.00	-8.14	-22.56
13	Fondazio ne	6, 7	0	-201.96	38.88	-246.56	321.33	-11.10	-30.54
			35	194.28	38.88	-122.36	304.33	-2.50	-20.44
			69	365.48	38.88	-39.11	293.63	-4.79	-21.34
14	Fondazio ne	6, 7	0	-273.48	57.80	-28.77	312.81	-4.36	31.69
			35	191.01	57.80	124.59	309.42	-5.77	26.26
			69	343.97	57.80	252.78	312.29	-14.54	29.29
15	Fondazio ne	7, 8	0	-224.15	92.35	263.32	-361.68	-7.70	-15.15

			35	201.18	92.35	165.05	-353.18	-4.44	-12.62
			69	335.53	92.35	72.01	-345.43	3.34	-25.23
16	Fondazio ne	7, 8	0	-261.30	111.87	107.88	-270.13	3.28	19.02
			35	-156.57	111.87	43.40	-265.66	-4.57	16.19
			69	288.97	111.87	-50.48	-265.86	-11.13	-29.85
17	Fondazio ne	8, 9	0	-311.61	98.23	55.34	-284.72	-14.12	40.73
			35	-171.94	98.23	-36.18	-289.74	-4.30	-22.98
			69	257.45	98.23	-103.03	-300.06	3.57	-19.03
18	Fondazio ne	8, 9	0	-364.05	76.96	-58.07	-355.21	3.72	18.88
			35	-209.03	76.97	-151.36	-370.10	1.54	-15.80
			69	253.04	76.97	-254.96	-387.31	10.08	-41.62
19	Fondazio ne	9, 10	0	-349.95	-85.99	-244.28	344.97	8.63	27.53
			35	-223.43	-85.99	-124.19	329.56	3.01	17.65
			69	308.71	-85.99	62.21	318.76	-7.90	40.29
20	Fondazio ne	9, 10	0	-398.63	66.25	63.68	294.10	-7.41	-62.46
			35	-224.12	66.25	134.11	288.63	9.21	-32.63
			69	255.55	66.25	255.07	289.67	16.55	-20.83
21	Fondazio ne	10, 11	0	-393.34	-112.11	258.49	261.70	11.69	22.70
			35	-284.29	-112.10	197.13	261.64	8.13	23.77
			69	368.97	-112.10	142.11	266.18	-7.11	62.71
22	Fondazio ne	10, 11	0	-431.58	107.01	151.86	194.07	-6.66	44.00
			35	-273.91	107.01	123.37	206.53	5.07	-16.59
			69	305.73	107.02	84.11	-230.65	15.34	53.77
23	Fondazio ne	11, 12	0	-475.46	-69.13	102.81	248.88	18.56	-68.72
			35	-296.42	-69.13	-118.43	231.10	4.30	26.90
			69	-281.95	-69.13	125.70	255.37	-3.88	42.32
24	Fondazio ne	11, 12	0	-510.21	109.57	-115.35	220.31	-3.78	-38.85
			35	-329.07	109.58	140.42	-271.59	5.65	-34.02
			69	-259.79	109.58	-150.91	-349.47	25.33	84.51
25	Fondazio ne	12, 13	0	-545.03	132.36	-116.44	379.22	22.18	-74.29
			35	-362.55	132.36	-201.65	386.19	6.64	21.49
			69	234.02	132.36	-266.26	-450.34	9.96	57.21
26	Fondazio ne	12, 13	0	-573.75	176.31	-219.14	-434.69	9.55	-74.80
			35	-391.03	176.32	-324.00	-524.38	7.85	-20.39
			69	223.92	176.33	-496.35	-647.01	16.12	-67.86
27	Fondazio ne	13, 14	0	-493.62	89.63	-426.03	498.97	15.03	71.47
			42	-272.99	89.63	-379.22	178.08	12.33	35.24
			83	142.33	89.64	-381.59	176.33	24.47	117.44
28	Fondazio ne	13, 14	0	-480.38	120.43	-307.46	245.95	23.96	127.97
			42	-278.63	120.43	-324.93	185.10	16.82	40.07
			83	155.76	120.44	-365.97	606.31	17.22	76.23
29	Fondazio ne	14, 16	0	90.83	-252.30	-153.82	687.35	-31.40	-223.18
			40	-107.71	-252.31	131.37	330.91	29.77	-104.57
			80	172.42	-252.32	127.66	328.68	-56.87	270.66
30	Fondazio ne	14, 16	0	140.27	-614.82	-180.01	368.21	-56.94	-242.25
			40	147.32	-614.83	90.69	484.10	16.19	98.04
			80	222.05	-614.86	233.24	978.81	-64.32	273.49
31	Fondazio ne	15, 17	0	-247.96	-223.36	167.77	-411.24	-67.89	-300.22
			33	-254.00	-223.39	-69.11	-299.47	7.64	-137.51
			66	-260.53	-223.42	-87.50	-401.93	52.91	211.25
32	Fondazio ne	15, 17	0	-230.78	-892.17	230.11	-485.19	53.23	-226.71
			33	-236.82	-892.20	70.42	-719.20	12.92	143.31
			66	-244.48	-892.25	-277.73	-1075.64	-62.66	292.08
33	Fondazio ne	16, 18	0	217.42	-303.40	-172.51	609.76	-79.17	-326.81
			33	243.03	-303.43	76.55	340.37	8.66	-190.00

			66	291.81	-303.46	80.04	397.66	57.93	225.71
34	Fondazio ne	16, 18	0	211.82	-898.47	-199.77	390.71	58.08	-235.26
			33	231.83	-898.49	-53.97	703.84	13.92	202.11
			66	279.97	-898.53	295.01	1145.30	-83.05	320.91
35	Fondazio ne	17, 19	0	-214.44	193.43	194.74	455.91	-89.02	-342.11
			33	-220.68	193.47	91.66	-359.89	12.04	-206.59
			66	-227.47	193.51	-109.65	-493.45	66.80	-281.64
36	Fondazio ne	17, 19	0	-191.01	-989.95	251.86	-565.20	66.87	284.64
			33	-193.43	-990.00	91.55	-943.67	10.91	194.56
			66	-207.72	-990.07	-445.96	-1374.25	-80.55	323.92
37	Fondazio ne	18, 20	0	193.05	371.79	-221.58	562.72	-110.34	-373.86
			33	196.17	371.83	-85.44	332.05	13.59	-266.81
			66	236.89	371.88	102.89	498.91	73.84	-278.52
38	Fondazio ne	18, 20	0	179.38	-1031.49	-221.54	477.43	73.98	269.64
			33	180.87	-1031.54	-107.79	938.25	9.95	244.48
			66	197.40	-1031.59	478.28	1445.93	-94.75	345.25
39	Fondazio ne	19, 21	0	-203.24	258.15	223.97	685.47	-83.50	-339.75
			33	-205.79	258.10	101.39	-251.30	14.52	-217.62
			66	-208.98	258.05	-85.97	-426.13	80.22	-311.88
40	Fondazio ne	19, 21	0	-212.91	-1157.26	244.75	-521.07	80.31	302.79
			33	-212.02	-1157.33	-91.55	-874.57	14.00	213.08
			66	-245.32	-1157.40	-421.39	-1337.72	-76.84	329.40
41	Fondazio ne	20, 22	0	198.85	334.29	-291.13	865.78	-93.40	-365.20
			33	198.56	334.24	-114.08	368.88	12.36	-247.40
			66	218.09	334.20	86.06	462.15	79.57	-284.94
42	Fondazio ne	20, 22	0	233.79	-1143.80	-221.71	505.65	79.70	263.30
			33	245.80	-1143.87	-70.43	887.60	12.75	227.46
			66	260.61	-1143.94	388.72	1400.00	-82.21	359.52
43	Fondazio ne	21, 23	0	-235.25	451.56	-283.81	825.93	-114.80	-420.02
			33	-237.89	451.48	-98.91	-332.11	13.01	-296.57
			66	-263.87	451.42	-72.25	-307.28	91.98	-359.52
44	Fondazio ne	21, 23	0	-275.90	-1302.86	222.02	-502.71	92.12	378.93
			33	-282.77	-1302.93	-132.94	-933.03	-18.44	323.14
			66	-313.94	-1303.01	-495.85	-1461.25	-133.13	444.20
45	Fondazio ne	22, 24	0	254.41	464.02	-223.58	838.89	-117.05	-431.91
			33	268.52	463.95	-70.32	297.80	9.67	-292.40
			66	283.88	463.89	61.79	367.53	89.29	-313.49
46	Fondazio ne	22, 24	0	307.64	-1257.88	-218.50	472.22	89.38	311.23
			33	321.10	-1257.96	-87.16	935.35	-10.80	295.82
			66	335.74	-1258.04	455.04	1528.37	-125.68	448.44
47	Fondazio ne	23, 25	0	-254.72	915.15	-427.28	1299.47	-138.64	-444.98
			33	-274.86	915.06	-100.12	772.18	-19.39	-338.92
			66	-318.57	914.99	132.67	306.69	94.07	-386.19
48	Fondazio ne	23, 25	0	-250.96	-740.47	162.96	-256.21	94.18	308.68
			33	-258.49	-740.55	-100.48	-706.26	26.34	249.07
			66	-282.34	-740.64	-376.47	-1256.70	-74.73	344.65
49	Fondazio ne	24, 26	0	296.57	773.11	339.08	-1251.84	-127.86	-460.13
			33	311.08	773.03	-74.47	-678.29	-10.53	-302.47
			66	326.71	772.95	-121.41	246.24	88.61	-324.39
50	Fondazio ne	24, 26	0	290.50	-955.53	-268.31	458.65	88.72	275.58
			33	298.85	-955.63	124.77	921.41	31.76	224.43
			66	313.92	-955.74	392.92	1566.93	-67.36	365.33
51	Fondazio ne	25, 26	0	-690.39	166.32	2453.78	-1030.27	-23.44	79.29
			49	-611.01	166.30	1977.91	-1026.64	-19.45	26.12
			97	-695.48	166.29	1512.26	-989.05	-14.84	-103.45

52	Fondazio ne	25, 26	0	-585.14	167.06	1404.92	-804.83	-16.34	82.59
			49	-501.67	167.05	1163.74	-555.36	-7.58	-6.35
			97	-608.95	167.04	955.16	-412.64	-14.00	-70.46
53	Fondazio ne	25, 26	0	-533.94	106.76	797.05	-624.71	-15.19	70.92
			49	-436.91	106.76	625.19	-383.51	-8.19	-2.06
			97	-557.37	106.75	505.39	204.44	-12.50	-62.05
54	Fondazio ne	25, 26	0	-492.41	78.56	386.47	-456.56	-13.71	60.94
			49	-380.04	78.55	263.79	-260.60	-6.74	2.84
			97	-508.09	78.54	197.12	120.01	-10.24	-52.38
55	Fondazio ne	25, 26	0	-446.41	-59.09	-128.15	-264.47	-11.43	51.32
			49	-317.35	-59.09	-147.69	142.06	-5.35	2.70
			97	-455.25	-59.08	-140.41	128.80	-8.10	-42.54
56	Fondazio ne	25, 26	0	-404.08	-36.67	-151.71	148.06	-9.32	-41.70
			49	-250.17	-36.67	-153.46	113.96	-4.15	2.58
			97	-401.51	-36.66	-138.52	135.20	-6.29	32.94
57	Fondazio ne	25, 26	0	-362.42	-18.28	-131.62	120.30	-7.37	-32.39
			49	-180.56	-18.28	-116.60	128.14	-3.03	2.62
			97	348.82	-18.28	-102.21	129.77	5.09	-26.03
58	Fondazio ne	25, 26	0	-319.66	-7.25	-88.59	132.77	5.68	25.81
			49	-117.39	-7.25	-71.25	129.06	-2.19	2.64
			97	299.87	-7.25	-60.37	124.02	4.07	-22.04
59	Fondazio ne	25, 26	0	-277.34	-4.78	-47.05	129.96	4.55	21.82
			49	-58.68	-4.78	-34.24	125.05	-1.66	2.78
			97	271.93	-4.78	-26.05	122.14	4.16	-20.68
60	Fondazio ne	25, 26	0	-245.60	-6.57	-11.81	124.54	3.93	20.73
			49	58.07	-6.57	-3.87	124.39	-1.67	3.39
			97	303.21	-6.57	11.32	127.33	4.88	-24.66
61	Fondazio ne	25, 26	0	-263.47	-5.57	22.49	122.63	3.71	24.29
			49	124.44	-5.57	32.14	128.34	-2.38	2.45
			97	350.96	-5.57	48.05	136.37	6.45	-32.88
62	Fondazio ne	25, 26	0	312.17	-8.51	62.64	126.16	5.22	33.08
			49	194.27	-8.51	75.08	134.13	-3.32	2.59
			97	400.16	-8.51	97.45	140.92	8.09	-41.64
63	Fondazio ne	25, 26	0	363.30	-18.97	112.48	135.37	6.95	42.15
			49	263.08	-18.97	130.12	135.82	-4.44	2.57
			97	451.28	-18.97	152.44	129.32	9.88	-50.62
64	Fondazio ne	25, 26	0	414.25	-37.31	161.06	141.87	8.81	51.34
			49	329.35	-37.31	178.94	119.39	5.65	2.44
			97	502.56	-37.32	183.53	154.67	-11.66	59.54
65	Fondazio ne	25, 26	0	463.32	-58.50	170.02	136.66	10.65	-60.51
			49	390.48	-58.50	177.18	155.65	6.88	2.34
			97	551.80	-58.50	157.54	-281.81	-13.54	68.55
66	Fondazio ne	25, 26	0	511.65	72.61	221.51	133.43	-12.56	-69.92
			49	442.39	72.62	-295.22	-275.92	8.16	2.41
			97	595.29	72.62	-433.07	-479.91	-15.57	77.66
67	Fondazio ne	25, 26	0	553.79	80.89	-569.55	-275.87	-14.61	-79.73
			49	484.41	80.89	-732.02	-475.18	9.78	-2.72
			97	632.78	80.89	-952.46	-757.84	-17.86	86.56
68	Fondazio ne	25, 26	0	582.03	183.52	-1127.57	-337.37	-16.91	-84.65
			49	509.95	183.53	-1296.09	-425.34	9.21	-6.24
			97	658.05	183.54	-1455.15	-707.14	-21.42	100.87
69	Fondazio ne	25, 26	0	656.21	277.56	-1617.36	-1113.93	-20.46	127.50
			49	605.34	277.57	-2129.54	-1069.34	25.31	-34.27
			97	762.34	277.58	-2610.38	-1077.84	31.16	96.73
70	Fondazio	25, 28	0	-264.37	379.96	152.53	1089.96	-103.26	-388.15

	ne								
			43	-274.17	379.85	240.74	317.86	37.13	-257.10
			85	-288.49	379.76	208.49	-520.39	122.45	-361.30
71	Fondazio ne	25, 28	0	-381.88	-1626.03	476.84	-597.45	122.64	412.62
			43	-391.09	-1626.15	134.70	-1316.15	-26.61	333.71
			85	-403.49	-1626.30	-717.01	-2196.99	-176.78	474.78
72	Fondazio ne	26, 27	0	326.57	253.96	-158.12	795.98	-83.84	-398.94
			33	341.01	253.88	-208.29	284.88	29.60	-270.32
			66	356.54	253.79	116.00	676.18	105.32	-320.71
73	Fondazio ne	26, 27	0	431.91	-1779.56	-369.95	686.15	105.51	431.50
			33	443.20	-1779.66	-92.12	1383.05	-27.01	394.10
			66	457.48	-1779.77	592.87	2145.77	-159.89	509.33
74	Fondazio ne	27, 29	0	477.64	885.58	391.12	-1307.93	-149.80	-521.05
			33	491.49	885.46	108.51	-604.32	13.27	-423.31
			66	506.26	885.34	114.87	450.65	133.65	-463.74
75	Fondazio ne	27, 29	0	559.79	-1734.66	-232.14	487.13	133.79	456.21
			33	551.61	-1734.78	83.72	1170.35	12.97	419.48
			66	565.57	-1734.91	579.76	1974.20	-145.80	497.14
76	Fondazio ne	28, 30	0	-470.60	919.87	-464.49	1404.48	-161.85	-525.51
			37	-479.19	919.75	-120.65	671.82	15.42	-401.29
			73	-488.27	919.63	-99.84	-364.16	138.19	-423.20
77	Fondazio ne	28, 30	0	-540.31	-1710.66	320.17	-626.19	138.27	431.16
			37	-549.69	-1710.79	-101.80	-1325.50	11.70	413.63
			73	-566.08	-1710.93	-708.83	-2146.36	-170.69	548.05
78	Fondazio ne	29, 31	0	559.34	1112.52	438.94	-1517.03	-183.93	-563.80
			33	570.57	1112.38	100.43	-646.65	-19.54	-498.50
			66	585.53	1112.26	107.79	281.20	146.79	-517.30
79	Fondazio ne	29, 31	0	634.75	-1695.41	-226.63	383.72	146.90	508.45
			33	638.46	-1695.54	108.17	1103.63	-18.45	505.80
			66	643.72	-1695.69	592.48	2005.64	-188.78	560.28
80	Fondazio ne	30, 32	0	-610.63	1108.22	-494.74	1606.26	-178.71	-588.13
			34	-625.74	1108.08	-138.33	775.10	-13.77	-462.90
			69	-641.39	1107.96	168.35	-213.28	143.15	-458.10
81	Fondazio ne	30, 32	0	-644.69	-1713.38	277.83	-552.41	143.21	455.38
			34	-660.23	-1713.52	157.32	-1266.00	-8.74	455.27
			69	-676.32	-1713.67	-712.42	-2105.85	-178.04	587.78
82	Fondazio ne	31, 33	0	620.81	1324.82	522.67	-1765.04	-166.97	-531.35
			33	608.22	1324.68	125.61	-854.27	11.93	-475.87
			66	615.97	1324.55	-124.98	213.89	147.73	-476.86
83	Fondazio ne	31, 33	0	738.77	-1569.47	-210.75	184.90	147.89	476.07
			33	713.81	-1569.60	100.65	969.92	11.96	463.81
			66	696.33	-1569.75	515.73	1894.57	-158.92	540.06
84	Fondazio ne	32, 34	0	-679.90	1311.12	-587.55	1811.84	-183.29	-598.84
			35	-695.88	1310.98	134.19	927.75	-8.95	-471.85
			69	-712.41	1310.84	172.64	131.77	150.33	-473.83
85	Fondazio ne	32, 34	0	-687.60	-1555.63	264.01	-444.17	150.37	480.49
			35	-696.17	-1555.77	-107.82	-1170.77	14.09	481.17
			69	-712.99	-1555.92	-630.84	-2070.70	-184.45	588.77
86	Fondazio ne	33, 35	0	666.94	1429.80	509.79	-1778.67	-191.77	-601.24
			33	665.94	1429.65	100.95	-841.21	-19.06	-511.60
			66	671.55	1429.51	-126.61	-158.04	148.75	-514.04
87	Fondazio ne	33, 35	0	770.85	-1497.43	-194.90	255.17	148.86	504.52
			33	750.05	-1497.57	95.90	998.75	-19.35	512.85
			66	751.55	-1497.73	550.14	1932.49	-198.87	610.47
88	Fondazio ne	34, 36	0	-721.64	1426.70	-545.33	1915.58	-188.42	-591.46

			35	-721.03	1426.54	-77.24	1011.73	-14.18	-483.13
			69	-730.28	1426.40	201.75	265.32	151.02	-493.69
89	Fondazio ne	34, 36	0	-718.23	-1518.26	208.42	-318.86	151.08	503.45
			35	-709.79	-1518.40	-71.34	-1036.93	15.72	477.29
			69	-715.66	-1518.55	-560.01	-1941.49	-186.32	582.43
90	Fondazio ne	35, 37	0	702.21	1530.99	611.33	-2034.92	-168.32	-565.13
			33	673.71	1530.84	127.78	-1109.43	13.66	-464.53
			66	663.16	1530.70	-189.32	-376.29	145.46	-460.88
91	Fondazio ne	35, 37	0	778.19	-1371.81	-180.34	244.93	145.30	450.01
			33	750.55	-1371.94	150.31	840.14	7.85	461.91
			66	744.90	-1372.09	491.47	1748.59	-167.19	569.13
92	Fondazio ne	36, 38	0	-725.22	1493.44	-545.55	1993.05	-182.22	-569.59
			35	-715.39	1493.29	-87.32	1064.48	14.13	-476.89
			69	-717.24	1493.15	260.43	302.71	154.21	-513.11
93	Fondazio ne	36, 38	0	-671.20	-1476.32	224.26	-284.73	154.26	515.45
			35	-661.99	-1476.45	107.02	-969.34	13.61	474.97
			69	-667.04	-1476.61	-507.77	-1866.75	-175.40	553.79
94	Fondazio ne	37, 39	0	668.24	1563.89	591.54	-1891.15	-190.43	-610.40
			33	657.62	1563.74	141.20	-976.64	-14.69	-498.89
			66	660.72	1563.60	-208.57	-180.19	145.57	-468.90
95	Fondazio ne	37, 39	0	706.53	-1330.11	-185.70	185.67	145.38	473.83
			33	694.82	-1330.24	-166.50	870.38	-14.51	509.51
			66	707.79	-1330.39	571.10	1761.09	-195.69	612.82
96	Fondazio ne	38, 40	0	-692.26	1452.71	-508.43	1947.25	-173.87	-534.15
			34	-682.60	1452.56	122.20	1031.66	13.28	-470.41
			69	-679.47	1452.42	265.61	273.44	148.98	-504.98
97	Fondazio ne	38, 40	0	-639.82	-1409.00	229.00	-218.13	149.00	499.14
			34	-616.02	-1409.14	-107.01	-868.55	12.47	464.67
			69	-602.00	-1409.30	-434.17	-1758.96	-172.03	541.88
98	Fondazio ne	39, 41	0	647.19	1648.89	745.99	-2171.76	-164.80	-557.99
			33	630.47	1648.74	184.11	-1297.82	8.24	-457.73
			66	614.56	1648.60	-212.71	-495.69	141.45	-430.38
99	Fondazio ne	39, 41	0	641.98	-1088.39	-98.38	-397.94	141.41	466.80
			33	625.86	-1088.52	94.96	560.81	-14.90	495.33
			66	610.56	-1088.65	356.31	1340.86	-189.40	588.18
100	Fondazio ne	40, 42	0	-701.48	1474.53	-465.49	1858.54	-164.38	-535.37
			35	-669.48	1474.38	-91.51	955.96	14.86	-453.12
			69	-655.73	1474.24	226.25	248.56	148.87	-483.72
101	Fondazio ne	40, 42	0	-696.16	-1416.20	193.05	-364.41	148.94	491.30
			35	-675.91	-1416.34	-127.63	-1092.00	14.57	449.36
			69	-662.23	-1416.49	-609.18	-1982.43	-162.69	540.90
102	Fondazio ne	41, 44	0	561.23	1817.40	572.14	-2198.99	-179.60	-531.53
			33	545.49	1817.26	-98.98	-1419.71	-22.75	-433.19
			66	530.62	1817.15	-404.91	-678.12	116.42	-427.55
103	Fondazio ne	41, 44	0	471.19	-453.80	-197.88	-586.89	116.32	331.52
			33	450.05	-453.91	-258.40	-286.47	38.64	285.60
			66	452.47	-454.01	-190.17	990.69	-76.45	386.22
104	Fondazio ne	42, 43	0	-752.41	1312.89	-552.95	1313.72	-155.19	-415.58
			23	-743.14	1312.78	-343.33	734.67	-70.11	-353.49
			46	-734.15	1312.69	-272.01	308.21	18.01	-365.62
105	Fondazio ne	43, 44	0	-1121.54	-294.49	3582.23	-1090.52	63.70	124.63
			49	-1011.25	-294.47	3055.81	-1156.33	32.50	64.77
			97	-1044.11	-294.46	2522.66	-1144.76	-14.04	127.53
106	Fondazio ne	43, 44	0	-962.12	-114.20	2162.28	-1187.28	-15.34	85.98
			49	-859.50	-114.20	1745.13	-857.90	-6.94	-7.23

			97	-904.85	-114.20	1404.02	-663.14	12.94	-73.31
107	Fondazio ne	43, 44	0	-840.81	-51.16	1129.76	-909.98	14.16	71.86
			49	-735.54	-51.16	861.09	-540.26	7.77	2.38
			97	-791.29	-51.16	679.77	-294.62	11.24	-63.41
108	Fondazio ne	43, 44	0	-770.62	55.59	483.75	-585.50	13.04	62.46
			49	-651.59	55.58	322.02	-304.87	6.03	-3.33
			97	-707.52	55.58	244.15	124.28	9.14	-52.81
109	Fondazio ne	43, 44	0	-684.75	41.31	-156.34	-331.41	10.59	52.27
			49	-555.58	41.31	-205.21	-163.61	4.90	2.55
			97	-618.48	41.31	-198.25	141.47	7.47	43.21
110	Fondazio ne	43, 44	0	-598.02	26.34	-215.27	165.56	8.86	-42.46
			49	-458.34	26.34	-217.89	116.61	3.81	2.57
			97	-531.80	26.34	-196.17	150.50	5.70	33.48
111	Fondazio ne	43, 44	0	-510.80	14.45	-183.60	124.05	7.04	-32.76
			49	-360.14	14.45	-161.73	136.99	3.01	2.63
			97	-449.10	14.45	-140.55	140.03	4.38	-26.25
112	Fondazio ne	43, 44	0	-425.47	8.43	-119.87	142.22	5.22	25.65
			49	-261.86	8.43	-95.00	136.87	-2.36	2.61
			97	-369.12	8.43	-79.39	129.01	3.58	-22.01
113	Fondazio ne	43, 44	0	-354.89	5.30	-60.36	138.70	4.07	21.76
			49	-165.22	5.30	-41.27	130.48	-1.83	2.68
			97	295.75	5.30	-29.74	124.69	3.53	-20.47
114	Fondazio ne	43, 44	0	-289.66	5.66	-14.03	129.96	3.30	20.20
			49	-84.84	5.66	-1.13	127.43	-1.75	2.73
			97	257.30	5.66	12.78	128.61	4.86	-24.33
115	Fondazio ne	43, 44	0	-247.70	-3.65	28.04	124.08	3.65	24.33
			49	103.59	-3.65	38.84	128.54	-2.41	2.88
			97	308.27	-3.65	55.87	135.38	6.51	-32.69
116	Fondazio ne	43, 44	0	-308.21	7.08	72.55	127.34	5.33	32.89
			49	185.83	7.08	86.58	134.06	-3.22	2.52
			97	372.55	7.08	108.84	138.70	8.29	-41.34
117	Fondazio ne	43, 44	0	376.21	20.82	125.71	136.15	7.09	41.85
			49	269.78	20.82	143.96	133.35	-4.17	2.57
			97	442.90	20.82	163.36	121.96	10.13	-50.29
118	Fondazio ne	43, 44	0	445.12	42.23	171.04	143.69	8.93	50.89
			49	352.21	42.23	188.66	114.03	-5.19	2.59
			97	512.16	42.24	185.93	160.11	-12.02	-59.43
119	Fondazio ne	43, 44	0	510.82	69.34	166.81	137.61	10.83	60.01
			49	432.58	69.34	172.60	155.71	-6.25	2.63
			97	576.29	69.35	145.31	-305.34	-13.99	68.63
120	Fondazio ne	43, 44	0	570.11	-95.43	-223.97	120.62	-12.78	-69.00
			49	503.06	-95.44	-297.00	-286.28	-7.28	2.86
			97	630.89	-95.45	-448.33	-519.55	-16.17	78.14
121	Fondazio ne	43, 44	0	621.88	-111.47	-619.63	-273.14	-14.94	-78.96
			49	561.93	-111.48	-788.29	-504.08	-8.72	2.97
			97	673.19	-111.48	-1033.86	-819.48	-18.47	86.78
122	Fondazio ne	43, 44	0	660.91	-188.88	-1254.97	-409.91	-17.20	-84.70
			49	601.94	-188.89	-1464.39	-539.26	-9.34	-6.70
			97	697.55	-188.90	-1698.45	-818.95	24.17	100.16
123	Fondazio ne	43, 44	0	734.59	-168.59	-1903.10	-1195.90	22.74	-101.36
			49	692.55	-168.61	-2463.69	-1168.65	-8.05	-17.43
			97	777.04	-168.63	-2986.58	-1081.72	-23.54	109.64
124	Fondazio ne	43, 45	0	-607.67	1255.20	-902.05	2915.00	-71.17	-393.26
			33	-594.59	1255.06	-128.11	2109.42	38.74	-283.78
			66	-582.09	1254.93	566.49	1521.30	122.22	-326.31

125	Fondazio ne	43, 45	0	-562.83	-961.61	-113.61	351.61	122.08	463.07
			33	-549.92	-961.72	-120.55	-499.95	-24.34	451.31
			66	-537.57	-961.85	-346.79	-1280.17	-176.20	549.40
126	Fondazio ne	44, 46	0	411.77	800.99	346.66	-1463.24	-82.70	-384.16
			33	397.01	800.88	-180.94	-787.28	29.51	-281.95
			66	411.79	800.78	-283.95	-200.94	107.74	-329.04
127	Fondazio ne	44, 46	0	437.24	-1339.21	-280.18	536.34	107.60	425.23
			33	437.18	-1339.31	148.59	1102.64	-30.45	431.10
			66	458.30	-1339.43	565.30	1773.05	-178.41	508.89
128	Fondazio ne	45, 47	0	-548.44	1697.92	-620.91	2137.41	-138.38	-493.54
			33	-534.83	1697.79	-100.06	1399.45	16.54	-389.66
			66	-521.76	1697.69	351.62	820.28	120.70	-400.58
129	Fondazio ne	45, 47	0	-514.51	-582.82	-86.67	515.18	120.51	383.89
			33	-496.11	-582.92	82.49	348.31	8.44	375.58
			66	-483.78	-583.03	200.50	-992.74	-137.08	492.57
130	Fondazio ne	46, 48	0	419.20	1524.24	712.17	-2013.89	-144.30	-465.53
			33	408.14	1524.12	171.29	-1381.78	12.67	-384.74
			66	420.15	1524.02	-277.69	-858.66	111.70	-394.45
131	Fondazio ne	46, 48	0	463.29	-746.27	-90.03	-501.56	111.48	387.59
			33	456.70	-746.37	-111.67	352.04	11.31	368.27
			66	452.56	-746.48	251.31	929.65	-133.45	465.34
132	Fondazio ne	47, 49	0	-462.74	1457.32	-401.43	1574.32	-136.67	-460.74
			33	-442.28	1457.22	89.48	914.63	11.99	-333.98
			66	-429.87	1457.13	251.66	394.46	98.79	-346.64
133	Fondazio ne	47, 49	0	-430.97	-466.80	46.61	297.92	98.54	352.23
			33	-401.47	-466.88	60.38	-382.24	-11.78	329.15
			66	-390.14	-466.97	-268.60	-973.86	-128.87	445.86
134	Fondazio ne	48, 50	0	366.21	1523.00	435.59	-1519.66	-130.34	-445.38
			33	352.36	1522.90	-124.81	-929.99	-15.90	-338.26
			66	350.47	1522.81	-321.13	-487.57	96.50	-366.26
135	Fondazio ne	48, 50	0	369.23	-454.75	-75.52	-213.43	96.33	361.48
			33	350.59	-454.83	-133.44	475.36	12.65	323.36
			66	353.78	-454.91	375.93	1030.78	-120.63	441.05
136	Fondazio ne	49, 51	0	-345.66	1311.77	-528.85	1724.71	-89.01	-353.40
			33	-312.27	1311.68	68.17	1166.72	14.16	-251.04
			66	-300.27	1311.60	264.04	672.31	85.48	-299.50
137	Fondazio ne	49, 51	0	-303.85	333.91	-62.90	619.84	85.18	309.03
			33	-274.94	333.96	139.88	390.13	14.04	265.76
			66	-277.22	334.02	267.20	608.06	-95.31	363.20
138	Fondazio ne	50, 52	0	257.85	1325.54	617.33	-1722.83	-80.90	-358.78
			33	242.53	1325.45	153.35	-1200.65	13.68	-231.52
			66	245.67	1325.37	-277.72	-739.98	85.29	-299.96
139	Fondazio ne	50, 52	0	270.09	-336.12	106.84	-535.64	85.29	335.12
			33	225.07	-336.17	-92.00	-241.65	16.25	263.62
			66	231.04	-336.22	153.59	563.11	-97.76	361.70
140	Fondazio ne	51, 53	0	-252.14	1139.82	-365.99	1357.71	-96.28	-332.07
			33	-218.59	1139.76	134.71	874.75	11.10	-267.14
			66	-216.64	1139.70	264.63	439.93	80.96	283.47
141	Fondazio ne	51, 53	0	-279.20	-370.14	62.23	383.65	80.73	-299.53
			33	-247.44	-370.10	82.65	193.48	17.16	293.24
			66	-222.40	-370.06	163.68	604.75	-113.58	352.59
142	Fondazio ne	52, 54	0	274.74	1181.30	410.36	-1468.25	-81.94	-306.71
			33	218.18	1181.23	-79.13	-1014.40	12.39	-231.32
			66	216.24	1181.17	-295.76	-632.67	81.76	-313.51
143	Fondazio	52, 54	0	300.12	253.94	56.30	-529.49	81.63	324.91

	ne								
			33	243.87	253.90	-124.80	-336.31	15.31	238.72
			66	221.84	253.85	-218.76	476.02	-88.39	329.41
144	Fondazio ne	53, 55	0	-254.58	1009.26	-348.05	1349.00	-84.66	-301.60
			33	-217.52	1009.21	62.94	910.16	15.69	-228.35
			66	-188.43	1009.18	289.29	599.06	67.31	256.50
145	Fondazio ne	53, 55	0	-242.47	302.38	-58.05	579.12	67.04	-241.41
			33	-210.07	302.34	189.08	450.40	9.52	209.65
			66	-190.14	302.31	313.48	-614.67	-78.59	308.04
146	Fondazio ne	54, 56	0	311.45	985.72	252.75	-1225.93	-70.15	-285.26
			33	253.36	985.67	-133.90	-836.18	14.57	-183.18
			66	226.96	985.63	-343.97	-562.01	65.63	279.34
147	Fondazio ne	54, 56	0	321.91	215.12	-103.05	-527.02	65.48	-248.09
			33	263.74	215.08	-221.00	-412.07	9.37	160.46
			66	238.32	215.04	-345.75	528.72	-71.97	293.56
148	Fondazio ne	55, 57	0	-213.17	630.99	-130.93	939.21	-63.87	-261.04
			40	-152.62	630.96	208.12	433.48	16.18	-118.11
			80	-134.76	630.93	282.36	213.36	-59.52	240.68
149	Fondazio ne	55, 57	0	-170.72	205.26	205.36	260.52	-59.32	-287.90
			40	-110.52	205.24	183.49	-343.99	30.70	123.97
			80	-108.45	205.23	112.39	-866.31	-43.88	230.02
150	Fondazio ne	56, 70	0	249.96	556.23	157.45	-877.29	-58.39	-248.03
			40	174.49	556.19	-226.77	-421.06	16.87	-91.48
			80	149.81	556.15	-294.96	-189.72	-57.71	245.33
151	Fondazio ne	56, 70	0	215.90	192.64	-203.77	-256.99	-57.56	-298.90
			40	142.17	192.62	-179.46	352.19	28.27	123.24
			80	141.14	192.60	-107.32	783.97	-43.31	220.46
152	Fondazio ne	57, 58	0	-182.97	-86.71	381.00	969.58	16.24	73.59
			42	308.29	-86.71	388.01	454.78	13.74	32.02
			83	496.85	-86.71	440.28	311.55	21.18	-95.74
153	Fondazio ne	57, 58	0	152.13	121.70	482.59	304.51	21.37	93.68
			42	315.57	121.70	508.39	210.96	14.53	-33.22
			83	528.61	121.70	595.22	-501.52	21.53	-65.01
154	Fondazio ne	58, 59	0	329.98	-114.03	642.59	793.08	20.52	59.24
			35	476.23	-114.03	434.40	630.67	10.19	25.40
			69	649.27	-114.02	307.99	-479.91	8.84	63.64
155	Fondazio ne	58, 59	0	311.78	126.00	331.89	-543.30	9.22	51.89
			35	447.66	126.00	251.48	-417.62	8.50	-18.19
			69	624.19	126.00	180.39	378.77	18.85	53.53
156	Fondazio ne	59, 60	0	320.42	-94.06	179.19	440.57	21.90	-59.37
			35	414.94	-94.06	171.84	-328.51	7.37	30.61
			69	588.68	-94.05	148.26	-245.53	-5.27	39.65
157	Fondazio ne	59, 60	0	322.97	79.15	-139.81	-307.07	-5.47	-40.50
			35	381.90	79.14	117.90	251.97	5.55	-22.52
			69	547.15	79.14	122.23	244.95	16.18	48.29
158	Fondazio ne	60, 61	0	321.17	-90.75	97.83	290.66	13.09	-36.48
			35	350.20	-90.75	-149.07	244.85	5.98	14.03
			69	492.46	-90.75	-192.50	215.25	-5.61	35.79
159	Fondazio ne	60, 61	0	383.21	111.55	-173.94	-309.84	-6.07	-47.15
			35	360.36	111.55	-250.69	-294.06	8.13	-23.45
			69	461.60	111.55	-327.30	288.49	12.96	21.28
160	Fondazio ne	61, 62	0	-248.75	80.81	-335.54	399.99	-17.55	-28.31
			35	282.69	80.81	-181.45	408.81	9.24	-33.32
			69	431.92	80.81	-64.77	422.68	-6.15	50.50
161	Fondazio ne	61, 62	0	-298.77	106.84	-79.46	430.70	-6.40	-28.04

			35	274.67	106.84	130.97	451.45	3.46	-16.07
			69	383.08	106.84	303.12	478.67	9.35	-24.38
162	Fondazio ne	62, 63	0	-244.29	-46.69	305.46	-416.85	10.87	35.37
			35	240.68	-46.69	194.82	-390.09	2.14	19.81
			69	381.75	-46.68	94.72	-364.00	4.62	-17.67
163	Fondazio ne	62, 63	0	-239.19	-91.13	124.56	267.96	4.42	22.18
			35	189.05	-91.13	71.52	246.37	4.57	25.31
			69	325.91	-91.13	49.94	230.19	-14.31	-36.48
164	Fondazio ne	63, 64	0	-275.62	-114.19	92.02	-237.12	-11.31	26.18
			35	165.17	-114.19	36.91	-224.85	4.90	-15.42
			69	264.72	-114.19	-35.78	-220.02	2.09	-19.74
165	Fondazio ne	63, 64	0	-316.83	-114.67	30.46	-221.31	1.85	23.41
			35	-172.88	-114.68	-42.63	-223.97	-5.23	15.47
			69	223.31	-114.68	-102.82	-233.70	-10.22	24.81
166	Fondazio ne	64, 65	0	-364.92	-90.48	-55.43	230.32	-13.04	-31.45
			35	-226.40	-90.48	-80.73	246.81	-4.77	25.21
			69	188.68	-90.49	-128.14	269.00	5.65	-31.15
167	Fondazio ne	64, 65	0	-409.42	-46.96	-104.54	-364.62	5.78	27.60
			35	-291.87	-46.96	-196.59	-391.70	-2.96	21.05
			69	200.18	-46.97	-303.78	-419.91	-10.20	36.86
168	Fondazio ne	65, 66	0	-410.05	121.19	-305.47	464.36	-8.37	30.64
			35	-257.43	121.19	-131.52	440.29	-4.07	-13.34
			69	-214.04	121.19	65.30	427.19	6.35	-37.72
169	Fondazio ne	65, 66	0	-436.85	91.54	51.67	412.63	5.89	-47.92
			35	-284.24	91.54	172.57	412.35	-8.48	33.27
			69	166.15	91.55	314.40	423.59	18.84	-38.90
170	Fondazio ne	66, 67	0	-462.90	104.33	304.26	-294.29	14.54	35.34
			35	-314.71	104.33	246.43	-283.23	-7.52	-23.55
			69	-299.09	104.33	182.98	-277.81	-6.54	50.12
171	Fondazio ne	66, 67	0	-495.91	-72.60	184.34	193.62	-6.09	42.00
			35	-347.85	-72.60	146.76	194.04	-6.01	11.73
			69	-237.93	-72.60	-94.87	240.98	-13.18	51.63
172	Fondazio ne	67, 68	0	-536.95	70.17	-129.64	230.57	-14.28	-54.98
			35	-386.22	70.17	-106.20	245.54	-5.30	-21.86
			69	-245.62	70.17	-125.89	-279.45	7.00	-50.10
173	Fondazio ne	67, 68	0	-562.15	-76.18	-138.55	-235.86	6.59	52.66
			35	-409.84	-76.19	-162.92	-298.35	-8.24	30.72
			69	-264.70	-76.19	-174.87	-430.75	-20.90	65.88
174	Fondazio ne	68, 69	0	-583.24	140.31	-181.37	-346.59	-18.01	-58.28
			35	-429.49	140.31	-248.51	-411.15	-9.10	-21.00
			69	-281.28	140.31	-325.79	-519.67	-11.38	-68.95
175	Fondazio ne	68, 69	0	-596.66	-105.87	-315.43	-472.87	-10.95	-75.34
			35	-431.99	-105.87	-436.55	-623.63	-10.02	24.36
			69	-281.85	-105.87	-626.71	826.39	-21.33	-71.50
176	Fondazio ne	69, 70	0	-524.22	106.99	-602.30	-464.82	-24.16	74.38
			42	-295.28	106.99	-514.81	212.39	-14.26	31.39
			83	-153.98	106.99	-465.96	287.14	-26.69	111.32
177	Fondazio ne	69, 70	0	-497.95	79.78	-461.30	340.32	-26.27	-113.06
			42	-300.88	79.78	-378.77	483.50	-10.43	-29.66
			83	189.71	79.79	-337.54	913.65	17.52	-84.95
178	Primo Impalcato	1, 2	0	-729.43	-14.91	193.54	-54.62	-388.37	499.77
			83	-729.43	-14.91	159.75	-54.62	-202.64	499.77
			166	-729.43	-14.91	126.17	-54.62	-545.82	499.77
179	Primo Impalcato	1, 15	0	510.33	-23.55	-213.94	183.40	391.45	329.60
			80	510.33	-23.55	-76.81	183.40	139.74	329.60

			159	510.33	-23.55	87.71	183.40	-182.78	329.60
180	Primo Impalcato	2, 3	0	-902.28	-7.29	149.07	-140.36	-551.34	-636.62
			69	-902.28	-7.29	54.17	-140.36	-130.91	-636.62
			138	-902.28	-7.29	-48.32	-140.36	404.44	-636.62
181	Primo Impalcato	3, 4	0	-599.65	2.02	25.78	-7.62	399.96	143.68
			69	-599.65	2.02	21.80	-7.62	319.65	143.68
			138	-599.65	2.02	-17.94	-7.62	279.46	143.68
182	Primo Impalcato	4, 5	0	-294.47	6.57	26.21	11.39	286.84	573.69
			69	-294.47	6.57	32.37	11.39	-167.65	573.69
			138	-294.47	6.57	38.59	11.39	-536.22	573.69
183	Primo Impalcato	5, 6	0	316.31	9.48	65.90	-184.77	-533.93	-490.66
			69	316.31	9.48	-65.34	-184.77	-219.47	-490.66
			138	316.31	9.48	-192.15	-184.77	173.24	-490.66
184	Primo Impalcato	6, 7	0	261.88	8.61	-168.05	238.73	171.28	250.28
			69	261.88	8.61	-5.82	238.73	281.70	250.28
			138	261.88	8.61	163.79	238.73	436.33	250.28
185	Primo Impalcato	7, 8	0	-217.00	12.92	187.63	-148.47	439.27	620.69
			69	-217.00	12.92	85.88	-148.47	-46.51	620.69
			138	-217.00	12.92	-22.31	-148.47	-445.93	620.69
186	Primo Impalcato	8, 9	0	494.16	8.91	20.88	-148.32	-443.60	-285.01
			69	494.16	8.91	-86.11	-148.32	-276.86	-285.01
			138	494.16	8.91	-187.37	-148.32	153.66	-285.01
187	Primo Impalcato	9, 10	0	451.82	8.58	-163.69	234.34	156.88	-466.68
			69	451.82	8.58	12.22	234.34	222.74	-466.68
			138	451.82	8.58	160.36	234.34	515.05	-466.68
188	Primo Impalcato	10, 11	0	434.76	6.53	183.91	-180.01	522.36	568.98
			69	434.76	6.53	61.74	-180.01	-161.64	568.98
			138	434.76	6.53	-69.85	-180.01	-305.15	568.98
189	Primo Impalcato	11, 12	0	694.24	-2.52	-46.97	32.64	-297.71	-122.78
			69	694.24	-2.52	-36.03	32.64	-310.84	-122.78
			138	694.24	-2.52	33.88	32.64	378.33	-122.78
190	Primo Impalcato	12, 13	0	946.31	-7.17	56.25	-132.32	382.67	-606.63
			69	946.31	-7.17	-52.80	-132.32	145.32	-606.63
			138	946.31	-7.17	-136.27	-132.32	538.10	-606.63
191	Primo Impalcato	13, 14	0	817.93	-15.10	-115.59	-76.32	532.83	546.70
			83	817.93	-15.10	-163.19	-76.32	195.65	546.70
			166	817.93	-15.10	-220.47	-76.32	-486.04	546.70
192	Primo Impalcato	14, 16	0	-542.48	-23.15	231.61	-210.20	-489.32	-456.20
			80	-542.48	-23.15	81.90	-210.20	133.35	-456.20
			159	-542.48	-23.15	-112.34	-210.20	290.88	-456.20
193	Primo Impalcato	15, 17	0	536.75	-27.92	-53.23	80.67	-179.83	-160.71
			66	536.75	-27.92	36.06	80.67	-142.56	-160.71
			132	536.75	-27.92	75.05	80.67	-162.20	-160.71
194	Primo Impalcato	16, 18	0	-592.43	-28.17	59.82	-98.33	264.65	-167.82
			66	-592.43	-28.17	-43.67	-98.33	198.76	-167.82
			132	-592.43	-28.17	-91.32	-98.33	-200.82	-167.82
195	Primo Impalcato	17, 19	0	555.20	-29.68	-43.86	55.26	-165.61	-204.95
			66	555.20	-29.68	26.70	55.26	114.58	-204.95
			132	555.20	-29.68	52.92	55.26	188.73	-204.95
196	Primo Impalcato	18, 20	0	-561.32	-28.97	57.22	-72.78	-212.65	231.28
			66	-561.32	-28.97	-38.78	-72.78	93.47	231.28
			132	-561.32	-28.97	-73.47	-72.78	172.10	231.28
197	Primo Impalcato	19, 21	0	599.29	-29.75	-102.14	138.99	196.46	197.34
			66	599.29	-29.75	-22.61	138.99	107.91	197.34
			132	599.29	-29.75	89.25	138.99	-148.82	197.34

198	Primo Impalcato	20, 22	0	648.34	-29.83	112.13	-149.59	160.92	152.96
			66	648.34	-29.83	-20.03	-149.59	105.15	152.96
			132	648.34	-29.83	-92.82	-149.59	-162.35	152.96
199	Primo Impalcato	21, 23	0	565.98	-28.25	-42.92	48.33	-147.05	208.47
			66	565.98	-28.25	-32.82	48.33	-120.43	208.47
			132	565.98	-28.25	-48.60	48.33	225.99	208.47
200	Primo Impalcato	22, 24	0	590.58	-28.98	47.11	-61.28	170.28	180.23
			66	590.58	-28.98	-27.06	-61.28	-98.02	180.23
			132	590.58	-28.98	-42.30	-61.28	-182.39	180.23
201	Primo Impalcato	23, 25	0	592.38	-26.49	-118.89	162.53	222.12	-189.86
			66	592.38	-26.49	-25.25	162.53	181.74	-189.86
			132	592.38	-26.49	108.35	162.53	229.26	-189.86
202	Primo Impalcato	24, 26	0	611.01	-26.92	95.23	-161.28	-178.95	-188.80
			66	611.01	-26.92	20.53	-161.28	-107.26	-188.80
			132	611.01	-26.92	-121.51	-161.28	176.18	-188.80
203	Primo Impalcato	25, 28	0	-534.79	-19.20	-45.36	42.43	229.70	-245.51
			85	-534.79	-19.20	-33.23	42.43	-140.40	-245.51
			170	-534.79	-19.20	58.31	42.43	255.93	-245.51
204	Primo Impalcato	26, 27	0	-578.31	-25.36	54.97	-57.38	186.17	-245.55
			66	-578.31	-25.36	-28.90	-57.38	-168.67	-245.55
			132	-578.31	-25.36	-50.44	-57.38	-260.53	-245.55
205	Primo Impalcato	27, 29	0	572.48	-20.02	106.50	-142.92	-251.41	-259.25
			66	572.48	-20.02	-18.79	-142.92	-148.84	-259.25
			132	572.48	-20.02	-92.34	-142.92	225.12	-259.25
206	Primo Impalcato	28, 30	0	-538.33	-16.96	-108.72	131.07	250.84	-253.55
			73	-538.33	-16.96	-34.12	131.07	-143.80	-253.55
			146	-538.33	-16.96	103.67	131.07	-206.42	-253.55
207	Primo Impalcato	29, 31	0	522.87	-13.82	52.19	-28.12	233.92	-171.82
			66	522.87	-13.82	45.11	-28.12	190.35	-171.82
			132	522.87	-13.82	45.63	-28.12	270.52	-171.82
208	Primo Impalcato	30, 32	0	-522.44	-13.05	-120.57	123.46	-202.28	-167.68
			69	-522.44	-13.05	52.25	123.46	-172.27	-167.68
			137	-522.44	-13.05	88.85	123.46	-238.52	-167.68
209	Primo Impalcato	31, 33	0	495.62	-9.10	90.42	-142.77	264.18	240.39
			66	495.62	-9.10	26.48	-142.77	-128.37	240.39
			132	495.62	-9.10	-99.23	-142.77	-230.12	240.39
210	Primo Impalcato	32, 34	0	-563.47	-8.23	-123.24	129.46	-244.16	248.60
			69	-563.47	-8.23	41.39	129.46	-148.42	248.60
			138	-563.47	-8.23	83.04	129.46	-260.15	248.60
211	Primo Impalcato	33, 35	0	423.40	-4.30	41.82	44.59	-237.05	170.86
			66	423.40	-4.30	46.68	44.59	-183.73	170.86
			132	423.40	-4.30	58.18	44.59	-232.94	170.86
212	Primo Impalcato	34, 36	0	-602.46	-3.07	-120.88	141.47	-259.74	184.50
			69	-602.46	-3.07	-31.68	141.47	-188.35	184.50
			138	-602.46	-3.07	90.79	141.47	-236.75	184.50
213	Primo Impalcato	35, 37	0	450.58	6.27	94.13	-131.68	-224.01	240.14
			66	450.58	6.27	33.58	-131.68	-135.94	240.14
			132	450.58	6.27	-98.77	-131.68	-205.25	240.14
214	Primo Impalcato	36, 38	0	-641.14	4.93	-114.48	141.96	-243.70	-274.05
			69	-641.14	4.93	-27.47	141.96	-148.56	-274.05
			138	-641.14	4.93	97.26	141.96	229.06	-274.05
215	Primo Impalcato	37, 39	0	417.79	10.12	-58.92	43.00	213.75	248.08
			66	417.79	10.12	-42.68	43.00	-150.73	248.08
			132	417.79	10.12	47.48	43.00	218.14	248.08
216	Primo	38, 40	0	701.94	10.08	-115.14	136.79	222.60	210.82

	Impalcato								
			69	701.94	10.08	31.26	136.79	190.32	210.82
			137	701.94	10.08	91.55	136.79	189.66	210.82
217	Primo Impalcato	39, 41	0	484.05	12.92	109.49	-118.97	206.80	-242.65
			66	484.05	12.92	59.90	-118.97	-141.57	-242.65
			132	484.05	12.92	-72.93	-118.97	-202.17	-242.65
218	Primo Impalcato	40, 42	0	766.63	14.20	-122.56	144.25	195.84	241.20
			69	766.63	14.20	-35.79	144.25	-134.03	241.20
			138	766.63	14.20	91.33	144.25	-229.02	241.20
219	Primo Impalcato	41, 44	0	490.41	10.96	100.38	-169.67	-212.12	-223.11
			66	490.41	10.96	-43.42	-169.67	150.49	-223.11
			132	490.41	10.96	-127.22	-169.67	-190.97	-223.11
220	Primo Impalcato	42, 43	0	844.88	27.04	-137.37	473.57	-225.30	-349.34
			23	844.88	27.04	-45.58	473.57	-192.45	-349.34
			46	844.88	27.04	93.73	473.57	181.55	-349.34
221	Primo Impalcato	43, 45	0	766.20	21.81	-72.21	58.73	182.57	-232.11
			66	766.20	21.81	-43.84	58.73	-155.94	-232.11
			132	766.20	21.81	-33.27	58.73	249.63	-232.11
222	Primo Impalcato	44, 46	0	493.22	19.77	24.03	48.18	-177.29	243.85
			66	493.22	19.77	37.98	48.18	165.46	243.85
			132	493.22	19.77	68.42	48.18	282.67	243.85
223	Primo Impalcato	45, 47	0	738.75	25.65	-145.26	200.86	255.52	246.55
			66	738.75	25.65	-24.14	200.86	-122.59	246.55
			132	738.75	25.65	128.00	200.86	-183.15	246.55
224	Primo Impalcato	46, 48	0	559.13	26.31	150.75	-210.26	298.96	263.83
			66	559.13	26.31	-31.76	-210.26	-190.62	263.83
			132	559.13	26.31	-151.00	-210.26	240.14	263.83
225	Primo Impalcato	47, 49	0	653.32	29.49	30.00	-17.64	-183.99	-181.54
			66	653.32	29.49	23.15	-17.64	-163.77	-181.54
			132	653.32	29.49	22.48	-17.64	-228.11	-181.54
226	Primo Impalcato	48, 50	0	585.27	28.45	-30.99	-24.62	227.57	-187.45
			66	585.27	28.45	-29.99	-24.62	-160.84	-187.45
			132	585.27	28.45	-40.09	-24.62	-195.19	-187.45
227	Primo Impalcato	49, 51	0	-639.04	32.46	-142.05	216.59	-237.44	-272.75
			66	-639.04	32.46	17.38	216.59	-103.18	-272.75
			132	-639.04	32.46	154.68	216.59	197.91	-272.75
228	Primo Impalcato	50, 52	0	631.00	31.95	139.40	-176.12	-209.16	-265.18
			66	631.00	31.95	33.70	-176.12	99.72	-265.18
			132	631.00	31.95	-108.25	-176.12	235.80	-265.18
229	Primo Impalcato	51, 53	0	540.62	31.22	35.43	-25.74	193.81	-203.46
			66	540.62	31.22	39.27	-25.74	144.76	-203.46
			132	540.62	31.22	45.63	-25.74	-225.26	-203.46
230	Primo Impalcato	52, 54	0	-544.28	32.28	62.07	-94.52	209.58	-156.36
			66	-544.28	32.28	-29.58	-94.52	139.29	-156.36
			132	-544.28	32.28	-87.26	-94.52	-149.85	-156.36
231	Primo Impalcato	53, 55	0	-521.36	31.72	-107.08	163.53	-222.66	272.43
			66	-521.36	31.72	-33.19	163.53	-204.34	272.43
			132	-521.36	31.72	126.28	163.53	-350.70	272.43
232	Primo Impalcato	54, 56	0	-480.57	31.29	82.71	-142.98	167.50	264.31
			66	-480.57	31.29	-50.47	-142.98	-146.39	264.31
			132	-480.57	31.29	-132.70	-142.98	-266.75	264.31
233	Primo Impalcato	55, 57	0	554.06	27.10	-45.21	137.90	-353.10	528.29
			80	554.06	27.10	97.80	137.90	166.98	528.29
			159	554.06	27.10	201.57	137.90	535.08	528.29
234	Primo Impalcato	56, 70	0	-496.70	27.24	45.43	-126.49	-257.16	-355.36

			80	-496.70	27.24	-70.23	-126.49	159.74	-355.36
			159	-496.70	27.24	-160.85	-126.49	367.81	-355.36
235	Primo Impalcato	57, 58	0	-916.95	11.19	217.11	50.22	517.52	-533.05
			83	-916.95	11.19	182.12	50.22	209.47	-533.05
			166	-916.95	11.19	148.97	50.22	504.56	-533.05
236	Primo Impalcato	58, 59	0	-1030.59	8.69	176.59	-171.88	513.28	613.31
			69	-1030.59	8.69	68.69	-171.88	130.91	613.31
			138	-1030.59	8.69	-63.55	-171.88	-369.16	613.31
237	Primo Impalcato	59, 60	0	-758.73	2.62	32.65	38.77	-364.54	117.48
			69	-758.73	2.62	41.80	38.77	-301.11	117.48
			138	-758.73	2.62	56.71	38.77	-269.76	117.48
238	Primo Impalcato	60, 61	0	-483.51	-6.49	85.59	-218.78	-274.27	-542.83
			69	-483.51	-6.49	-77.43	-218.78	157.63	-542.83
			138	-483.51	-6.49	-224.92	-218.78	527.16	-542.83
239	Primo Impalcato	61, 62	0	-491.09	-7.13	-196.12	283.01	524.11	471.94
			69	-491.09	-7.13	13.49	283.01	204.00	471.94
			138	-491.09	-7.13	197.57	283.01	148.95	471.94
240	Primo Impalcato	62, 63	0	-522.90	-8.23	226.71	-216.94	147.04	-257.31
			69	-522.90	-8.23	77.05	-216.94	-287.07	-257.31
			138	-522.90	-8.23	-73.85	-216.94	-432.77	-257.31
241	Primo Impalcato	63, 64	0	-294.99	-10.60	-40.07	53.83	-436.88	-635.09
			69	-294.99	-10.60	-8.48	53.83	52.66	-635.09
			138	-294.99	-10.60	41.53	53.83	440.44	-635.09
242	Primo Impalcato	64, 65	0	548.57	-7.89	77.85	-219.33	436.41	-225.61
			69	548.57	-7.89	-76.67	-219.33	287.06	-225.61
			138	548.57	-7.89	-227.55	-219.33	-175.93	-225.61
243	Primo Impalcato	65, 66	0	483.35	-7.24	-198.23	288.23	-177.07	473.42
			69	483.35	-7.24	-10.57	288.23	-204.19	473.42
			138	483.35	-7.24	203.64	288.23	-529.50	473.42
244	Primo Impalcato	66, 67	0	439.14	-6.31	233.34	-221.86	-532.73	-551.59
			69	439.14	-6.31	80.72	-221.86	158.66	-551.59
			138	439.14	-6.31	-83.76	-221.86	-254.31	-551.59
245	Primo Impalcato	67, 68	0	771.51	2.51	-52.40	39.94	-247.99	141.92
			69	771.51	2.51	-39.09	39.94	307.31	141.92
			138	771.51	2.51	-31.21	39.94	-369.04	141.92
246	Primo Impalcato	68, 69	0	1105.54	8.81	61.81	-176.76	-373.86	626.59
			69	1105.54	8.81	-69.45	-176.76	-106.58	626.59
			138	1105.54	8.81	-186.28	-176.76	-527.29	626.59
247	Primo Impalcato	69, 70	0	958.32	11.03	-157.35	41.10	-518.69	494.08
			83	958.32	11.03	-187.48	41.10	-215.70	494.08
			166	958.32	11.03	-218.46	41.10	-398.93	494.08
248	Primo Impalcato	1	0	956.84	38.03	-17.83	8.43	465.37	251.89
			188	956.84	38.03	-9.56	8.43	51.75	251.89
			376	956.84	38.03	-21.90	8.43	-485.28	251.89
249	Primo Impalcato	2	0	597.89	2.95	-245.89	-161.12	-20.88	-11.10
			188	597.89	2.95	-150.68	-161.12	0.24	-11.10
			376	597.89	2.95	-431.47	-161.12	20.85	-11.10
250	Primo Impalcato	3	0	-447.61	-3.35	-271.18	-171.85	-24.25	-12.87
			188	-447.61	-3.35	-173.19	-171.85	0.20	-12.87
			376	-447.61	-3.35	-459.52	-171.85	24.12	-12.87
251	Primo Impalcato	4	0	232.59	4.14	-174.09	-116.44	-23.67	-12.66
			188	232.59	4.14	-163.07	-116.44	0.21	-12.66
			376	232.59	4.14	-368.23	-116.44	23.95	-12.66
252	Primo Impalcato	5	0	145.99	-1.73	315.97	-181.40	-24.26	-12.81
			188	145.99	-1.73	-142.57	-181.40	-0.30	-12.81

			376	145.99	-1.73	-452.16	-181.40	23.92	-12.81
253	Primo Impalcato	6	0	328.31	-4.95	-133.97	-65.38	-21.07	-11.31
			188	328.31	-4.95	-104.28	-65.38	0.30	-11.31
			376	328.31	-4.95	-188.07	-65.38	21.44	-11.31
254	Primo Impalcato	7	0	-340.05	-3.64	190.75	-110.66	-21.23	-11.40
			188	-340.05	-3.64	-47.74	-110.66	0.30	-11.40
			376	-340.05	-3.64	-245.29	-110.66	21.64	-11.40
255	Primo Impalcato	8	0	44.27	-3.60	209.85	-121.57	-25.33	-13.24
			188	44.27	-3.60	49.42	-121.57	-0.58	-13.24
			376	44.27	-3.60	-266.21	-121.57	24.45	-13.24
256	Primo Impalcato	9	0	384.27	-4.92	165.60	79.95	-21.45	-11.52
			188	384.27	-4.92	104.75	79.95	0.33	-11.52
			376	384.27	-4.92	211.35	79.95	21.88	-11.52
257	Primo Impalcato	10	0	-366.78	-1.91	-306.49	178.31	-21.60	-11.61
			188	-366.78	-1.91	147.21	178.31	0.37	-11.61
			376	-366.78	-1.91	449.19	178.31	22.05	-11.61
258	Primo Impalcato	11	0	335.27	3.94	195.98	126.05	-25.05	-13.27
			188	335.27	3.94	166.47	126.05	-0.26	-13.27
			376	335.27	3.94	384.43	126.05	24.83	-13.27
259	Primo Impalcato	12	0	484.17	-3.33	250.02	159.84	-24.67	-13.12
			188	484.17	-3.33	178.16	159.84	-0.22	-13.12
			376	484.17	-3.33	438.10	159.84	24.67	-13.12
260	Primo Impalcato	13	0	703.61	2.87	238.62	160.68	-21.26	-11.29
			188	703.61	2.87	153.73	160.68	0.24	-11.29
			376	703.61	2.87	432.87	160.68	21.21	-11.29
261	Primo Impalcato	14	0	-1082.34	37.66	24.97	-12.98	466.68	253.85
			188	-1082.34	37.66	11.22	-12.98	55.36	253.85
			376	-1082.34	37.66	-30.16	-12.98	-489.11	253.85
262	Primo Impalcato	15	0	-1275.90	20.41	15.99	-8.21	-681.08	-542.12
			188	-1275.90	20.41	0.76	-8.21	528.67	-542.12
			376	-1275.90	20.41	-14.89	-8.21	1430.56	-542.12
263	Primo Impalcato	16	0	2007.25	22.98	-19.96	10.29	-1231.95	-825.37
			188	2007.25	22.98	-1.02	10.29	521.74	-825.37
			376	2007.25	22.98	18.76	10.29	1933.72	-825.37
264	Primo Impalcato	17	0	-1438.86	20.97	14.26	-7.59	-994.90	-914.64
			188	-1438.86	20.97	-0.93	-7.59	997.31	-914.64
			376	-1438.86	20.97	-14.30	-7.59	2573.61	-914.64
265	Primo Impalcato	18	0	2246.43	21.89	17.31	9.34	-1668.13	-1250.20
			188	2246.43	21.89	0.94	9.34	991.30	-1250.20
			376	2246.43	21.89	17.81	9.34	3159.58	-1250.20
266	Primo Impalcato	19	0	-1616.32	23.22	16.69	-8.65	-744.61	-1063.86
			188	-1616.32	23.22	-1.22	-8.65	1479.30	-1063.86
			376	-1616.32	23.22	-15.86	-8.65	3409.53	-1063.86
267	Primo Impalcato	20	0	2253.75	24.28	20.58	-10.74	-1266.77	-1287.14
			188	2253.75	24.28	1.11	-10.74	1492.35	-1287.14
			376	2253.75	24.28	-19.81	-10.74	3754.86	-1287.14
268	Primo Impalcato	21	0	-1621.27	24.94	-17.62	-9.23	804.15	-1349.49
			188	-1621.27	24.94	-1.38	-9.23	1981.30	-1349.49
			376	-1621.27	24.94	-17.11	-9.23	4434.25	-1349.49
269	Primo Impalcato	22	0	1896.77	22.59	22.13	-11.55	-887.47	-1388.23
			188	1896.77	22.59	1.20	-11.55	1972.52	-1388.23
			376	1896.77	22.59	-21.29	-11.55	4510.48	-1388.23
270	Primo Impalcato	23	0	-1969.66	21.97	21.01	-10.95	1174.03	-1747.20
			188	-1969.66	21.97	-1.48	-10.95	2449.94	-1747.20
			376	-1969.66	21.97	-20.17	-10.95	5632.51	-1747.20

271	Primo Impalcato	24	0	1971.40	21.18	23.37	-12.25	-791.33	-1599.01
			188	1971.40	21.18	1.06	-12.25	2443.88	-1599.01
			376	1971.40	21.18	-22.71	-12.25	5403.48	-1599.01
272	Primo Impalcato	25	0	-2624.68	19.46	21.85	-11.35	-1592.13	-2177.77
			188	-2624.68	19.46	-1.63	-11.35	2936.49	-2177.77
			376	-2624.68	19.46	-20.85	-11.35	6880.74	-2177.77
273	Primo Impalcato	26	0	2384.84	20.80	20.83	-11.13	-1129.35	-2003.04
			188	2384.84	20.80	1.16	-11.13	2927.66	-2003.04
			376	2384.84	20.80	-21.01	-11.13	6610.79	-2003.04
274	Primo Impalcato	27	0	2588.04	18.74	21.53	-11.32	-1167.64	-2204.48
			188	2588.04	18.74	0.56	-11.32	3303.36	-2204.48
			376	2588.04	18.74	-21.03	-11.32	7353.49	-2204.48
275	Primo Impalcato	28	0	-2739.14	15.16	-19.38	10.03	-1375.23	-2297.75
			188	-2739.14	15.16	-1.37	10.03	3327.36	-2297.75
			376	-2739.14	15.16	-18.37	10.03	7517.33	-2297.75
276	Primo Impalcato	29	0	2697.11	15.66	23.27	-12.25	-1464.97	-2488.77
			188	2697.11	15.66	0.98	-12.25	3589.55	-2488.77
			376	2697.11	15.66	-22.79	-12.25	8172.75	-2488.77
277	Primo Impalcato	30	0	-2896.28	13.89	21.56	-11.22	-1307.90	-2436.60
			188	-2896.28	13.89	-1.26	-11.22	3612.06	-2436.60
			376	-2896.28	13.89	-20.66	-11.22	8098.73	-2436.60
278	Primo Impalcato	31	0	2766.29	12.18	-24.98	13.05	-1651.05	-2679.17
			188	2766.29	12.18	0.61	13.05	3801.40	-2679.17
			376	2766.29	12.18	24.10	13.05	8733.56	-2679.17
279	Primo Impalcato	32	0	-2964.42	11.63	20.56	-10.88	-1239.83	-2493.54
			188	-2964.42	11.63	-1.07	-10.88	3814.48	-2493.54
			376	-2964.42	11.63	-20.37	-10.88	8398.76	-2493.54
280	Primo Impalcato	33	0	2667.59	9.42	-24.01	12.60	1468.28	-2660.74
			188	2667.59	9.42	0.83	12.60	3926.47	-2660.74
			376	2667.59	9.42	23.40	12.60	8832.15	-2660.74
281	Primo Impalcato	34	0	-2876.16	8.52	20.29	-10.83	-1425.46	-2659.34
			188	-2876.16	8.52	-1.15	-10.83	3928.96	-2659.34
			376	-2876.16	8.52	-20.46	-10.83	8842.31	-2659.34
282	Primo Impalcato	35	0	2828.91	5.90	-22.03	11.70	1487.46	-2683.33
			188	2828.91	5.90	-0.56	11.70	3951.77	-2683.33
			376	2828.91	5.90	21.98	11.70	8896.63	-2683.33
283	Primo Impalcato	36	0	-3022.61	-8.04	22.44	-11.85	1324.20	-2632.60
			188	-3022.61	-8.04	-1.18	-11.85	3954.37	-2632.60
			376	-3022.61	-8.04	-22.15	-11.85	8820.18	-2632.60
284	Primo Impalcato	37	0	2734.94	-9.88	-21.67	11.31	-1402.25	-2594.36
			188	2734.94	-9.88	-0.64	11.31	3907.65	-2594.36
			376	2734.94	-9.88	20.85	11.31	8661.02	-2594.36
285	Primo Impalcato	38	0	-3048.68	-9.22	22.03	-11.66	1485.02	-2657.70
			188	-3048.68	-9.22	-1.03	-11.66	3886.35	-2657.70
			376	-3048.68	-9.22	-21.83	-11.66	8779.67	-2657.70
286	Primo Impalcato	39	0	2825.49	-9.77	-22.33	11.95	-1554.02	-2614.48
			188	2825.49	-9.77	0.91	11.95	3758.58	-2614.48
			376	2825.49	-9.77	22.79	11.95	8571.96	-2614.48
287	Primo Impalcato	40	0	-2781.04	-10.88	20.41	-10.73	1505.26	-2587.21
			188	-2781.04	-10.88	0.69	-10.73	3740.39	-2587.21
			376	-2781.04	-10.88	-19.92	-10.73	8503.22	-2587.21
288	Primo Impalcato	41	0	2753.69	-11.66	-31.36	16.25	-1584.67	-2538.93
			188	2753.69	-11.66	-1.06	16.25	3592.63	-2538.93
			376	2753.69	-11.66	29.76	16.25	8239.15	-2538.93
289	Primo	42	0	-2224.93	-14.50	21.88	-11.57	1096.14	-2275.48

	Impalcato								
			188	-2224.93	-14.50	0.86	-11.57	3511.98	-2275.48
			376	-2224.93	-14.50	-21.64	-11.57	7699.94	-2275.48
290	Primo Impalcato	43	0	-2170.53	-15.21	23.85	-12.76	1128.48	-2270.03
			188	-2170.53	-15.21	-0.76	-12.76	3429.41	-2270.03
			376	-2170.53	-15.21	-24.12	-12.76	7633.38	-2270.03
291	Primo Impalcato	44	0	2402.35	-16.52	-28.54	14.78	-1204.70	-2295.39
			188	2402.35	-16.52	-1.34	14.78	3451.53	-2295.39
			376	2402.35	-16.52	27.05	14.78	7680.77	-2295.39
292	Primo Impalcato	45	0	-2313.57	-17.26	29.43	-15.54	1546.71	-2253.31
			188	-2313.57	-17.26	0.53	-15.54	3099.70	-2253.31
			376	-2313.57	-17.26	-28.99	-15.54	7206.74	-2253.31
293	Primo Impalcato	46	0	2223.05	-17.14	-30.14	15.49	-1505.70	-2233.24
			188	2223.05	-17.14	1.16	15.49	3113.25	-2233.24
			376	2223.05	-17.14	28.33	15.49	7182.68	-2233.24
294	Primo Impalcato	47	0	-2076.56	-21.58	30.33	-15.99	1238.40	-1887.59
			188	-2076.56	-21.58	0.77	-15.99	2684.60	-1887.59
			376	-2076.56	-21.58	-29.80	-15.99	6099.30	-1887.59
295	Primo Impalcato	48	0	1890.14	-22.02	-31.79	16.70	-1381.21	-1955.53
			188	1890.14	-22.02	0.95	16.70	2679.23	-1955.53
			376	1890.14	-22.02	31.01	16.70	6231.93	-1955.53
296	Primo Impalcato	49	0	-1916.88	-24.75	30.90	-16.11	-1011.84	-1548.04
			188	-1916.88	-24.75	1.03	-16.11	2182.29	-1548.04
			376	-1916.88	-24.75	-29.67	-16.11	5001.87	-1548.04
297	Primo Impalcato	50	0	-1829.35	-26.91	-33.49	17.62	816.39	-1462.94
			188	-1829.35	-26.91	1.19	17.62	2199.47	-1462.94
			376	-1829.35	-26.91	32.86	17.62	4850.22	-1462.94
298	Primo Impalcato	51	0	-1879.65	-26.76	28.84	-14.99	-1267.16	-1386.80
			188	-1879.65	-26.76	1.04	-14.99	1678.02	-1386.80
			376	-1879.65	-26.76	-27.51	-14.99	4145.63	-1386.80
299	Primo Impalcato	52	0	-1850.08	-25.09	-38.28	19.98	1062.86	-1319.92
			188	-1850.08	-25.09	1.12	19.98	1662.33	-1319.92
			376	-1850.08	-25.09	36.87	19.98	4067.94	-1319.92
300	Primo Impalcato	53	0	-2272.28	-25.65	24.93	-13.15	-1842.99	-1385.12
			188	-2272.28	-25.65	-0.75	-13.15	1146.67	-1385.12
			376	-2272.28	-25.65	-24.54	-13.15	3516.90	-1385.12
301	Primo Impalcato	54	0	-2002.14	-24.86	-35.02	18.39	-1300.64	-1131.11
			188	-2002.14	-24.86	0.67	18.39	1152.06	-1131.11
			376	-2002.14	-24.86	34.12	18.39	3102.16	-1131.11
302	Primo Impalcato	55	0	1990.07	-25.09	23.58	-12.09	-1433.85	-951.17
			188	1990.07	-25.09	-1.05	-12.09	616.07	-951.17
			376	1990.07	-25.09	-21.90	-12.09	2228.75	-951.17
303	Primo Impalcato	56	0	-1650.25	-22.59	-27.48	14.47	938.42	-699.20
			188	-1650.25	-22.59	0.92	14.47	619.55	-699.20
			376	-1650.25	-22.59	26.92	14.47	1785.26	-699.20
304	Primo Impalcato	57	0	1571.04	-38.91	16.26	-10.70	534.95	294.11
			188	1571.04	-38.91	-9.42	-10.70	55.18	294.11
			376	1571.04	-38.91	-25.02	-10.70	-572.16	294.11
305	Primo Impalcato	58	0	693.48	-2.50	261.35	176.83	-25.56	-13.56
			188	693.48	-2.50	95.95	176.83	0.26	-13.56
			376	693.48	-2.50	409.21	176.83	25.41	-13.56
306	Primo Impalcato	59	0	-476.70	3.21	205.55	139.42	-30.20	-16.03
			188	-476.70	3.21	132.66	139.42	-0.22	-16.03
			376	-476.70	3.21	364.19	139.42	30.06	-16.03
307	Primo Impalcato	60	0	349.40	-3.71	-157.07	101.14	-30.64	-16.20

			188	349.40	-3.71	132.94	101.14	-0.29	-16.20
			376	349.40	-3.71	307.32	101.14	30.29	-16.20
308	Primo Impalcato	61	0	428.65	1.59	-276.63	161.48	-26.15	-14.05
			188	428.65	1.59	124.43	161.48	0.44	-14.05
			376	428.65	1.59	399.36	161.48	26.69	-14.05
309	Primo Impalcato	62	0	-460.39	4.72	-152.19	77.06	-25.85	-13.88
			188	-460.39	4.72	86.23	77.06	0.38	-13.88
			376	-460.39	4.72	195.57	77.06	26.35	-13.88
310	Primo Impalcato	63	0	-151.31	3.45	222.93	-125.82	-29.88	-15.75
			188	-151.31	3.45	39.10	-125.82	-0.36	-15.75
			376	-151.31	3.45	-264.31	-125.82	29.33	-15.75
311	Primo Impalcato	64	0	153.66	3.45	222.13	-126.41	-29.95	-15.78
			188	153.66	3.45	-39.28	-126.41	-0.37	-15.78
			376	153.66	3.45	-267.81	-126.41	29.39	-15.78
312	Primo Impalcato	65	0	478.75	4.77	166.42	-86.70	-25.72	-13.83
			188	478.75	4.77	-89.19	-86.70	0.37	-13.83
			376	478.75	4.77	-215.24	-86.70	26.29	-13.83
313	Primo Impalcato	66	0	-408.66	1.33	278.61	-161.95	-25.69	-13.83
			188	-408.66	1.33	-124.17	-161.95	0.42	-13.83
			376	-408.66	1.33	-399.14	-161.95	26.32	-13.83
314	Primo Impalcato	67	0	-337.05	-3.75	-143.70	-96.22	-29.90	-15.82
			188	-337.05	-3.75	-133.00	-96.22	-0.31	-15.82
			376	-337.05	-3.75	-302.42	-96.22	29.57	-15.82
315	Primo Impalcato	68	0	-493.45	3.24	218.75	-148.32	-29.02	-15.42
			188	-493.45	3.24	-135.16	-148.32	0.23	-15.42
			376	-493.45	3.24	-382.05	-148.32	28.97	-15.42
316	Primo Impalcato	69	0	-678.45	-2.52	-254.89	-174.40	-24.51	-13.00
			188	-678.45	-2.52	-94.01	-174.40	0.24	-13.00
			376	-678.45	-2.52	-407.26	-174.40	24.36	-13.00
317	Primo Impalcato	70	0	-1573.16	-40.47	-34.68	20.00	493.77	268.43
			188	-1573.16	-40.47	7.12	20.00	60.23	268.43
			376	-1573.16	-40.47	41.49	20.00	-516.85	268.43
318	Fondazio ne	1, 71	0	-276.34	0.53	0.00	0.00	5.72	-7.66
			102	-276.34	0.53	0.00	0.00	6.93	-7.66
			204	-276.34	0.53	0.00	0.00	12.55	-7.66
319	Fondazio ne	1, 92	0	916.62	0.29	0.00	0.00	9.37	5.58
			103	916.62	0.29	0.00	0.00	6.25	5.58
			206	916.62	0.29	0.00	0.00	6.21	5.58
320	Primo Impalcato	92, 2	0	-971.61	0.64	0.00	0.00	-13.32	-14.88
			103	-971.61	0.64	0.00	0.00	2.21	-14.88
			206	-971.61	0.64	0.00	0.00	17.37	-14.88
321	Fondazio ne	6, 89	0	1021.58	-0.32	0.00	0.00	-13.67	-9.63
			100	1021.58	-0.32	0.00	0.00	-4.20	-9.63
			200	1021.58	-0.32	0.00	0.00	5.64	-9.63
322	Primo Impalcato	89, 7	0	-1033.88	0.37	0.00	0.00	12.90	12.91
			100	-1033.88	0.37	0.00	0.00	3.72	12.91
			200	-1033.88	0.37	0.00	0.00	-14.66	12.91
323	Fondazio ne	9, 90	0	1057.80	0.37	0.00	0.00	-11.90	-6.03
			100	1057.80	0.37	0.00	0.00	-6.70	-6.03
			200	1057.80	0.37	0.00	0.00	-7.06	-6.03
324	Primo Impalcato	90, 10	0	-1035.32	-0.65	0.00	0.00	12.62	14.60
			100	-1035.32	-0.65	0.00	0.00	-4.03	14.60
			200	-1035.32	-0.65	0.00	0.00	-17.98	14.60
325	Fondazio ne	13, 91	0	995.00	0.63	0.00	0.00	-16.75	-14.11
			103	995.00	0.63	0.00	0.00	-2.37	-14.11

			206	995.00	0.63	0.00	0.00	12.32	-14.11
326	Primo Impalcato	88, 14	0	398.32	0.64	0.00	0.00	-12.88	-7.00
			102	398.32	0.64	0.00	0.00	-8.69	-7.00
			204	398.32	0.64	0.00	0.00	6.98	-7.00
327	Primo Impalcato	91, 14	0	-915.13	0.28	0.00	0.00	-6.49	-5.16
			103	-915.13	0.28	0.00	0.00	-6.26	-5.16
			206	-915.13	0.28	0.00	0.00	9.00	-5.16
328	Primo Impalcato	71, 15	0	293.74	0.80	0.00	0.00	-11.82	-11.47
			102	293.74	0.80	0.00	0.00	2.24	-11.47
			204	293.74	0.80	0.00	0.00	12.01	-11.47
329	Fondazio ne	16, 88	0	-383.46	0.99	0.00	0.00	-17.74	-16.28
			102	-383.46	0.99	0.00	0.00	-2.19	-16.28
			204	-383.46	0.99	0.00	0.00	15.78	-16.28
330	Fondazio ne	17, 72	0	-304.47	-0.30	0.00	0.00	32.29	14.08
			100	-304.47	-0.30	0.00	0.00	21.58	14.08
			199	-304.47	-0.30	0.00	0.00	28.03	14.08
331	Primo Impalcato	87, 18	0	385.56	0.51	0.00	0.00	-33.48	22.46
			100	385.56	0.51	0.00	0.00	-23.11	22.46
			199	385.56	0.51	0.00	0.00	-42.20	22.46
332	Primo Impalcato	72, 19	0	372.11	1.33	0.00	0.00	-9.16	-21.48
			100	372.11	1.33	0.00	0.00	16.83	-21.48
			199	372.11	1.33	0.00	0.00	37.73	-21.48
333	Fondazio ne	20, 87	0	-586.54	1.39	0.00	0.00	-46.02	-27.31
			100	-586.54	1.39	0.00	0.00	-19.24	-27.31
			199	-586.54	1.39	0.00	0.00	12.27	-27.31
334	Fondazio ne	21, 73	0	-404.95	-0.64	0.00	0.00	47.66	13.14
			100	-404.95	-0.64	0.00	0.00	35.87	13.14
			199	-404.95	-0.64	0.00	0.00	32.04	13.14
335	Primo Impalcato	86, 22	0	430.50	-0.61	0.00	0.00	-33.23	14.12
			100	430.50	-0.61	0.00	0.00	-35.21	14.12
			199	430.50	-0.61	0.00	0.00	-47.64	14.12
336	Primo Impalcato	73, 23	0	492.01	1.95	0.00	0.00	20.11	-27.46
			100	492.01	1.95	0.00	0.00	30.31	-27.46
			199	492.01	1.95	0.00	0.00	56.39	-27.46
337	Fondazio ne	24, 86	0	-612.94	1.83	0.00	0.00	-54.78	-25.62
			100	-612.94	1.83	0.00	0.00	-30.54	-25.62
			199	-612.94	1.83	0.00	0.00	-17.74	-25.62
338	Fondazio ne	25, 74	0	-487.68	-1.67	0.00	0.00	71.64	26.76
			103	-487.68	-1.67	0.00	0.00	46.40	26.76
			206	-487.68	-1.67	0.00	0.00	43.61	26.76
339	Primo Impalcato	85, 26	0	-484.33	-1.13	0.00	0.00	-42.31	23.90
			100	-484.33	-1.13	0.00	0.00	-48.91	23.90
			199	-484.33	-1.13	0.00	0.00	-71.21	23.90
340	Fondazio ne	27, 85	0	-551.85	2.14	0.00	0.00	-75.21	-31.94
			100	-551.85	2.14	0.00	0.00	-44.11	-31.94
			199	-551.85	2.14	0.00	0.00	-27.51	-31.94
341	Primo Impalcato	74, 28	0	571.18	2.44	0.00	0.00	29.11	-33.20
			103	571.18	2.44	0.00	0.00	42.13	-33.20
			206	571.18	2.44	0.00	0.00	74.13	-33.20
342	Primo Impalcato	84, 29	0	-506.21	-1.62	0.00	0.00	-44.63	30.69
			100	-506.21	-1.62	0.00	0.00	-57.46	30.69
			199	-506.21	-1.62	0.00	0.00	-86.37	30.69
343	Fondazio ne	31, 84	0	-561.05	2.29	0.00	0.00	-90.60	-37.87
			100	-561.05	2.29	0.00	0.00	-54.52	-37.87
			199	-561.05	2.29	0.00	0.00	-39.24	-37.87

344	Primo Impalcato	83, 33	0	562.87	-2.06	0.00	0.00	-43.22	33.27
			100	562.87	-2.06	0.00	0.00	-59.08	33.27
			199	562.87	-2.06	0.00	0.00	-90.97	33.27
345	Fondazione	35, 83	0	-650.21	2.08	0.00	0.00	-92.33	-35.76
			100	-650.21	2.08	0.00	0.00	-58.65	-35.76
			199	-650.21	2.08	0.00	0.00	-44.31	-35.76
346	Primo Impalcato	82, 37	0	493.19	-2.15	0.00	0.00	-38.92	33.50
			100	493.19	-2.15	0.00	0.00	-56.69	33.50
			199	493.19	-2.15	0.00	0.00	-88.55	33.50
347	Fondazione	39, 82	0	-732.67	1.90	0.00	0.00	-87.83	-32.72
			100	-732.67	1.90	0.00	0.00	-57.50	-32.72
			199	-732.67	1.90	0.00	0.00	-46.21	-32.72
348	Primo Impalcato	78, 43	0	-530.94	-2.05	0.00	0.00	-29.68	33.99
			100	-530.94	-2.05	0.00	0.00	-48.11	33.99
			199	-530.94	-2.05	0.00	0.00	-81.18	33.99
349	Primo Impalcato	81, 44	0	458.28	-2.15	0.00	0.00	-30.06	31.99
			100	458.28	-2.15	0.00	0.00	-48.40	31.99
			199	458.28	-2.15	0.00	0.00	-79.10	31.99
350	Fondazione	45, 78	0	697.56	1.36	0.00	0.00	-77.62	-29.28
			100	697.56	1.36	0.00	0.00	-50.50	-29.28
			199	697.56	1.36	0.00	0.00	-45.21	-29.28
351	Fondazione	46, 81	0	-722.77	1.50	0.00	0.00	-75.19	-28.20
			100	-722.77	1.50	0.00	0.00	-49.91	-28.20
			199	-722.77	1.50	0.00	0.00	-45.11	-28.20
352	Primo Impalcato	77, 47	0	-554.24	-1.98	0.00	0.00	-21.99	29.72
			100	-554.24	-1.98	0.00	0.00	-33.63	29.72
			199	-554.24	-1.98	0.00	0.00	-62.00	29.72
353	Primo Impalcato	80, 48	0	546.26	-2.10	0.00	0.00	-22.70	30.26
			100	546.26	-2.10	0.00	0.00	-33.13	30.26
			199	546.26	-2.10	0.00	0.00	-62.26	30.26
354	Fondazione	49, 77	0	717.15	0.67	0.00	0.00	-54.57	-17.53
			100	717.15	0.67	0.00	0.00	-39.08	-17.53
			199	717.15	0.67	0.00	0.00	-36.46	-17.53
355	Fondazione	50, 80	0	-750.90	0.70	0.00	0.00	-53.06	-14.54
			100	-750.90	0.70	0.00	0.00	-39.76	-14.54
			199	-750.90	0.70	0.00	0.00	-33.53	-14.54
356	Primo Impalcato	76, 51	0	-617.02	-1.56	0.00	0.00	-13.08	28.75
			100	-617.02	-1.56	0.00	0.00	-21.47	28.75
			199	-617.02	-1.56	0.00	0.00	-49.73	28.75
357	Fondazione	53, 76	0	608.22	0.56	0.00	0.00	-45.64	-23.41
			100	608.22	0.56	0.00	0.00	-25.79	-23.41
			199	608.22	0.56	0.00	0.00	-36.28	-23.41
358	Primo Impalcato	75, 55	0	-371.19	-1.11	0.00	0.00	17.60	18.76
			102	-371.19	-1.11	0.00	0.00	-2.58	18.76
			204	-371.19	-1.11	0.00	0.00	-20.72	18.76
359	Fondazione	56, 79	0	404.56	-0.94	0.00	0.00	15.97	15.04
			102	404.56	-0.94	0.00	0.00	2.65	15.04
			204	404.56	-0.94	0.00	0.00	-14.97	15.04
360	Fondazione	57, 75	0	466.17	-0.68	0.00	0.00	-8.21	8.39
			102	466.17	-0.68	0.00	0.00	-10.00	8.39
			204	466.17	-0.68	0.00	0.00	-14.10	8.39
361	Fondazione	57, 93	0	1060.69	-0.31	0.00	0.00	8.98	4.85
			103	1060.69	-0.31	0.00	0.00	-5.70	4.85
			206	1060.69	-0.31	0.00	0.00	-5.38	4.85
362	Primo	93, 58	0	1168.26	-0.60	0.00	0.00	13.84	14.87

	Impalcato								
			103	1168.26	-0.60	0.00	0.00	-1.50	14.87
			206	1168.26	-0.60	0.00	0.00	-16.73	14.87
363	Fondazio ne	61, 95	0	1244.35	0.62	0.00	0.00	-15.75	-13.32
			100	1244.35	0.62	0.00	0.00	-3.32	-13.32
			200	1244.35	0.62	0.00	0.00	12.07	-13.32
364	Primo Impalcato	95, 62	0	-1275.75	-0.38	0.00	0.00	-6.05	-4.56
			100	-1275.75	-0.38	0.00	0.00	-5.85	-4.56
			200	-1275.75	-0.38	0.00	0.00	9.22	-4.56
365	Primo Impalcato	96, 65	0	1252.98	0.39	0.00	0.00	-5.78	-3.30
			100	1252.98	0.39	0.00	0.00	-5.86	-3.30
			200	1252.98	0.39	0.00	0.00	-8.47	-3.30
366	Fondazio ne	66, 96	0	-1238.19	0.62	0.00	0.00	-15.44	-13.37
			100	-1238.19	0.62	0.00	0.00	-3.01	-13.37
			200	-1238.19	0.62	0.00	0.00	12.38	-13.37
367	Fondazio ne	69, 94	0	-1106.22	-0.61	0.00	0.00	17.05	15.35
			103	-1106.22	-0.61	0.00	0.00	1.34	15.35
			206	-1106.22	-0.61	0.00	0.00	-14.51	15.35
368	Primo Impalcato	79, 70	0	-501.29	-0.60	0.00	0.00	13.69	8.70
			102	-501.29	-0.60	0.00	0.00	8.45	8.70
			204	-501.29	-0.60	0.00	0.00	-7.13	8.70
369	Primo Impalcato	94, 70	0	-1016.73	-0.31	0.00	0.00	5.97	5.37
			103	-1016.73	-0.31	0.00	0.00	5.72	5.37
			206	-1016.73	-0.31	0.00	0.00	-9.12	5.37
370	Primo Impalcato	1, 71	0	293.28	0.87	0.00	0.00	-15.19	9.28
			102	293.28	0.87	0.00	0.00	-8.05	9.28
			204	293.28	0.87	0.00	0.00	-11.86	9.28
371	Primo Impalcato	1, 92	0	-968.14	0.95	0.00	0.00	-14.70	11.61
			103	-968.14	0.95	0.00	0.00	-8.43	11.61
			206	-968.14	0.95	0.00	0.00	-14.47	11.61
372	Primo Impalcato	92, 2	0	914.18	-0.69	0.00	0.00	5.87	-5.40
			103	914.18	-0.69	0.00	0.00	7.81	-5.40
			206	914.18	-0.69	0.00	0.00	12.14	-5.40
373	Primo Impalcato	6, 89	0	-1031.18	-0.94	0.00	0.00	5.10	-6.39
			100	-1031.18	-0.94	0.00	0.00	7.90	-6.39
			200	-1031.18	-0.94	0.00	0.00	13.48	-6.39
374	Primo Impalcato	89, 7	0	1018.76	0.99	0.00	0.00	5.31	2.47
			100	1018.76	0.99	0.00	0.00	6.01	2.47
			200	1018.76	0.99	0.00	0.00	-7.65	2.47
375	Primo Impalcato	9, 90	0	-1032.67	-0.84	0.00	0.00	5.06	-8.94
			100	-1032.67	-0.84	0.00	0.00	6.21	-8.94
			200	-1032.67	-0.84	0.00	0.00	13.88	-8.94
376	Primo Impalcato	90, 10	0	1055.08	0.59	0.00	0.00	-6.96	5.43
			100	1055.08	0.59	0.00	0.00	-7.12	5.43
			200	1055.08	0.59	0.00	0.00	-10.26	5.43
377	Primo Impalcato	13, 91	0	-913.81	-0.65	0.00	0.00	-11.90	5.76
			103	-913.81	-0.65	0.00	0.00	-7.59	5.76
			206	-913.81	-0.65	0.00	0.00	-6.82	5.76
378	Primo Impalcato	88, 14	0	-381.15	0.85	0.00	0.00	16.02	13.90
			102	-381.15	0.85	0.00	0.00	7.79	13.90
			204	-381.15	0.85	0.00	0.00	19.05	13.90
379	Primo Impalcato	91, 14	0	991.58	1.03	0.00	0.00	13.46	11.40
			103	991.58	1.03	0.00	0.00	8.50	11.40
			206	991.58	1.03	0.00	0.00	16.24	11.40
380	Primo Impalcato	71, 15	0	-274.31	1.06	0.00	0.00	12.94	3.50

			102	-274.31	1.06	0.00	0.00	12.00	3.50
			204	-274.31	1.06	0.00	0.00	13.34	3.50
381	Primo Impalcato	16, 88	0	394.20	1.15	0.00	0.00	-16.08	-5.59
			102	394.20	1.15	0.00	0.00	-11.89	-5.59
			204	394.20	1.15	0.00	0.00	-13.62	-5.59
382	Primo Impalcato	17, 72	0	367.97	1.28	0.00	0.00	-13.08	-9.00
			100	367.97	1.28	0.00	0.00	-8.06	-9.00
			199	367.97	1.28	0.00	0.00	-10.04	-9.00
383	Primo Impalcato	87, 18	0	-580.16	1.36	0.00	0.00	12.78	-10.27
			100	-580.16	1.36	0.00	0.00	10.07	-10.27
			199	-580.16	1.36	0.00	0.00	13.98	-10.27
384	Primo Impalcato	72, 19	0	-302.56	1.07	0.00	0.00	27.29	9.54
			100	-302.56	1.07	0.00	0.00	18.18	9.54
			199	-302.56	1.07	0.00	0.00	13.17	9.54
385	Primo Impalcato	20, 87	0	382.05	1.07	0.00	0.00	-12.84	12.64
			100	382.05	1.07	0.00	0.00	-20.76	12.64
			199	382.05	1.07	0.00	0.00	-32.94	12.64
386	Primo Impalcato	21, 73	0	487.98	1.62	0.00	0.00	-14.04	-17.75
			100	487.98	1.62	0.00	0.00	5.11	-17.75
			199	487.98	1.62	0.00	0.00	21.63	-17.75
387	Primo Impalcato	86, 22	0	-607.69	1.56	0.00	0.00	-19.17	-16.12
			100	-607.69	1.56	0.00	0.00	4.66	-16.12
			199	-607.69	1.56	0.00	0.00	13.79	-16.12
388	Primo Impalcato	73, 23	0	-401.17	0.83	0.00	0.00	31.22	10.80
			100	-401.17	0.83	0.00	0.00	20.85	10.80
			199	-401.17	0.83	0.00	0.00	12.60	10.80
389	Primo Impalcato	24, 86	0	428.79	0.87	0.00	0.00	-10.83	12.11
			100	428.79	0.87	0.00	0.00	-20.99	12.11
			199	428.79	0.87	0.00	0.00	-32.54	12.11
390	Primo Impalcato	25, 74	0	567.35	1.53	0.00	0.00	-15.96	-21.52
			103	567.35	1.53	0.00	0.00	10.25	-21.52
			206	567.35	1.53	0.00	0.00	30.30	-21.52
391	Primo Impalcato	85, 26	0	-548.50	1.63	0.00	0.00	-28.56	-18.81
			100	-548.50	1.63	0.00	0.00	-10.61	-18.81
			199	-548.50	1.63	0.00	0.00	12.01	-18.81
392	Primo Impalcato	27, 85	0	-478.56	0.60	0.00	0.00	-9.84	18.24
			100	-478.56	0.60	0.00	0.00	-24.61	18.24
			199	-478.56	0.60	0.00	0.00	-42.05	18.24
393	Primo Impalcato	74, 28	0	-483.92	-0.47	0.00	0.00	43.77	20.95
			103	-483.92	-0.47	0.00	0.00	24.42	20.95
			206	-483.92	-0.47	0.00	0.00	12.74	20.95
394	Primo Impalcato	84, 29	0	-558.45	1.48	0.00	0.00	-40.15	-22.99
			100	-558.45	1.48	0.00	0.00	-17.36	-22.99
			199	-558.45	1.48	0.00	0.00	9.49	-22.99
395	Primo Impalcato	31, 84	0	-498.64	-0.67	0.00	0.00	-6.57	20.58
			100	-498.64	-0.67	0.00	0.00	-24.41	20.58
			199	-498.64	-0.67	0.00	0.00	-44.56	20.58
396	Primo Impalcato	83, 33	0	-646.05	1.17	0.00	0.00	-44.78	-23.87
			100	-646.05	1.17	0.00	0.00	-21.05	-23.87
			199	-646.05	1.17	0.00	0.00	6.69	-23.87
397	Primo Impalcato	35, 83	0	557.45	-0.98	0.00	0.00	4.98	22.79
			100	557.45	-0.98	0.00	0.00	-21.91	22.79
			199	557.45	-0.98	0.00	0.00	-43.72	22.79
398	Primo Impalcato	82, 37	0	-728.58	0.69	0.00	0.00	-46.59	-23.08
			100	-728.58	0.69	0.00	0.00	-23.63	-23.08

			199	-728.58	0.69	0.00	0.00	-4.28	-23.08
399	Primo Impalcato	39, 82	0	489.31	-1.22	0.00	0.00	7.66	21.74
			100	489.31	-1.22	0.00	0.00	-17.82	21.74
			199	489.31	-1.22	0.00	0.00	-39.36	21.74
400	Primo Impalcato	78, 43	0	694.94	0.43	0.00	0.00	-45.08	-20.77
			100	694.94	0.43	0.00	0.00	-24.48	-20.77
			199	694.94	0.43	0.00	0.00	-7.68	-20.77
401	Primo Impalcato	81, 44	0	-720.17	-0.54	0.00	0.00	-44.93	-20.75
			100	-720.17	-0.54	0.00	0.00	-24.34	-20.75
			199	-720.17	-0.54	0.00	0.00	-8.67	-20.75
402	Primo Impalcato	45, 78	0	-525.99	-1.56	0.00	0.00	13.23	19.08
			100	-525.99	-1.56	0.00	0.00	-13.17	19.08
			199	-525.99	-1.56	0.00	0.00	-30.37	19.08
403	Primo Impalcato	46, 81	0	453.53	-1.55	0.00	0.00	12.70	20.37
			100	453.53	-1.55	0.00	0.00	-11.96	20.37
			199	453.53	-1.55	0.00	0.00	-31.15	20.37
404	Primo Impalcato	77, 47	0	714.36	-0.93	0.00	0.00	-35.84	-13.53
			100	714.36	-0.93	0.00	0.00	-22.84	-13.53
			199	714.36	-0.93	0.00	0.00	-11.09	-13.53
405	Primo Impalcato	80, 48	0	-747.97	-0.91	0.00	0.00	-32.46	-11.87
			100	-747.97	-0.91	0.00	0.00	-21.82	-11.87
			199	-747.97	-0.91	0.00	0.00	-12.68	-11.87
406	Primo Impalcato	49, 77	0	-549.35	-1.75	0.00	0.00	13.73	18.34
			100	-549.35	-1.75	0.00	0.00	5.89	18.34
			199	-549.35	-1.75	0.00	0.00	-23.23	18.34
407	Primo Impalcato	50, 80	0	542.66	-1.83	0.00	0.00	14.49	18.84
			100	542.66	-1.83	0.00	0.00	5.97	18.84
			199	542.66	-1.83	0.00	0.00	-24.15	18.84
408	Primo Impalcato	76, 51	0	607.17	-1.20	0.00	0.00	-35.65	-13.71
			100	607.17	-1.20	0.00	0.00	-22.57	-13.71
			199	607.17	-1.20	0.00	0.00	-14.32	-13.71
409	Primo Impalcato	53, 76	0	-610.76	-1.60	0.00	0.00	16.48	10.92
			100	-610.76	-1.60	0.00	0.00	10.99	10.92
			199	-610.76	-1.60	0.00	0.00	-14.00	10.92
410	Primo Impalcato	75, 55	0	463.48	-1.31	0.00	0.00	-14.86	-6.28
			102	463.48	-1.31	0.00	0.00	-13.90	-6.28
			204	463.48	-1.31	0.00	0.00	-19.32	-6.28
411	Primo Impalcato	56, 79	0	-501.01	-1.21	0.00	0.00	16.45	3.81
			102	-501.01	-1.21	0.00	0.00	13.87	3.81
			204	-501.01	-1.21	0.00	0.00	13.78	3.81
412	Primo Impalcato	57, 75	0	-366.26	-0.79	0.00	0.00	18.87	-14.10
			102	-366.26	-0.79	0.00	0.00	8.15	-14.10
			204	-366.26	-0.79	0.00	0.00	17.77	-14.10
413	Primo Impalcato	57, 93	0	1162.92	-1.12	0.00	0.00	16.38	-11.25
			103	1162.92	-1.12	0.00	0.00	8.80	-11.25
			206	1162.92	-1.12	0.00	0.00	14.88	-11.25
414	Primo Impalcato	93, 58	0	1059.77	0.64	0.00	0.00	-5.84	-6.08
			103	1059.77	0.64	0.00	0.00	-6.07	-6.08
			206	1059.77	0.64	0.00	0.00	-10.14	-6.08
415	Primo Impalcato	61, 95	0	-1271.44	-0.55	0.00	0.00	9.55	-5.51
			100	-1271.44	-0.55	0.00	0.00	-5.64	-5.51
			200	-1271.44	-0.55	0.00	0.00	-6.28	-5.51
416	Primo Impalcato	95, 62	0	1240.40	0.78	0.00	0.00	13.37	9.18
			100	1240.40	0.78	0.00	0.00	5.31	9.18
			200	1240.40	0.78	0.00	0.00	5.32	9.18

417	Primo Impalcato	96, 65	0	-1235.30	0.79	0.00	0.00	13.69	9.38
			100	-1235.30	0.79	0.00	0.00	5.06	9.38
			200	-1235.30	0.79	0.00	0.00	6.04	9.38
418	Primo Impalcato	66, 96	0	1249.97	0.55	0.00	0.00	9.49	5.56
			100	1249.97	0.55	0.00	0.00	-5.37	5.56
			200	1249.97	0.55	0.00	0.00	-6.34	5.56
419	Primo Impalcato	69, 94	0	-1014.40	-0.65	0.00	0.00	9.90	5.51
			103	-1014.40	-0.65	0.00	0.00	6.21	5.51
			206	-1014.40	-0.65	0.00	0.00	5.67	5.51
420	Primo Impalcato	79, 70	0	404.88	-0.83	0.00	0.00	-15.05	10.64
			102	404.88	-0.83	0.00	0.00	-8.55	10.64
			204	404.88	-0.83	0.00	0.00	-15.84	10.64
421	Primo Impalcato	94, 70	0	-1101.00	-1.14	0.00	0.00	-15.62	-11.24
			103	-1101.00	-1.14	0.00	0.00	-8.82	-11.24
			206	-1101.00	-1.14	0.00	0.00	-14.10	-11.24
422	Copertura	1, 2	0	-816.85	-148.18	599.15	802.26	-2130.24	1069.65
			83	-816.85	-148.18	1138.13	802.26	-1488.86	1069.65
			166	-816.85	-148.18	1741.24	802.26	-1812.16	1069.65
423	Copertura	15, 1	0	1114.49	-108.65	1845.30	-1074.41	-909.54	1008.54
			80	1114.49	-108.65	-1039.56	-1074.41	-1498.23	1008.54
			159	1114.49	-108.65	-361.01	-1074.41	-2159.91	1008.54
424	Copertura	2, 3	0	-725.61	-145.03	1749.80	-531.06	-1804.37	-325.55
			69	-725.61	-145.03	1551.76	-531.06	-1859.88	-325.55
			138	-725.61	-145.03	1416.45	-531.06	-1922.62	-325.55
425	Copertura	3, 4	0	-581.84	70.33	1425.29	-514.67	-1921.73	-606.52
			69	-581.84	70.33	1206.97	-514.67	-1521.56	-606.52
			138	-581.84	70.33	1038.73	-514.67	-1134.68	-606.52
426	Copertura	4, 5	0	-468.26	138.17	1044.87	-476.48	-1138.14	-875.90
			69	-468.26	138.17	805.17	-476.48	-867.34	-875.90
			138	-468.26	138.17	-620.35	-476.48	-1196.09	-875.90
427	Copertura	5, 6	0	-407.06	118.74	-619.45	-397.13	-1195.91	-486.78
			69	-407.06	118.74	-729.29	-397.13	-1310.77	-486.78
			138	-407.06	118.74	-875.18	-397.13	-1442.43	-486.78
428	Copertura	6, 7	0	-229.68	126.14	-860.23	771.83	-1452.19	-576.71
			69	-229.68	126.14	-376.13	771.83	1055.07	-576.71
			138	-229.68	126.14	658.28	771.83	658.92	-576.71
429	Copertura	7, 8	0	78.27	158.55	672.43	-422.82	658.39	970.22
			69	78.27	158.55	470.56	-422.82	32.99	970.22
			138	78.27	158.55	-419.61	-422.82	-680.64	970.22
430	Copertura	8, 9	0	-190.58	134.75	410.83	-441.81	-676.66	-571.17
			69	-190.58	134.75	-685.41	-441.81	-1068.91	-571.17
			138	-190.58	134.75	-975.89	-441.81	1462.15	-571.17
431	Copertura	9, 10	0	289.24	109.91	-966.59	683.68	1458.41	-483.71
			69	289.24	109.91	820.81	683.68	1326.75	-483.71
			138	289.24	109.91	1050.55	683.68	1211.60	-483.71
432	Copertura	10, 11	0	437.83	144.72	1062.47	-476.34	1211.36	-888.75
			69	437.83	144.72	916.86	-476.34	872.36	-888.75
			138	437.83	144.72	1093.83	-476.34	1151.74	-888.75
433	Copertura	11, 12	0	583.05	-60.67	1086.60	-605.90	1148.42	-614.57
			69	583.05	-60.67	-1259.46	-605.90	1540.45	-614.57
			138	583.05	-60.67	-1461.33	-605.90	1945.97	-614.57
434	Copertura	12, 13	0	733.59	-142.50	-1453.71	-603.12	1947.18	-336.76
			69	733.59	-142.50	-1449.29	-603.12	1871.75	-336.76
			138	733.59	-142.50	-1655.33	-603.12	1804.01	-336.76
435	Copertura	13, 14	0	822.03	-145.87	-1647.14	815.08	1811.39	1094.90
			83	822.03	-145.87	-1077.77	815.08	1480.47	1094.90
			166	822.03	-145.87	-546.38	815.08	2149.87	1094.90
436	Copertura	16, 14	0	-1178.82	-103.10	2289.43	-1403.77	-893.47	1001.39
			80	-1178.82	-103.10	1229.21	-1403.77	-1488.12	1001.39
			159	-1178.82	-103.10	399.98	-1403.77	-2155.42	1001.39
437	Copertura	15, 17	0	1082.88	-114.72	1903.94	842.71	1190.06	957.06
			66	1082.88	-114.72	1850.56	842.71	747.82	957.06
			132	1082.88	-114.72	1823.78	842.71	654.30	957.06
438	Copertura	16, 18	0	-1175.64	-126.06	2336.95	999.12	1199.66	978.99
			66	-1175.64	-126.06	-2548.80	999.12	759.39	978.99
			132	-1175.64	-126.06	-2771.39	999.12	669.52	978.99
439	Copertura	17, 19	0	1194.35	-127.11	1883.85	-927.53	909.09	851.73
			66	1194.35	-127.11	1882.68	-927.53	433.27	851.73

			132	1194.35	-127.11	2018.18	-927.53	377.87	851.73
440	Copertura	18, 20	0	-1165.96	-104.54	-2836.19	-688.04	929.15	868.27
			66	-1165.96	-104.54	-2706.23	-688.04	438.10	868.27
			132	-1165.96	-104.54	-2590.22	-688.04	387.15	868.27
441	Copertura	19, 21	0	1222.83	-89.66	2075.04	976.22	481.33	818.83
			66	1222.83	-89.66	1915.58	976.22	302.50	818.83
			132	1222.83	-89.66	-2049.58	976.22	-790.54	818.83
442	Copertura	20, 22	0	-1146.08	-115.62	-2662.25	-1166.58	474.44	844.01
			66	-1146.08	-115.62	-1957.68	-1166.58	323.08	844.01
			132	-1146.08	-115.62	-1665.98	-1166.58	-849.92	844.01
443	Copertura	21, 23	0	1282.02	-103.78	-2103.23	-1045.06	579.23	757.62
			66	1282.02	-103.78	-1829.01	-1045.06	-558.98	757.62
			132	1282.02	-103.78	-1798.61	-1045.06	-812.31	757.62
444	Copertura	22, 24	0	-1147.59	-132.29	-1712.37	-1386.36	609.62	680.41
			66	-1147.59	-132.29	-1413.86	-1386.36	-585.20	680.41
			132	-1147.59	-132.29	-1384.78	-1386.36	-796.54	680.41
445	Copertura	23, 25	0	1456.80	-118.06	-1834.51	-1126.56	-621.45	1236.12
			66	1456.80	-118.06	-1940.80	-1126.56	-983.64	1236.12
			132	1456.80	-118.06	-2335.06	-1126.56	-1751.22	1236.12
446	Copertura	24, 26	0	-1277.81	-116.22	-1452.39	-1117.94	-644.51	-685.52
			66	-1277.81	-116.22	1428.75	-1117.94	-431.20	-685.52
			132	-1277.81	-116.22	1630.14	-1117.94	-703.64	-685.52
447	Copertura	25, 28	0	1615.96	-60.93	-2306.21	1025.04	-1437.44	-636.40
			85	1615.96	-60.93	-2353.54	1025.04	-949.37	-636.40
			170	1615.96	-60.93	-2546.55	1025.04	-569.27	-636.40
448	Copertura	26, 27	0	-1387.00	161.00	1720.21	907.90	-458.50	1312.05
			66	-1387.00	161.00	-1524.57	907.90	-917.35	1312.05
			132	-1387.00	161.00	-1642.95	907.90	-1603.49	1312.05
449	Copertura	27, 29	0	-1463.26	137.78	-1762.25	1060.45	-1476.46	629.52
			66	-1463.26	137.78	-1747.74	1060.45	-1302.36	629.52
			132	-1463.26	137.78	-1948.14	1060.45	-1455.62	629.52
450	Copertura	28, 30	0	1613.29	-111.76	-2517.65	1411.45	397.97	850.32
			73	1613.29	-111.76	-2496.22	1411.45	-597.53	850.32
			146	1613.29	-111.76	-3050.77	1411.45	-1137.59	850.32
451	Copertura	29, 31	0	-1479.77	-86.85	-2115.78	936.60	-1316.71	284.82
			66	-1479.77	-86.85	2039.30	936.60	-1264.38	284.82
			132	-1479.77	-86.85	2383.24	936.60	-1222.26	284.82
452	Copertura	30, 32	0	1608.92	-88.67	-2985.95	-1138.36	-904.15	487.74
			69	1608.92	-88.67	3197.89	-1138.36	-1072.11	487.74
			137	1608.92	-88.67	3441.32	-1138.36	-1259.55	487.74
453	Copertura	31, 33	0	-1556.30	116.29	2555.39	1049.82	-1352.89	-615.12
			66	-1556.30	116.29	2376.56	1049.82	-1117.13	-615.12
			132	-1556.30	116.29	2458.63	1049.82	-1272.20	-615.12
454	Copertura	32, 34	0	1643.09	108.90	3369.46	1310.66	-1241.74	-600.83
			69	1643.09	108.90	-2769.23	1310.66	-1059.81	-600.83
			138	1643.09	108.90	-2332.52	1310.66	-1249.19	-600.83
455	Copertura	33, 35	0	-1645.87	78.47	2678.41	-1031.90	-1257.86	-429.81
			66	-1645.87	78.47	2398.28	-1031.90	-1244.27	-429.81
			132	-1645.87	78.47	2517.64	-1031.90	-1309.91	-429.81
456	Copertura	34, 36	0	1668.08	59.84	-2253.20	1071.78	-1081.85	-321.18
			69	1668.08	59.84	-2052.76	1071.78	-1145.92	-321.18
			138	1668.08	59.84	-2153.04	1071.78	-1283.55	-321.18
457	Copertura	35, 37	0	-1686.55	-131.24	2738.35	-1369.83	-1481.92	-649.22
			66	-1686.55	-131.24	2907.72	-1369.83	-1103.22	-649.22
			132	-1686.55	-131.24	3218.40	-1369.83	-976.81	-649.22
458	Copertura	36, 38	0	1624.59	89.17	-2063.89	-960.16	-1284.04	-529.61
			69	1624.59	89.17	-1976.40	-960.16	-965.20	-529.61
			138	1624.59	89.17	2278.71	-960.16	-888.44	-529.61
459	Copertura	37, 39	0	-1658.31	-88.27	3462.30	-821.06	-1135.45	-747.78
			66	-1658.31	-88.27	-3254.91	-821.06	-955.52	-747.78
			132	-1658.31	-88.27	-3234.61	-821.06	-957.47	-747.78
460	Copertura	38, 40	0	1526.48	-75.76	2182.96	923.29	-890.47	493.53
			69	1526.48	-75.76	2119.00	923.29	-891.28	493.53
			137	1526.48	-75.76	2100.85	923.29	-1083.23	493.53
461	Copertura	39, 41	0	-1614.44	-138.86	-3496.34	-1711.55	-1186.45	-1641.52
			66	-1614.44	-138.86	-2608.96	-1711.55	-328.34	-1641.52
			132	-1614.44	-138.86	2060.72	-1711.55	1059.99	-1641.52
462	Copertura	40, 42	0	1430.06	-98.99	2010.91	941.75	-1149.73	982.43
			69	1430.06	-98.99	1981.58	941.75	-1370.01	982.43
			138	1430.06	-98.99	-1992.16	941.75	-1726.78	982.43
463	Copertura	41, 44	0	-1872.26	79.36	-2244.36	-1548.47	823.13	2264.40
			66	-1872.26	79.36	2153.36	-1548.47	-721.64	2264.40

			132	-1872.26	79.36	-2170.66	-1548.47	-2199.94	2264.40
464	Copertura	42, 43	0	1516.72	-388.36	-1889.13	1453.41	-1915.35	-3718.71
			23	1516.72	-388.36	1791.75	1453.41	-1133.48	-3718.71
			46	1516.72	-388.36	1945.93	1453.41	-683.64	-3718.71
465	Copertura	43, 45	0	1492.93	119.51	2007.99	-1237.90	-731.35	-508.25
			66	1492.93	119.51	2050.92	-1237.90	-972.96	-508.25
			132	1492.93	119.51	-2343.32	-1237.90	-1242.98	-508.25
466	Copertura	44, 46	0	-1788.11	-108.98	-2304.10	-1044.80	-2376.01	-1279.28
			66	-1788.11	-108.98	-2353.03	-1044.80	-1833.94	-1279.28
			132	-1788.11	-108.98	-2601.24	-1044.80	-1389.63	-1279.28
467	Copertura	45, 47	0	1382.08	103.57	-2406.83	1011.24	-1551.42	-870.74
			66	1382.08	103.57	-2049.46	1011.24	-1033.79	-870.74
			132	1382.08	103.57	-1962.96	1011.24	-806.23	-870.74
468	Copertura	46, 48	0	-1634.30	124.16	-2679.12	1019.39	-1679.63	-980.51
			66	-1634.30	124.16	-2444.35	1019.39	-1083.63	-980.51
			132	-1634.30	124.16	-2468.94	1019.39	-710.16	-980.51
469	Copertura	47, 49	0	1236.24	121.42	-2025.45	1500.21	-1095.12	-913.64
			66	1236.24	121.42	1518.97	1500.21	-834.50	-913.64
			132	1236.24	121.42	1524.94	1500.21	-760.92	-913.64
470	Copertura	48, 50	0	-1442.43	86.52	-2528.56	-967.64	-1031.24	-871.44
			66	-1442.43	86.52	-2230.34	-967.64	-785.84	-871.44
			132	-1442.43	86.52	-2128.52	-967.64	-744.69	-871.44
471	Copertura	49, 51	0	1190.24	139.58	1478.99	1522.10	-1115.18	-945.71
			66	1190.24	139.58	1560.34	1522.10	-519.56	-945.71
			132	1190.24	139.58	2320.58	1522.10	296.64	-945.71
472	Copertura	50, 52	0	-1338.88	122.49	-2137.00	1411.79	-1084.13	-915.28
			66	-1338.88	122.49	-1756.04	1411.79	-513.56	-915.28
			132	-1338.88	122.49	-1547.37	1411.79	294.17	-915.28
473	Copertura	51, 53	0	1184.16	118.34	2256.05	-997.06	-559.64	-1095.78
			66	1184.16	118.34	2680.93	-997.06	292.53	-1095.78
			132	1184.16	118.34	3124.28	-997.06	930.44	-1095.78
474	Copertura	52, 54	0	-1274.93	131.04	-1447.64	1248.34	-556.27	-1073.72
			66	-1274.93	131.04	-1782.21	1248.34	286.14	-1073.72
			132	-1274.93	131.04	-2434.52	1248.34	917.02	-1073.72
475	Copertura	53, 55	0	1068.84	143.94	3069.12	-950.25	523.88	-974.32
			66	1068.84	143.94	2866.44	-950.25	770.39	-974.32
			132	1068.84	143.94	-2680.93	-950.25	1172.51	-974.32
476	Copertura	54, 56	0	-1107.20	136.61	-2337.72	780.17	513.33	-953.33
			66	-1107.20	136.61	-2373.52	780.17	745.00	-953.33
			132	-1107.20	136.61	2430.81	780.17	1149.65	-953.33
477	Copertura	55, 57	0	960.78	-130.29	-2632.69	1610.63	910.58	-1089.75
			80	960.78	-130.29	-1354.39	1610.63	1451.90	-1089.75
			159	960.78	-130.29	203.94	1610.63	2205.66	-1089.75
478	Copertura	56, 70	0	-943.46	-129.02	2341.26	-1384.75	878.15	-1071.29
			80	-943.46	-129.02	1242.99	-1384.75	1451.76	-1071.29
			159	-943.46	-129.02	-215.51	-1384.75	2184.20	-1071.29
479	Copertura	57, 58	0	-965.46	91.63	518.73	1007.28	2174.37	-988.44
			83	-965.46	91.63	1270.24	1007.28	1592.58	-988.44
			166	-965.46	91.63	2078.44	1007.28	1831.77	-988.44
480	Copertura	58, 59	0	-846.12	149.29	2091.69	-541.95	1823.52	320.19
			69	-846.12	149.29	1823.17	-541.95	1845.11	320.19
			138	-846.12	149.29	1735.12	-541.95	1873.37	320.19
481	Copertura	59, 60	0	-668.10	69.21	1747.83	-664.93	1871.54	573.36
			69	-668.10	69.21	1468.12	-664.93	1492.92	573.36
			138	-668.10	69.21	1214.84	-664.93	1126.06	573.36
482	Copertura	60, 61	0	-508.25	111.96	1227.81	-558.25	1128.57	799.30
			69	-508.25	111.96	-966.22	-558.25	880.77	799.30
			138	-508.25	111.96	-938.56	-558.25	1151.96	799.30
483	Copertura	61, 62	0	-330.29	-104.43	-928.43	829.99	1151.84	442.81
			69	-330.29	-104.43	1005.62	829.99	1228.20	442.81
			138	-330.29	-104.43	1337.58	829.99	1319.81	442.81
484	Copertura	62, 63	0	189.64	-107.61	1352.73	-494.49	1323.10	525.76
			69	189.64	-107.61	1031.31	-494.49	961.24	525.76
			138	189.64	-107.61	714.32	-494.49	600.48	525.76
485	Copertura	63, 64	0	77.41	-159.51	730.84	-603.59	603.85	865.73
			69	77.41	-159.51	-397.31	-603.59	30.37	865.73
			138	77.41	-159.51	-666.54	-603.59	-591.07	865.73
486	Copertura	64, 65	0	-244.83	-103.98	-646.49	-507.12	-587.98	537.96
			69	-244.83	-103.98	-957.92	-507.12	-957.79	537.96
			138	-244.83	-103.98	-1274.22	-507.12	-1328.38	537.96
487	Copertura	65, 66	0	377.74	-107.27	-1255.53	885.11	-1325.78	440.49
			69	377.74	-107.27	-904.75	885.11	-1235.45	440.49

			138	377.74	-107.27	870.48	885.11	-1160.07	440.49
488	Copertura	66, 67	0	534.26	-108.94	883.13	-580.68	-1159.19	802.20
			69	534.26	-108.94	-932.77	-580.68	-885.34	802.20
			138	534.26	-108.94	-1185.67	-580.68	-1126.54	802.20
489	Copertura	67, 68	0	709.28	78.68	-1174.98	-712.96	-1123.91	572.68
			69	709.28	78.68	-1409.52	-712.96	-1490.03	572.68
			138	709.28	78.68	-1677.72	-712.96	-1868.02	572.68
490	Copertura	68, 69	0	891.56	150.68	-1661.50	-582.02	-1869.61	311.97
			69	891.56	150.68	-1834.21	-582.02	-1846.03	311.97
			138	891.56	150.68	-2044.84	-582.02	-1828.68	311.97
491	Copertura	69, 70	0	997.44	88.60	-2032.50	1006.84	-1837.52	-980.38
			83	997.44	88.60	-1264.89	1006.84	-1576.87	-980.38
			166	997.44	88.60	-574.94	1006.84	-2156.82	-980.38
492	Copertura	1	0	-1350.57	36.44	192.64	-84.70	-552.85	-236.40
			220	-1350.57	36.44	6.54	-84.70	-71.27	-236.40
			440	-1350.57	36.44	-180.04	-84.70	489.81	-236.40
493	Copertura	2	0	643.57	4.09	191.74	-102.83	-17.39	-7.95
			220	643.57	4.09	74.79	-102.83	-0.15	-7.95
			440	643.57	4.09	-264.83	-102.83	17.57	-7.95
494	Copertura	3	0	399.65	3.36	173.73	-100.95	-19.40	-8.90
			220	399.65	3.36	-55.36	-100.95	0.32	-8.90
			440	399.65	3.36	-271.17	-100.95	19.75	-8.90
495	Copertura	4	0	-191.75	-5.05	109.12	-64.21	-19.89	-9.02
			220	-191.75	-5.05	-32.48	-64.21	0.14	-9.02
			440	-191.75	-5.05	-173.54	-64.21	19.81	-9.02
496	Copertura	5	0	-176.99	-3.54	-184.06	112.72	-20.34	-9.30
			220	-176.99	-3.54	63.94	112.72	0.31	-9.30
			440	-176.99	-3.54	311.90	112.72	20.61	-9.30
497	Copertura	6	0	-370.83	-5.41	79.75	-46.35	-19.00	-8.54
			220	-370.83	-5.41	-27.83	-46.35	-0.36	-8.54
			440	-370.83	-5.41	-124.33	-46.35	18.57	-8.54
498	Copertura	7	0	369.78	-4.58	-96.59	66.53	-18.86	-8.48
			220	369.78	-4.58	-49.86	66.53	-0.35	-8.48
			440	369.78	-4.58	196.19	66.53	18.46	-8.48
499	Copertura	8	0	49.26	-4.63	-122.89	74.20	-20.27	-9.37
			220	49.26	-4.63	40.40	74.20	0.56	-9.37
			440	49.26	-4.63	203.61	74.20	20.97	-9.37
500	Copertura	9	0	-320.45	-5.28	-86.52	55.29	-18.75	-8.43
			220	-320.45	-5.28	35.19	55.29	-0.32	-8.43
			440	-320.45	-5.28	156.79	55.29	18.34	-8.43
501	Copertura	10	0	394.31	-4.00	167.79	-106.84	-18.64	-8.38
			220	394.31	-4.00	-67.30	-106.84	-0.32	-8.38
			440	394.31	-4.00	-302.34	-106.84	18.24	-8.38
502	Copertura	11	0	266.45	-4.85	-122.57	72.28	-19.49	-8.94
			220	266.45	-4.85	36.68	72.28	0.38	-8.94
			440	266.45	-4.85	195.56	72.28	19.86	-8.94
503	Copertura	12	0	-423.10	3.37	-164.15	94.11	-18.72	-8.59
			220	-423.10	3.37	-49.52	94.11	0.33	-8.59
			440	-423.10	3.37	250.62	94.11	19.09	-8.59
504	Copertura	13	0	-639.67	3.91	-184.76	99.11	-16.90	-7.73
			220	-639.67	3.91	-74.48	99.11	0.15	-7.73
			440	-639.67	3.91	257.04	99.11	17.10	-7.73
505	Copertura	57	0	1817.04	-44.72	220.67	-96.35	-512.36	-225.23
			220	1817.04	-44.72	9.28	-96.35	-78.54	-225.23
			440	1817.04	-44.72	-203.27	-96.35	482.33	-225.23
506	Copertura	58	0	721.72	-4.71	-142.50	82.65	-18.22	-8.32
			220	721.72	-4.71	-83.99	82.65	0.15	-8.32
			440	721.72	-4.71	253.39	82.65	18.37	-8.32
507	Copertura	59	0	438.21	-3.97	-143.87	79.11	-20.65	-9.49
			220	438.21	-3.97	-50.50	79.11	0.40	-9.49
			440	438.21	-3.97	205.65	79.11	21.12	-9.49
508	Copertura	60	0	286.42	3.87	-106.67	59.74	-22.20	-10.23
			220	286.42	3.87	-25.79	59.74	0.46	-10.23
			440	286.42	3.87	-156.54	59.74	22.81	-10.23
509	Copertura	61	0	-515.41	3.09	155.79	-98.12	-21.62	-9.73
			220	-515.41	3.09	-60.32	-98.12	-0.40	-9.73
			440	-515.41	3.09	-276.04	-98.12	21.20	-9.73
510	Copertura	62	0	390.24	4.83	86.29	-51.10	-22.24	-9.99
			220	390.24	4.83	27.91	-51.10	-0.43	-9.99
			440	390.24	4.83	-138.62	-51.10	21.74	-9.99
511	Copertura	63	0	145.76	4.63	-127.69	-78.46	-24.16	-11.07
			220	145.76	4.63	-44.94	-78.46	0.32	-11.07

			440	145.76	4.63	-217.55	-78.46	24.54	-11.07
512	Copertura	64	0	-152.35	4.93	-126.18	77.90	-24.33	-11.16
			220	-152.35	4.93	45.21	77.90	0.32	-11.16
			440	-152.35	4.93	216.59	77.90	24.76	-11.16
513	Copertura	65	0	-392.34	4.93	-95.41	55.85	-22.58	-10.13
			220	-392.34	4.93	27.65	55.85	-0.45	-10.13
			440	-392.34	4.93	150.40	55.85	22.00	-10.13
514	Copertura	66	0	522.51	2.72	-158.58	98.95	-22.38	-10.04
			220	522.51	2.72	59.38	98.95	-0.42	-10.04
			440	522.51	2.72	276.92	98.95	21.80	-10.04
515	Copertura	67	0	284.18	-3.98	100.27	-55.26	-23.60	-10.86
			220	284.18	-3.98	-22.67	-55.26	0.45	-10.86
			440	284.18	-3.98	-143.20	-55.26	24.19	-10.86
516	Copertura	68	0	-451.57	-3.92	149.20	83.22	-22.47	-10.33
			220	-451.57	-3.92	54.55	83.22	0.40	-10.33
			440	-451.57	-3.92	218.45	83.22	22.99	-10.33
517	Copertura	69	0	-725.99	-4.95	143.29	-81.30	-19.76	-8.98
			220	-725.99	-4.95	81.95	-81.30	-0.15	-8.98
			440	-725.99	-4.95	-247.40	-81.30	19.74	-8.98
518	Primo Impalcato	1, 74	0	889.50	-0.34	0.00	0.00	32.51	25.45
			118	889.50	-0.34	0.00	0.00	6.48	25.45
			235	889.50	-0.34	0.00	0.00	-27.95	25.45
519	Copertura	74, 2	0	-884.07	1.24	0.00	0.00	-24.23	-14.33
			118	-884.07	1.24	0.00	0.00	-7.84	-14.33
			235	-884.07	1.24	0.00	0.00	12.81	-14.33
520	Primo Impalcato	6, 71	0	946.14	-1.06	0.00	0.00	-26.74	-26.37
			115	946.14	-1.06	0.00	0.00	-6.21	-26.37
			231	946.14	-1.06	0.00	0.00	35.58	-26.37
521	Copertura	71, 7	0	-943.98	-0.93	0.00	0.00	28.48	20.52
			115	-943.98	-0.93	0.00	0.00	7.24	20.52
			231	-943.98	-0.93	0.00	0.00	-22.48	20.52
522	Primo Impalcato	9, 72	0	944.47	-0.60	0.00	0.00	16.69	15.03
			115	944.47	-0.60	0.00	0.00	-5.99	15.03
			231	944.47	-0.60	0.00	0.00	-20.63	15.03
523	Copertura	72, 10	0	-926.67	-0.88	0.00	0.00	-11.79	-11.30
			115	-926.67	-0.88	0.00	0.00	6.94	-11.30
			231	-926.67	-0.88	0.00	0.00	-16.03	-11.30
524	Copertura	73, 13	0	844.13	1.20	0.00	0.00	-22.65	-13.15
			118	844.13	1.20	0.00	0.00	-7.83	-13.15
			235	844.13	1.20	0.00	0.00	11.81	-13.15
525	Primo Impalcato	14, 73	0	-888.17	-0.55	0.00	0.00	33.28	24.87
			118	-888.17	-0.55	0.00	0.00	6.51	24.87
			235	-888.17	-0.55	0.00	0.00	-26.42	24.87
526	Primo Impalcato	57, 75	0	1018.97	-0.69	0.00	0.00	-25.53	-22.44
			118	1018.97	-0.69	0.00	0.00	-3.59	-22.44
			235	1018.97	-0.69	0.00	0.00	28.17	-22.44
527	Copertura	75, 58	0	-891.32	-1.25	0.00	0.00	23.40	11.53
			118	-891.32	-1.25	0.00	0.00	10.61	11.53
			235	-891.32	-1.25	0.00	0.00	13.04	11.53
528	Copertura	77, 61	0	1085.93	0.75	0.00	0.00	16.94	11.87
			115	1085.93	0.75	0.00	0.00	5.79	11.87
			231	1085.93	0.75	0.00	0.00	-14.01	11.87
529	Primo Impalcato	62, 77	0	-1101.69	0.59	0.00	0.00	-22.94	-20.57
			115	-1101.69	0.59	0.00	0.00	4.84	-20.57
			231	-1101.69	0.59	0.00	0.00	26.18	-20.57
530	Primo Impalcato	65, 78	0	1132.96	0.57	0.00	0.00	-22.07	-19.64
			115	1132.96	0.57	0.00	0.00	4.56	-19.64
			231	1132.96	0.57	0.00	0.00	25.04	-19.64
531	Copertura	78, 66	0	-1099.16	0.74	0.00	0.00	15.19	11.96
			115	-1099.16	0.74	0.00	0.00	-5.53	11.96
			231	-1099.16	0.74	0.00	0.00	-16.11	11.96
532	Primo Impalcato	69, 76	0	997.68	-1.28	0.00	0.00	-14.12	-12.47
			118	997.68	-1.28	0.00	0.00	-10.63	-12.47
			235	997.68	-1.28	0.00	0.00	-24.37	-12.47
533	Copertura	76, 70	0	-1029.06	-0.59	0.00	0.00	-29.17	-23.16

			118	-1029.06	-0.59	0.00	0.00	3.69	-23.16
			235	-1029.06	-0.59	0.00	0.00	25.33	-23.16
534	Copertura	1, 74	0	-883.32	0.99	0.00	0.00	34.40	22.85
			118	-883.32	0.99	0.00	0.00	-10.32	22.85
			235	-883.32	0.99	0.00	0.00	-25.59	22.85
535	Copertura	74, 2	0	891.50	0.36	0.00	0.00	-26.13	-21.81
			118	891.50	0.36	0.00	0.00	-2.25	-21.81
			235	891.50	0.36	0.00	0.00	26.02	-21.81
536	Copertura	6, 71	0	-945.48	-0.44	0.00	0.00	-31.13	-24.97
			115	-945.48	-0.44	0.00	0.00	3.91	-24.97
			231	-945.48	-0.44	0.00	0.00	28.82	-24.97
537	Copertura	71, 7	0	947.78	-0.87	0.00	0.00	34.84	26.70
			115	947.78	-0.87	0.00	0.00	-5.28	26.70
			231	947.78	-0.87	0.00	0.00	-30.37	26.70
538	Copertura	9, 72	0	-927.88	-0.82	0.00	0.00	18.13	11.64
			115	-927.88	-0.82	0.00	0.00	5.57	11.64
			231	-927.88	-0.82	0.00	0.00	-12.52	11.64
539	Copertura	72, 10	0	945.78	-0.54	0.00	0.00	-19.07	-14.58
			115	945.78	-0.54	0.00	0.00	-3.23	-14.58
			231	945.78	-0.54	0.00	0.00	15.32	-14.58
540	Copertura	73, 13	0	-888.73	0.34	0.00	0.00	-24.65	-20.61
			118	-888.73	0.34	0.00	0.00	-2.20	-20.61
			235	-888.73	0.34	0.00	0.00	24.47	-20.61
541	Copertura	14, 73	0	843.34	0.99	0.00	0.00	-33.07	21.73
			118	843.34	0.99	0.00	0.00	-10.11	21.73
			235	843.34	0.99	0.00	0.00	-24.44	21.73
542	Copertura	15, 125	0	-1307.70	-16.08	243.54	1717.74	-358.96	261.05
			75	-1307.70	-16.08	1047.06	1717.74	-386.36	261.05
			150	-1307.70	-16.08	2335.12	1717.74	-465.08	261.05
543	Copertura	127, 16	0	1519.77	-15.78	-2251.84	1648.52	466.23	272.66
			75	1519.77	-15.78	-1015.65	1648.52	390.53	272.66
			150	1519.77	-15.78	-222.88	1648.52	371.56	272.66
544	Copertura	17, 129	0	-2019.66	-17.68	-246.85	1562.75	-382.59	239.53
			75	-2019.66	-17.68	1000.58	1562.75	-424.81	239.53
			150	-2019.66	-17.68	2159.80	1562.75	-508.79	239.53
545	Copertura	130, 18	0	2630.49	-17.23	-2457.46	1806.45	512.57	264.36
			75	2630.49	-17.23	-1104.84	1806.45	431.89	264.36
			150	2630.49	-17.23	278.17	1806.45	401.65	264.36
546	Copertura	19, 135	0	-2396.91	-17.98	-309.40	2769.92	-404.63	247.68
			75	-2396.91	-17.98	1769.86	2769.92	-446.08	247.68
			150	-2396.91	-17.98	3847.16	2769.92	-524.36	247.68
547	Copertura	134, 20	0	2708.23	-17.65	-4020.62	2910.17	527.73	269.96
			75	2708.23	-17.65	-1838.22	2910.17	453.95	269.96
			150	2708.23	-17.65	347.04	2910.17	424.18	269.96
548	Copertura	21, 136	0	-2805.07	-18.02	-345.20	3320.76	-347.70	207.55
			75	-2805.07	-18.02	2145.89	3320.76	-419.15	207.55
			150	-2805.07	-18.02	4636.42	3320.76	-514.47	207.55
549	Copertura	138, 22	0	3088.92	-17.96	-4565.45	3277.32	515.73	220.99
			75	3088.92	-17.96	-2107.48	3277.32	421.42	220.99
			150	3088.92	-17.96	367.14	3277.32	356.20	220.99
550	Copertura	23, 141	0	-3967.30	-17.07	-383.83	3708.37	-422.96	275.44
			75	-3967.30	-17.07	2400.83	3708.37	-430.05	275.44
			150	-3967.30	-17.07	5182.00	3708.37	-493.66	275.44
551	Copertura	142, 24	0	3324.07	-16.07	-5358.60	3872.02	494.26	283.88
			75	3324.07	-16.07	-2454.95	3872.02	429.29	283.88
			150	3324.07	-16.07	453.30	3872.02	423.91	283.88
552	Copertura	25, 145	0	-3490.60	-14.93	-540.75	4669.39	-343.59	216.88
			75	-3490.60	-14.93	2962.35	4669.39	-363.43	216.88
			150	-3490.60	-14.93	6464.31	4669.39	-429.42	216.88
553	Copertura	146, 26	0	5468.97	-17.24	-6174.72	4420.92	450.79	263.94
			75	5468.97	-17.24	-2859.21	4420.92	379.37	263.94
			150	5468.97	-17.24	474.41	4420.92	365.48	263.94
554	Copertura	150, 27	0	3818.20	-14.26	-7269.07	5268.77	384.01	265.30
			75	3818.20	-14.26	-3318.29	5268.77	294.60	265.30
			150	3818.20	-14.26	642.36	5268.77	256.29	265.30
555	Copertura	28, 149	0	-5877.15	-11.17	-534.39	5219.40	-322.10	156.24
			75	-5877.15	-11.17	3381.05	5219.40	-318.81	156.24
			150	-5877.15	-11.17	7295.53	5219.40	-345.68	156.24
556	Copertura	154, 29	0	5286.67	-16.84	-7810.95	5596.10	289.41	204.20
			75	5286.67	-16.84	-3614.11	5596.10	200.21	204.20
			150	5286.67	-16.84	586.06	5596.10	149.41	204.20
557	Copertura	30, 153	0	-5287.63	-8.49	-612.63	5730.80	-241.15	104.07

			75	-5287.63	-8.49	3686.33	5730.80	-248.76	104.07
			150	-5287.63	-8.49	7984.36	5730.80	-274.78	104.07
558	Copertura	158, 31	0	5574.65	-11.84	-8239.81	5881.25	211.15	229.28
			75	5574.65	-11.84	-3829.02	5881.25	143.23	229.28
			150	5574.65	-11.84	584.05	5881.25	161.13	229.28
559	Copertura	32, 157	0	-5588.82	-5.04	-669.25	6096.96	-259.96	-140.61
			75	-5588.82	-5.04	3905.92	6096.96	-208.11	-140.61
			150	-5588.82	-5.04	8478.44	6096.96	-201.05	-140.61
560	Copertura	162, 33	0	5689.43	-12.88	-8312.74	5950.25	125.15	254.21
			75	5689.43	-12.88	-3850.34	5950.25	-102.50	254.21
			150	5689.43	-12.88	616.39	5950.25	-266.51	254.21
561	Copertura	34, 161	0	-5615.67	-2.07	-605.92	5845.55	260.38	158.00
			75	-5615.67	-2.07	3795.77	5845.55	-157.33	158.00
			150	-5615.67	-2.07	8179.91	5845.55	-116.42	158.00
562	Copertura	166, 35	0	5700.73	-9.33	-8391.60	5995.63	33.57	186.62
			75	5700.73	-9.33	-3895.13	5995.63	-106.51	186.62
			150	5700.73	-9.33	605.11	5995.63	-246.45	186.62
563	Copertura	36, 165	0	-5694.35	3.76	-654.13	6049.78	-117.11	83.18
			75	-5694.35	3.76	3896.21	6049.78	-55.08	83.18
			150	-5694.35	3.76	8433.41	6049.78	-22.46	83.18
564	Copertura	170, 37	0	5469.84	-9.93	-8462.81	6053.16	-83.12	197.17
			75	5469.84	-9.93	-3923.25	6053.16	-194.92	197.17
			150	5469.84	-9.93	620.82	6053.16	-340.83	197.17
565	Copertura	38, 169	0	-5659.84	6.16	-620.81	5967.51	186.31	155.12
			75	-5659.84	6.16	3855.89	5967.51	111.24	155.12
			150	-5659.84	6.16	8331.45	5967.51	82.58	155.12
566	Copertura	175, 39	0	5067.53	-7.04	-8115.00	5825.47	-141.79	110.84
			75	5067.53	-7.04	-3746.45	5825.47	-206.11	110.84
			150	5067.53	-7.04	629.85	5825.47	-287.57	110.84
567	Copertura	40, 173	0	-6160.38	7.97	-557.12	5591.68	76.81	-69.63
			75	-6160.38	7.97	3644.40	5591.68	105.88	-69.63
			150	-6160.38	7.97	7838.05	5591.68	142.53	-69.63
568	Copertura	178, 41	0	8615.45	-5.49	-7225.40	5119.31	-177.88	213.33
			75	8615.45	-5.49	-3386.57	5119.31	-282.66	213.33
			150	8615.45	-5.49	483.33	5119.31	-436.60	213.33
569	Copertura	42, 177	0	-1912.67	10.67	-841.09	5430.44	269.28	-230.70
			75	-1912.67	10.67	3316.66	5430.44	212.81	-230.70
			150	-1912.67	10.67	7387.61	5430.44	229.65	-230.70
570	Copertura	43, 181	0	-8064.68	6.01	-650.51	5165.68	381.56	185.27
			75	-8064.68	6.01	3278.32	5165.68	293.10	185.27
			150	-8064.68	6.01	7130.64	5165.68	267.38	185.27
571	Copertura	182, 44	0	2080.35	2.36	-7148.10	5187.60	-236.37	155.60
			75	2080.35	2.36	-3258.72	5187.60	-280.54	155.60
			150	2080.35	2.36	653.41	5187.60	-380.71	155.60
572	Copertura	45, 185	0	-4210.22	7.65	-497.63	4683.55	333.16	-74.25
			75	-4210.22	7.65	3042.27	4683.55	331.90	-74.25
			150	-4210.22	7.65	6554.81	4683.55	342.05	-74.25
573	Copertura	186, 46	0	5482.53	5.65	-6605.00	4750.13	-346.70	-84.93
			75	5482.53	5.65	-3042.68	4750.13	-329.05	-84.93
			150	5482.53	5.65	552.20	4750.13	-328.43	-84.93
574	Copertura	47, 189	0	-3892.36	9.94	-508.49	4311.96	481.74	172.20
			75	-3892.36	9.94	2729.46	4311.96	435.51	172.20
			150	-3892.36	9.94	5963.09	4311.96	423.78	172.20
575	Copertura	190, 48	0	4131.35	9.55	-5609.38	4027.74	-427.47	170.84
			75	4131.35	9.55	-2591.42	4027.74	-432.09	170.84
			150	4131.35	9.55	436.17	4027.74	-470.20	170.84
576	Copertura	49, 193	0	-3505.78	11.66	-396.62	3632.90	444.00	-123.61
			75	-3505.78	11.66	2341.69	3632.90	448.53	-123.61
			150	-3505.78	11.66	5066.31	3632.90	476.89	-123.61
577	Copertura	195, 50	0	3065.94	8.98	-5173.90	3718.74	-482.13	-133.85
			75	3065.94	8.98	-2384.96	3718.74	-447.49	-133.85
			150	3065.94	8.98	405.62	3718.74	-438.09	-133.85
578	Copertura	51, 197	0	-2646.27	12.42	-353.19	2953.59	560.62	221.05
			75	-2646.27	12.42	1864.38	2953.59	507.26	221.05
			150	-2646.27	12.42	4079.36	2953.59	511.25	221.05
579	Copertura	199, 52	0	2614.51	10.07	-3851.58	2777.95	-514.64	216.68
			75	2614.51	10.07	-1776.73	2777.95	-501.21	216.68
			150	2614.51	10.07	317.76	2777.95	-543.13	216.68
580	Copertura	53, 201	0	-2810.93	12.58	-307.13	2064.90	504.39	-172.25
			75	-2810.93	12.58	1251.78	2064.90	481.40	-172.25
			150	-2810.93	12.58	2799.35	2064.90	499.55	-172.25
581	Copertura	202, 54	0	2170.14	11.10	-2580.29	1877.16	-503.40	-169.98

			75	2170.14	11.10	-1173.28	1877.16	-474.86	-169.98
			150	2170.14	11.10	310.45	1877.16	-488.22	-169.98
582	Copertura	55, 205	0	-1870.60	10.98	322.22	-2261.18	441.17	-143.34
			75	-1870.60	10.98	-1375.61	-2261.18	434.93	-143.34
			150	-1870.60	10.98	-3071.29	-2261.18	449.63	-143.34
583	Copertura	206, 56	0	1417.49	8.02	3014.95	-2222.27	-454.36	-147.64
			75	1417.49	8.02	-1348.44	-2222.27	-431.71	-147.64
			150	1417.49	8.02	-320.05	-2222.27	-429.51	-147.64
584	Copertura	57, 75	0	-892.14	-1.37	0.00	0.00	-22.39	-19.92
			118	-892.14	-1.37	0.00	0.00	6.38	-19.92
			235	-892.14	-1.37	0.00	0.00	24.98	-19.92
585	Copertura	75, 58	0	1017.30	-0.37	0.00	0.00	26.46	20.36
			118	1017.30	-0.37	0.00	0.00	-4.01	20.36
			235	1017.30	-0.37	0.00	0.00	-21.90	20.36
586	Copertura	77, 61	0	-1104.27	0.62	0.00	0.00	24.89	19.05
			115	-1104.27	0.62	0.00	0.00	3.16	19.05
			231	-1104.27	0.62	0.00	0.00	-19.08	19.05
587	Copertura	62, 77	0	1088.05	0.73	0.00	0.00	-22.18	-16.11
			115	1088.05	0.73	0.00	0.00	-5.08	-16.11
			231	1088.05	0.73	0.00	0.00	18.07	-16.11
588	Copertura	65, 78	0	-1100.86	0.76	0.00	0.00	-20.34	-13.88
			115	-1100.86	0.76	0.00	0.00	-5.21	-13.88
			231	-1100.86	0.76	0.00	0.00	15.88	-13.88
589	Copertura	78, 66	0	1132.25	0.65	0.00	0.00	23.37	17.47
			115	1132.25	0.65	0.00	0.00	3.55	17.47
			231	1132.25	0.65	0.00	0.00	-16.93	17.47
590	Copertura	69, 76	0	-1028.63	-0.37	0.00	0.00	-22.91	21.14
			118	-1028.63	-0.37	0.00	0.00	3.52	21.14
			235	-1028.63	-0.37	0.00	0.00	-27.39	21.14
591	Copertura	76, 70	0	995.27	-1.33	0.00	0.00	-25.79	20.61
			118	995.27	-1.33	0.00	0.00	-6.44	20.61
			235	995.27	-1.33	0.00	0.00	23.19	20.61
592	Copertura	79, 81	0	-34.96	-3.38	107.00	-133.04	46.95	34.71
			80	-34.96	-3.38	1.42	-133.04	20.56	34.71
			159	-34.96	-3.38	-104.53	-133.04	-12.75	34.71
593	Copertura	80, 82	0	-28.29	-4.27	84.26	-125.90	28.64	24.60
			66	-28.29	-4.27	1.47	-125.90	18.65	24.60
			132	-28.29	-4.27	-82.03	-125.90	-19.99	24.60
594	Copertura	83, 84	0	-16.38	-4.70	75.37	-114.34	20.15	22.04
			66	-16.38	-4.70	0.83	-114.34	11.00	22.04
			132	-16.38	-4.70	-75.56	-114.34	-21.59	22.04
595	Copertura	85, 86	0	-47.12	-4.23	72.98	-108.65	-17.77	-23.07
			66	-47.12	-4.23	1.75	-108.65	-12.92	-23.07
			132	-47.12	-4.23	-70.44	-108.65	-22.44	-23.07
596	Copertura	87, 88	0	-85.90	-3.30	59.47	-86.63	-27.89	-30.41
			66	-85.90	-3.30	3.28	-86.63	-19.87	-30.41
			132	-85.90	-3.30	-54.90	-86.63	-29.40	-30.41
597	Copertura	89, 90	0	-57.43	-1.85	46.86	-69.69	-28.91	25.12
			66	-57.43	-1.85	1.85	-69.69	-17.00	25.12
			132	-57.43	-1.85	-45.14	-69.69	-28.85	25.12
598	Copertura	91, 92	0	-42.24	1.30	43.15	-66.09	-26.22	25.24
			66	-42.24	1.30	-1.26	-66.09	-17.97	25.24
			132	-42.24	1.30	-44.09	-66.09	23.60	25.24
599	Copertura	93, 94	0	68.76	2.04	56.94	-90.79	25.44	-29.51
			66	68.76	2.04	-4.75	-90.79	-13.75	-29.51
			132	68.76	2.04	-62.92	-90.79	-21.97	-29.51
600	Copertura	95, 96	0	83.03	3.55	75.69	-119.71	-27.19	-31.20
			66	83.03	3.55	-4.25	-119.71	-22.44	-31.20
			132	83.03	3.55	-82.34	-119.71	32.48	-31.20
601	Copertura	97, 106	0	14.57	4.85	92.22	-139.19	-29.39	-25.07
			66	14.57	4.85	0.71	-139.19	-18.06	-25.07
			132	14.57	4.85	-91.66	-139.19	-19.18	-25.07
602	Copertura	98, 99	0	-6.90	-3.35	108.48	-164.30	25.62	35.69
			66	-6.90	-3.35	1.49	-164.30	6.49	35.69
			132	-6.90	-3.35	-108.40	-164.30	-23.24	35.69
603	Copertura	100, 101	0	-10.64	-3.13	109.50	-166.44	25.67	40.21
			66	-10.64	-3.13	-1.07	-166.44	-7.07	40.21
			132	-10.64	-3.13	-110.20	-166.44	-30.29	40.21
604	Copertura	102, 103	0	-67.60	-2.91	107.19	-160.45	22.75	44.55
			66	-67.60	-2.91	1.44	-160.45	-12.24	44.55
			132	-67.60	-2.91	-104.60	-160.45	-37.20	44.55
605	Copertura	104, 105	0	-36.89	-1.94	100.44	-152.82	-20.44	-22.44

			66	-36.89	-1.94	-1.45	-152.82	-16.41	-22.44
			132	-36.89	-1.94	-101.29	-152.82	-27.92	-22.44
606	Copertura	107, 108	0	15.99	5.30	90.47	-136.84	25.28	-23.88
			66	15.99	5.30	0.55	-136.84	15.04	-23.88
			132	15.99	5.30	-90.33	-136.84	22.81	-23.88
607	Copertura	109, 110	0	41.01	4.87	74.36	-93.74	-22.72	-44.39
			80	41.01	4.87	0.40	-93.74	26.50	-44.39
			159	41.01	4.87	-74.69	-93.74	55.94	-44.39
608	Copertura	111, 112	0	20.80	1.23	106.15	-162.72	-28.12	-24.63
			66	20.80	1.23	-2.17	-162.72	-15.73	-24.63
			132	20.80	1.23	-108.82	-162.72	-22.48	-24.63
609	Copertura	113, 114	0	13.78	1.61	118.06	-178.99	-26.64	-31.96
			66	13.78	1.61	1.74	-178.99	-12.36	-31.96
			132	13.78	1.61	-118.21	-178.99	16.91	-31.96
610	Copertura	115, 116	0	142.03	1.94	134.43	-209.77	20.03	14.78
			66	142.03	1.94	-5.12	-209.77	-12.80	14.78
			132	142.03	1.94	-142.47	-209.77	-18.36	14.78
611	Copertura	117, 118	0	10.28	2.91	147.67	-221.60	-41.01	-43.94
			66	10.28	2.91	1.74	-221.60	-15.96	-43.94
			132	10.28	2.91	-144.85	-221.60	-20.35	-43.94
612	Copertura	119, 120	0	5.28	3.94	136.02	-205.40	-34.58	-44.47
			66	5.28	3.94	1.06	-205.40	-6.72	-44.47
			132	5.28	3.94	-135.11	-205.40	27.40	-44.47
613	Copertura	121, 122	0	15.11	3.20	127.80	-191.97	-25.36	-46.38
			66	15.11	3.20	1.63	-191.97	9.30	-46.38
			132	15.11	3.20	-126.00	-191.97	37.15	-46.38
614	Copertura	124, 125	0	2223.89	-1.89	117.33	-83.41	10.10	19.57
			99	2223.89	-1.89	35.44	-83.41	-15.00	19.57
			198	2223.89	-1.89	-49.00	-83.41	-31.31	19.57
615	Copertura	125, 127	0	-575.68	3.47	2365.06	-295.82	-488.05	-63.03
			775	-575.68	3.47	201.04	-295.82	1.72	-63.03
			1550	-575.68	3.47	-2270.97	-295.82	488.91	-63.03
616	Copertura	126, 127	0	-3014.46	-2.02	-146.96	102.13	8.37	18.53
			99	-3014.46	-2.02	-45.98	102.13	-15.75	18.53
			198	-3014.46	-2.02	56.23	102.13	-31.05	18.53
617	Copertura	128, 129	0	3484.21	-2.09	163.35	-105.67	8.04	20.37
			99	3484.21	-2.09	59.16	-105.67	-15.45	20.37
			198	3484.21	-2.09	-48.39	-105.67	-34.41	20.37
618	Copertura	129, 130	0	-790.15	3.63	2162.52	-274.78	-534.34	-69.11
			775	-790.15	3.63	513.10	-274.78	2.04	-69.11
			1550	-790.15	3.63	-2484.05	-274.78	536.81	-69.11
619	Copertura	131, 130	0	-4553.86	-2.47	-217.74	146.42	-9.80	17.83
			99	-4553.86	-2.47	-72.71	146.42	-19.34	17.83
			198	-4553.86	-2.47	73.47	146.42	-33.92	17.83
620	Copertura	132, 135	0	4174.66	-2.29	201.51	-131.23	8.92	22.00
			99	4174.66	-2.29	73.18	-131.23	-16.11	22.00
			198	4174.66	-2.29	-60.06	-131.23	-35.36	22.00
621	Copertura	133, 134	0	-5025.14	-2.62	-241.64	159.39	-9.33	19.36
			99	-5025.14	-2.62	-83.96	159.39	-20.21	19.36
			198	-5025.14	-2.62	77.07	159.39	-34.91	19.36
622	Copertura	135, 134	0	-554.81	3.82	3842.45	-491.34	-550.81	-71.23
			775	-554.81	3.82	303.72	-491.34	2.13	-71.23
			1550	-554.81	3.82	-4030.24	-491.34	553.54	-71.23
623	Copertura	137, 136	0	5354.72	-2.08	258.18	-166.74	11.78	22.84
			99	5354.72	-2.08	94.21	-166.74	-16.39	22.84
			198	5354.72	-2.08	-74.05	-166.74	-35.26	22.84
624	Copertura	136, 138	0	407.10	3.87	4623.14	-589.38	-540.81	-69.84
			775	407.10	3.87	-223.51	-589.38	2.09	-69.84
			1550	407.10	3.87	-4552.19	-589.38	541.65	-69.84
625	Copertura	139, 138	0	-5444.93	-2.31	-259.83	166.60	-7.27	19.80
			99	-5444.93	-2.31	-95.34	166.60	-18.57	19.80
			198	-5444.93	-2.31	73.95	166.60	-35.44	19.80
626	Copertura	140, 141	0	6802.89	-2.18	322.60	-204.13	11.75	21.28
			99	6802.89	-2.18	120.34	-204.13	-16.51	21.28
			198	6802.89	-2.18	-83.49	-204.13	-33.11	21.28
627	Copertura	141, 142	0	-774.01	3.61	5140.46	-668.33	-518.28	-66.87
			775	-774.01	3.61	-304.40	-668.33	2.20	-66.87
			1550	-774.01	3.61	-5334.73	-668.33	518.14	-66.87
628	Copertura	143, 142	0	-6520.16	-2.51	-311.53	198.04	-11.69	16.83
			99	-6520.16	-2.51	-115.38	198.04	-20.12	16.83
			198	-6520.16	-2.51	82.68	198.04	-31.63	16.83
629	Copertura	144, 145	0	8460.69	-1.68	397.01	-252.61	6.67	18.01

			99	8460.69	-1.68	146.72	-252.61	-13.45	18.01
			198	8460.69	-1.68	-107.10	-252.61	-29.84	18.01
630	Copertura	145, 146	0	1592.02	3.64	6441.06	-797.91	-450.85	-59.64
			775	1592.02	3.64	481.66	-797.91	11.70	-59.64
			1550	1592.02	3.64	-6137.85	-797.91	473.67	-59.64
631	Copertura	147, 146	0	-7631.07	-1.74	-367.57	232.47	9.93	20.90
			99	-7631.07	-1.74	-137.34	232.47	-16.26	20.90
			198	-7631.07	-1.74	94.68	232.47	-33.49	20.90
632	Copertura	148, 149	0	9005.84	-1.65	435.94	-278.32	-4.96	12.26
			99	9005.84	-1.65	160.23	-278.32	-12.62	12.26
			198	9005.84	-1.65	-117.93	-278.32	-22.35	12.26
633	Copertura	149, 150	0	-1408.72	2.84	7252.67	-925.46	-361.73	-49.35
			775	-1408.72	2.84	-435.26	-925.46	21.01	-49.35
			1550	-1408.72	2.84	-7234.86	-925.46	403.45	-49.35
634	Copertura	151, 150	0	-8850.89	-1.49	-417.38	263.82	-10.41	15.75
			99	-8850.89	-1.49	-155.99	263.82	-16.83	15.75
			198	-8850.89	-1.49	107.61	263.82	-27.25	15.75
635	Copertura	152, 153	0	9605.88	-1.21	460.02	-292.76	-4.91	10.08
			99	9605.88	-1.21	171.39	-292.76	-9.39	10.08
			198	9605.88	-1.21	-122.57	-292.76	-17.54	10.08
636	Copertura	153, 154	0	624.28	2.51	7944.86	-1009.66	-286.16	-38.30
			775	624.28	2.51	-342.73	-1009.66	10.92	-38.30
			1551	624.28	2.51	-7764.62	-1009.66	307.77	-38.30
637	Copertura	155, 154	0	-9748.71	-0.41	-460.49	291.40	12.75	20.60
			99	-9748.71	-0.41	-173.06	291.40	-11.52	20.60
			198	-9748.71	-0.41	119.49	291.40	-29.38	20.60
638	Copertura	156, 157	0	10069.69	-0.99	486.68	-310.55	6.11	6.19
			99	10069.69	-0.99	179.75	-310.55	-7.51	6.19
			198	10069.69	-0.99	-131.54	-310.55	-10.97	6.19
639	Copertura	157, 158	0	-666.47	1.82	8441.05	-1066.75	-208.09	-27.87
			775	-666.47	1.82	368.85	-1066.75	9.19	-27.87
			1551	-666.47	1.82	-8185.92	-1066.75	224.17	-27.87
640	Copertura	159, 158	0	-10300.65	0.47	-482.50	301.42	7.56	11.47
			99	-10300.65	0.47	-183.94	301.42	-12.29	11.47
			198	-10300.65	0.47	120.30	301.42	-20.74	11.47
641	Copertura	160, 161	0	10196.41	-0.62	481.43	-300.63	-8.22	3.30
			99	10196.41	-0.62	183.89	-300.63	-5.70	3.30
			198	10196.41	-0.62	-117.53	-300.63	-5.77	3.30
642	Copertura	161, 162	0	456.29	1.51	8120.57	-1051.72	-118.09	-16.36
			776	456.29	1.51	-287.65	-1051.72	9.65	-16.36
			1551	456.29	1.51	-8267.17	-1051.72	135.71	-16.36
643	Copertura	163, 162	0	-10434.34	1.39	-498.04	315.60	14.61	16.55
			99	-10434.34	1.39	-186.23	315.60	-8.58	16.55
			198	-10434.34	1.39	129.82	315.60	-20.66	16.55
644	Copertura	164, 165	0	10275.46	0.42	491.14	-310.59	-10.37	-7.77
			99	10275.46	0.42	184.48	-310.59	3.22	-7.77
			198	10275.46	0.42	-127.16	-310.59	5.31	-7.77
645	Copertura	165, 166	0	495.89	0.82	8383.25	-1068.62	-21.31	-3.91
			776	495.89	0.82	-266.87	-1068.62	9.97	-3.91
			1551	495.89	0.82	-8342.99	-1068.62	39.71	-3.91
646	Copertura	167, 166	0	-10477.65	1.61	-496.35	312.37	10.23	9.73
			99	-10477.65	1.61	-187.83	312.37	-9.30	9.73
			198	-10477.65	1.61	126.42	312.37	-13.60	9.73
647	Copertura	168, 169	0	10334.12	0.88	493.40	-311.36	-8.53	-9.21
			99	10334.12	0.88	185.14	-311.36	2.63	-9.21
			198	10334.12	0.88	-125.75	-311.36	10.39	-9.21
648	Copertura	169, 170	0	-680.04	0.54	8277.09	-1065.42	87.51	10.46
			776	-680.04	0.54	387.99	-1065.42	8.78	10.46
			1552	-680.04	0.54	-8423.49	-1065.42	-75.27	10.46
649	Copertura	171, 170	0	-10492.27	2.60	-502.35	319.01	15.58	13.91
			99	-10492.27	2.60	-186.64	319.01	-4.49	13.91
			198	-10492.27	2.60	133.89	319.01	-12.88	13.91
650	Copertura	172, 173	0	9922.32	1.09	468.60	-292.14	-9.43	-11.30
			99	9922.32	1.09	179.30	-292.14	3.65	-11.30
			198	9922.32	1.09	-116.53	-292.14	13.77	-11.30
651	Copertura	173, 175	0	-1330.90	-0.54	7784.17	-1012.27	151.94	18.71
			776	-1330.90	-0.54	-410.66	-1012.27	8.67	18.71
			1552	-1330.90	-0.54	-8081.17	-1012.27	-139.17	18.71
652	Copertura	174, 175	0	-10168.81	2.68	-489.39	311.65	-8.96	8.00
			99	-10168.81	2.68	-180.84	311.65	3.82	8.00
			198	-10168.81	2.68	130.81	311.65	-7.37	8.00
653	Copertura	176, 177	0	9339.59	1.49	430.06	-267.17	-14.42	-15.34

			99	9339.59	1.49	165.10	-267.17	5.66	-15.34
			198	9339.59	1.49	-101.57	-267.17	18.94	-15.34
654	Copertura	177, 178	0	4267.58	-0.99	7334.22	-915.55	241.80	27.03
			776	4267.58	-0.99	-549.20	-915.55	33.67	27.03
			1552	4267.58	-0.99	-7168.15	-915.55	-177.78	27.03
655	Copertura	179, 178	0	-9670.00	2.79	-468.04	294.90	14.06	7.08
			99	-9670.00	2.79	-175.61	294.90	7.88	7.08
			198	-9670.00	2.79	118.06	294.90	4.53	7.08
656	Copertura	180, 181	0	8797.13	2.50	424.11	-265.36	-11.81	-11.37
			99	8797.13	2.50	160.93	-265.36	5.20	-11.37
			198	8797.13	2.50	-103.17	-265.36	12.99	-11.37
657	Copertura	181, 182	0	-3649.81	-0.99	7062.42	-897.71	275.93	33.35
			775	-3649.81	-0.99	396.13	-897.71	19.11	33.35
			1550	-3649.81	-0.99	-7107.74	-897.71	-241.01	33.35
658	Copertura	183, 182	0	-9251.57	2.73	-426.25	267.99	13.07	-8.26
			99	-9251.57	2.73	-162.29	267.99	6.82	-8.26
			198	-9251.57	2.73	106.83	267.99	6.79	-8.26
659	Copertura	184, 185	0	8605.68	3.01	400.74	-250.86	-9.81	-13.15
			99	8605.68	3.01	152.49	-250.86	6.40	-13.15
			198	8605.68	3.01	-99.69	-250.86	16.98	-13.15
660	Copertura	185, 186	0	1120.48	-1.54	6503.27	-842.15	356.44	45.96
			775	1120.48	-1.54	-501.73	-842.15	1.96	45.96
			1550	1120.48	-1.54	-6553.79	-842.15	-357.03	45.96
661	Copertura	187, 186	0	-8750.57	3.45	-415.04	262.65	12.22	-8.27
			99	-8750.57	3.45	-154.68	262.65	10.55	-8.27
			198	-8750.57	3.45	107.21	262.65	13.42	-8.27
662	Copertura	188, 189	0	7562.60	3.69	363.22	-233.13	-11.80	-16.56
			99	7562.60	3.69	132.35	-233.13	9.17	-16.56
			198	7562.60	3.69	-100.85	-233.13	22.45	-16.56
663	Copertura	189, 190	0	768.49	-2.18	5944.44	-735.97	441.09	57.00
			775	768.49	-2.18	-472.69	-735.97	-2.23	57.00
			1550	768.49	-2.18	-5577.18	-735.97	-443.20	57.00
664	Copertura	191, 190	0	-7650.66	3.86	-360.48	228.13	-12.08	-15.45
			99	-7650.66	3.86	-134.61	228.13	11.07	-15.45
			198	-7650.66	3.86	93.79	228.13	20.75	-15.45
665	Copertura	192, 193	0	6095.32	3.73	289.34	-184.49	-13.19	-19.20
			99	6095.32	3.73	107.41	-184.49	10.17	-19.20
			198	6095.32	3.73	-79.45	-184.49	25.54	-19.20
666	Copertura	193, 195	0	439.13	-2.48	5043.53	-655.52	497.69	64.34
			775	439.13	-2.48	-267.76	-655.52	1.76	64.34
			1550	439.13	-2.48	-5159.42	-655.52	-499.57	64.34
667	Copertura	194, 195	0	-5949.82	4.07	-284.05	182.15	13.49	-13.55
			99	-5949.82	4.07	-104.86	182.15	14.82	-13.55
			198	-5949.82	4.07	80.20	182.15	21.50	-13.55
668	Copertura	196, 197	0	5288.44	4.11	250.48	-161.74	-17.62	-21.15
			99	5288.44	4.11	90.32	-161.74	12.96	-21.15
			198	5288.44	4.11	-73.38	-161.74	26.80	-21.15
669	Copertura	197, 199	0	-534.53	-2.55	4070.48	-499.76	532.56	68.74
			775	-534.53	-2.55	339.36	-499.76	1.71	68.74
			1550	-534.53	-2.55	-3832.98	-499.76	-532.98	68.74
670	Copertura	198, 199	0	-4755.97	4.34	-220.81	140.07	12.02	-15.51
			99	-4755.97	4.34	-84.40	140.07	15.25	-15.51
			198	-4755.97	4.34	58.93	140.07	23.24	-15.51
671	Copertura	200, 201	0	5080.99	3.88	243.34	-162.72	-13.28	-19.59
			99	5080.99	3.88	82.17	-162.72	10.85	-19.59
			198	5080.99	3.88	-80.30	-162.72	26.84	-19.59
672	Copertura	201, 202	0	-969.37	-2.46	2826.42	-310.28	520.53	67.14
			775	-969.37	-2.46	669.73	-310.28	1.81	67.14
			1550	-969.37	-2.46	-2588.91	-310.28	-520.73	67.14
673	Copertura	203, 202	0	-4304.57	4.09	-202.63	132.50	-9.69	-16.00
			99	-4304.57	4.09	-71.43	132.50	13.30	-16.00
			198	-4304.57	4.09	61.59	132.50	24.53	-16.00
674	Copertura	204, 205	0	3439.81	3.72	169.43	-118.04	-12.48	-17.73
			99	3439.81	3.72	53.12	-118.04	9.65	-17.73
			198	3439.81	3.72	-65.48	-118.04	23.69	-17.73
675	Copertura	205, 206	0	-747.71	-2.14	-3105.56	396.55	468.28	60.54
			775	-747.71	-2.14	294.23	396.55	-2.11	60.54
			1550	-747.71	-2.14	3043.84	396.55	-470.02	60.54
676	Copertura	207, 206	0	-2869.78	4.01	-148.89	106.10	-13.04	-11.47
			99	-2869.78	4.01	-44.60	106.10	14.18	-11.47
			198	-2869.78	4.01	62.56	106.10	19.11	-11.47
677	Copertura	79	0	1486.32	54.59	-75.77	112.42	-127.39	-241.28

			125	1486.32	54.59	64.81	112.42	194.05	-241.28
			250	1486.32	54.59	205.32	112.42	489.56	-241.28
678	Copertura	124	0	-1050.57	18.95	40.33	-40.26	-1453.52	-659.68
			155	-1050.57	18.95	-22.48	-40.26	-506.77	-659.68
			310	-1050.57	18.95	-84.50	-40.26	-683.19	-659.68
679	Copertura	80	0	1797.38	40.24	15.05	90.24	-763.87	-897.95
			45	1797.38	40.24	54.98	90.24	-993.04	-897.95
			90	1797.38	40.24	95.56	90.24	-1236.87	-897.95
680	Copertura	128	0	-1493.66	19.83	40.31	-39.63	-2203.22	-974.64
			155	-1493.66	19.83	-21.52	-39.63	-843.51	-974.64
			310	-1493.66	19.83	-82.82	-39.63	-1007.13	-974.64
681	Copertura	82	0	2393.86	33.42	5.96	104.32	-1172.33	-1305.01
			43	2393.86	33.42	48.64	104.32	-1411.76	-1305.01
			85	2393.86	33.42	92.28	104.32	-1679.13	-1305.01
682	Copertura	132	0	-1577.46	22.34	41.28	-40.69	-2760.50	-1042.68
			155	-1577.46	22.34	-21.91	-40.69	-1276.95	-1042.68
			310	-1577.46	22.34	-84.88	-40.69	-739.91	-1042.68
683	Copertura	83	0	2200.00	34.82	11.54	89.99	-1148.33	-1329.44
			43	2200.00	34.82	48.02	89.99	-1165.89	-1329.44
			85	2200.00	34.82	86.38	89.99	-1261.89	-1329.44
684	Copertura	137	0	-1753.56	24.37	42.70	-41.74	-3579.53	-1293.93
			155	-1753.56	24.37	-22.13	-41.74	-1643.39	-1293.93
			310	-1753.56	24.37	-86.72	-41.74	812.28	-1293.93
685	Copertura	84	0	2064.83	33.38	10.41	98.84	-1230.11	-1311.76
			43	2064.83	33.38	47.25	98.84	-1023.29	-1311.76
			85	2064.83	33.38	89.36	98.84	-896.39	-1311.76
686	Copertura	140	0	-2033.20	21.55	42.46	-41.63	-4481.47	-1688.27
			155	-2033.20	21.55	-22.26	-41.63	-2015.44	-1688.27
			310	-2033.20	21.55	-86.62	-41.63	1170.69	-1688.27
687	Copertura	85	0	1993.18	29.85	22.53	69.20	-1395.41	-1524.61
			43	1993.18	29.85	46.82	69.20	-1035.30	-1524.61
			85	1993.18	29.85	75.64	69.20	-788.08	-1524.61
688	Copertura	144	0	-2696.28	18.43	41.51	-40.95	-5515.19	-2140.29
			155	-2696.28	18.43	-22.54	-40.95	-2374.32	-2140.29
			310	-2696.28	18.43	-85.94	-40.95	-1598.73	-2140.29
689	Copertura	86	0	2375.08	31.54	7.21	100.51	-1759.16	-1807.54
			43	2375.08	31.54	40.88	100.51	-1397.73	-1807.54
			85	2375.08	31.54	83.72	100.51	-1135.04	-1807.54
690	Copertura	87	0	2677.03	22.62	35.16	42.49	-1894.47	-2092.61
			43	2677.03	22.62	40.20	42.49	-1466.66	-2092.61
			85	2677.03	22.62	56.78	42.49	-1164.11	-2092.61
691	Copertura	148	0	-2721.04	12.96	91.26	-65.26	-6005.17	-2180.06
			155	-2721.04	12.96	-15.98	-65.26	-2756.98	-2180.06
			310	-2721.04	12.96	-111.19	-65.26	-1374.36	-2180.06
692	Copertura	88	0	2785.14	26.57	-17.57	96.72	-2170.49	-2341.52
			43	2785.14	26.57	30.75	96.72	-1752.84	-2341.52
			85	2785.14	26.57	69.67	96.72	-1469.20	-2341.52
693	Copertura	152	0	-2574.06	13.53	117.54	-79.99	-6402.29	-2290.78
			155	-2574.06	13.53	-13.77	-79.99	-2970.49	-2290.78
			310	-2574.06	13.53	-131.55	-79.99	-1304.33	-2290.78
694	Copertura	89	0	2777.69	13.73	26.66	46.54	-2366.38	-2475.22
			43	2777.69	13.73	29.76	46.54	-1936.95	-2475.22
			85	2777.69	13.73	48.08	46.54	-1649.34	-2475.22
695	Copertura	156	0	-2619.06	10.83	131.30	-88.12	-6746.04	-2381.83
			155	-2619.06	10.83	-11.32	-88.12	-3167.04	-2381.83
			310	-2619.06	10.83	-143.70	-88.12	-1238.10	-2381.83
696	Copertura	90	0	2801.00	15.16	9.15	57.64	-2326.33	-2479.30
			43	2801.00	15.16	25.94	57.64	-1824.78	-2479.30
			85	2801.00	15.16	49.71	57.64	1469.76	-2479.30
697	Copertura	160	0	-2533.56	8.05	146.30	-97.82	-6777.78	-2415.99
			155	-2533.56	8.05	-10.20	-97.82	-3249.97	-2415.99
			310	-2533.56	8.05	-156.98	-97.82	-1419.49	-2415.99
698	Copertura	91	0	2819.17	-13.41	20.42	46.61	-2341.75	-2494.07
			43	2819.17	-13.41	24.25	46.61	-1841.12	-2494.07
			85	2819.17	-13.41	43.00	46.61	1487.29	-2494.07
699	Copertura	164	0	-2649.81	9.36	154.39	-102.32	-6867.33	-2419.51
			155	-2649.81	9.36	-9.39	-102.32	-3276.60	-2419.51
			310	-2649.81	9.36	-163.14	-102.32	1320.07	-2419.51
700	Copertura	92	0	2960.46	-11.92	15.72	38.00	-2243.90	-2502.67
			43	2960.46	-11.92	27.29	38.00	-1733.05	-2502.67
			85	2960.46	-11.92	43.30	38.00	-1402.90	-2502.67
701	Copertura	168	0	-2668.64	-11.08	164.53	-107.48	-6872.67	-2476.55

			155	-2668.64	-11.08	-9.10	-107.48	-3197.56	-2476.55
			310	-2668.64	-11.08	-169.25	-107.48	1482.76	-2476.55
702	Copertura	93	0	2734.88	-21.05	-12.43	90.18	-2306.81	-2443.71
			43	2734.88	-21.05	29.07	90.18	-1862.33	-2443.71
			85	2734.88	-21.05	67.46	90.18	-1554.93	-2443.71
703	Copertura	172	0	-2418.37	-10.25	168.65	-110.46	-6562.39	-2393.96
			155	-2418.37	-10.25	-9.60	-110.46	-3085.17	-2393.96
			310	-2418.37	-10.25	-173.85	-110.46	1503.19	-2393.96
704	Copertura	94	0	2524.23	-18.67	36.46	32.08	-2226.10	-2327.61
			43	2524.23	-18.67	46.62	32.08	-1844.10	-2327.61
			85	2524.23	-18.67	59.12	32.08	-1588.38	-2327.61
705	Copertura	176	0	-2235.08	-15.70	171.50	-113.06	-6147.34	-2198.06
			155	-2235.08	-15.70	-8.26	-113.06	-2930.25	-2198.06
			310	-2235.08	-15.70	-179.02	-113.06	1100.93	-2198.06
706	Copertura	180	0	-2179.11	-15.97	41.82	-43.27	-5882.30	-2086.51
			155	-2179.11	-15.97	-25.42	-43.27	-2880.56	-2086.51
			310	-2179.11	-15.97	-92.44	-43.27	1118.47	-2086.51
707	Copertura	95	0	2623.02	-25.88	-12.49	124.26	-1976.25	-2167.64
			43	2623.02	-25.88	43.72	124.26	-1523.39	-2167.64
			85	2623.02	-25.88	96.53	124.26	-1202.67	-2167.64
708	Copertura	184	0	-2192.24	-16.89	42.54	-44.47	-5651.98	-2138.33
			155	-2192.24	-16.89	-26.93	-44.47	-2587.89	-2138.33
			310	-2192.24	-16.89	-95.43	-44.47	1554.34	-2138.33
709	Copertura	96	0	2235.37	-25.23	40.52	47.41	-1975.01	-2125.71
			43	2235.37	-25.23	57.50	47.41	-1679.94	-2125.71
			85	2235.37	-25.23	74.95	47.41	-1509.82	-2125.71
710	Copertura	188	0	-2278.98	-21.05	44.39	-46.16	-5009.82	-1867.34
			155	-2278.98	-21.05	-27.75	-46.16	-2201.21	-1867.34
			310	-2278.98	-21.05	-98.90	-46.16	1236.57	-1867.34
711	Copertura	97	0	2164.76	-34.06	12.07	117.31	-1717.06	-1878.38
			43	2164.76	-34.06	60.56	117.31	-1489.83	-1878.38
			85	2164.76	-34.06	110.59	117.31	-1378.51	-1878.38
712	Copertura	192	0	-1790.38	-24.38	46.13	-47.94	-4021.98	-1504.81
			155	-1790.38	-24.38	-28.42	-47.94	-1828.66	-1504.81
			310	-1790.38	-24.38	-102.61	-47.94	-1020.17	-1504.81
713	Copertura	106	0	-1684.13	-34.67	14.59	103.39	-1263.94	-1410.62
			43	-1684.13	-34.67	56.89	103.39	-1001.88	-1410.62
			85	-1684.13	-34.67	100.55	103.39	825.22	-1410.62
714	Copertura	196	0	-2002.50	-25.82	46.90	-48.35	-3412.26	-1409.13
			155	-2002.50	-25.82	-28.35	-48.35	-1449.24	-1409.13
			310	-2002.50	-25.82	-103.16	-48.35	-1261.01	-1409.13
715	Copertura	107	0	-1589.05	-41.34	11.86	115.23	-1234.71	-1173.23
			43	-1589.05	-41.34	58.79	115.23	-1117.85	-1173.23
			85	-1589.05	-41.34	107.39	115.23	1058.56	-1173.23
716	Copertura	200	0	-2230.56	-24.47	44.46	-46.25	-3142.41	-1543.43
			155	-2230.56	-24.47	-27.45	-46.25	-961.58	-1543.43
			310	-2230.56	-24.47	-99.03	-46.25	-1857.97	-1543.43
717	Copertura	108	0	-1811.49	-35.87	14.74	101.83	-1040.34	-1163.87
			43	-1811.49	-35.87	56.35	101.83	-1151.70	-1163.87
			85	-1811.49	-35.87	99.73	101.83	-1303.94	-1163.87
718	Copertura	204	0	2047.62	-22.74	41.00	-43.75	-2094.82	-1117.56
			155	2047.62	-22.74	-26.94	-43.75	-604.99	-1117.56
			310	2047.62	-22.74	-94.71	-43.75	-1448.09	-1117.56
719	Copertura	109	0	-1762.67	-30.22	12.43	124.01	-621.21	-829.69
			43	-1762.67	-30.22	59.49	124.01	767.47	-829.69
			85	-1762.67	-30.22	111.21	124.01	951.10	-829.69
720	Copertura	110	0	1780.87	-83.21	87.72	93.16	282.51	-251.86
			43	1780.87	-83.21	126.40	93.16	388.16	-251.86
			85	1780.87	-83.21	165.98	93.16	494.58	-251.86
721	Copertura	14	0	1330.42	21.84	-233.65	139.51	-516.87	-211.06
			95	1330.42	21.84	-101.15	139.51	-317.86	-211.06
			190	1330.42	21.84	33.61	139.51	-127.55	-211.06
722	Copertura	15	0	-1153.68	15.31	67.00	-20.97	129.12	1019.90
			65	-1153.68	15.31	53.65	-20.97	-675.85	1019.90
			130	-1153.68	15.31	42.72	-20.97	-1336.50	1019.90
723	Copertura	16	0	1119.54	13.44	-92.51	58.30	148.28	1244.28
			65	1119.54	13.44	-55.27	58.30	-857.08	1244.28
			130	1119.54	13.44	-19.82	58.30	-1664.56	1244.28
724	Copertura	17	0	-1862.54	17.12	64.49	-18.18	177.41	1633.93
			65	-1862.54	17.12	53.96	-18.18	-981.88	1633.93
			130	-1862.54	17.12	45.26	-18.18	-2041.05	1633.93
725	Copertura	18	0	1601.64	13.11	-102.70	73.48	235.93	1985.64

			65	1601.64	13.11	-56.45	73.48	-1282.08	1985.64
			130	1601.64	13.11	-11.94	73.48	-2570.22	1985.64
726	Copertura	19	0	-2493.33	17.34	67.29	-18.96	236.45	2085.37
			65	-2493.33	17.34	55.48	-18.96	-1204.79	2085.37
			130	-2493.33	17.34	45.60	-18.96	-2559.25	2085.37
727	Copertura	20	0	2433.49	12.98	-102.37	72.22	262.58	2365.68
			65	2433.49	12.98	-55.98	72.22	-1436.98	2365.68
			130	2433.49	12.98	-11.75	72.22	-2972.64	2365.68
728	Copertura	21	0	-2972.30	18.04	68.87	-19.48	284.79	2735.05
			65	-2972.30	18.04	56.39	-19.48	-1545.40	2735.05
			130	-2972.30	18.04	45.15	-19.48	-3322.51	2735.05
729	Copertura	22	0	3026.97	14.36	-106.81	75.11	305.56	2748.78
			65	3026.97	14.36	-58.00	75.11	-1559.69	2748.78
			130	3026.97	14.36	-10.61	75.11	-3343.29	2748.78
730	Copertura	23	0	-3655.11	17.04	68.60	-20.58	351.17	3403.50
			65	-3655.11	17.04	56.23	-20.58	-1947.88	3403.50
			130	-3655.11	17.04	46.60	-20.58	-4159.08	3403.50
731	Copertura	24	0	3929.33	10.59	-105.79	74.85	367.61	3303.83
			65	3929.33	10.59	-57.38	74.85	-1880.20	3303.83
			130	3929.33	10.59	-12.89	74.85	-4026.57	3303.83
732	Copertura	25	0	-4124.71	15.21	71.30	-24.43	473.10	4189.41
			65	-4124.71	15.21	56.58	-24.43	-2397.40	4189.41
			130	-4124.71	15.21	44.18	-24.43	-5118.54	4189.41
733	Copertura	26	0	4461.24	15.55	-130.53	102.27	408.37	3893.94
			65	4461.24	15.55	-64.20	102.27	-2214.51	3893.94
			130	4461.24	15.55	6.89	102.27	-4744.67	3893.94
734	Copertura	27	0	5168.13	8.38	-151.26	138.47	480.88	4453.16
			65	5168.13	8.38	-61.68	138.47	-2536.61	4453.16
			130	5168.13	8.38	29.12	138.47	-5429.88	4453.16
735	Copertura	28	0	-4921.34	12.18	44.91	93.66	480.10	4550.99
			65	-4921.34	12.18	42.23	93.66	-2612.98	4550.99
			130	-4921.34	12.18	82.82	93.66	-5569.62	4550.99
736	Copertura	29	0	5299.45	10.96	-225.21	221.84	501.55	4885.94
			65	5299.45	10.96	-81.70	221.84	-2806.57	4885.94
			130	5299.45	10.96	63.67	221.84	-5981.13	4885.94
737	Copertura	30	0	-5437.24	11.49	-80.02	137.70	546.24	4880.07
			65	-5437.24	11.49	34.94	137.70	-2772.81	4880.07
			130	-5437.24	11.49	104.21	137.70	-5943.30	4880.07
738	Copertura	31	0	5866.27	4.67	-233.82	232.13	513.95	5140.89
			65	5866.27	4.67	-83.05	232.13	-2957.70	5140.89
			130	5866.27	4.67	68.83	232.13	-6297.96	5140.89
739	Copertura	32	0	-5671.79	10.06	-89.60	156.14	577.05	5134.86
			65	-5671.79	10.06	29.34	156.14	-2924.83	5134.86
			130	-5671.79	10.06	115.17	156.14	-6260.77	5134.86
740	Copertura	33	0	5710.60	7.26	-270.45	269.34	542.15	5262.31
			65	5710.60	7.26	-95.68	269.34	-3033.62	5262.31
			130	5710.60	7.26	82.79	269.34	-6448.80	5262.31
741	Copertura	34	0	-5834.58	9.09	-105.66	175.73	558.51	5196.37
			65	-5834.58	9.09	25.93	175.73	-2920.21	5196.37
			130	-5834.58	9.09	126.64	175.73	-6296.89	5196.37
742	Copertura	35	0	6002.12	-7.50	-288.19	289.18	528.53	5268.51
			65	6002.12	-7.50	-100.62	289.18	-3038.26	5268.51
			130	6002.12	-7.50	91.32	289.18	-6461.26	5268.51
743	Copertura	36	0	-5754.54	4.63	-116.18	188.55	578.05	5248.01
			65	-5754.54	4.63	23.82	188.55	-2966.90	5248.01
			130	-5754.54	4.63	131.44	188.55	-6376.89	5248.01
744	Copertura	37	0	5675.81	-5.82	-308.30	313.24	529.31	5275.73
			65	5675.81	-5.82	-104.75	313.24	-3068.75	5275.73
			130	5675.81	-5.82	100.21	313.24	-6496.27	5275.73
745	Copertura	38	0	-5693.01	5.81	-129.36	206.76	564.28	5235.06
			65	-5693.01	5.81	23.31	206.76	-2978.75	5235.06
			130	-5693.01	5.81	140.53	206.76	-6380.10	5235.06
746	Copertura	39	0	5634.26	-9.74	-321.55	326.47	539.50	5102.41
			65	5634.26	-9.74	-110.03	326.47	-2994.67	5102.41
			130	5634.26	-9.74	104.31	326.47	-6308.99	5102.41
747	Copertura	40	0	-5597.04	-3.89	-132.61	209.96	516.19	5006.92
			65	-5597.04	-3.89	24.55	209.96	-2841.65	5006.92
			130	-5597.04	-3.89	142.60	209.96	-6095.21	5006.92
748	Copertura	41	0	4937.90	-6.83	-266.37	268.62	410.77	4800.95
			65	4937.90	-6.83	-92.49	268.62	-2852.71	4800.95
			130	4937.90	-6.83	84.96	268.62	-5972.07	4800.95
749	Copertura	42	0	-5418.19	-9.34	-125.96	207.84	550.25	4764.44

			65	-5418.19	-9.34	21.69	207.84	-2622.08	4764.44
			130	-5418.19	-9.34	144.66	207.84	-5718.23	4764.44
750	Copertura	43	0	-5305.02	-12.27	91.42	-48.90	426.26	4478.73
			65	-5305.02	-12.27	62.11	-48.90	-2557.28	4478.73
			130	-5305.02	-12.27	33.73	-48.90	-5458.32	4478.73
751	Copertura	44	0	5003.56	-9.11	-221.35	189.44	551.99	4684.78
			65	5003.56	-9.11	-98.22	189.44	-2593.47	4684.78
			130	5003.56	-9.11	26.21	189.44	-5635.06	4684.78
752	Copertura	45	0	-4867.95	-11.93	95.38	-51.42	459.40	4326.01
			65	-4867.95	-11.93	64.43	-51.42	-2440.51	4326.01
			130	-4867.95	-11.93	34.72	-51.42	-5251.42	4326.01
753	Copertura	46	0	4556.47	-8.30	-148.91	110.29	464.77	4324.71
			65	4556.47	-8.30	-77.43	110.29	-2507.61	4324.71
			130	4556.47	-8.30	8.32	110.29	-5316.80	4324.71
754	Copertura	47	0	-4005.85	-15.69	99.91	-55.37	410.32	3795.83
			65	-4005.85	-15.69	67.42	-55.37	-2181.25	3795.83
			130	-4005.85	-15.69	36.59	-55.37	-4646.94	3795.83
755	Copertura	48	0	4091.26	-14.95	-151.39	118.20	407.48	3794.25
			65	4091.26	-14.95	-74.97	118.20	-2181.56	3794.25
			130	4091.26	-14.95	11.10	118.20	-4646.21	3794.25
756	Copertura	49	0	-3462.77	-17.03	104.39	-55.96	328.48	3057.08
			65	-3462.77	-17.03	69.48	-55.96	-1746.85	3057.08
			130	-3462.77	-17.03	35.02	-55.96	-3732.87	3057.08
757	Copertura	50	0	3446.34	-13.90	-147.04	117.05	316.50	3008.11
			65	3446.34	-13.90	-71.63	117.05	-1709.58	3008.11
			130	3446.34	-13.90	6.12	117.05	-3664.02	3008.11
758	Copertura	51	0	-2498.01	-17.35	105.24	-56.93	275.34	2557.07
			65	-2498.01	-17.35	69.33	-56.93	-1501.54	2557.07
			130	-2498.01	-17.35	33.73	-56.93	-3162.05	2557.07
759	Copertura	52	0	2695.36	-14.48	-145.19	116.01	262.18	2329.10
			65	2695.36	-14.48	-69.93	116.01	-1335.02	2329.10
			130	2695.36	-14.48	7.90	116.01	-2846.72	2329.10
760	Copertura	53	0	-2031.28	-17.77	102.57	-57.48	247.73	2248.09
			65	-2031.28	-17.77	67.23	-57.48	-1440.69	2248.09
			130	-2031.28	-17.77	34.24	-57.48	-2899.43	2248.09
761	Copertura	54	0	2024.35	-17.01	-135.19	107.41	214.41	1962.83
			65	2024.35	-17.01	-66.94	107.41	-1211.93	1962.83
			130	2024.35	-17.01	7.99	107.41	-2485.79	1962.83
762	Copertura	55	0	-1002.49	-16.01	100.03	-60.39	182.55	1454.45
			65	-1002.49	-16.01	64.75	-60.39	-982.22	1454.45
			130	-1002.49	-16.01	35.12	-60.39	-1925.68	1454.45
763	Copertura	56	0	1095.21	-11.54	-133.91	107.50	170.13	1292.48
			65	1095.21	-11.54	-65.50	107.50	-852.96	1292.48
			130	1095.21	-11.54	7.46	107.50	-1691.03	1292.48
764	Copertura	70	0	1796.56	-40.57	-237.14	111.07	-543.93	-225.51
			95	1796.56	-40.57	-131.70	111.07	-330.86	-225.51
			190	1796.56	-40.57	-27.76	111.07	-121.93	-225.51
765	Copertura	81	0	1753.52	19.93	-76.02	109.16	-1228.58	-972.58
			80	1753.52	19.93	12.38	109.16	-548.83	-972.58
			160	1753.52	19.93	98.67	109.16	-766.25	-972.58
766	Copertura	126	0	1759.88	16.06	-16.82	75.55	-1811.29	-991.40
			30	1759.88	16.06	7.12	75.55	-1517.55	-991.40
			60	1759.88	16.06	28.57	75.55	-1225.59	-991.40
767	Copertura	98	0	2303.52	27.50	-64.13	91.67	-1969.40	-1412.90
			82	2303.52	27.50	11.76	91.67	-919.17	-1412.90
			165	2303.52	27.50	86.86	91.67	-1169.07	-1412.90
768	Copertura	99	0	2259.18	26.76	-63.08	90.35	-2405.97	-1368.37
			82	2259.18	26.76	11.94	90.35	-1409.04	-1368.37
			165	2259.18	26.76	85.81	90.35	-1152.70	-1368.37
769	Copertura	100	0	1968.34	27.31	-61.26	87.97	-2833.05	-1339.76
			82	1968.34	27.31	11.79	87.97	-1793.57	-1339.76
			165	1968.34	27.31	84.06	87.97	-1226.02	-1339.76
770	Copertura	101	0	2034.64	31.44	-67.12	97.00	-3426.75	-1535.06
			82	2034.64	31.44	12.93	97.00	-2185.75	-1535.06
			165	2034.64	31.44	92.64	97.00	-1399.00	-1535.06
771	Copertura	102	0	2287.67	21.61	-41.12	68.02	-4055.77	-1843.37
			82	2287.67	21.61	15.71	68.02	-2594.47	-1843.37
			165	2287.67	21.61	71.04	68.02	-1755.93	-1843.37
772	Copertura	103	0	2694.37	32.50	-59.25	87.81	-4591.23	-2119.80
			82	2694.37	32.50	15.14	87.81	-2969.03	-2119.80
			165	2694.37	32.50	86.08	87.81	-1897.13	-2119.80
773	Copertura	104	0	2711.90	15.12	19.70	39.13	-5043.91	-2387.72

			82	2711.90	15.12	17.95	39.13	-3201.93	-2387.72
			165	2711.90	15.12	47.37	39.13	-2168.41	-2387.72
774	Copertura	105	0	2784.73	25.21	-25.64	52.71	-5297.52	-2530.09
			82	2784.73	25.21	23.87	52.71	-3395.44	-2530.09
			165	2784.73	25.21	62.17	52.71	-2367.71	-2530.09
775	Copertura	111	0	2737.11	-15.48	-26.96	39.30	-5362.12	-2515.96
			80	2737.11	-15.48	22.04	39.30	-3457.92	-2515.96
			160	2737.11	-15.48	49.70	39.30	-2325.61	-2515.96
776	Copertura	112	0	2814.27	15.10	-18.51	34.97	-5479.65	-2541.80
			82	2814.27	15.10	29.03	34.97	-3527.49	-2541.80
			165	2814.27	15.10	53.00	34.97	-2341.28	-2541.80
777	Copertura	113	0	2907.73	-18.65	35.68	45.37	-5505.78	-2535.79
			82	2907.73	-18.65	26.56	45.37	-3469.86	-2535.79
			165	2907.73	-18.65	59.28	45.37	-2244.25	-2535.79
778	Copertura	114	0	2769.17	-13.60	29.26	32.03	-5351.60	-2501.55
			82	2769.17	-13.60	28.17	32.03	-3356.07	-2501.55
			165	2769.17	-13.60	47.49	32.03	-2305.15	-2501.55
779	Copertura	115	0	2450.48	-15.54	-62.21	96.52	-5040.11	-2385.45
			82	2450.48	-15.54	17.82	96.52	-3177.62	-2385.45
			165	2450.48	-15.54	96.82	96.52	-2227.76	-2385.45
780	Copertura	116	0	2686.18	-14.71	-26.75	53.73	-4788.50	-2211.57
			82	2686.18	-14.71	26.39	53.73	-3032.00	-2211.57
			165	2686.18	-14.71	67.32	53.73	-1974.41	-2211.57
781	Copertura	117	0	2157.52	-36.47	-84.89	125.81	-4451.78	-2173.36
			82	2157.52	-36.47	18.95	125.81	-2790.82	-2173.36
			165	2157.52	-36.47	122.31	125.81	-1978.00	-2173.36
782	Copertura	118	0	2240.42	-23.75	-76.01	108.54	-3885.50	-1928.62
			82	2240.42	-23.75	14.70	108.54	-2382.03	-1928.62
			165	2240.42	-23.75	103.27	108.54	-1714.19	-1928.62
783	Copertura	131	0	2376.74	13.56	-10.55	89.44	-2787.61	-1394.74
			30	2376.74	13.56	19.70	89.44	-2377.62	-1394.74
			60	2376.74	13.56	45.59	89.44	-1971.17	-1394.74
784	Copertura	133	0	2132.20	14.57	-11.32	89.05	-3213.89	-1376.34
			30	2132.20	14.57	18.85	89.05	-2807.81	-1376.34
			60	2132.20	14.57	45.50	89.05	-2404.05	-1376.34
785	Copertura	139	0	2061.78	16.48	-8.95	92.90	-3602.88	-1307.07
			30	2061.78	16.48	21.62	92.90	-3217.03	-1307.07
			60	2061.78	16.48	49.46	92.90	-2835.37	-1307.07
786	Copertura	143	0	1910.85	11.87	-10.93	89.34	-4337.84	-1536.63
			30	1910.85	11.87	19.12	89.34	-3880.58	-1536.63
			60	1910.85	11.87	45.62	89.34	-3424.33	-1536.63
787	Copertura	147	0	2367.97	21.31	6.12	115.82	-5112.05	-1810.25
			30	2367.97	21.31	38.58	115.82	-4584.57	-1810.25
			60	2367.97	21.31	72.97	115.82	-4058.21	-1810.25
788	Copertura	151	0	2564.04	-11.94	35.59	40.66	-5846.89	-2117.41
			30	2564.04	-11.94	38.72	40.66	-5217.11	-2117.41
			60	2564.04	-11.94	46.83	40.66	-4588.83	-2117.41
789	Copertura	155	0	2793.08	20.29	82.15	52.02	-6441.02	-2356.02
			30	2793.08	20.29	93.22	52.02	-5741.73	-2356.02
			60	2793.08	20.29	104.92	52.02	-5045.17	-2356.02
790	Copertura	159	0	2645.97	9.60	82.67	36.26	-6780.00	-2508.61
			30	2645.97	9.60	85.33	36.26	-6036.73	-2508.61
			60	2645.97	9.60	88.64	36.26	-5296.09	-2508.61
791	Copertura	119	0	-1585.19	-35.00	-75.22	109.65	-3117.13	-1419.98
			82	-1585.19	-35.00	15.40	109.65	-2009.41	-1419.98
			165	-1585.19	-35.00	105.68	109.65	-1267.40	-1419.98
792	Copertura	120	0	-1673.27	-28.85	-74.37	106.27	-2378.30	-1236.65
			82	-1673.27	-28.85	14.63	106.27	-1545.43	-1236.65
			165	-1673.27	-28.85	100.68	106.27	-1230.02	-1236.65
793	Copertura	121	0	-1696.67	-25.36	-74.93	108.33	-1962.79	-1233.54
			82	-1696.67	-25.36	15.65	108.33	-1073.55	-1233.54
			165	-1696.67	-25.36	103.49	108.33	-1045.07	-1233.54
794	Copertura	122	0	-1819.75	-34.97	-67.61	93.26	-1336.83	-889.86
			82	-1819.75	-34.97	9.29	93.26	-660.87	-889.86
			165	-1819.75	-34.97	85.97	93.26	-619.44	-889.86
795	Copertura	123	0	1824.81	-40.57	-27.76	114.88	-121.93	-236.98
			82	1824.81	-40.57	67.81	114.88	140.80	-236.98
			165	1824.81	-40.57	162.24	114.88	281.95	-236.98
796	Copertura	163	0	2841.31	16.11	104.48	34.80	-6946.03	-2486.74
			33	2841.31	16.11	110.34	34.80	-6152.40	-2486.74
			65	2841.31	16.11	116.32	34.80	-5360.90	-2486.74
797	Copertura	167	0	2673.36	12.84	109.46	34.66	-6955.76	-2506.12

			30	2673.36	12.84	111.18	34.66	-6212.99	-2506.12
			60	2673.36	12.84	115.96	34.66	-5480.21	-2506.12
798	Copertura	171	0	3014.03	14.67	126.05	27.47	-6997.63	-2511.90
			30	3014.03	14.67	128.69	27.47	-6250.45	-2511.90
			60	3014.03	14.67	131.41	27.47	-5505.00	-2511.90
799	Copertura	174	0	2613.04	-12.94	126.15	38.75	-6797.45	-2454.53
			30	2613.04	-12.94	127.90	38.75	-6073.89	-2454.53
			60	2613.04	-12.94	131.39	38.75	-5352.31	-2454.53
800	Copertura	179	0	2574.66	-7.93	108.42	-70.05	-6439.31	-2368.55
			30	2574.66	-7.93	90.48	-70.05	-5737.64	-2368.55
			60	2574.66	-7.93	74.40	-70.05	-5038.45	-2368.55
801	Copertura	183	0	2512.59	-16.27	21.57	186.26	-6061.03	-2191.03
			30	2512.59	-16.27	74.49	186.26	-5424.33	-2191.03
			60	2512.59	-16.27	130.34	186.26	-4788.79	-2191.03
802	Copertura	187	0	2281.42	-10.44	-7.02	112.62	-5731.53	-2179.17
			30	2281.42	-10.44	31.19	112.62	-5089.33	-2179.17
			60	2281.42	-10.44	63.43	112.62	-4449.55	-2179.17
803	Copertura	191	0	2083.45	-21.35	2.91	114.97	-5006.43	-1896.69
			30	2083.45	-21.35	34.54	114.97	-4445.93	-1896.69
			60	2083.45	-21.35	68.86	114.97	-3887.90	-1896.69
804	Copertura	194	0	-1702.90	17.35	-6.70	106.16	-3947.85	-1425.44
			30	-1702.90	17.35	33.61	106.16	-3530.76	-1425.44
			60	-1702.90	17.35	64.03	106.16	-3114.52	-1425.44
805	Copertura	198	0	-1510.64	-18.62	4.92	103.99	-3067.37	-1208.68
			30	-1510.64	-18.62	32.16	103.99	-2723.02	-1208.68
			60	-1510.64	-18.62	62.12	103.99	-2380.44	-1208.68
806	Copertura	203	0	-1820.95	-21.14	-4.63	94.70	-2688.17	-1242.34
			30	-1820.95	-21.14	26.56	94.70	-2322.68	-1242.34
			60	-1820.95	-21.14	54.38	94.70	-1959.80	-1242.34
807	Copertura	207	0	-1654.65	-13.19	6.29	98.33	-1839.55	-857.44
			30	-1654.65	-13.19	32.72	98.33	-1588.99	-857.44
			60	-1654.65	-13.19	60.85	98.33	-1339.83	-857.44

1.1.7.2 Piastre SLV

Tabella 14.I

Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	-22.932	15.134	12.142	7017.685	1162.528	1116.878	93.778	24.182
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	24.183	-11.901	-6.648	-7070.241	-1738.225	858.017	96.869	37.404
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	-15.312	6.886	7.262	4414.417	676.042	-922.104	61.033	-18.029

1.1.8 Risultati Condizioni (Sisma Y).

1.1.8.1 Sollecitazioni SLV

Tabella 15.I

Sollecitazioni									
Asta	Imp.	Fili	X [cm]	N [daN]	Mt [daNm]	Mxz [daNm]	Txz [daN]	Mxy [daNm]	Txy [daN]
1	Fondazio ne	1, 2	0	269.82	-1192.61	-1154.15	4354.04	125.59	404.50
			42	305.82	-1192.48	476.75	2994.59	-39.67	221.82
			83	347.25	-1192.37	1441.50	1915.46	-77.63	-372.34
2	Fondazio ne	1, 2	0	609.98	-754.39	560.36	1722.39	-77.17	287.71
			42	618.09	-754.30	1065.41	875.37	-67.63	36.21
			83	638.58	-754.22	1253.34	226.02	-69.79	-274.35
3	Fondazio ne	1, 15	0	-1039.46	1200.54	-976.70	4790.34	-55.20	-62.26
			40	-945.97	1200.45	661.70	3513.98	-49.89	-23.24
			80	-1046.31	1200.38	1849.97	2526.75	-43.24	-92.08
4	Fondazio ne	1, 15	0	-360.77	1044.26	1056.06	2553.83	-43.12	-51.56
			40	-256.03	1044.21	1917.19	1828.92	-28.02	-82.67
			80	410.88	1044.16	2534.77	1348.28	39.95	-143.35
5	Fondazio ne	2, 3	0	946.08	-753.43	754.90	776.04	-65.31	222.62
			35	955.74	-753.37	920.92	342.20	-41.10	-46.27
			69	967.76	-753.32	957.49	-139.02	-37.30	-241.80
6	Fondazio ne	2, 3	0	956.10	104.43	697.49	146.33	-37.12	211.10
			35	938.57	104.47	666.64	-283.98	-15.58	-58.16
			69	923.55	104.51	554.10	-525.77	36.67	-261.20
7	Fondazio ne	3, 4	0	966.27	-567.02	395.80	381.38	39.29	277.81
			35	949.37	-566.97	467.77	175.33	-19.05	89.66
			69	933.13	-566.92	472.38	-122.14	-48.40	-226.52
8	Fondazio ne	3, 4	0	962.90	233.19	371.91	-243.89	-48.23	230.81
			35	946.68	233.24	275.44	-400.24	-16.95	-88.29
			69	931.11	233.28	126.09	-548.59	41.64	-278.68
9	Fondazio ne	4, 5	0	957.44	-504.58	72.37	367.38	40.02	272.64
			35	941.91	-504.53	134.19	233.79	-16.39	69.60
			69	927.03	-504.50	177.36	-124.98	-46.65	-230.18
10	Fondazio ne	4, 5	0	952.39	299.93	103.73	-170.32	-46.51	232.12
			35	937.55	299.96	66.51	-293.06	-19.23	-87.24
			69	923.37	300.00	-86.79	-423.00	38.55	-265.85
11	Fondazio ne	5, 6	0	944.22	-460.54	-120.31	332.88	36.75	258.61
			35	929.60	-460.49	-30.16	200.17	-18.30	80.98
			69	916.06	-460.46	57.07	75.15	-43.28	-228.07
12	Fondazio ne	5, 6	0	944.67	237.99	-40.59	-80.37	-43.16	221.49
			35	926.03	238.02	-71.51	-202.37	-18.79	-51.95
			69	913.07	238.05	-149.48	-324.83	31.15	-252.25
13	Fondazio ne	6, 7	0	857.73	-417.10	-212.44	514.82	40.03	261.26
			35	845.19	-417.06	-44.64	397.89	-13.05	73.70
			69	833.29	-417.03	87.58	289.74	-39.72	-225.97
14	Fondazio ne	6, 7	0	859.66	197.42	-13.00	244.14	-39.61	225.84
			35	843.53	197.44	87.73	151.18	-12.48	-86.07
			69	832.11	197.48	138.59	116.10	47.47	-261.46
15	Fondazio ne	7, 8	0	775.23	-400.08	-112.48	327.87	29.13	239.84
			35	764.26	-400.05	98.56	244.61	-16.63	41.42
			69	753.95	-400.02	80.10	180.29	36.87	-212.62
16	Fondazio ne	7, 8	0	759.04	249.62	66.87	-157.34	36.80	222.24
			35	748.55	249.65	23.69	-220.99	-15.59	-55.92
			69	738.73	249.67	-70.96	-299.89	32.66	-243.10
17	Fondazio ne	8, 9	0	746.37	-323.78	-94.23	234.68	29.92	236.97
			35	731.97	-323.75	-36.95	154.29	-14.76	60.12
			69	722.57	-323.72	44.52	84.87	34.84	-218.17
18	Fondazio	8, 9	0	735.53	127.10	-51.97	89.74	34.78	214.96

	ne								
			35	710.67	127.12	-82.95	-163.63	-15.05	-45.60
			69	701.65	127.14	-141.01	-243.13	28.97	-234.65
19	Fondazio ne	9, 10	0	640.68	-341.72	-206.83	448.83	33.18	238.29
			35	631.96	-341.69	-56.01	371.22	-12.13	36.52
			69	623.92	-341.67	77.71	301.32	32.05	-214.40
20	Fondazio ne	9, 10	0	660.82	-124.54	-9.71	256.55	32.00	212.69
			35	622.78	-124.55	81.97	197.13	-11.91	-63.79
			69	614.87	-124.57	152.41	147.50	43.94	-240.16
21	Fondazio ne	10, 11	0	551.58	-313.15	121.84	261.63	30.92	225.22
			35	544.02	-313.14	111.61	222.07	-14.73	37.16
			69	537.19	-313.12	99.59	191.43	30.77	-206.18
22	Fondazio ne	10, 11	0	539.00	-142.53	81.85	141.37	30.74	212.04
			35	520.83	-142.54	56.60	151.45	-12.31	-25.64
			69	514.14	-142.55	61.39	196.06	29.59	-227.81
23	Fondazio ne	11, 12	0	534.63	-193.42	-22.73	203.97	26.65	220.88
			35	502.43	-193.40	55.61	172.60	-12.85	36.08
			69	485.94	-193.39	99.25	148.75	30.77	-209.97
24	Fondazio ne	11, 12	0	534.03	-134.20	64.48	104.26	30.76	211.80
			35	486.67	-134.21	69.65	124.69	-12.43	-44.55
			69	467.59	-134.23	82.45	184.54	30.51	-220.35
25	Fondazio ne	12, 13	0	548.28	-142.44	64.71	143.47	27.34	215.51
			35	495.29	-142.43	71.88	119.98	-13.83	25.43
			69	447.55	-142.43	96.69	159.82	29.26	-209.95
26	Fondazio ne	12, 13	0	592.96	136.89	79.68	-149.85	29.26	198.76
			35	538.32	136.90	-69.52	-231.05	-9.92	-29.33
			69	484.91	136.91	110.42	-321.13	35.13	-225.06
27	Fondazio ne	13, 14	0	405.87	-124.60	-52.66	142.87	46.14	251.89
			42	343.42	-124.62	-67.84	105.65	-21.03	-31.19
			83	282.73	-124.64	85.21	-221.18	44.84	-253.97
28	Fondazio ne	13, 14	0	404.09	140.24	97.40	-307.44	44.87	285.22
			42	339.85	140.26	143.70	-444.49	-25.18	-58.36
			83	276.39	140.29	-338.13	-591.78	44.86	-238.68
29	Fondazio ne	14, 16	0	-271.74	-119.67	-64.24	501.70	14.44	44.94
			40	-216.30	-119.66	118.48	378.32	9.09	-41.25
			80	401.35	-119.66	251.27	284.76	27.41	99.79
30	Fondazio ne	14, 16	0	-199.18	-206.04	172.65	308.29	27.61	58.05
			40	172.56	-206.04	290.19	234.14	-18.63	51.51
			80	334.50	-206.04	392.07	213.23	-37.26	84.97
31	Fondazio ne	15, 17	0	-1013.61	359.02	2403.09	-1892.01	33.03	122.44
			33	-1008.67	359.00	1737.43	-2170.00	-16.32	66.42
			66	-1098.41	358.98	999.92	-2429.57	-17.34	19.75
32	Fondazio ne	15, 17	0	-326.53	223.34	948.90	-2578.74	-17.03	-36.07
			33	-293.46	223.32	89.74	-2802.21	-20.81	-25.59
			66	-427.78	223.31	-900.17	-3002.61	-21.77	-75.77
33	Fondazio ne	16, 18	0	-193.53	195.54	396.64	-492.64	-31.22	-96.84
			33	260.80	195.54	271.43	-471.28	-10.63	-59.87
			66	410.31	195.54	147.98	-460.25	13.18	-46.06
34	Fondazio ne	16, 18	0	-112.32	-195.52	138.03	-465.94	13.24	51.51
			33	157.65	-195.53	-32.74	-448.94	-6.81	48.64
			66	315.29	-195.54	-165.94	-492.20	-20.22	67.99
35	Fondazio ne	17, 19	0	-1110.01	515.08	-793.37	2118.46	-26.73	54.82
			33	-1118.34	515.06	-134.68	1935.40	-18.16	42.76
			66	-1205.87	515.05	533.87	1901.79	-7.43	-74.93
36	Fondazio ne	17, 19	0	-395.98	331.53	209.47	1815.24	-7.46	72.49

			33	-351.15	331.52	802.82	1899.66	-17.14	41.43
			66	-473.63	331.52	1427.91	2034.18	-25.80	-44.20
37	Fondazio ne	18, 20	0	-154.59	117.93	-124.90	330.82	-27.07	-64.73
			33	237.19	117.93	-59.01	252.29	-6.65	-64.41
			66	386.41	117.93	123.21	334.20	15.97	-65.37
38	Fondazio ne	18, 20	0	-108.31	-137.24	-63.79	281.08	16.01	62.04
			33	125.80	-137.26	176.06	446.25	-6.17	59.53
			66	296.76	-137.27	366.15	643.61	-23.72	59.97
39	Fondazio ne	19, 21	0	-1085.08	146.16	1506.79	-2212.74	-19.88	64.20
			33	-1080.88	146.15	799.22	-2165.73	-14.41	-37.38
			66	-1168.60	146.14	121.80	-2132.88	-8.28	-41.62
40	Fondazio ne	19, 21	0	-406.36	225.57	162.43	-2116.10	-8.13	53.46
			33	-343.39	225.57	-546.15	-2127.30	-12.68	-65.28
			66	-461.76	225.57	-1243.28	-2161.07	35.99	-91.25
41	Fondazio ne	20, 22	0	-131.09	160.15	374.09	766.59	-16.31	-65.58
			33	192.37	160.15	170.84	594.78	-6.62	-40.24
			66	347.62	160.15	-41.93	-475.67	13.90	-47.48
42	Fondazio ne	20, 22	0	-154.48	234.82	-53.07	-482.13	13.81	60.03
			33	163.42	234.82	-88.60	-430.33	8.76	73.79
			66	298.86	234.82	-202.37	-399.17	-35.42	95.32
43	Fondazio ne	21, 23	0	-1127.99	424.28	-1067.63	1898.40	48.09	126.31
			33	-1102.96	424.28	-479.75	1779.97	12.28	102.76
			66	-1188.69	424.28	131.84	1767.29	21.27	90.61
44	Fondazio ne	21, 23	0	-413.36	274.68	-139.14	1900.83	21.11	85.46
			33	-329.13	274.67	533.33	2056.27	-11.37	109.41
			66	-435.02	274.67	1234.05	2271.05	-51.07	133.98
45	Fondazio ne	22, 24	0	-130.62	185.46	-178.80	491.20	-48.72	-127.41
			33	157.30	185.46	-72.56	301.20	-10.73	-108.09
			66	304.36	185.46	-40.63	281.62	22.87	-94.73
46	Fondazio ne	22, 24	0	-204.19	-142.32	22.67	244.26	22.67	85.54
			33	161.91	-142.31	122.02	440.08	-7.75	104.78
			66	287.66	-142.31	319.71	687.34	-46.52	130.18
47	Fondazio ne	23, 25	0	-1217.60	230.00	1443.76	-2693.68	-40.52	-109.84
			33	-1159.01	230.00	583.77	-2572.61	-8.50	-86.44
			66	-1241.03	230.01	-245.10	-2510.72	16.64	-65.45
48	Fondazio ne	23, 25	0	-530.15	-210.27	-155.25	-2446.35	16.46	-107.73
			33	-415.13	-210.28	-939.72	-2432.76	42.12	-116.62
			66	-502.00	-210.28	-1735.22	-2490.89	75.48	-135.77
49	Fondazio ne	24, 26	0	-140.43	258.49	347.68	846.35	-35.72	-102.16
			33	175.03	258.49	125.50	-637.73	-6.16	-77.52
			66	289.98	258.50	-43.30	-531.58	15.65	-54.80
50	Fondazio ne	24, 26	0	-221.63	96.32	24.36	-546.83	15.42	45.73
			33	167.69	96.33	-138.66	-474.83	-10.68	54.20
			66	305.62	96.33	-251.07	-487.82	-24.02	73.63
51	Fondazio ne	25, 26	0	-135.36	-146.44	245.18	-590.49	165.20	454.46
			49	-124.24	-146.43	175.25	444.48	70.41	240.93
			97	-115.70	-146.43	286.73	489.52	-89.29	-439.16
52	Fondazio ne	25, 26	0	-107.44	-64.72	93.44	-277.49	-88.47	301.29
			49	-86.87	-64.71	128.61	-46.29	-47.93	-58.85
			97	-82.92	-64.71	121.80	148.70	50.51	-354.33
53	Fondazio ne	25, 26	0	-152.09	-76.32	-110.68	-136.40	50.83	325.04
			49	-124.88	-76.32	-147.71	-21.87	-28.94	6.50
			97	-109.62	-76.32	-130.31	90.93	49.20	-320.21
54	Fondazio ne	25, 26	0	-172.16	-36.13	-145.31	-16.83	49.46	320.78
			49	-147.14	-36.13	-144.42	38.45	-29.28	-1.19

			97	-125.62	-36.13	-123.96	65.90	49.40	-319.90
55	Fondazio ne	25, 26	0	-177.96	-12.87	-117.29	38.63	49.63	318.59
			49	-154.68	-12.87	-101.80	45.84	-28.38	-1.28
			97	-135.21	-12.87	-86.34	39.84	49.65	-317.94
56	Fondazio ne	25, 26	0	-167.72	-3.96	-75.56	53.06	49.88	316.97
			49	-145.64	-3.96	-58.79	38.60	-27.72	-1.42
			97	-129.62	-3.96	-50.31	20.50	49.60	-315.68
57	Fondazio ne	25, 26	0	-147.88	4.89	-41.60	49.49	49.82	315.10
			49	-126.79	4.89	-28.26	29.46	-27.28	-1.45
			97	-118.96	4.89	-24.66	-15.45	49.57	-313.91
58	Fondazio ne	25, 26	0	-122.21	4.03	-19.00	38.56	49.78	313.48
			49	-102.09	4.03	-10.59	21.52	-26.89	1.18
			97	-103.72	4.02	-9.78	-14.71	49.36	-312.08
59	Fondazio ne	25, 26	0	-93.33	2.64	-6.83	26.96	49.58	311.51
			49	-74.52	2.64	-5.04	17.99	-26.55	3.57
			97	-91.03	2.64	-4.51	-16.72	50.03	-310.79
60	Fondazio ne	25, 26	0	-71.19	0.97	2.83	17.88	49.93	310.46
			49	-59.17	0.97	3.10	-17.72	-26.12	-3.23
			97	-88.36	0.97	3.06	22.08	49.21	-308.68
61	Fondazio ne	25, 26	0	-38.61	1.07	4.33	-12.39	49.43	308.60
			49	-47.13	1.07	5.37	19.49	-25.88	2.28
			97	-83.31	1.07	8.91	29.79	49.21	-307.53
62	Fondazio ne	25, 26	0	-13.02	1.55	11.92	-10.78	49.40	307.23
			49	-46.13	1.55	13.54	23.82	-25.65	1.09
			97	-84.89	1.55	20.86	39.28	49.03	-305.96
63	Fondazio ne	25, 26	0	16.19	2.69	25.90	-13.99	49.20	305.80
			49	51.03	2.69	30.09	31.01	-25.47	-1.28
			97	90.13	2.69	41.35	48.48	48.86	-304.57
64	Fondazio ne	25, 26	0	38.85	4.51	48.73	23.75	49.01	304.34
			49	68.07	4.51	57.16	39.74	-25.29	0.97
			97	98.94	4.51	70.42	51.84	48.72	-303.27
65	Fondazio ne	25, 26	0	57.75	6.92	78.62	40.63	48.86	302.95
			49	86.44	6.92	91.66	45.14	-25.05	0.98
			97	116.88	6.92	102.85	38.45	48.61	-301.98
66	Fondazio ne	25, 26	0	71.45	9.34	111.49	69.39	48.75	301.95
			49	99.95	9.34	132.07	44.65	-24.97	0.97
			97	130.17	9.34	134.60	-36.25	48.20	-300.36
67	Fondazio ne	25, 26	0	77.25	11.54	135.35	95.43	48.34	300.67
			49	105.62	11.55	155.58	-21.07	-25.02	-1.93
			97	135.78	11.55	127.63	-144.72	47.74	-299.08
68	Fondazio ne	25, 26	0	69.99	-12.24	-101.68	145.35	47.88	297.34
			49	-97.96	-12.25	123.67	-36.58	-24.31	9.87
			97	128.07	-12.25	-58.55	-263.75	54.06	-300.04
69	Fondazio ne	25, 26	0	61.46	-19.13	-63.17	-240.56	54.10	335.82
			49	-88.14	-19.13	-115.88	-203.24	-41.71	61.03
			97	-118.23	-19.13	-274.18	-516.50	28.05	-269.95
70	Fondazio ne	25, 28	0	-1545.18	453.06	-1425.04	1696.26	-111.15	-164.15
			43	-1500.85	453.06	-755.87	1612.01	-43.63	-162.97
			85	-1611.92	453.06	-65.02	1748.93	27.56	-162.40
71	Fondazio ne	25, 28	0	-729.04	431.66	-249.13	1859.61	27.60	62.57
			43	-622.49	431.67	583.54	2136.16	7.00	60.47
			85	-755.96	431.68	1565.31	2591.64	-26.05	79.77
72	Fondazio ne	26, 27	0	-119.61	-70.70	-198.82	484.83	15.67	61.75
			33	125.40	-70.70	-113.59	283.63	10.87	35.57
			66	296.52	-70.70	13.81	301.82	12.23	19.55

73	Fondazio ne	26, 27	0	-237.89	128.25	38.42	277.53	12.00	29.03
			33	149.83	128.24	128.02	470.25	4.90	-45.76
			66	304.46	128.24	337.25	714.70	18.18	-63.19
74	Fondazio ne	27, 29	0	-139.36	112.70	416.72	946.96	19.72	68.85
			33	146.57	112.69	160.42	703.47	1.99	52.03
			66	281.79	112.68	-50.20	-506.82	-14.74	36.82
75	Fondazio ne	27, 29	0	-243.59	200.54	59.30	553.51	-14.50	-50.55
			33	176.45	200.53	-135.96	-488.80	6.85	-61.69
			66	283.62	200.52	-266.11	-486.53	26.14	-75.71
76	Fondazio ne	28, 30	0	-2069.61	71.25	1835.83	-2385.35	-32.46	-77.00
			37	-2042.79	71.24	1031.61	-1966.80	-11.80	-67.82
			73	-2133.05	71.23	382.61	-1687.72	30.23	-60.10
77	Fondazio ne	28, 30	0	-1489.11	-460.57	492.70	-1180.76	30.00	89.05
			37	-1443.12	-460.55	139.62	-948.59	-19.20	95.37
			73	-1539.27	-460.54	-212.30	-790.14	52.30	100.61
78	Fondazio ne	29, 31	0	-155.02	-124.70	-211.21	479.60	30.14	82.99
			33	121.04	-124.70	-111.70	303.58	8.10	69.87
			66	255.89	-124.70	22.85	303.21	-16.10	57.98
79	Fondazio ne	29, 31	0	-233.59	134.24	57.22	260.24	-15.84	47.89
			33	119.16	134.23	139.52	367.35	3.53	58.76
			66	271.62	134.23	303.49	542.61	22.85	-68.81
80	Fondazio ne	30, 32	0	-1218.94	-334.29	368.93	-1017.02	49.47	-98.76
			34	-1159.91	-334.28	65.70	-720.59	16.26	-95.77
			69	-1251.97	-334.28	-175.30	-568.85	16.30	-93.85
81	Fondazio ne	30, 32	0	-881.55	-306.23	-50.65	-637.48	16.11	35.88
			34	-816.24	-306.22	-216.52	-555.33	-6.44	36.94
			69	-915.34	-306.22	-398.55	-554.23	-13.01	43.98
82	Fondazio ne	31, 33	0	-177.31	88.64	401.95	851.78	15.48	49.66
			33	140.34	88.64	164.73	681.20	3.12	40.65
			66	288.95	88.63	-47.31	-557.65	11.50	35.65
83	Fondazio ne	31, 33	0	-217.02	-157.91	-70.26	582.28	11.23	-44.87
			33	102.93	-157.91	-132.19	-512.25	-5.65	-47.10
			66	266.94	-157.90	-268.90	-472.44	21.52	-49.41
84	Fondazio ne	32, 34	0	-751.30	-111.93	158.84	-576.04	-15.78	39.41
			35	-649.50	-111.92	-87.98	-404.16	-2.72	-36.51
			69	-752.12	-111.92	-171.16	-322.92	9.42	-33.71
85	Fondazio ne	32, 34	0	-473.61	-211.43	-84.85	-338.84	9.41	42.91
			35	-347.40	-211.43	-177.64	-312.83	-9.57	46.63
			69	-468.40	-211.44	-279.52	-326.88	-26.36	-51.48
86	Fondazio ne	33, 35	0	-200.73	129.51	-206.45	397.34	-20.47	-41.91
			33	136.70	129.51	-103.34	330.82	7.11	-39.77
			66	286.54	129.51	-16.13	288.28	10.06	-37.81
87	Fondazio ne	33, 35	0	-204.18	207.70	46.38	287.15	9.79	51.87
			33	42.47	207.70	105.22	292.80	7.56	47.40
			66	211.53	207.70	230.30	319.80	-22.27	42.28
88	Fondazio ne	34, 36	0	-384.48	223.30	188.73	-366.10	-22.36	43.58
			35	-234.95	223.30	55.65	-310.78	-8.38	-37.67
			69	-359.99	223.30	-71.07	-314.62	3.79	-30.78
89	Fondazio ne	34, 36	0	-194.15	-259.12	-49.03	-321.72	3.99	-17.32
			35	53.11	-259.12	-84.11	-356.53	5.79	-12.95
			69	271.43	-259.13	-221.24	-406.71	8.54	19.06
90	Fondazio ne	35, 37	0	-233.21	59.76	303.01	627.02	-26.33	-54.18
			33	-158.24	59.76	138.17	585.45	7.79	-60.24
			66	287.11	59.76	-59.16	563.72	13.54	-67.15
91	Fondazio	35, 37	0	-224.27	-126.16	-36.32	563.67	13.33	61.96

	ne								
			33	-39.70	-126.16	-157.39	562.51	-6.47	54.13
			66	185.03	-126.16	-330.84	580.86	-22.35	45.69
92	Fondazio ne	36, 38	0	-289.88	-105.42	185.81	-214.36	14.41	32.75
			35	164.71	-105.42	140.28	-255.57	6.28	33.10
			69	345.11	-105.43	88.58	-312.47	-9.45	39.59
93	Fondazio ne	36, 38	0	530.37	-185.06	126.01	-328.31	-9.52	-41.17
			35	424.06	-185.07	-51.37	-403.58	6.38	-41.21
			69	573.46	-185.08	-184.38	-497.59	19.11	-41.86
94	Fondazio ne	37, 39	0	-273.48	152.15	-253.77	374.16	-15.49	-26.37
			33	-165.72	152.15	-122.19	367.83	9.37	-24.65
			66	309.30	152.15	-46.46	371.28	9.19	-36.61
95	Fondazio ne	37, 39	0	-261.40	-154.35	-33.13	356.93	9.56	49.31
			33	-105.81	-154.35	138.92	358.82	-8.70	55.46
			66	198.36	-154.35	278.34	361.23	-27.46	63.00
96	Fondazio ne	38, 40	0	666.00	-209.93	266.90	-272.42	15.60	32.82
			34	563.76	-209.94	170.64	-351.89	7.46	31.16
			69	681.42	-209.95	51.60	-479.30	-8.37	29.75
97	Fondazio ne	38, 40	0	960.36	-279.71	153.43	-493.32	-8.64	-36.09
			34	870.59	-279.72	-47.09	-647.30	-10.54	-52.87
			69	951.01	-279.73	-294.25	-842.65	29.56	-70.88
98	Fondazio ne	39, 41	0	-307.74	-191.06	322.38	501.30	-28.48	-80.53
			33	-212.87	-191.06	197.21	461.43	-5.02	-69.04
			66	-345.46	-191.06	84.00	494.86	18.80	-59.27
99	Fondazio ne	39, 41	0	-294.46	-93.95	130.51	372.39	19.17	64.68
			33	-173.64	-93.95	-42.62	489.56	-9.36	79.46
			66	242.97	-93.95	191.52	641.43	-37.47	98.91
100	Fondazio ne	40, 42	0	1161.12	-304.15	141.70	-433.35	-33.87	-85.28
			35	1076.86	-304.17	-43.97	-629.32	-10.17	-66.06
			69	1129.26	-304.19	-269.28	-852.77	13.49	-45.85
101	Fondazio ne	40, 42	0	1591.10	-220.24	-171.26	-1117.67	13.69	-31.94
			35	1505.64	-220.27	-555.70	-1413.37	12.62	-47.02
			69	1535.93	-220.30	-1108.61	-1759.20	26.09	-64.58
102	Fondazio ne	41, 44	0	-305.16	291.82	-85.46	-358.07	-33.09	-83.32
			33	-154.45	291.82	70.82	358.08	-9.68	-65.83
			66	162.61	291.83	158.07	455.60	-12.47	-47.52
103	Fondazio ne	41, 44	0	-312.91	162.25	-105.62	496.37	-12.72	22.71
			33	-132.23	162.26	-228.81	610.69	11.49	35.46
			66	93.60	162.26	447.27	828.89	-14.10	-56.73
104	Fondazio ne	42, 43	0	1844.90	205.57	-761.89	-749.92	19.03	-135.50
			23	1788.36	205.55	-933.68	-918.07	49.04	-137.08
			46	1768.44	205.55	-1158.12	-1081.87	80.65	-142.35
105	Fondazio ne	43, 44	0	-124.18	-283.60	-189.68	961.00	139.08	417.87
			49	-91.46	-283.58	226.36	533.80	62.09	191.71
			97	-72.54	-283.57	398.62	329.39	-76.70	-402.03
106	Fondazio ne	43, 44	0	110.76	-174.46	298.64	218.47	-76.23	303.65
			49	87.14	-174.45	339.93	-43.32	-40.10	-50.07
			97	72.31	-174.44	291.78	-179.57	53.30	-348.62
107	Fondazio ne	43, 44	0	147.86	-84.76	238.25	61.06	53.58	325.11
			49	127.94	-84.75	235.65	-56.40	-26.17	9.25
			97	113.67	-84.75	196.41	-113.21	51.10	-319.22
108	Fondazio ne	43, 44	0	182.45	-42.70	174.76	-39.30	51.45	321.23
			49	164.42	-42.70	157.17	-53.80	-27.06	1.14
			97	150.35	-42.70	132.57	-59.55	50.70	-319.05
109	Fondazio ne	43, 44	0	178.75	-20.21	109.25	-56.09	50.98	319.08

			49	161.42	-20.21	87.62	-47.08	-26.89	2.13
			97	150.35	-20.21	72.24	-32.62	50.54	-317.44
110	Fondazio ne	43, 44	0	166.90	-7.89	57.17	-52.41	50.80	317.30
			49	150.17	-7.89	40.67	-32.87	-26.70	1.72
			97	143.90	-7.89	33.86	-18.29	50.30	-315.59
111	Fondazio ne	43, 44	0	149.28	-1.92	25.71	-40.85	50.54	315.50
			49	133.03	-1.92	17.38	-22.13	-26.53	1.58
			97	132.34	-1.92	15.92	-17.19	50.09	-313.91
112	Fondazio ne	43, 44	0	128.37	-1.64	13.54	-28.73	50.31	313.80
			49	112.56	-1.64	-11.29	-17.81	-26.36	1.61
			97	118.16	-1.64	-10.05	16.75	49.86	-312.24
113	Fondazio ne	43, 44	0	106.29	-2.69	-8.19	-19.68	50.08	312.14
			49	94.47	-2.69	-7.16	-16.85	-26.18	1.12
			97	108.95	-2.69	-5.70	17.00	49.63	-310.66
114	Fondazio ne	43, 44	0	82.96	-2.95	-4.09	-15.69	49.86	310.35
			49	78.25	-2.95	-3.79	-16.53	-25.91	2.20
			97	100.31	-2.95	-3.50	-19.72	49.67	-309.32
115	Fondazio ne	43, 44	0	64.76	-2.66	-4.46	-13.54	49.92	309.26
			49	69.63	-2.66	-4.69	-17.17	-25.70	1.08
			97	98.63	-2.66	-7.25	-25.42	49.24	-307.37
116	Fondazio ne	43, 44	0	51.88	1.65	-9.83	-12.78	49.43	307.34
			49	68.51	1.65	-11.03	-20.82	-25.56	-1.48
			97	99.28	1.65	-16.94	-32.33	49.20	-306.32
117	Fondazio ne	43, 44	0	47.10	3.15	-22.14	-14.18	49.39	306.05
			49	-72.10	3.15	-25.56	-26.11	-25.33	1.07
			97	-103.76	3.15	-34.74	-37.51	49.00	-304.74
118	Fondazio ne	43, 44	0	47.83	7.52	-42.42	-22.62	49.18	304.63
			49	-79.36	7.52	-49.40	-31.54	-25.17	1.06
			97	-111.30	7.52	-59.61	-35.45	48.80	-303.35
119	Fondazio ne	43, 44	0	56.76	15.34	-68.84	-38.23	48.98	303.31
			49	-88.28	15.34	-80.46	-33.92	-25.04	0.94
			97	-120.27	15.34	-87.12	-20.04	48.53	-301.92
120	Fondazio ne	43, 44	0	64.56	26.24	-95.40	-62.17	48.72	302.04
			49	-96.07	26.24	-111.82	-28.12	-25.00	1.04
			97	-128.10	26.25	-106.20	-31.02	48.19	-300.50
121	Fondazio ne	43, 44	0	68.18	36.17	-106.15	-86.39	48.38	300.96
			49	-99.59	36.17	-121.98	-10.06	-25.08	-2.54
			97	-131.73	36.17	-86.87	124.10	47.59	-298.96
122	Fondazio ne	43, 44	0	75.61	52.09	-72.67	-131.86	47.78	296.38
			49	-89.32	52.10	-91.75	-35.90	-23.90	-12.96
			97	-121.52	52.10	-33.74	247.44	55.08	-301.13
123	Fondazio ne	43, 44	0	75.93	-65.93	61.23	-135.05	55.12	337.20
			49	78.49	-65.94	-79.95	249.19	-41.20	61.29
			97	-94.85	-65.94	242.30	559.52	24.99	-266.09
124	Fondazio ne	43, 45	0	979.91	506.94	-1021.42	2275.17	-60.78	-116.58
			33	897.08	506.92	-340.24	1970.49	-24.37	-109.20
			66	959.37	506.91	295.24	1794.46	13.62	-110.43
125	Fondazio ne	43, 45	0	1646.27	298.03	-111.59	2329.83	13.79	50.84
			33	1564.68	298.02	661.65	2261.32	12.26	37.92
			66	1576.07	298.02	1403.75	2243.09	-12.68	51.93
126	Fondazio ne	44, 46	0	-292.67	-65.47	363.04	674.69	24.59	55.93
			33	-120.13	-65.46	161.62	462.64	11.05	-57.55
			66	218.61	-65.46	47.47	333.58	14.03	59.97
127	Fondazio ne	44, 46	0	-296.74	229.58	83.66	449.96	14.10	73.76
			33	-132.63	229.58	96.93	413.62	11.07	78.89

			66	110.90	229.58	249.21	614.08	-38.06	-85.20
128	Fondazio ne	45, 47	0	662.35	-105.73	1591.34	-2276.57	-10.02	61.71
			33	565.09	-105.73	842.92	-2273.53	10.75	-34.46
			66	651.13	-105.73	111.83	-2346.39	14.30	-28.03
129	Fondazio ne	45, 47	0	1396.70	-198.57	208.97	-2430.12	14.61	33.56
			33	1314.38	-198.57	-621.09	-2541.28	7.73	63.94
			66	1357.17	-198.58	-1465.13	-2672.54	-28.47	-96.06
130	Fondazio ne	46, 48	0	-325.53	191.40	297.08	-614.14	32.56	97.00
			33	-177.14	191.40	124.84	-613.81	7.69	74.68
			66	-242.63	191.40	-62.98	-637.83	-19.30	-68.04
131	Fondazio ne	46, 48	0	-302.46	199.56	56.77	-540.86	-19.57	-61.12
			33	-173.63	199.55	-159.75	603.63	5.69	-91.97
			66	110.70	199.54	-359.26	766.99	41.31	-124.37
132	Fondazio ne	47, 49	0	603.00	389.73	-1226.29	2293.00	-39.45	-119.47
			33	499.58	389.73	-534.88	2054.71	8.51	-86.15
			66	569.41	389.73	128.36	1919.18	19.94	-57.93
133	Fondazio ne	47, 49	0	1306.95	395.51	-127.35	1856.18	20.30	59.13
			33	1222.60	395.50	494.99	1880.69	11.02	85.23
			66	1251.11	395.49	1118.77	1982.63	-41.15	120.52
134	Fondazio ne	48, 50	0	-308.79	-167.13	338.84	-657.04	49.13	139.96
			33	-175.61	-167.13	145.69	430.46	8.79	106.41
			66	-259.44	-167.14	43.29	292.27	-20.97	75.24
135	Fondazio ne	48, 50	0	-297.18	150.51	37.30	341.03	-21.22	-63.54
			33	-138.47	150.50	104.49	358.43	-8.77	-93.83
			66	118.67	150.50	230.81	563.19	44.14	-131.01
136	Fondazio ne	49, 51	0	548.38	185.59	1270.50	-2136.18	-32.25	-92.02
			33	438.65	185.60	578.78	-2116.11	10.56	-62.37
			66	498.26	185.61	-144.04	-2137.40	-12.00	36.56
137	Fondazio ne	49, 51	0	1245.60	156.63	-91.87	-2165.16	-12.34	-43.41
			33	1160.79	156.63	-792.06	-2210.26	14.55	-38.12
			66	1165.83	156.63	-1554.32	-2369.05	17.34	-67.26
138	Fondazio ne	50, 52	0	-323.27	-204.02	281.66	-425.77	31.55	94.80
			33	-196.23	-204.02	171.80	-420.61	-6.92	60.78
			66	-271.28	-204.02	63.84	471.87	-8.56	33.76
139	Fondazio ne	50, 52	0	-305.09	133.83	95.10	-325.69	-8.67	-32.04
			33	-119.17	133.84	-64.83	466.69	9.31	-20.55
			66	159.58	133.84	200.40	621.88	5.44	-57.26
140	Fondazio ne	51, 53	0	523.61	382.90	-1456.51	2101.68	24.37	60.68
			33	410.02	382.90	-805.81	1929.40	17.92	-48.11
			66	456.27	382.91	-203.38	1810.00	17.79	69.04
141	Fondazio ne	51, 53	0	1223.53	535.61	-538.23	1904.85	17.98	-65.07
			33	1138.41	535.61	155.35	1933.08	15.78	60.27
			66	1134.67	535.62	813.92	2142.64	-31.39	-84.18
142	Fondazio ne	52, 54	0	-313.11	-49.73	184.25	425.15	7.08	30.02
			33	-112.49	-49.72	75.43	274.96	5.72	23.46
			66	88.71	-49.71	-92.04	-294.33	-9.66	67.23
143	Fondazio ne	52, 54	0	-364.37	116.84	84.11	-278.18	-9.43	-60.83
			33	-180.34	116.83	-133.18	305.94	4.50	-16.09
			66	110.37	116.82	-226.75	415.12	5.23	-36.05
144	Fondazio ne	53, 55	0	463.27	225.93	890.64	-2962.96	28.11	115.15
			33	342.20	225.94	-95.61	-2709.64	20.46	63.15
			66	391.55	225.96	-910.78	-2453.64	28.79	-44.67
145	Fondazio ne	53, 55	0	1111.82	401.03	-1007.13	-2462.35	29.03	-44.68
			33	1024.84	401.05	-1760.36	-2203.75	16.60	-100.17
			66	1037.05	401.07	-2427.03	-1902.88	40.91	-157.62

146	Fondazio ne	54, 56	0	-434.42	-136.40	201.41	437.61	8.98	-56.37
			33	-255.65	-136.39	-176.28	337.51	4.81	27.92
			66	152.47	-136.38	-259.46	-361.86	-14.29	59.64
147	Fondazio ne	54, 56	0	-528.65	189.77	-256.38	-436.21	-14.23	-36.75
			33	-357.63	189.77	-372.33	-456.50	10.49	58.94
			66	267.10	189.77	-493.61	-466.30	32.22	92.81
148	Fondazio ne	55, 57	0	454.85	1116.90	-2524.84	1390.59	49.59	-167.11
			40	303.62	1116.94	-1927.64	1788.70	29.41	-97.13
			80	406.20	1117.00	-1094.22	2528.90	42.25	-45.06
149	Fondazio ne	55, 57	0	1094.19	1170.21	-1791.67	2415.03	42.58	-82.27
			40	993.38	1170.28	-657.60	3420.11	53.34	-26.13
			80	1075.41	1170.37	951.23	4757.54	57.37	-76.32
150	Fondazio ne	56, 70	0	-380.24	-223.75	-489.82	310.82	38.37	-90.44
			40	-191.66	-223.74	-351.16	279.18	16.61	-50.40
			80	192.74	-223.74	-199.05	343.36	-27.52	60.51
151	Fondazio ne	56, 70	0	-460.60	-139.47	-290.65	266.37	-27.32	97.14
			40	258.14	-139.47	-136.32	380.11	-7.24	-42.35
			80	256.50	-139.47	81.39	554.08	-12.08	52.04
152	Fondazio ne	57, 58	0	-276.09	-1163.82	1206.92	-4404.60	128.83	419.01
			42	-305.15	-1163.69	-386.49	-2988.11	-38.25	226.32
			83	-341.49	-1163.57	-1342.49	-1899.20	-82.26	-377.46
153	Fondazio ne	57, 58	0	-601.22	-827.52	-660.47	-1574.24	-81.82	276.59
			42	-567.32	-827.42	-1100.71	-719.09	-68.65	35.34
			83	-584.52	-827.34	-1217.10	-218.27	-69.20	-284.78
154	Fondazio ne	58, 59	0	-1013.15	-743.65	-677.83	-957.63	-64.12	225.68
			35	-986.34	-743.58	-907.75	-459.90	-40.09	-44.07
			69	-962.84	-743.53	-992.20	-100.66	-39.50	-238.05
155	Fondazio ne	58, 59	0	-1008.03	66.97	-725.82	-101.94	-39.31	215.35
			35	-981.75	67.02	-692.24	292.97	-16.28	-54.79
			69	-956.03	67.07	-563.90	566.34	34.56	-259.38
156	Fondazio ne	59, 60	0	-998.43	-549.19	-400.58	-394.60	36.43	271.56
			35	-972.76	-549.14	-475.16	-157.36	-19.28	79.90
			69	-947.64	-549.10	-479.92	139.61	-48.89	-230.39
157	Fondazio ne	59, 60	0	-993.34	251.10	-384.99	272.61	-48.73	236.46
			35	-968.34	251.14	-271.49	452.39	-17.59	-81.82
			69	-943.88	251.19	-105.19	620.38	38.92	-272.48
158	Fondazio ne	60, 61	0	-994.19	-487.32	-54.57	-344.89	37.97	269.36
			35	-966.77	-487.27	-123.05	-211.81	-17.33	71.10
			69	-939.84	-487.23	-158.26	113.02	-46.71	-233.75
159	Fondazio ne	60, 61	0	-1010.28	250.33	-85.63	220.84	-46.54	221.55
			35	-983.59	250.36	43.93	356.35	-19.38	-68.91
			69	-957.39	250.40	152.97	491.21	34.24	-262.75
160	Fondazio ne	61, 62	0	-918.59	-495.15	213.23	-542.64	44.57	273.94
			35	-892.68	-495.11	44.49	-412.47	-14.57	82.52
			69	-867.26	-495.08	-97.72	-292.87	-42.07	-225.95
161	Fondazio ne	61, 62	0	-921.20	223.46	23.24	-230.74	-41.93	228.68
			35	-895.89	223.49	-75.22	-132.07	-13.19	-73.86
			69	-871.05	223.52	117.94	153.52	42.94	-269.74
162	Fondazio ne	62, 63	0	-837.88	-391.77	84.31	-285.96	29.38	244.15
			35	-813.27	-391.74	-96.62	-183.04	-17.74	55.05
			69	-791.03	-391.71	-113.47	-91.21	-39.09	-215.73
163	Fondazio ne	62, 63	0	-824.18	189.79	-67.28	-64.25	-38.99	226.19
			35	-800.13	189.81	-53.61	118.16	-15.05	-68.53
			69	-777.14	189.84	40.62	208.86	35.07	-247.99
164	Fondazio	63, 64	0	-802.56	-381.48	92.19	-311.03	31.15	242.22

	ne								
			35	-779.10	-381.45	-28.95	-223.20	-15.23	49.26
			69	-756.08	-381.43	-53.25	-148.89	37.27	-222.50
165	Fondazio ne	63, 64	0	-783.16	225.17	23.08	124.47	37.18	221.09
			35	-760.32	225.19	15.73	182.10	-13.72	-54.65
			69	-737.91	225.22	78.15	265.95	34.34	-245.35
166	Fondazio ne	64, 65	0	-762.38	-315.43	94.84	-229.82	32.31	241.78
			35	-740.10	-315.40	37.85	-148.80	-14.07	58.78
			69	-718.25	-315.38	42.65	-78.29	35.05	-215.49
167	Fondazio ne	64, 65	0	-747.91	125.25	53.59	-81.24	34.98	213.49
			35	-726.13	125.27	82.59	160.86	-14.06	-50.91
			69	-704.77	125.29	140.21	244.21	31.88	-240.07
168	Fondazio ne	65, 66	0	-650.52	-341.83	194.44	-426.63	34.91	240.49
			35	-630.52	-341.81	50.80	-346.85	-11.24	41.15
			69	-613.11	-341.79	-67.96	-275.10	33.50	-216.30
169	Fondazio ne	65, 66	0	-646.13	106.43	16.49	-256.80	33.46	220.93
			35	-624.63	106.44	-78.53	-195.56	-12.32	-55.20
			69	-604.17	106.46	-148.76	-144.68	38.40	-235.81
170	Fondazio ne	66, 67	0	-553.62	-283.82	114.45	-231.83	26.54	220.49
			35	-535.20	-283.80	-107.75	192.80	-14.85	30.35
			69	-518.76	-283.79	-95.37	-163.79	31.46	-211.25
171	Fondazio ne	66, 67	0	-547.87	121.16	-75.97	-133.06	31.43	213.35
			35	-527.98	121.18	-57.29	-139.35	-11.76	-25.83
			69	-508.49	121.19	-54.62	-180.63	29.79	-226.82
172	Fondazio ne	67, 68	0	-530.72	-180.83	26.58	-183.91	27.81	223.38
			35	-511.24	-180.82	-63.20	-154.15	-12.51	29.39
			69	-492.16	-180.81	-94.82	-133.04	29.60	-207.22
173	Fondazio ne	67, 68	0	-524.91	-121.37	-72.09	-99.88	29.59	205.04
			35	-499.04	-121.39	-71.71	-112.36	-10.89	-33.70
			69	-480.32	-121.40	-78.77	-169.57	31.05	-226.34
174	Fondazio ne	68, 69	0	-536.35	-138.47	-74.22	-139.88	28.78	220.50
			35	-481.26	-138.46	-75.50	-123.35	-11.45	19.67
			69	-462.44	-138.46	-96.29	-172.32	29.07	-204.87
175	Fondazio ne	68, 69	0	-576.00	139.13	-87.99	-147.65	29.07	198.64
			35	-519.69	139.14	-72.46	224.50	-10.05	-30.44
			69	-464.58	139.16	-103.26	330.66	34.93	-225.04
176	Fondazio ne	69, 70	0	-407.18	-156.32	-51.90	-135.42	41.49	247.10
			42	-343.05	-156.34	-72.94	-135.89	-21.35	-26.04
			83	-280.51	-156.36	-93.68	253.21	49.46	-259.76
177	Fondazio ne	69, 70	0	-391.60	177.25	-105.12	341.22	49.50	298.05
			42	-326.03	177.28	-136.83	474.52	-26.56	-66.40
			83	-261.23	177.30	341.46	682.49	37.17	-229.81
178	Primo Impalcato	1, 2	0	-843.63	102.20	-833.63	594.05	-985.44	-1233.06
			83	-843.63	102.20	-341.43	594.05	-367.10	-1233.06
			166	-843.63	102.20	165.01	594.05	1111.34	-1233.06
179	Primo Impalcato	1, 15	0	-2625.66	-4.64	6710.37	-5302.92	898.22	674.29
			80	-2625.66	-4.64	2494.57	-5302.92	561.15	674.29
			159	-2625.66	-4.64	-1739.44	-5302.92	383.23	674.29
180	Primo Impalcato	2, 3	0	-1181.44	-6.74	163.70	-87.02	1063.72	996.51
			69	-1181.44	-6.74	105.00	-87.02	463.33	996.51
			138	-1181.44	-6.74	58.76	-87.02	792.67	996.51
181	Primo Impalcato	3, 4	0	-960.70	-5.38	59.35	-29.25	780.30	339.35
			69	-960.70	-5.38	39.18	-29.25	-547.99	339.35
			138	-960.70	-5.38	19.39	-29.25	-318.40	339.35
182	Primo Impalcato	4, 5	0	-758.41	-11.52	26.66	-8.07	-328.60	-779.99

			69	-758.41	-11.52	23.15	-8.07	255.64	-779.99
			138	-758.41	-11.52	21.88	-8.07	754.12	-779.99
183	Primo Impalcato	5, 6	0	-713.83	-14.10	33.59	-78.50	753.57	704.30
			69	-713.83	-14.10	-21.56	-78.50	270.11	704.30
			138	-713.83	-14.10	-75.11	-78.50	-220.52	704.30
184	Primo Impalcato	6, 7	0	-600.74	-14.35	-65.34	98.24	-218.00	289.51
			69	-600.74	-14.35	5.31	98.24	-417.70	289.51
			138	-600.74	-14.35	70.25	98.24	-617.45	289.51
185	Primo Impalcato	7, 8	0	-487.22	-20.63	80.22	-62.31	-619.48	-892.76
			69	-487.22	-20.63	37.24	-62.31	19.90	-892.76
			138	-487.22	-20.63	-5.86	-62.31	628.72	-892.76
186	Primo Impalcato	8, 9	0	-665.76	-20.23	9.26	-62.09	620.33	301.64
			69	-665.76	-20.23	-35.03	-62.09	412.25	301.64
			138	-665.76	-20.23	-77.86	-62.09	204.29	301.64
187	Primo Impalcato	9, 10	0	-566.75	-22.61	-67.87	99.88	209.05	681.85
			69	-566.75	-22.61	1.52	99.88	-274.00	681.85
			138	-566.75	-22.61	69.97	99.88	-737.98	681.85
188	Primo Impalcato	10, 11	0	-469.78	-24.18	79.98	-76.75	-742.96	-750.05
			69	-469.78	-24.18	27.04	-76.75	-228.79	-750.05
			138	-469.78	-24.18	-25.97	-76.75	296.42	-750.05
189	Primo Impalcato	11, 12	0	-691.54	-20.24	-13.34	22.15	288.88	-192.32
			69	-691.54	-20.24	3.89	22.15	418.83	-192.32
			138	-691.54	-20.24	18.25	22.15	548.86	-192.32
190	Primo Impalcato	12, 13	0	922.30	-20.77	30.85	-55.55	558.10	879.34
			69	922.30	-20.77	-10.64	-55.55	54.45	879.34
			138	922.30	-20.77	-46.13	-55.55	-655.45	879.34
191	Primo Impalcato	13, 14	0	706.81	-20.60	-37.71	-92.77	-648.49	-497.03
			83	706.81	-20.60	-102.60	-92.77	-286.78	-497.03
			166	706.81	-20.60	-175.19	-92.77	-191.58	-497.03
192	Primo Impalcato	14, 16	0	-556.49	-7.84	659.87	-520.11	-145.78	-195.20
			80	-556.49	-7.84	247.39	-520.11	257.62	-195.20
			159	-556.49	-7.84	-183.05	-520.11	381.08	-195.20
193	Primo Impalcato	15, 17	0	-1765.86	-7.54	1612.86	-3009.72	388.50	507.98
			66	-1765.86	-7.54	-380.39	-3009.72	-104.96	507.98
			132	-1765.86	-7.54	-2360.88	-3009.72	-308.69	507.98
194	Primo Impalcato	16, 18	0	-515.93	-6.63	213.99	-373.31	372.06	457.43
			66	-515.93	-6.63	-45.30	-373.31	-74.14	457.43
			132	-515.93	-6.63	-279.39	-373.31	-245.41	457.43
195	Primo Impalcato	17, 19	0	-1109.06	-1.12	907.39	-1194.04	-291.22	-82.56
			66	-1109.06	-1.12	136.02	-1194.04	-283.91	-82.56
			132	-1109.06	-1.12	-669.21	-1194.04	-279.05	-82.56
196	Primo Impalcato	18, 20	0	-562.30	-0.64	126.19	-175.58	-244.04	43.91
			66	-562.30	-0.64	36.98	-175.58	-252.57	43.91
			132	-562.30	-0.64	-108.93	-175.58	-261.23	43.91
197	Primo Impalcato	19, 21	0	-492.26	5.95	2676.01	-3989.49	-299.77	-481.54
			66	-492.26	5.95	48.04	-3989.49	-41.35	-481.54
			132	-492.26	5.95	-2592.41	-3989.49	336.45	-481.54
198	Primo Impalcato	20, 22	0	-498.84	5.99	322.67	-475.88	-263.78	-439.93
			66	-498.84	5.99	-18.13	-475.88	-29.73	-439.93
			132	-498.84	5.99	-305.59	-475.88	317.02	-439.93
199	Primo Impalcato	21, 23	0	975.69	1.96	755.68	-1110.29	319.47	110.35
			66	975.69	1.96	34.89	-1110.29	253.05	110.35
			132	975.69	1.96	-709.96	-1110.29	188.18	110.35
200	Primo Impalcato	22, 24	0	-585.07	-1.99	90.81	-147.79	320.13	110.11
			66	-585.07	-1.99	-18.33	-147.79	248.83	110.11

			132	-585.07	-1.99	-104.59	-147.79	178.90	110.11
201	Primo Impalcato	23, 25	0	1732.46	-4.97	2654.03	-4053.06	204.93	440.55
			66	1732.46	-4.97	-24.97	-4053.06	-94.73	440.55
			132	1732.46	-4.97	-2696.02	-4053.06	-384.94	440.55
202	Primo Impalcato	24, 26	0	-552.14	-6.15	321.73	-486.30	186.10	408.69
			66	-552.14	-6.15	10.68	-486.30	-87.77	408.69
			132	-552.14	-6.15	-320.20	-486.30	-357.19	408.69
203	Primo Impalcato	25, 28	0	3467.10	-2.81	667.84	-897.36	-370.90	-237.01
			85	3467.10	-2.81	-111.30	-897.36	-169.47	-237.01
			170	3467.10	-2.81	-858.11	-897.36	-35.25	-237.01
204	Primo Impalcato	26, 27	0	-645.07	5.85	112.14	-166.69	-367.99	-270.04
			66	-645.07	5.85	16.86	-166.69	-189.95	-270.04
			132	-645.07	5.85	-112.86	-166.69	41.57	-270.04
205	Primo Impalcato	27, 29	0	-652.14	4.52	313.13	-480.86	45.42	-262.78
			66	-652.14	4.52	10.90	-480.86	148.72	-262.78
			132	-652.14	4.52	-321.70	-480.86	321.97	-262.78
206	Primo Impalcato	28, 30	0	5200.74	3.14	2436.15	-2970.91	-34.73	-237.80
			73	5200.74	3.14	271.41	-2970.91	189.59	-237.80
			146	5200.74	3.14	-1904.91	-2970.91	362.88	-237.80
207	Primo Impalcato	29, 31	0	-725.71	-5.81	95.16	-158.24	339.28	359.21
			66	-725.71	-5.81	18.99	-158.24	102.23	359.21
			132	-725.71	-5.81	-122.61	-158.24	-134.94	359.21
208	Primo Impalcato	30, 32	0	3948.24	-2.97	1466.56	-2271.54	371.98	372.90
			69	3948.24	-2.97	-107.11	-2271.54	116.57	372.90
			137	3948.24	-2.97	-1656.36	-2271.54	-140.44	372.90
209	Primo Impalcato	31, 33	0	-774.31	3.01	327.64	-483.23	-116.27	123.93
			66	-774.31	3.01	-12.61	-483.23	-197.48	123.93
			132	-774.31	3.01	-318.94	-483.23	-278.73	123.93
210	Primo Impalcato	32, 34	0	2693.74	-1.20	1670.52	-2416.16	-121.69	142.37
			69	2693.74	-1.20	-7.80	-2416.16	-216.67	142.37
			138	2693.74	-1.20	-1663.79	-2416.16	-311.78	142.37
211	Primo Impalcato	33, 35	0	-846.42	6.50	108.76	-169.61	-301.53	-419.44
			66	-846.42	6.50	-7.84	-169.61	-45.63	-419.44
			132	-846.42	6.50	-115.15	-169.61	255.36	-419.44
212	Primo Impalcato	34, 36	0	1436.52	5.02	1665.97	-2414.41	-321.70	-399.94
			69	1436.52	5.02	-5.58	-2414.41	-45.83	-399.94
			138	1436.52	5.02	-1665.92	-2414.41	230.27	-399.94
213	Primo Impalcato	35, 37	0	-877.28	2.39	328.05	-492.20	233.07	-47.23
			66	-877.28	2.39	-9.39	-492.20	231.62	-47.23
			132	-877.28	2.39	-321.96	-492.20	234.93	-47.23
214	Primo Impalcato	36, 38	0	216.98	1.29	1668.02	-2424.46	217.11	-35.03
			69	216.98	1.29	-12.44	-2424.46	214.20	-35.03
			138	216.98	1.29	-1677.75	-2424.46	213.95	-35.03
215	Primo Impalcato	37, 39	0	-965.32	-5.78	104.83	-158.26	261.45	432.83
			66	-965.32	-5.78	-21.54	-158.26	47.74	432.83
			132	-965.32	-5.78	-106.12	-158.26	-315.04	432.83
216	Primo Impalcato	38, 40	0	-1265.61	-4.86	1657.35	-2307.81	227.28	403.07
			69	-1265.61	-4.86	79.51	-2307.81	50.39	403.07
			137	-1265.61	-4.86	-1504.43	-2307.81	-325.41	403.07
217	Primo Impalcato	39, 41	0	-1002.24	4.55	299.71	-365.21	-285.51	-123.38
			66	-1002.24	4.55	69.97	-365.21	-214.31	-123.38
			132	-1002.24	4.55	-184.80	-365.21	-144.89	-123.38
218	Primo Impalcato	40, 42	0	-2538.33	2.18	1850.13	-2846.44	-313.86	166.52
			69	-2538.33	2.18	-121.01	-2846.44	-202.04	166.52
			138	-2538.33	2.18	-2078.78	-2846.44	-109.35	166.52

219	Primo Impalcato	41, 44	0	-665.05	-6.83	185.59	-360.60	-161.35	-225.16
			66	-665.05	-6.83	-85.54	-360.60	35.02	-225.16
			132	-665.05	-6.83	-305.47	-360.60	136.59	-225.16
220	Primo Impalcato	42, 43	0	-3777.48	20.27	1241.76	-7135.50	-115.64	-566.54
			23	-3777.48	20.27	-406.61	-7135.50	-59.77	-566.54
			46	-3777.48	20.27	-2043.20	-7135.50	153.66	-566.54
221	Primo Impalcato	43, 45	0	-2844.44	2.30	1266.02	-1619.21	-136.33	-127.86
			66	-2844.44	2.30	206.87	-1619.21	210.90	-127.86
			132	-2844.44	2.30	-871.44	-1619.21	287.10	-127.86
222	Primo Impalcato	44, 46	0	-697.48	4.10	114.95	-151.53	-118.44	-144.94
			66	-697.48	4.10	23.24	-151.53	202.19	-144.94
			132	-697.48	4.10	-86.43	-151.53	289.16	-144.94
223	Primo Impalcato	45, 47	0	-1988.33	6.04	2495.95	-3889.00	300.47	376.24
			66	-1988.33	6.04	-72.20	-3889.00	54.84	376.24
			132	-1988.33	6.04	-2637.52	-3889.00	-202.64	376.24
224	Primo Impalcato	46, 48	0	-746.04	6.35	351.61	-542.79	316.98	399.70
			66	-746.04	6.35	18.20	-542.79	-84.56	399.70
			132	-746.04	6.35	-364.98	-542.79	-222.01	399.70
225	Primo Impalcato	47, 49	0	-1177.31	3.16	723.13	-1102.02	-190.49	-70.39
			66	-1177.31	3.16	-18.67	-1102.02	-213.97	-70.39
			132	-1177.31	3.16	-731.58	-1102.02	-239.70	-70.39
226	Primo Impalcato	48, 50	0	-747.87	4.07	101.72	-139.49	-196.74	-75.17
			66	-747.87	4.07	28.53	-139.49	-215.83	-75.17
			132	-747.87	4.07	-84.12	-139.49	-240.19	-75.17
227	Primo Impalcato	49, 51	0	334.78	6.63	2613.22	-4018.32	-255.40	-402.96
			66	334.78	6.63	-50.10	-4018.32	-37.65	-402.96
			132	334.78	6.63	-2692.45	-4018.32	277.27	-402.96
228	Primo Impalcato	50, 52	0	804.81	6.64	301.59	-402.03	-265.41	-397.11
			66	804.81	6.64	36.70	-402.03	32.81	-397.11
			132	804.81	6.64	-233.99	-402.03	263.83	-397.11
229	Primo Impalcato	51, 53	0	778.79	1.81	643.70	-1162.43	260.59	-105.77
			66	778.79	1.81	-143.01	-1162.43	239.90	-105.77
			132	778.79	1.81	-891.02	-1162.43	223.36	-105.77
230	Primo Impalcato	52, 54	0	-408.42	2.60	145.53	-215.27	239.73	-62.29
			66	-408.42	2.60	31.50	-215.27	208.17	-62.29
			132	-408.42	2.60	-146.42	-215.27	176.90	-62.29
231	Primo Impalcato	53, 55	0	1469.30	-5.11	2391.19	-3043.24	238.39	413.74
			66	1469.30	-5.11	385.30	-3043.24	133.35	413.74
			132	1469.30	-5.11	-1627.57	-3043.24	-343.40	413.74
232	Primo Impalcato	54, 56	0	-250.43	-4.86	183.92	-321.60	198.18	400.77
			66	-250.43	-4.86	37.99	-321.60	-90.57	400.77
			132	-250.43	-4.86	-247.22	-321.60	-352.68	400.77
233	Primo Impalcato	55, 57	0	2415.02	-3.21	1717.88	-5289.16	-341.45	682.23
			80	2415.02	-3.21	-2500.06	-5289.16	-510.09	682.23
			159	2415.02	-3.21	-6703.83	-5289.16	-889.56	682.23
234	Primo Impalcato	56, 70	0	-313.68	-6.19	164.72	-434.01	-326.42	-191.08
			80	-313.68	-6.19	-194.97	-434.01	-209.98	-191.08
			159	-313.68	-6.19	-532.23	-434.01	146.95	-191.08
235	Primo Impalcato	57, 58	0	791.95	102.13	848.45	-599.17	-942.87	-1103.23
			83	791.95	102.13	350.53	-599.17	-304.22	-1103.23
			166	791.95	102.13	-162.81	-599.17	941.42	-1103.23
236	Primo Impalcato	58, 59	0	1135.16	-5.24	-161.44	86.59	888.89	740.67
			69	1135.16	-5.24	-103.67	86.59	451.08	740.67
			138	1135.16	-5.24	-66.44	86.59	643.45	740.67
237	Primo	59, 60	0	967.34	-6.44	-65.95	24.25	633.10	299.70

	Impalcato								
			69	967.34	-6.44	-49.42	24.25	427.55	299.70
			138	967.34	-6.44	-33.49	24.25	-224.31	299.70
238	Primo Impalcato	60, 61	0	807.49	-12.99	-41.39	76.36	-231.04	-552.54
			69	807.49	-12.99	15.31	76.36	198.81	-552.54
			138	807.49	-12.99	66.85	76.36	539.66	-552.54
239	Primo Impalcato	61, 62	0	733.80	-12.71	57.98	-85.95	541.91	517.07
			69	733.80	-12.71	-8.85	-85.95	187.91	517.07
			138	733.80	-12.71	-61.01	-85.95	197.73	517.07
240	Primo Impalcato	62, 63	0	648.45	-16.05	-69.98	66.40	196.10	191.70
			69	648.45	-16.05	-25.98	66.40	-308.54	191.70
			138	648.45	-16.05	22.00	66.40	-440.29	191.70
241	Primo Impalcato	63, 64	0	507.68	-19.03	12.45	-18.77	-444.22	-650.05
			69	507.68	-19.03	-5.58	-18.77	-43.27	-650.05
			138	507.68	-19.03	-13.90	-18.77	470.85	-650.05
242	Primo Impalcato	64, 65	0	567.10	-21.40	-24.25	65.48	463.76	-242.74
			69	567.10	-21.40	22.80	65.48	303.05	-242.74
			138	567.10	-21.40	67.87	65.48	143.08	-242.74
243	Primo Impalcato	65, 66	0	489.04	-21.87	59.09	-85.46	145.99	490.10
			69	489.04	-21.87	1.91	-85.46	-204.66	490.10
			138	489.04	-21.87	-59.42	-85.46	-535.83	490.10
244	Primo Impalcato	66, 67	0	425.04	-25.56	-68.08	65.77	-538.92	-552.23
			69	425.04	-25.56	-22.89	65.77	-161.90	-552.23
			138	425.04	-25.56	23.59	65.77	-237.00	-552.23
245	Primo Impalcato	67, 68	0	583.46	-20.68	13.18	-18.70	-235.47	-125.21
			69	583.46	-20.68	5.65	-18.70	307.21	-125.21
			138	583.46	-20.68	-15.76	-18.70	390.47	-125.21
246	Primo Impalcato	68, 69	0	772.12	-19.66	-26.46	46.36	397.95	638.50
			69	772.12	-19.66	7.15	46.36	72.36	638.50
			138	772.12	-19.66	38.14	46.36	-485.88	638.50
247	Primo Impalcato	69, 70	0	-574.08	-20.04	30.12	94.48	-478.67	-393.44
			83	-574.08	-20.04	91.43	94.48	-230.93	-393.44
			166	-574.08	-20.04	165.55	94.48	-199.14	-393.44
248	Primo Impalcato	1	0	8509.78	-79.51	257.25	-28.04	-516.44	213.57
			188	8509.78	-79.51	237.82	-28.04	-136.46	213.57
			376	8509.78	-79.51	273.53	-28.04	-333.06	213.57
249	Primo Impalcato	2	0	-555.48	-14.49	1852.31	-332.62	10.64	5.94
			188	-555.48	-14.49	1312.06	-332.62	-0.86	5.94
			376	-555.48	-14.49	1148.39	-332.62	-11.71	5.94
250	Primo Impalcato	3	0	362.11	-5.83	848.67	424.69	-10.33	5.43
			188	362.11	-5.83	1314.14	424.69	-0.32	5.43
			376	362.11	-5.83	2089.07	424.69	-10.10	5.43
251	Primo Impalcato	4	0	346.92	-6.69	613.78	428.43	-13.42	-7.22
			188	346.92	-6.69	1281.55	428.43	0.16	-7.22
			376	346.92	-6.69	2080.44	428.43	13.74	-7.22
252	Primo Impalcato	5	0	197.14	2.73	854.87	479.63	-14.37	-7.70
			188	197.14	2.73	1237.69	479.63	-0.11	-7.70
			376	197.14	2.73	2103.40	479.63	14.59	-7.70
253	Primo Impalcato	6	0	199.89	7.46	676.92	313.57	-13.34	-7.15
			188	199.89	7.46	1153.63	313.57	0.22	-7.15
			376	199.89	7.46	1722.77	313.57	13.54	-7.15
254	Primo Impalcato	7	0	-166.75	5.76	746.94	342.09	-13.44	-7.19
			188	-166.75	5.76	1056.05	342.09	0.18	-7.19
			376	-166.75	5.76	1673.90	342.09	13.58	-7.19
255	Primo Impalcato	8	0	-23.80	6.05	735.13	347.71	-14.57	-7.71

			188	-23.80	6.05	936.58	347.71	-0.26	-7.71
			376	-23.80	6.05	1552.51	347.71	14.43	-7.71
256	Primo Impalcato	9	0	165.96	8.44	529.00	235.35	-12.97	-6.91
			188	165.96	8.44	788.01	235.35	0.14	-6.91
			376	165.96	8.44	1215.58	235.35	13.02	-6.91
257	Primo Impalcato	10	0	-136.55	4.33	589.93	285.75	-12.79	-6.82
			188	-136.55	4.33	645.29	285.75	0.13	-6.82
			376	-136.55	4.33	1139.44	285.75	12.87	-6.82
258	Primo Impalcato	11	0	-27.35	8.26	367.66	179.37	-13.77	-7.34
			188	-27.35	8.26	485.36	179.37	-0.14	-7.34
			376	-27.35	8.26	805.13	179.37	13.82	-7.34
259	Primo Impalcato	12	0	-120.36	6.64	404.72	215.11	-13.68	-7.32
			188	-120.36	6.64	345.10	215.11	-0.09	-7.32
			376	-120.36	6.64	711.15	215.11	13.85	-7.32
260	Primo Impalcato	13	0	182.57	5.53	369.81	-168.22	-13.41	-7.15
			188	182.57	5.53	219.49	-168.22	0.25	-7.15
			376	182.57	5.53	495.02	-168.22	13.48	-7.15
261	Primo Impalcato	14	0	1291.51	41.00	62.52	-41.12	449.22	235.23
			188	1291.51	41.00	21.60	-41.12	42.67	235.23
			376	1291.51	41.00	94.19	-41.12	-436.44	235.23
262	Primo Impalcato	15	0	-1753.07	9.15	-370.21	193.53	854.71	433.98
			188	-1753.07	9.15	-6.80	193.53	104.87	433.98
			376	-1753.07	9.15	357.46	193.53	-807.26	433.98
263	Primo Impalcato	16	0	359.32	5.06	-62.04	32.69	-500.67	-344.52
			188	359.32	5.06	-1.22	32.69	186.64	-344.52
			376	359.32	5.06	60.87	32.69	811.19	-344.52
264	Primo Impalcato	17	0	2859.68	9.83	-327.19	181.04	303.11	139.66
			188	2859.68	9.83	13.31	181.04	159.34	139.66
			376	2859.68	9.83	353.53	181.04	349.15	139.66
265	Primo Impalcato	18	0	826.90	7.46	-59.80	32.61	-451.93	-302.74
			188	826.90	7.46	1.73	32.61	209.55	-302.74
			376	826.90	7.46	62.82	32.61	712.09	-302.74
266	Primo Impalcato	19	0	-2162.39	-8.31	-350.40	192.11	230.53	-186.22
			188	-2162.39	-8.31	10.90	192.11	201.13	-186.22
			376	-2162.39	-8.31	371.93	192.11	513.28	-186.22
267	Primo Impalcato	20	0	1185.03	-8.56	-65.67	35.40	-368.41	-264.05
			188	1185.03	-8.56	1.11	35.40	206.38	-264.05
			376	1185.03	-8.56	67.44	35.40	650.91	-264.05
268	Primo Impalcato	21	0	1617.70	-7.18	-358.53	196.11	686.77	440.57
			188	1617.70	-7.18	10.33	196.11	186.21	440.57
			376	1617.70	-7.18	378.84	196.11	-984.77	440.57
269	Primo Impalcato	22	0	1217.47	-6.89	-67.78	36.47	-791.35	-493.91
			188	1217.47	-6.89	1.04	36.47	186.11	-493.91
			376	1217.47	-6.89	69.35	36.47	1080.50	-493.91
270	Primo Impalcato	23	0	-3039.91	9.59	-364.00	198.64	-797.89	-473.16
			188	-3039.91	9.59	9.70	198.64	178.41	-473.16
			376	-3039.91	9.59	382.90	198.64	998.22	-473.16
271	Primo Impalcato	24	0	1604.38	9.49	-69.88	37.52	-841.06	-492.46
			188	1604.38	9.49	0.95	37.52	155.29	-492.46
			376	1604.38	9.49	71.20	37.52	1024.18	-492.46
272	Primo Impalcato	25	0	-1854.81	3.64	-360.57	196.59	-733.32	429.02
			188	-1854.81	3.64	9.36	196.59	179.13	429.02
			376	-1854.81	3.64	378.59	196.59	-897.66	429.02
273	Primo Impalcato	26	0	1381.27	-4.29	-70.09	37.63	483.50	271.75
			188	1381.27	-4.29	0.90	37.63	184.98	271.75

			376	1381.27	-4.29	71.40	37.63	563.62	271.75
274	Primo Impalcato	27	0	1530.09	-8.79	-70.15	37.67	415.99	253.04
			188	1530.09	-8.79	1.08	37.67	112.49	253.04
			376	1530.09	-8.79	71.50	37.67	547.25	253.04
275	Primo Impalcato	28	0	-3142.09	-10.25	-344.05	190.19	-608.54	-339.77
			188	-3142.09	-10.25	13.67	190.19	232.01	-339.77
			376	-3142.09	-10.25	371.07	190.19	770.14	-339.77
276	Primo Impalcato	29	0	1135.01	-2.02	-71.48	38.38	582.68	354.95
			188	1135.01	-2.02	1.05	38.38	135.44	354.95
			376	1135.01	-2.02	72.82	38.38	-757.40	354.95
277	Primo Impalcato	30	0	-1383.90	-3.27	-402.43	217.94	-1032.43	-578.64
			188	-1383.90	-3.27	7.66	217.94	222.51	-578.64
			376	-1383.90	-3.27	417.04	217.94	-1247.21	-578.64
278	Primo Impalcato	31	0	1171.95	7.88	-72.85	39.10	-495.19	264.76
			188	1171.95	7.88	1.25	39.10	82.72	264.76
			376	1171.95	7.88	74.19	39.10	-514.56	264.76
279	Primo Impalcato	32	0	-829.60	10.73	-390.25	213.26	-257.59	-154.80
			188	-829.60	10.73	10.90	213.26	200.63	-154.80
			376	-829.60	10.73	411.60	213.26	453.33	-154.80
280	Primo Impalcato	33	0	616.88	5.42	-75.36	40.24	-430.20	-248.25
			188	616.88	5.42	1.29	40.24	100.76	-248.25
			376	616.88	5.42	75.96	40.24	-509.70	-248.25
281	Primo Impalcato	34	0	-402.54	-3.78	-392.07	213.81	-462.44	-270.17
			188	-402.54	-3.78	10.09	213.81	187.41	-270.17
			376	-402.54	-3.78	411.87	213.81	660.57	-270.17
282	Primo Impalcato	35	0	576.09	-7.08	-77.02	41.08	-559.15	-311.24
			188	576.09	-7.08	1.35	41.08	44.82	-311.24
			376	576.09	-7.08	77.46	41.08	626.14	-311.24
283	Primo Impalcato	36	0	264.25	-6.81	-393.49	214.52	248.35	134.30
			188	264.25	-6.81	9.98	214.52	171.52	134.30
			376	264.25	-6.81	413.12	214.52	402.52	134.30
284	Primo Impalcato	37	0	428.56	8.94	-78.06	41.49	-411.61	-240.00
			188	428.56	8.94	1.42	41.49	-40.33	-240.00
			376	428.56	8.94	77.95	41.49	490.92	-240.00
285	Primo Impalcato	38	0	556.63	7.79	-394.28	215.24	420.56	211.98
			188	556.63	7.79	10.58	215.24	150.94	211.98
			376	556.63	7.79	415.02	215.24	-480.82	211.98
286	Primo Impalcato	39	0	684.00	7.06	-75.60	40.57	-613.19	-342.66
			188	684.00	7.06	1.69	40.57	-70.99	-342.66
			376	684.00	7.06	77.34	40.57	676.37	-342.66
287	Primo Impalcato	40	0	951.54	4.58	-405.35	219.78	686.22	364.10
			188	951.54	4.58	8.08	219.78	119.22	364.10
			376	951.54	4.58	421.04	219.78	776.28	364.10
288	Primo Impalcato	41	0	-1207.92	-6.65	-86.07	45.45	-791.47	-403.22
			188	-1207.92	-6.65	1.11	45.45	-46.36	-403.22
			376	-1207.92	-6.65	84.84	45.45	725.74	-403.22
289	Primo Impalcato	42	0	2639.56	-8.85	-380.50	207.70	158.23	131.02
			188	2639.56	-8.85	10.37	207.70	110.31	131.02
			376	2639.56	-8.85	400.45	207.70	352.58	131.02
290	Primo Impalcato	43	0	1045.72	-8.62	-354.10	195.20	-339.20	-134.14
			188	1045.72	-8.62	13.20	195.20	115.77	-134.14
			376	1045.72	-8.62	379.87	195.20	245.88	-134.14
291	Primo Impalcato	44	0	-1561.11	-7.48	-74.25	40.24	-520.94	-247.92
			188	-1561.11	-7.48	1.47	40.24	97.47	-247.92
			376	-1561.11	-7.48	77.07	40.24	504.48	-247.92

292	Primo Impalcato	45	0	-1646.93	5.59	-381.10	206.29	-180.49	-122.80
			188	-1646.93	5.59	6.99	206.29	103.76	-122.80
			376	-1646.93	5.59	394.56	206.29	310.11	-122.80
293	Primo Impalcato	46	0	-1395.72	-5.42	-77.72	41.61	746.94	412.16
			188	-1395.72	-5.42	0.86	41.61	122.67	412.16
			376	-1395.72	-5.42	78.74	41.61	822.92	412.16
294	Primo Impalcato	47	0	2841.68	8.46	-369.84	202.03	-743.49	-398.72
			188	2841.68	8.46	10.19	202.03	23.33	-398.72
			376	2841.68	8.46	389.81	202.03	755.79	-398.72
295	Primo Impalcato	48	0	-1619.92	8.85	-77.31	41.49	1001.06	538.40
			188	-1619.92	8.85	0.84	41.49	61.77	538.40
			376	-1619.92	8.85	78.70	41.49	-1024.10	538.40
296	Primo Impalcato	49	0	-1736.77	-7.88	-366.43	200.30	-705.50	-388.04
			188	-1736.77	-7.88	10.28	200.30	-45.30	-388.04
			376	-1736.77	-7.88	386.71	200.30	754.00	-388.04
297	Primo Impalcato	50	0	-1260.17	8.19	-74.96	40.60	721.04	402.20
			188	-1260.17	8.19	1.46	40.60	-48.68	402.20
			376	-1260.17	8.19	77.71	40.60	-797.91	402.20
298	Primo Impalcato	51	0	2395.87	-7.09	-358.66	196.54	-300.60	-195.05
			188	2395.87	-7.09	10.93	196.54	-110.86	-195.05
			376	2395.87	-7.09	380.33	196.54	-440.59	-195.05
299	Primo Impalcato	52	0	-1067.49	-7.39	-82.42	44.22	101.98	85.42
			188	-1067.49	-7.39	0.87	44.22	-118.79	85.42
			376	-1067.49	-7.39	83.84	44.22	-232.44	85.42
300	Primo Impalcato	53	0	-3183.56	8.15	-335.67	185.58	595.62	289.60
			188	-3183.56	8.15	13.27	185.58	-104.58	289.60
			376	-3183.56	8.15	362.11	185.58	-567.88	289.60
301	Primo Impalcato	54	0	-828.15	7.20	-79.58	42.78	79.51	89.71
			188	-828.15	7.20	1.19	42.78	-144.32	89.71
			376	-828.15	7.20	81.26	42.78	-294.00	89.71
302	Primo Impalcato	55	0	2070.15	7.57	-378.89	198.06	-1108.65	576.98
			188	2070.15	7.57	-6.96	198.06	-70.26	576.98
			376	2070.15	7.57	365.82	198.06	-1061.57	576.98
303	Primo Impalcato	56	0	-524.26	2.76	-70.44	37.63	-510.68	-334.49
			188	-524.26	2.76	-0.97	37.63	-149.28	-334.49
			376	-524.26	2.76	71.03	37.63	758.07	-334.49
304	Primo Impalcato	57	0	-8384.45	-76.10	237.60	-35.29	432.94	168.17
			188	-8384.45	-76.10	237.87	-35.29	134.78	168.17
			376	-8384.45	-76.10	292.99	-35.29	-254.26	168.17
305	Primo Impalcato	58	0	656.08	-13.92	1830.40	-302.97	-8.63	-4.93
			188	656.08	-13.92	1312.38	-302.97	0.82	-4.93
			376	656.08	-13.92	1114.01	-302.97	9.92	-4.93
306	Primo Impalcato	59	0	-416.83	-4.69	783.27	390.77	7.58	3.99
			188	-416.83	-4.69	1330.45	390.77	0.33	3.99
			376	-416.83	-4.69	2043.85	390.77	-7.44	3.99
307	Primo Impalcato	60	0	-384.18	-5.10	601.33	421.33	11.36	6.10
			188	-384.18	-5.10	1290.25	421.33	0.12	6.10
			376	-384.18	-5.10	2075.15	421.33	-11.59	6.10
308	Primo Impalcato	61	0	-267.31	2.84	751.92	426.77	11.37	6.15
			188	-267.31	2.84	1248.03	426.77	-0.23	6.15
			376	-267.31	2.84	2026.36	426.77	-11.76	6.15
309	Primo Impalcato	62	0	119.70	6.08	767.36	348.94	11.68	6.28
			188	119.70	6.08	1165.11	348.94	-0.18	6.28
			376	119.70	6.08	1775.23	348.94	-11.93	6.28
310	Primo	63	0	60.74	5.28	738.22	330.18	13.02	6.93

	Impalcato								
			188	60.74	5.28	1056.21	330.18	0.10	6.93
			376	60.74	5.28	1643.57	330.18	-13.05	6.93
311	Primo Impalcato	64	0	-41.85	5.30	712.92	325.51	13.08	6.94
			188	-41.85	5.30	930.42	325.51	0.11	6.94
			376	-41.85	5.30	1502.69	325.51	-13.01	6.94
312	Primo Impalcato	65	0	-138.68	7.09	571.34	252.64	11.59	6.18
			188	-138.68	7.09	788.24	252.64	-0.11	6.18
			376	-138.68	7.09	1219.63	252.64	-11.67	6.18
313	Primo Impalcato	66	0	109.60	4.39	499.64	232.16	11.45	6.12
			188	109.60	4.39	643.76	232.16	-0.11	6.12
			376	109.60	4.39	1046.19	232.16	-11.56	6.12
314	Primo Impalcato	67	0	41.66	6.86	332.31	158.50	12.55	6.68
			188	41.66	6.86	480.33	158.50	0.12	6.68
			376	41.66	6.86	763.76	158.50	-12.57	6.68
315	Primo Impalcato	68	0	124.68	5.77	315.00	163.72	12.44	6.66
			188	124.68	5.77	344.90	163.72	-0.09	6.66
			376	124.68	5.77	618.77	163.72	-12.62	6.66
316	Primo Impalcato	69	0	179.78	4.67	374.59	-160.78	12.32	6.57
			188	179.78	4.67	210.53	-160.78	-0.22	6.57
			376	179.78	4.67	458.33	-160.78	-12.39	6.57
317	Primo Impalcato	70	0	-1223.70	34.64	91.82	-56.87	-401.94	-213.07
			188	-1223.70	34.64	18.01	-56.87	-36.10	-213.07
			376	-1223.70	34.64	122.71	-56.87	400.26	-213.07
318	Fondazio ne	1, 71	0	5461.00	-0.26	0.00	0.00	-15.48	-8.96
			102	5461.00	-0.26	0.00	0.00	-6.33	-8.96
			204	5461.00	-0.26	0.00	0.00	2.85	-8.96
319	Fondazio ne	1, 92	0	-533.85	-0.44	0.00	0.00	-14.21	23.57
			103	-533.85	-0.44	0.00	0.00	-22.58	23.57
			206	-533.85	-0.44	0.00	0.00	-39.86	23.57
320	Primo Impalcato	92, 2	0	1161.54	-1.94	0.00	0.00	17.22	25.58
			103	1161.54	-1.94	0.00	0.00	-13.22	25.58
			206	1161.54	-1.94	0.00	0.00	-38.29	25.58
321	Fondazio ne	6, 89	0	664.86	1.45	0.00	0.00	-51.31	-19.20
			100	664.86	1.45	0.00	0.00	-33.53	-19.20
			200	664.86	1.45	0.00	0.00	-26.92	-19.20
322	Primo Impalcato	89, 7	0	-665.55	-1.12	0.00	0.00	-40.22	-20.87
			100	-665.55	-1.12	0.00	0.00	-34.41	-20.87
			200	-665.55	-1.12	0.00	0.00	-51.11	-20.87
323	Fondazio ne	9, 90	0	631.93	1.44	0.00	0.00	-31.92	-10.04
			100	631.93	1.44	0.00	0.00	-21.91	-10.04
			200	631.93	1.44	0.00	0.00	-12.66	-10.04
324	Primo Impalcato	90, 10	0	-639.04	-0.96	0.00	0.00	-34.79	-17.83
			100	-639.04	-0.96	0.00	0.00	-22.45	-17.83
			200	-639.04	-0.96	0.00	0.00	-34.60	-17.83
325	Fondazio ne	13, 91	0	789.90	0.75	0.00	0.00	23.64	20.79
			103	789.90	0.75	0.00	0.00	-2.87	20.79
			206	789.90	0.75	0.00	0.00	19.20	20.79
326	Primo Impalcato	88, 14	0	970.07	0.25	0.00	0.00	-3.46	-4.94
			102	970.07	0.25	0.00	0.00	-4.79	-4.94
			204	970.07	0.25	0.00	0.00	9.63	-4.94
327	Primo Impalcato	91, 14	0	-717.40	0.33	0.00	0.00	-10.27	-10.70
			103	-717.40	0.33	0.00	0.00	-7.56	-10.70
			206	-717.40	0.33	0.00	0.00	14.06	-10.70
328	Primo Impalcato	71, 15	0	-4880.63	-0.53	0.00	0.00	14.50	15.48

			102	-4880.63	-0.53	0.00	0.00	-1.42	15.48
			204	-4880.63	-0.53	0.00	0.00	-17.11	15.48
329	Fondazio ne	16, 88	0	-908.95	0.49	0.00	0.00	-15.34	-13.82
			102	-908.95	0.49	0.00	0.00	-1.42	-13.82
			204	-908.95	0.49	0.00	0.00	12.90	-13.82
330	Fondazio ne	17, 72	0	6000.56	0.09	0.00	0.00	-10.52	-7.44
			100	6000.56	0.09	0.00	0.00	3.42	-7.44
			199	6000.56	0.09	0.00	0.00	6.73	-7.44
331	Primo Impalcato	87, 18	0	1027.56	-0.16	0.00	0.00	6.48	8.40
			100	1027.56	-0.16	0.00	0.00	-4.07	8.40
			199	1027.56	-0.16	0.00	0.00	-12.16	8.40
332	Primo Impalcato	72, 19	0	-5907.68	0.15	0.00	0.00	5.54	8.57
			100	-5907.68	0.15	0.00	0.00	3.65	8.57
			199	-5907.68	0.15	0.00	0.00	12.02	8.57
333	Fondazio ne	20, 87	0	-1080.53	0.12	0.00	0.00	-11.84	-7.90
			100	-1080.53	0.12	0.00	0.00	-4.24	-7.90
			199	-1080.53	0.12	0.00	0.00	6.05	-7.90
334	Fondazio ne	21, 73	0	6152.51	0.30	0.00	0.00	-19.83	-15.07
			100	6152.51	0.30	0.00	0.00	5.27	-15.07
			199	6152.51	0.30	0.00	0.00	11.52	-15.07
335	Primo Impalcato	86, 22	0	1103.84	-0.30	0.00	0.00	12.44	16.57
			100	1103.84	-0.30	0.00	0.00	-5.62	16.57
			199	1103.84	-0.30	0.00	0.00	-21.86	16.57
336	Primo Impalcato	73, 23	0	-6386.96	0.18	0.00	0.00	-10.23	13.50
			100	-6386.96	0.18	0.00	0.00	6.15	13.50
			199	-6386.96	0.18	0.00	0.00	-19.11	13.50
337	Fondazio ne	24, 86	0	-1204.72	-0.20	0.00	0.00	-20.59	-14.52
			100	-1204.72	-0.20	0.00	0.00	-6.30	-14.52
			199	-1204.72	-0.20	0.00	0.00	-10.56	-14.52
338	Fondazio ne	25, 74	0	7370.88	-0.38	0.00	0.00	14.64	11.77
			103	7370.88	-0.38	0.00	0.00	2.92	11.77
			206	7370.88	-0.38	0.00	0.00	-11.64	11.77
339	Primo Impalcato	85, 26	0	1149.91	0.25	0.00	0.00	-5.62	-5.90
			100	1149.91	0.25	0.00	0.00	-2.68	-5.90
			199	1149.91	0.25	0.00	0.00	7.50	-5.90
340	Fondazio ne	27, 85	0	-1264.81	-0.16	0.00	0.00	5.93	3.59
			100	-1264.81	-0.16	0.00	0.00	-3.08	3.59
			199	-1264.81	-0.16	0.00	0.00	-3.42	3.59
341	Primo Impalcato	74, 28	0	-7458.80	0.33	0.00	0.00	-4.84	-7.55
			103	-7458.80	0.33	0.00	0.00	5.02	-7.55
			206	-7458.80	0.33	0.00	0.00	12.63	-7.55
342	Primo Impalcato	84, 29	0	1140.03	0.39	0.00	0.00	-8.49	-9.98
			100	1140.03	0.39	0.00	0.00	-2.90	-9.98
			199	1140.03	0.39	0.00	0.00	12.78	-9.98
343	Fondazio ne	31, 84	0	-1301.44	0.24	0.00	0.00	10.69	-6.96
			100	-1301.44	0.24	0.00	0.00	3.83	-6.96
			199	-1301.44	0.24	0.00	0.00	-4.36	-6.96
344	Primo Impalcato	83, 33	0	1182.54	-0.38	0.00	0.00	-6.35	6.57
			100	1182.54	-0.38	0.00	0.00	-2.73	6.57
			199	1182.54	-0.38	0.00	0.00	-6.83	6.57
345	Fondazio ne	35, 83	0	-1302.16	-0.43	0.00	0.00	-6.84	-7.14
			100	-1302.16	-0.43	0.00	0.00	2.36	-7.14
			199	-1302.16	-0.43	0.00	0.00	7.90	-7.14
346	Primo Impalcato	82, 37	0	1312.46	0.49	0.00	0.00	6.75	4.52
			100	1312.46	0.49	0.00	0.00	-2.92	4.52

			199	1312.46	0.49	0.00	0.00	-4.72	4.52
347	Fondazio ne	39, 82	0	-1223.71	0.52	0.00	0.00	-9.16	-8.67
			100	-1223.71	0.52	0.00	0.00	-1.93	-8.67
			199	-1223.71	0.52	0.00	0.00	8.15	-8.67
348	Primo Impalcato	78, 43	0	6403.74	0.18	0.00	0.00	1.97	1.92
			100	6403.74	0.18	0.00	0.00	-1.69	1.92
			199	6403.74	0.18	0.00	0.00	3.30	1.92
349	Primo Impalcato	81, 44	0	1355.44	-0.06	0.00	0.00	5.15	8.38
			100	1355.44	-0.06	0.00	0.00	-4.33	8.38
			199	1355.44	-0.06	0.00	0.00	-12.61	8.38
350	Fondazio ne	45, 78	0	-6543.49	0.18	0.00	0.00	6.06	5.12
			100	-6543.49	0.18	0.00	0.00	-1.40	5.12
			199	-6543.49	0.18	0.00	0.00	-5.03	5.12
351	Fondazio ne	46, 81	0	-1234.48	0.29	0.00	0.00	-14.39	-11.56
			100	-1234.48	0.29	0.00	0.00	-2.93	-11.56
			199	-1234.48	0.29	0.00	0.00	8.90	-11.56
352	Primo Impalcato	77, 47	0	6488.57	-0.20	0.00	0.00	9.46	12.93
			100	6488.57	-0.20	0.00	0.00	-4.23	12.93
			199	6488.57	-0.20	0.00	0.00	-16.52	12.93
353	Primo Impalcato	80, 48	0	1293.32	0.30	0.00	0.00	-12.09	-16.00
			100	1293.32	0.30	0.00	0.00	4.37	-16.00
			199	1293.32	0.30	0.00	0.00	19.79	-16.00
354	Fondazio ne	49, 77	0	-6278.52	-0.22	0.00	0.00	-16.70	-13.37
			100	-6278.52	-0.22	0.00	0.00	-4.13	-13.37
			199	-6278.52	-0.22	0.00	0.00	9.97	-13.37
355	Fondazio ne	50, 80	0	-1211.49	0.23	0.00	0.00	18.46	14.77
			100	-1211.49	0.23	0.00	0.00	4.99	14.77
			199	-1211.49	0.23	0.00	0.00	10.99	14.77
356	Primo Impalcato	76, 51	0	6014.66	-0.10	0.00	0.00	-4.33	7.04
			100	6014.66	-0.10	0.00	0.00	3.51	7.04
			199	6014.66	-0.10	0.00	0.00	-10.47	7.04
357	Fondazio ne	53, 76	0	-6169.20	-0.20	0.00	0.00	-10.54	-8.29
			100	-6169.20	-0.20	0.00	0.00	-2.34	-8.29
			199	-6169.20	-0.20	0.00	0.00	6.69	-8.29
358	Primo Impalcato	75, 55	0	5009.62	-0.62	0.00	0.00	-15.46	-16.16
			102	5009.62	-0.62	0.00	0.00	-1.35	-16.16
			204	5009.62	-0.62	0.00	0.00	17.54	-16.16
359	Fondazio ne	56, 79	0	1110.88	-0.44	0.00	0.00	13.77	12.45
			102	1110.88	-0.44	0.00	0.00	-1.24	12.45
			204	1110.88	-0.44	0.00	0.00	-11.69	12.45
360	Fondazio ne	57, 75	0	-5628.52	0.31	0.00	0.00	-14.55	-7.95
			102	-5628.52	0.31	0.00	0.00	-6.90	-7.95
			204	-5628.52	0.31	0.00	0.00	2.20	-7.95
361	Fondazio ne	57, 93	0	442.81	-0.38	0.00	0.00	-11.56	21.96
			103	442.81	-0.38	0.00	0.00	-21.96	21.96
			206	442.81	-0.38	0.00	0.00	-39.61	21.96
362	Primo Impalcato	93, 58	0	-1055.55	-1.86	0.00	0.00	13.68	22.03
			103	-1055.55	-1.86	0.00	0.00	-13.36	22.03
			206	-1055.55	-1.86	0.00	0.00	-34.88	22.03
363	Fondazio ne	61, 95	0	-604.44	1.84	0.00	0.00	-50.74	-18.31
			100	-604.44	1.84	0.00	0.00	-34.49	-18.31
			200	-604.44	1.84	0.00	0.00	-30.95	-18.31
364	Primo Impalcato	95, 62	0	543.59	-1.26	0.00	0.00	-34.97	8.55
			100	543.59	-1.26	0.00	0.00	-38.41	8.55
			200	543.59	-1.26	0.00	0.00	-44.17	8.55

365	Primo Impalcato	96, 65	0	-558.17	1.32	0.00	0.00	13.09	-9.39
			100	-558.17	1.32	0.00	0.00	20.78	-9.39
			200	-558.17	1.32	0.00	0.00	30.16	-9.39
366	Fondazione	66, 96	0	570.82	-0.76	0.00	0.00	30.28	-12.85
			100	570.82	-0.76	0.00	0.00	22.25	-12.85
			200	570.82	-0.76	0.00	0.00	30.71	-12.85
367	Fondazione	69, 94	0	-734.96	0.67	0.00	0.00	18.23	16.02
			103	-734.96	0.67	0.00	0.00	-3.10	16.02
			206	-734.96	0.67	0.00	0.00	14.86	16.02
368	Primo Impalcato	79, 70	0	-1175.86	-0.23	0.00	0.00	-2.34	-4.25
			102	-1175.86	-0.23	0.00	0.00	-4.28	-4.25
			204	-1175.86	-0.23	0.00	0.00	8.51	-4.25
369	Primo Impalcato	94, 70	0	664.90	0.31	0.00	0.00	-8.40	-7.62
			103	664.90	0.31	0.00	0.00	-6.61	-7.62
			206	664.90	0.31	0.00	0.00	10.07	-7.62
370	Primo Impalcato	1, 71	0	-4882.29	-2.57	0.00	0.00	20.94	12.67
			102	-4882.29	-2.57	0.00	0.00	14.91	12.67
			204	-4882.29	-2.57	0.00	0.00	14.63	12.67
371	Primo Impalcato	1, 92	0	1156.97	-1.76	0.00	0.00	15.14	15.44
			103	1156.97	-1.76	0.00	0.00	11.30	15.44
			206	1156.97	-1.76	0.00	0.00	18.92	15.44
372	Primo Impalcato	92, 2	0	-527.44	-1.47	0.00	0.00	-39.41	17.64
			103	-527.44	-1.47	0.00	0.00	-57.26	17.64
			206	-527.44	-1.47	0.00	0.00	-75.27	17.64
373	Primo Impalcato	6, 89	0	-660.36	1.39	0.00	0.00	-21.25	11.90
			100	-660.36	1.39	0.00	0.00	-29.53	11.90
			200	-660.36	1.39	0.00	0.00	-40.65	11.90
374	Primo Impalcato	89, 7	0	659.66	2.05	0.00	0.00	-27.37	-8.78
			100	659.66	2.05	0.00	0.00	-20.25	-8.78
			200	659.66	2.05	0.00	0.00	-13.34	-8.78
375	Primo Impalcato	9, 90	0	-634.04	0.92	0.00	0.00	-22.44	-14.46
			100	-634.04	0.92	0.00	0.00	-23.36	-14.46
			200	-634.04	0.92	0.00	0.00	-35.71	-14.46
376	Primo Impalcato	90, 10	0	626.82	1.59	0.00	0.00	-13.80	-10.46
			100	626.82	1.59	0.00	0.00	-9.07	-10.46
			200	626.82	1.59	0.00	0.00	-10.67	-10.46
377	Primo Impalcato	13, 91	0	-712.06	1.32	0.00	0.00	-19.07	-4.88
			103	-712.06	1.32	0.00	0.00	-14.13	-4.88
			206	-712.06	1.32	0.00	0.00	-9.26	-4.88
378	Primo Impalcato	88, 14	0	-912.57	1.10	0.00	0.00	13.49	8.29
			102	-912.57	1.10	0.00	0.00	8.20	8.29
			204	-912.57	1.10	0.00	0.00	7.85	8.29
379	Primo Impalcato	91, 14	0	784.33	0.85	0.00	0.00	20.58	14.72
			103	784.33	0.85	0.00	0.00	8.68	14.72
			206	784.33	0.85	0.00	0.00	11.56	14.72
380	Primo Impalcato	71, 15	0	5462.23	1.08	0.00	0.00	4.53	-5.09
			102	5462.23	1.08	0.00	0.00	8.86	-5.09
			204	5462.23	1.08	0.00	0.00	13.34	-5.09
381	Primo Impalcato	16, 88	0	971.42	0.60	0.00	0.00	6.65	2.99
			102	971.42	0.60	0.00	0.00	-4.70	2.99
			204	971.42	0.60	0.00	0.00	-3.21	2.99
382	Primo Impalcato	17, 72	0	-5909.13	0.89	0.00	0.00	-2.95	-2.45
			100	-5909.13	0.89	0.00	0.00	4.11	-2.45
			199	-5909.13	0.89	0.00	0.00	5.91	-2.45
383	Primo	87, 18	0	-1081.21	0.72	0.00	0.00	6.07	2.36

	Impalcato								
			100	-1081.21	0.72	0.00	0.00	3.77	2.36
			199	-1081.21	0.72	0.00	0.00	2.31	2.36
384	Primo Impalcato	72, 19	0	6002.34	-0.79	0.00	0.00	6.74	2.51
			100	6002.34	-0.79	0.00	0.00	4.29	2.51
			199	6002.34	-0.79	0.00	0.00	-2.43	2.51
385	Primo Impalcato	20, 87	0	1031.61	-0.79	0.00	0.00	1.98	-3.08
			100	1031.61	-0.79	0.00	0.00	3.76	-3.08
			199	1031.61	-0.79	0.00	0.00	6.60	-3.08
386	Primo Impalcato	21, 73	0	-6388.33	-0.63	0.00	0.00	3.50	4.55
			100	-6388.33	-0.63	0.00	0.00	6.40	4.55
			199	-6388.33	-0.63	0.00	0.00	-10.34	4.55
387	Primo Impalcato	86, 22	0	-1204.92	-0.60	0.00	0.00	-10.60	-4.61
			100	-1204.92	-0.60	0.00	0.00	-6.83	-4.61
			199	-1204.92	-0.60	0.00	0.00	-3.50	-4.61
388	Primo Impalcato	73, 23	0	6153.97	0.68	0.00	0.00	11.88	5.06
			100	6153.97	0.68	0.00	0.00	6.85	5.06
			199	6153.97	0.68	0.00	0.00	-2.80	5.06
389	Primo Impalcato	24, 86	0	1107.51	0.67	0.00	0.00	-2.89	-5.61
			100	1107.51	0.67	0.00	0.00	-7.26	-5.61
			199	1107.51	0.67	0.00	0.00	12.83	-5.61
390	Primo Impalcato	25, 74	0	-7459.99	0.67	0.00	0.00	-7.63	5.43
			103	-7459.99	0.67	0.00	0.00	-4.40	5.43
			206	-7459.99	0.67	0.00	0.00	-4.71	5.43
391	Primo Impalcato	85, 26	0	-1260.32	0.57	0.00	0.00	-3.38	-1.59
			100	-1260.32	0.57	0.00	0.00	-1.92	-1.59
			199	-1260.32	0.57	0.00	0.00	-2.76	-1.59
392	Primo Impalcato	27, 85	0	1153.12	-0.63	0.00	0.00	1.26	3.32
			100	1153.12	-0.63	0.00	0.00	-3.09	3.32
			199	1153.12	-0.63	0.00	0.00	-6.27	3.32
393	Primo Impalcato	74, 28	0	7371.80	-0.60	0.00	0.00	-12.08	-6.78
			103	7371.80	-0.60	0.00	0.00	-5.18	-6.78
			206	7371.80	-0.60	0.00	0.00	-4.80	-6.78
394	Primo Impalcato	84, 29	0	-1297.22	-0.20	0.00	0.00	-4.10	-3.14
			100	-1297.22	-0.20	0.00	0.00	-2.93	-3.14
			199	-1297.22	-0.20	0.00	0.00	-3.63	-3.14
395	Primo Impalcato	31, 84	0	1143.05	0.36	0.00	0.00	-2.21	5.24
			100	1143.05	0.36	0.00	0.00	-4.13	5.24
			199	1143.05	0.36	0.00	0.00	-9.21	5.24
396	Primo Impalcato	83, 33	0	-1299.02	-0.09	0.00	0.00	8.59	-5.62
			100	-1299.02	-0.09	0.00	0.00	3.05	-5.62
			199	-1299.02	-0.09	0.00	0.00	-3.50	-5.62
397	Primo Impalcato	35, 83	0	1183.60	-0.27	0.00	0.00	3.83	4.51
			100	1183.60	-0.27	0.00	0.00	2.55	4.51
			199	1183.60	-0.27	0.00	0.00	-6.80	4.51
398	Primo Impalcato	82, 37	0	-1224.41	-0.31	0.00	0.00	8.72	6.72
			100	-1224.41	-0.31	0.00	0.00	3.53	6.72
			199	-1224.41	-0.31	0.00	0.00	-4.99	6.72
399	Primo Impalcato	39, 82	0	1309.02	0.16	0.00	0.00	4.46	6.00
			100	1309.02	0.16	0.00	0.00	1.59	6.00
			199	1309.02	0.16	0.00	0.00	7.53	6.00
400	Primo Impalcato	78, 43	0	-6544.66	-0.68	0.00	0.00	-5.52	-3.09
			100	-6544.66	-0.68	0.00	0.00	-2.49	-3.09
			199	-6544.66	-0.68	0.00	0.00	-2.17	-3.09
401	Primo Impalcato	81, 44	0	-1235.98	-0.60	0.00	0.00	9.16	4.66

			100	-1235.98	-0.60	0.00	0.00	4.62	4.66
			199	-1235.98	-0.60	0.00	0.00	2.48	4.66
402	Primo Impalcato	45, 78	0	6404.81	0.62	0.00	0.00	-3.96	2.53
			100	6404.81	0.62	0.00	0.00	-1.91	2.53
			199	6404.81	0.62	0.00	0.00	-2.06	2.53
403	Primo Impalcato	46, 81	0	1350.01	0.58	0.00	0.00	3.38	1.67
			100	1350.01	0.58	0.00	0.00	3.75	1.67
			199	1350.01	0.58	0.00	0.00	4.90	1.67
404	Primo Impalcato	77, 47	0	-6279.99	0.59	0.00	0.00	10.15	3.89
			100	-6279.99	0.59	0.00	0.00	6.29	3.89
			199	-6279.99	0.59	0.00	0.00	2.94	3.89
405	Primo Impalcato	80, 48	0	-1212.81	0.61	0.00	0.00	11.13	4.46
			100	-1212.81	0.61	0.00	0.00	-6.78	4.46
			199	-1212.81	0.61	0.00	0.00	-4.33	4.46
406	Primo Impalcato	49, 77	0	6489.94	-0.60	0.00	0.00	2.98	-3.74
			100	6489.94	-0.60	0.00	0.00	6.10	-3.74
			199	6489.94	-0.60	0.00	0.00	9.55	-3.74
407	Primo Impalcato	50, 80	0	1292.96	-0.58	0.00	0.00	3.44	5.70
			100	1292.96	-0.58	0.00	0.00	-6.74	5.70
			199	1292.96	-0.58	0.00	0.00	-12.19	5.70
408	Primo Impalcato	76, 51	0	-6169.13	-0.69	0.00	0.00	6.74	-3.92
			100	-6169.13	-0.69	0.00	0.00	-3.32	-3.92
			199	-6169.13	-0.69	0.00	0.00	3.17	-3.92
409	Primo Impalcato	53, 76	0	6016.36	0.74	0.00	0.00	2.97	1.87
			100	6016.36	0.74	0.00	0.00	-3.24	1.87
			199	6016.36	0.74	0.00	0.00	-4.68	1.87
410	Primo Impalcato	75, 55	0	-5629.20	0.89	0.00	0.00	4.10	-5.65
			102	-5629.20	0.89	0.00	0.00	7.80	-5.65
			204	-5629.20	0.89	0.00	0.00	13.48	-5.65
411	Primo Impalcato	56, 79	0	-1175.97	0.46	0.00	0.00	-5.45	-2.36
			102	-1175.97	0.46	0.00	0.00	-3.55	-2.36
			204	-1175.97	0.46	0.00	0.00	-1.86	-2.36
412	Primo Impalcato	57, 75	0	5011.59	-2.41	0.00	0.00	22.25	14.57
			102	5011.59	-2.41	0.00	0.00	14.24	14.57
			204	5011.59	-2.41	0.00	0.00	-15.56	14.57
413	Primo Impalcato	57, 93	0	-1053.13	-1.72	0.00	0.00	16.70	13.65
			103	-1053.13	-1.72	0.00	0.00	10.44	13.65
			206	-1053.13	-1.72	0.00	0.00	14.85	13.65
414	Primo Impalcato	93, 58	0	436.83	-1.20	0.00	0.00	-39.31	16.78
			103	436.83	-1.20	0.00	0.00	-56.38	16.78
			206	436.83	-1.20	0.00	0.00	-73.50	16.78
415	Primo Impalcato	61, 95	0	540.09	-0.74	0.00	0.00	-25.08	12.20
			100	540.09	-0.74	0.00	0.00	-26.33	12.20
			200	540.09	-0.74	0.00	0.00	-35.36	12.20
416	Primo Impalcato	95, 62	0	-600.77	1.58	0.00	0.00	-32.51	-13.43
			100	-600.77	1.58	0.00	0.00	-19.95	-13.43
			200	-600.77	1.58	0.00	0.00	-14.50	-13.43
417	Primo Impalcato	96, 65	0	567.10	0.75	0.00	0.00	31.13	-11.13
			100	567.10	0.75	0.00	0.00	21.98	-11.13
			200	567.10	0.75	0.00	0.00	22.10	-11.13
418	Primo Impalcato	66, 96	0	-554.31	1.49	0.00	0.00	7.33	-9.34
			100	-554.31	1.49	0.00	0.00	7.98	-9.34
			200	-554.31	1.49	0.00	0.00	14.07	-9.34
419	Primo Impalcato	69, 94	0	660.34	1.06	0.00	0.00	-18.63	-6.12
			103	660.34	1.06	0.00	0.00	-12.53	-6.12

			206	660.34	1.06	0.00	0.00	-7.69	-6.12
420	Primo Impalcato	79, 70	0	1111.67	0.90	0.00	0.00	-12.22	-8.07
			102	1111.67	0.90	0.00	0.00	6.95	-8.07
			204	1111.67	0.90	0.00	0.00	6.83	-8.07
421	Primo Impalcato	94, 70	0	-730.09	-0.72	0.00	0.00	15.82	12.57
			103	-730.09	-0.72	0.00	0.00	7.36	12.57
			206	-730.09	-0.72	0.00	0.00	11.51	12.57
422	Copertura	1, 2	0	-1749.56	1630.47	-1701.39	490.89	-269.05	307.38
			83	-1749.56	1630.47	-1500.36	490.89	-360.63	307.38
			166	-1749.56	1630.47	-1321.97	490.89	-585.99	307.38
423	Copertura	15, 1	0	3026.47	98.97	9876.53	-752.81	1895.49	1292.90
			80	3026.47	98.97	9330.51	-752.81	869.50	1292.90
			159	3026.47	98.97	8859.96	-752.81	-250.58	1292.90
424	Copertura	2, 3	0	-1634.97	245.97	-1254.50	825.50	-582.27	-420.12
			69	-1634.97	245.97	-689.69	825.50	-556.98	-420.12
			138	-1634.97	245.97	203.43	825.50	800.04	-420.12
425	Copertura	3, 4	0	-1499.97	-51.48	208.24	469.77	805.74	-516.55
			69	-1499.97	-51.48	325.57	469.77	759.65	-516.55
			138	-1499.97	-51.48	564.32	469.77	764.89	-516.55
426	Copertura	4, 5	0	-1374.13	-137.01	560.79	-140.66	765.11	543.44
			69	-1374.13	-137.01	605.24	-140.66	826.58	543.44
			138	-1374.13	-137.01	683.51	-140.66	1146.23	543.44
427	Copertura	5, 6	0	-1282.41	-179.81	676.32	-202.26	1147.96	-149.62
			69	-1282.41	-179.81	673.80	-202.26	1226.14	-149.62
			138	-1282.41	-179.81	680.33	-202.26	1305.30	-149.62
428	Copertura	6, 7	0	-1239.68	-178.95	672.14	431.00	1304.44	-294.83
			69	-1239.68	-178.95	457.71	431.00	1129.99	-294.83
			138	-1239.68	-178.95	505.15	431.00	966.94	-294.83
429	Copertura	7, 8	0	-1197.41	-295.59	514.75	-251.63	980.43	434.94
			69	-1197.41	-295.59	344.86	-251.63	793.94	434.94
			138	-1197.41	-295.59	202.12	-251.63	874.66	434.94
430	Copertura	8, 9	0	-1246.42	-267.82	205.03	-244.89	881.50	362.36
			69	-1246.42	-267.82	163.39	-244.89	868.69	362.36
			138	-1246.42	-267.82	-193.91	-244.89	893.11	362.36
431	Copertura	9, 10	0	-1232.36	-320.14	-182.25	436.82	911.58	384.86
			69	-1232.36	-320.14	126.61	436.82	673.48	384.86
			138	-1232.36	-320.14	424.89	436.82	443.17	384.86
432	Copertura	10, 11	0	-1218.80	-335.22	436.73	-276.29	447.47	682.32
			69	-1218.80	-335.22	254.74	-276.29	-123.55	682.32
			138	-1218.80	-335.22	-178.50	-276.29	-505.35	682.32
433	Copertura	11, 12	0	-1343.10	-273.44	-185.88	-384.62	-499.55	535.82
			69	-1343.10	-273.44	-270.58	-384.62	-868.86	535.82
			138	-1343.10	-273.44	-489.98	-384.62	-1238.41	535.82
434	Copertura	12, 13	0	-1479.20	-330.42	-479.46	-416.24	-1229.69	494.70
			69	-1479.20	-330.42	-751.35	-416.24	-1363.36	494.70
			138	-1479.20	-330.42	-1031.57	-416.24	-1517.12	494.70
435	Copertura	13, 14	0	-1441.54	-316.28	-1034.87	387.79	-1502.27	647.27
			83	-1441.54	-316.28	-716.55	387.79	-1687.54	647.27
			166	-1441.54	-316.28	-404.67	387.79	-2033.38	647.27
436	Copertura	16, 14	0	-105.53	-73.41	1603.09	-496.57	906.08	-1291.09
			80	-105.53	-73.41	1246.38	-496.57	1371.20	-1291.09
			159	-105.53	-73.41	1014.46	-496.57	1987.50	-1291.09
437	Copertura	15, 17	0	2662.78	166.79	12777.81	-5568.22	-1019.34	1465.44
			66	2662.78	166.79	9525.04	-5568.22	-804.90	1465.44
			132	2662.78	166.79	6438.04	-5568.22	-1199.85	1465.44
438	Copertura	16, 18	0	-214.16	154.18	1853.18	-1435.85	-1673.37	-1365.20
			66	-214.16	154.18	1567.00	-1435.85	-836.39	-1365.20
			132	-214.16	154.18	-1818.22	-1435.85	-247.66	-1365.20
439	Copertura	17, 19	0	2390.08	-58.52	9328.73	-4124.46	837.87	1738.61
			66	2390.08	-58.52	7007.30	-4124.46	-417.82	1738.61
			132	2390.08	-58.52	4752.15	-4124.46	-1476.25	1738.61
440	Copertura	18, 20	0	-219.82	-54.55	2065.41	-765.96	-1122.23	1565.82
			66	-219.82	-54.55	-2050.59	-765.96	-402.92	1565.82
			132	-219.82	-54.55	-2240.40	-765.96	-997.88	1565.82
441	Copertura	19, 21	0	2120.81	-141.76	7606.50	-5461.45	949.96	1167.44
			66	2120.81	-141.76	4129.88	-5461.45	-581.33	1167.44
			132	2120.81	-141.76	-877.01	-5461.45	-1165.80	1167.44
442	Copertura	20, 22	0	-167.58	-138.33	-2447.28	-1384.41	-879.09	-882.76
			66	-167.58	-138.33	-1738.81	-1384.41	-570.69	-882.76
			132	-167.58	-138.33	-1107.80	-1384.41	-880.62	-882.76

443	Copertura	21, 23	0	1796.34	-37.70	3532.27	-2878.91	1098.54	1587.18
			66	1796.34	-37.70	1655.17	-2878.91	161.95	1587.18
			132	1796.34	-37.70	-850.92	-2878.91	-1004.13	1587.18
444	Copertura	22, 24	0	-135.42	-67.13	-1306.04	747.94	-811.29	-1225.83
			66	-135.42	-67.13	-959.12	747.94	174.61	-1225.83
			132	-135.42	-67.13	-671.07	747.94	809.54	-1225.83
445	Copertura	23, 25	0	1645.70	117.26	2674.81	-3668.14	1148.69	841.70
			66	1645.70	117.26	909.99	-3668.14	778.60	841.70
			132	1645.70	117.26	-2514.45	-3668.14	615.12	841.70
446	Copertura	24, 26	0	-326.68	140.32	897.91	-1027.60	-791.59	-463.57
			66	-326.68	140.32	866.09	-1027.60	682.60	-463.57
			132	-326.68	140.32	1377.61	-1027.60	671.16	-463.57
447	Copertura	25, 28	0	1340.50	54.64	2035.67	-595.82	1997.92	2065.75
			85	1340.50	54.64	1778.71	-595.82	244.13	2065.75
			170	1340.50	54.64	1696.91	-595.82	-1514.54	2065.75
448	Copertura	26, 27	0	-243.89	120.59	1226.10	769.74	-1616.50	-2175.44
			66	-243.89	120.59	1130.72	769.74	185.39	-2175.44
			132	-243.89	120.59	1265.37	769.74	1256.44	-2175.44
449	Copertura	27, 29	0	-159.11	-89.13	1361.02	-928.97	303.15	-819.89
			66	-159.11	-89.13	1086.05	-928.97	-691.22	-819.89
			132	-159.11	-89.13	1159.11	-928.97	-1226.17	-819.89
450	Copertura	28, 30	0	977.23	-69.78	4324.05	-2719.77	483.48	1131.65
			73	977.23	-69.78	2400.70	-2719.77	-686.09	1131.65
			146	977.23	-69.78	993.53	-2719.77	-1491.65	1131.65
451	Copertura	29, 31	0	-190.61	131.73	928.45	-921.88	-974.43	-1118.44
			66	-190.61	131.73	996.78	-921.88	-242.07	-1118.44
			132	-190.61	131.73	1083.15	-921.88	507.40	-1118.44
452	Copertura	30, 32	0	845.70	-88.38	3294.82	-3217.99	1121.61	1503.50
			69	845.70	-88.38	1357.29	-3217.99	-268.85	1503.50
			137	845.70	-88.38	-1578.20	-3217.99	-960.17	1503.50
453	Copertura	31, 33	0	-498.90	-50.72	1170.46	-684.71	-675.14	-764.02
			66	-498.90	-50.72	938.16	-684.71	579.32	-764.02
			132	-498.90	-50.72	1289.77	-684.71	935.72	-764.02
454	Copertura	32, 34	0	832.11	46.21	2468.86	-2678.87	853.73	1228.25
			69	832.11	46.21	805.24	-2678.87	528.20	1228.25
			138	832.11	46.21	-1933.86	-2678.87	-1289.65	1228.25
455	Copertura	33, 35	0	-534.06	-137.68	1082.34	-769.58	1385.39	1550.85
			66	-534.06	-137.68	-612.57	-769.58	367.94	1550.85
			132	-534.06	-137.68	-696.44	-769.58	668.43	1550.85
456	Copertura	34, 36	0	583.20	-113.60	2089.10	-2914.94	1504.20	1786.07
			69	583.20	-113.60	-439.16	-2914.94	347.96	1786.07
			138	583.20	-113.60	-2189.41	-2914.94	-985.55	1786.07
457	Copertura	35, 37	0	-357.12	-35.33	-843.24	-539.07	-555.31	1353.95
			66	-357.12	-35.33	-765.16	-539.07	-458.89	1353.95
			132	-357.12	-35.33	-1018.02	-539.07	-1303.45	1353.95
458	Copertura	36, 38	0	-514.02	-34.23	1911.92	-2643.65	791.21	1550.49
			69	-514.02	-34.23	-1107.68	-2643.65	-435.36	1550.49
			138	-514.02	-34.23	-2682.20	-2643.65	-1427.24	1550.49
459	Copertura	37, 39	0	-360.61	127.56	-884.51	-725.95	-1002.38	-993.25
			66	-360.61	127.56	-698.13	-725.95	-481.12	-993.25
			132	-360.61	127.56	-724.45	-725.95	661.47	-993.25
460	Copertura	38, 40	0	-838.97	117.85	1503.26	-3414.84	1352.77	1390.27
			69	-838.97	117.85	-1412.60	-3414.84	-445.03	1390.27
			137	-838.97	117.85	-3369.72	-3414.84	-741.26	1390.27
461	Copertura	39, 41	0	-681.59	125.36	963.45	1364.70	-332.88	-2146.69
			66	-681.59	125.36	-979.50	1364.70	1150.48	-2146.69
			132	-681.59	125.36	1717.79	1364.70	2566.74	-2146.69
462	Copertura	40, 42	0	-1365.03	-63.29	-462.29	-3321.45	901.08	2546.67
			69	-1365.03	-63.29	-2545.65	-3321.45	-946.28	2546.67
			138	-1365.03	-63.29	-4699.66	-3321.45	-2699.75	2546.67
463	Copertura	41, 44	0	-720.62	68.92	1721.51	-554.15	2031.05	2565.98
			66	-720.62	68.92	1785.54	-554.15	576.63	2565.98
			132	-720.62	68.92	2001.20	-554.15	-1861.51	2565.98
464	Copertura	42, 43	0	-1358.46	-511.25	-1746.96	-2333.46	-1608.28	-2876.16
			23	-1358.46	-511.25	-2133.90	-2333.46	1010.24	-2876.16
			46	-1358.46	-511.25	-2525.29	-2333.46	888.62	-2876.16
465	Copertura	43, 45	0	-1471.67	-60.25	1588.34	-1536.47	2493.12	3079.01
			66	-1471.67	-60.25	1045.44	-1536.47	532.63	3079.01
			132	-1471.67	-60.25	1440.31	-1536.47	-1580.63	3079.01
466	Copertura	44, 46	0	-548.96	-102.26	1910.83	788.60	-2901.45	-2746.15
			66	-548.96	-102.26	1699.27	788.60	-1211.48	-2746.15
			132	-548.96	-102.26	1554.15	788.60	-916.23	-2746.15

467	Copertura	45, 47	0	-1620.22	113.66	3169.84	-3985.54	808.09	1374.69
			66	-1620.22	113.66	731.25	-3985.54	-758.77	1374.69
			132	-1620.22	113.66	-2622.18	-3985.54	-1527.90	1374.69
468	Copertura	46, 48	0	-397.05	122.22	1546.49	760.86	-922.24	-1209.50
			66	-397.05	122.22	1109.21	760.86	-739.86	-1209.50
			132	-397.05	122.22	827.70	760.86	-1122.38	-1209.50
469	Copertura	47, 49	0	-2021.05	-74.57	998.61	-3292.18	1180.35	1567.28
			66	-2021.05	-74.57	-1631.28	-3292.18	340.16	1567.28
			132	-2021.05	-74.57	-3755.24	-3292.18	-906.94	1567.28
470	Copertura	48, 50	0	-579.30	-51.18	812.04	-422.25	1051.71	-1289.67
			66	-579.30	-51.18	886.26	-422.25	291.70	-1289.67
			132	-579.30	-51.18	1121.14	-422.25	660.25	-1289.67
471	Copertura	49, 51	0	-2510.70	-124.64	1138.24	-5584.97	876.63	1310.26
			66	-2510.70	-124.64	-4578.55	-5584.97	587.43	1310.26
			132	-2510.70	-124.64	-8234.38	-5584.97	-1175.72	1310.26
472	Copertura	50, 52	0	-862.72	-124.23	1010.82	-1195.92	-536.90	-1010.38
			66	-862.72	-124.23	1567.24	-1195.92	583.64	-1010.38
			132	-862.72	-124.23	2192.95	-1195.92	1182.94	-1010.38
473	Copertura	51, 53	0	-2799.97	-54.31	-5436.21	-4030.96	1685.39	1614.21
			66	-2799.97	-54.31	-7657.60	-4030.96	662.56	1614.21
			132	-2799.97	-54.31	-9961.52	-4030.96	-470.58	1614.21
474	Copertura	52, 54	0	-866.38	-65.22	2027.71	-1208.82	-1186.88	-1513.47
			66	-866.38	-65.22	2118.47	-1208.82	635.82	-1513.47
			132	-866.38	-65.22	-2452.79	-1208.82	936.21	-1513.47
475	Copertura	53, 55	0	-2957.94	-162.58	-7109.37	-5711.62	1330.35	1800.06
			66	-2957.94	-162.58	-9855.39	-5711.62	793.39	1800.06
			132	-2957.94	-162.58	-12697.47	-5711.62	1197.71	1800.06
476	Copertura	54, 56	0	-665.14	125.96	-2220.41	1208.66	-421.67	-1727.51
			66	-665.14	125.96	-1900.92	1208.66	829.29	-1727.51
			132	-665.14	125.96	-1823.27	1208.66	1937.88	-1727.51
477	Copertura	55, 57	0	-3382.70	89.80	-9797.97	634.79	2058.42	1118.75
			80	-3382.70	89.80	-9302.00	634.79	1227.83	1118.75
			159	-3382.70	89.80	-8824.90	634.79	-667.23	1118.75
478	Copertura	56, 70	0	-707.26	74.93	-1536.97	-524.45	1098.27	-1185.66
			80	-707.26	74.93	-1163.28	-524.45	1704.43	-1185.66
			159	-707.26	74.93	-940.23	-524.45	2440.17	-1185.66
479	Copertura	57, 58	0	1536.57	1645.45	1666.16	-362.76	-721.10	-893.87
			83	1536.57	1645.45	1396.91	-362.76	-224.17	-893.87
			166	1536.57	1645.45	1131.15	-362.76	907.10	-893.87
480	Copertura	58, 59	0	1423.00	216.44	1057.58	-836.56	903.71	-546.82
			69	1423.00	216.44	485.84	-836.56	1093.06	-546.82
			138	1423.00	216.44	156.73	-836.56	1440.89	-546.82
481	Copertura	59, 60	0	1348.53	-60.29	148.63	-475.53	1446.47	768.64
			69	1348.53	-60.29	-433.47	-475.53	1186.75	768.64
			138	1348.53	-60.29	-757.35	-475.53	985.84	768.64
482	Copertura	60, 61	0	1292.19	-117.16	-750.29	-163.63	986.85	980.66
			69	1292.19	-117.16	-862.05	-163.63	923.12	980.66
			138	1292.19	-117.16	-974.08	-163.63	1503.43	980.66
483	Copertura	61, 62	0	1281.09	-175.30	-967.64	-367.36	1510.27	298.45
			69	1281.09	-175.30	-800.01	-367.36	1698.06	298.45
			138	1281.09	-175.30	-717.25	-367.36	1889.63	298.45
484	Copertura	62, 63	0	1264.53	-189.11	-716.11	173.37	1884.50	-550.75
			69	1264.53	-189.11	-606.51	173.37	1531.31	-550.75
			138	1264.53	-189.11	-498.09	173.37	1194.71	-550.75
485	Copertura	63, 64	0	1213.25	-321.57	-497.67	201.65	1204.10	-877.68
			69	1213.25	-321.57	-377.53	201.65	783.51	-877.68
			138	1213.25	-321.57	-266.58	201.65	1103.59	-877.68
486	Copertura	64, 65	0	1208.54	-263.86	-265.71	149.91	1106.62	-595.20
			69	1208.54	-263.86	211.53	149.91	1281.50	-595.20
			138	1208.54	-263.86	236.88	149.91	1487.43	-595.20
487	Copertura	65, 66	0	1180.44	-323.46	232.29	-364.76	1507.51	531.58
			69	1180.44	-323.46	120.34	-364.76	1148.70	531.58
			138	1180.44	-323.46	324.77	-364.76	797.19	531.58
488	Copertura	66, 67	0	1151.71	-312.01	333.70	201.21	799.31	1113.65
			69	1151.71	-312.01	238.36	201.21	-222.18	1113.65
			138	1151.71	-312.01	248.87	201.21	-756.93	1113.65
489	Copertura	67, 68	0	1221.04	-290.03	253.55	302.97	-750.54	783.70
			69	1221.04	-290.03	345.06	302.97	-1291.24	783.70
			138	1221.04	-290.03	476.57	302.97	-1831.97	783.70
490	Copertura	68, 69	0	1296.65	-298.28	472.06	336.08	-1823.24	638.40
			69	1296.65	-298.28	609.43	336.08	-1829.76	638.40
			138	1296.65	-298.28	827.34	336.08	-1869.03	638.40

491	Copertura	69, 70	0	1259.58	-329.74	832.76	-316.11	-1856.25	-1171.09
			83	1259.58	-329.74	578.58	-316.11	-1732.93	-1171.09
			166	1259.58	-329.74	337.79	-316.11	-2488.75	-1171.09
492	Copertura	1	0	801.12	86.63	-6939.63	3063.40	1607.50	648.63
			220	801.12	86.63	-200.17	3063.40	192.66	648.63
			440	801.12	86.63	6539.32	3063.40	-1248.10	648.63
493	Copertura	2	0	-636.32	14.23	-1569.35	806.24	-11.91	-5.87
			220	-636.32	14.23	210.40	806.24	-1.48	-5.87
			440	-636.32	14.23	1979.36	806.24	14.00	-5.87
494	Copertura	3	0	368.53	6.73	-294.25	258.10	-11.36	-5.22
			220	368.53	6.73	281.36	258.10	-0.26	-5.22
			440	368.53	6.73	846.52	258.10	11.63	-5.22
495	Copertura	4	0	363.32	5.66	-90.15	156.80	-11.28	-5.11
			220	363.32	5.66	274.14	156.80	0.15	-5.11
			440	363.32	5.66	614.95	156.80	11.22	-5.11
496	Copertura	5	0	141.17	3.03	233.26	241.33	-11.84	-5.43
			220	141.17	3.03	325.19	241.33	0.24	-5.43
			440	141.17	3.03	849.04	241.33	12.08	-5.43
497	Copertura	6	0	-96.67	7.99	-103.90	178.26	-11.48	-5.20
			220	-96.67	7.99	295.71	178.26	-0.07	-5.20
			440	-96.67	7.99	686.79	178.26	11.40	-5.20
498	Copertura	7	0	140.21	8.00	-167.23	203.22	-11.59	-5.23
			220	140.21	8.00	300.76	203.22	-0.11	-5.23
			440	140.21	8.00	743.44	203.22	11.43	-5.23
499	Copertura	8	0	-23.67	9.17	196.75	206.41	-12.46	-5.74
			220	-23.67	9.17	282.43	206.41	0.23	-5.74
			440	-23.67	9.17	730.24	206.41	12.81	-5.74
500	Copertura	9	0	-146.97	11.42	-100.73	139.91	-11.82	-5.33
			220	-146.97	11.42	223.90	139.91	-0.15	-5.33
			440	-146.97	11.42	528.77	139.91	11.62	-5.33
501	Copertura	10	0	169.60	9.01	-181.82	167.98	-11.88	-5.34
			220	169.60	9.01	214.53	167.98	-0.16	-5.34
			440	169.60	9.01	576.32	167.98	11.63	-5.34
502	Copertura	11	0	108.56	11.46	85.51	95.51	-12.46	-5.69
			220	108.56	11.46	156.73	95.51	0.13	-5.69
			440	108.56	11.46	362.95	95.51	12.55	-5.69
503	Copertura	12	0	-138.74	9.64	160.21	-120.34	-12.24	-5.61
			220	-138.74	9.64	136.60	-120.34	0.20	-5.61
			440	-138.74	9.64	395.10	-120.34	12.45	-5.61
504	Copertura	13	0	-438.62	6.82	-192.85	131.84	-11.27	-5.19
			220	-438.62	6.82	97.34	131.84	0.32	-5.19
			440	-438.62	6.82	387.31	131.84	11.58	-5.19
505	Copertura	57	0	643.28	88.03	-6914.85	3051.86	-1560.63	-625.02
			220	643.28	88.03	-200.77	3051.86	-194.58	-625.02
			440	643.28	88.03	6513.34	3051.86	1190.57	-625.02
506	Copertura	58	0	678.24	13.39	-1556.33	797.76	10.23	5.12
			220	678.24	13.39	204.90	797.76	1.46	5.12
			440	678.24	13.39	1955.08	797.76	12.36	5.12
507	Copertura	59	0	-389.36	6.12	-253.76	234.94	9.29	4.28
			220	-389.36	6.12	277.37	234.94	0.25	4.28
			440	-389.36	6.12	783.16	234.94	-9.55	4.28
508	Copertura	60	0	-334.70	4.04	-67.78	149.19	8.67	3.96
			220	-334.70	4.04	277.49	149.19	-0.23	3.96
			440	-334.70	4.04	605.15	149.19	-8.77	3.96
509	Copertura	61	0	112.84	4.23	154.46	204.72	8.41	3.81
			220	112.84	4.23	313.19	204.72	0.07	3.81
			440	112.84	4.23	760.26	204.72	-8.36	3.81
510	Copertura	62	0	-171.84	6.79	171.86	203.55	8.56	3.87
			220	-171.84	6.79	298.89	203.55	0.08	3.87
			440	-171.84	6.79	741.75	203.55	-8.48	3.87
511	Copertura	63	0	-44.64	9.42	-174.59	203.25	9.17	4.20
			220	-44.64	9.42	295.19	203.25	-0.13	4.20
			440	-44.64	9.42	737.34	203.25	-9.29	4.20
512	Copertura	64	0	78.12	10.19	-181.77	198.84	9.29	4.24
			220	78.12	10.19	279.58	198.84	-0.11	4.24
			440	78.12	10.19	711.34	198.84	-9.38	4.24
513	Copertura	65	0	139.72	10.54	-133.12	154.74	8.91	4.01
			220	139.72	10.54	229.35	154.74	0.15	4.01
			440	139.72	10.54	565.04	154.74	-8.75	4.01
514	Copertura	66	0	-151.36	9.64	-123.85	134.34	8.95	4.02
			220	-151.36	9.64	197.65	134.34	0.14	4.02
			440	-151.36	9.64	487.33	134.34	-8.76	4.02

515	Copertura	67	0	-101.53	10.27	63.24	81.99	9.43	4.30
			220	-101.53	10.27	150.34	81.99	-0.14	4.30
			440	-101.53	10.27	328.12	81.99	-9.50	4.30
516	Copertura	68	0	147.27	9.32	107.42	87.21	9.31	4.27
			220	147.27	9.32	120.64	87.21	-0.20	4.27
			440	147.27	9.32	307.13	87.21	-9.48	4.27
517	Copertura	69	0	468.81	6.83	-176.96	128.49	8.57	3.95
			220	468.81	6.83	105.77	128.49	-0.33	3.95
			440	468.81	6.83	388.43	128.49	-8.80	3.95
518	Primo Impalcato	1, 74	0	879.96	4.48	0.00	0.00	-261.57	-157.83
			118	879.96	4.48	0.00	0.00	-82.16	-157.83
			235	879.96	4.48	0.00	0.00	111.21	-157.83
519	Copertura	74, 2	0	-1020.60	-1.24	0.00	0.00	-92.64	-28.69
			118	-1020.60	-1.24	0.00	0.00	-59.86	-28.69
			235	-1020.60	-1.24	0.00	0.00	-37.18	-28.69
520	Primo Impalcato	6, 71	0	587.40	1.74	0.00	0.00	-28.82	26.31
			115	587.40	1.74	0.00	0.00	-11.37	26.31
			231	587.40	1.74	0.00	0.00	-33.05	26.31
521	Copertura	71, 7	0	-584.45	1.20	0.00	0.00	-30.07	-18.52
			115	-584.45	1.20	0.00	0.00	-20.18	-18.52
			231	-584.45	1.20	0.00	0.00	-28.20	-18.52
522	Primo Impalcato	9, 72	0	600.99	1.70	0.00	0.00	26.56	24.62
			115	600.99	1.70	0.00	0.00	-3.68	24.62
			231	600.99	1.70	0.00	0.00	-31.46	24.62
523	Copertura	72, 10	0	-597.59	1.32	0.00	0.00	-21.12	10.66
			115	-597.59	1.32	0.00	0.00	-17.54	10.66
			231	-597.59	1.32	0.00	0.00	-22.19	10.66
524	Copertura	73, 13	0	583.27	-1.21	0.00	0.00	22.83	13.36
			118	583.27	-1.21	0.00	0.00	7.25	13.36
			235	583.27	-1.21	0.00	0.00	8.67	13.36
525	Primo Impalcato	14, 73	0	-640.42	-0.81	0.00	0.00	42.59	-32.57
			118	-640.42	-0.81	0.00	0.00	13.39	-32.57
			235	-640.42	-0.81	0.00	0.00	36.50	-32.57
526	Primo Impalcato	57, 75	0	-750.76	4.55	0.00	0.00	-255.24	-151.73
			118	-750.76	4.55	0.00	0.00	-82.34	-151.73
			235	-750.76	4.55	0.00	0.00	102.55	-151.73
527	Copertura	75, 58	0	947.97	-0.91	0.00	0.00	-86.28	-24.64
			118	947.97	-0.91	0.00	0.00	-57.77	-24.64
			235	947.97	-0.91	0.00	0.00	-34.58	-24.64
528	Copertura	77, 61	0	-429.33	1.13	0.00	0.00	20.58	20.73
			115	-429.33	1.13	0.00	0.00	10.25	20.73
			231	-429.33	1.13	0.00	0.00	28.65	20.73
529	Primo Impalcato	62, 77	0	431.74	-0.56	0.00	0.00	49.28	-34.51
			115	431.74	-0.56	0.00	0.00	15.87	-34.51
			231	431.74	-0.56	0.00	0.00	40.09	-34.51
530	Primo Impalcato	65, 78	0	-454.42	1.72	0.00	0.00	-36.34	-32.98
			115	-454.42	1.72	0.00	0.00	-2.48	-32.98
			231	-454.42	1.72	0.00	0.00	39.69	-32.98
531	Copertura	78, 66	0	445.50	1.17	0.00	0.00	-29.03	18.69
			115	445.50	1.17	0.00	0.00	-16.22	18.69
			231	445.50	1.17	0.00	0.00	-30.80	18.69
532	Primo Impalcato	69, 76	0	-466.21	-0.90	0.00	0.00	6.58	8.52
			118	-466.21	-0.90	0.00	0.00	-4.88	8.52
			235	-466.21	-0.90	0.00	0.00	-14.09	8.52
533	Copertura	76, 70	0	502.13	-0.84	0.00	0.00	-26.41	-24.60
			118	502.13	-0.84	0.00	0.00	-13.27	-24.60
			235	502.13	-0.84	0.00	0.00	-34.83	-24.60
534	Copertura	1, 74	0	-1019.83	5.34	0.00	0.00	280.86	159.43
			118	-1019.83	5.34	0.00	0.00	93.69	159.43
			235	-1019.83	5.34	0.00	0.00	-94.70	159.43
535	Copertura	74, 2	0	879.66	0.47	0.00	0.00	107.48	54.47
			118	879.66	0.47	0.00	0.00	46.44	54.47
			235	879.66	0.47	0.00	0.00	-35.17	54.47
536	Copertura	6, 71	0	-582.66	0.48	0.00	0.00	34.34	25.61
			115	-582.66	0.48	0.00	0.00	-8.59	25.61

			231	-582.66	0.48	0.00	0.00	-30.66	25.61
537	Copertura	71, 7	0	585.59	1.23	0.00	0.00	-31.69	-27.42
			115	585.59	1.23	0.00	0.00	4.22	-27.42
			231	585.59	1.23	0.00	0.00	33.46	-27.42
538	Copertura	9, 72	0	-595.45	1.40	0.00	0.00	27.74	15.72
			115	-595.45	1.40	0.00	0.00	-13.16	15.72
			231	-595.45	1.40	0.00	0.00	-22.33	15.72
539	Copertura	72, 10	0	599.00	1.75	0.00	0.00	-28.79	-19.90
			115	599.00	1.75	0.00	0.00	8.49	-19.90
			231	599.00	1.75	0.00	0.00	23.93	-19.90
540	Copertura	73, 13	0	-639.82	1.40	0.00	0.00	34.67	29.63
			118	-639.82	1.40	0.00	0.00	7.54	29.63
			235	-639.82	1.40	0.00	0.00	-36.45	29.63
541	Copertura	14, 73	0	583.39	-0.78	0.00	0.00	-44.75	-29.05
			118	583.39	-0.78	0.00	0.00	-11.55	-29.05
			235	583.39	-0.78	0.00	0.00	24.45	-29.05
542	Copertura	15, 125	0	1249.18	119.09	-327.55	-1567.66	-1635.99	-1395.23
			75	1249.18	119.09	-851.12	-1567.66	-589.59	-1395.23
			150	1249.18	119.09	-2026.60	-1567.66	456.92	-1395.23
543	Copertura	127, 16	0	1198.39	-9.00	-1693.79	1266.15	-345.73	372.96
			75	1198.39	-9.00	-744.61	1266.15	-538.43	372.96
			150	1198.39	-9.00	224.63	1266.15	-808.76	372.96
544	Copertura	17, 129	0	-365.61	121.68	170.38	-1182.86	-1698.75	-1466.33
			75	-365.61	121.68	-767.88	-1182.86	-599.55	-1466.33
			150	-365.61	121.68	-1654.02	-1182.86	502.05	-1466.33
545	Copertura	130, 18	0	467.32	-12.38	1643.88	-1210.54	-408.90	-563.63
			75	467.32	-12.38	735.98	-1210.54	-654.30	-563.63
			150	467.32	-12.38	-172.04	-1210.54	-1055.15	-563.63
546	Copertura	19, 135	0	-1247.84	122.21	254.72	1661.29	-1626.20	-1427.18
			75	-1247.84	122.21	991.56	1661.29	-556.27	-1427.18
			150	-1247.84	122.21	2237.50	1661.29	515.54	-1427.18
547	Copertura	134, 20	0	-1224.14	-10.09	-2228.60	1639.81	-420.99	-504.93
			75	-1224.14	-10.09	-998.79	1639.81	-643.99	-504.93
			150	-1224.14	-10.09	231.59	1639.81	-1002.65	-504.93
548	Copertura	21, 136	0	1212.81	123.37	175.37	-952.18	-1418.17	-1260.54
			75	1212.81	123.37	-623.06	-952.18	-476.44	-1260.54
			150	1212.81	123.37	-1335.82	-952.18	497.54	-1260.54
549	Copertura	138, 22	0	-1367.20	-9.74	1460.36	-1091.57	-401.69	257.07
			75	-1367.20	-9.74	641.69	-1091.57	-544.30	257.07
			150	-1367.20	-9.74	177.01	-1091.57	-729.61	257.07
550	Copertura	23, 141	0	599.19	123.72	125.32	566.24	-1446.83	-1284.64
			75	599.19	123.72	316.73	566.24	-483.59	-1284.64
			150	599.19	123.72	741.28	566.24	495.90	-1284.64
551	Copertura	142, 24	0	961.55	-10.54	-666.23	495.88	-400.03	280.62
			75	961.55	-10.54	-295.00	495.88	-551.38	280.62
			150	961.55	-10.54	94.80	495.88	-755.61	280.62
552	Copertura	25, 145	0	-1093.43	122.41	214.83	-1461.16	-1612.66	-1410.83
			75	-1093.43	122.41	-989.41	-1461.16	-554.81	-1410.83
			150	-1093.43	122.41	-2083.60	-1461.16	504.16	-1410.83
553	Copertura	146, 26	0	1271.56	-10.89	2327.59	-1760.41	-425.90	-521.41
			75	1271.56	-10.89	1007.41	-1760.41	-655.11	-521.41
			150	1271.56	-10.89	-313.88	-1760.41	-1025.13	-521.41
554	Copertura	150, 27	0	1630.98	-11.19	-1278.48	896.44	-432.21	-603.31
			75	1630.98	-11.19	-607.63	896.44	-691.09	-603.31
			150	1630.98	-11.19	-146.79	896.44	-1120.51	-603.31
555	Copertura	28, 149	0	1275.76	121.85	456.29	1008.16	-1707.22	-1472.82
			75	1275.76	121.85	793.46	1008.16	-603.22	-1472.82
			150	1275.76	121.85	1443.43	1008.16	503.51	-1472.82
556	Copertura	154, 29	0	-1482.67	-11.10	1695.28	-1253.36	-400.88	314.25
			75	-1482.67	-11.10	756.08	-1253.36	-558.62	314.25
			150	-1482.67	-11.10	-243.48	-1253.36	-784.83	314.25
557	Copertura	30, 153	0	1494.80	123.13	720.67	-1300.01	-1441.36	-1286.24
			75	1494.80	123.13	956.63	-1300.01	-476.80	-1286.24
			150	1494.80	123.13	-1624.11	-1300.01	488.25	-1286.24
558	Copertura	158, 31	0	-284.67	-11.02	954.44	-681.28	-394.64	250.28
			75	-284.67	-11.02	445.79	-681.28	-536.75	250.28
			150	-284.67	-11.02	-155.59	-681.28	-720.92	250.28
559	Copertura	32, 157	0	429.34	123.59	747.63	-904.49	-1449.16	-1280.98
			75	429.34	123.59	715.76	-904.49	-496.32	-1280.98
			150	429.34	123.59	-957.77	-904.49	486.73	-1280.98
560	Copertura	162, 33	0	907.65	-10.59	1671.20	-1232.90	-423.01	452.68
			75	907.65	-10.59	747.56	-1232.90	-629.28	452.68

			150	907.65	-10.59	-244.43	-1232.90	-950.46	452.68
561	Copertura	34, 161	0	-1406.31	122.94	875.30	-1320.22	-1586.13	-1400.47
			75	-1406.31	122.94	926.01	-1320.22	-536.06	-1400.47
			150	-1406.31	122.94	-1426.50	-1320.22	515.15	-1400.47
562	Copertura	166, 35	0	-335.17	-11.48	-1035.75	804.13	-446.24	-634.66
			75	-335.17	-11.48	-482.47	804.13	-717.46	-634.66
			150	-335.17	-11.48	-195.78	804.13	-1169.37	-634.66
563	Copertura	36, 165	0	681.84	122.96	916.38	-1237.32	-1752.14	-1523.08
			75	681.84	122.96	823.87	-1237.32	-611.10	-1523.08
			150	681.84	122.96	1174.18	-1237.32	535.38	-1523.08
564	Copertura	170, 37	0	-1265.11	-10.99	-1315.42	1021.55	-425.11	415.82
			75	-1265.11	-10.99	-585.83	1021.55	-614.60	415.82
			150	-1265.11	-10.99	-225.16	1021.55	-909.17	415.82
565	Copertura	38, 169	0	1363.04	122.78	989.61	-1317.00	-1526.02	-1358.28
			75	1363.04	122.78	842.25	-1317.00	-507.37	-1358.28
			150	1363.04	122.78	-1201.54	-1317.00	511.52	-1358.28
566	Copertura	175, 39	0	-1398.58	-10.89	1497.63	-1204.53	-396.67	238.32
			75	-1398.58	-10.89	595.63	-1204.53	-536.93	238.32
			150	-1398.58	-10.89	-314.48	-1204.53	-710.10	238.32
567	Copertura	40, 173	0	-630.75	123.04	1049.31	-1454.31	-1448.09	-1271.53
			75	-630.75	123.04	932.59	-1454.31	-495.11	-1271.53
			150	-630.75	123.04	-1366.07	-1454.31	485.19	-1271.53
568	Copertura	178, 41	0	4710.26	-10.20	1173.15	-1029.04	-366.22	331.98
			75	4710.26	-10.20	-505.44	-1029.04	-536.64	331.98
			150	4710.26	-10.20	-387.21	-1029.04	-777.74	331.98
569	Copertura	42, 177	0	5993.25	123.12	1365.47	-1792.31	-1540.39	-1372.19
			75	5993.25	123.12	813.72	-1792.31	-511.36	-1372.19
			150	5993.25	123.12	1541.53	-1792.31	518.13	-1372.19
570	Copertura	43, 181	0	-4758.55	123.78	-534.99	-1329.74	-1680.73	-1480.65
			75	-4758.55	123.78	-671.94	-1329.74	-571.10	-1480.65
			150	-4758.55	123.78	-1666.37	-1329.74	542.03	-1480.65
571	Copertura	182, 44	0	-4718.04	-10.91	1449.32	-1049.41	-397.66	-597.95
			75	-4718.04	-10.91	664.77	-1049.41	-666.74	-597.95
			150	-4718.04	-10.91	282.51	-1049.41	-1096.18	-597.95
572	Copertura	45, 185	0	1348.24	123.81	-207.74	1343.16	-1698.94	-1497.75
			75	1348.24	123.81	816.97	1343.16	-576.95	-1497.75
			150	1348.24	123.81	1822.87	1343.16	550.47	-1497.75
573	Copertura	186, 46	0	1176.49	-11.35	-1877.46	1405.65	-458.40	-581.47
			75	1176.49	-11.35	-823.43	1405.65	-704.07	-581.47
			150	1176.49	-11.35	243.61	1405.65	-1115.90	-581.47
574	Copertura	47, 189	0	-1171.38	124.21	-174.21	729.53	-1396.43	-1286.44
			75	-1171.38	124.21	393.25	729.53	-436.01	-1286.44
			150	-1171.38	124.21	940.20	729.53	533.93	-1286.44
575	Copertura	190, 48	0	889.64	-10.28	-838.00	649.38	-440.97	299.59
			75	889.64	-10.28	-350.97	649.38	-597.55	299.59
			150	889.64	-10.28	136.13	649.38	-813.45	299.59
576	Copertura	49, 193	0	-874.74	124.56	-154.49	729.36	-1455.75	-1310.28
			75	-874.74	124.56	449.90	729.36	-474.34	-1310.28
			150	-874.74	124.56	971.47	729.36	526.96	-1310.28
577	Copertura	195, 50	0	864.88	-9.37	1030.56	-764.51	-430.48	222.59
			75	864.88	-9.37	-457.21	-764.51	-584.93	222.59
			150	864.88	-9.37	-116.48	-764.51	-743.28	222.59
578	Copertura	51, 197	0	-1598.75	122.89	291.40	-1858.65	-1510.82	-1367.77
			75	-1598.75	122.89	-1103.26	-1858.65	-485.19	-1367.77
			150	-1598.75	122.89	-2497.17	-1858.65	541.19	-1367.77
579	Copertura	199, 52	0	1397.64	-10.52	2376.12	-1762.03	-446.05	414.37
			75	1397.64	-10.52	1054.60	-1762.03	-637.87	414.37
			150	1397.64	-10.52	-266.95	-1762.03	-931.07	414.37
580	Copertura	53, 201	0	-565.48	122.32	174.32	-1066.94	-1715.91	-1499.49
			75	-565.48	122.32	681.08	-1066.94	-592.44	-1499.49
			150	-565.48	122.32	-1480.25	-1066.94	535.85	-1499.49
581	Copertura	202, 54	0	-310.62	-12.09	-1398.56	1025.01	-442.47	-605.73
			75	-310.62	-12.09	-629.89	1025.01	-704.19	-605.73
			150	-310.62	-12.09	139.78	1025.01	-1135.20	-605.73
582	Copertura	55, 205	0	-1145.35	119.70	322.70	-1421.32	-1668.56	-1437.45
			75	-1145.35	119.70	-744.52	-1421.32	-590.51	-1437.45
			150	-1145.35	119.70	1810.29	-1421.32	489.07	-1437.45
583	Copertura	206, 56	0	1487.37	-13.25	1587.62	-1203.51	-381.49	413.85
			75	1487.37	-13.25	685.37	-1203.51	-584.48	413.85
			150	1487.37	-13.25	-227.80	-1203.51	-881.66	413.85
584	Copertura	57, 75	0	946.34	5.26	0.00	0.00	273.83	153.69
			118	946.34	5.26	0.00	0.00	93.82	153.69

			235	946.34	5.26	0.00	0.00	-87.90	153.69
585	Copertura	75, 58	0	-752.00	0.46	0.00	0.00	99.40	47.01
			118	-752.00	0.46	0.00	0.00	46.52	47.01
			235	-752.00	0.46	0.00	0.00	-25.04	47.01
586	Copertura	77, 61	0	431.97	0.98	0.00	0.00	38.33	26.24
			115	431.97	0.98	0.00	0.00	8.78	26.24
			231	431.97	0.98	0.00	0.00	-26.10	26.24
587	Copertura	62, 77	0	-429.86	1.12	0.00	0.00	-28.76	-22.11
			115	-429.86	1.12	0.00	0.00	4.28	-22.11
			231	-429.86	1.12	0.00	0.00	22.28	-22.11
588	Copertura	65, 78	0	446.14	1.26	0.00	0.00	-33.70	-22.55
			115	446.14	1.26	0.00	0.00	-12.25	-22.55
			231	446.14	1.26	0.00	0.00	-30.29	-22.55
589	Copertura	78, 66	0	-455.18	1.89	0.00	0.00	37.94	26.36
			115	-455.18	1.89	0.00	0.00	9.64	26.36
			231	-455.18	1.89	0.00	0.00	-29.60	26.36
590	Copertura	69, 76	0	503.20	1.44	0.00	0.00	26.33	20.90
			118	503.20	1.44	0.00	0.00	-8.37	20.90
			235	503.20	1.44	0.00	0.00	-25.25	20.90
591	Copertura	76, 70	0	-468.00	-0.88	0.00	0.00	-15.21	-20.56
			118	-468.00	-0.88	0.00	0.00	11.23	-20.56
			235	-468.00	-0.88	0.00	0.00	34.04	-20.56
592	Copertura	79, 81	0	-133.78	1.96	322.66	-402.44	-17.01	-16.99
			80	-133.78	1.96	3.01	-402.44	-19.93	-16.99
			159	-133.78	1.96	-317.22	-402.44	25.44	-16.99
593	Copertura	80, 82	0	-107.15	-0.31	270.36	-405.92	39.13	45.93
			66	-107.15	-0.31	2.33	-405.92	-9.39	45.93
			132	-107.15	-0.31	-265.79	-405.92	-23.73	45.93
594	Copertura	83, 84	0	-13.83	-0.51	253.18	-383.07	-27.20	-45.28
			66	-13.83	-0.51	-0.43	-383.07	-3.41	-45.28
			132	-13.83	-0.51	-252.47	-383.07	32.59	-45.28
595	Copertura	85, 86	0	-12.19	-0.34	249.32	-377.80	19.13	43.34
			66	-12.19	-0.34	-0.25	-377.80	-10.46	43.34
			132	-12.19	-0.34	-249.38	-377.80	-38.35	43.34
596	Copertura	87, 88	0	-15.02	0.22	246.83	-373.97	-2.78	-27.04
			66	-15.02	0.22	-0.60	-373.97	17.22	-27.04
			132	-15.02	0.22	-246.81	-373.97	35.06	-27.04
597	Copertura	89, 90	0	22.02	0.41	246.17	-373.82	-13.89	14.31
			66	22.02	0.41	-0.97	-373.82	-21.81	14.31
			132	22.02	0.41	-247.26	-373.82	-30.56	14.31
598	Copertura	91, 92	0	40.40	-0.91	238.15	-361.61	25.63	-5.26
			66	40.40	-0.91	-1.00	-361.61	24.44	-5.26
			132	40.40	-0.91	-239.17	-361.61	25.15	-5.26
599	Copertura	93, 94	0	-18.86	1.05	240.78	-365.58	-33.99	-24.34
			66	-18.86	1.05	-0.85	-365.58	-22.79	-24.34
			132	-18.86	1.05	-241.79	-365.58	13.69	-24.34
600	Copertura	95, 96	0	-15.14	-0.94	241.12	-365.53	-13.38	-25.70
			66	-15.14	-0.94	-0.99	-365.53	22.20	-25.70
			132	-15.14	-0.94	-241.37	-365.53	34.24	-25.70
601	Copertura	97, 106	0	-19.12	1.04	244.13	-369.60	-21.73	-9.40
			66	-19.12	1.04	-0.97	-369.60	-22.40	-9.40
			132	-19.12	1.04	-243.75	-369.60	-25.59	-9.40
602	Copertura	98, 99	0	-14.08	0.43	356.52	-541.86	-23.39	-25.78
			66	-14.08	0.43	-1.48	-541.86	-14.00	-25.78
			132	-14.08	0.43	-358.73	-541.86	20.12	-25.78
603	Copertura	100, 101	0	-3.54	-0.59	358.55	-543.28	-26.86	-25.48
			66	-3.54	-0.59	-0.40	-543.28	12.99	-25.48
			132	-3.54	-0.59	-358.58	-543.28	17.22	-25.48
604	Copertura	102, 103	0	-8.00	1.10	354.82	-537.16	-41.71	-48.36
			66	-8.00	1.10	-0.60	-537.16	-10.20	-48.36
			132	-8.00	1.10	-354.23	-537.16	22.50	-48.36
605	Copertura	104, 105	0	5.76	1.25	350.99	-531.40	36.99	47.97
			66	5.76	1.25	-0.85	-531.40	5.55	47.97
			132	5.76	1.25	-350.45	-531.40	26.42	47.97
606	Copertura	107, 108	0	21.26	0.37	251.56	-381.76	24.11	-6.95
			66	21.26	0.37	-0.60	-381.76	22.48	-6.95
			132	21.26	0.37	-252.36	-381.76	21.06	-6.95
607	Copertura	109, 110	0	88.49	-1.26	215.55	-270.47	-38.44	-18.66
			80	88.49	-1.26	-0.65	-270.47	27.05	-18.66
			159	88.49	-1.26	-214.51	-270.47	17.44	-18.66
608	Copertura	111, 112	0	51.18	1.48	351.14	-531.38	-37.55	-54.96
			66	51.18	1.48	-0.50	-531.38	-1.32	-54.96

			132	51.18	1.48	-350.81	-531.38	35.06	-54.96
609	Copertura	113, 114	0	-17.44	2.01	347.69	-526.55	30.70	49.92
			66	-17.44	2.01	0.39	-526.55	2.32	49.92
			132	-17.44	2.01	-347.35	-526.55	-35.21	49.92
610	Copertura	115, 116	0	-16.28	-1.85	350.33	-530.47	-9.78	-15.41
			66	-16.28	-1.85	-2.42	-530.47	-1.44	-15.41
			132	-16.28	-1.85	-349.89	-530.47	10.58	-15.41
611	Copertura	117, 118	0	-6.78	1.82	356.47	-540.35	-36.59	-48.40
			66	-6.78	1.82	-0.78	-540.35	-4.70	-48.40
			132	-6.78	1.82	-356.79	-540.35	-27.32	-48.40
612	Copertura	119, 120	0	-2.11	1.92	360.51	-546.57	-32.28	-50.09
			66	-2.11	1.92	-0.58	-546.57	1.41	-50.09
			132	-2.11	1.92	-360.97	-546.57	33.85	-50.09
613	Copertura	121, 122	0	26.19	1.33	359.71	-541.90	24.71	-49.55
			66	26.19	1.33	2.72	-541.90	8.51	-49.55
			132	26.19	1.33	-355.60	-541.90	40.91	-49.55
614	Copertura	124, 125	0	1202.31	-31.15	41.76	-32.03	47.82	-62.12
			99	1202.31	-31.15	12.90	-32.03	105.34	-62.12
			198	1202.31	-31.15	-28.26	-32.03	164.30	-62.12
615	Copertura	125, 127	0	362.48	-12.16	-2029.26	-240.26	560.51	59.15
			775	362.48	-12.16	254.42	-240.26	107.91	59.15
			1550	362.48	-12.16	-1706.22	-240.26	-356.77	59.15
616	Copertura	126, 127	0	-646.47	5.28	-28.85	18.17	21.28	-5.45
			99	-646.47	5.28	-12.66	18.17	16.49	-5.45
			198	-646.47	5.28	-15.87	18.17	13.06	-5.45
617	Copertura	128, 129	0	798.62	-30.94	44.12	-32.11	56.24	-61.80
			99	798.62	-30.94	13.50	-32.11	111.26	-61.80
			198	798.62	-30.94	-21.80	-32.11	168.25	-61.80
618	Copertura	129, 130	0	234.85	-11.36	-1675.15	215.42	604.31	65.73
			775	234.85	-11.36	-144.02	215.42	101.06	65.73
			1550	234.85	-11.36	1664.63	215.42	-415.19	65.73
619	Copertura	131, 130	0	923.93	6.26	44.94	-35.78	34.14	11.95
			99	923.93	6.26	-14.52	-35.78	22.33	11.95
			198	923.93	6.26	-27.39	-35.78	12.12	11.95
620	Copertura	132, 135	0	865.37	-30.87	60.94	-51.24	59.40	-62.14
			99	865.37	-30.87	10.74	-51.24	113.40	-62.14
			198	865.37	-30.87	-41.03	-51.24	168.60	-62.14
621	Copertura	133, 134	0	871.90	6.24	62.39	-51.18	32.03	10.75
			99	871.90	6.24	-13.89	-51.18	21.55	10.75
			198	871.90	6.24	-39.64	-51.18	11.52	10.75
622	Copertura	135, 134	0	192.38	-11.36	2270.19	-292.53	621.01	67.79
			775	192.38	-11.36	-110.95	-292.53	101.56	67.79
			1550	192.38	-11.36	-2264.36	-292.53	-430.23	67.79
623	Copertura	137, 136	0	1031.40	-30.77	49.31	-32.52	55.82	-61.67
			99	1031.40	-30.77	17.44	-32.52	111.40	-61.67
			198	1031.40	-30.77	-18.65	-32.52	170.43	-61.67
624	Copertura	136, 138	0	124.99	-11.29	-1352.23	182.70	606.33	65.75
			775	124.99	-11.29	-84.38	182.70	101.93	65.75
			1550	124.99	-11.29	1480.19	182.70	-412.98	65.75
625	Copertura	139, 138	0	1257.43	5.98	58.00	-40.47	25.10	8.44
			99	1257.43	5.98	17.89	-40.47	16.95	8.44
			198	1257.43	5.98	-26.53	-40.47	10.01	8.44
626	Copertura	140, 141	0	-1274.38	-30.92	-50.03	32.34	56.82	-61.97
			99	-1274.38	-30.92	-17.93	32.34	112.27	-61.97
			198	-1274.38	-30.92	14.17	32.34	170.61	-61.97
627	Copertura	141, 142	0	399.79	-11.17	735.04	-89.78	604.71	65.53
			775	399.79	-11.17	43.83	-89.78	102.41	65.53
			1550	399.79	-11.17	-656.69	-89.78	-411.15	65.53
628	Copertura	143, 142	0	1335.86	6.16	54.57	-34.95	27.27	10.05
			99	1335.86	6.16	19.90	-34.95	17.60	10.05
			198	1335.86	6.16	-14.83	-34.95	10.55	10.05
629	Copertura	144, 145	0	-1078.20	-31.00	-57.60	42.28	58.50	-60.02
			99	-1078.20	-31.00	20.38	42.28	112.96	-60.02
			198	-1078.20	-31.00	32.08	42.28	168.60	-60.02
630	Copertura	145, 146	0	-1060.60	-11.05	-2115.23	289.00	608.69	67.28
			775	-1060.60	-11.05	188.86	289.00	94.31	67.28
			1550	-1060.60	-11.05	2364.81	289.00	-434.60	67.28
631	Copertura	147, 146	0	-1298.81	6.43	-63.30	52.42	33.71	12.08
			99	-1298.81	6.43	-15.78	52.42	21.88	12.08
			198	-1298.81	6.43	41.33	52.42	11.81	12.08
632	Copertura	148, 149	0	-1136.99	-31.15	-64.61	50.44	61.97	-60.12
			99	-1136.99	-31.15	-16.80	50.44	114.26	-60.12

			198	-1136.99	-31.15	35.58	50.44	167.79	-60.12
633	Copertura	149, 150	0	821.63	-11.04	1478.83	-179.52	606.66	67.51
			775	821.63	-11.04	193.26	-179.52	90.63	67.51
			1550	821.63	-11.04	-1306.90	-179.52	-440.63	67.51
634	Copertura	151, 150	0	-846.10	6.66	-54.12	42.57	37.88	-14.47
			99	-846.10	6.66	-12.04	42.57	23.75	-14.47
			198	-846.10	6.66	30.52	42.57	12.67	-14.47
635	Copertura	152, 153	0	-1481.42	-30.84	-61.51	43.01	54.34	-59.73
			99	-1481.42	-30.84	-22.18	43.01	110.63	-59.73
			198	-1481.42	-30.84	29.46	43.01	169.09	-59.73
636	Copertura	153, 154	0	-284.21	-11.06	-1651.93	217.24	595.11	64.83
			775	-284.21	-11.06	212.17	217.24	98.49	64.83
			1551	-284.21	-11.06	1718.94	217.24	-410.53	64.83
637	Copertura	155, 154	0	-878.11	6.03	-43.63	31.90	29.39	11.59
			99	-878.11	6.03	-12.01	31.90	18.26	11.59
			198	-878.11	6.03	26.08	31.90	11.60	11.59
638	Copertura	156, 157	0	-764.95	-30.95	-46.72	37.60	58.07	-61.71
			99	-764.95	-30.95	-9.61	37.60	112.25	-61.71
			198	-764.95	-30.95	28.01	37.60	169.97	-61.71
639	Copertura	157, 158	0	-273.67	-11.08	-983.93	126.11	595.08	64.58
			775	-273.67	-11.08	83.67	126.11	99.59	64.58
			1551	-273.67	-11.08	972.31	126.11	-406.60	64.58
640	Copertura	159, 158	0	930.19	6.22	46.54	-33.79	29.84	12.78
			99	930.19	6.22	13.06	-33.79	17.84	12.78
			198	930.19	6.22	20.95	-33.79	11.90	12.78
641	Copertura	160, 161	0	-850.93	-30.93	-39.72	33.31	57.42	-60.70
			99	-850.93	-30.93	-13.88	33.31	112.58	-60.70
			198	-850.93	-30.93	27.37	33.31	168.69	-60.70
642	Copertura	161, 162	0	280.41	-10.95	-1449.38	202.96	621.02	68.01
			776	280.41	-10.95	-140.52	202.96	98.83	68.01
			1551	280.41	-10.95	1699.86	202.96	-434.17	68.01
643	Copertura	163, 162	0	877.84	6.48	43.35	36.90	35.13	-14.23
			99	877.84	6.48	11.33	36.90	21.46	-14.23
			198	877.84	6.48	30.04	36.90	12.08	-14.23
644	Copertura	164, 165	0	-940.92	-31.20	-54.78	42.88	60.63	-61.46
			99	-940.92	-31.20	-14.48	42.88	114.58	-61.46
			198	-940.92	-31.20	30.74	42.88	169.52	-61.46
645	Copertura	165, 166	0	164.60	-11.02	1200.97	-144.48	639.42	70.50
			776	164.60	-11.02	-88.83	-144.48	99.10	70.50
			1551	164.60	-11.02	-1041.09	-144.48	-454.90	70.50
646	Copertura	167, 166	0	617.49	6.92	16.83	-13.96	39.07	-15.25
			99	617.49	6.92	9.40	-13.96	24.18	-15.25
			198	617.49	6.92	-11.60	-13.96	13.51	-15.25
647	Copertura	168, 169	0	-1156.34	-30.80	-64.47	49.13	56.99	-60.85
			99	-1156.34	-30.80	-18.48	49.13	111.71	-60.85
			198	-1156.34	-30.80	33.48	49.13	168.37	-60.85
648	Copertura	169, 170	0	-273.16	-11.16	-1202.40	163.30	617.18	67.71
			776	-273.16	-11.16	-112.62	163.30	98.44	67.71
			1552	-273.16	-11.16	-1332.39	163.30	-433.76	67.71
649	Copertura	171, 170	0	510.30	6.33	24.77	-17.83	32.60	-12.71
			99	510.30	6.33	7.37	-17.83	20.69	-12.71
			198	510.30	6.33	-17.66	-17.83	13.54	-12.71
650	Copertura	172, 173	0	-1486.77	-30.82	-62.10	43.70	54.72	-60.13
			99	-1486.77	-30.82	-22.81	43.70	110.91	-60.13
			198	-1486.77	-30.82	26.23	43.70	169.34	-60.13
651	Copertura	173, 175	0	-1207.93	-11.10	-1361.97	185.04	592.97	64.53
			776	-1207.93	-11.10	-96.55	185.04	98.07	64.53
			1552	-1207.93	-11.10	1509.56	185.04	-408.58	64.53
652	Copertura	174, 175	0	863.17	6.16	31.63	-19.32	29.69	-12.55
			99	863.17	6.16	12.66	-19.32	17.87	-12.55
			198	863.17	6.16	-17.50	-19.32	12.38	-12.55
653	Copertura	176, 177	0	-1449.71	-30.83	-96.64	74.56	53.56	-63.87
			99	-1449.71	-30.83	-24.09	74.56	110.41	-63.87
			198	-1449.71	-30.83	51.60	74.56	169.12	-63.87
654	Copertura	177, 178	0	4745.30	-11.08	1542.45	-170.78	625.14	64.48
			776	4745.30	-11.08	-469.36	-170.78	127.27	64.48
			1552	4745.30	-11.08	1211.50	-170.78	-375.95	64.48
655	Copertura	179, 178	0	1714.33	5.72	78.64	-57.59	25.02	8.75
			99	1714.33	5.72	22.36	-57.59	16.53	8.75
			198	1714.33	5.72	38.56	-57.59	9.20	8.75
656	Copertura	180, 181	0	-1103.27	-31.02	-69.81	52.17	55.16	-64.92
			99	-1103.27	-31.02	18.17	52.17	112.23	-64.92

			198	-1103.27	-31.02	-33.88	52.17	170.59	-64.92
657	Copertura	181, 182	0	-4358.08	-11.33	-1689.02	204.29	648.31	67.87
			775	-4358.08	-11.33	373.08	204.29	129.40	67.87
			1550	-4358.08	-11.33	1479.68	204.29	-404.61	67.87
658	Copertura	183, 182	0	1259.08	6.21	56.68	-40.94	29.70	8.96
			99	1259.08	6.21	16.21	-40.94	20.86	8.96
			198	1259.08	6.21	30.49	-40.94	12.10	8.96
659	Copertura	184, 185	0	619.99	-30.94	-40.90	37.50	57.52	-61.68
			99	619.99	-30.94	-4.52	37.50	114.00	-61.68
			198	619.99	-30.94	33.55	37.50	171.99	-61.68
660	Copertura	185, 186	0	1015.97	-11.51	1848.00	-242.16	655.53	72.32
			775	1015.97	-11.51	122.54	-242.16	100.76	72.32
			1550	1015.97	-11.51	-1906.43	-242.16	-465.89	72.32
661	Copertura	187, 186	0	-1372.23	6.63	-71.32	53.36	34.72	11.36
			99	-1372.23	6.63	-18.46	53.36	23.70	11.36
			198	-1372.23	6.63	34.69	53.36	16.24	11.36
662	Copertura	188, 189	0	-852.18	-30.49	-25.45	14.16	55.00	-62.19
			99	-852.18	-30.49	-12.45	14.16	112.25	-62.19
			198	-852.18	-30.49	6.74	14.16	171.93	-62.19
663	Copertura	189, 190	0	300.16	-11.48	939.65	-113.98	643.28	70.76
			775	300.16	-11.48	110.72	-113.98	100.55	70.76
			1550	300.16	-11.48	-827.26	-113.98	-453.75	70.76
664	Copertura	191, 190	0	-1364.85	6.40	-49.76	30.52	31.40	-11.66
			99	-1364.85	6.40	-19.47	30.52	20.58	-11.66
			198	-1364.85	6.40	10.83	30.52	15.45	-11.66
665	Copertura	192, 193	0	-983.69	-30.58	44.33	-32.99	54.28	-62.48
			99	-983.69	-30.58	-14.36	-32.99	112.62	-62.48
			198	-983.69	-30.58	21.49	-32.99	173.15	-62.48
666	Copertura	193, 195	0	-108.65	-11.56	988.61	-131.41	638.13	69.89
			775	-108.65	-11.56	61.68	-131.41	101.75	69.89
			1550	-108.65	-11.56	1048.61	-131.41	-445.27	69.89
667	Copertura	194, 195	0	-1009.08	6.44	-46.24	33.01	30.86	12.45
			99	-1009.08	6.44	-13.50	33.01	19.74	12.45
			198	-1009.08	6.44	20.04	33.01	14.47	12.45
668	Copertura	196, 197	0	1015.08	-30.44	72.93	-61.94	56.25	-62.56
			99	1015.08	-30.44	11.50	-61.94	112.59	-62.56
			198	1015.08	-30.44	-50.04	-61.94	170.26	-62.56
669	Copertura	197, 199	0	-122.45	-11.55	-2541.75	319.59	649.13	71.39
			775	-122.45	-11.55	77.96	319.59	101.63	71.39
			1550	-122.45	-11.55	2411.98	319.59	-457.68	71.39
670	Copertura	198, 199	0	-680.61	6.39	-48.58	43.65	35.47	12.89
			99	-680.61	6.39	7.77	43.65	23.08	12.89
			198	-680.61	6.39	38.67	43.65	14.27	12.89
671	Copertura	200, 201	0	1216.75	-30.79	68.51	-51.55	55.50	-62.57
			99	1216.75	-30.79	17.70	-51.55	111.88	-62.57
			198	1216.75	-30.79	-35.46	-51.55	170.24	-62.57
672	Copertura	201, 202	0	-276.99	-11.73	-1515.44	-185.01	639.02	70.20
			775	-276.99	-11.73	186.31	-185.01	101.14	70.20
			1550	-276.99	-11.73	-1421.00	-185.01	-449.69	70.20
673	Copertura	203, 202	0	590.89	6.49	40.68	-32.97	36.38	-12.01
			99	590.89	6.49	8.42	-32.97	24.85	-12.01
			198	590.89	6.49	-25.06	-32.97	17.51	-12.01
674	Copertura	204, 205	0	-1516.09	-30.96	-44.95	33.03	48.94	-63.45
			99	-1516.09	-30.96	17.47	33.03	106.41	-63.45
			198	-1516.09	-30.96	22.23	33.03	165.18	-63.45
675	Copertura	205, 206	0	-367.03	-11.87	-1802.36	218.74	592.75	63.30
			775	-367.03	-11.87	-222.09	218.74	107.62	63.30
			1550	-367.03	-11.87	1601.71	218.74	-388.84	63.30
676	Copertura	207, 206	0	634.77	5.98	22.21	-18.06	36.69	14.61
			99	634.77	5.98	12.17	-18.06	22.35	14.61
			198	634.77	5.98	-17.04	-18.06	11.47	14.61
677	Copertura	79	0	712.09	-34.10	-222.72	331.46	-103.84	-207.48
			125	712.09	-34.10	192.49	331.46	177.31	-207.48
			250	712.09	-34.10	606.49	331.46	421.39	-207.48
678	Copertura	124	0	5715.21	4.49	-1254.05	1357.46	-514.40	-422.96
			155	5715.21	4.49	850.08	1357.46	262.00	-422.96
			310	5715.21	4.49	2954.12	1357.46	863.11	-422.96
679	Copertura	80	0	882.01	-15.45	52.34	257.12	-406.55	210.59
			45	882.01	-15.45	168.03	257.12	-449.24	210.59
			90	882.01	-15.45	283.72	257.12	-494.96	210.59
680	Copertura	128	0	-1545.41	-9.49	-1265.25	1350.22	-548.90	-254.65
			155	-1545.41	-9.49	827.66	1350.22	-237.83	-254.65

			310	-1545.41	-9.49	2920.48	1350.22	304.31	-254.65
681	Copertura	82	0	823.31	7.67	5.23	373.25	-313.36	272.85
			43	823.31	7.67	161.21	373.25	-380.05	272.85
			85	823.31	7.67	320.42	373.25	-451.52	272.85
682	Copertura	132	0	1879.03	11.29	-1274.19	1360.29	-630.50	-227.20
			155	1879.03	11.29	834.32	1360.29	-299.83	-227.20
			310	1879.03	11.29	2942.73	1360.29	229.86	-227.20
683	Copertura	83	0	1103.99	-7.43	34.88	290.89	-243.45	261.62
			43	1103.99	-7.43	158.85	290.89	-301.44	261.62
			85	1103.99	-7.43	282.92	290.89	-365.77	261.62
684	Copertura	137	0	-3001.77	11.11	-1277.20	1363.55	-585.75	-388.87
			155	-3001.77	11.11	836.35	1363.55	-315.92	-388.87
			310	-3001.77	11.11	2949.83	1363.55	682.97	-388.87
685	Copertura	84	0	1513.22	-11.73	29.15	299.27	-546.68	398.66
			43	1513.22	-11.73	156.39	299.27	-665.84	398.66
			85	1513.22	-11.73	284.05	299.27	-787.29	398.66
686	Copertura	140	0	-1577.76	-11.97	-1277.92	1364.68	667.00	465.51
			155	-1577.76	-11.97	837.38	1364.68	-236.40	465.51
			310	-1577.76	-11.97	2952.62	1364.68	-798.94	465.51
687	Copertura	85	0	1378.56	5.27	31.55	291.92	-520.93	463.28
			43	1378.56	5.27	155.86	291.92	-680.41	463.28
			85	1378.56	5.27	280.37	291.92	-841.82	463.28
688	Copertura	144	0	-3596.48	8.65	-1278.00	1363.51	692.54	425.62
			155	-3596.48	8.65	835.50	1363.51	-280.01	425.62
			310	-3596.48	8.65	2948.93	1363.51	-735.12	425.62
689	Copertura	86	0	1687.62	15.80	31.83	289.40	269.25	-389.31
			43	1687.62	15.80	155.26	289.40	354.43	-389.31
			85	1687.62	15.80	278.71	289.40	490.23	-389.31
690	Copertura	87	0	1346.75	-5.54	31.19	292.38	217.47	-290.90
			43	1346.75	-5.54	154.96	292.38	315.48	-290.90
			85	1346.75	-5.54	279.67	292.38	415.89	-290.90
691	Copertura	148	0	2961.78	14.98	-1272.80	1354.55	751.21	439.94
			155	2961.78	14.98	826.77	1354.55	-103.86	439.94
			310	2961.78	14.98	2926.32	1354.55	-615.15	439.94
692	Copertura	88	0	1422.12	-18.04	32.37	285.41	398.72	-293.96
			43	1422.12	-18.04	153.79	285.41	470.21	-293.96
			85	1422.12	-18.04	275.23	285.41	578.43	-293.96
693	Copertura	152	0	-1107.40	7.48	-1278.15	1366.62	649.77	539.52
			155	-1107.40	7.48	841.55	1366.62	227.38	539.52
			310	-1107.40	7.48	2958.50	1366.62	-1027.25	539.52
694	Copertura	89	0	979.34	-11.68	26.91	298.13	238.90	333.74
			43	979.34	-11.68	153.79	298.13	363.81	333.74
			85	979.34	-11.68	280.93	298.13	-497.87	333.74
695	Copertura	156	0	-799.70	-13.81	-1277.59	1362.20	303.90	159.17
			155	-799.70	-13.81	834.27	1362.20	87.42	159.17
			310	-799.70	-13.81	2945.25	1362.20	-257.28	159.17
696	Copertura	90	0	964.79	19.20	33.65	285.52	313.82	290.25
			43	964.79	19.20	155.44	285.52	-369.72	290.25
			85	964.79	19.20	277.23	285.52	-430.61	290.25
697	Copertura	160	0	-320.24	7.35	-1282.03	1364.07	-92.30	174.54
			155	-320.24	7.35	833.72	1364.07	-188.97	174.54
			310	-320.24	7.35	2946.60	1364.07	-457.47	174.54
698	Copertura	91	0	377.46	17.65	30.02	284.74	-377.74	211.36
			43	377.46	17.65	148.77	284.74	-467.42	211.36
			85	377.46	17.65	270.14	284.74	-557.26	211.36
699	Copertura	164	0	253.00	9.66	-1284.53	1365.12	-188.22	-108.22
			155	253.00	9.66	833.09	1365.12	185.02	-108.22
			310	253.00	9.66	2947.37	1365.12	246.56	-108.22
700	Copertura	92	0	-560.71	-20.33	36.00	268.13	-312.59	151.23
			43	-560.71	-20.33	150.12	268.13	-361.65	151.23
			85	-560.71	-20.33	264.48	268.13	-410.79	151.23
701	Copertura	168	0	628.45	11.12	-1286.95	1366.24	-264.80	-166.21
			155	628.45	11.12	832.43	1366.24	186.34	-166.21
			310	628.45	11.12	2948.55	1366.24	419.49	-166.21
702	Copertura	93	0	-1073.80	-23.86	34.40	275.15	-397.18	277.85
			43	-1073.80	-23.86	148.94	275.15	-503.79	277.85
			85	-1073.80	-23.86	266.27	275.15	-610.87	277.85
703	Copertura	172	0	446.82	10.11	-1288.89	1370.47	-246.25	-269.69
			155	446.82	10.11	836.56	1370.47	-270.36	-269.69
			310	446.82	10.11	2959.60	1370.47	683.34	-269.69
704	Copertura	94	0	-1122.45	10.09	32.63	287.22	-394.07	508.90
			43	-1122.45	10.09	155.13	287.22	-597.14	508.90

			85	-1122.45	10.09	277.65	287.22	-800.47	508.90
705	Copertura	176	0	-2197.91	9.34	-1289.04	1365.72	-412.54	-92.79
			155	-2197.91	9.34	829.43	1365.72	-272.06	-92.79
			310	-2197.91	9.34	2944.72	1365.72	136.25	-92.79
706	Copertura	180	0	708.17	9.04	-1268.99	1350.24	755.12	359.96
			155	708.17	9.04	824.69	1350.24	198.32	359.96
			310	708.17	9.04	2916.77	1350.24	-361.99	359.96
707	Copertura	95	0	-1266.40	9.86	35.24	277.11	-219.39	362.41
			43	-1266.40	9.86	151.82	277.11	-372.78	362.41
			85	-1266.40	9.86	268.64	277.11	-526.88	362.41
708	Copertura	184	0	3062.36	7.30	-1272.75	1360.54	436.87	173.30
			155	3062.36	7.30	836.48	1360.54	238.15	173.30
			310	3062.36	7.30	2944.94	1360.54	-183.06	173.30
709	Copertura	96	0	-1653.67	-21.55	36.02	290.70	-455.58	-456.63
			43	-1653.67	-21.55	155.31	290.70	592.96	-456.63
			85	-1653.67	-21.55	279.20	290.70	747.79	-456.63
710	Copertura	188	0	-1589.09	-9.32	-1272.16	1358.05	387.13	362.53
			155	-1589.09	-9.32	832.95	1358.05	193.28	362.53
			310	-1589.09	-9.32	2937.81	1358.05	-743.67	362.53
711	Copertura	97	0	-1311.91	-18.34	34.14	288.36	599.29	-483.22
			43	-1311.91	-18.34	155.77	288.36	800.46	-483.22
			85	-1311.91	-18.34	278.75	288.36	1001.71	-483.22
712	Copertura	192	0	3006.03	9.71	-1271.10	1357.46	-502.69	384.06
			155	3006.03	9.71	832.99	1357.46	-187.31	384.06
			310	3006.03	9.71	2937.04	1357.46	-703.33	384.06
713	Copertura	106	0	-1584.74	19.52	34.93	282.60	458.62	-346.05
			43	-1584.74	19.52	155.16	282.60	584.94	-346.05
			85	-1584.74	19.52	275.40	282.60	719.09	-346.05
714	Copertura	196	0	-2153.61	8.26	-1268.37	1354.52	-718.78	-308.36
			155	-2153.61	8.26	831.19	1354.52	-243.70	-308.36
			310	-2153.61	8.26	2930.68	1354.52	-296.84	-308.36
715	Copertura	107	0	-1057.34	18.53	31.95	301.39	152.98	-199.63
			43	-1057.34	18.53	158.56	301.39	97.26	-199.63
			85	-1057.34	18.53	287.11	301.39	101.22	-199.63
716	Copertura	200	0	1910.26	-7.94	-1260.46	1345.20	-785.79	-424.64
			155	1910.26	-7.94	824.67	1345.20	160.77	-424.64
			310	1910.26	-7.94	2909.70	1345.20	598.57	-424.64
717	Copertura	108	0	729.36	-15.41	38.55	285.59	119.13	181.26
			43	729.36	-15.41	160.34	285.59	81.75	181.26
			85	729.36	-15.41	282.16	285.59	82.13	181.26
718	Copertura	204	0	-5989.01	4.60	-1249.90	1352.99	626.06	561.19
			155	-5989.01	4.60	847.30	1352.99	254.13	561.19
			310	-5989.01	4.60	2944.41	1352.99	-1118.24	561.19
719	Copertura	109	0	-959.93	-22.60	39.36	327.99	-400.63	200.91
			43	-959.93	-22.60	174.54	327.99	-452.32	200.91
			85	-959.93	-22.60	314.32	327.99	-505.73	200.91
720	Copertura	110	0	-617.70	-37.64	247.46	257.98	-211.61	161.37
			43	-617.70	-37.64	355.04	257.98	-279.83	161.37
			85	-617.70	-37.64	464.20	257.98	-348.29	161.37
721	Copertura	14	0	517.19	46.79	-702.18	423.84	-452.04	-185.50
			95	517.19	46.79	-299.96	423.84	-276.40	-185.50
			190	517.19	46.79	117.77	423.84	-102.78	-185.50
722	Copertura	15	0	5009.50	-13.00	-2796.57	1246.64	184.65	473.75
			65	5009.50	-13.00	-1996.78	1246.64	-168.10	473.75
			130	5009.50	-13.00	-1200.06	1246.64	-472.70	473.75
723	Copertura	16	0	1067.47	-9.79	-288.80	184.77	38.25	308.40
			65	1067.47	-9.79	-168.80	184.77	-187.75	308.40
			130	1067.47	-9.79	-49.30	184.77	-387.97	308.40
724	Copertura	17	0	-1544.00	-21.73	-2795.91	1240.97	-23.40	371.37
			65	-1544.00	-21.73	-2000.19	1240.97	-263.57	371.37
			130	-1544.00	-21.73	-1207.88	1240.97	-504.97	371.37
725	Copertura	18	0	337.19	-12.48	-352.91	258.46	37.17	386.65
			65	337.19	-12.48	-184.98	258.46	245.08	386.65
			130	337.19	-12.48	-18.37	258.46	495.96	386.65
726	Copertura	19	0	1265.39	-18.19	-2818.27	1252.98	114.14	421.90
			65	1265.39	-18.19	-2014.49	1252.98	-298.92	421.90
			130	1265.39	-18.19	-1213.04	1252.98	-569.90	421.90
727	Copertura	20	0	995.10	-10.15	-350.74	255.56	85.58	-413.79
			65	995.10	-10.15	-184.65	255.56	328.79	-413.79
			130	995.10	-10.15	-19.75	255.56	596.61	-413.79
728	Copertura	21	0	-2738.05	-16.31	-2829.06	1257.86	-90.04	343.89
			65	-2738.05	-16.31	-2021.19	1257.86	-313.21	343.89

			130	-2738.05	-16.31	-1217.58	1257.86	-536.68	343.89
729	Copertura	22	0	708.83	-7.42	-355.37	259.71	84.27	-442.58
			65	708.83	-7.42	-186.63	259.71	325.73	-442.58
			130	708.83	-7.42	-19.27	259.71	612.10	-442.58
730	Copertura	23	0	-687.43	-16.21	-2832.80	1260.48	45.64	497.48
			65	-687.43	-16.21	-2023.59	1260.48	294.17	497.48
			130	-687.43	-16.21	-1221.11	1260.48	617.01	497.48
731	Copertura	24	0	870.70	-7.92	-353.11	256.63	-33.34	-497.16
			65	870.70	-7.92	-186.42	256.63	329.45	-497.16
			130	870.70	-7.92	-21.59	256.63	652.54	-497.16
732	Copertura	25	0	-3264.06	-18.58	-2833.54	1259.44	-84.82	-446.34
			65	-3264.06	-18.58	-2021.57	1259.44	346.95	-446.34
			130	-3264.06	-18.58	-1218.00	1259.44	635.01	-446.34
733	Copertura	26	0	847.38	-12.29	-352.37	258.52	69.32	572.31
			65	847.38	-12.29	-184.37	258.52	-347.14	572.31
			130	847.38	-12.29	-18.09	258.52	-718.50	572.31
734	Copertura	27	0	977.71	-14.11	-350.43	258.78	-98.49	324.19
			65	977.71	-14.11	-183.83	258.78	-306.45	324.19
			130	977.71	-14.11	-18.97	258.78	-516.66	324.19
735	Copertura	28	0	2514.26	-18.91	-2825.55	1251.48	-420.27	-510.00
			65	2514.26	-18.91	-2015.97	1251.48	-521.80	-510.00
			130	2514.26	-18.91	-1213.29	1251.48	702.70	-510.00
736	Copertura	29	0	892.96	-10.91	-348.93	259.40	-96.02	255.99
			65	892.96	-10.91	-182.53	259.40	-260.87	255.99
			130	892.96	-10.91	-26.87	259.40	-426.92	255.99
737	Copertura	30	0	796.11	-14.86	-2838.68	1258.54	-664.37	-634.20
			65	796.11	-14.86	-2024.32	1258.54	-590.01	-634.20
			130	796.11	-14.86	-1218.99	1258.54	619.57	-634.20
738	Copertura	31	0	542.84	-11.10	-347.69	258.97	-83.82	-354.91
			65	542.84	-11.10	-181.66	258.97	295.67	-354.91
			130	542.84	-11.10	-27.82	258.97	524.16	-354.91
739	Copertura	32	0	-385.11	-16.43	-2827.28	1248.70	-712.47	-542.66
			65	-385.11	-16.43	-2020.10	1248.70	-484.98	-542.66
			130	-385.11	-16.43	-1220.59	1248.70	302.32	-542.66
740	Copertura	33	0	-534.86	-11.68	-334.41	241.01	-91.32	-366.59
			65	-534.86	-11.68	-181.62	241.01	260.34	-366.59
			130	-534.86	-11.68	-30.72	241.01	494.61	-366.59
741	Copertura	34	0	609.81	-17.77	-2823.98	1245.95	-792.36	-544.09
			65	609.81	-17.77	-2019.21	1245.95	-446.21	-544.09
			130	609.81	-17.77	-1220.54	1245.95	-124.81	-544.09
742	Copertura	35	0	449.63	-16.23	-357.92	266.45	-99.52	-189.99
			65	449.63	-16.23	-186.08	266.45	145.23	-189.99
			130	449.63	-16.23	-17.05	266.45	217.99	-189.99
743	Copertura	36	0	793.68	-21.28	-2823.62	1246.28	-845.08	-664.49
			65	793.68	-21.28	-2017.80	1246.28	-498.31	-664.49
			130	793.68	-21.28	-1223.86	1246.28	-196.47	-664.49
744	Copertura	37	0	-536.12	-13.35	-347.34	256.10	-107.29	-227.67
			65	-536.12	-13.35	-180.88	256.10	144.50	-227.67
			130	-536.12	-13.35	-19.30	256.10	249.72	-227.67
745	Copertura	38	0	1169.65	-18.01	-2819.76	1242.16	-924.39	-778.78
			65	1169.65	-18.01	-2015.88	1242.16	-534.94	-778.78
			130	1169.65	-18.01	-1226.52	1242.16	-237.31	-778.78
746	Copertura	39	0	600.63	-11.43	-346.58	255.15	-100.16	-296.61
			65	600.63	-11.43	-180.74	255.15	166.11	-296.61
			130	600.63	-11.43	-16.87	255.15	337.64	-296.61
747	Copertura	40	0	896.79	-16.47	-2816.91	1239.73	-1007.79	-870.58
			65	896.79	-16.47	-2015.34	1239.73	-543.32	-870.58
			130	896.79	-16.47	-1228.99	1239.73	-199.83	-870.58
748	Copertura	41	0	-833.13	-7.31	-350.91	262.25	-245.49	-682.65
			65	-833.13	-7.31	-180.72	262.25	451.63	-682.65
			130	-833.13	-7.31	-30.03	262.25	855.70	-682.65
749	Copertura	42	0	-1462.56	-18.56	-2800.25	1225.37	-1055.59	-996.09
			65	-1462.56	-18.56	-2006.57	1225.37	-547.83	-996.09
			130	-1462.56	-18.56	-1229.83	1225.37	-334.41	-996.09
750	Copertura	43	0	516.19	-21.47	-2815.01	1246.77	-104.26	-492.80
			65	516.19	-21.47	-2007.71	1246.77	367.74	-492.80
			130	516.19	-21.47	-1212.52	1246.77	685.57	-492.80
751	Copertura	44	0	654.80	-13.42	-353.30	262.18	153.36	502.68
			65	654.80	-13.42	-182.89	262.18	334.01	502.68
			130	654.80	-13.42	-17.94	262.18	655.84	502.68
752	Copertura	45	0	2655.40	-22.85	-2830.44	1256.87	127.01	344.66
			65	2655.40	-22.85	-2015.93	1256.87	179.68	344.66

			130	2655.40	-22.85	-1213.65	1256.87	396.14	344.66
753	Copertura	46	0	-744.72	17.38	-353.79	262.15	-32.25	562.86
			65	-744.72	17.38	-183.78	262.15	-392.06	562.86
			130	-744.72	17.38	-18.73	262.15	-757.85	562.86
754	Copertura	47	0	-1097.47	-17.00	-2827.74	1255.36	-60.93	-291.26
			65	-1097.47	-17.00	-2014.84	1255.36	172.71	-291.26
			130	-1097.47	-17.00	-1215.69	1255.36	361.70	-291.26
755	Copertura	48	0	331.78	-12.66	-354.84	262.66	-21.88	479.95
			65	331.78	-12.66	-185.43	262.66	-307.98	479.95
			130	331.78	-12.66	-20.77	262.66	-619.91	479.95
756	Copertura	49	0	2481.35	-18.95	-2825.88	1255.42	93.25	324.53
			65	2481.35	-18.95	-2013.08	1255.42	-270.72	324.53
			130	2481.35	-18.95	-1213.11	1255.42	-458.88	324.53
757	Copertura	50	0	-773.65	-13.79	-358.59	265.57	-48.81	339.98
			65	-773.65	-13.79	-186.14	265.57	-256.06	339.98
			130	-773.65	-13.79	-19.16	265.57	-476.88	339.98
758	Copertura	51	0	-1471.31	-18.25	-2814.86	1250.50	-133.38	443.64
			65	-1471.31	-18.25	-2006.87	1250.50	-359.60	443.64
			130	-1471.31	-18.25	-1209.11	1250.50	-645.92	443.64
759	Copertura	52	0	-734.18	-11.67	-360.63	266.61	-97.61	326.02
			65	-734.18	-11.67	-187.34	266.61	-245.62	326.02
			130	-734.18	-11.67	-19.74	266.61	-456.67	326.02
760	Copertura	53	0	1485.69	-23.70	-2789.60	1236.38	-66.17	501.07
			65	1485.69	-23.70	-1993.00	1236.38	-391.71	501.07
			130	1485.69	-23.70	-1203.62	1236.38	-717.39	501.07
761	Copertura	54	0	-894.25	-18.09	-348.20	256.01	37.36	-295.85
			65	-894.25	-18.09	-184.84	256.01	220.56	-295.85
			130	-894.25	-18.09	-22.98	256.01	412.57	-295.85
762	Copertura	55	0	-5110.29	-14.87	-2788.61	1242.55	-170.85	-569.90
			65	-5110.29	-14.87	-1990.12	1242.55	-214.61	-569.90
			130	-5110.29	-14.87	-1195.54	1242.55	581.29	-569.90
763	Copertura	56	0	-929.47	-8.81	-347.68	255.91	-45.21	-205.56
			65	-929.47	-8.81	-182.69	255.91	147.53	-205.56
			130	-929.47	-8.81	-19.50	255.91	280.83	-205.56
764	Copertura	70	0	-485.22	42.28	-654.89	304.73	389.79	165.63
			95	-485.22	42.28	-365.52	304.73	233.43	165.63
			190	-485.22	42.28	-77.02	304.73	80.99	165.63
765	Copertura	81	0	469.49	-25.41	-243.84	354.05	-326.87	240.46
			80	469.49	-25.41	39.60	354.05	-326.13	240.46
			160	469.49	-25.41	322.69	354.05	-408.08	240.46
766	Copertura	126	0	868.23	11.53	-49.90	203.67	-416.81	249.32
			30	868.23	11.53	25.17	203.67	-370.99	249.32
			60	868.23	11.53	75.38	203.67	-325.99	249.32
767	Copertura	98	0	875.26	-16.52	-201.60	284.97	-426.75	289.21
			82	875.26	-16.52	33.39	284.97	-300.32	289.21
			165	875.26	-16.52	267.79	284.97	-312.98	289.21
768	Copertura	99	0	958.15	19.78	-212.86	304.01	522.83	283.72
			82	958.15	19.78	38.03	304.01	-319.96	283.72
			165	958.15	19.78	287.95	304.01	-243.46	283.72
769	Copertura	100	0	1373.82	20.91	-204.65	294.97	-392.71	436.98
			82	1373.82	20.91	38.51	294.97	-295.53	436.98
			165	1373.82	20.91	281.21	294.97	-547.15	436.98
770	Copertura	101	0	1313.17	-15.55	-204.57	294.58	-415.16	505.11
			82	1313.17	-15.55	38.38	294.58	-214.10	505.11
			165	1313.17	-15.55	280.68	294.58	-520.97	505.11
771	Copertura	102	0	1541.43	-23.23	-204.90	295.10	-563.66	-412.50
			82	1541.43	-23.23	38.47	295.10	-359.57	-412.50
			165	1541.43	-23.23	281.19	295.10	269.13	-412.50
772	Copertura	103	0	-1224.80	4.97	-203.43	291.69	-397.18	-331.11
			82	-1224.80	4.97	38.33	291.69	-135.48	-331.11
			165	-1224.80	4.97	277.09	291.69	217.43	-331.11
773	Copertura	104	0	1321.68	17.07	-203.72	293.14	-265.86	-339.45
			82	1321.68	17.07	38.18	293.14	300.25	-339.45
			165	1321.68	17.07	279.16	293.14	398.79	-339.45
774	Copertura	105	0	-839.63	-3.57	-200.13	286.36	366.34	349.68
			82	-839.63	-3.57	37.85	286.36	-130.90	349.68
			165	-839.63	-3.57	272.45	286.36	238.77	349.68
775	Copertura	111	0	875.08	-11.55	-205.26	304.71	369.59	296.49
			80	875.08	-11.55	38.10	304.71	-243.98	296.49
			160	875.08	-11.55	280.91	304.71	314.05	296.49
776	Copertura	112	0	-257.02	9.09	-186.65	274.53	135.81	277.34
			82	-257.02	9.09	40.07	274.53	159.13	277.34

			165	-257.02	9.09	265.58	274.53	-378.16	277.34
777	Copertura	113	0	426.80	5.05	-197.74	287.00	182.03	176.87
			82	426.80	5.05	38.80	287.00	175.27	176.87
			165	426.80	5.05	274.97	287.00	-312.20	176.87
778	Copertura	114	0	-894.37	10.23	-196.28	284.53	171.28	321.89
			82	-894.37	10.23	38.49	284.53	-243.88	321.89
			165	-894.37	10.23	272.37	284.53	-396.77	321.89
779	Copertura	115	0	-1272.00	14.38	-199.50	287.74	588.24	577.07
			82	-1272.00	14.38	37.72	287.74	-115.00	577.07
			165	-1272.00	14.38	274.41	287.74	-395.10	577.07
780	Copertura	116	0	-1550.90	16.43	-201.76	290.20	457.58	408.81
			82	-1550.90	16.43	38.20	290.20	-124.05	408.81
			165	-1550.90	16.43	276.20	290.20	-219.17	408.81
781	Copertura	117	0	-1790.70	12.96	-202.30	289.79	-543.44	-478.62
			82	-1790.70	12.96	36.53	289.79	256.74	-478.62
			165	-1790.70	12.96	274.99	289.79	-455.94	-478.62
782	Copertura	118	0	-1579.87	-6.37	-202.51	291.16	-345.75	-560.89
			82	-1579.87	-6.37	37.32	291.16	-152.27	-560.89
			165	-1579.87	-6.37	277.02	291.16	599.67	-560.89
783	Copertura	131	0	883.06	19.59	-19.80	282.09	540.79	320.68
			30	883.06	19.59	76.26	282.09	474.64	320.68
			60	883.06	19.59	156.13	282.09	-426.78	320.68
784	Copertura	133	0	1200.43	18.16	-22.59	274.72	658.61	275.77
			30	1200.43	18.16	69.66	274.72	590.84	275.77
			60	1200.43	18.16	147.19	274.72	523.19	275.77
785	Copertura	139	0	1578.22	17.45	-18.38	280.30	669.99	473.75
			30	1578.22	17.45	74.77	280.30	530.58	473.75
			60	1578.22	17.45	154.93	280.30	-393.11	473.75
786	Copertura	143	0	1460.34	19.74	-17.09	279.46	707.09	502.11
			30	1460.34	19.74	74.51	279.46	559.74	502.11
			60	1460.34	19.74	154.95	279.46	-414.74	502.11
787	Copertura	147	0	1750.14	20.04	-21.31	277.09	-781.69	-417.71
			30	1750.14	20.04	77.36	277.09	-656.88	-417.71
			60	1750.14	20.04	154.61	277.09	-564.06	-417.71
788	Copertura	151	0	1428.44	25.95	-23.30	279.72	-570.21	-291.93
			30	1428.44	25.95	78.25	279.72	-483.69	-291.93
			60	1428.44	25.95	153.12	279.72	-397.62	-291.93
789	Copertura	155	0	1492.90	22.43	24.12	273.35	-470.13	-366.67
			30	1492.90	22.43	78.93	273.35	-361.73	-366.67
			60	1492.90	22.43	154.60	273.35	-266.98	-366.67
790	Copertura	159	0	1075.15	25.62	-22.80	275.76	570.40	342.25
			30	1075.15	25.62	79.87	275.76	468.28	342.25
			60	1075.15	25.62	155.41	275.76	366.48	342.25
791	Copertura	119	0	-1726.86	9.88	-204.70	293.47	-289.90	-412.98
			82	-1726.86	9.88	37.46	293.47	-161.07	-412.98
			165	-1726.86	9.88	278.67	293.47	458.39	-412.98
792	Copertura	120	0	-1136.59	-7.42	-205.27	295.63	-390.14	-172.90
			82	-1136.59	-7.42	38.30	295.63	248.06	-172.90
			165	-1136.59	-7.42	281.63	295.63	153.18	-172.90
793	Copertura	121	0	567.42	5.86	-214.98	307.11	361.60	159.47
			82	567.42	5.86	38.21	307.11	230.92	159.47
			165	567.42	5.86	290.88	307.11	118.89	159.47
794	Copertura	122	0	-1143.54	15.90	-198.54	272.70	213.61	248.25
			82	-1143.54	15.90	27.77	272.70	267.73	248.25
			165	-1143.54	15.90	250.60	272.70	-400.75	248.25
795	Copertura	123	0	-488.69	42.28	-77.02	326.90	80.99	171.69
			82	-488.69	42.28	192.88	326.90	-102.24	171.69
			165	-488.69	42.28	461.95	326.90	-212.00	171.69
796	Copertura	163	0	1060.97	26.63	-32.90	261.31	535.01	314.50
			33	1060.97	26.63	72.98	261.31	432.77	314.50
			65	1060.97	26.63	148.54	261.31	369.43	314.50
797	Copertura	167	0	527.69	27.99	-22.43	291.03	231.43	258.41
			30	527.69	27.99	89.34	291.03	161.53	258.41
			60	527.69	27.99	167.69	291.03	136.95	258.41
798	Copertura	171	0	-682.11	26.56	-17.28	273.45	274.44	177.84
			30	-682.11	26.56	72.99	273.45	228.10	177.84
			60	-682.11	26.56	151.75	273.45	182.18	177.84
799	Copertura	174	0	1166.45	25.21	-15.84	273.97	369.17	341.47
			30	1166.45	25.21	74.16	273.97	268.04	341.47
			60	1166.45	25.21	152.10	273.97	171.12	341.47
800	Copertura	179	0	-1206.96	16.67	-25.22	281.67	934.41	578.96
			30	-1206.96	16.67	78.50	281.67	760.78	578.96

			60	-1206.96	16.67	153.88	281.67	587.20	578.96
801	Copertura	183	0	-1122.18	13.00	19.57	278.75	711.65	426.74
			30	-1122.18	13.00	77.26	278.75	583.81	426.74
			60	-1122.18	13.00	156.38	278.75	456.07	426.74
802	Copertura	187	0	-1552.74	23.78	16.14	278.00	-829.17	-475.46
			30	-1552.74	23.78	76.73	278.00	-686.69	-475.46
			60	-1552.74	23.78	155.25	278.00	-544.30	-475.46
803	Copertura	191	0	-1235.16	23.70	17.39	277.81	-669.67	-550.39
			30	-1235.16	23.70	76.65	277.81	-507.08	-550.39
			60	-1235.16	23.70	155.33	277.81	-344.88	-550.39
804	Copertura	194	0	-1473.87	27.59	16.05	280.42	-523.11	-393.66
			30	-1473.87	27.59	77.04	280.42	-405.51	-393.66
			60	-1473.87	27.59	157.26	280.42	-288.32	-393.66
805	Copertura	198	0	-1117.41	26.65	-18.75	282.84	-505.08	-189.38
			30	-1117.41	26.65	76.74	282.84	-448.31	-189.38
			60	-1117.41	26.65	156.73	282.84	-391.55	-189.38
806	Copertura	203	0	-849.74	22.90	21.66	272.54	453.07	-152.80
			30	-849.74	22.90	69.72	272.54	407.82	-152.80
			60	-849.74	22.90	145.94	272.54	362.71	-152.80
807	Copertura	207	0	-767.36	27.49	-17.79	279.44	300.54	261.42
			30	-767.36	27.49	79.46	279.44	231.19	261.42
			60	-767.36	27.49	158.33	279.44	214.58	261.42

1.1.8.2 Piastre SLV

Tabella 16.I

Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	-6.383	30.361	-19.718	661.167	-1558.412	765.337	42.315	-49.936
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	-16.283	20.470	-17.552	-1829.402	-3099.361	1697.173	74.753	-81.810
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	16.128	-13.154	-17.612	1884.339	3066.679	2416.269	45.877	-80.813

1.1.9 Risultati Condizioni (Vento (+X)).

1.1.9.1 Sollecitazioni SLU

Tabella 17.I

Sollecitazioni									
Asta	Imp.	Fili	X [cm]	N [daN]	Mt [daNm]	Mxz [daNm]	Txz [daN]	Mxy [daNm]	Txy [daN]
1	Fondazio ne	1, 2	0	-111.88	-22.33	83.47	171.92	2.08	2.41
			42	-99.15	-22.33	138.47	110.44	0.90	3.28
			83	-86.47	-22.33	174.18	78.15	-0.65	4.19
2	Fondazio ne	1, 2	0	-72.94	-24.24	159.99	70.62	-0.65	1.01

			42	-60.30	-24.24	184.29	62.05	-1.26	1.96
			83	-47.70	-24.24	208.91	70.98	-2.28	2.93
3	Fondazio ne	1, 15	0	14.48	20.85	-26.77	154.49	-12.76	-38.98
			40	14.33	20.83	20.09	81.58	2.93	-40.04
			80	14.18	20.82	38.46	11.06	19.11	-41.41
4	Fondazio ne	1, 15	0	13.77	-145.55	56.73	-32.08	19.12	51.61
			40	13.63	-145.56	30.25	-101.20	-1.08	49.99
			80	13.50	-145.58	-23.65	-170.16	-20.59	48.16
5	Fondazio ne	2, 3	0	-120.62	6.21	210.72	-162.28	-1.73	-3.49
			35	-110.17	6.21	155.22	-146.45	-0.56	-3.24
			69	-99.76	6.21	105.92	-126.90	0.51	-2.97
6	Fondazio ne	2, 3	0	-99.52	1.47	103.94	-104.08	0.51	2.37
			35	-89.15	1.47	69.52	-83.45	-0.35	2.64
			69	-78.82	1.47	42.14	-63.52	-1.31	2.92
7	Fondazio ne	3, 4	0	-86.75	18.06	54.42	-68.71	-1.23	-2.38
			35	-76.45	18.06	31.84	-50.66	-0.46	-2.10
			69	-66.18	18.06	15.05	-35.33	0.22	-1.82
8	Fondazio ne	3, 4	0	-71.82	2.39	19.43	-41.17	0.22	1.27
			35	-61.58	2.39	5.37	-29.06	-0.27	1.55
			69	-51.36	2.39	-5.10	-20.39	-0.85	1.83
9	Fondazio ne	4, 5	0	-59.93	16.68	6.23	-32.41	-0.71	-1.44
			35	-49.73	16.68	-5.99	-27.23	-0.27	-1.16
			69	-39.55	16.68	-17.02	-25.49	0.09	-0.89
10	Fondazio ne	4, 5	0	-42.94	6.22	-10.66	-24.39	0.09	0.89
			35	-32.78	6.22	-21.27	-25.88	-0.27	1.15
			69	-22.63	6.22	-32.91	-30.26	-0.71	1.41
11	Fondazio ne	5, 6	0	-26.02	14.50	-19.97	-21.56	-0.54	-0.34
			35	-15.88	14.50	-30.54	-28.32	-0.47	-0.09
			69	-5.75	14.50	-43.77	-36.90	-0.48	0.15
12	Fondazio ne	5, 6	0	0.46	-5.35	-40.57	-66.67	-0.48	-0.14
			35	10.59	-5.34	-67.24	-76.32	-0.47	0.08
			69	20.73	-5.34	-97.28	-85.91	-0.53	0.29
13	Fondazio ne	6, 7	0	-51.54	-23.42	-101.72	177.79	-0.47	-0.92
			35	-41.41	-23.41	-43.85	169.86	-0.19	-0.72
			69	-31.29	-23.41	11.79	164.98	0.03	-0.55
14	Fondazio ne	6, 7	0	-16.10	-24.53	-5.98	169.57	0.03	-0.01
			35	-5.99	-24.53	50.15	168.14	0.00	0.15
			69	4.11	-24.53	106.33	169.63	-0.08	0.28
15	Fondazio ne	7, 8	0	-67.31	7.37	105.67	-108.72	0.19	-0.51
			35	-57.22	7.36	66.63	-105.80	0.35	-0.39
			69	-47.15	7.36	28.60	-103.14	0.47	-0.29
16	Fondazio ne	7, 8	0	-36.85	22.22	40.21	-70.12	0.46	0.72
			35	-26.80	22.22	14.29	-68.74	0.20	0.80
			69	-16.76	22.22	-11.44	-69.16	-0.08	0.87
17	Fondazio ne	8, 9	0	-12.06	19.53	10.92	-61.97	0.15	0.61
			35	-2.03	19.53	-12.81	-64.30	-0.07	0.67
			69	8.01	19.53	-37.66	-68.45	-0.31	0.71
18	Fondazio ne	8, 9	0	19.98	9.27	-25.71	-95.99	-0.31	0.49
			35	30.02	9.27	-61.75	-101.47	-0.49	0.52
			69	40.07	9.27	-99.79	-107.35	-0.67	0.53
19	Fondazio ne	9, 10	0	-33.92	-26.95	-103.90	176.76	-0.32	-1.00
			35	-23.87	-26.95	-45.80	172.06	0.03	-1.01
			69	-13.82	-26.95	11.10	169.97	0.38	-1.04
20	Fondazio ne	9, 10	0	4.21	-25.27	-6.37	160.18	0.38	0.31
			35	14.25	-25.27	46.96	161.12	0.28	0.26

			69	24.30	-25.27	101.08	164.61	0.20	0.19
21	Fondazio ne	10, 11	0	-47.51	-10.32	98.17	-77.79	0.13	-0.51
			35	-37.47	-10.32	70.12	-73.17	0.32	-0.59
			69	-27.45	-10.32	43.61	-69.07	0.54	-0.69
22	Fondazio ne	10, 11	0	-18.68	16.14	44.24	-36.91	0.53	-0.15
			35	-8.66	16.14	29.98	-34.51	0.61	-0.27
			69	1.36	16.14	16.14	-34.57	0.72	-0.39
23	Fondazio ne	11, 12	0	0.86	6.33	29.15	-51.34	0.84	1.83
			35	10.88	6.33	9.01	-54.37	0.23	1.70
			69	20.90	6.33	-12.74	-60.71	-0.33	1.56
24	Fondazio ne	11, 12	0	21.89	21.79	-5.05	-54.33	-0.33	-1.67
			35	31.92	21.79	-27.37	-63.97	0.27	-1.82
			69	41.96	21.79	-53.54	-76.56	0.92	-1.97
25	Fondazio ne	12, 13	0	41.22	2.19	-40.63	-66.03	0.95	2.61
			35	51.28	2.19	-67.92	-80.78	0.08	2.46
			69	61.36	2.19	-100.51	-96.55	-0.74	2.30
26	Fondazio ne	12, 13	0	69.83	5.77	-99.05	-114.46	-0.74	-1.97
			35	79.93	5.77	-143.21	-129.53	-0.03	-2.13
			69	90.07	5.77	-192.12	-141.43	0.73	-2.29
27	Fondazio ne	13, 14	0	22.83	-28.23	-194.16	78.85	1.06	2.87
			42	35.04	-28.23	-165.40	73.48	0.04	2.01
			83	47.27	-28.23	-135.83	83.76	-0.61	1.14
28	Fondazio ne	13, 14	0	70.23	-28.96	-142.60	65.53	-0.61	3.23
			42	82.49	-28.96	-112.13	96.89	-1.78	2.37
			83	94.80	-28.96	-63.47	153.83	-2.58	1.49
29	Fondazio ne	14, 16	0	-15.28	28.77	37.35	-165.48	-10.82	-34.30
			40	-15.07	28.76	-15.20	-99.31	1.79	-29.14
			80	-14.87	28.75	-42.12	-36.41	12.38	-24.19
30	Fondazio ne	14, 16	0	-18.20	-84.05	-39.33	-6.65	12.38	24.71
			40	-18.01	-84.06	-29.93	53.83	1.60	29.49
			80	-17.83	-84.07	3.22	112.97	-11.05	34.16
31	Fondazio ne	15, 17	0	12.09	50.47	6.03	70.70	-24.17	-73.14
			33	11.99	50.45	19.91	13.30	-0.11	-72.65
			66	11.89	50.44	14.81	-44.45	23.78	-72.16
32	Fondazio ne	15, 17	0	12.80	-210.33	50.10	-89.14	23.79	72.70
			33	12.70	-210.34	11.08	-147.64	-0.29	73.22
			66	12.61	-210.36	-47.44	-207.31	-24.55	73.81
33	Fondazio ne	16, 18	0	-28.57	36.65	-6.87	-64.68	-13.94	-46.93
			33	-28.43	36.64	-20.23	-16.18	0.75	-42.07
			66	-28.30	36.62	-17.63	32.04	13.83	-37.23
34	Fondazio ne	16, 18	0	-23.16	-146.85	-38.43	44.85	13.84	37.05
			33	-23.04	-146.86	-15.69	93.19	0.81	41.91
			66	-22.92	-146.87	23.08	142.06	-13.83	46.80
35	Fondazio ne	17, 19	0	2.64	101.54	-8.77	84.21	-29.91	-86.37
			33	2.55	101.52	9.05	23.49	-1.51	-85.75
			66	2.47	101.51	6.67	-38.22	26.69	-85.16
36	Fondazio ne	17, 19	0	5.94	-205.74	38.12	-72.49	26.70	83.41
			33	5.85	-205.76	3.87	-135.43	-0.93	84.03
			66	5.77	-205.77	-51.40	-199.86	-28.77	84.71
37	Fondazio ne	18, 20	0	-19.29	63.50	2.81	-67.53	-18.57	-57.70
			33	-19.18	63.48	-11.35	-18.08	-0.34	-52.80
			66	-19.09	63.47	-9.10	32.01	16.28	-47.90
38	Fondazio ne	18, 20	0	-15.55	-168.96	-32.46	46.84	16.28	47.95
			33	-15.46	-168.97	-8.63	97.83	-0.35	52.85
			66	-15.37	-168.98	32.21	150.01	-18.61	57.79

39	Fondazio ne	19, 21	0	2.25	128.57	-20.12	108.32	-28.44	-86.10
			33	2.17	128.55	4.84	42.64	-0.14	-85.41
			66	2.09	128.53	7.94	-24.12	27.93	-84.75
40	Fondazio ne	19, 21	0	4.79	-214.26	25.71	-53.08	27.93	83.67
			33	4.71	-214.28	-2.97	-121.09	0.21	84.34
			66	4.64	-214.30	-54.33	-190.50	-27.74	85.06
41	Fondazio ne	20, 22	0	-15.72	91.69	12.27	-79.39	-18.90	-60.79
			33	-15.63	91.68	-5.18	-26.11	0.35	-55.84
			66	-15.56	91.66	-4.88	28.20	17.96	-50.92
42	Fondazio ne	20, 22	0	-13.57	-175.50	-24.14	45.76	17.96	49.95
			33	-13.50	-175.51	0.06	101.24	0.67	54.88
			66	-13.43	-175.53	42.79	158.04	-18.26	59.84
43	Fondazio ne	21, 23	0	0.73	165.07	-41.85	150.05	-32.28	-94.11
			33	0.65	165.05	-3.92	79.64	-1.34	-93.38
			66	0.58	165.04	10.67	8.60	29.36	-92.69
44	Fondazio ne	21, 23	0	7.69	-206.23	15.14	-30.58	29.36	96.37
			33	7.61	-206.25	-6.75	-102.32	-2.56	97.06
			66	7.54	-206.27	-52.45	-174.82	-34.71	97.79
45	Fondazio ne	22, 24	0	-10.94	123.70	29.11	-110.16	-22.31	-67.56
			33	-10.88	123.69	2.27	-52.31	-0.83	-62.59
			66	-10.82	123.67	-5.35	6.34	19.00	-57.65
46	Fondazio ne	22, 24	0	-12.01	-166.01	-14.57	23.67	19.01	59.18
			33	-11.96	-166.02	3.03	83.16	-1.34	64.12
			66	-11.91	-166.04	40.40	143.57	-23.32	69.10
47	Fondazio ne	23, 25	0	15.27	226.32	-59.14	205.39	-33.03	-91.01
			33	15.20	226.30	-3.36	132.59	-3.12	-90.30
			66	15.14	226.28	28.41	59.93	26.57	-89.67
48	Fondazio ne	23, 25	0	37.32	-97.46	8.66	27.55	26.56	61.24
			33	37.27	-97.48	5.78	-45.12	6.26	61.83
			66	37.23	-97.50	-21.12	-117.98	-14.25	62.44
49	Fondazio ne	24, 26	0	-18.71	162.63	37.26	-145.71	-21.88	-64.15
			33	-18.67	162.61	-0.78	-84.70	-1.53	-59.19
			66	-18.63	162.60	-18.62	-23.33	17.19	-54.28
50	Fondazio ne	24, 26	0	-29.18	-100.77	-18.33	4.42	17.18	34.40
			33	-29.15	-100.78	-6.69	66.30	5.03	39.28
			66	-29.14	-100.80	25.49	128.90	-8.74	44.18
51	Fondazio ne	25, 26	0	-187.45	-2.56	449.83	-82.80	0.40	0.45
			49	-172.07	-2.56	385.94	-155.96	0.17	0.51
			97	-156.83	-2.56	300.43	-175.55	-0.09	0.57
52	Fondazio ne	25, 26	0	-164.95	4.06	278.93	-111.40	-0.09	-0.11
			49	-149.84	4.06	224.11	-96.97	-0.05	-0.03
			97	-134.84	4.06	181.58	-63.19	-0.06	0.07
53	Fondazio ne	25, 26	0	-153.81	2.95	142.69	-101.20	-0.05	0.15
			49	-138.92	2.95	100.49	-59.28	-0.15	0.26
			97	-124.15	2.95	79.17	-16.50	-0.31	0.38
54	Fondazio ne	25, 26	0	-143.15	-0.62	52.76	-71.91	-0.30	-0.25
			49	-128.48	-0.62	24.49	-33.11	-0.21	-0.12
			97	-113.91	-0.62	13.63	-0.69	-0.19	0.02
55	Fondazio ne	25, 26	0	-129.84	-0.83	-1.75	-31.49	-0.19	-0.14
			49	-115.36	-0.83	-13.55	-6.35	-0.15	-0.01
			97	-100.98	-0.83	-14.82	11.83	-0.18	0.13
56	Fondazio ne	25, 26	0	-114.71	-0.66	-19.85	-6.07	-0.18	-0.16
			49	-100.41	-0.66	-22.49	6.04	-0.14	-0.02
			97	-86.19	-0.66	-20.47	13.25	-0.16	0.12
57	Fondazio	25, 26	0	-98.42	-0.43	-20.52	6.84	-0.17	-0.17

	ne								
			49	-84.27	-0.43	-19.03	10.40	-0.12	-0.04
			97	-70.19	-0.43	-16.44	11.45	-0.13	0.09
58	Fondazio ne	25, 26	0	-81.45	-0.12	-14.59	11.15	-0.13	-0.13
			49	-67.43	-0.12	-12.03	10.68	-0.09	-0.02
			97	-53.45	-0.12	-9.90	9.48	-0.11	0.09
59	Fondazio ne	25, 26	0	-64.22	0.16	-7.78	10.81	-0.11	-0.18
			49	-50.29	0.16	-5.63	9.49	-0.05	-0.09
			97	-36.41	0.16	-4.06	8.43	-0.03	0.00
60	Fondazio ne	25, 26	0	-45.64	0.29	-1.75	9.35	-0.03	-0.05
			49	-31.79	0.29	-0.12	8.82	-0.03	0.02
			97	-17.96	0.29	1.40	8.90	-0.05	0.08
61	Fondazio ne	25, 26	0	-28.53	0.13	3.26	8.66	-0.05	-0.12
			49	-14.72	0.13	4.85	9.29	-0.01	-0.07
			97	-0.92	0.13	6.84	10.25	0.02	-0.04
62	Fondazio ne	25, 26	0	-11.28	-0.08	8.64	9.14	0.01	-0.04
			49	2.51	-0.08	10.57	10.09	0.03	-0.02
			97	16.31	-0.08	12.85	10.49	0.03	-0.01
63	Fondazio ne	25, 26	0	5.73	-0.51	14.34	10.80	0.03	-0.05
			49	19.53	-0.51	16.71	9.97	0.06	-0.06
			97	33.35	-0.51	18.19	7.03	0.09	-0.07
64	Fondazio ne	25, 26	0	22.31	-1.16	18.19	11.81	0.08	-0.02
			49	36.15	-1.16	19.85	5.76	0.10	-0.05
			97	50.02	-1.16	17.58	-4.50	0.13	-0.08
65	Fondazio ne	25, 26	0	38.09	-1.86	13.29	9.72	0.13	0.02
			49	51.99	-1.86	11.70	-5.79	0.13	-0.03
			97	65.94	-1.86	1.11	-27.33	0.16	-0.08
66	Fondazio ne	25, 26	0	52.49	-1.61	-10.76	0.83	0.15	0.01
			49	66.48	-1.61	-19.68	-27.02	0.16	-0.05
			97	80.53	-1.61	-43.58	-60.47	0.20	-0.11
67	Fondazio ne	25, 26	0	65.32	0.76	-67.84	-24.71	0.20	0.06
			49	79.42	0.76	-91.63	-61.74	0.18	0.00
			97	93.59	0.76	-133.50	-98.06	0.20	-0.07
68	Fondazio ne	25, 26	0	74.99	5.52	-165.90	-27.05	0.20	0.06
			49	89.22	5.52	-189.45	-55.99	0.19	0.00
			97	103.52	5.52	-223.38	-67.77	0.20	-0.06
69	Fondazio ne	25, 26	0	96.44	10.72	-252.94	-154.17	0.21	-0.83
			49	110.82	10.72	-328.11	-136.58	0.62	-0.88
			97	125.29	10.72	-384.35	-73.16	1.06	-0.91
70	Fondazio ne	25, 28	0	30.80	104.77	-34.65	173.76	-19.83	-57.23
			43	30.77	104.74	19.24	79.83	5.05	-59.83
			85	30.76	104.72	33.20	-14.23	31.04	-62.48
71	Fondazio ne	25, 28	0	22.12	-248.93	54.85	-55.67	31.05	84.52
			43	22.12	-248.96	11.01	-150.97	-4.32	81.97
			85	22.14	-248.98	-73.81	-248.59	-38.65	79.61
72	Fondazio ne	26, 27	0	-23.69	66.47	8.96	-91.90	-11.05	-48.23
			33	-23.68	66.46	-10.95	-28.63	4.05	-43.33
			66	-23.68	66.44	-9.87	35.32	17.54	-38.41
73	Fondazio ne	26, 27	0	-11.09	-208.69	-29.57	53.00	17.55	59.05
			33	-11.10	-208.71	-1.40	117.88	-2.75	64.00
			66	-11.11	-208.73	48.36	183.90	-24.69	69.01
74	Fondazio ne	27, 29	0	-5.40	139.22	32.64	-122.18	-22.32	-69.66
			33	-5.41	139.20	3.33	-55.32	-0.17	-64.62
			66	-5.43	139.19	-3.81	12.09	20.33	-59.60
75	Fondazio ne	27, 29	0	0.61	-184.44	-17.28	22.04	20.33	57.71

			33	0.59	-184.46	1.20	90.04	0.46	62.74
			66	0.57	-184.48	42.23	158.73	-21.08	67.82
76	Fondazio ne	28, 30	0	3.06	185.49	-46.76	175.52	-34.64	-95.02
			37	3.07	185.47	1.78	90.37	0.08	-95.24
			73	3.10	185.45	19.12	4.55	34.89	-95.51
77	Fondazio ne	28, 30	0	1.81	-235.88	35.36	-48.51	34.89	96.24
			37	1.83	-235.90	1.85	-135.30	-0.18	95.98
			73	1.85	-235.93	-63.58	-223.41	-35.19	95.83
78	Fondazio ne	29, 31	0	2.26	157.36	37.33	-140.38	-23.84	-72.28
			33	2.25	157.34	2.40	-71.30	-0.83	-67.18
			66	2.23	157.32	-9.71	-2.11	20.50	-62.12
79	Fondazio ne	29, 31	0	7.12	-169.98	-16.50	8.93	20.51	61.74
			33	7.11	-170.00	-2.11	78.30	-0.71	66.81
			66	7.10	-170.02	35.22	147.99	-23.60	71.93
80	Fondazio ne	30, 32	0	-4.19	196.80	-51.58	189.63	-34.89	-99.65
			34	-4.17	196.77	-0.91	106.22	-0.85	-99.11
			69	-4.15	196.75	21.15	22.57	33.00	-98.62
81	Fondazio ne	30, 32	0	-1.24	-225.75	27.33	-36.21	33.01	97.41
			34	-1.22	-225.77	0.54	-120.31	-0.44	97.91
			69	-1.20	-225.79	-55.17	-205.10	-34.07	98.48
82	Fondazio ne	31, 33	0	1.09	164.72	37.38	-145.66	-20.72	-67.16
			33	1.08	164.70	0.83	-75.88	0.60	-62.04
			66	1.07	164.69	-12.72	-6.27	20.24	-56.97
83	Fondazio ne	31, 33	0	6.98	-159.82	-16.26	3.32	20.24	56.69
			33	6.98	-159.84	-3.69	72.88	0.69	61.77
			66	6.97	-159.86	31.85	142.55	-20.54	66.89
84	Fondazio ne	32, 34	0	-3.84	211.46	-49.62	192.00	-33.84	-97.39
			35	-3.82	211.43	1.84	106.32	-0.33	-96.89
			69	-3.81	211.41	23.75	20.74	33.02	-96.45
85	Fondazio ne	32, 34	0	0.43	-198.31	24.84	-28.32	33.02	95.48
			35	0.44	-198.34	0.29	-114.04	0.00	95.92
			69	0.46	-198.36	-53.90	-200.14	-33.18	96.43
86	Fondazio ne	33, 35	0	2.63	167.15	38.33	-149.28	-22.91	-70.10
			33	2.62	167.13	0.55	-79.70	-0.63	-64.98
			66	2.62	167.12	-14.31	-10.46	19.98	-59.89
87	Fondazio ne	33, 35	0	8.58	-151.59	-15.95	0.81	19.98	59.80
			33	8.58	-151.61	-4.29	69.83	-0.60	64.88
			66	8.58	-151.63	30.13	138.80	-22.85	70.00
88	Fondazio ne	34, 36	0	-2.49	207.63	-49.18	197.50	-32.94	-94.87
			35	-2.48	207.61	4.10	111.43	-0.30	-94.37
			69	-2.47	207.59	27.75	25.77	32.18	-93.92
89	Fondazio ne	34, 36	0	0.57	-197.45	23.28	-14.48	32.18	93.90
			35	0.59	-197.47	3.53	-100.05	-0.29	94.34
			69	0.60	-197.50	-45.78	-185.80	-32.92	94.84
90	Fondazio ne	35, 37	0	-1.38	167.95	38.65	-152.73	-19.88	-65.19
			33	-1.37	167.93	-0.40	-83.98	0.79	-60.08
			66	-1.37	167.91	-16.84	-15.72	19.78	-55.02
91	Fondazio ne	35, 37	0	4.28	-146.51	-16.19	-0.22	19.77	55.48
			33	4.28	-146.52	-5.05	67.72	0.63	60.54
			66	4.29	-146.54	28.49	135.52	-20.18	65.62
92	Fondazio ne	36, 38	0	-2.05	206.96	-46.99	199.01	-32.65	-93.95
			35	-2.04	206.94	6.88	113.40	-0.32	-93.46
			69	-2.02	206.92	31.30	28.22	31.85	-93.03
93	Fondazio ne	36, 38	0	5.97	-193.70	26.17	-14.51	31.85	92.43
			35	5.98	-193.72	6.48	-99.62	-0.12	92.85

			69	5.99	-193.74	-42.61	-184.98	-32.23	93.32
94	Fondazio ne	37, 39	0	-0.76	168.76	37.65	-151.46	-22.41	-69.02
			33	-0.75	168.74	-1.18	-83.96	-0.47	-63.93
			66	-0.75	168.73	-17.83	-17.00	19.79	-58.89
95	Fondazio ne	37, 39	0	2.25	-141.78	-14.18	1.31	19.79	59.47
			33	2.26	-141.80	-2.76	67.89	-0.66	64.50
			66	2.26	-141.81	30.60	134.26	-22.78	69.56
96	Fondazio ne	38, 40	0	-1.68	199.58	-41.36	191.39	-31.78	-90.76
			34	-1.66	199.56	9.67	106.63	-0.78	-90.22
			69	-1.65	199.54	31.70	22.07	30.04	-89.76
97	Fondazio ne	38, 40	0	14.57	-188.94	26.01	-10.72	30.03	87.89
			34	14.59	-188.97	7.84	-95.46	-0.15	88.34
			69	14.61	-188.99	-39.44	-180.72	-30.48	88.82
98	Fondazio ne	39, 41	0	-6.41	174.47	41.50	-156.56	-19.99	-64.95
			33	-6.40	174.45	0.73	-90.63	0.61	-59.91
			66	-6.40	174.43	-18.40	-25.40	19.56	-54.92
99	Fondazio ne	39, 41	0	-7.47	-129.01	-8.90	-6.65	19.55	58.80
			33	-7.47	-129.02	-0.42	58.00	-0.67	63.78
			66	-7.47	-129.04	29.33	122.18	-22.54	68.78
100	Fondazio ne	40, 42	0	7.05	188.51	-38.40	173.57	-29.49	-85.24
			35	7.08	188.48	6.61	87.36	-0.15	-84.84
			69	7.11	188.46	21.86	1.06	29.06	-84.52
101	Fondazio ne	40, 42	0	19.22	-195.39	20.58	-36.82	29.06	77.95
			35	19.26	-195.41	-7.07	-123.50	2.11	78.26
			69	19.30	-195.43	-64.71	-210.68	-24.95	78.60
102	Fondazio ne	41, 44	0	-17.55	189.56	44.92	-177.17	-22.36	-64.46
			33	-17.56	189.55	-3.05	-113.70	-1.91	-59.48
			66	-17.57	189.53	-30.22	-51.18	16.91	-54.56
103	Fondazio ne	41, 44	0	-28.30	-68.89	-16.17	-21.88	16.90	33.28
			33	-28.32	-68.90	-13.17	39.93	5.11	38.15
			66	-28.35	-68.92	10.15	101.32	-8.29	43.03
104	Fondazio ne	42, 43	0	13.34	149.28	-46.81	102.18	-24.21	-73.72
			23	13.37	149.26	-30.00	44.05	-7.93	-67.88
			46	13.40	149.24	-26.54	-13.81	7.01	-62.07
105	Fondazio ne	43, 44	0	-207.95	-18.13	479.47	-37.77	10.22	12.20
			49	-192.40	-18.13	434.70	-120.88	4.31	12.10
			97	-177.01	-18.13	365.34	-143.14	-1.55	11.97
106	Fondazio ne	43, 44	0	-185.76	-2.38	317.78	-128.32	-1.55	-1.76
			49	-170.51	-2.38	254.98	-112.20	-0.67	-1.87
			97	-155.39	-2.38	205.89	-74.58	0.27	-1.99
107	Fondazio ne	43, 44	0	-167.95	-0.71	159.33	-115.73	0.27	0.24
			49	-152.96	-0.71	111.12	-69.31	0.18	0.12
			97	-138.09	-0.71	85.96	-22.24	0.16	-0.01
108	Fondazio ne	43, 44	0	-152.30	1.71	52.78	-74.21	0.16	0.15
			49	-137.54	1.71	24.30	-31.74	0.12	0.02
			97	-122.89	1.71	14.85	3.65	0.14	-0.11
109	Fondazio ne	43, 44	0	-136.94	1.06	-1.76	-35.25	0.14	0.14
			49	-122.39	1.06	-14.83	-7.85	0.10	0.02
			97	-107.94	1.06	-16.43	11.92	0.12	-0.11
110	Fondazio ne	43, 44	0	-120.58	0.70	-22.10	-6.92	0.12	0.13
			49	-106.22	0.70	-24.90	6.19	0.09	0.01
			97	-91.94	0.70	-22.66	13.96	0.11	-0.10
111	Fondazio ne	43, 44	0	-103.49	0.43	-22.48	7.19	0.11	0.13
			49	-89.29	0.43	-20.76	10.98	0.07	0.03
			97	-75.16	0.43	-17.89	12.04	0.09	-0.07

112	Fondazio ne	43, 44	0	-85.96	0.15	-15.73	11.76	0.09	0.13
			49	-71.89	0.15	-12.91	11.18	0.05	0.03
			97	-57.88	0.15	-10.59	9.80	0.05	-0.05
113	Fondazio ne	43, 44	0	-68.25	-0.08	-8.23	11.48	0.06	0.08
			49	-54.28	-0.08	-5.81	9.95	0.03	0.01
			97	-40.37	-0.08	-4.08	8.68	0.04	-0.05
114	Fondazio ne	43, 44	0	-50.67	-0.14	-2.03	9.91	0.05	0.09
			49	-36.78	-0.14	-0.19	9.17	0.02	0.04
			97	-22.93	-0.14	1.45	9.04	0.00	0.01
115	Fondazio ne	43, 44	0	-32.54	-0.14	3.35	8.63	0.01	0.05
			49	-18.71	-0.14	4.87	9.06	-0.01	0.03
			97	-4.89	-0.14	6.70	9.84	-0.02	0.02
116	Fondazio ne	43, 44	0	-15.31	0.14	8.53	9.01	-0.02	0.03
			49	-1.50	0.14	10.35	9.78	-0.03	0.02
			97	12.31	0.14	12.44	10.03	-0.05	0.04
117	Fondazio ne	43, 44	0	1.68	0.54	13.96	10.35	-0.04	0.01
			49	15.49	0.54	16.07	9.40	-0.05	0.03
			97	29.32	0.54	17.26	6.42	-0.07	0.06
118	Fondazio ne	43, 44	0	18.11	1.09	17.11	11.50	-0.07	-0.01
			49	31.96	1.09	18.63	5.51	-0.07	0.03
			97	45.83	1.09	16.28	-4.51	-0.10	0.08
119	Fondazio ne	43, 44	0	33.67	1.46	11.79	10.20	-0.10	-0.02
			49	47.57	1.46	10.54	-4.82	-0.10	0.03
			97	61.51	1.46	0.61	-25.55	-0.13	0.10
120	Fondazio ne	43, 44	0	48.00	1.47	-11.64	2.98	-0.13	-0.07
			49	61.98	1.47	-19.24	-23.68	-0.11	0.00
			97	76.01	1.47	-41.14	-55.55	-0.13	0.07
121	Fondazio ne	43, 44	0	60.86	-0.17	-66.18	-18.89	-0.13	0.05
			49	74.94	-0.17	-86.68	-54.03	-0.17	0.13
			97	89.08	-0.17	-124.32	-88.36	-0.25	0.20
122	Fondazio ne	43, 44	0	71.29	-7.11	-158.10	-33.13	-0.25	-0.24
			49	85.49	-7.11	-184.17	-60.34	-0.16	-0.16
			97	99.77	-7.11	-219.91	-71.02	-0.09	-0.10
123	Fondazio ne	43, 44	0	90.99	-3.59	-245.61	-137.59	-0.09	-0.80
			49	105.34	-3.59	-312.62	-119.84	0.28	-0.74
			97	119.77	-3.59	-360.97	-57.84	0.63	-0.69
124	Fondazio ne	43, 45	0	21.68	136.32	-92.27	325.83	-5.94	-47.36
			33	21.73	136.30	1.66	243.73	9.57	-46.65
			66	21.80	136.28	68.74	163.17	24.86	-45.98
125	Fondazio ne	43, 45	0	27.28	-182.90	24.48	-21.43	24.86	84.53
			33	27.35	-182.92	4.26	-100.89	-3.15	85.23
			66	27.43	-182.94	-42.06	-179.60	-31.40	85.99
126	Fondazio ne	44, 46	0	-25.93	77.52	17.21	-116.15	-9.96	-45.00
			33	-25.97	77.51	-11.03	-55.10	4.09	-40.12
			66	-26.02	77.49	-19.18	5.60	16.52	-35.25
127	Fondazio ne	44, 46	0	-17.33	-185.40	-34.36	79.79	16.53	55.45
			33	-17.39	-185.42	1.99	140.46	-2.58	60.35
			66	-17.45	-185.43	58.40	201.32	-23.31	65.31
128	Fondazio ne	45, 47	0	13.58	205.15	-43.95	188.32	-28.83	-88.26
			33	13.67	205.13	5.32	110.62	0.16	-87.49
			66	13.77	205.11	29.16	34.17	28.91	-86.76
129	Fondazio ne	45, 47	0	12.86	-157.40	19.04	-15.93	28.91	86.51
			33	12.96	-157.42	1.29	-91.40	0.25	87.24
			66	13.06	-157.44	-41.24	-166.07	-28.67	88.02
130	Fondazio	46, 48	0	-14.81	160.82	50.14	-160.31	-20.46	-63.31

	ne								
			33	-14.88	160.81	7.27	-99.69	-0.38	-58.35
			66	-14.95	160.79	-15.70	-39.75	18.06	-53.41
131	Fondazio ne	46, 48	0	-6.37	-137.19	-10.91	1.77	18.06	51.07
			33	-6.45	-137.21	-0.51	61.07	0.39	56.00
			66	-6.53	-137.23	29.37	119.84	-18.91	60.98
132	Fondazio ne	47, 49	0	7.61	200.31	-42.27	172.17	-30.88	-90.32
			33	7.72	200.29	2.34	98.56	-1.21	-89.53
			66	7.83	200.27	22.88	26.29	28.21	-88.78
133	Fondazio ne	47, 49	0	5.09	-150.09	9.88	10.30	28.21	89.04
			33	5.21	-150.11	1.49	-60.83	-1.30	89.79
			66	5.32	-150.13	-30.21	-130.94	-31.05	90.57
134	Fondazio ne	48, 50	0	-14.94	171.94	38.25	-150.10	-20.43	-63.64
			33	-15.02	171.92	-1.67	-92.08	-0.25	-58.67
			66	-15.11	171.91	-22.60	-35.03	18.29	-53.72
135	Fondazio ne	48, 50	0	-7.67	-115.91	-10.77	2.03	18.29	55.41
			33	-7.76	-115.93	-0.79	58.26	-0.81	60.35
			66	-7.86	-115.94	27.64	113.82	-21.55	65.32
136	Fondazio ne	49, 51	0	9.32	209.02	-49.19	185.90	-26.94	-83.47
			33	9.44	209.00	0.73	117.04	0.47	-82.70
			66	9.56	208.98	28.18	49.74	27.64	-81.98
137	Fondazio ne	49, 51	0	7.35	-124.51	8.00	25.76	27.64	83.46
			33	7.47	-124.52	5.56	-40.19	-0.02	84.17
			66	7.60	-124.54	-18.45	-104.96	-27.91	84.91
138	Fondazio ne	50, 52	0	-17.26	173.44	45.73	-163.36	-17.97	-59.19
			33	-17.36	173.43	0.89	-108.71	0.74	-54.23
			66	-17.47	173.42	-26.11	-55.25	17.82	-49.30
139	Fondazio ne	50, 52	0	-14.99	-91.52	-7.74	-18.53	17.82	51.54
			33	-15.10	-91.53	-5.15	33.89	0.00	56.46
			66	-15.22	-91.55	14.58	85.43	-19.45	61.41
140	Fondazio ne	51, 53	0	8.61	209.85	-43.06	182.94	-28.40	-83.46
			33	8.74	209.84	6.77	119.48	-0.98	-82.73
			66	8.87	209.82	35.90	57.49	26.21	-82.06
141	Fondazio ne	51, 53	0	8.86	-92.73	9.07	31.14	26.20	82.85
			33	8.99	-92.75	9.25	-29.67	-1.24	83.50
			66	9.13	-92.76	-10.47	-89.52	-28.91	84.17
142	Fondazio ne	52, 54	0	-19.33	165.10	37.06	-157.96	-17.44	-56.04
			33	-19.45	165.09	-6.67	-107.39	0.23	-51.10
			66	-19.59	165.08	-33.89	-57.93	16.29	-46.20
143	Fondazio ne	52, 54	0	-19.87	-66.51	-11.61	-29.70	16.28	46.72
			33	-20.01	-66.52	-13.34	18.94	0.06	51.62
			66	-20.16	-66.54	0.89	67.03	-17.78	56.53
144	Fondazio ne	53, 55	0	12.64	198.73	-37.99	181.74	-23.78	-71.67
			33	12.78	198.72	12.21	122.86	-0.24	-71.03
			66	12.93	198.70	43.16	65.04	23.11	-70.45
145	Fondazio ne	53, 55	0	18.05	-48.31	12.71	44.04	23.10	69.85
			33	18.20	-48.32	17.77	-13.12	-0.04	70.40
			66	18.36	-48.34	4.02	-69.98	-23.37	70.96
146	Fondazio ne	54, 56	0	-23.74	142.90	22.54	-142.29	-15.04	-48.92
			33	-23.90	142.88	-16.51	-94.64	0.30	-44.02
			66	-24.06	142.87	-39.90	-47.37	14.02	-39.14
147	Fondazio ne	54, 56	0	-27.16	-41.32	-20.62	-22.72	14.02	37.58
			33	-27.34	-41.33	-20.28	24.60	0.81	42.44
			66	-27.52	-41.34	-4.26	72.41	-14.00	47.32
148	Fondazio ne	55, 57	0	12.02	136.69	-18.52	153.90	-19.93	-46.83

			40	12.22	136.67	29.03	85.56	-0.96	-48.57
			80	12.42	136.66	49.39	17.00	18.65	-50.10
149	Fondazio ne	55, 57	0	15.60	-14.93	38.66	-14.34	18.64	40.45
			40	15.81	-14.94	19.09	-84.27	2.83	39.18
			80	16.04	-14.95	-28.73	-156.51	-12.55	38.23
150	Fondazio ne	56, 70	0	-18.80	80.98	4.98	-116.25	-11.21	-34.68
			40	-19.03	80.96	-29.59	-57.71	1.64	-29.99
			80	-19.27	80.95	-40.60	2.39	12.61	-25.18
151	Fondazio ne	56, 70	0	-14.93	-32.62	-42.04	38.56	12.61	24.37
			40	-15.18	-32.63	-14.30	101.31	1.94	29.35
			80	-15.44	-32.64	39.06	167.55	-10.75	34.55
152	Fondazio ne	57, 58	0	-114.89	20.25	88.34	150.04	-1.91	-1.87
			42	-102.05	20.25	134.34	88.97	-0.94	-2.82
			83	-89.26	20.25	161.08	56.45	0.44	-3.80
153	Fondazio ne	57, 58	0	-70.80	22.98	161.98	69.76	0.43	-1.09
			42	-58.06	22.98	185.78	60.52	1.09	-2.10
			83	-45.35	22.98	209.53	68.35	2.18	-3.13
154	Fondazio ne	58, 59	0	-120.66	-9.60	209.81	-156.01	1.65	3.43
			35	-110.11	-9.60	156.24	-141.46	0.52	3.13
			69	-99.61	-9.60	108.38	-123.49	-0.51	2.82
155	Fondazio ne	58, 59	0	-97.30	-1.87	109.98	-109.20	-0.51	-2.43
			35	-86.83	-1.87	73.44	-90.53	0.38	-2.74
			69	-76.40	-1.87	43.20	-73.04	1.38	-3.05
156	Fondazio ne	59, 60	0	-82.48	-21.53	56.10	-83.88	1.30	2.54
			35	-72.08	-21.53	27.78	-68.78	0.47	2.23
			69	-61.71	-21.53	4.13	-56.89	-0.24	1.92
157	Fondazio ne	59, 60	0	-65.38	-5.18	11.77	-62.85	-0.24	-1.60
			35	-55.04	-5.18	-10.44	-54.51	0.37	-1.91
			69	-44.72	-5.18	-30.38	-49.72	1.08	-2.21
158	Fondazio ne	60, 61	0	-48.50	-14.50	-19.88	-39.57	0.94	1.19
			35	-38.20	-14.50	-35.22	-37.94	0.58	0.89
			69	-27.91	-14.50	-50.46	-38.88	0.32	0.60
159	Fondazio ne	60, 61	0	-23.19	12.00	-48.60	-68.76	0.33	-0.25
			35	-12.91	12.00	-74.80	-71.39	0.46	-0.53
			69	-2.64	12.00	-102.02	-74.45	0.69	-0.79
160	Fondazio ne	61, 62	0	-74.97	26.48	-109.80	173.93	0.76	1.50
			35	-64.71	26.48	-52.22	172.21	0.28	1.25
			69	-54.48	26.48	5.25	173.38	-0.11	1.02
161	Fondazio ne	61, 62	0	-41.31	32.33	-16.06	177.98	-0.10	-0.28
			35	-31.09	32.33	43.99	182.58	0.03	-0.49
			69	-20.89	32.33	106.19	190.27	0.23	-0.68
162	Fondazio ne	62, 63	0	-95.00	-4.01	102.19	-99.15	-0.10	0.89
			35	-84.82	-4.01	67.53	-89.82	-0.38	0.72
			69	-74.68	-4.01	36.14	-80.50	-0.60	0.57
163	Fondazio ne	62, 63	0	-67.20	-17.27	43.03	-42.35	-0.60	-0.79
			35	-57.08	-17.27	27.85	-34.14	-0.30	-0.93
			69	-46.98	-17.27	15.22	-27.74	0.04	-1.06
164	Fondazio ne	63, 64	0	-47.09	-25.59	34.86	-59.35	-0.19	-0.19
			35	-37.01	-25.59	13.15	-55.26	-0.11	-0.30
			69	-26.95	-25.59	-7.61	-53.90	0.02	-0.40
165	Fondazio ne	63, 64	0	-24.88	-25.44	7.85	-53.71	0.02	-0.25
			35	-14.82	-25.44	-12.86	-55.18	0.12	-0.33
			69	-4.78	-25.44	-34.55	-59.37	0.25	-0.41
166	Fondazio ne	64, 65	0	-4.60	-17.89	-14.79	-28.39	0.02	-0.84
			35	5.45	-17.89	-27.66	-34.91	0.32	-0.90

			69	15.49	-17.90	-43.10	-43.26	0.64	-0.95
167	Fondazio ne	64, 65	0	23.64	-4.58	-35.93	-80.66	0.64	0.70
			35	33.69	-4.58	-67.38	-90.14	0.40	0.67
			69	43.76	-4.59	-102.15	-99.65	0.17	0.66
168	Fondazio ne	65, 66	0	-28.51	30.91	-105.66	186.38	-0.15	-0.52
			35	-18.44	30.91	-44.81	178.49	0.02	-0.51
			69	-8.38	30.91	13.82	173.66	0.20	-0.48
169	Fondazio ne	65, 66	0	6.33	25.20	-6.38	170.11	0.20	1.22
			35	16.40	25.20	49.96	168.72	-0.23	1.27
			69	26.47	25.20	106.35	170.27	-0.68	1.34
170	Fondazio ne	66, 67	0	-44.05	9.83	99.41	-75.81	-0.61	-0.59
			35	-33.98	9.83	71.74	-72.83	-0.42	-0.50
			69	-23.93	9.83	45.10	-70.12	-0.27	-0.40
171	Fondazio ne	66, 67	0	-16.50	-15.13	46.43	-38.44	-0.27	0.51
			35	-6.46	-15.13	31.43	-37.19	-0.46	0.63
			69	3.58	-15.13	16.49	-38.21	-0.70	0.76
172	Fondazio ne	67, 68	0	2.59	-6.46	28.75	-47.93	-0.82	-1.80
			35	12.64	-6.46	9.64	-51.74	-0.22	-1.66
			69	22.68	-6.46	-11.32	-58.68	0.32	-1.51
173	Fondazio ne	67, 68	0	23.57	-20.96	-4.45	-53.75	0.32	1.57
			35	33.63	-20.96	-26.66	-63.83	-0.25	1.73
			69	43.70	-20.97	-52.84	-76.73	-0.87	1.90
174	Fondazio ne	68, 69	0	42.53	-2.03	-41.04	-62.68	-0.91	-2.73
			35	52.61	-2.03	-67.22	-77.62	0.00	-2.55
			69	62.72	-2.03	-98.74	-93.46	0.85	-2.38
175	Fondazio ne	68, 69	0	70.65	-3.62	-98.41	-112.23	0.85	2.34
			35	80.79	-3.63	-141.80	-127.27	0.02	2.52
			69	90.96	-3.63	-189.92	-139.07	-0.88	2.71
176	Fondazio ne	69, 70	0	24.25	30.20	-192.33	77.62	-1.22	-3.33
			42	36.49	30.20	-164.05	72.42	-0.02	-2.43
			83	48.76	30.20	-134.89	82.88	0.80	-1.53
177	Fondazio ne	69, 70	0	71.10	30.24	-145.56	70.61	0.80	-3.14
			42	83.40	30.24	-112.97	102.11	1.92	-2.23
			83	95.75	30.24	-62.11	159.22	2.66	-1.30
178	Primo Impalcato	1, 2	0	-204.56	-2.39	108.31	-33.73	-75.85	-35.79
			83	-204.56	-2.39	80.28	-33.73	-46.10	-35.79
			166	-204.56	-2.39	52.24	-33.73	-16.34	-35.79
179	Primo Impalcato	1, 15	0	-37.76	-5.79	-6.93	12.82	85.42	128.39
			80	-37.76	-5.79	3.26	12.82	3.49	77.29
			159	-37.76	-5.79	13.45	12.82	-36.78	23.58
180	Primo Impalcato	2, 3	0	-151.31	-0.61	64.23	-62.23	-17.59	-10.46
			69	-151.31	-0.61	21.29	-62.23	-10.38	-10.46
			138	-151.31	-0.61	-21.65	-62.23	-3.16	-10.46
181	Primo Impalcato	3, 4	0	-149.21	0.17	-6.62	1.69	-3.55	-1.62
			69	-149.21	0.17	-5.45	1.69	-2.43	-1.62
			138	-149.21	0.17	-4.28	1.69	-1.32	-1.62
182	Primo Impalcato	4, 5	0	-147.21	0.63	10.46	5.24	-1.41	0.19
			69	-147.21	0.63	14.07	5.24	-1.54	0.19
			138	-147.21	0.63	17.69	5.24	-1.67	0.19
183	Primo Impalcato	5, 6	0	-145.27	0.96	33.71	-96.15	-1.55	-0.05
			69	-145.27	0.96	-32.64	-96.15	-1.52	-0.05
			138	-145.27	0.96	-98.99	-96.15	-1.48	-0.05
184	Primo Impalcato	6, 7	0	-99.41	1.15	-86.36	125.03	-1.38	-0.34
			69	-99.41	1.15	-0.09	125.03	-1.14	-0.34
			138	-99.41	1.15	86.18	125.03	-0.91	-0.34

185	Primo Impalcato	7, 8	0	-56.10	1.22	98.78	-77.76	-0.62	-0.71
			69	-56.10	1.22	45.13	-77.76	-0.13	-0.71
			138	-56.10	1.22	-8.52	-77.76	0.36	-0.71
186	Primo Impalcato	8, 9	0	-54.19	1.16	8.55	-77.59	0.62	-0.61
			69	-54.19	1.16	-44.98	-77.59	1.04	-0.61
			138	-54.19	1.16	-98.52	-77.59	1.46	-0.61
187	Primo Impalcato	9, 10	0	-13.70	0.97	-85.91	124.03	1.79	-0.08
			69	-13.70	0.97	-0.33	124.03	1.84	-0.08
			138	-13.70	0.97	85.25	124.03	1.89	-0.08
188	Primo Impalcato	10, 11	0	33.30	0.65	97.82	-96.27	1.84	-0.34
			69	33.30	0.65	31.39	-96.27	2.07	-0.34
			138	33.30	0.65	-35.03	-96.27	2.30	-0.34
189	Primo Impalcato	11, 12	0	35.20	0.14	-19.25	18.62	2.25	-2.44
			69	35.20	0.14	-6.40	18.62	3.93	-2.44
			138	35.20	0.14	6.45	18.62	5.61	-2.44
190	Primo Impalcato	12, 13	0	37.11	-0.65	21.48	-59.74	5.33	-8.73
			69	37.11	-0.65	-19.74	-59.74	11.35	-8.73
			138	37.11	-0.65	-60.96	-59.74	17.37	-8.73
191	Primo Impalcato	13, 14	0	85.69	-2.42	-48.77	-38.98	16.62	-18.10
			83	85.69	-2.42	-81.17	-38.98	31.66	-18.10
			166	85.69	-2.42	-113.57	-38.98	46.71	-18.10
192	Primo Impalcato	14, 16	0	25.31	-5.16	18.61	-22.83	48.02	65.88
			80	25.31	-5.16	0.45	-22.83	5.72	40.33
			159	25.31	-5.16	-17.70	-22.83	-15.76	13.48
193	Primo Impalcato	15, 17	0	-37.33	-4.77	15.79	-14.86	-32.91	20.61
			66	-37.33	-4.77	5.99	-14.86	-34.23	-16.62
			132	-37.33	-4.77	-3.82	-14.86	-10.98	-53.85
194	Primo Impalcato	16, 18	0	23.03	-4.65	-13.72	10.65	-14.23	13.20
			66	23.03	-4.65	-6.69	10.65	-16.80	-5.41
			132	23.03	-4.65	0.34	10.65	-7.08	-24.02
195	Primo Impalcato	17, 19	0	-33.84	-3.83	0.38	-0.50	-8.80	31.40
			66	-33.84	-3.83	0.05	-0.50	-17.23	-5.83
			132	-33.84	-3.83	-0.28	-0.50	-1.10	-43.06
196	Primo Impalcato	18, 20	0	22.04	-3.82	-0.40	-1.15	-8.11	16.71
			66	22.04	-3.82	-1.16	-1.15	-13.00	-1.90
			132	22.04	-3.82	-1.92	-1.15	-5.60	-20.51
197	Primo Impalcato	19, 21	0	-27.73	-2.90	4.09	-6.98	-1.52	35.90
			66	-27.73	-2.90	-0.52	-6.98	-12.93	-1.33
			132	-27.73	-2.90	-5.12	-6.98	0.23	-38.55
198	Primo Impalcato	20, 22	0	15.17	-2.92	-1.98	3.06	-5.74	18.33
			66	15.17	-2.92	0.04	3.06	-11.69	-0.28
			132	15.17	-2.92	2.06	3.06	-5.37	-18.89
199	Primo Impalcato	21, 23	0	-26.86	-2.06	-0.84	-0.96	1.60	33.80
			66	-26.86	-2.06	-1.47	-0.96	-8.42	-3.43
			132	-26.86	-2.06	-2.11	-0.96	6.13	-40.66
200	Primo Impalcato	22, 24	0	12.65	-2.00	1.91	-1.54	-5.97	17.37
			66	12.65	-2.00	0.90	-1.54	-11.29	-1.25
			132	12.65	-2.00	-0.12	-1.54	-4.32	-19.86
201	Primo Impalcato	23, 25	0	-22.54	-1.50	1.71	-3.01	6.09	40.06
			66	-22.54	-1.50	-0.28	-3.01	-8.06	2.84
			132	-22.54	-1.50	-2.27	-3.01	2.35	-34.39
202	Primo Impalcato	24, 26	0	8.66	-1.30	-1.09	1.28	-4.43	15.86
			66	8.66	-1.30	-0.24	1.28	-8.76	-2.75
			132	8.66	-1.30	0.60	1.28	-0.80	-21.36
203	Primo	25, 28	0	-22.69	-0.57	1.47	-0.76	4.90	62.18

	Impalcato								
			85	-22.69	-0.57	0.83	-0.76	-21.79	0.61
			170	-22.69	-0.57	0.18	-0.76	3.85	-60.95
204	Primo Impalcato	26, 27	0	6.71	-0.62	0.22	0.74	-0.98	18.56
			66	6.71	-0.62	0.70	0.74	-7.09	-0.05
			132	6.71	-0.62	1.19	0.74	-0.91	-18.66
205	Primo Impalcato	27, 29	0	5.27	-0.18	-1.67	2.83	-0.98	17.77
			66	5.27	-0.18	0.21	2.83	-6.57	-0.84
			132	5.27	-0.18	2.08	2.83	0.13	-19.45
206	Primo Impalcato	28, 30	0	-13.97	0.02	2.04	-2.85	2.18	39.80
			73	-13.97	0.02	-0.04	-2.85	-10.21	-5.88
			146	-13.97	0.02	-2.12	-2.85	10.76	-51.56
207	Primo Impalcato	29, 31	0	5.74	0.15	0.75	1.09	0.29	17.40
			66	5.74	0.15	1.47	1.09	-5.05	-1.21
			132	5.74	0.15	2.19	1.09	1.90	-19.83
208	Primo Impalcato	30, 32	0	-12.63	0.22	-1.41	0.49	10.20	40.28
			69	-12.63	0.22	-1.07	0.49	-3.63	0.11
			137	-12.63	0.22	-0.74	0.49	10.05	-40.06
209	Primo Impalcato	31, 33	0	6.34	0.34	-1.15	2.04	1.67	17.84
			66	6.34	0.34	0.20	2.04	-3.97	-0.77
			132	6.34	0.34	1.55	2.04	2.68	-19.38
210	Primo Impalcato	32, 34	0	-11.08	0.32	-0.79	0.36	9.91	41.62
			69	-11.08	0.32	-0.54	0.36	-4.74	0.84
			138	-11.08	0.32	-0.29	0.36	8.75	-39.93
211	Primo Impalcato	33, 35	0	12.08	0.44	-1.31	2.95	3.02	18.04
			66	12.08	0.44	0.64	2.95	-2.74	-0.57
			132	12.08	0.44	2.59	2.95	3.77	-19.18
212	Primo Impalcato	34, 36	0	-9.34	0.42	-0.87	0.85	8.77	40.92
			69	-9.34	0.42	-0.29	0.85	-5.40	0.15
			138	-9.34	0.42	0.30	0.85	8.57	-40.63
213	Primo Impalcato	35, 37	0	13.79	0.50	-0.72	1.47	3.42	17.78
			66	13.79	0.50	0.25	1.47	-2.17	-0.83
			132	13.79	0.50	1.22	1.47	4.52	-19.44
214	Primo Impalcato	36, 38	0	-7.45	0.49	-0.62	1.08	8.59	43.49
			69	-7.45	0.49	0.12	1.08	-7.35	2.72
			138	-7.45	0.49	0.87	1.08	4.85	-38.06
215	Primo Impalcato	37, 39	0	21.36	0.46	-1.97	2.65	5.02	17.75
			66	21.36	0.46	-0.22	2.65	-0.55	-0.86
			132	21.36	0.46	1.53	2.65	6.16	-19.47
216	Primo Impalcato	38, 40	0	-5.37	0.60	-0.22	1.00	4.57	45.44
			69	-5.37	0.60	0.46	1.00	-12.80	5.26
			137	-5.37	0.60	1.15	1.00	-2.64	-34.91
217	Primo Impalcato	39, 41	0	19.66	0.31	0.19	1.24	5.73	19.91
			66	19.66	0.31	1.01	1.24	-1.27	1.30
			132	19.66	0.31	1.82	1.24	4.01	-17.31
218	Primo Impalcato	40, 42	0	-2.96	0.78	-0.14	-1.67	-4.03	15.54
			69	-2.96	0.78	-1.29	-1.67	-0.68	-25.23
			138	-2.96	0.78	-2.44	-1.67	30.79	-66.00
219	Primo Impalcato	41, 44	0	25.06	0.17	-0.48	-0.75	4.10	19.93
			66	25.06	0.17	-0.97	-0.75	-2.91	1.31
			132	25.06	0.17	-1.46	-0.75	2.36	-17.30
220	Primo Impalcato	42, 43	0	0.22	0.31	-5.28	5.14	29.93	-0.73
			23	0.22	0.31	-4.10	5.14	30.41	-3.45
			46	0.22	0.31	-2.92	5.14	31.51	-6.17
221	Primo Impalcato	43, 45	0	-6.52	0.21	-0.43	-0.95	32.49	67.20

			66	-6.52	0.21	-1.05	-0.95	0.42	29.97
			132	-6.52	0.21	-1.68	-0.95	-7.08	-7.26
222	Primo Impalcato	44, 46	0	26.34	0.55	-0.80	2.19	2.97	20.86
			66	26.34	0.55	0.64	2.19	-4.65	2.25
			132	26.34	0.55	2.08	2.19	0.01	-16.37
223	Primo Impalcato	45, 47	0	-8.56	0.71	0.46	-0.46	-6.76	35.56
			66	-8.56	0.71	0.15	-0.46	-17.95	-1.67
			132	-8.56	0.71	-0.15	-0.46	-4.56	-38.90
224	Primo Impalcato	46, 48	0	28.95	0.86	1.21	-1.87	-0.56	20.99
			66	28.95	0.86	-0.02	-1.87	-8.27	2.38
			132	28.95	0.86	-1.26	-1.87	-3.70	-16.23
225	Primo Impalcato	47, 49	0	-15.37	1.49	2.04	-3.81	-3.66	35.02
			66	-15.37	1.49	-0.47	-3.81	-14.49	-2.20
			132	-15.37	1.49	-2.98	-3.81	-0.75	-39.43
226	Primo Impalcato	48, 50	0	32.49	1.52	0.51	-0.10	-2.60	20.39
			66	32.49	1.52	0.44	-0.10	-9.92	1.77
			132	32.49	1.52	0.37	-0.10	-4.94	-16.84
227	Primo Impalcato	49, 51	0	-18.38	2.46	-0.87	1.00	-2.10	37.19
			66	-18.38	2.46	-0.21	1.00	-14.35	-0.04
			132	-18.38	2.46	0.45	1.00	-2.04	-37.27
228	Primo Impalcato	50, 52	0	33.34	2.46	1.98	-2.78	-5.81	20.32
			66	33.34	2.46	0.14	-2.78	-13.08	1.71
			132	33.34	2.46	-1.69	-2.78	-8.07	-16.90
229	Primo Impalcato	51, 53	0	-25.54	3.48	2.62	-3.52	-1.64	43.17
			66	-25.54	3.48	0.30	-3.52	-17.85	5.94
			132	-25.54	3.48	-2.03	-3.52	-9.48	-31.29
230	Primo Impalcato	52, 54	0	31.90	3.52	0.51	-1.70	-6.33	20.58
			66	31.90	3.52	-0.61	-1.70	-13.77	1.97
			132	31.90	3.52	-1.74	-1.70	-8.93	-16.64
231	Primo Impalcato	53, 55	0	-29.65	4.54	0.42	10.03	-11.64	53.91
			66	-29.65	4.54	7.04	10.03	-34.94	16.68
			132	-29.65	4.54	13.66	10.03	-33.66	-20.54
232	Primo Impalcato	54, 56	0	31.76	4.38	-0.50	-10.71	-8.85	23.45
			66	31.76	4.38	-7.57	-10.71	-18.19	4.84
			132	31.76	4.38	-14.64	-10.71	-15.24	-13.77
233	Primo Impalcato	55, 57	0	-30.60	5.64	18.26	-24.97	-37.47	-22.42
			80	-30.60	5.64	-1.59	-24.97	1.87	-76.12
			159	-30.60	5.64	-21.44	-24.97	82.87	-127.22
234	Primo Impalcato	56, 70	0	28.39	5.01	-15.00	18.66	-14.60	-11.21
			80	28.39	5.01	-0.16	18.66	5.07	-38.06
			159	28.39	5.01	14.67	18.66	45.57	-63.61
235	Primo Impalcato	57, 58	0	-205.99	2.52	111.53	-36.49	73.18	33.57
			83	-205.99	2.52	81.21	-36.49	45.27	33.57
			166	-205.99	2.52	50.88	-36.49	17.37	33.57
236	Primo Impalcato	58, 59	0	-152.11	0.56	62.95	-60.54	18.45	10.73
			69	-152.11	0.56	21.17	-60.54	11.05	10.73
			138	-152.11	0.56	-20.60	-60.54	3.64	10.73
237	Primo Impalcato	59, 60	0	-149.99	-0.20	-5.51	17.76	4.00	2.07
			69	-149.99	-0.20	6.74	17.76	2.57	2.07
			138	-149.99	-0.20	18.99	17.76	1.14	2.07
238	Primo Impalcato	60, 61	0	-147.93	-0.67	34.85	-95.87	1.22	-0.19
			69	-147.93	-0.67	-31.29	-95.87	1.35	-0.19
			138	-147.93	-0.67	-97.44	-95.87	1.48	-0.19
239	Primo Impalcato	61, 62	0	-98.01	-0.97	-84.81	123.27	1.54	-0.21
			69	-98.01	-0.97	0.24	123.27	1.68	-0.21

			138	-98.01	-0.97	85.30	123.27	1.83	-0.21
240	Primo Impalcato	62, 63	0	-56.65	-1.15	97.95	-94.15	1.50	0.48
			69	-56.65	-1.15	32.99	-94.15	1.17	0.48
			138	-56.65	-1.15	-31.98	-94.15	0.84	0.48
241	Primo Impalcato	63, 64	0	-54.81	-1.19	-15.91	23.07	0.58	0.84
			69	-54.81	-1.19	0.01	23.07	0.00	0.84
			138	-54.81	-1.19	15.92	23.07	-0.58	0.84
242	Primo Impalcato	64, 65	0	-52.98	-1.14	31.99	-94.08	-0.84	0.53
			69	-52.98	-1.14	-32.92	-94.08	-1.20	0.53
			138	-52.98	-1.14	-97.83	-94.08	-1.57	0.53
243	Primo Impalcato	65, 66	0	-13.49	-0.95	-85.19	122.91	-1.88	-0.02
			69	-13.49	-0.95	-0.38	122.91	-1.86	-0.02
			138	-13.49	-0.95	84.43	122.91	-1.85	-0.02
244	Primo Impalcato	66, 67	0	33.04	-0.63	97.02	-95.68	-1.81	0.23
			69	33.04	-0.63	31.00	-95.68	-1.97	0.23
			138	33.04	-0.63	-35.02	-95.68	-2.13	0.23
245	Primo Impalcato	67, 68	0	34.94	-0.14	-19.25	18.75	-2.08	2.24
			69	34.94	-0.14	-6.31	18.75	-3.63	2.24
			138	34.94	-0.14	6.63	18.75	-5.17	2.24
246	Primo Impalcato	68, 69	0	36.86	0.62	21.65	-59.68	-4.89	8.54
			69	36.86	0.62	-19.53	-59.68	-10.78	8.54
			138	36.86	0.62	-60.70	-59.68	-16.68	8.54
247	Primo Impalcato	69, 70	0	85.42	2.30	-48.49	-39.35	-15.88	18.77
			83	85.42	2.30	-81.19	-39.35	-31.48	18.77
			166	85.42	2.30	-113.90	-39.35	-47.08	18.77
248	Primo Impalcato	1	0	215.46	9.74	2.19	-1.05	-27.79	7.00
			188	215.46	9.74	0.22	-1.05	3.84	-44.97
			376	215.46	9.74	-1.75	-1.05	157.51	-122.83
249	Primo Impalcato	2	0	-85.97	0.15	14.86	-19.24	-7.44	-3.93
			188	-85.97	0.15	-21.31	-19.24	-0.05	-3.93
			376	-85.97	0.15	-57.47	-19.24	7.34	-3.93
250	Primo Impalcato	3	0	34.14	-0.08	-2.38	-12.61	-9.01	-4.77
			188	34.14	-0.08	-26.09	-12.61	-0.05	-4.77
			376	34.14	-0.08	-49.80	-12.61	8.92	-4.77
251	Primo Impalcato	4	0	4.48	-0.14	-11.84	-7.05	-8.77	-4.70
			188	4.48	-0.14	-25.10	-7.05	0.07	-4.70
			376	4.48	-0.14	-38.35	-7.05	8.91	-4.70
252	Primo Impalcato	5	0	28.70	-0.17	-12.50	-4.31	-9.36	-4.90
			188	28.70	-0.17	-20.61	-4.31	-0.14	-4.90
			376	28.70	-0.17	-28.72	-4.31	9.07	-4.90
253	Primo Impalcato	6	0	165.66	-0.21	-8.02	-2.86	-7.40	-4.02
			188	165.66	-0.21	-13.38	-2.86	0.15	-4.02
			376	165.66	-0.21	-18.75	-2.86	7.71	-4.02
254	Primo Impalcato	7	0	-179.50	-0.23	-3.45	-0.28	-7.37	-4.01
			188	-179.50	-0.23	-3.97	-0.28	0.16	-4.01
			376	-179.50	-0.23	-4.50	-0.28	7.69	-4.01
255	Primo Impalcato	8	0	12.15	-0.23	3.24	0.91	-9.83	-5.06
			188	12.15	-0.23	4.94	0.91	-0.31	-5.06
			376	12.15	-0.23	6.65	0.91	9.21	-5.06
256	Primo Impalcato	9	0	201.93	-0.21	9.40	2.12	-7.35	-4.00
			188	201.93	-0.21	13.39	2.12	0.17	-4.00
			376	201.93	-0.21	17.38	2.12	7.68	-4.00
257	Primo Impalcato	10	0	-156.40	-0.17	12.22	4.92	-7.33	-3.99
			188	-156.40	-0.17	21.48	4.92	0.17	-3.99
			376	-156.40	-0.17	30.73	4.92	7.67	-3.99

258	Primo Impalcato	11	0	-53.02	-0.12	12.52	7.34	-9.18	-4.83
			188	-53.02	-0.12	26.32	7.34	-0.10	-4.83
			376	-53.02	-0.12	40.12	7.34	8.97	-4.83
259	Primo Impalcato	12	0	-15.60	-0.03	6.31	11.01	-8.82	-4.67
			188	-15.60	-0.03	27.00	11.01	-0.05	-4.67
			376	-15.60	-0.03	47.70	11.01	8.73	-4.67
260	Primo Impalcato	13	0	106.70	0.23	-3.41	13.50	-7.32	-3.86
			188	106.70	0.23	21.98	13.50	-0.05	-3.86
			376	106.70	0.23	47.36	13.50	7.21	-3.86
261	Primo Impalcato	14	0	-231.11	7.51	-2.00	1.13	-44.44	-20.78
			188	-231.11	7.51	0.12	1.13	17.03	-46.76
			376	-231.11	7.51	2.25	1.13	139.50	-85.69
262	Primo Impalcato	15	0	34.31	4.93	0.00	0.06	-166.74	-100.91
			188	34.31	4.93	0.11	0.06	106.83	-198.20
			376	34.31	4.93	0.23	0.06	608.89	-343.99
263	Primo Impalcato	16	0	-57.33	3.89	-0.58	0.24	-75.31	-79.75
			188	-57.33	3.89	-0.13	0.24	116.55	-128.39
			376	-57.33	3.89	0.33	0.24	422.65	-201.28
264	Primo Impalcato	17	0	29.00	3.02	-0.99	0.51	-238.30	-188.73
			188	29.00	3.02	-0.02	0.51	194.65	-279.39
			376	29.00	3.02	0.95	0.51	840.52	-415.23
265	Primo Impalcato	18	0	-41.07	2.95	0.56	-0.29	-102.94	-141.60
			188	-41.07	2.95	0.01	-0.29	202.34	-186.93
			376	-41.07	2.95	-0.53	-0.29	614.07	-254.84
266	Primo Impalcato	19	0	26.48	2.19	-0.99	0.53	-232.50	-222.46
			188	26.48	2.19	0.00	0.53	263.87	-313.13
			376	26.48	2.19	0.99	0.53	973.16	-448.97
267	Primo Impalcato	20	0	-36.35	2.26	0.79	-0.42	-101.28	-177.39
			188	-36.35	2.26	0.00	-0.42	271.29	-222.72
			376	-36.35	2.26	-0.79	-0.42	750.29	-290.63
268	Primo Impalcato	21	0	34.67	1.63	-0.85	0.45	-222.89	-245.09
			188	34.67	1.63	0.00	0.45	316.03	-335.76
			376	34.67	1.63	0.85	0.45	1067.87	-471.60
269	Primo Impalcato	22	0	-39.04	1.65	0.76	-0.40	-95.81	-202.52
			188	-39.04	1.65	0.00	-0.40	323.99	-247.84
			376	-39.04	1.65	-0.75	-0.40	850.23	-315.76
270	Primo Impalcato	23	0	37.40	1.35	-0.48	0.25	-230.99	-269.43
			188	37.40	1.35	-0.01	0.25	353.69	-360.09
			376	37.40	1.35	0.46	0.25	1151.28	-495.94
271	Primo Impalcato	24	0	-38.50	1.06	0.53	-0.28	-94.35	-221.17
			188	-38.50	1.06	0.01	-0.28	360.50	-266.49
			376	-38.50	1.06	-0.51	-0.28	921.81	-334.40
272	Primo Impalcato	25	0	63.97	1.10	-0.37	0.18	-260.24	-295.69
			188	63.97	1.10	-0.02	0.18	382.50	-396.44
			376	63.97	1.10	0.33	0.18	1261.84	-547.40
273	Primo Impalcato	26	0	-55.79	0.63	0.56	-0.29	-94.25	-235.29
			188	-55.79	0.63	0.02	-0.29	387.16	-280.61
			376	-55.79	0.63	-0.52	-0.29	975.02	-348.53
274	Primo Impalcato	27	0	-45.89	0.31	0.48	-0.27	-91.93	-237.77
			188	-45.89	0.31	-0.02	-0.27	394.15	-283.10
			376	-45.89	0.31	-0.53	-0.27	986.68	-351.01
275	Primo Impalcato	28	0	53.06	0.03	-0.63	0.34	-273.65	-304.34
			188	53.06	0.03	0.02	0.34	388.71	-409.00
			376	53.06	0.03	0.66	0.34	1296.86	-565.81
276	Primo	29	0	-47.50	0.03	0.37	-0.19	-93.75	-239.80

	Impalcato								
			188	-47.50	0.03	0.01	-0.19	396.14	-285.13
			376	-47.50	0.03	-0.35	-0.19	992.48	-353.04
277	Primo Impalcato	30	0	56.25	-0.29	-0.55	0.29	-254.93	-298.98
			188	56.25	-0.29	-0.01	0.29	389.90	-394.98
			376	56.25	-0.29	0.53	0.29	1260.18	-538.82
278	Primo Impalcato	31	0	-50.17	-0.16	0.09	-0.06	-95.29	-238.93
			188	-50.17	-0.16	-0.02	-0.06	392.96	-284.26
			376	-50.17	-0.16	-0.13	-0.06	987.66	-352.17
279	Primo Impalcato	32	0	58.65	-0.23	-0.30	0.16	-241.32	-290.35
			188	58.65	-0.23	0.00	0.16	385.37	-384.14
			376	58.65	-0.23	0.30	0.16	1232.34	-524.68
280	Primo Impalcato	33	0	-50.62	-0.28	0.02	-0.02	-95.57	-235.70
			188	-50.62	-0.28	-0.01	-0.02	386.62	-281.03
			376	-50.62	-0.28	-0.04	-0.02	975.25	-348.94
281	Primo Impalcato	34	0	60.95	-0.23	-0.15	0.08	-240.96	-286.79
			188	60.95	-0.23	-0.01	0.08	379.28	-380.86
			376	60.95	-0.23	0.13	0.08	1220.46	-521.82
282	Primo Impalcato	35	0	-53.71	-0.33	-0.11	0.05	-94.86	-231.13
			188	-53.71	-0.33	-0.02	0.05	378.72	-276.45
			376	-53.71	-0.33	0.07	0.05	958.76	-344.37
283	Primo Impalcato	36	0	65.19	-0.28	-0.08	0.04	-244.39	-284.39
			188	65.19	-0.28	-0.01	0.04	371.35	-378.47
			376	65.19	-0.28	0.07	0.04	1208.02	-519.42
284	Primo Impalcato	37	0	-49.86	-0.34	-0.17	0.08	-95.72	-226.91
			188	-49.86	-0.34	-0.02	0.08	369.94	-272.24
			376	-49.86	-0.34	0.14	0.08	942.04	-340.15
285	Primo Impalcato	38	0	65.57	-0.46	-0.12	0.06	-243.35	-279.06
			188	65.57	-0.46	0.00	0.06	362.12	-372.85
			376	65.57	-0.46	0.12	0.06	1187.86	-513.38
286	Primo Impalcato	39	0	-52.74	-0.24	-0.19	0.10	-98.90	-224.42
			188	-52.74	-0.24	0.00	0.10	362.08	-269.75
			376	-52.74	-0.24	0.19	0.10	929.51	-337.66
287	Primo Impalcato	40	0	59.25	-1.00	-0.23	0.13	-210.25	-255.35
			188	59.25	-1.00	0.01	0.13	350.66	-349.15
			376	59.25	-1.00	0.26	0.13	1131.83	-489.68
288	Primo Impalcato	41	0	-55.66	-0.19	-0.41	0.21	-102.06	-223.73
			188	-55.66	-0.19	-0.01	0.21	357.63	-269.06
			376	-55.66	-0.19	0.39	0.21	923.76	-336.97
289	Primo Impalcato	42	0	43.27	-0.73	0.04	-0.01	-168.79	-246.46
			188	43.27	-0.73	0.02	-0.01	347.64	-308.05
			376	43.27	-0.73	0.00	-0.01	1008.73	-400.34
290	Primo Impalcato	43	0	41.72	-0.06	0.40	-0.21	-169.42	-248.66
			188	41.72	-0.06	0.00	-0.21	349.69	-308.55
			376	41.72	-0.06	-0.41	-0.21	1009.44	-398.28
291	Primo Impalcato	44	0	-58.45	-0.25	-0.24	0.12	-99.30	-222.63
			188	-58.45	-0.25	-0.01	0.12	358.31	-267.95
			376	-58.45	-0.25	0.23	0.12	922.36	-335.87
292	Primo Impalcato	45	0	47.59	0.23	0.58	-0.30	-193.59	-238.08
			188	47.59	0.23	0.02	-0.30	332.14	-328.74
			376	47.59	0.23	-0.53	-0.30	1070.80	-464.59
293	Primo Impalcato	46	0	-38.15	-0.41	-0.35	0.17	-97.89	-214.45
			188	-38.15	-0.41	-0.04	0.17	344.34	-259.78
			376	-38.15	-0.41	0.28	0.17	893.02	-327.69
294	Primo Impalcato	47	0	36.44	-0.65	0.58	-0.30	-225.33	-248.64

			188	36.44	-0.65	0.01	-0.30	320.26	-339.31
			376	36.44	-0.65	-0.56	-0.30	1078.78	-475.15
295	Primo Impalcato	48	0	-30.93	-0.81	-0.48	0.26	-97.48	-205.92
			188	-30.93	-0.81	0.01	0.26	328.72	-251.24
			376	-30.93	-0.81	0.49	0.26	861.35	-319.16
296	Primo Impalcato	49	0	38.85	-1.31	0.70	-0.36	-228.28	-236.09
			188	38.85	-1.31	0.02	-0.36	293.72	-326.76
			376	38.85	-1.31	-0.67	-0.36	1028.64	-462.60
297	Primo Impalcato	50	0	-36.66	-1.31	-0.60	0.32	-97.35	-191.53
			188	-36.66	-1.31	0.01	0.32	301.79	-236.85
			376	-36.66	-1.31	0.62	0.32	807.37	-304.77
298	Primo Impalcato	51	0	32.65	-1.96	0.76	-0.39	-234.42	-216.04
			188	32.65	-1.96	0.02	-0.39	249.88	-306.70
			376	32.65	-1.96	-0.72	-0.39	947.09	-442.54
299	Primo Impalcato	52	0	-41.09	-2.01	-0.68	0.36	-101.96	-170.63
			188	-41.09	-2.01	0.01	0.36	257.89	-215.95
			376	-41.09	-2.01	0.69	0.36	724.18	-283.87
300	Primo Impalcato	53	0	29.36	-2.83	0.68	-0.34	-238.53	-185.14
			188	29.36	-2.83	0.04	-0.34	187.67	-275.80
			376	29.36	-2.83	-0.60	-0.34	826.79	-411.64
301	Primo Impalcato	54	0	-40.69	-2.75	-0.53	0.27	-106.12	-139.10
			188	-40.69	-2.75	-0.02	0.27	194.44	-184.42
			376	-40.69	-2.75	0.49	0.27	601.46	-252.34
302	Primo Impalcato	55	0	42.48	-4.79	-0.45	0.17	-167.61	-99.85
			188	42.48	-4.79	-0.13	0.17	103.98	-197.15
			376	42.48	-4.79	0.19	0.17	604.05	-342.93
303	Primo Impalcato	56	0	-57.75	-3.77	0.73	-0.31	-74.98	-77.95
			188	-57.75	-3.77	0.14	-0.31	113.50	-126.59
			376	-57.75	-3.77	-0.45	-0.31	416.21	-199.48
304	Primo Impalcato	57	0	212.38	-9.69	-1.17	0.76	-27.26	6.91
			188	212.38	-9.69	0.25	0.76	4.53	-45.05
			376	212.38	-9.69	1.67	0.76	158.36	-122.91
305	Primo Impalcato	58	0	-84.91	-0.17	-10.92	18.15	-7.46	-3.95
			188	-84.91	-0.17	23.20	18.15	-0.04	-3.95
			376	-84.91	-0.17	57.33	18.15	7.38	-3.95
306	Primo Impalcato	59	0	23.19	0.08	3.72	12.73	-9.04	-4.79
			188	23.19	0.08	27.66	12.73	-0.03	-4.79
			376	23.19	0.08	51.59	12.73	8.97	-4.79
307	Primo Impalcato	60	0	49.55	0.14	12.33	7.54	-9.37	-4.93
			188	49.55	0.14	26.50	7.54	-0.10	-4.93
			376	49.55	0.14	40.67	7.54	9.17	-4.93
308	Primo Impalcato	61	0	151.24	0.17	12.46	4.79	-7.45	-4.05
			188	151.24	0.17	21.46	4.79	0.17	-4.05
			376	151.24	0.17	30.46	4.79	7.79	-4.05
309	Primo Impalcato	62	0	-193.34	0.21	9.55	1.99	-7.41	-4.02
			188	-193.34	0.21	13.30	1.99	0.15	-4.02
			376	-193.34	0.21	17.04	1.99	7.71	-4.02
310	Primo Impalcato	63	0	-58.66	0.23	3.52	0.68	-9.29	-4.86
			188	-58.66	0.23	4.80	0.68	-0.15	-4.86
			376	-58.66	0.23	6.09	0.68	9.00	-4.86
311	Primo Impalcato	64	0	58.19	0.23	-2.58	-0.54	-9.27	-4.85
			188	58.19	0.23	-3.59	-0.54	-0.15	-4.85
			376	58.19	0.23	-4.60	-0.54	8.98	-4.85
312	Primo Impalcato	65	0	192.68	0.21	-8.46	-1.89	-7.35	-3.99
			188	192.68	0.21	-12.01	-1.89	0.15	-3.99

			376	192.68	0.21	-15.56	-1.89	7.65	-3.99
313	Primo Impalcato	66	0	-150.65	0.16	-11.25	-4.66	-7.33	-3.99
			188	-150.65	0.16	-20.01	-4.66	0.16	-3.99
			376	-150.65	0.16	-28.76	-4.66	7.66	-3.99
314	Primo Impalcato	67	0	-44.33	0.12	-11.60	-6.99	-9.17	-4.82
			188	-44.33	0.12	-24.74	-6.99	-0.10	-4.82
			376	-44.33	0.12	-37.89	-6.99	8.96	-4.82
315	Primo Impalcato	68	0	-8.06	0.04	-5.31	-10.71	-8.82	-4.67
			188	-8.06	0.04	-25.44	-10.71	-0.05	-4.67
			376	-8.06	0.04	-45.57	-10.71	8.73	-4.67
316	Primo Impalcato	69	0	113.36	-0.21	5.01	-13.65	-7.33	-3.87
			188	113.36	-0.21	-20.65	-13.65	-0.05	-3.87
			376	113.36	-0.21	-46.31	-13.65	7.23	-3.87
317	Primo Impalcato	70	0	-240.44	-7.35	2.63	-1.39	-44.91	-21.19
			188	-240.44	-7.35	0.01	-1.39	17.33	-47.17
			376	-240.44	-7.35	-2.61	-1.39	140.57	-86.10
318	Fondazio ne	1, 71	0	3.37	0.13	0.00	0.00	0.99	-1.54
			102	3.37	0.13	0.00	0.00	2.55	-1.54
			204	3.37	0.13	0.00	0.00	4.12	-1.54
319	Fondazio ne	1, 92	0	279.06	0.02	0.00	0.00	1.06	0.09
			103	279.06	0.02	0.00	0.00	0.96	0.09
			206	279.06	0.02	0.00	0.00	0.87	0.09
320	Primo Impalcato	92, 2	0	-283.35	0.08	0.00	0.00	-1.09	-1.47
			103	-283.35	0.08	0.00	0.00	0.42	-1.47
			206	-283.35	0.08	0.00	0.00	1.93	-1.47
321	Fondazio ne	6, 89	0	345.56	-0.03	0.00	0.00	0.48	0.29
			100	345.56	-0.03	0.00	0.00	0.19	0.29
			200	345.56	-0.03	0.00	0.00	-0.10	0.29
322	Primo Impalcato	89, 7	0	-351.41	-0.01	0.00	0.00	0.50	0.20
			100	-351.41	-0.01	0.00	0.00	0.30	0.20
			200	-351.41	-0.01	0.00	0.00	0.10	0.20
323	Fondazio ne	9, 90	0	352.83	0.00	0.00	0.00	-0.41	0.13
			100	352.83	0.00	0.00	0.00	-0.54	0.13
			200	352.83	0.00	0.00	0.00	-0.67	0.13
324	Primo Impalcato	90, 10	0	-341.10	-0.03	0.00	0.00	-0.14	0.32
			100	-341.10	-0.03	0.00	0.00	-0.46	0.32
			200	-341.10	-0.03	0.00	0.00	-0.78	0.32
325	Fondazio ne	13, 91	0	283.31	0.07	0.00	0.00	-1.53	-1.17
			103	283.31	0.07	0.00	0.00	-0.33	-1.17
			206	283.31	0.07	0.00	0.00	0.87	-1.17
326	Primo Impalcato	88, 14	0	3.91	0.08	0.00	0.00	-3.03	-1.08
			102	3.91	0.08	0.00	0.00	-1.93	-1.08
			204	3.91	0.08	0.00	0.00	-0.83	-1.08
327	Primo Impalcato	91, 14	0	-279.11	0.02	0.00	0.00	-0.89	-0.06
			103	-279.11	0.02	0.00	0.00	-0.83	-0.06
			206	-279.11	0.02	0.00	0.00	-0.78	-0.06
328	Primo Impalcato	71, 15	0	24.82	0.26	0.00	0.00	-2.58	-3.26
			102	24.82	0.26	0.00	0.00	0.75	-3.26
			204	24.82	0.26	0.00	0.00	4.08	-3.26
329	Fondazio ne	16, 88	0	-37.69	0.18	0.00	0.00	-3.01	-2.24
			102	-37.69	0.18	0.00	0.00	-0.73	-2.24
			204	-37.69	0.18	0.00	0.00	1.56	-2.24
330	Fondazio ne	17, 72	0	21.17	-0.09	0.00	0.00	7.33	1.92
			100	21.17	-0.09	0.00	0.00	5.42	1.92
			199	21.17	-0.09	0.00	0.00	3.51	1.92

331	Primo Impalcato	87, 18	0	-17.29	-0.06	0.00	0.00	-3.46	1.06
			100	-17.29	-0.06	0.00	0.00	-4.52	1.06
			199	-17.29	-0.06	0.00	0.00	-5.57	1.06
332	Primo Impalcato	72, 19	0	-12.93	0.25	0.00	0.00	1.18	-3.58
			100	-12.93	0.25	0.00	0.00	4.75	-3.58
			199	-12.93	0.25	0.00	0.00	8.31	-3.58
333	Fondazione	20, 87	0	5.28	0.22	0.00	0.00	-6.57	-2.75
			100	5.28	0.22	0.00	0.00	-3.83	-2.75
			199	5.28	0.22	0.00	0.00	-1.08	-2.75
334	Fondazione	21, 73	0	16.78	-0.17	0.00	0.00	9.29	2.63
			100	16.78	-0.17	0.00	0.00	6.67	2.63
			199	16.78	-0.17	0.00	0.00	4.05	2.63
335	Primo Impalcato	86, 22	0	-16.52	-0.14	0.00	0.00	-3.87	1.91
			100	-16.52	-0.14	0.00	0.00	-5.77	1.91
			199	-16.52	-0.14	0.00	0.00	-7.67	1.91
336	Primo Impalcato	73, 23	0	-5.75	0.27	0.00	0.00	2.67	-3.63
			100	-5.75	0.27	0.00	0.00	6.29	-3.63
			199	-5.75	0.27	0.00	0.00	9.91	-3.63
337	Fondazione	24, 86	0	4.31	0.23	0.00	0.00	-8.21	-2.80
			100	4.31	0.23	0.00	0.00	-5.42	-2.80
			199	4.31	0.23	0.00	0.00	-2.63	-2.80
338	Fondazione	25, 74	0	19.80	-0.28	0.00	0.00	10.52	3.25
			103	19.80	-0.28	0.00	0.00	7.17	3.25
			206	19.80	-0.28	0.00	0.00	3.81	3.25
339	Primo Impalcato	85, 26	0	-17.73	-0.19	0.00	0.00	-3.90	2.46
			100	-17.73	-0.19	0.00	0.00	-6.35	2.46
			199	-17.73	-0.19	0.00	0.00	-8.81	2.46
340	Fondazione	27, 85	0	1.52	0.23	0.00	0.00	-8.73	-2.61
			100	1.52	0.23	0.00	0.00	-6.13	-2.61
			199	1.52	0.23	0.00	0.00	-3.53	-2.61
341	Primo Impalcato	74, 28	0	-2.90	0.32	0.00	0.00	3.18	-3.55
			103	-2.90	0.32	0.00	0.00	6.85	-3.55
			206	-2.90	0.32	0.00	0.00	10.52	-3.55
342	Primo Impalcato	84, 29	0	-11.66	-0.21	0.00	0.00	-3.72	2.58
			100	-11.66	-0.21	0.00	0.00	-6.29	2.58
			199	-11.66	-0.21	0.00	0.00	-8.86	2.58
343	Fondazione	31, 84	0	-3.87	0.21	0.00	0.00	-8.80	-2.51
			100	-3.87	0.21	0.00	0.00	-6.30	-2.51
			199	-3.87	0.21	0.00	0.00	-3.80	-2.51
344	Primo Impalcato	83, 33	0	-8.07	-0.22	0.00	0.00	-3.52	2.58
			100	-8.07	-0.22	0.00	0.00	-6.09	2.58
			199	-8.07	-0.22	0.00	0.00	-8.65	2.58
345	Fondazione	35, 83	0	-8.40	0.19	0.00	0.00	-8.54	-2.37
			100	-8.40	0.19	0.00	0.00	-6.17	-2.37
			199	-8.40	0.19	0.00	0.00	-3.81	-2.37
346	Primo Impalcato	82, 37	0	-5.52	-0.21	0.00	0.00	-3.39	2.47
			100	-5.52	-0.21	0.00	0.00	-5.86	2.47
			199	-5.52	-0.21	0.00	0.00	-8.32	2.47
347	Fondazione	39, 82	0	-10.50	0.19	0.00	0.00	-8.24	-2.30
			100	-10.50	0.19	0.00	0.00	-5.95	-2.30
			199	-10.50	0.19	0.00	0.00	-3.65	-2.30
348	Primo Impalcato	78, 43	0	-1.41	-0.19	0.00	0.00	-3.67	2.62
			100	-1.41	-0.19	0.00	0.00	-6.28	2.62
			199	-1.41	-0.19	0.00	0.00	-8.90	2.62
349	Primo	81, 44	0	-4.36	-0.20	0.00	0.00	-3.20	2.54

	Impalcato								
			100	-4.36	-0.20	0.00	0.00	-5.72	2.54
			199	-4.36	-0.20	0.00	0.00	-8.25	2.54
350	Fondazio ne	45, 78	0	15.65	0.23	0.00	0.00	-9.07	-2.97
			100	15.65	0.23	0.00	0.00	-6.11	-2.97
			199	15.65	0.23	0.00	0.00	-3.15	-2.97
351	Fondazio ne	46, 81	0	-10.65	0.18	0.00	0.00	-7.88	-2.18
			100	-10.65	0.18	0.00	0.00	-5.71	-2.18
			199	-10.65	0.18	0.00	0.00	-3.54	-2.18
352	Primo Impalcato	77, 47	0	-3.88	-0.24	0.00	0.00	-2.62	3.37
			100	-3.88	-0.24	0.00	0.00	-5.98	3.37
			199	-3.88	-0.24	0.00	0.00	-9.33	3.37
353	Primo Impalcato	80, 48	0	4.08	-0.21	0.00	0.00	-2.53	2.56
			100	4.08	-0.21	0.00	0.00	-5.08	2.56
			199	4.08	-0.21	0.00	0.00	-7.63	2.56
354	Fondazio ne	49, 77	0	15.66	0.17	0.00	0.00	-8.97	-2.73
			100	15.66	0.17	0.00	0.00	-6.25	-2.73
			199	15.66	0.17	0.00	0.00	-3.53	-2.73
355	Fondazio ne	50, 80	0	-14.30	0.14	0.00	0.00	-7.26	-1.89
			100	-14.30	0.14	0.00	0.00	-5.37	-1.89
			199	-14.30	0.14	0.00	0.00	-3.49	-1.89
356	Primo Impalcato	76, 51	0	-6.55	-0.24	0.00	0.00	-1.18	3.46
			100	-6.55	-0.24	0.00	0.00	-4.63	3.46
			199	-6.55	-0.24	0.00	0.00	-8.07	3.46
357	Fondazio ne	53, 76	0	16.00	0.09	0.00	0.00	-7.22	-1.96
			100	16.00	0.09	0.00	0.00	-5.27	-1.96
			199	16.00	0.09	0.00	0.00	-3.31	-1.96
358	Primo Impalcato	75, 55	0	31.60	-0.26	0.00	0.00	2.55	3.24
			102	31.60	-0.26	0.00	0.00	-0.75	3.24
			204	31.60	-0.26	0.00	0.00	-4.06	3.24
359	Fondazio ne	56, 79	0	-39.90	-0.18	0.00	0.00	2.97	2.20
			102	-39.90	-0.18	0.00	0.00	0.73	2.20
			204	-39.90	-0.18	0.00	0.00	-1.51	2.20
360	Fondazio ne	57, 75	0	-2.32	-0.12	0.00	0.00	-1.01	1.49
			102	-2.32	-0.12	0.00	0.00	-2.53	1.49
			204	-2.32	-0.12	0.00	0.00	-4.05	1.49
361	Fondazio ne	57, 93	0	281.20	-0.03	0.00	0.00	-1.03	-0.05
			103	281.20	-0.03	0.00	0.00	-0.97	-0.05
			206	281.20	-0.03	0.00	0.00	-0.92	-0.05
362	Primo Impalcato	93, 58	0	-285.61	-0.08	0.00	0.00	1.07	1.46
			103	-285.61	-0.08	0.00	0.00	-0.43	1.46
			206	-285.61	-0.08	0.00	0.00	-1.93	1.46
363	Fondazio ne	61, 95	0	344.33	0.03	0.00	0.00	-0.77	-0.31
			100	344.33	0.03	0.00	0.00	-0.46	-0.31
			200	344.33	0.03	0.00	0.00	-0.14	-0.31
364	Primo Impalcato	95, 62	0	-357.68	0.00	0.00	0.00	-0.66	-0.13
			100	-357.68	0.00	0.00	0.00	-0.53	-0.13
			200	-357.68	0.00	0.00	0.00	-0.40	-0.13
365	Primo Impalcato	96, 65	0	352.01	0.00	0.00	0.00	-0.63	-0.13
			100	352.01	0.00	0.00	0.00	-0.50	-0.13
			200	352.01	0.00	0.00	0.00	-0.37	-0.13
366	Fondazio ne	66, 96	0	-341.19	0.03	0.00	0.00	-0.73	-0.31
			100	-341.19	0.03	0.00	0.00	-0.42	-0.31
			200	-341.19	0.03	0.00	0.00	-0.11	-0.31
367	Fondazio ne	69, 94	0	284.75	-0.07	0.00	0.00	1.50	1.15

			103	284.75	-0.07	0.00	0.00	0.33	1.15
			206	284.75	-0.07	0.00	0.00	-0.85	1.15
368	Primo Impalcato	79, 70	0	5.10	-0.07	0.00	0.00	2.95	1.03
			102	5.10	-0.07	0.00	0.00	1.90	1.03
			204	5.10	-0.07	0.00	0.00	0.84	1.03
369	Primo Impalcato	94, 70	0	-279.90	-0.02	0.00	0.00	0.84	0.03
			103	-279.90	-0.02	0.00	0.00	0.81	0.03
			206	-279.90	-0.02	0.00	0.00	0.79	0.03
370	Primo Impalcato	1, 71	0	24.82	0.12	0.00	0.00	-1.79	0.39
			102	24.82	0.12	0.00	0.00	-2.19	0.39
			204	24.82	0.12	0.00	0.00	-2.59	0.39
371	Primo Impalcato	1, 92	0	-283.35	0.29	0.00	0.00	-3.35	-1.15
			103	-283.35	0.29	0.00	0.00	-2.17	-1.15
			206	-283.35	0.29	0.00	0.00	-0.98	-1.15
372	Primo Impalcato	92, 2	0	279.06	-0.03	0.00	0.00	0.64	0.41
			103	279.06	-0.03	0.00	0.00	0.22	0.41
			206	279.06	-0.03	0.00	0.00	-0.20	0.41
373	Primo Impalcato	6, 89	0	-351.41	-0.03	0.00	0.00	0.61	0.08
			100	-351.41	-0.03	0.00	0.00	0.53	0.08
			200	-351.41	-0.03	0.00	0.00	0.45	0.08
374	Primo Impalcato	89, 7	0	345.56	-0.04	0.00	0.00	-0.05	0.17
			100	345.56	-0.04	0.00	0.00	-0.22	0.17
			200	345.56	-0.04	0.00	0.00	-0.39	0.17
375	Primo Impalcato	9, 90	0	-341.10	-0.05	0.00	0.00	0.20	0.19
			100	-341.10	-0.05	0.00	0.00	0.01	0.19
			200	-341.10	-0.05	0.00	0.00	-0.18	0.19
376	Primo Impalcato	90, 10	0	352.83	-0.01	0.00	0.00	-0.63	0.00
			100	352.83	-0.01	0.00	0.00	-0.63	0.00
			200	352.83	-0.01	0.00	0.00	-0.63	0.00
377	Primo Impalcato	13, 91	0	-279.11	-0.01	0.00	0.00	-0.20	0.26
			103	-279.11	-0.01	0.00	0.00	-0.47	0.26
			206	-279.11	-0.01	0.00	0.00	-0.73	0.26
378	Primo Impalcato	88, 14	0	-37.69	0.12	0.00	0.00	1.49	-0.21
			102	-37.69	0.12	0.00	0.00	1.70	-0.21
			204	-37.69	0.12	0.00	0.00	1.91	-0.21
379	Primo Impalcato	91, 14	0	283.31	0.21	0.00	0.00	0.79	-0.85
			103	283.31	0.21	0.00	0.00	1.67	-0.85
			206	283.31	0.21	0.00	0.00	2.55	-0.85
380	Primo Impalcato	71, 15	0	3.37	0.22	0.00	0.00	4.22	2.11
			102	3.37	0.22	0.00	0.00	2.06	2.11
			204	3.37	0.22	0.00	0.00	-0.09	2.11
381	Primo Impalcato	16, 88	0	3.91	0.18	0.00	0.00	-1.08	0.96
			102	3.91	0.18	0.00	0.00	-2.05	0.96
			204	3.91	0.18	0.00	0.00	-3.03	0.96
382	Primo Impalcato	17, 72	0	-12.93	0.17	0.00	0.00	-4.64	-3.03
			100	-12.93	0.17	0.00	0.00	-1.62	-3.03
			199	-12.93	0.17	0.00	0.00	1.40	-3.03
383	Primo Impalcato	87, 18	0	5.28	0.19	0.00	0.00	-1.27	-2.14
			100	5.28	0.19	0.00	0.00	0.86	-2.14
			199	5.28	0.19	0.00	0.00	3.00	-2.14
384	Primo Impalcato	72, 19	0	21.17	0.11	0.00	0.00	3.39	2.46
			100	21.17	0.11	0.00	0.00	0.93	2.46
			199	21.17	0.11	0.00	0.00	-1.52	2.46
385	Primo Impalcato	20, 87	0	-17.29	0.09	0.00	0.00	-0.01	1.67
			100	-17.29	0.09	0.00	0.00	-1.67	1.67

			199	-17.29	0.09	0.00	0.00	-3.33	1.67
386	Primo Impalcato	21, 73	0	-5.75	0.11	0.00	0.00	-3.62	-3.23
			100	-5.75	0.11	0.00	0.00	-0.39	-3.23
			199	-5.75	0.11	0.00	0.00	2.83	-3.23
387	Primo Impalcato	86, 22	0	4.31	0.14	0.00	0.00	-2.76	-2.48
			100	4.31	0.14	0.00	0.00	-0.29	-2.48
			199	4.31	0.14	0.00	0.00	2.19	-2.48
388	Primo Impalcato	73, 23	0	16.78	0.06	0.00	0.00	4.03	3.03
			100	16.78	0.06	0.00	0.00	1.01	3.03
			199	16.78	0.06	0.00	0.00	-2.00	3.03
389	Primo Impalcato	24, 86	0	-16.52	0.01	0.00	0.00	0.60	2.22
			100	-16.52	0.01	0.00	0.00	-1.61	2.22
			199	-16.52	0.01	0.00	0.00	-3.83	2.22
390	Primo Impalcato	25, 74	0	-2.90	0.08	0.00	0.00	-3.61	-3.35
			103	-2.90	0.08	0.00	0.00	-0.15	-3.35
			206	-2.90	0.08	0.00	0.00	3.30	-3.35
391	Primo Impalcato	85, 26	0	1.52	0.08	0.00	0.00	-3.60	-2.57
			100	1.52	0.08	0.00	0.00	-1.04	-2.57
			199	1.52	0.08	0.00	0.00	1.52	-2.57
392	Primo Impalcato	27, 85	0	-17.73	-0.04	0.00	0.00	1.05	2.50
			100	-17.73	-0.04	0.00	0.00	-1.45	2.50
			199	-17.73	-0.04	0.00	0.00	-3.94	2.50
393	Primo Impalcato	74, 28	0	19.80	-0.04	0.00	0.00	3.92	3.46
			103	19.80	-0.04	0.00	0.00	0.35	3.46
			206	19.80	-0.04	0.00	0.00	-3.22	3.46
394	Primo Impalcato	84, 29	0	-3.87	0.05	0.00	0.00	-3.85	-2.54
			100	-3.87	0.05	0.00	0.00	-1.32	-2.54
			199	-3.87	0.05	0.00	0.00	1.20	-2.54
395	Primo Impalcato	31, 84	0	-11.66	-0.06	0.00	0.00	1.31	2.55
			100	-11.66	-0.06	0.00	0.00	-1.24	2.55
			199	-11.66	-0.06	0.00	0.00	-3.78	2.55
396	Primo Impalcato	83, 33	0	-8.40	0.03	0.00	0.00	-3.85	-2.46
			100	-8.40	0.03	0.00	0.00	-1.40	-2.46
			199	-8.40	0.03	0.00	0.00	1.05	-2.46
397	Primo Impalcato	35, 83	0	-8.07	-0.06	0.00	0.00	1.37	2.49
			100	-8.07	-0.06	0.00	0.00	-1.11	2.49
			199	-8.07	-0.06	0.00	0.00	-3.59	2.49
398	Primo Impalcato	82, 37	0	-10.50	0.02	0.00	0.00	-3.69	-2.35
			100	-10.50	0.02	0.00	0.00	-1.35	-2.35
			199	-10.50	0.02	0.00	0.00	1.00	-2.35
399	Primo Impalcato	39, 82	0	-5.52	-0.05	0.00	0.00	1.36	2.42
			100	-5.52	-0.05	0.00	0.00	-1.05	2.42
			199	-5.52	-0.05	0.00	0.00	-3.47	2.42
400	Primo Impalcato	78, 43	0	15.65	0.00	0.00	0.00	-3.14	-2.37
			100	15.65	0.00	0.00	0.00	-0.77	-2.37
			199	15.65	0.00	0.00	0.00	1.59	-2.37
401	Primo Impalcato	81, 44	0	-10.65	0.02	0.00	0.00	-3.55	-2.31
			100	-10.65	0.02	0.00	0.00	-1.25	-2.31
			199	-10.65	0.02	0.00	0.00	1.04	-2.31
402	Primo Impalcato	45, 78	0	-1.41	-0.02	0.00	0.00	2.59	3.22
			100	-1.41	-0.02	0.00	0.00	-0.61	3.22
			199	-1.41	-0.02	0.00	0.00	-3.82	3.22
403	Primo Impalcato	46, 81	0	-4.36	-0.07	0.00	0.00	1.52	2.41
			100	-4.36	-0.07	0.00	0.00	-0.88	2.41
			199	-4.36	-0.07	0.00	0.00	-3.28	2.41

404	Primo Impalcato	77, 47	0	15.66	-0.01	0.00	0.00	-3.53	-2.97
			100	15.66	-0.01	0.00	0.00	-0.58	-2.97
			199	15.66	-0.01	0.00	0.00	2.38	-2.97
405	Primo Impalcato	80, 48	0	-14.30	0.00	0.00	0.00	-3.46	-2.13
			100	-14.30	0.00	0.00	0.00	-1.34	-2.13
			199	-14.30	0.00	0.00	0.00	0.78	-2.13
406	Primo Impalcato	49, 77	0	-3.88	-0.09	0.00	0.00	3.51	3.13
			100	-3.88	-0.09	0.00	0.00	0.39	3.13
			199	-3.88	-0.09	0.00	0.00	-2.73	3.13
407	Primo Impalcato	50, 80	0	4.08	-0.11	0.00	0.00	1.99	2.32
			100	4.08	-0.11	0.00	0.00	-0.32	2.32
			199	4.08	-0.11	0.00	0.00	-2.64	2.32
408	Primo Impalcato	76, 51	0	16.00	-0.10	0.00	0.00	-3.21	-2.45
			100	16.00	-0.10	0.00	0.00	-0.76	-2.45
			199	16.00	-0.10	0.00	0.00	1.69	-2.45
409	Primo Impalcato	53, 76	0	-6.55	-0.16	0.00	0.00	4.52	2.96
			100	-6.55	-0.16	0.00	0.00	1.57	2.96
			199	-6.55	-0.16	0.00	0.00	-1.38	2.96
410	Primo Impalcato	75, 55	0	-2.32	-0.21	0.00	0.00	-4.15	-2.13
			102	-2.32	-0.21	0.00	0.00	-1.98	-2.13
			204	-2.32	-0.21	0.00	0.00	0.20	-2.13
411	Primo Impalcato	56, 79	0	5.10	-0.17	0.00	0.00	1.03	-0.94
			102	5.10	-0.17	0.00	0.00	1.99	-0.94
			204	5.10	-0.17	0.00	0.00	2.95	-0.94
412	Primo Impalcato	57, 75	0	31.60	-0.13	0.00	0.00	1.79	-0.38
			102	31.60	-0.13	0.00	0.00	2.17	-0.38
			204	31.60	-0.13	0.00	0.00	2.56	-0.38
413	Primo Impalcato	57, 93	0	-285.61	-0.28	0.00	0.00	3.30	1.14
			103	-285.61	-0.28	0.00	0.00	2.13	1.14
			206	-285.61	-0.28	0.00	0.00	0.96	1.14
414	Primo Impalcato	93, 58	0	281.20	0.03	0.00	0.00	-0.70	-0.38
			103	281.20	0.03	0.00	0.00	-0.31	-0.38
			206	281.20	0.03	0.00	0.00	0.08	-0.38
415	Primo Impalcato	61, 95	0	-357.68	0.01	0.00	0.00	-0.64	-0.01
			100	-357.68	0.01	0.00	0.00	-0.63	-0.01
			200	-357.68	0.01	0.00	0.00	-0.62	-0.01
416	Primo Impalcato	95, 62	0	344.33	0.05	0.00	0.00	-0.19	-0.19
			100	344.33	0.05	0.00	0.00	0.01	-0.19
			200	344.33	0.05	0.00	0.00	0.20	-0.19
417	Primo Impalcato	96, 65	0	-341.19	0.05	0.00	0.00	-0.15	-0.19
			100	-341.19	0.05	0.00	0.00	0.03	-0.19
			200	-341.19	0.05	0.00	0.00	0.22	-0.19
418	Primo Impalcato	66, 96	0	352.01	0.01	0.00	0.00	-0.60	-0.01
			100	352.01	0.01	0.00	0.00	-0.59	-0.01
			200	352.01	0.01	0.00	0.00	-0.59	-0.01
419	Primo Impalcato	69, 94	0	-279.90	0.01	0.00	0.00	0.13	-0.27
			103	-279.90	0.01	0.00	0.00	0.41	-0.27
			206	-279.90	0.01	0.00	0.00	0.69	-0.27
420	Primo Impalcato	79, 70	0	-39.90	-0.12	0.00	0.00	-1.44	0.22
			102	-39.90	-0.12	0.00	0.00	-1.67	0.22
			204	-39.90	-0.12	0.00	0.00	-1.89	0.22
421	Primo Impalcato	94, 70	0	284.75	-0.21	0.00	0.00	-0.77	0.85
			103	284.75	-0.21	0.00	0.00	-1.65	0.85
			206	284.75	-0.21	0.00	0.00	-2.52	0.85
422	Copertura	1, 2	0	-265.72	-4.92	28.87	389.66	-369.98	-58.49

			83	-265.72	-4.92	352.76	389.66	-321.36	-58.49
			166	-265.72	-4.92	676.66	389.66	-272.73	-58.49
423	Copertura	15, 1	0	-37.23	10.92	16.27	-9.85	80.05	269.26
			80	-37.23	10.92	8.44	-9.85	-140.29	285.03
			159	-37.23	10.92	0.61	-9.85	-373.10	300.64
424	Copertura	2, 3	0	-190.91	-21.01	680.15	-108.87	-272.34	-45.33
			69	-190.91	-21.01	605.04	-108.87	-241.07	-45.33
			138	-190.91	-21.01	529.92	-108.87	-209.79	-45.33
425	Copertura	3, 4	0	-188.25	-7.56	535.63	-206.93	-209.48	-41.55
			69	-188.25	-7.56	392.85	-206.93	-180.81	-41.55
			138	-188.25	-7.56	250.07	-206.93	-152.14	-41.55
426	Copertura	4, 5	0	-185.54	3.20	256.01	-214.96	-152.18	-36.31
			69	-185.54	3.20	107.68	-214.96	-127.12	-36.31
			138	-185.54	3.20	-40.64	-214.96	-102.07	-36.31
427	Copertura	5, 6	0	-182.58	10.38	-34.28	-142.26	-102.36	-31.76
			69	-182.58	10.38	-132.44	-142.26	-80.44	-31.76
			138	-182.58	10.38	-230.60	-142.26	-58.53	-31.76
428	Copertura	6, 7	0	-102.82	14.12	-225.02	292.05	-59.09	-28.74
			69	-102.82	14.12	-23.51	292.05	-39.27	-28.74
			138	-102.82	14.12	178.00	292.05	-19.44	-28.74
429	Copertura	7, 8	0	-23.59	15.53	183.59	-141.34	-20.17	-27.88
			69	-23.59	15.53	86.07	-141.34	-0.93	-27.88
			138	-23.59	15.53	-11.46	-141.34	18.31	-27.88
430	Copertura	8, 9	0	-20.43	14.40	-4.81	-153.66	17.80	-28.89
			69	-20.43	14.40	-110.84	-153.66	37.74	-28.89
			138	-20.43	14.40	-216.86	-153.66	57.67	-28.89
431	Copertura	9, 10	0	58.15	10.56	-211.26	256.15	57.00	-31.74
			69	58.15	10.56	-34.52	256.15	78.90	-31.74
			138	58.15	10.56	142.23	256.15	100.79	-31.74
432	Copertura	10, 11	0	139.16	3.91	147.80	-191.52	100.47	-36.39
			69	139.16	3.91	15.65	-191.52	125.58	-36.39
			138	139.16	3.91	-116.50	-191.52	150.69	-36.39
433	Copertura	11, 12	0	142.09	-6.09	-110.24	-253.39	150.63	-41.63
			69	142.09	-6.09	-285.07	-253.39	179.35	-41.63
			138	142.09	-6.09	-459.91	-253.39	208.07	-41.63
434	Copertura	12, 13	0	144.84	-19.77	-454.02	-159.42	208.33	-46.35
			69	144.84	-19.77	-564.02	-159.42	240.31	-46.35
			138	144.84	-19.77	-674.01	-159.42	272.29	-46.35
435	Copertura	13, 14	0	226.56	-9.69	-670.47	358.52	272.56	-60.92
			83	226.56	-9.69	-372.47	358.52	323.20	-60.92
			166	226.56	-9.69	-74.46	358.52	373.83	-60.92
436	Copertura	16, 14	0	46.56	-6.57	-43.51	38.55	77.66	276.49
			80	46.56	-6.57	-12.86	38.55	-145.29	284.37
			159	46.56	-6.57	17.80	38.55	-374.47	292.18
437	Copertura	15, 17	0	-46.24	-3.12	18.48	3.19	13.28	178.73
			66	-46.24	-3.12	20.58	3.19	-101.28	168.43
			132	-46.24	-3.12	22.69	3.19	-209.05	158.13
438	Copertura	16, 18	0	59.10	-7.35	-39.85	-22.26	14.31	175.10
			66	59.10	-7.35	-54.54	-22.26	-99.56	169.95
			132	59.10	-7.35	-69.23	-22.26	-210.02	164.80
439	Copertura	17, 19	0	-53.81	-6.59	25.66	-11.06	-124.35	89.78
			66	-53.81	-6.59	18.36	-11.06	-180.20	79.47
			132	-53.81	-6.59	11.06	-11.06	-229.25	69.17
440	Copertura	18, 20	0	69.33	-6.89	-66.98	8.52	-126.22	82.84
			66	69.33	-6.89	-61.36	8.52	-179.19	77.69
			132	69.33	-6.89	-55.74	8.52	-228.77	72.54
441	Copertura	19, 21	0	-59.39	-5.39	14.26	-16.71	-162.37	38.71
			66	-59.39	-5.39	3.23	-16.71	-184.52	28.40
			132	-59.39	-5.39	-7.79	-16.71	-199.86	18.10
442	Copertura	20, 22	0	77.59	-4.80	-53.70	22.00	-164.49	33.70
			66	77.59	-4.80	-39.18	22.00	-185.03	28.55
			132	77.59	-4.80	-24.66	22.00	-202.18	23.40
443	Copertura	21, 23	0	-62.94	-2.66	-4.43	-4.57	-151.68	16.95
			66	-62.94	-2.66	-7.45	-4.57	-159.47	6.65
			132	-62.94	-2.66	-10.46	-4.57	-160.45	-3.66
444	Copertura	22, 24	0	83.73	-4.08	-23.15	14.55	-154.17	10.19
			66	83.73	-4.08	-13.54	14.55	-159.19	5.04
			132	83.73	-4.08	-3.94	14.55	-160.81	-0.12
445	Copertura	23, 25	0	-64.82	1.26	-7.13	0.27	-128.49	19.83
			66	-64.82	1.26	-6.95	0.27	-138.18	9.53
			132	-64.82	1.26	-6.77	0.27	-141.06	-0.78
446	Copertura	24, 26	0	87.78	-3.46	-2.71	8.59	-130.16	-0.80

			66	87.78	-3.46	2.96	8.59	-127.93	-5.95
			132	87.78	-3.46	8.63	8.59	-122.31	-11.10
447	Copertura	25, 28	0	-65.27	0.37	-3.35	-4.52	-122.89	-14.86
			85	-65.27	0.37	-7.19	-4.52	-102.25	-33.70
			170	-65.27	0.37	-11.03	-4.52	-65.60	-52.55
448	Copertura	26, 27	0	93.12	-1.95	12.20	5.68	-103.06	17.87
			66	93.12	-1.95	15.96	5.68	-113.16	12.72
			132	93.12	-1.95	19.71	5.68	-119.85	7.57
449	Copertura	27, 29	0	91.57	0.80	23.62	2.81	-113.52	-35.60
			66	91.57	0.80	25.47	2.81	-88.32	-40.75
			132	91.57	0.80	27.32	2.81	-59.73	-45.90
450	Copertura	28, 30	0	-68.81	-2.68	-3.92	-13.01	-59.26	6.46
			73	-68.81	-2.68	-13.42	-13.01	-59.16	-6.72
			146	-68.81	-2.68	-22.91	-13.01	-49.44	-19.90
451	Copertura	29, 31	0	90.03	0.94	36.02	-4.99	-60.47	-18.88
			66	90.03	0.94	32.73	-4.99	-46.31	-24.03
			132	90.03	0.94	29.43	-4.99	-28.75	-29.18
452	Copertura	30, 32	0	-71.42	-1.15	-13.97	-9.50	-50.25	-6.51
			69	-71.42	-1.15	-20.48	-9.50	-41.92	-17.81
			137	-71.42	-1.15	-26.99	-9.50	-25.85	-29.10
453	Copertura	31, 33	0	87.09	0.59	38.13	-11.94	-34.35	-9.70
			66	87.09	0.59	30.25	-11.94	-26.25	-14.85
			132	87.09	0.59	22.38	-11.94	-14.75	-20.00
454	Copertura	32, 34	0	-74.24	0.46	-17.49	-4.73	-31.22	-2.72
			69	-74.24	0.46	-20.76	-4.73	-25.38	-14.21
			138	-74.24	0.46	-24.02	-4.73	-11.61	-25.71
455	Copertura	33, 35	0	84.72	0.69	32.58	-12.07	-22.46	-6.40
			66	84.72	0.69	24.61	-12.07	-16.54	-11.55
			132	84.72	0.69	16.65	-12.07	-7.21	-16.71
456	Copertura	34, 36	0	-77.38	0.90	-14.16	-4.34	-19.62	0.41
			69	-77.38	0.90	-17.15	-4.34	-15.94	-11.09
			138	-77.38	0.90	-20.15	-4.34	-4.32	-22.58
457	Copertura	35, 37	0	81.70	1.00	27.05	-13.38	-16.66	-8.42
			66	81.70	1.00	18.22	-13.38	-9.40	-13.57
			132	81.70	1.00	9.39	-13.38	1.26	-18.72
458	Copertura	36, 38	0	-80.79	0.54	-10.08	-10.06	-13.90	-1.53
			69	-80.79	0.54	-17.03	-10.06	-8.88	-13.03
			138	-80.79	0.54	-23.97	-10.06	4.08	-24.52
459	Copertura	37, 39	0	78.83	2.28	20.43	-7.84	-9.08	-17.59
			66	78.83	2.28	15.25	-7.84	4.23	-22.74
			132	78.83	2.28	10.08	-7.84	20.94	-27.89
460	Copertura	38, 40	0	-84.61	-1.93	-13.62	-17.93	-6.18	-4.35
			69	-84.61	-1.93	-25.90	-17.93	0.67	-15.65
			137	-84.61	-1.93	-38.18	-17.93	15.26	-26.94
461	Copertura	39, 41	0	76.31	3.52	21.44	-8.88	10.98	-38.09
			66	76.31	3.52	15.58	-8.88	37.82	-43.24
			132	76.31	3.52	9.72	-8.88	68.06	-48.39
462	Copertura	40, 42	0	-89.19	-6.45	-27.02	-17.30	5.82	8.51
			69	-89.19	-6.45	-38.96	-17.30	3.92	-2.99
			138	-89.19	-6.45	-50.90	-17.30	9.95	-14.48
463	Copertura	41, 44	0	62.38	0.32	17.45	-8.23	60.72	83.54
			66	62.38	0.32	12.02	-8.23	7.29	78.39
			132	62.38	0.32	6.58	-8.23	-42.75	73.24
464	Copertura	42, 43	0	-88.53	0.37	-37.73	-6.15	1.89	-60.24
			23	-88.53	0.37	-39.14	-6.15	15.80	-60.68
			46	-88.53	0.37	-40.56	-6.15	29.81	-61.12
465	Copertura	43, 45	0	-86.44	7.01	-37.58	4.51	21.81	78.39
			66	-86.44	7.01	-34.60	4.51	-26.53	68.08
			132	-86.44	7.01	-31.62	4.51	-68.07	57.78
466	Copertura	44, 46	0	68.04	-1.46	13.35	-5.75	-49.22	21.57
			66	68.04	-1.46	9.55	-5.75	-61.75	16.42
			132	68.04	-1.46	5.76	-5.75	-70.89	11.27
467	Copertura	45, 47	0	-83.95	4.00	-28.82	11.91	-80.19	48.66
			66	-83.95	4.00	-20.96	11.91	-108.90	38.36
			132	-83.95	4.00	-13.10	11.91	-130.82	28.05
468	Copertura	46, 48	0	68.26	0.40	7.66	-10.32	-81.61	40.71
			66	68.26	0.40	0.85	-10.32	-106.77	35.55
			132	68.26	0.40	-5.96	-10.32	-128.54	30.40
469	Copertura	47, 49	0	-80.29	3.06	-10.21	12.71	-153.25	25.44
			66	-80.29	3.06	-1.82	12.71	-166.64	15.14
			132	-80.29	3.06	6.56	12.71	-173.23	4.83
470	Copertura	48, 50	0	67.62	2.29	-3.87	-17.81	-150.98	23.44

			66	67.62	2.29	-15.62	-17.81	-164.75	18.29
			132	67.62	2.29	-27.38	-17.81	-175.11	13.14
471	Copertura	49, 51	0	-74.83	4.38	9.59	14.63	-212.32	-7.63
			66	-74.83	4.38	19.25	14.63	-203.88	-17.93
			132	-74.83	4.38	28.91	14.63	-188.64	-28.24
472	Copertura	50, 52	0	64.79	4.43	-25.99	-23.06	-212.21	-11.30
			66	64.79	4.43	-41.20	-23.06	-203.05	-16.45
			132	64.79	4.43	-56.42	-23.06	-190.50	-21.60
473	Copertura	51, 53	0	-67.13	6.03	32.11	2.08	-248.19	-66.36
			66	-67.13	6.03	33.48	2.08	-200.99	-76.66
			132	-67.13	6.03	34.85	2.08	-146.99	-86.97
474	Copertura	52, 54	0	59.55	5.84	-55.30	-14.95	-249.82	-71.53
			66	59.55	5.84	-65.17	-14.95	-200.91	-76.68
			132	59.55	5.84	-75.04	-14.95	-148.60	-81.83
475	Copertura	53, 55	0	-57.17	2.59	38.39	-19.35	-226.64	-158.18
			66	-57.17	2.59	25.62	-19.35	-118.84	-168.49
			132	-57.17	2.59	12.85	-19.35	-4.24	-178.79
476	Copertura	54, 56	0	51.16	7.50	-75.27	19.39	-225.67	-163.81
			66	51.16	7.50	-62.47	19.39	-115.86	-168.96
			132	51.16	7.50	-49.67	19.39	-2.64	-174.11
477	Copertura	55, 57	0	-45.54	-10.92	17.20	-22.72	-94.19	-275.46
			80	-45.54	-10.92	-0.87	-22.72	131.08	-291.22
			159	-45.54	-10.92	-18.93	-22.72	368.81	-306.83
478	Copertura	56, 70	0	41.90	5.89	-49.89	39.09	-92.07	-278.88
			80	41.90	5.89	-18.81	39.09	132.78	-286.76
			159	41.90	5.89	12.27	39.09	363.87	-294.57
479	Copertura	57, 58	0	-269.40	8.01	34.40	370.84	365.85	59.78
			83	-269.40	8.01	342.66	370.84	316.17	59.78
			166	-269.40	8.01	650.91	370.84	266.48	59.78
480	Copertura	58, 59	0	-193.26	20.28	654.33	-139.69	266.15	45.09
			69	-193.26	20.28	557.94	-139.69	235.04	45.09
			138	-193.26	20.28	461.55	-139.69	203.92	45.09
481	Copertura	59, 60	0	-190.59	6.84	467.27	-241.18	203.65	41.02
			69	-190.59	6.84	300.86	-241.18	175.34	41.02
			138	-190.59	6.84	134.44	-241.18	147.04	41.02
482	Copertura	60, 61	0	-187.71	-3.59	140.58	-177.11	147.09	35.74
			69	-187.71	-3.59	18.37	-177.11	122.43	35.74
			138	-187.71	-3.59	-103.84	-177.11	97.77	35.74
483	Copertura	61, 62	0	-106.45	-10.43	-98.33	278.61	98.09	30.99
			69	-106.45	-10.43	93.91	278.61	76.71	30.99
			138	-106.45	-10.43	286.15	278.61	55.33	30.99
484	Copertura	62, 63	0	-29.04	-14.21	291.77	-124.19	55.99	28.12
			69	-29.04	-14.21	206.08	-124.19	36.59	28.12
			138	-29.04	-14.21	120.38	-124.19	17.19	28.12
485	Copertura	63, 64	0	-26.02	-15.24	126.89	-182.75	17.68	27.07
			69	-26.02	-15.24	0.79	-182.75	-1.00	27.07
			138	-26.02	-15.24	-125.30	-182.75	-19.68	27.07
486	Copertura	64, 65	0	-22.99	-14.12	-118.78	-123.80	-19.19	27.93
			69	-22.99	-14.12	-204.20	-123.80	-38.46	27.93
			138	-22.99	-14.12	-289.62	-123.80	-57.73	27.93
487	Copertura	65, 66	0	55.78	-10.36	-283.96	283.70	-57.07	30.54
			69	55.78	-10.36	-88.21	283.70	-78.15	30.54
			138	55.78	-10.36	107.54	283.70	-99.22	30.54
488	Copertura	66, 67	0	137.80	-3.83	113.13	-174.39	-98.90	34.94
			69	137.80	-3.83	-7.20	-174.39	-123.01	34.94
			138	137.80	-3.83	-127.52	-174.39	-147.12	34.94
489	Copertura	67, 68	0	140.72	6.00	-121.27	-244.48	-147.06	39.93
			69	140.72	6.00	-289.96	-244.48	-174.61	39.93
			138	140.72	6.00	-458.66	-244.48	-202.16	39.93
490	Copertura	68, 69	0	143.47	19.31	-452.77	-158.00	-202.41	44.33
			69	143.47	19.31	-561.79	-158.00	-233.00	44.33
			138	143.47	19.31	-670.81	-158.00	-263.59	44.33
491	Copertura	69, 70	0	225.42	8.05	-667.17	355.51	-263.86	58.13
			83	225.42	8.05	-371.67	355.51	-312.18	58.13
			166	225.42	8.05	-76.17	355.51	-360.50	58.13
492	Copertura	1	0	-241.61	2.81	-7.38	3.07	-39.46	27.41
			220	-241.61	2.81	-0.63	3.07	-58.68	-17.71
			440	-241.61	2.81	6.12	3.07	72.71	-109.51
493	Copertura	2	0	298.67	0.64	19.98	-2.45	-4.73	-2.17
			220	298.67	0.64	14.60	-2.45	0.04	-2.17
			440	298.67	0.64	9.22	-2.45	4.82	-2.17
494	Copertura	3	0	98.06	0.31	13.45	-3.78	-5.71	-2.66

			220	98.06	0.31	5.15	-3.78	0.15	-2.66
			440	98.06	0.31	-3.16	-3.78	6.02	-2.66
495	Copertura	4	0	8.03	-0.04	10.76	-5.24	-5.94	-2.71
			220	8.03	-0.04	-0.78	-5.24	0.02	-2.71
			440	8.03	-0.04	-12.31	-5.24	5.97	-2.71
496	Copertura	5	0	-72.70	-0.29	7.19	-4.55	-6.36	-2.96
			220	-72.70	-0.29	-2.82	-4.55	0.15	-2.96
			440	-72.70	-0.29	-12.84	-4.55	6.66	-2.96
497	Copertura	6	0	-187.84	-0.44	3.98	-2.93	-5.58	-2.46
			220	-187.84	-0.44	-2.45	-2.93	-0.18	-2.46
			440	-187.84	-0.44	-8.89	-2.93	5.22	-2.46
498	Copertura	7	0	188.59	-0.50	0.92	-0.83	-5.58	-2.46
			220	188.59	-0.50	-0.91	-0.83	-0.18	-2.46
			440	188.59	-0.50	-2.73	-0.83	5.23	-2.46
499	Copertura	8	0	12.32	-0.50	-1.13	1.01	-6.65	-3.16
			220	12.32	-0.50	1.09	1.01	0.30	-3.16
			440	12.32	-0.50	3.30	1.01	7.24	-3.16
500	Copertura	9	0	-167.15	-0.44	-3.34	2.77	-5.60	-2.47
			220	-167.15	-0.44	2.76	2.77	-0.17	-2.47
			440	-167.15	-0.44	8.87	2.77	5.26	-2.47
501	Copertura	10	0	197.20	-0.30	-6.65	4.48	-5.57	-2.46
			220	197.20	-0.30	3.21	4.48	-0.17	-2.46
			440	197.20	-0.30	13.07	4.48	5.24	-2.46
502	Copertura	11	0	61.87	-0.06	-10.01	5.24	-6.26	-2.93
			220	61.87	-0.06	1.51	5.24	0.17	-2.93
			440	61.87	-0.06	13.03	5.24	6.61	-2.93
503	Copertura	12	0	-93.97	0.25	-13.68	4.72	-5.90	-2.75
			220	-93.97	0.25	-3.29	4.72	0.16	-2.75
			440	-93.97	0.25	7.09	4.72	6.21	-2.75
504	Copertura	13	0	-299.64	0.56	-25.51	6.26	-5.01	-2.30
			220	-299.64	0.56	-11.75	6.26	0.06	-2.30
			440	-299.64	0.56	2.01	6.26	5.13	-2.30
505	Copertura	57	0	-234.76	-2.46	-8.21	3.84	-44.79	25.32
			220	-234.76	-2.46	0.23	3.84	-59.41	-19.80
			440	-234.76	-2.46	8.67	3.84	76.57	-111.60
506	Copertura	58	0	307.03	-0.58	-22.41	3.92	-4.78	-2.19
			220	307.03	-0.58	-13.79	3.92	0.05	-2.19
			440	307.03	-0.58	-5.17	3.92	4.87	-2.19
507	Copertura	59	0	101.49	-0.28	-13.44	4.07	-5.72	-2.67
			220	101.49	-0.28	-4.48	4.07	0.17	-2.67
			440	101.49	-0.28	4.48	4.07	6.05	-2.67
508	Copertura	60	0	-64.07	0.06	-10.42	5.28	-6.14	-2.87
			220	-64.07	0.06	1.19	5.28	0.18	-2.87
			440	-64.07	0.06	12.80	5.28	6.50	-2.87
509	Copertura	61	0	-204.36	0.30	-6.84	4.58	-5.51	-2.43
			220	-204.36	0.30	3.23	4.58	-0.16	-2.43
			440	-204.36	0.30	13.30	4.58	5.18	-2.43
510	Copertura	62	0	163.85	0.44	-3.29	2.80	-5.61	-2.47
			220	163.85	0.44	2.86	2.80	-0.18	-2.47
			440	163.85	0.44	9.01	2.80	5.25	-2.47
511	Copertura	63	0	58.56	0.49	-1.03	1.04	-6.51	-3.02
			220	58.56	0.49	1.26	1.04	0.14	-3.02
			440	58.56	0.49	3.56	1.04	6.78	-3.02
512	Copertura	64	0	-58.95	0.49	1.12	-0.85	-6.52	-3.03
			220	-58.95	0.49	-0.75	-0.85	0.14	-3.03
			440	-58.95	0.49	-2.62	-0.85	6.80	-3.03
513	Copertura	65	0	-164.28	0.43	3.26	-2.55	-5.66	-2.49
			220	-164.28	0.43	-2.34	-2.55	-0.18	-2.49
			440	-164.28	0.43	-7.94	-2.55	5.30	-2.49
514	Copertura	66	0	204.43	0.30	6.53	-4.23	-5.59	-2.47
			220	204.43	0.30	-2.78	-4.23	-0.17	-2.47
			440	204.43	0.30	-12.09	-4.23	5.26	-2.47
515	Copertura	67	0	70.10	0.06	9.84	-4.98	-6.26	-2.92
			220	70.10	0.06	-1.13	-4.98	0.17	-2.92
			440	70.10	0.06	-12.09	-4.98	6.60	-2.92
516	Copertura	68	0	-86.49	-0.25	13.31	-4.40	-5.89	-2.75
			220	-86.49	-0.25	3.62	-4.40	0.16	-2.75
			440	-86.49	-0.25	-6.07	-4.40	6.21	-2.75
517	Copertura	69	0	-294.98	-0.55	24.18	-5.55	-5.01	-2.30
			220	-294.98	-0.55	11.96	-5.55	0.06	-2.30
			440	-294.98	-0.55	-0.26	-5.55	5.13	-2.30
518	Primo	1, 74	0	213.65	-0.09	0.00	0.00	-0.39	-0.27

	Impalcato								
			118	213.65	-0.09	0.00	0.00	-0.08	-0.27
			235	213.65	-0.09	0.00	0.00	0.24	-0.27
519	Copertura	74, 2	0	-168.80	0.19	0.00	0.00	-1.63	-0.11
			118	-168.80	0.19	0.00	0.00	-1.50	-0.11
			235	-168.80	0.19	0.00	0.00	-1.37	-0.11
520	Primo Impalcato	6, 71	0	256.56	-0.07	0.00	0.00	-0.15	0.14
			115	256.56	-0.07	0.00	0.00	-0.31	0.14
			231	256.56	-0.07	0.00	0.00	-0.47	0.14
521	Copertura	71, 7	0	-258.31	-0.05	0.00	0.00	0.51	0.01
			115	-258.31	-0.05	0.00	0.00	0.49	0.01
			231	-258.31	-0.05	0.00	0.00	0.47	0.01
522	Primo Impalcato	9, 72	0	262.51	-0.04	0.00	0.00	-0.59	-0.08
			115	262.51	-0.04	0.00	0.00	-0.50	-0.08
			231	262.51	-0.04	0.00	0.00	-0.41	-0.08
523	Copertura	72, 10	0	-254.32	-0.06	0.00	0.00	0.36	0.18
			115	-254.32	-0.06	0.00	0.00	0.16	0.18
			231	-254.32	-0.06	0.00	0.00	-0.04	0.18
524	Copertura	73, 13	0	183.68	0.17	0.00	0.00	-1.41	-0.20
			118	183.68	0.17	0.00	0.00	-1.18	-0.20
			235	183.68	0.17	0.00	0.00	-0.94	-0.20
525	Primo Impalcato	14, 73	0	-233.36	-0.03	0.00	0.00	0.53	0.11
			118	-233.36	-0.03	0.00	0.00	0.40	0.11
			235	-233.36	-0.03	0.00	0.00	0.27	0.11
526	Primo Impalcato	57, 75	0	217.55	0.10	0.00	0.00	-0.13	-0.04
			118	217.55	0.10	0.00	0.00	-0.08	-0.04
			235	217.55	0.10	0.00	0.00	-0.03	-0.04
527	Copertura	75, 58	0	-169.77	-0.19	0.00	0.00	1.40	0.06
			118	-169.77	-0.19	0.00	0.00	1.33	0.06
			235	-169.77	-0.19	0.00	0.00	1.25	0.06
528	Copertura	77, 61	0	250.42	0.06	0.00	0.00	-0.36	-0.18
			115	250.42	0.06	0.00	0.00	-0.15	-0.18
			231	250.42	0.06	0.00	0.00	0.05	-0.18
529	Primo Impalcato	62, 77	0	-263.44	0.04	0.00	0.00	0.59	0.07
			115	-263.44	0.04	0.00	0.00	0.50	0.07
			231	-263.44	0.04	0.00	0.00	0.42	0.07
530	Primo Impalcato	65, 78	0	265.84	0.04	0.00	0.00	0.56	0.07
			115	265.84	0.04	0.00	0.00	0.48	0.07
			231	265.84	0.04	0.00	0.00	0.40	0.07
531	Copertura	78, 66	0	-254.89	0.06	0.00	0.00	-0.36	-0.17
			115	-254.89	0.06	0.00	0.00	-0.17	-0.17
			231	-254.89	0.06	0.00	0.00	0.03	-0.17
532	Primo Impalcato	69, 76	0	184.59	-0.17	0.00	0.00	-0.96	0.20
			118	184.59	-0.17	0.00	0.00	-1.19	0.20
			235	184.59	-0.17	0.00	0.00	-1.42	0.20
533	Copertura	76, 70	0	-233.60	0.03	0.00	0.00	0.29	-0.02
			118	-233.60	0.03	0.00	0.00	0.32	-0.02
			235	-233.60	0.03	0.00	0.00	0.35	-0.02
534	Copertura	1, 74	0	-168.80	0.18	0.00	0.00	-0.40	0.50
			118	-168.80	0.18	0.00	0.00	-0.98	0.50
			235	-168.80	0.18	0.00	0.00	-1.56	0.50
535	Copertura	74, 2	0	213.65	-0.04	0.00	0.00	0.20	0.34
			118	213.65	-0.04	0.00	0.00	-0.20	0.34
			235	213.65	-0.04	0.00	0.00	-0.60	0.34
536	Copertura	6, 71	0	-258.31	-0.05	0.00	0.00	0.27	-0.10
			115	-258.31	-0.05	0.00	0.00	0.39	-0.10
			231	-258.31	-0.05	0.00	0.00	0.50	-0.10
537	Copertura	71, 7	0	256.56	-0.07	0.00	0.00	-0.47	0.03
			115	256.56	-0.07	0.00	0.00	-0.50	0.03
			231	256.56	-0.07	0.00	0.00	-0.53	0.03
538	Copertura	9, 72	0	-254.32	-0.07	0.00	0.00	0.55	0.08
			115	-254.32	-0.07	0.00	0.00	0.46	0.08
			231	-254.32	-0.07	0.00	0.00	0.37	0.08
539	Copertura	72, 10	0	262.51	-0.02	0.00	0.00	-0.42	-0.17
			115	262.51	-0.02	0.00	0.00	-0.21	-0.17
			231	262.51	-0.02	0.00	0.00	-0.01	-0.17

540	Copertura	73, 13	0	-233.36	-0.03	0.00	0.00	0.25	0.42
			118	-233.36	-0.03	0.00	0.00	-0.25	0.42
			235	-233.36	-0.03	0.00	0.00	-0.75	0.42
541	Copertura	14, 73	0	183.68	0.18	0.00	0.00	-1.13	0.11
			118	183.68	0.18	0.00	0.00	-1.26	0.11
			235	183.68	0.18	0.00	0.00	-1.39	0.11
542	Copertura	15, 125	0	-55.55	-2.07	-41.56	1.29	-90.97	-11.71
			75	-55.55	-2.07	-40.60	1.29	-82.19	-11.71
			150	-55.55	-2.07	-39.63	1.29	-73.41	-11.71
543	Copertura	127, 16	0	32.30	-2.05	-94.64	84.88	73.48	-11.10
			75	32.30	-2.05	-30.98	84.88	81.81	-11.10
			150	32.30	-2.05	32.68	84.88	90.14	-11.10
544	Copertura	17, 129	0	-157.65	-2.04	-61.66	78.34	-82.01	-11.18
			75	-157.65	-2.04	-2.90	78.34	-73.63	-11.18
			150	-157.65	-2.04	55.85	78.34	-65.24	-11.18
545	Copertura	130, 18	0	141.12	-2.08	-217.38	175.31	65.28	-10.78
			75	141.12	-2.08	-85.89	175.31	73.37	-10.78
			150	141.12	-2.08	45.59	175.31	81.45	-10.78
546	Copertura	19, 135	0	-282.12	-1.62	-73.22	176.59	-64.69	-8.89
			75	-282.12	-1.62	59.22	176.59	-58.03	-8.89
			150	-282.12	-1.62	191.66	176.59	-51.36	-8.89
547	Copertura	134, 20	0	267.14	-1.34	-354.68	271.90	51.79	-7.58
			75	267.14	-1.34	-150.76	271.90	57.47	-7.58
			150	267.14	-1.34	53.17	271.90	63.16	-7.58
548	Copertura	21, 136	0	-376.43	-1.10	-79.84	250.65	-46.63	-6.38
			75	-376.43	-1.10	108.15	250.65	-41.85	-6.38
			150	-376.43	-1.10	296.14	250.65	-37.06	-6.38
549	Copertura	138, 22	0	358.64	-1.27	-455.11	342.26	36.93	-6.37
			75	358.64	-1.27	-198.41	342.26	41.71	-6.37
			150	358.64	-1.27	58.28	342.26	46.48	-6.37
550	Copertura	23, 141	0	-444.43	-0.66	-85.52	296.48	-31.05	-4.11
			75	-444.43	-0.66	136.84	296.48	-27.97	-4.11
			150	-444.43	-0.66	359.20	296.48	-24.88	-4.11
551	Copertura	142, 24	0	414.31	-0.60	-527.20	392.72	25.00	-3.50
			75	414.31	-0.60	-232.66	392.72	27.62	-3.50
			150	414.31	-0.60	61.87	392.72	30.24	-3.50
552	Copertura	25, 145	0	-432.89	-0.24	-89.60	303.64	-17.80	-2.21
			75	-432.89	-0.24	138.13	303.64	-16.14	-2.21
			150	-432.89	-0.24	365.86	303.64	-14.49	-2.21
553	Copertura	146, 26	0	468.28	-0.66	-564.84	419.99	14.38	-2.75
			75	468.28	-0.66	-249.85	419.99	16.44	-2.75
			150	468.28	-0.66	65.15	419.99	18.50	-2.75
554	Copertura	150, 27	0	409.46	-0.22	-586.61	436.50	5.46	-0.64
			75	409.46	-0.22	-259.24	436.50	5.95	-0.64
			150	409.46	-0.22	68.14	436.50	6.43	-0.64
555	Copertura	28, 149	0	-516.31	0.14	-88.42	306.67	-6.10	-0.77
			75	-516.31	0.14	141.58	306.67	-5.52	-0.77
			150	-516.31	0.14	371.58	306.67	-4.94	-0.77
556	Copertura	154, 29	0	483.34	-0.34	-594.11	438.80	-1.18	-0.27
			75	483.34	-0.34	-265.02	438.80	-0.97	-0.27
			150	483.34	-0.34	64.08	438.80	-0.77	-0.27
557	Copertura	30, 153	0	-475.38	0.39	-89.00	328.78	0.87	0.22
			75	-475.38	0.39	157.58	328.78	0.71	0.22
			150	-475.38	0.39	404.17	328.78	0.54	0.22
558	Copertura	158, 31	0	473.62	-0.17	-588.71	434.84	-4.54	0.53
			75	473.62	-0.17	-262.58	434.84	-4.93	0.53
			150	473.62	-0.17	63.55	434.84	-5.33	0.53
559	Copertura	32, 157	0	-486.15	0.55	-86.90	333.04	5.21	0.94
			75	-486.15	0.55	162.87	333.04	4.51	0.94
			150	-486.15	0.55	412.65	333.04	3.81	0.94
560	Copertura	162, 33	0	459.83	-0.24	-577.05	426.60	-6.68	0.58
			75	459.83	-0.24	-257.10	426.60	-7.11	0.58
			150	459.83	-0.24	62.85	426.60	-7.54	0.58
561	Copertura	34, 161	0	-478.31	0.66	-84.99	324.36	7.74	1.33
			75	-478.31	0.66	158.28	324.36	6.74	1.33
			150	-478.31	0.66	401.55	324.36	5.75	1.33
562	Copertura	166, 35	0	444.72	-0.18	-561.22	415.44	-7.87	0.86
			75	444.72	-0.18	-249.63	415.44	-8.51	0.86
			150	444.72	-0.18	61.95	415.44	-9.16	0.86
563	Copertura	36, 165	0	-462.56	0.71	-83.37	311.54	9.26	1.55
			75	-462.56	0.71	150.29	311.54	8.09	1.55
			150	-462.56	0.71	383.95	311.54	6.92	1.55

564	Copertura	170, 37	0	426.36	-0.18	-543.81	403.51	-8.55	0.97
			75	426.36	-0.18	-241.17	403.51	-9.27	0.97
			150	426.36	-0.18	61.46	403.51	-10.00	0.97
565	Copertura	38, 169	0	-450.27	0.71	-80.00	299.42	9.97	1.60
			75	-450.27	0.71	144.57	299.42	8.78	1.60
			150	-450.27	0.71	369.13	299.42	7.58	1.60
566	Copertura	175, 39	0	406.70	-0.20	-526.53	391.46	-8.26	0.92
			75	406.70	-0.20	-232.94	391.46	-8.95	0.92
			150	406.70	-0.20	60.65	391.46	-9.64	0.92
567	Copertura	40, 173	0	-460.10	0.63	-74.80	302.90	9.39	1.29
			75	-460.10	0.63	152.37	302.90	8.43	1.29
			150	-460.10	0.63	379.54	302.90	7.46	1.29
568	Copertura	178, 41	0	547.24	-0.15	-524.01	385.80	-5.89	0.78
			75	547.24	-0.15	-234.67	385.80	-6.48	0.78
			150	547.24	-0.15	54.68	385.80	-7.06	0.78
569	Copertura	42, 177	0	-370.33	0.69	-72.94	344.74	7.97	1.24
			75	-370.33	0.69	185.62	344.74	7.04	1.24
			150	-370.33	0.69	444.18	344.74	6.12	1.24
570	Copertura	43, 181	0	-552.85	0.37	-72.77	343.59	7.60	1.15
			75	-552.85	0.37	184.93	343.59	6.74	1.15
			150	-552.85	0.37	442.62	343.59	5.88	1.15
571	Copertura	182, 44	0	366.68	-0.09	-521.46	388.73	-5.25	0.70
			75	366.68	-0.09	-229.92	388.73	-5.78	0.70
			150	366.68	-0.09	61.63	388.73	-6.30	0.70
572	Copertura	45, 185	0	-398.87	0.52	-76.46	291.81	11.46	1.89
			75	-398.87	0.52	142.40	291.81	10.05	1.89
			150	-398.87	0.52	361.26	291.81	8.63	1.89
573	Copertura	186, 46	0	427.63	0.05	-495.39	370.99	-9.19	1.03
			75	427.63	0.05	-217.15	370.99	-9.96	1.03
			150	427.63	0.05	61.10	370.99	-10.74	1.03
574	Copertura	47, 189	0	-380.96	0.70	-77.69	256.38	21.64	3.06
			75	-380.96	0.70	114.59	256.38	19.34	3.06
			150	-380.96	0.70	306.88	256.38	17.04	3.06
575	Copertura	190, 48	0	370.95	0.49	-464.36	349.39	-17.25	2.96
			75	370.95	0.49	-202.32	349.39	-19.47	2.96
			150	370.95	0.49	59.73	349.39	-21.69	2.96
576	Copertura	49, 193	0	-337.74	1.14	-76.56	218.77	37.78	5.23
			75	-337.74	1.14	87.52	218.77	33.85	5.23
			150	-337.74	1.14	251.60	218.77	29.93	5.23
577	Copertura	195, 50	0	319.45	0.58	-413.90	313.56	-30.49	4.12
			75	319.45	0.58	-178.73	313.56	-33.58	4.12
			150	319.45	0.58	56.44	313.56	-36.67	4.12
578	Copertura	51, 197	0	-257.25	1.66	-72.28	157.23	57.55	7.98
			75	-257.25	1.66	45.64	157.23	51.56	7.98
			150	-257.25	1.66	163.56	157.23	45.58	7.98
579	Copertura	199, 52	0	240.58	1.44	-325.52	251.57	-45.75	7.80
			75	240.58	1.44	-136.85	251.57	-51.60	7.80
			150	240.58	1.44	51.83	251.57	-57.45	7.80
580	Copertura	53, 201	0	-146.25	2.18	-61.03	68.80	77.07	10.57
			75	-146.25	2.18	-9.43	68.80	69.14	10.57
			150	-146.25	2.18	42.17	68.80	61.20	10.57
581	Copertura	202, 54	0	129.65	1.56	-205.77	166.88	-61.87	9.17
			75	129.65	1.56	-80.61	166.88	-68.75	9.17
			150	129.65	1.56	44.55	166.88	-75.63	9.17
582	Copertura	55, 205	0	-44.96	2.24	-41.65	-3.66	87.63	11.34
			75	-44.96	2.24	-44.39	-3.66	79.12	11.34
			150	-44.96	2.24	-47.13	-3.66	70.62	11.34
583	Copertura	206, 56	0	28.28	1.99	-85.05	78.91	-70.77	11.04
			75	28.28	1.99	-25.86	78.91	-79.05	11.04
			150	28.28	1.99	33.32	78.91	-87.33	11.04
584	Copertura	57, 75	0	-169.77	-0.17	0.00	0.00	0.97	-0.15
			118	-169.77	-0.17	0.00	0.00	1.15	-0.15
			235	-169.77	-0.17	0.00	0.00	1.33	-0.15
585	Copertura	75, 58	0	217.55	0.04	0.00	0.00	0.01	-0.25
			118	217.55	0.04	0.00	0.00	0.31	-0.25
			235	217.55	0.04	0.00	0.00	0.61	-0.25
586	Copertura	77, 61	0	-263.44	0.02	0.00	0.00	0.42	0.18
			115	-263.44	0.02	0.00	0.00	0.21	0.18
			231	-263.44	0.02	0.00	0.00	0.01	0.18
587	Copertura	62, 77	0	250.42	0.07	0.00	0.00	-0.54	-0.07
			115	250.42	0.07	0.00	0.00	-0.45	-0.07
			231	250.42	0.07	0.00	0.00	-0.37	-0.07

588	Copertura	65, 78	0	-254.89	0.07	0.00	0.00	-0.54	-0.07
			115	-254.89	0.07	0.00	0.00	-0.46	-0.07
			231	-254.89	0.07	0.00	0.00	-0.37	-0.07
589	Copertura	78, 66	0	265.84	0.02	0.00	0.00	0.40	0.17
			115	265.84	0.02	0.00	0.00	0.21	0.17
			231	265.84	0.02	0.00	0.00	0.01	0.17
590	Copertura	69, 76	0	-233.60	0.03	0.00	0.00	-0.73	-0.43
			118	-233.60	0.03	0.00	0.00	-0.23	-0.43
			235	-233.60	0.03	0.00	0.00	0.27	-0.43
591	Copertura	76, 70	0	184.59	-0.18	0.00	0.00	-1.40	-0.21
			118	184.59	-0.18	0.00	0.00	-1.16	-0.21
			235	184.59	-0.18	0.00	0.00	-0.91	-0.21
592	Copertura	79, 81	0	1.32	-0.22	2.04	-2.48	8.05	7.46
			80	1.32	-0.22	0.07	-2.48	2.12	7.46
			159	1.32	-0.22	-1.90	-2.48	-3.81	7.46
593	Copertura	80, 82	0	2.73	-0.65	1.22	-1.71	-0.74	1.88
			66	2.73	-0.65	0.09	-1.71	-1.98	1.88
			132	2.73	-0.65	-1.04	-1.71	-3.23	1.88
594	Copertura	83, 84	0	-0.15	-0.44	0.54	-0.78	-1.27	0.79
			66	-0.15	-0.44	0.03	-0.78	-1.79	0.79
			132	-0.15	-0.44	-0.48	-0.78	-2.31	0.79
595	Copertura	85, 86	0	-2.99	-0.19	0.10	0.07	-1.23	0.05
			66	-2.99	-0.19	0.15	0.07	-1.27	0.05
			132	-2.99	-0.19	0.20	0.07	-1.30	0.05
596	Copertura	87, 88	0	-5.03	-0.02	-1.06	1.95	-0.88	-0.08
			66	-5.03	-0.02	0.23	1.95	-0.82	-0.08
			132	-5.03	-0.02	1.52	1.95	-0.76	-0.08
597	Copertura	89, 90	0	-1.46	0.05	-2.20	3.44	-0.46	-0.22
			66	-1.46	0.05	0.07	3.44	-0.32	-0.22
			132	-1.46	0.05	2.34	3.44	-0.18	-0.22
598	Copertura	91, 92	0	-0.35	0.07	-2.48	3.81	-0.20	-0.26
			66	-0.35	0.07	0.03	3.81	-0.03	-0.26
			132	-0.35	0.07	2.54	3.81	0.14	-0.26
599	Copertura	93, 94	0	5.11	0.05	-1.81	2.41	0.27	0.08
			66	5.11	0.05	-0.22	2.41	0.22	0.08
			132	5.11	0.05	1.37	2.41	0.17	0.08
600	Copertura	95, 96	0	5.96	0.08	-0.37	0.20	-0.60	-0.07
			66	5.96	0.08	-0.24	0.20	-0.56	-0.07
			132	5.96	0.08	-0.11	0.20	-0.51	-0.07
601	Copertura	97, 106	0	0.40	0.22	1.06	-1.57	-1.60	-0.12
			66	0.40	0.22	0.02	-1.57	-1.52	-0.12
			132	0.40	0.22	-1.02	-1.57	-1.44	-0.12
602	Copertura	98, 99	0	0.40	-0.37	1.03	-1.41	0.36	3.52
			66	0.40	-0.37	0.09	-1.41	-1.96	3.52
			132	0.40	-0.37	-0.84	-1.41	-4.28	3.52
603	Copertura	100, 101	0	-0.55	-0.20	0.74	-1.14	-0.59	1.66
			66	-0.55	-0.20	-0.02	-1.14	-1.68	1.66
			132	-0.55	-0.20	-0.77	-1.14	-2.78	1.66
604	Copertura	102, 103	0	-5.20	-0.07	0.74	-0.92	-0.82	0.43
			66	-5.20	-0.07	0.13	-0.92	-1.11	0.43
			132	-5.20	-0.07	-0.48	-0.92	-1.39	0.43
605	Copertura	104, 105	0	-1.31	0.02	0.23	-0.44	-0.71	-0.29
			66	-1.31	0.02	-0.06	-0.44	-0.52	-0.29
			132	-1.31	0.02	-0.35	-0.44	-0.33	-0.29
606	Copertura	107, 108	0	0.76	0.52	1.04	-1.53	-2.75	-1.09
			66	0.76	0.52	0.03	-1.53	-2.03	-1.09
			132	0.76	0.52	-0.98	-1.53	-1.31	-1.09
607	Copertura	109, 110	0	1.92	0.58	-0.42	0.52	-3.27	-7.05
			80	1.92	0.58	0.00	0.52	2.34	-7.05
			159	1.92	0.58	0.41	0.52	7.94	-7.05
608	Copertura	111, 112	0	-0.57	0.09	0.36	-0.65	-0.55	-0.56
			66	-0.57	0.09	-0.07	-0.65	-0.18	-0.56
			132	-0.57	0.09	-0.50	-0.65	0.19	-0.56
609	Copertura	113, 114	0	0.32	0.06	0.58	-0.79	-0.20	-0.48
			66	0.32	0.06	0.06	-0.79	0.12	-0.48
			132	0.32	0.06	-0.46	-0.79	0.44	-0.48
610	Copertura	115, 116	0	10.00	0.02	0.91	-1.83	0.09	0.19
			66	10.00	0.02	-0.30	-1.83	-0.03	0.19
			132	10.00	0.02	-1.51	-1.83	-0.15	0.19
611	Copertura	117, 118	0	0.64	0.07	2.09	-3.05	-1.50	-0.60
			66	0.64	0.07	0.08	-3.05	-1.10	-0.60
			132	0.64	0.07	-1.93	-3.05	-0.70	-0.60

612	Copertura	119, 120	0	-0.05	0.24	1.89	-2.77	-3.50	-2.13
			66	-0.05	0.24	0.06	-2.77	-2.09	-2.13
			132	-0.05	0.24	-1.77	-2.77	-0.68	-2.13
613	Copertura	121, 122	0	1.20	0.36	1.13	-1.48	-4.48	-4.21
			66	1.20	0.36	0.15	-1.48	-1.70	-4.21
			132	1.20	0.36	-0.83	-1.48	1.07	-4.21
614	Copertura	124, 125	0	-0.35	-0.59	7.72	-6.08	-0.98	1.75
			99	-0.35	-0.59	1.69	-6.08	-2.71	1.75
			198	-0.35	-0.59	-4.35	-6.08	-4.45	1.75
615	Copertura	125, 127	0	-59.80	0.40	-43.98	-3.07	-77.16	-9.96
			775	-59.80	0.40	-67.80	-3.07	0.02	-9.96
			1550	-59.80	0.40	-91.62	-3.07	77.19	-9.96
616	Copertura	126, 127	0	-127.21	-0.58	-9.18	6.15	-2.13	1.15
			99	-127.21	-0.58	-3.08	6.15	-3.27	1.15
			198	-127.21	-0.58	3.02	6.15	-4.40	1.15
617	Copertura	128, 129	0	133.19	-0.50	14.83	-10.61	0.24	2.29
			99	133.19	-0.50	4.30	-10.61	-2.03	2.29
			198	133.19	-0.50	-6.23	-10.61	-4.31	2.29
618	Copertura	129, 130	0	-63.95	0.40	49.62	-16.91	-68.83	-8.88
			775	-63.95	0.40	-81.46	-16.91	0.03	-8.88
			1550	-63.95	0.40	-212.54	-16.91	68.88	-8.88
619	Copertura	131, 130	0	-280.86	-0.48	-16.91	10.96	-0.59	1.89
			99	-280.86	-0.48	-6.04	10.96	-2.47	1.89
			198	-280.86	-0.48	4.84	10.96	-4.35	1.89
620	Copertura	132, 135	0	304.18	-0.40	22.83	-15.48	0.36	1.89
			99	304.18	-0.40	7.46	-15.48	-1.51	1.89
			198	304.18	-0.40	-7.90	-15.48	-3.39	1.89
621	Copertura	133, 134	0	-449.58	-0.42	-24.63	15.60	-1.82	0.58
			99	-449.58	-0.42	-9.15	15.60	-2.40	0.58
			198	-449.58	-0.42	6.33	15.60	-2.98	0.58
622	Copertura	135, 134	0	-62.39	0.30	183.76	-34.33	-54.18	-7.00
			775	-62.39	0.30	-82.30	-34.33	0.06	-7.00
			1550	-62.39	0.30	-348.35	-34.33	54.31	-7.00
623	Copertura	137, 136	0	433.05	-0.30	28.82	-19.09	0.27	1.34
			99	433.05	-0.30	9.87	-19.09	-1.06	1.34
			198	433.05	-0.30	-9.08	-19.09	-2.39	1.34
624	Copertura	136, 138	0	-61.69	0.24	287.05	-47.40	-39.06	-5.04
			775	-61.69	0.24	-80.26	-47.40	0.00	-5.04
			1550	-61.69	0.24	-447.58	-47.40	39.07	-5.04
625	Copertura	139, 138	0	-572.84	-0.26	-30.52	19.17	0.03	1.33
			99	-572.84	-0.26	-11.50	19.17	-1.29	1.33
			198	-572.84	-0.26	7.53	19.17	-2.60	1.33
626	Copertura	140, 141	0	513.39	-0.22	32.74	-21.52	0.01	0.74
			99	513.39	-0.22	11.38	-21.52	-0.73	0.74
			198	513.39	-0.22	-9.98	-21.52	-1.46	0.74
627	Copertura	141, 142	0	-70.56	0.14	349.23	-56.01	-26.13	-3.37
			775	-70.56	0.14	-84.84	-56.01	0.02	-3.37
			1550	-70.56	0.14	-518.91	-56.01	26.16	-3.37
628	Copertura	143, 142	0	-660.30	-0.21	-34.46	21.54	-1.12	0.12
			99	-660.30	-0.21	-13.09	21.54	-1.24	0.12
			198	-660.30	-0.21	8.29	21.54	-1.36	0.12
629	Copertura	144, 145	0	527.33	-0.15	34.23	-22.59	-0.21	0.24
			99	527.33	-0.15	11.81	-22.59	-0.45	0.24
			198	527.33	-0.15	-10.61	-22.59	-0.69	0.24
630	Copertura	145, 146	0	-49.19	0.10	355.25	-58.79	-15.10	-1.97
			775	-49.19	0.10	-100.40	-58.79	0.14	-1.97
			1550	-49.19	0.10	-556.05	-58.79	15.39	-1.97
631	Copertura	147, 146	0	-704.61	-0.08	-36.68	22.91	0.29	0.78
			99	-704.61	-0.08	-13.95	22.91	-0.48	0.78
			198	-704.61	-0.08	8.78	22.91	-1.26	0.78
632	Copertura	148, 149	0	533.79	-0.08	35.20	-23.28	0.22	0.08
			99	533.79	-0.08	12.10	-23.28	0.14	0.08
			198	533.79	-0.08	-11.00	-23.28	0.06	0.08
633	Copertura	149, 150	0	-128.17	0.03	360.58	-60.52	-4.95	-0.69
			775	-128.17	0.03	-108.56	-60.52	0.43	-0.69
			1550	-128.17	0.03	-577.69	-60.52	5.81	-0.69
634	Copertura	151, 150	0	-731.80	-0.04	-37.68	23.48	-0.53	-0.05
			99	-731.80	-0.04	-14.38	23.48	-0.48	-0.05
			198	-731.80	-0.04	8.92	23.48	-0.43	-0.05
635	Copertura	152, 153	0	571.07	-0.05	36.05	-23.63	0.29	-0.11
			99	571.07	-0.05	12.59	-23.63	0.40	-0.11
			198	571.07	-0.05	-10.86	-23.63	0.51	-0.11

636	Copertura	153, 154	0	-59.30	0.02	393.31	-63.09	0.90	0.11
			775	-59.30	0.02	-95.86	-63.09	0.03	0.11
			1551	-59.30	0.02	-585.02	-63.09	-0.83	0.11
637	Copertura	155, 154	0	-738.77	0.04	-38.30	23.88	0.26	0.38
			99	-738.77	0.04	-14.61	23.88	-0.12	0.38
			198	-738.77	0.04	9.09	23.88	-0.50	0.38
638	Copertura	156, 157	0	577.92	-0.03	36.09	-23.60	0.11	-0.36
			99	577.92	-0.03	12.67	-23.60	0.47	-0.36
			198	577.92	-0.03	-10.75	-23.60	0.83	-0.36
639	Copertura	157, 158	0	-64.88	-0.02	401.90	-63.29	4.42	0.57
			775	-64.88	-0.02	-88.87	-63.29	-0.02	0.57
			1551	-64.88	-0.02	-579.65	-63.29	-4.46	0.57
640	Copertura	159, 158	0	-733.18	0.06	-38.07	23.75	-0.07	0.05
			99	-733.18	0.06	-14.50	23.75	-0.11	0.05
			198	-733.18	0.06	9.06	23.75	-0.16	0.05
641	Copertura	160, 161	0	562.92	-0.02	35.39	-23.18	0.04	-0.49
			99	562.92	-0.02	12.39	-23.18	0.52	-0.49
			198	562.92	-0.02	-10.61	-23.18	1.01	-0.49
642	Copertura	161, 162	0	-68.10	-0.02	390.94	-61.83	6.50	0.84
			776	-68.10	-0.02	-88.59	-61.83	-0.04	0.84
			1551	-68.10	-0.02	-568.11	-61.83	-6.57	0.84
643	Copertura	163, 162	0	-718.84	0.09	-37.39	23.34	0.30	0.26
			99	-718.84	0.09	-14.23	23.34	0.04	0.26
			198	-718.84	0.09	8.94	23.34	-0.22	0.26
644	Copertura	164, 165	0	540.77	-0.01	34.40	-22.58	0.03	-0.55
			99	540.77	-0.01	11.99	-22.58	0.57	-0.55
			198	540.77	-0.01	-10.42	-22.58	1.12	-0.55
645	Copertura	165, 166	0	-68.69	-0.03	373.52	-59.69	7.76	1.01
			776	-68.69	-0.03	-89.47	-59.69	-0.04	1.01
			1551	-68.69	-0.03	-552.45	-59.69	-7.85	1.01
646	Copertura	167, 166	0	-699.15	0.10	-36.51	22.81	0.17	0.15
			99	-699.15	0.10	-13.88	22.81	0.03	0.15
			198	-699.15	0.10	8.76	22.81	-0.11	0.15
647	Copertura	168, 169	0	519.87	0.00	33.37	-21.94	0.14	-0.50
			99	519.87	0.00	11.60	-21.94	0.64	-0.50
			198	519.87	0.00	-10.18	-21.94	1.14	-0.50
648	Copertura	169, 170	0	-71.78	-0.03	358.96	-57.63	8.44	1.09
			776	-71.78	-0.03	-88.13	-57.63	-0.05	1.09
			1552	-71.78	-0.03	-535.22	-57.63	-8.54	1.09
649	Copertura	171, 170	0	-678.46	0.11	-35.55	22.23	0.15	0.12
			99	-678.46	0.11	-13.48	22.23	0.03	0.12
			198	-678.46	0.11	8.59	22.23	-0.10	0.12
650	Copertura	172, 173	0	524.80	0.00	33.16	-21.70	0.56	-0.23
			99	524.80	0.00	11.62	-21.70	0.79	-0.23
			198	524.80	0.00	-9.91	-21.70	1.02	-0.23
651	Copertura	173, 175	0	-77.73	-0.03	369.63	-57.21	8.23	1.06
			776	-77.73	-0.03	-74.22	-57.21	0.00	1.06
			1552	-77.73	-0.03	-518.07	-57.21	-8.23	1.06
652	Copertura	174, 175	0	-659.92	0.10	-34.77	21.78	0.15	0.15
			99	-659.92	0.10	-13.16	21.78	0.01	0.15
			198	-659.92	0.10	8.46	21.78	-0.14	0.15
653	Copertura	176, 177	0	594.90	-0.01	33.82	-21.65	0.31	-0.41
			99	594.90	-0.01	12.32	-21.65	0.71	-0.41
			198	594.90	-0.01	-9.17	-21.65	1.12	-0.41
654	Copertura	177, 178	0	65.04	-0.05	435.01	-61.24	6.95	0.83
			776	65.04	-0.05	-40.18	-61.24	0.53	0.83
			1552	65.04	-0.05	-515.38	-61.24	-5.89	0.83
655	Copertura	179, 178	0	-657.16	0.07	-35.06	22.01	0.03	0.05
			99	-657.16	0.07	-13.21	22.01	-0.01	0.05
			198	-657.16	0.07	8.63	22.01	-0.06	0.05
656	Copertura	180, 181	0	592.64	0.01	34.06	-21.85	-0.14	-0.39
			99	592.64	0.01	12.37	-21.85	0.25	-0.39
			198	592.64	0.01	-9.32	-21.85	0.64	-0.39
657	Copertura	181, 182	0	-119.31	-0.04	433.30	-61.06	6.37	0.75
			775	-119.31	-0.04	-39.89	-61.06	0.54	0.75
			1550	-119.31	-0.04	-513.09	-61.06	-5.29	0.75
658	Copertura	183, 182	0	-661.84	0.07	-34.51	21.60	0.10	0.05
			99	-661.84	0.07	-13.07	21.60	0.05	0.05
			198	-661.84	0.07	8.37	21.60	0.00	0.05
659	Copertura	184, 185	0	504.41	0.02	31.56	-20.64	-0.42	-0.67
			99	504.41	0.02	11.08	-20.64	0.25	-0.67
			198	504.41	0.02	-9.40	-20.64	0.92	-0.67

660	Copertura	185, 186	0	-31.21	-0.07	351.86	-54.14	9.34	1.21
			775	-31.21	-0.07	-67.71	-54.14	-0.07	1.21
			1550	-31.21	-0.07	-487.27	-54.14	-9.47	1.21
661	Copertura	187, 186	0	-625.17	0.10	-33.08	20.76	0.65	0.18
			99	-625.17	0.10	-12.48	20.76	0.47	0.18
			198	-625.17	0.10	8.12	20.76	0.29	0.18
662	Copertura	188, 189	0	443.45	0.09	29.25	-19.34	-0.05	-0.72
			99	443.45	0.09	10.05	-19.34	0.66	-0.72
			198	443.45	0.09	-9.15	-19.34	1.37	-0.72
663	Copertura	189, 190	0	-58.52	-0.13	297.73	-48.67	18.14	2.34
			775	-58.52	-0.13	-79.48	-48.67	-0.02	2.34
			1550	-58.52	-0.13	-456.69	-48.67	-18.18	2.34
664	Copertura	191, 190	0	-585.25	0.13	-31.12	19.54	-0.12	-0.62
			99	-585.25	0.13	-11.73	19.54	0.50	-0.62
			198	-585.25	0.13	7.67	19.54	1.11	-0.62
665	Copertura	192, 193	0	377.79	0.19	26.27	-17.56	-0.02	-1.13
			99	377.79	0.19	8.84	-17.56	1.10	-1.13
			198	377.79	0.19	-8.59	-17.56	2.23	-1.13
666	Copertura	193, 195	0	-63.74	-0.18	243.01	-41.93	31.73	4.10
			775	-63.74	-0.18	-81.94	-41.93	-0.03	4.10
			1550	-63.74	-0.18	-406.89	-41.93	-31.79	4.10
667	Copertura	194, 195	0	-522.39	0.27	-28.07	17.67	1.44	-0.02
			99	-522.39	0.27	-10.53	17.67	1.46	-0.02
			198	-522.39	0.27	7.01	17.67	1.48	-0.02
668	Copertura	196, 197	0	270.12	0.30	21.26	-14.54	-0.12	-1.75
			99	270.12	0.30	6.83	-14.54	1.62	-1.75
			198	270.12	0.30	-7.60	-14.54	3.35	-1.75
669	Copertura	197, 199	0	-62.64	-0.31	155.96	-30.67	48.30	6.23
			775	-62.64	-0.31	-81.75	-30.67	0.01	6.23
			1550	-62.64	-0.31	-319.47	-30.67	-48.29	6.23
670	Copertura	198, 199	0	-413.99	0.34	-23.11	14.70	-0.05	-1.57
			99	-413.99	0.34	-8.53	14.70	1.51	-1.57
			198	-413.99	0.34	6.06	14.70	3.07	-1.57
671	Copertura	200, 201	0	116.71	0.41	14.05	-10.15	-0.02	-2.21
			99	116.71	0.41	3.98	-10.15	2.18	-2.21
			198	116.71	0.41	-6.09	-10.15	4.37	-2.21
672	Copertura	201, 202	0	-64.70	-0.37	36.08	-15.31	64.78	8.36
			775	-64.70	-0.37	-82.55	-15.31	-0.04	8.36
			1550	-64.70	-0.37	-201.17	-15.31	-64.87	8.36
673	Copertura	203, 202	0	-266.19	0.51	-16.03	10.39	1.92	-0.81
			99	-266.19	0.51	-5.71	10.39	2.72	-0.81
			198	-266.19	0.51	4.60	10.39	3.52	-0.81
674	Copertura	204, 205	0	-9.30	0.51	7.31	-5.83	1.18	-1.74
			99	-9.30	0.51	1.52	-5.83	2.91	-1.74
			198	-9.30	0.51	-4.26	-5.83	4.63	-1.74
675	Copertura	205, 206	0	-55.80	-0.41	-51.39	-1.97	74.45	9.60
			775	-55.80	-0.41	-66.69	-1.97	0.03	9.60
			1550	-55.80	-0.41	-81.98	-1.97	-74.39	9.60
676	Copertura	207, 206	0	-116.52	0.56	-8.94	6.05	1.44	-1.44
			99	-116.52	0.56	-2.94	6.05	2.87	-1.44
			198	-116.52	0.56	3.07	6.05	4.30	-1.44
677	Copertura	79	0	227.73	8.11	-2.07	2.94	-59.63	-23.41
			125	227.73	8.11	1.61	2.94	-14.64	-48.57
			250	227.73	8.11	5.28	2.94	61.81	-73.74
678	Copertura	124	0	9.74	1.23	-0.59	0.94	-132.22	127.72
			155	9.74	1.23	0.88	0.94	-239.62	10.86
			310	9.74	1.23	2.34	0.94	-165.89	-105.99
679	Copertura	80	0	-20.24	2.94	-0.25	4.05	-131.49	-47.07
			45	-20.24	2.94	1.57	4.05	-106.49	-64.03
			90	-20.24	2.94	3.40	4.05	-73.86	-80.99
680	Copertura	128	0	31.16	2.54	-0.86	1.32	-234.38	111.23
			155	31.16	2.54	1.18	1.32	-322.40	2.35
			310	31.16	2.54	3.22	1.32	-241.68	-106.52
681	Copertura	82	0	-47.89	5.16	0.71	-1.05	-179.99	-73.06
			43	-47.89	5.16	0.26	-1.05	-145.63	-88.04
			85	-47.89	5.16	-0.19	-1.05	-104.88	-103.01
682	Copertura	132	0	39.98	2.20	-1.05	1.43	-348.03	71.78
			155	39.98	2.20	1.17	1.43	-374.91	-37.09
			310	39.98	2.20	3.38	1.43	-233.04	-145.96
683	Copertura	83	0	-48.45	2.48	0.12	0.72	-207.25	-110.26
			43	-48.45	2.48	0.42	0.72	-157.02	-125.23
			85	-48.45	2.48	0.73	0.72	-100.41	-140.21

684	Copertura	137	0	35.26	1.55	-1.18	1.49	-433.44	41.77
			155	35.26	1.55	1.12	1.49	-413.81	-67.10
			310	35.26	1.55	3.43	1.49	-225.42	-175.97
685	Copertura	84	0	-39.57	3.10	0.02	0.70	-228.08	-138.78
			43	-39.57	3.10	0.32	0.70	-165.69	-153.76
			85	-39.57	3.10	0.61	0.70	-96.91	-168.74
686	Copertura	140	0	51.17	0.78	-1.27	1.49	-489.23	26.00
			155	51.17	0.78	1.04	1.49	-445.16	-82.87
			310	51.17	0.78	3.34	1.49	-232.34	-191.74
687	Copertura	85	0	-51.27	0.98	1.06	-1.76	-241.55	-157.71
			43	-51.27	0.98	0.31	-1.76	-171.08	-172.69
			85	-51.27	0.98	-0.44	-1.76	-94.23	-187.67
688	Copertura	144	0	63.58	0.12	-1.34	1.52	-514.65	39.82
			155	63.58	0.12	1.02	1.52	-482.49	-81.32
			310	63.58	0.12	3.38	1.52	-262.56	-202.47
689	Copertura	86	0	-54.89	1.39	-0.82	1.16	-251.06	-167.97
			43	-54.89	1.39	-0.32	1.16	-176.21	-182.95
			85	-54.89	1.39	0.17	1.16	-94.98	-197.93
690	Copertura	87	0	-60.52	0.00	1.64	-4.70	-253.60	-173.89
			43	-60.52	0.00	-0.37	-4.70	-176.23	-188.86
			85	-60.52	0.00	-2.37	-4.70	-92.47	-203.84
691	Copertura	148	0	69.01	0.35	1.90	-0.22	-527.51	44.76
			155	69.01	0.35	1.57	-0.22	-499.31	-81.14
			310	69.01	0.35	1.23	-0.22	-275.98	-207.04
692	Copertura	88	0	-52.89	0.31	-1.49	0.62	-257.07	-175.53
			43	-52.89	0.31	-1.22	0.62	-179.00	-190.51
			85	-52.89	0.31	-0.96	0.62	-94.54	-205.49
693	Copertura	152	0	59.58	0.26	3.42	-1.05	-539.27	23.57
			155	59.58	0.26	1.79	-1.05	-486.40	-91.79
			310	59.58	0.26	0.16	-1.05	-254.73	-207.14
694	Copertura	89	0	-60.23	-0.42	0.61	-4.52	-257.41	-173.86
			43	-60.23	-0.42	-1.32	-4.52	-180.05	-188.84
			85	-60.23	-0.42	-3.24	-4.52	-96.31	-203.82
695	Copertura	156	0	58.52	-0.09	3.97	-1.40	-538.80	16.68
			155	58.52	-0.09	1.81	-1.40	-477.33	-95.99
			310	58.52	-0.09	-0.35	-1.40	-241.22	-208.67
696	Copertura	90	0	-57.63	-0.25	-0.29	-2.98	-254.92	-170.78
			43	-57.63	-0.25	-1.56	-2.98	-178.88	-185.76
			85	-57.63	-0.25	-2.83	-2.98	-96.45	-200.74
697	Copertura	160	0	61.44	-0.25	4.42	-1.66	-528.92	20.09
			155	61.44	-0.25	1.84	-1.66	-472.48	-92.92
			310	61.44	-0.25	-0.73	-1.66	-240.87	-205.94
698	Copertura	91	0	-62.81	-0.49	0.28	-4.34	-251.07	-166.70
			43	-62.81	-0.49	-1.56	-4.34	-176.77	-181.68
			85	-62.81	-0.49	-3.41	-4.34	-96.08	-196.66
699	Copertura	164	0	65.41	-0.31	4.75	-1.86	-514.81	25.76
			155	65.41	-0.31	1.87	-1.86	-467.15	-87.26
			310	65.41	-0.31	-1.01	-1.86	-244.31	-200.27
700	Copertura	92	0	-58.58	-0.49	0.06	-4.01	-247.77	-162.11
			43	-58.58	-0.49	-1.65	-4.01	-175.43	-177.09
			85	-58.58	-0.49	-3.36	-4.01	-96.69	-192.07
701	Copertura	168	0	65.50	-0.18	5.04	-2.01	-500.20	29.78
			155	65.50	-0.18	1.91	-2.01	-459.04	-82.89
			310	65.50	-0.18	-1.21	-2.01	-243.24	-195.56
702	Copertura	93	0	-59.37	-0.31	-1.51	-0.03	-247.46	-157.50
			43	-59.37	-0.31	-1.52	-0.03	-177.08	-172.48
			85	-59.37	-0.31	-1.53	-0.03	-100.31	-187.46
703	Copertura	172	0	56.58	0.39	5.53	-2.27	-495.98	20.45
			155	56.58	0.39	2.00	-2.27	-440.35	-92.23
			310	56.58	0.39	-1.53	-2.27	-210.08	-204.90
704	Copertura	94	0	-57.64	-0.28	1.71	-5.18	-248.53	-156.54
			43	-57.64	-0.28	-0.50	-5.18	-178.56	-171.52
			85	-57.64	-0.28	-2.71	-5.18	-102.20	-186.50
705	Copertura	176	0	50.08	0.14	7.09	-3.19	-501.98	-33.47
			155	50.08	0.14	2.15	-3.19	-392.86	-107.33
			310	50.08	0.14	-2.80	-3.19	-169.25	-181.19
706	Copertura	180	0	50.40	-0.50	-1.27	1.34	-499.25	-34.09
			155	50.40	-0.50	0.81	1.34	-390.77	-105.88
			310	50.40	-0.50	2.89	1.34	-171.03	-177.67
707	Copertura	95	0	-65.57	-0.49	-1.60	2.37	-246.47	-156.82
			43	-65.57	-0.49	-0.59	2.37	-176.38	-171.80
			85	-65.57	-0.49	0.42	2.37	-99.90	-186.78

708	Copertura	184	0	46.74	-0.96	-1.22	1.27	-473.34	19.26
			155	46.74	-0.96	0.75	1.27	-418.81	-89.62
			310	46.74	-0.96	2.72	1.27	-195.53	-198.49
709	Copertura	96	0	-46.32	-0.41	2.10	-3.89	-239.35	-149.55
			43	-46.32	-0.41	0.44	-3.89	-172.36	-164.53
			85	-46.32	-0.41	-1.22	-3.89	-98.99	-179.50
710	Copertura	188	0	47.87	-0.78	-1.31	1.32	-440.13	40.06
			155	47.87	-0.78	0.73	1.32	-417.84	-68.82
			310	47.87	-0.78	2.78	1.32	-226.80	-177.69
711	Copertura	97	0	-42.66	-1.64	0.04	1.46	-231.03	-141.47
			43	-42.66	-1.64	0.66	1.46	-167.49	-156.45
			85	-42.66	-1.64	1.29	1.46	-97.56	-171.43
712	Copertura	192	0	40.00	-1.20	-1.43	1.37	-397.16	55.14
			155	40.00	-1.20	0.69	1.37	-398.25	-53.73
			310	40.00	-1.20	2.81	1.37	-230.59	-162.61
713	Copertura	106	0	-35.48	-1.21	0.30	0.82	-219.15	-126.73
			43	-35.48	-1.21	0.65	0.82	-161.89	-141.71
			85	-35.48	-1.21	1.00	0.82	-98.25	-156.69
714	Copertura	196	0	43.23	-1.89	-1.61	1.46	-325.48	79.69
			155	43.23	-1.89	0.66	1.46	-364.62	-29.18
			310	43.23	-1.89	2.93	1.46	-235.01	-138.05
715	Copertura	107	0	-40.02	-3.75	-0.02	1.80	-201.71	-103.19
			43	-40.02	-3.75	0.75	1.80	-154.50	-118.17
			85	-40.02	-3.75	1.52	1.80	-100.90	-133.15
716	Copertura	200	0	36.73	-2.33	-1.82	1.60	-223.16	114.85
			155	36.73	-2.33	0.65	1.60	-316.80	5.97
			310	36.73	-2.33	3.13	1.60	-241.68	-102.90
717	Copertura	108	0	-49.70	-2.82	0.35	0.41	-176.94	-69.04
			43	-49.70	-2.82	0.53	0.41	-144.30	-84.02
			85	-49.70	-2.82	0.70	0.41	-105.26	-99.00
718	Copertura	204	0	5.35	-1.09	-2.12	2.02	-126.47	129.85
			155	5.35	-1.09	1.01	2.02	-237.18	13.00
			310	5.35	-1.09	4.15	2.02	-166.77	-103.85
719	Copertura	109	0	-23.68	-4.98	-0.54	1.07	-124.87	-44.18
			43	-23.68	-4.98	-0.09	1.07	-102.60	-60.25
			85	-23.68	-4.98	0.37	1.07	-73.46	-76.33
720	Copertura	110	0	222.44	-10.82	0.44	-1.72	3.74	-59.52
			43	222.44	-10.82	-0.29	-1.72	30.97	-68.11
			85	222.44	-10.82	-1.02	-1.72	61.85	-76.70
721	Copertura	14	0	225.25	0.07	-3.10	1.62	-67.20	2.17
			95	225.25	0.07	-1.56	1.62	-67.83	-2.36
			190	225.25	0.07	-0.02	1.62	-59.85	-15.95
722	Copertura	15	0	5.37	2.36	-4.28	2.70	55.61	146.08
			65	5.37	2.36	-2.53	2.70	-38.12	140.43
			130	5.37	2.36	-0.78	2.70	-124.50	123.47
723	Copertura	16	0	68.59	1.83	-1.60	1.44	33.46	133.69
			65	68.59	1.83	-0.67	1.44	-52.82	130.86
			130	68.59	1.83	0.26	1.44	-135.43	122.38
724	Copertura	17	0	-64.09	2.69	-5.01	3.61	65.12	226.00
			65	-64.09	2.69	-2.66	3.61	-80.64	220.73
			130	-64.09	2.69	-0.32	3.61	-219.55	204.93
725	Copertura	18	0	144.54	2.35	-0.18	-0.54	45.13	223.08
			65	144.54	2.35	-0.53	-0.54	-99.30	220.45
			130	144.54	2.35	-0.88	-0.54	-240.31	212.55
726	Copertura	19	0	-170.94	2.19	-4.81	3.32	72.03	312.58
			65	-170.94	2.19	-2.66	3.32	-130.01	307.31
			130	-170.94	2.19	-0.50	3.32	-325.20	291.51
727	Copertura	20	0	258.41	1.12	-0.70	0.68	51.08	305.98
			65	258.41	1.12	-0.26	0.68	-147.23	303.34
			130	258.41	1.12	0.18	0.68	-342.13	295.44
728	Copertura	21	0	-262.79	1.55	-4.46	2.83	77.11	377.58
			65	-262.79	1.55	-2.62	2.83	-167.18	372.32
			130	-262.79	1.55	-0.78	2.83	-404.62	356.51
729	Copertura	22	0	349.72	1.53	-0.24	-0.23	57.56	371.86
			65	349.72	1.53	-0.39	-0.23	-183.57	369.22
			130	349.72	1.53	-0.54	-0.23	-421.28	361.32
730	Copertura	23	0	-301.32	0.91	-3.99	2.22	81.60	420.94
			65	-301.32	0.91	-2.55	2.22	-190.87	415.67
			130	-301.32	0.91	-1.10	2.22	-456.49	399.87
731	Copertura	24	0	398.68	0.41	-0.63	0.55	61.26	415.00
			65	398.68	0.41	-0.27	0.55	-207.92	412.36
			130	398.68	0.41	0.09	0.55	-473.68	404.46

732	Copertura	25	0	-298.85	0.37	-3.66	1.77	90.48	446.97
			65	-298.85	0.37	-2.52	1.77	-198.78	441.11
			130	-298.85	0.37	-1.37	1.77	-480.42	423.52
733	Copertura	26	0	422.90	0.74	-2.91	2.59	63.64	439.31
			65	422.90	0.74	-1.23	2.59	-221.34	436.67
			130	422.90	0.74	0.46	2.59	-502.89	428.77
734	Copertura	27	0	439.37	-0.10	-5.09	6.22	65.37	452.55
			65	439.37	-0.10	-1.05	6.22	-228.22	449.92
			130	439.37	-0.10	2.99	6.22	-518.38	442.02
735	Copertura	28	0	-298.18	0.24	-8.80	7.83	91.46	457.18
			65	-298.18	0.24	-3.70	7.83	-204.39	451.09
			130	-298.18	0.24	1.39	7.83	-492.31	432.81
736	Copertura	29	0	446.59	0.03	-10.16	11.77	63.92	456.14
			65	446.59	0.03	-2.51	11.77	-231.99	453.50
			130	446.59	0.03	5.14	11.77	-524.49	445.60
737	Copertura	30	0	-332.29	0.07	-11.06	10.53	87.45	461.81
			65	-332.29	0.07	-4.21	10.53	-211.52	456.22
			130	-332.29	0.07	2.63	10.53	-503.23	439.48
738	Copertura	31	0	441.78	-0.28	-10.49	12.17	63.88	453.90
			65	441.78	-0.28	-2.58	12.17	-230.59	451.27
			130	441.78	-0.28	5.33	12.17	-521.63	443.37
739	Copertura	32	0	-337.81	-0.15	-11.62	11.22	85.26	459.57
			65	-337.81	-0.15	-4.33	11.22	-212.28	454.12
			130	-337.81	-0.15	2.96	11.22	-502.73	437.76
740	Copertura	33	0	426.73	-0.17	-12.10	13.86	62.72	445.95
			65	426.73	-0.17	-3.09	13.86	-226.58	443.31
			130	426.73	-0.17	5.92	13.86	-512.45	435.41
741	Copertura	34	0	-324.75	-0.27	-12.10	11.81	84.52	451.96
			65	-324.75	-0.27	-4.42	11.81	-208.07	446.49
			130	-324.75	-0.27	3.25	11.81	-493.55	430.09
742	Copertura	35	0	416.76	-0.29	-12.53	14.41	61.60	436.09
			65	416.76	-0.29	-3.16	14.41	-221.29	433.46
			130	416.76	-0.29	6.21	14.41	-500.76	425.56
743	Copertura	36	0	-305.82	-0.32	-12.47	12.28	83.70	441.24
			65	-305.82	-0.32	-4.49	12.28	-201.93	435.78
			130	-305.82	-0.32	3.49	12.28	-480.44	419.37
744	Copertura	37	0	397.97	-0.33	-13.35	15.37	60.14	424.84
			65	397.97	-0.33	-3.36	15.37	-215.43	422.20
			130	397.97	-0.33	6.63	15.37	-487.58	414.30
745	Copertura	38	0	-291.56	-0.28	-12.88	12.82	82.43	429.79
			65	-291.56	-0.28	-4.55	12.82	-195.76	424.34
			130	-291.56	-0.28	3.78	12.82	-466.85	407.98
746	Copertura	39	0	392.49	-0.33	-13.78	15.96	59.36	416.48
			65	392.49	-0.33	-3.41	15.96	-210.79	413.85
			130	392.49	-0.33	6.97	15.96	-477.51	405.95
747	Copertura	40	0	-303.52	-0.04	-13.76	14.02	79.28	424.28
			65	-303.52	-0.04	-4.65	14.02	-195.32	418.83
			130	-303.52	-0.04	4.46	14.02	-462.83	402.47
748	Copertura	41	0	385.15	-0.28	-10.12	12.27	57.83	414.68
			65	385.15	-0.28	-2.15	12.27	-211.14	412.05
			130	385.15	-0.28	5.83	12.27	-476.69	404.15
749	Copertura	42	0	-355.90	-0.09	-15.87	16.62	66.08	415.74
			65	-355.90	-0.09	-5.06	16.62	-203.38	412.17
			130	-355.90	-0.09	5.74	16.62	-468.20	401.45
750	Copertura	43	0	-354.25	-0.40	-2.60	0.95	66.12	413.34
			65	-354.25	-0.40	-1.99	0.95	-201.79	409.86
			130	-354.25	-0.40	-1.37	0.95	-465.20	399.44
751	Copertura	44	0	386.24	-0.16	-6.67	6.36	63.41	418.35
			65	386.24	-0.16	-2.54	6.36	-207.95	415.72
			130	386.24	-0.16	1.60	6.36	-475.89	407.82
752	Copertura	45	0	-299.21	-0.66	-2.28	0.60	79.47	407.99
			65	-299.21	-0.66	-1.90	0.60	-184.58	402.72
			130	-299.21	-0.66	-1.51	0.60	-441.78	386.92
753	Copertura	46	0	375.56	0.02	-1.96	1.26	59.24	398.20
			65	375.56	0.02	-1.14	1.26	-199.02	395.56
			130	375.56	0.02	-0.32	1.26	-453.85	387.66
754	Copertura	47	0	-257.18	-0.80	-2.19	0.60	78.62	383.57
			65	-257.18	-0.80	-1.80	0.60	-169.56	378.30
			130	-257.18	-0.80	-1.41	0.60	-410.89	362.50
755	Copertura	48	0	356.88	-0.74	-2.59	2.32	57.84	377.92
			65	356.88	-0.74	-1.08	2.32	-187.24	375.29
			130	356.88	-0.74	0.43	2.32	-428.89	367.38

756	Copertura	49	0	-220.70	-1.31	-1.90	0.24	75.24	350.20
			65	-220.70	-1.31	-1.74	0.24	-151.25	344.94
			130	-220.70	-1.31	-1.59	0.24	-370.89	329.13
757	Copertura	50	0	318.81	-0.42	-1.98	1.29	54.30	343.88
			65	318.81	-0.42	-1.14	1.29	-168.66	341.25
			130	318.81	-0.42	-0.30	1.29	-388.19	333.35
758	Copertura	51	0	-144.67	-2.00	-1.54	-0.28	70.63	295.37
			65	-144.67	-2.00	-1.73	-0.28	-120.22	290.10
			130	-144.67	-2.00	-1.91	-0.28	-304.22	274.30
759	Copertura	52	0	243.46	-1.87	-2.56	2.56	50.41	290.51
			65	243.46	-1.87	-0.90	2.56	-137.85	287.88
			130	243.46	-1.87	0.77	2.56	-322.68	279.97
760	Copertura	53	0	-47.38	-2.58	-1.35	-0.61	64.47	217.47
			65	-47.38	-2.58	-1.75	-0.61	-75.75	212.20
			130	-47.38	-2.58	-2.15	-0.61	-209.11	196.40
761	Copertura	54	0	132.53	-1.44	-1.33	0.78	42.89	211.63
			65	132.53	-1.44	-0.83	0.78	-94.09	208.99
			130	132.53	-1.44	-0.32	0.78	-227.65	201.09
762	Copertura	55	0	7.03	-2.32	-2.11	0.28	55.16	141.63
			65	7.03	-2.32	-1.92	0.28	-35.68	135.97
			130	7.03	-2.32	-1.74	0.28	-119.16	119.01
763	Copertura	56	0	59.21	-2.09	-1.77	1.78	34.92	133.05
			65	59.21	-2.09	-0.61	1.78	-50.95	130.23
			130	59.21	-2.09	0.55	1.78	-133.15	121.75
764	Copertura	70	0	221.91	-2.88	-0.69	0.20	-69.68	-1.19
			95	221.91	-2.88	-0.50	0.20	-67.12	-5.72
			190	221.91	-2.88	-0.30	0.20	-55.94	-19.31
765	Copertura	81	0	-21.85	3.66	-1.05	1.26	-156.21	15.12
			80	-21.85	3.66	-0.04	1.26	-156.25	-15.03
			160	-21.85	3.66	0.96	1.26	-132.16	-45.18
766	Copertura	126	0	-19.37	-0.15	-0.70	2.58	-144.61	30.28
			30	-19.37	-0.15	0.08	2.58	-152.00	18.97
			60	-19.37	-0.15	0.85	2.58	-155.99	7.66
767	Copertura	98	0	-46.28	1.95	-1.12	1.75	-255.02	-17.11
			82	-46.28	1.95	0.31	1.75	-229.03	-46.02
			165	-46.28	1.95	1.75	1.75	-179.23	-74.94
768	Copertura	99	0	-49.23	3.75	-0.77	0.87	-340.35	-51.64
			82	-49.23	3.75	-0.06	0.87	-285.92	-80.55
			165	-49.23	3.75	0.66	0.87	-207.68	-109.47
769	Copertura	100	0	-38.80	0.79	-0.40	0.55	-409.88	-81.74
			82	-38.80	0.79	0.05	0.55	-330.67	-110.65
			165	-38.80	0.79	0.50	0.55	-227.65	-139.57
770	Copertura	101	0	-51.19	2.21	-0.85	1.23	-453.76	-99.83
			82	-51.19	2.21	0.16	1.23	-359.66	-128.74
			165	-51.19	2.21	1.17	1.23	-241.74	-157.66
771	Copertura	102	0	-54.96	0.09	1.99	-1.83	-479.97	-110.20
			82	-54.96	0.09	0.49	-1.83	-377.32	-139.11
			165	-54.96	0.09	-1.02	-1.83	-250.87	-168.03
772	Copertura	103	0	-58.57	0.87	0.04	0.33	-492.51	-116.14
			82	-58.57	0.87	0.31	0.33	-384.97	-145.05
			165	-58.57	0.87	0.58	0.33	-253.62	-173.97
773	Copertura	104	0	-54.84	-0.45	4.26	-4.41	-498.37	-117.62
			82	-54.84	-0.45	0.63	-4.41	-389.62	-146.53
			165	-54.84	-0.45	-3.00	-4.41	-257.05	-175.45
774	Copertura	105	0	-56.79	0.04	3.44	-3.05	-496.41	-116.24
			82	-56.79	0.04	0.92	-3.05	-388.79	-145.16
			165	-56.79	0.04	-1.59	-3.05	-257.36	-174.07
775	Copertura	111	0	-61.07	-0.43	4.45	-4.44	-482.38	-114.54
			80	-61.07	-0.43	0.91	-4.44	-379.85	-142.55
			160	-61.07	-0.43	-2.63	-4.44	-254.97	-170.56
776	Copertura	112	0	-59.00	-0.28	4.36	-3.98	-478.34	-109.13
			82	-59.00	-0.28	1.08	-3.98	-376.57	-138.04
			165	-59.00	-0.28	-2.20	-3.98	-251.00	-166.96
777	Copertura	113	0	-62.39	-0.35	4.70	-4.36	-466.78	-104.02
			82	-62.39	-0.35	1.11	-4.36	-369.22	-132.94
			165	-62.39	-0.35	-2.48	-4.36	-247.85	-161.85
778	Copertura	114	0	-56.96	-0.59	5.14	-5.14	-459.04	-99.59
			82	-56.96	-0.59	0.91	-5.14	-365.13	-128.51
			165	-56.96	-0.59	-3.32	-5.14	-247.41	-157.42
779	Copertura	115	0	-60.05	-0.11	0.47	-0.07	-458.89	-98.79
			82	-60.05	-0.11	0.41	-0.07	-365.64	-127.70
			165	-60.05	-0.11	0.35	-0.07	-248.58	-156.62

780	Copertura	116	0	-65.37	0.11	3.94	-3.59	-457.15	-99.06
			82	-65.37	0.11	0.98	-3.59	-363.68	-127.98
			165	-65.37	0.11	-1.97	-3.59	-246.39	-156.89
781	Copertura	117	0	-46.52	-0.92	-1.20	2.07	-437.98	-91.65
			82	-46.52	-0.92	0.50	2.07	-350.61	-120.56
			165	-46.52	-0.92	2.21	2.07	-239.43	-149.48
782	Copertura	118	0	-44.23	-0.04	-0.65	1.07	-416.37	-83.76
			82	-44.23	-0.04	0.22	1.07	-335.49	-112.67
			165	-44.23	-0.04	1.10	1.07	-230.81	-141.59
783	Copertura	131	0	-47.69	1.59	-0.91	1.35	-257.22	7.48
			30	-47.69	1.59	-0.50	1.35	-257.89	-3.06
			60	-47.69	1.59	-0.10	1.35	-255.39	-13.59
784	Copertura	133	0	-47.82	-0.53	-0.69	1.26	-366.75	-34.09
			30	-47.82	-0.53	-0.31	1.26	-354.95	-44.62
			60	-47.82	-0.53	0.07	1.26	-339.98	-55.16
785	Copertura	139	0	-39.94	1.38	-0.32	1.10	-451.81	-59.01
			30	-39.94	1.38	0.01	1.10	-432.52	-69.55
			60	-39.94	1.38	0.34	1.10	-410.08	-80.08
786	Copertura	143	0	-50.05	-0.57	-0.49	0.68	-508.14	-80.41
			30	-50.05	-0.57	-0.29	0.68	-482.43	-90.95
			60	-50.05	-0.57	-0.08	0.68	-453.57	-101.48
787	Copertura	147	0	-55.89	0.91	0.71	3.37	-539.58	-88.69
			30	-55.89	0.91	1.72	3.37	-511.39	-99.23
			60	-55.89	0.91	2.73	3.37	-480.04	-109.76
788	Copertura	151	0	-57.64	-0.52	3.45	-4.88	-556.06	-95.50
			30	-57.64	-0.52	1.98	-4.88	-525.83	-106.04
			60	-57.64	-0.52	0.52	-4.88	-492.44	-116.57
789	Copertura	155	0	-55.29	0.25	6.35	-3.10	-562.77	-96.83
			30	-55.29	0.25	5.42	-3.10	-532.14	-107.37
			60	-55.29	0.25	4.49	-3.10	-498.35	-117.90
790	Copertura	159	0	-56.35	-0.28	6.41	-4.37	-559.69	-94.89
			30	-56.35	-0.28	5.10	-4.37	-529.64	-105.42
			60	-56.35	-0.28	3.79	-4.37	-496.44	-115.95
791	Copertura	119	0	-33.91	-2.65	-0.69	1.22	-380.27	-68.78
			82	-33.91	-2.65	0.32	1.22	-311.72	-97.70
			165	-33.91	-2.65	1.32	1.22	-219.37	-126.61
792	Copertura	120	0	-41.55	-1.00	-0.70	1.04	-325.29	-46.45
			82	-41.55	-1.00	0.16	1.04	-275.14	-75.36
			165	-41.55	-1.00	1.02	1.04	-201.18	-104.28
793	Copertura	121	0	-48.17	-4.14	-0.60	1.17	-241.76	-10.12
			82	-48.17	-4.14	0.36	1.17	-221.52	-39.04
			165	-48.17	-4.14	1.33	1.17	-177.47	-67.95
794	Copertura	122	0	-23.16	-1.71	0.46	-0.86	-157.55	10.84
			82	-23.16	-1.71	-0.25	-0.86	-153.69	-20.20
			165	-23.16	-1.71	-0.96	-0.86	-124.29	-51.23
795	Copertura	123	0	221.91	-2.88	-0.30	0.20	-55.94	-19.31
			82	221.91	-2.88	-0.14	0.20	-33.22	-35.89
			165	221.91	-2.88	0.03	0.20	3.16	-52.47
796	Copertura	163	0	-61.70	0.12	7.31	-3.84	-549.82	-92.22
			33	-61.70	0.12	6.06	-3.84	-517.91	-103.66
			65	-61.70	0.12	4.81	-3.84	-482.27	-115.11
797	Copertura	167	0	-58.37	-0.09	7.61	-4.58	-537.24	-87.50
			30	-58.37	-0.09	6.23	-4.58	-509.42	-98.03
			60	-58.37	-0.09	4.86	-4.58	-478.43	-108.57
798	Copertura	171	0	-63.17	-0.15	8.09	-4.68	-523.10	-83.43
			30	-63.17	-0.15	6.69	-4.68	-496.49	-93.97
			60	-63.17	-0.15	5.28	-4.68	-466.72	-104.50
799	Copertura	174	0	-56.17	-0.15	8.49	-4.82	-512.24	-78.04
			30	-56.17	-0.15	7.05	-4.82	-487.25	-88.57
			60	-56.17	-0.15	5.60	-4.82	-459.10	-99.11
800	Copertura	179	0	-61.88	-0.20	7.42	-10.08	-511.71	-77.53
			30	-61.88	-0.20	4.40	-10.08	-486.87	-88.07
			60	-61.88	-0.20	1.38	-10.08	-458.87	-98.60
801	Copertura	183	0	-63.54	-0.04	1.61	6.41	-510.39	-78.18
			30	-63.54	-0.04	3.53	6.41	-485.36	-88.71
			60	-63.54	-0.04	5.45	6.41	-457.17	-99.25
802	Copertura	187	0	-49.57	0.57	0.03	1.44	-486.93	-71.18
			30	-49.57	0.57	0.46	1.44	-464.00	-81.71
			60	-49.57	0.57	0.89	1.44	-437.91	-92.25
803	Copertura	191	0	-41.18	-0.74	0.25	1.70	-460.01	-62.09
			30	-41.18	-0.74	0.76	1.70	-439.80	-72.62
			60	-41.18	-0.74	1.27	1.70	-416.44	-83.16

804	Copertura	194	0	-36.68	0.85	0.44	1.27	-416.26	-49.84
			30	-36.68	0.85	0.82	1.27	-399.72	-60.38
			60	-36.68	0.85	1.20	1.27	-380.03	-70.91
805	Copertura	198	0	-38.78	-1.68	0.48	0.99	-345.80	-23.25
			30	-38.78	-1.68	0.78	0.99	-337.24	-33.78
			60	-38.78	-1.68	1.08	0.99	-325.53	-44.31
806	Copertura	203	0	-49.65	0.34	0.55	-0.03	-243.68	6.74
			30	-49.65	0.34	0.54	-0.03	-244.12	-3.79
			60	-49.65	0.34	0.53	-0.03	-241.40	-14.33
807	Copertura	207	0	-21.67	-0.63	1.07	0.35	-142.09	37.66
			30	-21.67	-0.63	1.18	0.35	-151.69	26.35
			60	-21.67	-0.63	1.28	0.35	-157.90	15.05

1.1.9.2 Piastre SLU

Tabella 18.I

Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNm/cm]	M2-2 [daNm/cm]	M1-2 [daNm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	-4.954	-0.767	-0.573	1044.641	156.771	120.149	12.874	-3.177
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	-4.585	-0.636	0.669	998.935	-209.566	-117.274	12.023	3.843
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	-4.541	-0.586	-0.894	925.563	126.062	120.664	11.992	2.870

1.1.10 Risultati Condizioni (Vento (-X)).

1.1.10.1 Sollecitazioni SLU

Tabella 19.I

Sollecitazioni									
Asta	Imp.	Fili	X [cm]	N [daN]	Mt [daNm]	Mxz [daNm]	Txz [daN]	Mxy [daNm]	Txy [daN]
1	Fondazione	1, 2	0	93.43	30.87	-60.63	-165.98	-2.68	-1.76
			42	81.19	30.87	-114.67	-110.58	-1.77	-2.63
			83	69.00	30.87	-151.20	-81.00	-0.50	-3.48
2	Fondazione	1, 2	0	50.89	29.52	-130.14	-86.53	-0.50	-0.96
			42	38.73	29.52	-161.27	-78.17	0.08	-1.81
			83	26.60	29.52	-192.43	-85.70	1.01	-2.66
3	Fondazione	1, 15	0	-14.37	-34.85	36.62	-162.03	10.73	34.39
			40	-14.17	-34.84	-14.82	-97.10	-1.93	29.30
			80	-13.98	-34.83	-41.07	-35.28	-12.60	24.42
4	Fondazione	1, 15	0	-20.09	88.26	-41.55	4.53	-12.60	-25.40
			40	-19.90	88.27	-27.88	64.11	-1.56	-30.12
			80	-19.73	88.28	9.20	122.50	11.33	-34.72

5	Fondazio ne	2, 3	0	92.13	-2.33	-191.54	149.09	0.68	2.24
			35	82.06	-2.32	-140.35	135.13	-0.06	2.09
			69	72.02	-2.32	-94.67	117.70	-0.76	1.94
6	Fondazio ne	2, 3	0	65.43	-1.15	-92.39	88.97	-0.76	-2.28
			35	55.42	-1.15	-62.88	70.46	0.05	-2.43
			69	45.43	-1.15	-39.71	52.48	0.92	-2.57
7	Fondazio ne	3, 4	0	48.49	-17.85	-52.09	64.98	0.88	1.96
			35	38.52	-17.85	-30.56	48.60	0.23	1.82
			69	28.57	-17.85	-14.30	34.63	-0.38	1.69
8	Fondazio ne	3, 4	0	30.21	-3.72	-19.70	38.13	-0.38	-1.42
			35	20.26	-3.72	-6.56	27.03	0.14	-1.55
			69	10.33	-3.72	3.28	19.06	0.69	-1.67
9	Fondazio ne	4, 5	0	15.59	-18.33	-9.17	33.98	0.57	1.23
			35	5.66	-18.33	3.62	29.20	0.17	1.11
			69	-4.27	-18.33	15.32	27.62	-0.20	1.01
10	Fondazio ne	4, 5	0	-3.39	-7.83	7.71	26.38	-0.20	-1.12
			35	-13.32	-7.83	18.96	27.84	0.21	-1.22
			69	-23.26	-7.83	31.20	32.05	0.64	-1.30
11	Fondazio ne	5, 6	0	-21.82	-16.02	17.29	24.35	0.47	0.18
			35	-31.76	-16.02	28.74	30.83	0.42	0.10
			69	-41.72	-16.02	42.75	39.09	0.40	0.04
12	Fondazio ne	5, 6	0	-49.31	4.13	38.66	69.11	0.40	-0.07
			35	-59.28	4.13	66.09	78.41	0.43	-0.12
			69	-69.28	4.13	96.76	87.66	0.48	-0.16
13	Fondazio ne	6, 7	0	1.76	22.44	100.56	-175.49	0.42	0.75
			35	-8.25	22.44	43.40	-167.89	0.16	0.73
			69	-18.27	22.44	-11.62	-163.30	-0.09	0.73
14	Fondazio ne	6, 7	0	-34.07	23.86	5.64	-167.46	-0.09	-0.19
			35	-44.10	23.86	-49.83	-166.28	-0.02	-0.17
			69	-54.14	23.86	-105.41	-167.98	0.03	-0.13
15	Fondazio ne	7, 8	0	16.07	-7.57	-105.01	108.61	-0.24	0.32
			35	6.02	-7.57	-66.05	105.51	-0.36	0.38
			69	-4.02	-7.57	-28.16	102.68	-0.51	0.46
16	Fondazio ne	7, 8	0	-14.44	-22.18	-39.79	70.02	-0.51	-0.89
			35	-24.49	-22.18	-13.94	68.47	-0.21	-0.80
			69	-34.55	-22.18	11.68	68.72	0.04	-0.69
17	Fondazio ne	8, 9	0	-39.17	-19.18	-10.57	61.52	-0.19	-0.79
			35	-49.24	-19.18	12.98	63.67	0.06	-0.67
			69	-59.34	-19.19	37.60	67.63	0.27	-0.53
18	Fondazio ne	8, 9	0	-71.04	-8.62	25.95	95.66	0.27	-0.69
			35	-81.16	-8.62	61.86	100.93	0.48	-0.54
			69	-91.31	-8.62	99.69	106.58	0.64	-0.37
19	Fondazio ne	9, 10	0	-15.43	28.15	104.41	-179.92	0.29	0.88
			35	-25.60	28.14	45.20	-175.48	-0.04	1.07
			69	-35.78	28.14	-12.90	-173.66	-0.45	1.28
20	Fondazio ne	9, 10	0	-52.85	26.73	5.45	-163.37	-0.44	-0.50
			35	-63.05	26.73	-48.99	-164.58	-0.31	-0.28
			69	-73.28	26.73	-104.31	-168.31	-0.25	-0.03
21	Fondazio ne	10, 11	0	0.81	11.74	-100.54	76.52	-0.18	0.38
			35	-9.43	11.74	-72.91	71.75	-0.36	0.64
			69	-19.67	11.74	-46.86	67.65	-0.62	0.91
22	Fondazio ne	10, 11	0	-26.30	-15.05	-46.50	35.12	-0.62	0.02
			35	-36.56	-15.05	-32.79	32.91	-0.68	0.31
			69	-46.82	-15.05	-19.38	33.41	-0.83	0.60
23	Fondazio	11, 12	0	-43.32	-5.35	-31.63	52.85	-0.97	-2.04

	ne								
			35	-53.60	-5.35	-10.80	56.63	-0.32	-1.74
			69	-63.91	-5.35	11.98	64.09	0.23	-1.44
24	Fondazio ne	11, 12	0	-60.99	-22.50	4.93	55.78	0.23	1.88
			35	-71.32	-22.50	28.06	66.91	-0.47	2.19
			69	-81.68	-22.50	55.62	81.37	-1.28	2.50
25	Fondazio ne	12, 13	0	-75.93	-2.68	42.61	76.10	-1.36	-3.07
			35	-86.32	-2.68	73.81	93.07	-0.36	-2.77
			69	-96.74	-2.68	111.14	111.34	0.55	-2.46
26	Fondazio ne	12, 13	0	-99.13	-10.79	108.96	124.68	0.54	2.91
			35	-109.59	-10.79	157.17	142.35	-0.51	3.21
			69	-120.10	-10.79	211.01	156.70	-1.67	3.50
27	Fondazio ne	13, 14	0	-44.73	22.26	210.26	-67.68	-2.22	-3.16
			42	-57.39	22.26	186.74	-60.01	-1.12	-2.13
			83	-70.08	22.26	163.12	-69.35	-0.45	-1.14
28	Fondazio ne	13, 14	0	-88.31	19.34	160.88	-56.41	-0.45	-3.57
			42	-101.05	19.34	134.13	-89.00	0.83	-2.61
			83	-113.84	19.34	88.10	-150.10	1.72	-1.67
29	Fondazio ne	14, 16	0	16.06	-13.40	-27.86	155.05	12.57	38.07
			40	15.85	-13.39	19.37	82.79	-2.75	39.06
			80	15.65	-13.38	38.33	12.78	-18.53	40.38
30	Fondazio ne	14, 16	0	11.72	138.42	49.51	-16.79	-18.54	-49.89
			40	11.53	138.43	29.20	-85.48	0.98	-48.31
			80	11.34	138.45	-18.36	-154.00	19.84	-46.52
31	Fondazio ne	15, 17	0	-26.12	-40.36	-3.79	-71.45	14.20	47.93
			33	-25.99	-40.35	-19.48	-23.54	-0.83	43.12
			66	-25.87	-40.34	-19.41	24.07	-14.27	38.33
32	Fondazio ne	15, 17	0	-24.07	150.67	-41.73	59.40	-14.27	-38.64
			33	-23.96	150.69	-14.28	107.14	-0.73	-43.44
			66	-23.85	150.70	29.00	155.41	14.41	-48.29
33	Fondazio ne	16, 18	0	18.86	-46.85	4.80	67.18	23.34	70.63
			33	18.71	-46.84	17.59	10.12	0.12	70.11
			66	18.56	-46.82	11.51	-47.28	-22.93	69.60
34	Fondazio ne	16, 18	0	11.68	200.24	42.81	-62.29	-22.94	-69.88
			33	11.54	200.26	12.72	-120.39	0.21	-70.43
			66	11.40	200.27	-36.71	-179.58	23.55	-71.04
35	Fondazio ne	17, 19	0	-15.46	-71.24	1.07	-62.94	19.04	58.67
			33	-15.36	-71.22	-11.68	-14.12	0.48	53.81
			66	-15.27	-71.21	-8.22	35.31	-16.48	48.97
36	Fondazio ne	17, 19	0	-14.67	160.59	-33.60	61.42	-16.48	-48.34
			33	-14.59	160.60	-5.08	111.71	0.27	-53.19
			66	-14.50	160.62	40.21	163.12	18.63	-58.08
37	Fondazio ne	18, 20	0	10.59	-92.32	-10.00	85.92	28.90	83.93
			33	10.46	-92.31	8.47	25.70	1.31	83.29
			66	10.33	-92.29	6.91	-35.51	-26.07	82.68
38	Fondazio ne	18, 20	0	7.23	210.85	34.65	-54.06	-26.08	-82.03
			33	7.10	210.87	6.58	-116.47	1.09	-82.66
			66	6.98	210.89	-42.34	-180.38	28.48	-83.35
39	Fondazio ne	19, 21	0	-11.83	-93.87	14.36	-84.20	18.86	60.55
			33	-11.75	-93.85	-4.83	-31.84	-0.31	55.65
			66	-11.68	-93.84	-6.60	21.36	-17.87	50.78
40	Fondazio ne	19, 21	0	-11.47	171.74	-22.32	44.62	-17.87	-50.04
			33	-11.40	171.75	1.30	98.81	-0.56	-54.92
			66	-11.34	171.77	42.99	154.12	18.38	-59.83
41	Fondazio ne	20, 22	0	10.13	-126.77	-20.58	105.71	28.12	85.30

			33	10.01	-126.75	3.60	40.49	0.09	84.60
			66	9.90	-126.73	6.07	-25.88	-27.72	83.94
42	Fondazio ne	20, 22	0	8.91	210.51	26.13	-47.11	-27.72	-82.66
			33	8.80	210.53	-0.52	-114.79	-0.33	-83.33
			66	8.69	210.55	-49.75	-183.93	27.29	-84.06
43	Fondazio ne	21, 23	0	-7.34	-126.79	31.79	-116.35	22.30	67.71
			33	-7.28	-126.77	2.62	-60.21	0.77	62.79
			66	-7.22	-126.75	-7.92	-3.53	-19.14	57.89
44	Fondazio ne	21, 23	0	-10.64	165.40	-12.86	28.09	-19.14	-60.37
			33	-10.58	165.42	5.83	85.38	1.59	-65.27
			66	-10.53	165.44	43.54	143.32	23.94	-70.19
45	Fondazio ne	22, 24	0	9.44	-160.73	-36.61	137.51	31.70	92.10
			33	9.33	-160.71	-2.78	67.24	1.43	91.36
			66	9.23	-160.69	7.72	-3.87	-28.60	90.68
46	Fondazio ne	22, 24	0	12.18	196.55	15.79	-24.52	-28.60	-92.85
			33	12.08	196.57	-4.13	-96.51	2.15	-93.53
			66	11.99	196.59	-47.97	-169.46	33.13	-94.26
47	Fondazio ne	23, 25	0	-15.98	-178.76	48.33	-166.03	22.61	65.53
			33	-15.93	-178.75	3.14	-107.82	1.80	60.62
			66	-15.89	-178.73	-22.86	-49.71	-17.40	55.77
48	Fondazio ne	23, 25	0	-30.17	76.73	-7.35	-23.46	-17.40	-36.60
			33	-30.14	76.74	-5.51	34.67	-4.52	-41.43
			66	-30.11	76.76	15.54	92.98	9.94	-46.26
49	Fondazio ne	24, 26	0	23.97	-203.40	-47.19	181.36	31.15	86.41
			33	23.89	-203.38	0.55	107.82	2.75	85.70
			66	23.81	-203.36	23.98	34.04	-25.42	85.06
50	Fondazio ne	24, 26	0	39.71	117.28	21.11	1.60	-25.41	-55.87
			33	39.64	117.30	9.42	-72.64	-6.87	-56.46
			66	39.59	117.31	-26.89	-147.61	11.86	-57.07
51	Fondazio ne	25, 26	0	120.97	1.53	-353.79	61.99	-0.10	-0.19
			49	106.61	1.53	-304.28	120.83	0.00	-0.22
			97	92.32	1.53	-237.21	137.17	0.11	-0.25
52	Fondazio ne	25, 26	0	99.45	-3.68	-220.61	86.23	0.11	0.09
			49	85.24	-3.68	-177.55	75.47	0.07	0.04
			97	71.10	-3.68	-143.93	49.24	0.06	-0.01
53	Fondazio ne	25, 26	0	86.28	-2.52	-113.36	78.79	0.06	-0.13
			49	72.20	-2.52	-80.04	45.96	0.14	-0.19
			97	58.18	-2.52	-63.11	12.33	0.25	-0.25
54	Fondazio ne	25, 26	0	73.92	0.52	-42.26	55.95	0.25	0.17
			49	59.95	0.52	-19.85	25.37	0.18	0.11
			97	46.03	0.52	-11.17	-0.23	0.14	0.05
55	Fondazio ne	25, 26	0	59.85	0.77	1.06	24.11	0.14	0.07
			49	45.96	0.77	10.49	4.22	0.12	0.02
			97	32.12	0.77	11.60	-10.18	0.12	-0.03
56	Fondazio ne	25, 26	0	44.61	0.61	15.66	4.00	0.12	0.07
			49	30.80	0.61	17.85	-5.62	0.10	0.02
			97	17.01	0.61	16.33	-11.38	0.10	-0.01
57	Fondazio ne	25, 26	0	28.59	0.39	16.45	-6.25	0.10	0.06
			49	14.81	0.39	15.36	-9.15	0.08	0.04
			97	1.05	0.39	13.36	-10.10	0.07	0.02
58	Fondazio ne	25, 26	0	12.05	0.09	11.92	-9.71	0.07	0.02
			49	-1.70	0.09	9.95	-9.52	0.06	0.01
			97	-15.46	0.09	8.23	-8.83	0.06	0.02
59	Fondazio ne	25, 26	0	-4.71	-0.17	6.48	-9.50	0.06	0.08
			49	-18.47	-0.17	4.79	-8.81	0.02	0.10

			97	-32.25	-0.17	3.36	-8.46	-0.04	0.14
60	Fondazio ne	25, 26	0	-22.97	-0.29	1.22	-8.60	-0.04	-0.09
			49	-36.78	-0.29	-0.24	-8.81	0.00	-0.04
			97	-50.61	-0.29	-1.93	-9.62	0.00	0.02
61	Fondazio ne	25, 26	0	-39.71	-0.14	-3.90	-8.50	0.01	0.01
			49	-53.57	-0.14	-5.57	-9.83	-0.02	0.08
			97	-67.48	-0.14	-7.96	-11.43	-0.07	0.16
62	Fondazio ne	25, 26	0	-56.69	0.08	-10.07	-9.66	-0.07	-0.08
			49	-70.64	0.08	-12.35	-11.13	-0.06	0.02
			97	-84.65	0.08	-15.19	-11.85	-0.09	0.13
63	Fondazio ne	25, 26	0	-73.42	0.51	-17.02	-12.03	-0.09	-0.06
			49	-87.50	0.51	-19.94	-11.18	-0.09	0.06
			97	-101.64	0.51	-21.85	-7.73	-0.15	0.19
64	Fondazio ne	25, 26	0	-89.62	1.19	-21.91	-13.42	-0.15	-0.10
			49	-103.83	1.19	-24.01	-6.17	-0.13	0.04
			97	-118.13	1.19	-21.38	6.21	-0.19	0.18
65	Fondazio ne	25, 26	0	-104.70	1.94	-16.22	-10.97	-0.19	-0.13
			49	-119.09	1.94	-14.40	7.80	-0.16	0.02
			97	-133.57	1.94	-1.66	33.92	-0.20	0.17
66	Fondazio ne	25, 26	0	-117.86	1.67	12.74	-0.28	-0.20	-0.12
			49	-132.44	1.67	23.45	33.54	-0.18	0.03
			97	-147.12	1.67	52.36	74.21	-0.23	0.17
67	Fondazio ne	25, 26	0	-128.64	-0.88	81.81	30.51	-0.23	-0.17
			49	-143.43	-0.88	110.51	75.63	-0.18	-0.03
			97	-158.33	-0.88	161.28	120.01	-0.20	0.11
68	Fondazio ne	25, 26	0	-134.42	-5.66	200.50	33.06	-0.20	-0.19
			49	-149.43	-5.66	228.85	68.65	-0.14	-0.06
			97	-164.57	-5.66	270.08	83.64	-0.14	0.05
69	Fondazio ne	25, 26	0	-155.57	-10.93	305.53	186.98	-0.14	0.93
			49	-170.83	-10.93	396.48	166.61	-0.62	1.03
			97	-186.23	-10.93	465.04	91.00	-1.14	1.11
70	Fondazio ne	25, 28	0	-25.05	-81.43	25.83	-137.38	14.11	44.58
			43	-25.04	-81.41	-16.57	-62.14	-3.87	40.04
			85	-25.04	-81.39	-26.96	13.34	-19.93	35.54
71	Fondazio ne	25, 28	0	-18.17	197.09	-44.89	46.02	-19.94	-50.14
			43	-18.18	197.10	-9.12	122.65	2.33	-54.71
			85	-18.20	197.13	59.66	201.32	26.57	-59.40
72	Fondazio ne	26, 27	0	35.29	-82.82	-10.39	110.60	14.52	61.62
			33	35.25	-82.80	13.65	34.95	-5.71	61.00
			66	35.22	-82.78	12.61	-41.44	-25.74	60.37
73	Fondazio ne	26, 27	0	17.69	249.03	35.19	-62.39	-25.75	-90.31
			33	17.67	249.05	1.87	-139.80	4.16	-90.99
			66	17.66	249.07	-57.21	-218.49	34.31	-91.77
74	Fondazio ne	27, 29	0	10.98	-168.33	-39.32	147.43	31.49	93.71
			33	10.97	-168.31	-3.78	67.81	0.70	92.90
			66	10.97	-168.29	5.37	-12.40	-29.83	92.13
75	Fondazio ne	27, 29	0	2.62	221.28	21.11	-23.50	-29.83	-89.37
			33	2.62	221.30	0.03	-104.34	-0.21	-90.16
			66	2.62	221.32	-47.85	-185.97	29.68	-91.02
76	Fondazio ne	28, 30	0	-5.49	-142.68	37.25	-140.18	23.48	68.35
			37	-5.52	-142.67	-1.38	-71.42	-0.56	63.40
			73	-5.55	-142.65	-14.80	-1.99	-22.81	58.49
77	Fondazio ne	28, 30	0	-3.03	190.25	-29.37	41.09	-22.81	-59.58
			37	-3.06	190.27	-1.57	111.43	-0.17	-64.51
			73	-3.09	190.29	52.13	182.96	24.29	-69.51

78	Fondazio ne	29, 31	0	2.55	-187.94	-41.99	163.80	32.95	96.41
			33	2.55	-187.92	-1.47	81.71	1.28	95.53
			66	2.55	-187.89	11.93	-0.51	-30.11	94.69
79	Fondazio ne	29, 31	0	-4.73	206.76	20.91	-12.72	-30.11	-94.11
			33	-4.73	206.78	3.11	-95.20	1.09	-94.97
			66	-4.73	206.80	-41.97	-178.12	32.58	-95.88
80	Fondazio ne	30, 32	0	2.19	-153.45	41.09	-151.90	24.19	72.23
			34	2.16	-153.43	0.68	-84.07	0.32	67.19
			69	2.13	-153.42	-16.45	-15.93	-21.83	62.17
81	Fondazio ne	30, 32	0	1.15	183.65	-23.17	32.11	-21.83	-61.47
			34	1.12	183.66	-0.44	100.74	0.08	-66.49
			69	1.10	183.68	45.92	170.04	23.72	-71.57
82	Fondazio ne	31, 33	0	3.96	-196.03	-43.65	171.95	29.33	90.57
			33	3.96	-196.01	-0.62	88.85	-0.41	89.66
			66	3.96	-195.99	15.01	5.89	-29.85	88.79
83	Fondazio ne	31, 33	0	-5.16	197.21	20.72	-4.64	-29.85	-88.31
			33	-5.16	197.23	5.50	-87.62	-0.57	-89.19
			66	-5.16	197.25	-37.14	-170.82	29.02	-90.12
84	Fondazio ne	32, 34	0	3.54	-167.07	39.98	-155.30	23.62	71.05
			35	3.51	-167.05	-1.50	-85.15	-0.01	65.97
			69	3.48	-167.03	-18.77	-14.99	-21.90	60.93
85	Fondazio ne	32, 34	0	1.24	162.05	-21.18	25.34	-21.91	-60.23
			35	1.22	162.07	-0.30	95.74	-0.26	-65.27
			69	1.19	162.09	44.94	166.56	23.13	-70.36
86	Fondazio ne	33, 35	0	2.17	-199.05	-43.37	173.65	32.03	94.39
			33	2.17	-199.03	0.20	90.43	1.04	93.46
			66	2.17	-199.01	16.35	7.49	-29.66	92.57
87	Fondazio ne	33, 35	0	-7.58	190.26	20.54	-4.96	-29.66	-92.48
			33	-7.59	190.28	5.23	-87.79	1.01	-93.37
			66	-7.59	190.30	-37.41	-170.72	31.97	-94.31
88	Fondazio ne	34, 36	0	3.50	-164.57	39.82	-160.83	23.02	69.46
			35	3.48	-164.55	-3.43	-89.92	-0.07	64.37
			69	3.46	-164.54	-22.25	-19.22	-21.40	59.32
89	Fondazio ne	34, 36	0	1.69	162.24	-20.16	14.19	-21.40	-59.25
			35	1.67	162.25	-3.06	84.92	-0.09	-64.31
			69	1.65	162.27	38.48	155.93	22.97	-69.40
90	Fondazio ne	35, 37	0	5.79	-201.67	-45.85	181.33	28.66	89.17
			33	5.79	-201.65	0.31	98.53	-0.61	88.24
			66	5.79	-201.63	19.22	16.14	-29.59	87.37
91	Fondazio ne	35, 37	0	-3.64	185.92	20.62	-1.75	-29.59	-87.92
			33	-3.65	185.94	6.48	-83.89	-0.43	-88.79
			66	-3.65	185.96	-34.75	-166.01	29.02	-89.70
92	Fondazio ne	36, 38	0	3.64	-163.94	37.95	-162.46	22.83	68.96
			35	3.62	-163.92	-5.83	-91.44	-0.08	63.86
			69	3.60	-163.90	-25.16	-20.66	-21.24	58.81
93	Fondazio ne	36, 38	0	-1.57	161.31	-22.99	15.02	-21.24	-58.34
			35	-1.59	161.33	-5.59	85.86	-0.24	-63.39
			69	-1.61	161.35	36.31	157.07	22.51	-68.48
94	Fondazio ne	37, 39	0	4.20	-204.90	-44.08	179.48	31.94	94.42
			33	4.20	-204.88	1.62	97.56	0.94	93.51
			66	4.20	-204.86	20.37	16.12	-29.78	92.66
95	Fondazio ne	37, 39	0	-1.60	181.18	18.01	-5.50	-29.78	-93.38
			33	-1.61	181.21	2.81	-86.65	1.18	-94.23
			66	-1.61	181.23	-39.17	-167.70	32.41	-95.11
96	Fondazio	38, 40	0	3.92	-157.37	33.13	-156.02	22.28	67.05

	ne								
			34	3.90	-157.35	-8.17	-85.18	0.19	61.97
			69	3.89	-157.33	-25.22	-14.38	-20.17	56.93
97	Fondazio ne	38, 40	0	-6.67	161.68	-23.45	13.96	-20.17	-55.77
			34	-6.69	161.70	-6.50	85.05	-0.21	-60.80
			69	-6.71	161.72	34.89	156.74	21.49	-65.87
98	Fondazio ne	39, 41	0	9.68	-214.61	-51.04	190.01	29.17	89.83
			33	9.68	-214.58	-1.67	109.34	-0.33	88.96
			66	9.68	-214.56	21.20	29.39	-29.55	88.16
99	Fondazio ne	39, 41	0	9.78	165.09	11.00	6.70	-29.55	-93.33
			33	9.78	165.11	0.10	-72.66	1.38	-94.11
			66	9.79	165.13	-36.92	-151.57	32.57	-94.92
100	Fondazio ne	40, 42	0	-0.65	-150.16	30.88	-140.55	20.97	64.59
			35	-0.67	-150.14	-5.09	-67.94	-0.44	59.54
			69	-0.69	-150.12	-15.97	4.89	-20.11	54.53
101	Fondazio ne	40, 42	0	-7.17	172.56	-18.32	38.71	-20.11	-51.69
			35	-7.19	172.58	7.66	111.98	-1.42	-56.70
			69	-7.21	172.60	59.01	185.76	19.01	-61.73
102	Fondazio ne	41, 44	0	23.29	-235.54	-55.20	217.18	32.42	88.58
			33	23.31	-235.51	3.55	139.03	3.32	87.80
			66	23.33	-235.49	36.67	61.94	-25.53	87.11
103	Fondazio ne	41, 44	0	37.75	89.29	20.38	25.96	-25.52	-55.78
			33	37.79	89.31	16.33	-50.36	-7.01	-56.42
			66	37.84	89.33	-12.83	-126.28	11.71	-57.06
104	Fondazio ne	42, 43	0	-1.85	-127.32	42.16	-85.69	18.55	55.52
			23	-1.87	-127.31	28.11	-36.47	6.49	49.35
			46	-1.89	-127.29	25.37	12.54	-4.15	43.20
105	Fondazio ne	43, 44	0	147.74	16.15	-410.17	35.63	-7.60	-8.94
			49	133.13	16.15	-370.19	106.03	-3.27	-8.87
			97	118.62	16.15	-309.33	125.08	1.03	-8.80
106	Fondazio ne	43, 44	0	123.50	2.05	-267.62	107.91	1.03	1.21
			49	109.08	2.05	-214.41	94.67	0.43	1.28
			97	94.75	2.05	-172.58	63.37	-0.21	1.34
107	Fondazio ne	43, 44	0	103.79	0.55	-133.40	96.21	-0.21	-0.14
			49	89.54	0.55	-92.99	57.52	-0.16	-0.08
			97	75.36	0.55	-71.79	18.24	-0.14	-0.01
108	Fondazio ne	43, 44	0	86.69	-1.50	-44.16	61.39	-0.14	-0.09
			49	72.57	-1.50	-20.30	25.95	-0.11	-0.03
			97	58.51	-1.50	-12.31	-3.60	-0.11	0.03
109	Fondazio ne	43, 44	0	70.08	-0.95	1.42	28.80	-0.11	-0.08
			49	56.07	-0.95	12.39	5.91	-0.08	-0.03
			97	42.10	-0.95	13.79	-10.63	-0.08	0.02
110	Fondazio ne	43, 44	0	52.93	-0.64	18.46	5.18	-0.08	-0.06
			49	39.00	-0.64	20.88	-5.82	-0.06	-0.02
			97	25.10	-0.64	19.07	-12.38	-0.06	0.01
111	Fondazio ne	43, 44	0	35.37	-0.38	18.93	-6.60	-0.06	-0.05
			49	21.50	-0.38	17.58	-9.86	-0.05	-0.03
			97	7.64	-0.38	15.23	-10.89	-0.04	-0.02
112	Fondazio ne	43, 44	0	17.56	-0.12	13.43	-10.45	-0.04	-0.03
			49	3.71	-0.12	11.14	-10.16	-0.02	-0.04
			97	-10.14	-0.12	9.17	-9.28	0.00	-0.05
113	Fondazio ne	43, 44	0	-0.35	0.10	7.13	-10.32	-0.01	0.02
			49	-14.20	0.10	5.11	-9.40	-0.01	-0.01
			97	-28.06	0.10	3.46	-8.83	0.00	-0.04
114	Fondazio ne	43, 44	0	-18.10	0.14	1.52	-9.25	0.00	0.00

			49	-31.98	0.14	-0.18	-9.24	0.01	-0.05
			97	-45.89	0.14	-2.02	-9.84	0.05	-0.10
115	Fondazio ne	43, 44	0	-36.41	0.14	-4.07	-8.60	0.04	0.04
			49	-50.35	0.14	-5.73	-9.74	0.04	-0.03
			97	-64.32	0.14	-8.02	-11.16	0.07	-0.10
116	Fondazio ne	43, 44	0	-53.80	-0.14	-10.22	-9.66	0.07	0.06
			49	-67.82	-0.14	-12.45	-10.95	0.06	-0.02
			97	-81.90	-0.14	-15.14	-11.47	0.09	-0.12
117	Fondazio ne	43, 44	0	-70.87	-0.58	-17.06	-11.71	0.09	0.08
			49	-85.00	-0.58	-19.77	-10.67	0.08	-0.03
			97	-99.20	-0.58	-21.37	-7.02	0.11	-0.14
118	Fondazio ne	43, 44	0	-87.18	-1.18	-21.28	-13.33	0.11	0.10
			49	-101.46	-1.18	-23.29	-5.89	0.09	-0.02
			97	-115.81	-1.18	-20.48	6.62	0.13	-0.14
119	Fondazio ne	43, 44	0	-102.27	-1.60	-14.96	-11.80	0.13	0.10
			49	-116.71	-1.60	-13.52	7.01	0.11	-0.02
			97	-131.24	-1.60	-1.19	33.01	0.16	-0.15
120	Fondazio ne	43, 44	0	-115.55	-1.71	14.07	-2.84	0.16	0.17
			49	-130.18	-1.71	23.47	30.66	0.11	0.04
			97	-144.91	-1.71	50.86	70.78	0.12	-0.09
121	Fondazio ne	43, 44	0	-126.61	-0.01	82.28	24.57	0.12	-0.08
			49	-141.44	-0.01	107.92	68.93	0.19	-0.20
			97	-156.39	-0.01	155.23	112.44	0.32	-0.32
122	Fondazio ne	43, 44	0	-133.70	7.95	197.82	42.38	0.32	0.45
			49	-148.76	7.95	230.51	77.17	0.13	0.33
			97	-163.94	7.95	275.73	91.48	-0.01	0.23
123	Fondazio ne	43, 44	0	-152.37	2.80	308.08	174.68	0.00	1.08
			49	-167.67	2.80	392.89	153.59	-0.51	0.99
			97	-183.11	2.80	454.93	77.25	-0.97	0.90
124	Fondazio ne	43, 45	0	-10.03	-121.40	82.70	-283.30	5.74	39.72
			33	-10.06	-121.38	0.72	-213.80	-6.54	34.72
			66	-10.09	-121.36	-58.55	-145.70	-17.18	29.75
125	Fondazio ne	43, 45	0	-15.80	145.79	-16.84	11.57	-17.18	-55.22
			33	-15.84	145.80	-1.93	78.63	1.86	-60.21
			66	-15.88	145.82	34.99	144.90	22.56	-65.23
126	Fondazio ne	44, 46	0	34.73	-94.79	-19.19	139.43	13.63	59.40
			33	34.79	-94.77	14.32	63.83	-5.86	58.75
			66	34.87	-94.75	22.94	-11.48	-25.15	58.12
127	Fondazio ne	44, 46	0	20.57	237.03	44.09	-104.56	-25.15	-88.39
			33	20.65	237.05	-2.87	-179.97	4.12	-89.07
			66	20.75	237.07	-74.77	-255.75	33.64	-89.82
128	Fondazio ne	45, 47	0	-9.96	-177.50	41.11	-168.06	19.99	64.75
			33	-10.01	-177.48	-3.54	-102.81	-0.55	59.73
			66	-10.06	-177.47	-26.87	-38.83	-19.43	54.74
129	Fondazio ne	45, 47	0	-10.34	121.10	-13.71	3.54	-19.43	-54.67
			33	-10.39	121.12	-2.12	66.48	-0.57	-59.66
			66	-10.45	121.14	30.09	128.54	19.95	-64.69
130	Fondazio ne	46, 48	0	15.27	-200.24	-62.39	197.79	30.20	88.48
			33	15.36	-200.22	-9.64	122.18	1.13	87.71
			66	15.47	-200.20	18.29	47.31	-27.69	86.97
131	Fondazio ne	46, 48	0	1.09	177.66	14.49	-4.17	-27.70	-83.39
			33	1.19	177.68	0.83	-78.35	-0.06	-84.13
			66	1.30	177.70	-37.21	-151.98	27.84	-84.92
132	Fondazio ne	47, 49	0	-8.51	-169.63	35.19	-146.35	21.52	65.80
			33	-8.58	-169.62	-2.99	-85.36	0.64	60.77

			66	-8.64	-169.60	-21.26	-25.64	-18.59	55.77
133	Fondazio ne	47, 49	0	-7.69	113.02	-7.40	-12.04	-18.59	-55.90
			33	-7.76	113.03	-1.66	46.57	0.68	-60.89
			66	-7.83	113.05	23.26	104.20	21.61	-65.91
134	Fondazio ne	48, 50	0	13.45	-214.28	-46.18	182.77	29.84	88.88
			33	13.56	-214.26	2.07	109.96	0.65	88.09
			66	13.68	-214.24	26.47	38.26	-28.30	87.34
135	Fondazio ne	48, 50	0	0.27	153.93	14.20	-8.18	-28.30	-89.96
			33	0.39	153.95	-0.23	-78.99	1.51	-90.71
			66	0.50	153.97	-37.91	-149.05	31.58	-91.50
136	Fondazio ne	49, 51	0	-13.87	-173.37	42.06	-159.72	17.88	59.03
			33	-13.94	-173.36	-1.27	-103.26	-0.78	54.02
			66	-14.02	-173.34	-26.21	-48.21	-17.78	49.06
137	Fondazio ne	49, 51	0	-13.81	89.21	-6.67	-28.34	-17.78	-50.16
			33	-13.90	89.22	-7.09	25.48	-0.41	-55.12
			66	-13.99	89.24	10.07	78.24	18.60	-60.10
138	Fondazio ne	50, 52	0	12.34	-217.86	-58.47	201.99	27.39	84.86
			33	12.46	-217.84	-3.26	132.99	-0.48	84.08
			66	12.59	-217.83	29.42	65.46	-28.11	83.36
139	Fondazio ne	50, 52	0	6.00	126.39	8.61	18.78	-28.11	-86.51
			33	6.13	126.41	3.83	-47.44	0.56	-87.22
			66	6.26	126.42	-22.63	-112.51	29.46	-87.97
140	Fondazio ne	51, 53	0	-16.50	-167.02	32.26	-151.28	18.44	57.57
			33	-16.59	-167.00	-9.08	-99.61	0.26	52.60
			66	-16.69	-166.99	-33.57	-49.11	-16.28	47.66
141	Fondazio ne	51, 53	0	-18.14	63.78	-11.02	-28.14	-16.27	-47.71
			33	-18.24	63.79	-12.07	21.49	0.28	-52.64
			66	-18.36	63.80	3.15	70.53	18.47	-57.58
142	Fondazio ne	52, 54	0	10.03	-214.19	-50.15	197.54	27.45	82.42
			33	10.16	-214.18	4.44	133.78	0.37	81.69
			66	10.30	-214.16	38.26	71.60	-26.47	81.01
143	Fondazio ne	52, 54	0	7.47	94.83	9.97	35.30	-26.47	-82.31
			33	7.61	94.84	11.51	-25.60	0.80	-82.97
			66	7.75	94.86	-6.87	-85.50	28.29	-83.65
144	Fondazio ne	53, 55	0	-23.79	-144.66	23.82	-143.21	13.94	47.08
			33	-23.91	-144.65	-15.40	-94.70	-0.79	42.15
			66	-24.04	-144.64	-38.69	-46.68	-13.89	37.25
145	Fondazio ne	53, 55	0	-28.05	38.07	-18.83	-29.49	-13.88	-37.19
			33	-28.19	38.08	-20.62	18.46	-0.81	-42.07
			66	-28.34	38.10	-6.55	66.74	13.88	-46.96
146	Fondazio ne	54, 56	0	10.84	-201.49	-38.14	189.48	25.37	74.60
			33	10.98	-201.47	14.61	130.59	0.86	73.94
			66	11.13	-201.46	48.10	72.74	-23.44	73.35
147	Fondazio ne	54, 56	0	13.23	50.96	16.52	42.14	-23.43	-70.94
			33	13.38	50.97	20.93	-15.12	0.07	-71.50
			66	13.54	50.98	6.49	-72.21	23.76	-72.06
148	Fondazio ne	55, 57	0	-18.27	-81.78	2.70	-111.96	11.08	34.30
			40	-18.46	-81.77	-30.08	-52.99	-1.62	29.59
			80	-18.66	-81.76	-39.17	7.41	-12.43	24.77
149	Fondazio ne	55, 57	0	-14.78	30.48	-42.64	38.45	-12.43	-24.16
			40	-14.99	30.49	-14.92	101.36	-1.84	-29.16
			80	-15.20	30.50	38.47	167.64	10.77	-34.36
150	Fondazio ne	56, 70	0	11.81	-137.10	-18.05	159.83	20.25	47.52
			40	12.01	-137.08	31.76	90.98	1.01	49.24
			80	12.21	-137.07	54.13	21.59	-18.87	50.76

151	Fondazio ne	56, 70	0	13.65	17.66	40.50	-16.25	-18.86	-40.94
			40	13.87	17.68	19.94	-87.43	-2.84	-39.68
			80	14.08	17.69	-29.46	-161.39	12.73	-38.75
152	Fondazio ne	57, 58	0	95.59	-30.04	-63.20	-154.72	2.75	1.68
			42	83.24	-30.04	-112.20	-97.65	1.87	2.57
			83	70.93	-30.04	-142.95	-66.23	0.62	3.45
153	Fondazio ne	57, 58	0	47.78	-29.13	-134.85	-84.61	0.62	1.11
			42	35.50	-29.13	-164.76	-74.33	-0.02	1.98
			83	23.25	-29.13	-193.88	-79.81	-1.03	2.86
154	Fondazio ne	58, 59	0	90.38	4.51	-191.33	141.04	-0.72	-2.25
			35	80.21	4.51	-142.58	128.97	0.03	-2.08
			69	70.06	4.51	-98.64	113.63	0.72	-1.92
155	Fondazio ne	58, 59	0	61.70	1.50	-99.52	94.71	0.72	2.27
			35	51.58	1.50	-67.61	78.57	-0.09	2.43
			69	41.48	1.50	-41.16	63.33	-0.96	2.59
156	Fondazio ne	59, 60	0	42.49	20.75	-53.94	78.95	-0.93	-1.98
			35	32.41	20.75	-27.03	65.76	-0.27	-1.82
			69	22.34	20.75	-4.21	55.41	0.33	-1.67
157	Fondazio ne	59, 60	0	21.94	6.30	-12.46	59.42	0.33	1.68
			35	11.88	6.30	8.72	52.24	-0.28	1.83
			69	1.83	6.30	27.97	48.25	-0.93	1.97
158	Fondazio ne	60, 61	0	2.31	15.48	16.60	40.67	-0.81	-0.94
			35	-7.74	15.48	32.37	39.52	-0.51	-0.81
			69	-17.80	15.48	48.16	40.69	-0.25	-0.69
159	Fondazio ne	60, 61	0	-24.43	-10.55	45.34	70.21	-0.26	0.42
			35	-34.49	-10.55	72.01	72.87	-0.42	0.52
			69	-44.57	-10.55	99.68	75.81	-0.62	0.61
160	Fondazio ne	61, 62	0	25.50	-25.18	106.62	-170.32	-0.69	-1.30
			35	15.42	-25.18	50.20	-168.80	-0.25	-1.23
			69	5.34	-25.18	-6.16	-170.20	0.16	-1.17
161	Fondazio ne	61, 62	0	-8.83	-31.10	14.33	-174.32	0.16	0.48
			35	-18.90	-31.10	-44.52	-179.16	-0.01	0.51
			69	-28.99	-31.10	-105.60	-187.06	-0.19	0.53
162	Fondazio ne	62, 63	0	43.24	4.55	-102.11	99.60	0.15	-0.70
			35	33.16	4.55	-67.36	90.07	0.39	-0.71
			69	23.09	4.55	-35.93	80.57	0.64	-0.73
163	Fondazio ne	62, 63	0	15.27	17.63	-43.07	43.02	0.63	0.96
			35	5.21	17.63	-27.71	34.63	0.31	0.92
			69	-4.85	17.63	-14.95	28.07	0.00	0.86
164	Fondazio ne	63, 64	0	-4.87	25.53	-34.65	59.50	0.23	0.37
			35	-14.93	25.53	-12.92	55.25	0.11	0.31
			69	-24.99	25.53	7.80	53.73	0.02	0.23
165	Fondazio ne	63, 64	0	-26.94	25.35	-7.62	53.74	0.02	0.42
			35	-37.02	25.35	13.08	55.05	-0.11	0.32
			69	-47.11	25.35	34.71	59.07	-0.20	0.22
166	Fondazio ne	64, 65	0	-46.93	17.39	15.10	27.96	0.03	1.03
			35	-57.04	17.39	27.80	34.30	-0.31	0.91
			69	-67.17	17.39	43.02	42.45	-0.60	0.77
167	Fondazio ne	64, 65	0	-74.74	3.82	36.21	80.48	-0.60	-0.54
			35	-84.90	3.82	67.58	89.74	-0.39	-0.69
			69	-95.09	3.82	102.20	99.01	-0.12	-0.86
168	Fondazio ne	65, 66	0	-20.60	-32.36	106.34	-189.79	0.20	0.67
			35	-30.82	-32.35	44.30	-182.16	0.01	0.48
			69	-41.04	-32.35	-15.61	-177.62	-0.12	0.27
169	Fondazio	65, 66	0	-54.51	-26.86	5.58	-173.63	-0.13	-1.05

	ne								
			35	-64.76	-26.86	-51.98	-172.54	0.27	-1.27
			69	-75.03	-26.86	-109.70	-174.35	0.75	-1.52
170	Fondazio ne	66, 67	0	-1.86	-11.53	-101.71	74.54	0.69	0.71
			35	-12.15	-11.53	-74.48	71.37	0.48	0.45
			69	-22.44	-11.53	-48.31	68.60	0.37	0.18
171	Fondazio ne	66, 67	0	-27.41	13.70	-48.47	36.54	0.37	-0.40
			35	-37.71	13.70	-34.06	35.42	0.56	-0.69
			69	-48.03	13.70	-19.62	36.80	0.85	-0.98
172	Fondazio ne	67, 68	0	-43.70	5.09	-30.86	49.47	0.98	1.99
			35	-54.04	5.09	-11.05	53.93	0.34	1.68
			69	-64.39	5.09	10.89	61.87	-0.18	1.38
173	Fondazio ne	67, 68	0	-61.08	21.13	5.01	55.00	-0.18	-1.80
			35	-71.46	21.13	27.93	66.43	0.49	-2.12
			69	-81.87	21.13	55.36	81.00	1.28	-2.43
174	Fondazio ne	68, 69	0	-75.39	1.94	43.94	72.81	1.36	3.15
			35	-85.83	1.94	74.01	89.72	0.33	2.83
			69	-96.30	1.94	110.16	107.72	-0.59	2.52
175	Fondazio ne	68, 69	0	-98.10	7.88	109.61	121.29	-0.59	-3.33
			35	-108.61	7.88	156.58	138.51	0.61	-3.63
			69	-119.16	7.88	209.00	152.22	1.91	-3.93
176	Fondazio ne	69, 70	0	-44.65	-25.23	209.48	-65.35	2.47	3.53
			42	-57.37	-25.23	186.75	-58.67	1.22	2.50
			83	-70.12	-25.23	163.45	-69.24	0.39	1.49
177	Fondazio ne	69, 70	0	-88.27	-21.74	166.18	-63.99	0.40	3.75
			42	-101.07	-21.74	136.01	-98.07	-0.96	2.78
			83	-113.92	-21.74	85.85	-161.02	-1.92	1.84
178	Primo Impalcato	1, 2	0	82.91	2.34	-110.20	36.18	46.00	18.03
			83	82.91	2.34	-80.12	36.18	31.02	18.03
			166	82.91	2.34	-50.05	36.18	16.04	18.03
179	Primo Impalcato	1, 15	0	29.59	5.15	13.20	-17.53	-50.57	-68.16
			80	29.59	5.15	-0.74	-17.53	-6.45	-42.62
			159	29.59	5.15	-14.67	-17.53	16.85	-15.77
180	Primo Impalcato	2, 3	0	34.76	0.63	-62.20	61.53	16.82	8.45
			69	34.76	0.63	-19.74	61.53	10.99	8.45
			138	34.76	0.63	22.71	61.53	5.17	8.45
181	Primo Impalcato	3, 4	0	32.86	-0.15	7.72	-2.66	5.45	2.22
			69	32.86	-0.15	5.88	-2.66	3.92	2.22
			138	32.86	-0.15	4.05	-2.66	2.38	2.22
182	Primo Impalcato	4, 5	0	31.04	-0.63	-10.63	-5.25	2.45	0.40
			69	31.04	-0.63	-14.25	-5.25	2.17	0.40
			138	31.04	-0.63	-17.88	-5.25	1.89	0.40
183	Primo Impalcato	5, 6	0	29.21	-0.97	-33.86	96.28	1.77	0.26
			69	29.21	-0.97	32.57	96.28	1.59	0.26
			138	29.21	-0.97	99.00	96.28	1.41	0.26
184	Primo Impalcato	6, 7	0	-14.18	-1.16	86.38	-125.02	1.31	0.36
			69	-14.18	-1.16	0.11	-125.02	1.06	0.36
			138	-14.18	-1.16	-86.15	-125.02	0.81	0.36
185	Primo Impalcato	7, 8	0	-56.66	-1.23	-98.76	77.77	0.52	0.69
			69	-56.66	-1.23	-45.10	77.77	0.04	0.69
			138	-56.66	-1.23	8.56	77.77	-0.44	0.69
186	Primo Impalcato	8, 9	0	-58.58	-1.16	-8.53	77.70	-0.70	0.56
			69	-58.58	-1.16	45.09	77.70	-1.09	0.56
			138	-58.58	-1.16	98.70	77.70	-1.47	0.56
187	Primo Impalcato	9, 10	0	-100.71	-0.98	86.07	-124.42	-1.81	-0.15

			69	-100.71	-0.98	0.22	-124.42	-1.70	-0.15
			138	-100.71	-0.98	-85.63	-124.42	-1.60	-0.15
188	Primo Impalcato	10, 11	0	-150.74	-0.67	-98.25	96.47	-1.53	-0.22
			69	-150.74	-0.67	-31.68	96.47	-1.38	-0.22
			138	-150.74	-0.67	34.89	96.47	-1.23	-0.22
189	Primo Impalcato	11, 12	0	-152.79	-0.19	19.01	-17.79	-1.14	1.98
			69	-152.79	-0.19	6.73	-17.79	-2.51	1.98
			138	-152.79	-0.19	-5.55	-17.79	-3.88	1.98
190	Primo Impalcato	12, 13	0	-154.89	0.59	-20.66	60.28	-3.50	10.87
			69	-154.89	0.59	20.93	60.28	-11.00	10.87
			138	-154.89	0.59	62.53	60.28	-18.50	10.87
191	Primo Impalcato	13, 14	0	-208.02	2.53	50.41	38.72	-17.35	35.01
			83	-208.02	2.53	82.60	38.72	-46.45	35.01
			166	-208.02	2.53	114.78	38.72	-75.56	35.01
192	Primo Impalcato	14, 16	0	-32.70	5.69	-19.98	23.93	-81.02	-125.07
			80	-32.70	5.69	-0.95	23.93	-1.73	-73.97
			159	-32.70	5.69	18.08	23.93	35.90	-20.26
193	Primo Impalcato	15, 17	0	32.33	4.55	-13.76	10.69	14.64	-14.10
			66	32.33	4.55	-6.70	10.69	17.81	4.51
			132	32.33	4.55	0.35	10.69	8.69	23.12
194	Primo Impalcato	16, 18	0	-29.37	4.74	13.50	-10.69	32.32	-19.84
			66	-29.37	4.74	6.45	-10.69	33.13	17.39
			132	-29.37	4.74	-0.61	-10.69	9.36	54.62
195	Primo Impalcato	17, 19	0	31.39	3.74	-0.82	0.33	7.26	-17.75
			66	31.39	3.74	-0.60	0.33	12.83	0.86
			132	31.39	3.74	-0.38	0.33	6.13	19.47
196	Primo Impalcato	18, 20	0	-27.22	3.73	-0.70	1.71	10.47	-30.13
			66	-27.22	3.73	0.43	1.71	18.07	7.10
			132	-27.22	3.73	1.56	1.71	1.09	44.33
197	Primo Impalcato	19, 21	0	27.11	2.80	-1.93	3.19	5.94	-18.05
			66	27.11	2.80	0.18	3.19	11.71	0.56
			132	27.11	2.80	2.29	3.19	5.20	19.17
198	Primo Impalcato	20, 22	0	-20.25	2.79	0.60	-1.51	1.78	-36.56
			66	-20.25	2.79	-0.40	-1.51	13.62	0.67
			132	-20.25	2.79	-1.40	-1.51	0.89	37.90
199	Primo Impalcato	21, 23	0	27.46	1.92	0.69	0.47	4.25	-16.28
			66	27.46	1.92	1.00	0.47	8.86	2.33
			132	27.46	1.92	1.31	0.47	1.18	20.94
200	Primo Impalcato	22, 24	0	-18.10	1.88	-2.44	1.94	1.04	-36.06
			66	-18.10	1.88	-1.15	1.94	12.56	1.17
			132	-18.10	1.88	0.13	1.94	-0.50	38.40
201	Primo Impalcato	23, 25	0	24.44	1.30	0.00	0.28	1.04	-18.67
			66	24.44	1.30	0.18	0.28	7.22	-0.06
			132	24.44	1.30	0.36	0.28	1.12	18.55
202	Primo Impalcato	24, 26	0	-13.91	1.22	-0.50	1.02	0.08	-34.31
			66	-13.91	1.22	0.17	1.02	10.44	2.91
			132	-13.91	1.22	0.84	1.02	-3.77	40.14
203	Primo Impalcato	25, 28	0	26.36	0.51	-0.93	0.00	-0.24	-30.47
			85	26.36	0.51	-0.93	0.00	12.58	0.31
			170	26.36	0.51	-0.93	0.00	-0.76	31.09
204	Primo Impalcato	26, 27	0	-12.66	0.57	-0.16	-0.51	-4.09	-37.31
			66	-12.66	0.57	-0.50	-0.51	8.24	-0.08
			132	-12.66	0.57	-0.83	-0.51	-3.99	37.15
205	Primo Impalcato	27, 29	0	-10.32	0.21	0.08	-0.59	-3.45	-36.21
			66	-10.32	0.21	-0.31	-0.59	8.17	1.02

			132	-10.32	0.21	-0.69	-0.59	-4.79	38.25
206	Primo Impalcato	28, 30	0	19.24	0.09	0.29	-0.17	-0.03	-19.68
			73	19.24	0.09	0.16	-0.17	6.00	3.16
			146	19.24	0.09	0.03	-0.17	-4.64	25.99
207	Primo Impalcato	29, 31	0	-11.31	-0.04	-1.00	-0.45	-5.44	-36.04
			66	-11.31	-0.04	-1.30	-0.45	6.06	1.19
			132	-11.31	-0.04	-1.60	-0.45	-7.01	38.42
208	Primo Impalcato	30, 32	0	16.48	-0.08	2.57	-2.61	-4.39	-19.93
			69	16.48	-0.08	0.78	-2.61	2.38	0.16
			137	16.48	-0.08	-1.00	-2.61	-4.61	20.24
209	Primo Impalcato	31, 33	0	-11.19	-0.16	-0.45	0.37	-6.27	-36.62
			66	-11.19	-0.16	-0.20	0.37	5.62	0.61
			132	-11.19	-0.16	0.04	0.37	-7.07	37.84
210	Primo Impalcato	32, 34	0	13.45	-0.15	2.27	-2.68	-4.56	-20.58
			69	13.45	-0.15	0.41	-2.68	2.61	-0.20
			138	13.45	-0.15	-1.44	-2.68	-4.29	20.19
211	Primo Impalcato	33, 35	0	-16.62	-0.22	0.86	-2.21	-7.87	-36.90
			66	-16.62	-0.22	-0.60	-2.21	4.19	0.33
			132	-16.62	-0.22	-2.06	-2.21	-8.31	37.56
212	Primo Impalcato	34, 36	0	10.11	-0.21	2.46	-3.25	-4.32	-20.38
			69	10.11	-0.21	0.21	-3.25	2.71	0.00
			138	10.11	-0.21	-2.03	-3.25	-4.32	20.38
213	Primo Impalcato	35, 37	0	-17.75	-0.25	-0.88	0.94	-7.49	-36.88
			66	-17.75	-0.25	-0.26	0.94	4.57	0.34
			132	-17.75	-0.25	0.36	0.94	-7.94	37.57
214	Primo Impalcato	36, 38	0	6.47	-0.25	2.37	-3.57	-4.36	-21.81
			69	6.47	-0.25	-0.10	-3.57	3.66	-1.43
			138	6.47	-0.25	-2.56	-3.57	-2.39	18.96
215	Primo Impalcato	37, 39	0	-25.01	-0.25	1.47	-2.07	-8.83	-36.86
			66	-25.01	-0.25	0.11	-2.07	3.22	0.37
			132	-25.01	-0.25	-1.25	-2.07	-9.31	37.60
216	Primo Impalcato	38, 40	0	2.51	-0.32	2.19	-3.48	-2.28	-23.12
			69	2.51	-0.32	-0.19	-3.48	6.68	-3.04
			137	2.51	-0.32	-2.57	-3.48	1.88	17.05
217	Primo Impalcato	39, 41	0	-23.71	-0.21	-1.67	0.58	-8.48	-38.23
			66	-23.71	-0.21	-1.29	0.58	4.46	-1.00
			132	-23.71	-0.21	-0.91	0.58	-7.16	36.23
218	Primo Impalcato	40, 42	0	-1.83	-0.46	2.52	-1.86	2.55	-8.61
			69	-1.83	-0.46	1.24	-1.86	1.45	11.78
			138	-1.83	-0.46	-0.04	-1.86	-13.70	32.16
219	Primo Impalcato	41, 44	0	-26.97	-0.13	-0.79	3.03	-7.13	-37.91
			66	-26.97	-0.13	1.21	3.03	5.60	-0.68
			132	-26.97	-0.13	3.21	3.03	-6.23	36.55
220	Primo Impalcato	42, 43	0	-6.74	-0.26	6.33	-10.86	-13.29	0.51
			23	-6.74	-0.26	3.83	-10.86	-13.56	1.87
			46	-6.74	-0.26	1.34	-10.86	-14.15	3.23
221	Primo Impalcato	43, 45	0	0.58	-0.38	1.20	0.14	-14.58	-34.41
			66	0.58	-0.38	1.30	0.14	1.99	-15.80
			132	0.58	-0.38	1.39	0.14	6.27	2.81
222	Primo Impalcato	44, 46	0	-29.21	-0.58	1.08	-2.67	-7.31	-40.20
			66	-29.21	-0.58	-0.69	-2.67	6.94	-2.97
			132	-29.21	-0.58	-2.45	-2.67	-3.39	34.26
223	Primo Impalcato	45, 47	0	3.46	-0.88	1.67	-2.74	6.20	-18.56
			66	3.46	-0.88	-0.13	-2.74	12.31	0.05
			132	3.46	-0.88	-1.94	-2.74	6.13	18.66

224	Primo Impalcato	46, 48	0	-31.47	-0.96	-3.34	4.57	-2.36	-39.18
			66	-31.47	-0.96	-0.32	4.57	11.22	-1.95
			132	-31.47	-0.96	2.70	4.57	0.22	35.27
225	Primo Impalcato	47, 49	0	11.02	-1.63	-1.72	2.87	5.86	-18.23
			66	11.02	-1.63	0.17	2.87	11.75	0.38
			132	11.02	-1.63	2.06	2.87	5.36	18.99
226	Primo Impalcato	48, 50	0	-36.33	-1.64	-0.52	-0.27	-1.35	-38.13
			66	-36.33	-1.64	-0.69	-0.27	11.53	-0.90
			132	-36.33	-1.64	-0.87	-0.27	-0.16	36.33
227	Primo Impalcato	49, 51	0	14.60	-2.59	2.24	-3.64	6.30	-18.53
			66	14.60	-2.59	-0.16	-3.64	12.39	0.08
			132	14.60	-2.59	-2.56	-3.64	6.19	18.69
228	Primo Impalcato	50, 52	0	-38.43	-2.57	-4.06	4.83	1.06	-39.08
			66	-38.43	-2.57	-0.87	4.83	14.56	-1.85
			132	-38.43	-2.57	2.32	4.83	3.49	35.38
229	Primo Impalcato	51, 53	0	21.88	-3.57	-2.59	2.32	6.39	-19.58
			66	21.88	-3.57	-1.06	2.32	13.17	-0.97
			132	21.88	-3.57	0.47	2.32	7.67	17.64
230	Primo Impalcato	52, 54	0	-35.94	-3.61	-1.72	2.71	1.58	-44.09
			66	-35.94	-3.61	0.07	2.71	18.39	-6.86
			132	-35.94	-3.61	1.85	2.71	10.63	30.37
231	Primo Impalcato	53, 55	0	25.15	-4.45	-0.13	-10.68	9.09	-23.08
			66	25.15	-4.45	-7.18	-10.68	18.18	-4.47
			132	25.15	-4.45	-14.23	-10.68	14.99	14.14
232	Primo Impalcato	54, 56	0	-34.74	-4.60	-1.50	13.66	10.94	-54.28
			66	-34.74	-4.60	7.51	13.66	34.48	-17.05
			132	-34.74	-4.60	16.53	13.66	33.45	20.18
233	Primo Impalcato	55, 57	0	25.01	-5.09	-17.08	21.83	17.17	15.32
			80	25.01	-5.09	0.28	21.83	-5.77	42.17
			159	25.01	-5.09	17.64	21.83	-49.53	67.71
234	Primo Impalcato	56, 70	0	-34.07	-5.63	14.44	-16.42	32.49	16.05
			80	-34.07	-5.63	1.39	-16.42	-1.79	69.76
			159	-34.07	-5.63	-11.66	-16.42	-77.73	120.86
235	Primo Impalcato	57, 58	0	84.13	-2.38	-111.59	37.64	-44.94	-17.21
			83	84.13	-2.38	-80.31	37.64	-30.64	-17.21
			166	84.13	-2.38	-49.03	37.64	-16.33	-17.21
236	Primo Impalcato	58, 59	0	35.24	-0.63	-61.20	59.92	-17.05	-8.52
			69	35.24	-0.63	-19.85	59.92	-11.17	-8.52
			138	35.24	-0.63	21.49	59.92	-5.30	-8.52
237	Primo Impalcato	59, 60	0	33.32	0.14	6.47	-18.64	-5.57	-2.43
			69	33.32	0.14	-6.39	-18.64	-3.89	-2.43
			138	33.32	0.14	-19.25	-18.64	-2.21	-2.43
238	Primo Impalcato	60, 61	0	31.41	0.64	-35.03	95.74	-2.27	-0.34
			69	31.41	0.64	31.03	95.74	-2.03	-0.34
			138	31.41	0.64	97.09	95.74	-1.80	-0.34
239	Primo Impalcato	61, 62	0	-15.26	0.96	84.49	-122.96	-1.85	-0.01
			69	-15.26	0.96	-0.35	-122.96	-1.84	-0.01
			138	-15.26	0.96	-85.19	-122.96	-1.83	-0.01
240	Primo Impalcato	62, 63	0	-54.82	1.15	-97.83	94.08	-1.52	-0.54
			69	-54.82	1.15	-32.92	94.08	-1.15	-0.54
			138	-54.82	1.15	32.00	94.08	-0.78	-0.54
241	Primo Impalcato	63, 64	0	-56.65	1.18	15.93	-23.06	-0.52	-0.85
			69	-56.65	1.18	0.02	-23.06	0.07	-0.85
			138	-56.65	1.18	-15.89	-23.06	0.66	-0.85
242	Primo	64, 65	0	-58.50	1.14	-31.96	94.14	0.92	-0.50

	Impalcato								
			69	-58.50	1.14	33.00	94.14	1.26	-0.50
			138	-58.50	1.14	97.95	94.14	1.61	-0.50
243	Primo Impalcato	65, 66	0	-100.17	0.95	85.30	-123.20	1.92	0.23
			69	-100.17	0.95	0.29	-123.20	1.77	0.23
			138	-100.17	0.95	-84.72	-123.20	1.61	0.23
244	Primo Impalcato	66, 67	0	-150.22	0.64	-97.34	95.81	1.55	0.34
			69	-150.22	0.64	-31.23	95.81	1.32	0.34
			138	-150.22	0.64	34.88	95.81	1.09	0.34
245	Primo Impalcato	67, 68	0	-152.28	0.17	19.03	-17.81	1.00	-1.73
			69	-152.28	0.17	6.74	-17.81	2.20	-1.73
			138	-152.28	0.17	-5.55	-17.81	3.39	-1.73
246	Primo Impalcato	68, 69	0	-154.40	-0.60	-20.62	60.20	3.00	-10.72
			69	-154.40	-0.60	20.92	60.20	10.40	-10.72
			138	-154.40	-0.60	62.46	60.20	17.79	-10.72
247	Primo Impalcato	69, 70	0	-207.81	-2.39	50.37	38.32	16.56	-36.42
			83	-207.81	-2.39	82.22	38.32	46.83	-36.42
			166	-207.81	-2.39	114.07	38.32	77.11	-36.42
248	Primo Impalcato	1	0	-227.04	-7.31	-2.86	1.50	46.67	21.71
			188	-227.04	-7.31	-0.04	1.50	-16.55	47.69
			376	-227.04	-7.31	2.78	1.50	-140.77	86.62
249	Primo Impalcato	2	0	113.41	-0.21	-4.52	13.55	7.31	3.86
			188	113.41	-0.21	20.95	13.55	0.05	3.86
			376	113.41	-0.21	46.41	13.55	-7.20	3.86
250	Primo Impalcato	3	0	-18.67	0.04	5.56	10.76	8.79	4.65
			188	-18.67	0.04	25.79	10.76	0.06	4.65
			376	-18.67	0.04	46.03	10.76	-8.68	4.65
251	Primo Impalcato	4	0	1.48	0.12	11.96	6.92	8.57	4.59
			188	1.48	0.12	24.97	6.92	-0.06	4.59
			376	1.48	0.12	37.99	6.92	-8.70	4.59
252	Primo Impalcato	5	0	-27.71	0.17	12.07	4.50	9.23	4.83
			188	-27.71	0.17	20.52	4.50	0.14	4.83
			376	-27.71	0.17	28.98	4.50	-8.94	4.83
253	Primo Impalcato	6	0	-166.16	0.21	7.74	2.94	7.33	3.98
			188	-166.16	0.21	13.27	2.94	-0.15	3.98
			376	-166.16	0.21	18.81	2.94	-7.64	3.98
254	Primo Impalcato	7	0	179.52	0.23	3.30	0.28	7.34	3.99
			188	179.52	0.23	3.82	0.28	-0.16	3.99
			376	179.52	0.23	4.35	0.28	-7.67	3.99
255	Primo Impalcato	8	0	-12.30	0.23	-3.42	-0.91	9.85	5.07
			188	-12.30	0.23	-5.13	-0.91	0.31	5.07
			376	-12.30	0.23	-6.84	-0.91	-9.22	5.07
256	Primo Impalcato	9	0	-202.23	0.21	-9.76	-2.05	7.40	4.03
			188	-202.23	0.21	-13.62	-2.05	-0.17	4.03
			376	-202.23	0.21	-17.47	-2.05	-7.74	4.03
257	Primo Impalcato	10	0	157.70	0.17	-12.76	-4.81	7.44	4.05
			188	157.70	0.17	-21.79	-4.81	-0.18	4.05
			376	157.70	0.17	-30.83	-4.81	-7.79	4.05
258	Primo Impalcato	11	0	58.37	0.14	-12.57	-7.59	9.37	4.93
			188	58.37	0.14	-26.84	-7.59	0.10	4.93
			376	58.37	0.14	-41.12	-7.59	-9.17	4.93
259	Primo Impalcato	12	0	30.00	0.08	-3.57	-12.95	9.04	4.79
			188	30.00	0.08	-27.93	-12.95	0.04	4.79
			376	30.00	0.08	-52.28	-12.95	-8.97	4.79
260	Primo Impalcato	13	0	-82.27	-0.17	12.15	-18.84	7.48	3.95

			188	-82.27	-0.17	-23.27	-18.84	0.05	3.95
			376	-82.27	-0.17	-58.70	-18.84	-7.38	3.95
261	Primo Impalcato	14	0	212.25	-9.89	1.49	-0.90	24.18	-8.28
			188	212.25	-9.89	-0.21	-0.90	-5.05	43.69
			376	212.25	-9.89	-1.90	-0.90	-156.31	121.55
262	Primo Impalcato	15	0	-50.85	-3.86	-0.73	0.32	74.60	79.00
			188	-50.85	-3.86	-0.13	0.32	-115.85	127.65
			376	-50.85	-3.86	0.48	0.32	-420.54	200.53
263	Primo Impalcato	16	0	42.62	-4.86	0.46	-0.18	167.87	100.80
			188	42.62	-4.86	0.12	-0.18	-105.49	198.09
			376	42.62	-4.86	-0.21	-0.18	-607.34	343.87
264	Primo Impalcato	17	0	-35.56	-2.86	0.38	-0.19	103.67	140.64
			188	-35.56	-2.86	0.02	-0.19	-199.81	185.97
			376	-35.56	-2.86	-0.35	-0.19	-609.73	253.88
265	Primo Impalcato	18	0	29.32	-3.02	-0.59	0.30	237.40	187.36
			188	29.32	-3.02	-0.03	0.30	-192.98	278.02
			376	29.32	-3.02	0.54	0.30	-836.27	413.86
266	Primo Impalcato	19	0	-32.43	-2.18	0.51	-0.27	100.18	174.96
			188	-32.43	-2.18	0.00	-0.27	-267.82	220.29
			376	-32.43	-2.18	-0.51	-0.27	-742.25	288.20
267	Primo Impalcato	20	0	30.77	-2.13	-0.68	0.35	234.27	221.24
			188	30.77	-2.13	-0.01	0.35	-259.80	311.90
			376	30.77	-2.13	0.65	0.35	-966.79	447.74
268	Primo Impalcato	21	0	-33.55	-1.57	0.43	-0.23	95.15	199.18
			188	-33.55	-1.57	0.00	-0.23	-318.38	244.51
			376	-33.55	-1.57	-0.43	-0.23	-838.35	312.42
269	Primo Impalcato	22	0	36.07	-1.53	-0.56	0.29	224.71	242.87
			188	36.07	-1.53	-0.01	0.29	-310.03	333.53
			376	36.07	-1.53	0.54	0.29	-1057.69	469.38
270	Primo Impalcato	23	0	-36.99	-1.13	0.15	-0.07	99.05	219.91
			188	-36.99	-1.13	0.02	-0.07	-353.44	265.23
			376	-36.99	-1.13	-0.12	-0.07	-912.38	333.14
271	Primo Impalcato	24	0	39.95	-0.99	-0.27	0.13	222.59	260.05
			188	39.95	-0.99	-0.02	0.13	-344.45	350.71
			376	39.95	-0.99	0.23	0.13	-1124.39	486.55
272	Primo Impalcato	25	0	-58.72	-0.81	0.06	-0.02	113.68	239.28
			188	-58.72	-0.81	0.02	-0.02	-379.58	289.65
			376	-58.72	-0.81	-0.02	-0.02	-991.12	365.12
273	Primo Impalcato	26	0	58.06	-0.59	-0.29	0.14	223.43	274.34
			188	58.06	-0.59	-0.02	0.14	-370.47	365.00
			376	58.06	-0.59	0.24	0.14	-1177.28	500.84
274	Primo Impalcato	27	0	47.77	-0.33	-0.25	0.14	221.23	276.01
			188	47.77	-0.33	0.02	0.14	-375.81	366.67
			376	47.77	-0.33	0.29	0.14	-1185.76	502.51
275	Primo Impalcato	28	0	-54.17	-0.13	0.32	-0.17	120.66	245.71
			188	-54.17	-0.13	0.00	-0.17	-386.39	298.04
			376	-54.17	-0.13	-0.32	-0.17	-1016.31	376.44
276	Primo Impalcato	29	0	46.90	-0.07	-0.10	0.05	223.18	278.27
			188	46.90	-0.07	-0.01	0.05	-378.10	368.93
			376	46.90	-0.07	0.08	0.05	-1192.31	504.77
277	Primo Impalcato	30	0	-56.16	0.09	0.23	-0.11	111.78	243.98
			188	-56.16	0.09	0.02	-0.11	-388.27	291.97
			376	-56.16	0.09	-0.20	-0.11	-1001.02	363.88
278	Primo Impalcato	31	0	50.79	0.06	0.15	-0.07	224.38	278.21
			188	50.79	0.06	0.01	-0.07	-376.81	368.88

			376	50.79	0.06	-0.13	-0.07	-1190.91	504.72
279	Primo Impalcato	32	0	-58.41	0.10	0.03	-0.01	105.14	239.82
			188	-58.41	0.10	0.02	-0.01	-386.15	286.72
			376	-58.41	0.10	0.00	-0.01	-987.56	356.97
280	Primo Impalcato	33	0	49.98	0.15	0.22	-0.12	224.41	276.55
			188	49.98	0.15	0.00	-0.12	-373.65	367.21
			376	49.98	0.15	-0.22	-0.12	-1184.63	503.06
281	Primo Impalcato	34	0	-61.47	0.12	-0.09	0.06	105.10	238.17
			188	-61.47	0.12	0.02	0.06	-383.20	285.20
			376	-61.47	0.12	0.13	0.06	-981.96	355.67
282	Primo Impalcato	35	0	54.51	0.16	0.35	-0.18	223.92	274.20
			188	54.51	0.16	0.01	-0.18	-369.72	364.86
			376	54.51	0.16	-0.33	-0.18	-1176.26	500.70
283	Primo Impalcato	36	0	-66.05	0.14	-0.15	0.09	106.83	236.91
			188	-66.05	0.14	0.02	0.09	-379.09	283.94
			376	-66.05	0.14	0.18	0.09	-975.47	354.41
284	Primo Impalcato	37	0	49.38	0.19	0.43	-0.22	224.12	272.03
			188	49.38	0.19	0.01	-0.22	-365.44	362.69
			376	49.38	0.19	-0.40	-0.22	-1167.90	498.53
285	Primo Impalcato	38	0	-66.57	0.23	-0.11	0.07	106.58	234.25
			188	-66.57	0.23	0.01	0.07	-374.24	281.14
			376	-66.57	0.23	0.14	0.07	-965.17	351.40
286	Primo Impalcato	39	0	54.25	0.13	0.47	-0.25	225.83	270.86
			188	54.25	0.13	-0.01	-0.25	-361.54	361.52
			376	54.25	0.13	-0.48	-0.25	-1161.81	497.37
287	Primo Impalcato	40	0	-58.54	0.52	-0.04	0.02	90.29	222.16
			188	-58.54	0.52	0.00	0.02	-367.79	269.06
			376	-58.54	0.52	0.03	0.02	-936.00	339.32
288	Primo Impalcato	41	0	57.05	0.16	0.76	-0.40	229.27	271.46
			188	57.05	0.16	0.00	-0.40	-359.22	362.12
			376	57.05	0.16	-0.75	-0.40	-1160.63	497.97
289	Primo Impalcato	42	0	-37.84	0.46	-0.31	0.16	68.64	216.07
			188	-37.84	0.46	-0.01	0.16	-364.11	246.86
			376	-37.84	0.46	0.28	0.16	-869.18	293.00
290	Primo Impalcato	43	0	-37.45	0.15	-0.64	0.35	69.81	217.90
			188	-37.45	0.15	0.01	0.35	-365.65	247.84
			376	-37.45	0.15	0.66	0.35	-871.43	292.70
291	Primo Impalcato	44	0	60.66	0.25	0.54	-0.29	226.09	271.04
			188	60.66	0.25	0.00	-0.29	-361.61	361.71
			376	60.66	0.25	-0.54	-0.29	-1162.24	497.55
292	Primo Impalcato	45	0	-46.62	0.15	-0.87	0.46	81.18	209.40
			188	-46.62	0.15	-0.01	0.46	-351.56	254.73
			376	-46.62	0.15	0.84	0.46	-890.75	322.64
293	Primo Impalcato	46	0	40.76	0.43	0.66	-0.33	224.00	261.58
			188	40.76	0.43	0.03	-0.33	-345.91	352.24
			376	40.76	0.43	-0.59	-0.33	-1128.74	488.08
294	Primo Impalcato	47	0	-35.92	0.80	-0.87	0.46	97.33	210.10
			188	-35.92	0.80	0.00	0.46	-336.72	255.42
			376	-35.92	0.80	0.86	0.46	-877.21	323.34
295	Primo Impalcato	48	0	30.56	0.88	0.86	-0.46	225.03	252.82
			188	30.56	0.88	-0.01	-0.46	-328.41	343.48
			376	30.56	0.88	-0.88	-0.46	-1094.76	479.32
296	Primo Impalcato	49	0	-42.15	1.42	-0.92	0.49	98.01	195.01
			188	-42.15	1.42	0.00	0.49	-307.68	240.34
			376	-42.15	1.42	0.91	0.49	-819.81	308.25

297	Primo Impalcato	50	0	37.81	1.36	1.04	-0.56	226.56	238.15
			188	37.81	1.36	-0.01	-0.56	-299.31	328.81
			376	37.81	1.36	-1.06	-0.56	-1038.09	464.66
298	Primo Impalcato	51	0	-37.89	2.07	-0.90	0.47	101.20	172.06
			188	-37.89	2.07	-0.01	0.47	-261.34	217.38
			376	-37.89	2.07	0.89	0.47	-730.32	285.30
299	Primo Impalcato	52	0	36.94	2.02	1.26	-0.67	236.59	219.21
			188	36.94	2.02	0.00	-0.67	-253.66	309.87
			376	36.94	2.02	-1.26	-0.67	-956.83	445.71
300	Primo Impalcato	53	0	-41.28	2.78	-0.67	0.34	103.68	139.13
			188	-41.28	2.78	-0.02	0.34	-196.96	184.46
			376	-41.28	2.78	0.62	0.34	-604.04	252.37
301	Primo Impalcato	54	0	31.11	2.93	1.23	-0.64	242.36	187.94
			188	31.11	2.93	0.03	-0.64	-189.11	278.60
			376	31.11	2.93	-1.18	-0.64	-833.50	414.44
302	Primo Impalcato	55	0	-56.45	3.80	0.54	-0.22	74.90	78.58
			188	-56.45	3.80	0.13	-0.22	-114.76	127.22
			376	-56.45	3.80	-0.28	-0.22	-418.65	200.11
303	Primo Impalcato	56	0	42.17	4.85	0.00	-0.07	167.39	99.86
			188	42.17	4.85	-0.14	-0.07	-104.20	197.15
			376	42.17	4.85	-0.28	-0.07	-604.29	342.94
304	Primo Impalcato	57	0	-233.77	7.30	1.97	-1.09	46.51	21.76
			188	-233.77	7.30	-0.08	-1.09	-16.79	47.74
			376	-233.77	7.30	-2.13	-1.09	-141.10	86.66
305	Primo Impalcato	58	0	110.60	0.22	3.02	-13.01	7.31	3.86
			188	110.60	0.22	-21.44	-13.01	0.05	3.86
			376	110.60	0.22	-45.89	-13.01	-7.22	3.86
306	Primo Impalcato	59	0	-8.84	-0.03	-6.14	-10.72	8.82	4.67
			188	-8.84	-0.03	-26.29	-10.72	0.04	4.67
			376	-8.84	-0.03	-46.44	-10.72	-8.73	4.67
307	Primo Impalcato	60	0	-44.46	-0.12	-12.09	-7.18	9.18	4.83
			188	-44.46	-0.12	-25.58	-7.18	0.10	4.83
			376	-44.46	-0.12	-39.08	-7.18	-8.97	4.83
308	Primo Impalcato	61	0	-150.33	-0.17	-11.72	-4.83	7.34	3.99
			188	-150.33	-0.17	-20.80	-4.83	-0.16	3.99
			376	-150.33	-0.17	-29.87	-4.83	-7.67	3.99
309	Primo Impalcato	62	0	192.99	-0.21	-8.98	-2.01	7.35	3.99
			188	192.99	-0.21	-12.76	-2.01	-0.15	3.99
			376	192.99	-0.21	-16.55	-2.01	-7.66	3.99
310	Primo Impalcato	63	0	58.28	-0.23	-3.13	-0.64	9.28	4.86
			188	58.28	-0.23	-4.33	-0.64	0.15	4.86
			376	58.28	-0.23	-5.54	-0.64	-8.98	4.86
311	Primo Impalcato	64	0	-58.51	-0.23	2.94	0.57	9.30	4.87
			188	-58.51	-0.23	4.02	0.57	0.15	4.87
			376	-58.51	-0.23	5.10	0.57	-9.00	4.87
312	Primo Impalcato	65	0	-192.83	-0.20	8.94	1.84	7.41	4.02
			188	-192.83	-0.20	12.41	1.84	-0.15	4.02
			376	-192.83	-0.20	15.87	1.84	-7.72	4.02
313	Primo Impalcato	66	0	151.94	-0.16	11.87	4.55	7.45	4.05
			188	151.94	-0.16	20.41	4.55	-0.17	4.05
			376	151.94	-0.16	28.96	4.55	-7.79	4.05
314	Primo Impalcato	67	0	50.28	-0.13	11.65	7.23	9.36	4.93
			188	50.28	-0.13	25.23	7.23	0.10	4.93
			376	50.28	-0.13	38.82	7.23	-9.17	4.93
315	Primo	68	0	23.73	-0.08	2.33	12.68	9.04	4.79

	Impalcato								
			188	23.73	-0.08	26.16	12.68	0.03	4.79
			376	23.73	-0.08	49.99	12.68	-8.97	4.79
316	Primo Impalcato	69	0	-86.54	0.15	-14.75	19.27	7.48	3.95
			188	-86.54	0.15	21.48	19.27	0.05	3.95
			376	-86.54	0.15	57.70	19.27	-7.38	3.95
317	Primo Impalcato	70	0	227.94	9.86	-1.40	0.71	24.31	-8.19
			188	227.94	9.86	-0.07	0.71	-5.08	43.78
			376	227.94	9.86	1.27	0.71	-156.51	121.64
318	Fondazio ne	1, 71	0	6.71	-0.08	0.00	0.00	-0.82	1.08
			102	6.71	-0.08	0.00	0.00	-1.92	1.08
			204	6.71	-0.08	0.00	0.00	-3.02	1.08
319	Fondazio ne	1, 92	0	-278.04	-0.02	0.00	0.00	-0.78	0.03
			103	-278.04	-0.02	0.00	0.00	-0.82	0.03
			206	-278.04	-0.02	0.00	0.00	-0.85	0.03
320	Primo Impalcato	92, 2	0	284.29	-0.07	0.00	0.00	0.85	1.14
			103	284.29	-0.07	0.00	0.00	-0.33	1.14
			206	284.29	-0.07	0.00	0.00	-1.50	1.14
321	Fondazio ne	6, 89	0	-344.54	0.03	0.00	0.00	-0.48	-0.29
			100	-344.54	0.03	0.00	0.00	-0.19	-0.29
			200	-344.54	0.03	0.00	0.00	0.10	-0.29
322	Primo Impalcato	89, 7	0	347.70	0.01	0.00	0.00	-0.50	-0.20
			100	347.70	0.01	0.00	0.00	-0.30	-0.20
			200	347.70	0.01	0.00	0.00	-0.09	-0.20
323	Fondazio ne	9, 90	0	-358.11	0.00	0.00	0.00	0.41	-0.13
			100	-358.11	0.00	0.00	0.00	0.54	-0.13
			200	-358.11	0.00	0.00	0.00	0.67	-0.13
324	Primo Impalcato	90, 10	0	344.07	0.03	0.00	0.00	0.15	-0.32
			100	344.07	0.03	0.00	0.00	0.46	-0.32
			200	344.07	0.03	0.00	0.00	0.78	-0.32
325	Fondazio ne	13, 91	0	-284.13	-0.09	0.00	0.00	1.98	1.49
			103	-284.13	-0.09	0.00	0.00	0.44	1.49
			206	-284.13	-0.09	0.00	0.00	-1.09	1.49
326	Primo Impalcato	88, 14	0	-3.15	-0.12	0.00	0.00	4.09	1.51
			102	-3.15	-0.12	0.00	0.00	2.55	1.51
			204	-3.15	-0.12	0.00	0.00	1.01	1.51
327	Primo Impalcato	91, 14	0	280.32	-0.03	0.00	0.00	0.92	-0.07
			103	280.32	-0.03	0.00	0.00	0.99	-0.07
			206	280.32	-0.03	0.00	0.00	1.06	-0.07
328	Primo Impalcato	71, 15	0	-38.94	-0.18	0.00	0.00	1.55	2.22
			102	-38.94	-0.18	0.00	0.00	-0.72	2.22
			204	-38.94	-0.18	0.00	0.00	-2.99	2.22
329	Fondazio ne	16, 88	0	32.38	-0.26	0.00	0.00	4.08	3.26
			102	32.38	-0.26	0.00	0.00	0.75	3.26
			204	32.38	-0.26	0.00	0.00	-2.57	3.26
330	Fondazio ne	17, 72	0	-13.16	0.06	0.00	0.00	-5.52	-1.06
			100	-13.16	0.06	0.00	0.00	-4.46	-1.06
			199	-13.16	0.06	0.00	0.00	-3.40	-1.06
331	Primo Impalcato	87, 18	0	14.88	0.09	0.00	0.00	3.46	-1.93
			100	14.88	0.09	0.00	0.00	5.39	-1.93
			199	14.88	0.09	0.00	0.00	7.32	-1.93
332	Primo Impalcato	72, 19	0	2.85	-0.22	0.00	0.00	-1.09	2.72
			100	2.85	-0.22	0.00	0.00	-3.80	2.72
			199	2.85	-0.22	0.00	0.00	-6.51	2.72
333	Fondazio ne	20, 87	0	-5.77	-0.25	0.00	0.00	8.25	3.55

			100	-5.77	-0.25	0.00	0.00	4.71	3.55
			199	-5.77	-0.25	0.00	0.00	1.17	3.55
334	Fondazio ne	21, 73	0	-10.39	0.14	0.00	0.00	-7.54	-1.86
			100	-10.39	0.14	0.00	0.00	-5.68	-1.86
			199	-10.39	0.14	0.00	0.00	-3.83	-1.86
335	Primo Impalcato	86, 22	0	12.36	0.17	0.00	0.00	3.85	-2.70
			100	12.36	0.17	0.00	0.00	6.53	-2.70
			199	12.36	0.17	0.00	0.00	9.22	-2.70
336	Primo Impalcato	73, 23	0	-0.40	-0.23	0.00	0.00	-2.58	2.76
			100	-0.40	-0.23	0.00	0.00	-5.33	2.76
			199	-0.40	-0.23	0.00	0.00	-8.09	2.76
337	Fondazio ne	24, 86	0	-0.51	-0.25	0.00	0.00	9.73	3.53
			100	-0.51	-0.25	0.00	0.00	6.21	3.53
			199	-0.51	-0.25	0.00	0.00	2.69	3.53
338	Fondazio ne	25, 74	0	-12.74	0.24	0.00	0.00	-8.43	-2.34
			103	-12.74	0.24	0.00	0.00	-6.02	-2.34
			206	-12.74	0.24	0.00	0.00	-3.60	-2.34
339	Primo Impalcato	85, 26	0	13.88	0.22	0.00	0.00	3.89	-3.23
			100	13.88	0.22	0.00	0.00	7.11	-3.23
			199	13.88	0.22	0.00	0.00	10.33	-3.23
340	Fondazio ne	27, 85	0	2.89	-0.25	0.00	0.00	10.20	3.34
			100	2.89	-0.25	0.00	0.00	6.87	3.34
			199	2.89	-0.25	0.00	0.00	3.54	3.34
341	Primo Impalcato	74, 28	0	-3.41	-0.27	0.00	0.00	-3.11	2.57
			103	-3.41	-0.27	0.00	0.00	-5.77	2.57
			206	-3.41	-0.27	0.00	0.00	-8.42	2.57
342	Primo Impalcato	84, 29	0	7.27	0.24	0.00	0.00	3.76	-3.31
			100	7.27	0.24	0.00	0.00	7.06	-3.31
			199	7.27	0.24	0.00	0.00	10.35	-3.31
343	Fondazio ne	31, 84	0	8.16	-0.24	0.00	0.00	10.31	3.28
			100	8.16	-0.24	0.00	0.00	7.04	3.28
			199	8.16	-0.24	0.00	0.00	3.77	3.28
344	Primo Impalcato	83, 33	0	3.80	0.24	0.00	0.00	3.65	-3.31
			100	3.80	0.24	0.00	0.00	6.94	-3.31
			199	3.80	0.24	0.00	0.00	10.24	-3.31
345	Fondazio ne	35, 83	0	12.61	-0.23	0.00	0.00	10.18	3.20
			100	12.61	-0.23	0.00	0.00	6.99	3.20
			199	12.61	-0.23	0.00	0.00	3.79	3.20
346	Primo Impalcato	82, 37	0	1.00	0.23	0.00	0.00	3.58	-3.25
			100	1.00	0.23	0.00	0.00	6.82	-3.25
			199	1.00	0.23	0.00	0.00	10.07	-3.25
347	Fondazio ne	39, 82	0	15.11	-0.22	0.00	0.00	10.04	3.17
			100	15.11	-0.22	0.00	0.00	6.88	3.17
			199	15.11	-0.22	0.00	0.00	3.72	3.17
348	Primo Impalcato	78, 43	0	6.44	0.19	0.00	0.00	3.46	-2.21
			100	6.44	0.19	0.00	0.00	5.66	-2.21
			199	6.44	0.19	0.00	0.00	7.86	-2.21
349	Primo Impalcato	81, 44	0	0.04	0.23	0.00	0.00	3.36	-3.40
			100	0.04	0.23	0.00	0.00	6.75	-3.40
			199	0.04	0.23	0.00	0.00	10.14	-3.40
350	Fondazio ne	45, 78	0	-19.93	-0.19	0.00	0.00	7.85	2.24
			100	-19.93	-0.19	0.00	0.00	5.61	2.24
			199	-19.93	-0.19	0.00	0.00	3.38	2.24
351	Fondazio ne	46, 81	0	15.70	-0.22	0.00	0.00	9.69	3.00
			100	15.70	-0.22	0.00	0.00	6.71	3.00

			199	15.70	-0.22	0.00	0.00	3.72	3.00
352	Primo Impalcato	77, 47	0	8.09	0.21	0.00	0.00	2.55	-2.63
			100	8.09	0.21	0.00	0.00	5.18	-2.63
			199	8.09	0.21	0.00	0.00	7.80	-2.63
353	Primo Impalcato	80, 48	0	-10.75	0.24	0.00	0.00	2.65	-3.41
			100	-10.75	0.24	0.00	0.00	6.04	-3.41
			199	-10.75	0.24	0.00	0.00	9.43	-3.41
354	Fondazio ne	49, 77	0	-20.40	-0.14	0.00	0.00	7.39	1.92
			100	-20.40	-0.14	0.00	0.00	5.48	1.92
			199	-20.40	-0.14	0.00	0.00	3.57	1.92
355	Fondazio ne	50, 80	0	21.01	-0.17	0.00	0.00	9.04	2.70
			100	21.01	-0.17	0.00	0.00	6.35	2.70
			199	21.01	-0.17	0.00	0.00	3.66	2.70
356	Primo Impalcato	76, 51	0	6.59	0.21	0.00	0.00	1.09	-2.66
			100	6.59	0.21	0.00	0.00	3.74	-2.66
			199	6.59	0.21	0.00	0.00	6.40	-2.66
357	Fondazio ne	53, 76	0	-18.89	-0.06	0.00	0.00	5.48	1.09
			100	-18.89	-0.06	0.00	0.00	4.39	1.09
			199	-18.89	-0.06	0.00	0.00	3.31	1.09
358	Primo Impalcato	75, 55	0	-36.76	0.18	0.00	0.00	-1.53	-2.21
			102	-36.76	0.18	0.00	0.00	0.73	-2.21
			204	-36.76	0.18	0.00	0.00	2.99	-2.21
359	Fondazio ne	56, 79	0	25.03	0.25	0.00	0.00	-4.05	-3.23
			102	25.03	0.25	0.00	0.00	-0.76	-3.23
			204	25.03	0.25	0.00	0.00	2.54	-3.23
360	Fondazio ne	57, 75	0	2.81	0.08	0.00	0.00	0.83	-1.06
			102	2.81	0.08	0.00	0.00	1.91	-1.06
			204	2.81	0.08	0.00	0.00	2.99	-1.06
361	Fondazio ne	57, 93	0	-279.82	0.02	0.00	0.00	0.75	-0.06
			103	-279.82	0.02	0.00	0.00	0.81	-0.06
			206	-279.82	0.02	0.00	0.00	0.87	-0.06
362	Primo Impalcato	93, 58	0	284.66	0.07	0.00	0.00	-0.85	-1.13
			103	284.66	0.07	0.00	0.00	0.32	-1.13
			206	284.66	0.07	0.00	0.00	1.49	-1.13
363	Fondazio ne	61, 95	0	-341.35	-0.03	0.00	0.00	0.76	0.31
			100	-341.35	-0.03	0.00	0.00	0.44	0.31
			200	-341.35	-0.03	0.00	0.00	0.13	0.31
364	Primo Impalcato	95, 62	0	352.30	0.00	0.00	0.00	0.65	0.13
			100	352.30	0.00	0.00	0.00	0.52	0.13
			200	352.30	0.00	0.00	0.00	0.39	0.13
365	Primo Impalcato	96, 65	0	-357.77	0.00	0.00	0.00	0.63	0.13
			100	-357.77	0.00	0.00	0.00	0.50	0.13
			200	-357.77	0.00	0.00	0.00	0.37	0.13
366	Fondazio ne	66, 96	0	344.70	-0.03	0.00	0.00	0.74	0.31
			100	344.70	-0.03	0.00	0.00	0.43	0.31
			200	344.70	-0.03	0.00	0.00	0.13	0.31
367	Fondazio ne	69, 94	0	-283.80	0.08	0.00	0.00	-1.95	-1.49
			103	-283.80	0.08	0.00	0.00	-0.42	-1.49
			206	-283.80	0.08	0.00	0.00	1.11	-1.49
368	Primo Impalcato	79, 70	0	5.84	0.12	0.00	0.00	-4.04	-1.49
			102	5.84	0.12	0.00	0.00	-2.53	-1.49
			204	5.84	0.12	0.00	0.00	-1.01	-1.49
369	Primo Impalcato	94, 70	0	280.65	0.03	0.00	0.00	-0.88	0.09
			103	280.65	0.03	0.00	0.00	-0.97	0.09
			206	280.65	0.03	0.00	0.00	-1.06	0.09

370	Primo Impalcato	1, 71	0	-38.94	-0.11	0.00	0.00	1.85	0.18
			102	-38.94	-0.11	0.00	0.00	1.67	0.18
			204	-38.94	-0.11	0.00	0.00	1.48	0.18
371	Primo Impalcato	1, 92	0	284.29	-0.21	0.00	0.00	2.51	0.85
			103	284.29	-0.21	0.00	0.00	1.64	0.85
			206	284.29	-0.21	0.00	0.00	0.77	0.85
372	Primo Impalcato	92, 2	0	-278.04	0.01	0.00	0.00	-0.70	-0.26
			103	-278.04	0.01	0.00	0.00	-0.43	-0.26
			206	-278.04	0.01	0.00	0.00	-0.16	-0.26
373	Primo Impalcato	6, 89	0	347.70	0.03	0.00	0.00	-0.61	-0.08
			100	347.70	0.03	0.00	0.00	-0.53	-0.08
			200	347.70	0.03	0.00	0.00	-0.45	-0.08
374	Primo Impalcato	89, 7	0	-344.54	0.04	0.00	0.00	0.05	-0.17
			100	-344.54	0.04	0.00	0.00	0.23	-0.17
			200	-344.54	0.04	0.00	0.00	0.40	-0.17
375	Primo Impalcato	9, 90	0	344.07	0.05	0.00	0.00	-0.20	-0.19
			100	344.07	0.05	0.00	0.00	0.00	-0.19
			200	344.07	0.05	0.00	0.00	0.19	-0.19
376	Primo Impalcato	90, 10	0	-358.11	0.01	0.00	0.00	0.63	-0.01
			100	-358.11	0.01	0.00	0.00	0.64	-0.01
			200	-358.11	0.01	0.00	0.00	0.65	-0.01
377	Primo Impalcato	13, 91	0	280.32	0.03	0.00	0.00	-0.11	-0.39
			103	280.32	0.03	0.00	0.00	0.29	-0.39
			206	280.32	0.03	0.00	0.00	0.69	-0.39
378	Primo Impalcato	88, 14	0	32.38	-0.13	0.00	0.00	-2.57	-0.36
			102	32.38	-0.13	0.00	0.00	-2.20	-0.36
			204	32.38	-0.13	0.00	0.00	-1.83	-0.36
379	Primo Impalcato	91, 14	0	-284.13	-0.29	0.00	0.00	-0.98	1.17
			103	-284.13	-0.29	0.00	0.00	-2.18	1.17
			206	-284.13	-0.29	0.00	0.00	-3.38	1.17
380	Primo Impalcato	71, 15	0	6.71	-0.18	0.00	0.00	-3.02	-0.96
			102	6.71	-0.18	0.00	0.00	-2.04	-0.96
			204	6.71	-0.18	0.00	0.00	-1.06	-0.96
381	Primo Impalcato	16, 88	0	-3.15	-0.21	0.00	0.00	-0.14	-2.12
			102	-3.15	-0.21	0.00	0.00	2.02	-2.12
			204	-3.15	-0.21	0.00	0.00	4.18	-2.12
382	Primo Impalcato	17, 72	0	2.85	-0.19	0.00	0.00	2.96	2.13
			100	2.85	-0.19	0.00	0.00	0.84	2.13
			199	2.85	-0.19	0.00	0.00	-1.28	2.13
383	Primo Impalcato	87, 18	0	-5.77	-0.18	0.00	0.00	1.38	3.01
			100	-5.77	-0.18	0.00	0.00	-1.62	3.01
			199	-5.77	-0.18	0.00	0.00	-4.62	3.01
384	Primo Impalcato	72, 19	0	-13.16	-0.09	0.00	0.00	-3.28	-1.65
			100	-13.16	-0.09	0.00	0.00	-1.63	-1.65
			199	-13.16	-0.09	0.00	0.00	0.02	-1.65
385	Primo Impalcato	20, 87	0	14.88	-0.11	0.00	0.00	-1.58	-2.47
			100	14.88	-0.11	0.00	0.00	0.88	-2.47
			199	14.88	-0.11	0.00	0.00	3.34	-2.47
386	Primo Impalcato	21, 73	0	-0.40	-0.13	0.00	0.00	2.11	2.42
			100	-0.40	-0.13	0.00	0.00	-0.30	2.42
			199	-0.40	-0.13	0.00	0.00	-2.71	2.42
387	Primo Impalcato	86, 22	0	-0.51	-0.10	0.00	0.00	2.84	3.24
			100	-0.51	-0.10	0.00	0.00	-0.39	3.24
			199	-0.51	-0.10	0.00	0.00	-3.62	3.24
388	Primo	73, 23	0	-10.39	-0.02	0.00	0.00	-3.79	-2.21

	Impalcato								
			100	-10.39	-0.02	0.00	0.00	-1.59	-2.21
			199	-10.39	-0.02	0.00	0.00	0.61	-2.21
389	Primo Impalcato	24, 86	0	12.36	-0.03	0.00	0.00	-2.12	-2.99
			100	12.36	-0.03	0.00	0.00	0.85	-2.99
			199	12.36	-0.03	0.00	0.00	3.83	-2.99
390	Primo Impalcato	25, 74	0	-3.41	-0.09	0.00	0.00	1.84	2.44
			103	-3.41	-0.09	0.00	0.00	-0.68	2.44
			206	-3.41	-0.09	0.00	0.00	-3.20	2.44
391	Primo Impalcato	85, 26	0	2.89	-0.05	0.00	0.00	3.62	3.31
			100	2.89	-0.05	0.00	0.00	0.32	3.31
			199	2.89	-0.05	0.00	0.00	-2.98	3.31
392	Primo Impalcato	27, 85	0	13.88	0.01	0.00	0.00	-2.55	-3.26
			100	13.88	0.01	0.00	0.00	0.70	-3.26
			199	13.88	0.01	0.00	0.00	3.95	-3.26
393	Primo Impalcato	74, 28	0	-12.74	0.06	0.00	0.00	-3.67	-2.47
			103	-12.74	0.06	0.00	0.00	-1.13	-2.47
			206	-12.74	0.06	0.00	0.00	1.42	-2.47
394	Primo Impalcato	84, 29	0	8.16	-0.03	0.00	0.00	3.84	3.29
			100	8.16	-0.03	0.00	0.00	0.56	3.29
			199	8.16	-0.03	0.00	0.00	-2.72	3.29
395	Primo Impalcato	31, 84	0	7.27	0.02	0.00	0.00	-2.74	-3.30
			100	7.27	0.02	0.00	0.00	0.55	-3.30
			199	7.27	0.02	0.00	0.00	3.83	-3.30
396	Primo Impalcato	83, 33	0	12.61	-0.01	0.00	0.00	3.86	3.25
			100	12.61	-0.01	0.00	0.00	0.62	3.25
			199	12.61	-0.01	0.00	0.00	-2.61	3.25
397	Primo Impalcato	35, 83	0	3.80	0.03	0.00	0.00	-2.77	-3.26
			100	3.80	0.03	0.00	0.00	0.48	-3.26
			199	3.80	0.03	0.00	0.00	3.73	-3.26
398	Primo Impalcato	82, 37	0	15.11	-0.01	0.00	0.00	3.79	3.20
			100	15.11	-0.01	0.00	0.00	0.60	3.20
			199	15.11	-0.01	0.00	0.00	-2.58	3.20
399	Primo Impalcato	39, 82	0	1.00	0.02	0.00	0.00	-2.78	-3.23
			100	1.00	0.02	0.00	0.00	0.44	-3.23
			199	1.00	0.02	0.00	0.00	3.66	-3.23
400	Primo Impalcato	78, 43	0	-19.93	-0.03	0.00	0.00	3.38	1.99
			100	-19.93	-0.03	0.00	0.00	1.39	1.99
			199	-19.93	-0.03	0.00	0.00	-0.59	1.99
401	Primo Impalcato	81, 44	0	15.70	0.00	0.00	0.00	3.75	3.14
			100	15.70	0.00	0.00	0.00	0.62	3.14
			199	15.70	0.00	0.00	0.00	-2.50	3.14
402	Primo Impalcato	45, 78	0	6.44	0.06	0.00	0.00	-1.32	-2.45
			100	6.44	0.06	0.00	0.00	1.12	-2.45
			199	6.44	0.06	0.00	0.00	3.57	-2.45
403	Primo Impalcato	46, 81	0	0.04	0.05	0.00	0.00	-3.02	-3.26
			100	0.04	0.05	0.00	0.00	0.23	-3.26
			199	0.04	0.05	0.00	0.00	3.47	-3.26
404	Primo Impalcato	77, 47	0	-20.40	0.00	0.00	0.00	3.55	2.18
			100	-20.40	0.00	0.00	0.00	1.38	2.18
			199	-20.40	0.00	0.00	0.00	-0.80	2.18
405	Primo Impalcato	80, 48	0	21.01	0.03	0.00	0.00	3.65	2.95
			100	21.01	0.03	0.00	0.00	0.72	2.95
			199	21.01	0.03	0.00	0.00	-2.22	2.95
406	Primo Impalcato	49, 77	0	8.09	0.12	0.00	0.00	-2.06	-2.37

			100	8.09	0.12	0.00	0.00	0.30	-2.37
			199	8.09	0.12	0.00	0.00	2.66	-2.37
407	Primo Impalcato	50, 80	0	-10.75	0.09	0.00	0.00	-3.52	-3.16
			100	-10.75	0.09	0.00	0.00	-0.37	-3.16
			199	-10.75	0.09	0.00	0.00	2.78	-3.16
408	Primo Impalcato	76, 51	0	-18.89	0.08	0.00	0.00	3.19	1.65
			100	-18.89	0.08	0.00	0.00	1.55	1.65
			199	-18.89	0.08	0.00	0.00	-0.10	1.65
409	Primo Impalcato	53, 76	0	6.59	0.18	0.00	0.00	-2.90	-2.10
			100	6.59	0.18	0.00	0.00	-0.82	-2.10
			199	6.59	0.18	0.00	0.00	1.27	-2.10
410	Primo Impalcato	75, 55	0	2.81	0.17	0.00	0.00	3.00	0.97
			102	2.81	0.17	0.00	0.00	2.01	0.97
			204	2.81	0.17	0.00	0.00	1.02	0.97
411	Primo Impalcato	56, 79	0	5.84	0.21	0.00	0.00	0.11	2.07
			102	5.84	0.21	0.00	0.00	-2.01	2.07
			204	5.84	0.21	0.00	0.00	-4.12	2.07
412	Primo Impalcato	57, 75	0	-36.76	0.11	0.00	0.00	-1.85	-0.19
			102	-36.76	0.11	0.00	0.00	-1.66	-0.19
			204	-36.76	0.11	0.00	0.00	-1.47	-0.19
413	Primo Impalcato	57, 93	0	284.66	0.20	0.00	0.00	-2.47	-0.83
			103	284.66	0.20	0.00	0.00	-1.62	-0.83
			206	284.66	0.20	0.00	0.00	-0.77	-0.83
414	Primo Impalcato	93, 58	0	-279.82	-0.01	0.00	0.00	0.72	0.25
			103	-279.82	-0.01	0.00	0.00	0.46	0.25
			206	-279.82	-0.01	0.00	0.00	0.21	0.25
415	Primo Impalcato	61, 95	0	352.30	-0.01	0.00	0.00	0.61	0.00
			100	352.30	-0.01	0.00	0.00	0.61	0.00
			200	352.30	-0.01	0.00	0.00	0.61	0.00
416	Primo Impalcato	95, 62	0	-341.35	-0.05	0.00	0.00	0.17	0.19
			100	-341.35	-0.05	0.00	0.00	-0.02	0.19
			200	-341.35	-0.05	0.00	0.00	-0.21	0.19
417	Primo Impalcato	96, 65	0	344.70	-0.05	0.00	0.00	0.17	0.19
			100	344.70	-0.05	0.00	0.00	-0.02	0.19
			200	344.70	-0.05	0.00	0.00	-0.21	0.19
418	Primo Impalcato	66, 96	0	-357.77	-0.01	0.00	0.00	0.62	0.01
			100	-357.77	-0.01	0.00	0.00	0.60	0.01
			200	-357.77	-0.01	0.00	0.00	0.59	0.01
419	Primo Impalcato	69, 94	0	280.65	-0.03	0.00	0.00	0.21	0.42
			103	280.65	-0.03	0.00	0.00	-0.22	0.42
			206	280.65	-0.03	0.00	0.00	-0.65	0.42
420	Primo Impalcato	79, 70	0	25.03	0.13	0.00	0.00	2.53	0.33
			102	25.03	0.13	0.00	0.00	2.20	0.33
			204	25.03	0.13	0.00	0.00	1.86	0.33
421	Primo Impalcato	94, 70	0	-283.80	0.29	0.00	0.00	0.99	-1.15
			103	-283.80	0.29	0.00	0.00	2.18	-1.15
			206	-283.80	0.29	0.00	0.00	3.36	-1.15
422	Copertura	1, 2	0	223.50	8.01	-78.76	-372.96	368.35	59.57
			83	223.50	8.01	-388.77	-372.96	318.83	59.57
			166	223.50	8.01	-698.79	-372.96	269.31	59.57
423	Copertura	15, 1	0	43.24	5.80	-35.26	29.58	-81.53	-278.33
			80	43.24	5.80	-11.74	29.58	142.87	-286.21
			159	43.24	5.80	11.78	29.58	373.52	-294.01
424	Copertura	2, 3	0	142.99	19.78	-702.35	129.36	269.05	45.37
			69	142.99	19.78	-613.09	129.36	237.75	45.37
			138	142.99	19.78	-523.83	129.36	206.44	45.37
425	Copertura	3, 4	0	140.24	6.14	-529.73	212.22	206.19	40.83
			69	140.24	6.14	-383.30	212.22	178.02	40.83

			138	140.24	6.14	-236.87	212.22	149.85	40.83
426	Copertura	4, 5	0	137.47	-3.87	-242.96	213.33	149.91	35.73
			69	137.47	-3.87	-95.76	213.33	125.26	35.73
			138	137.47	-3.87	51.43	213.33	100.61	35.73
427	Copertura	5, 6	0	134.47	-10.60	44.96	139.51	100.91	31.37
			69	134.47	-10.60	141.22	139.51	79.26	31.37
			138	134.47	-10.60	237.49	139.51	57.61	31.37
428	Copertura	6, 7	0	54.23	-14.20	231.84	-295.72	58.18	28.44
			69	54.23	-14.20	27.79	-295.72	38.56	28.44
			138	54.23	-14.20	-176.25	-295.72	18.93	28.44
429	Copertura	7, 8	0	-26.14	-15.61	-181.87	141.69	19.66	27.62
			69	-26.14	-15.61	-84.11	141.69	0.60	27.62
			138	-26.14	-15.61	13.66	141.69	-18.46	27.62
430	Copertura	8, 9	0	-29.30	-14.49	7.01	154.06	-17.95	28.67
			69	-29.30	-14.49	113.31	154.06	-37.74	28.67
			138	-29.30	-14.49	219.62	154.06	-57.52	28.67
431	Copertura	9, 10	0	-106.74	-10.55	214.05	-252.33	-56.84	31.62
			69	-106.74	-10.55	39.95	-252.33	-78.66	31.62
			138	-106.74	-10.55	-134.16	-252.33	-100.48	31.62
432	Copertura	10, 11	0	-187.15	-3.53	-139.66	193.00	-100.16	36.49
			69	-187.15	-3.53	-6.49	193.00	-125.33	36.49
			138	-187.15	-3.53	126.68	193.00	-150.51	36.49
433	Copertura	11, 12	0	-190.03	7.12	120.52	248.90	-150.46	41.88
			69	-190.03	7.12	292.26	248.90	-179.35	41.88
			138	-190.03	7.12	464.00	248.90	-208.25	41.88
434	Copertura	12, 13	0	-192.72	20.69	458.25	140.82	-208.54	45.95
			69	-192.72	20.69	555.42	140.82	-240.25	45.95
			138	-192.72	20.69	652.59	140.82	-271.95	45.95
435	Copertura	13, 14	0	-269.57	7.74	649.12	-376.78	-272.31	60.15
			83	-269.57	7.74	335.93	-376.78	-322.31	60.15
			166	-269.57	7.74	22.74	-376.78	-372.31	60.15
436	Copertura	16, 14	0	-44.69	-10.14	13.14	-17.37	-80.25	-267.13
			80	-44.69	-10.14	-0.67	-17.37	138.39	-282.89
			159	-44.69	-10.14	-14.47	-17.37	369.50	-298.50
437	Copertura	15, 17	0	53.32	7.79	-34.97	-16.11	-12.04	-176.44
			66	53.32	7.79	-45.60	-16.11	102.71	-171.29
			132	53.32	7.79	-56.23	-16.11	214.06	-166.13
438	Copertura	16, 18	0	-57.72	2.36	8.49	16.08	-8.78	-178.31
			66	-57.72	2.36	19.10	16.08	105.51	-168.00
			132	-57.72	2.36	29.71	16.08	212.99	-157.70
439	Copertura	17, 19	0	61.89	6.59	-56.71	10.71	130.39	-84.33
			66	61.89	6.59	-49.64	10.71	184.35	-79.18
			132	61.89	6.59	-42.57	10.71	234.91	-74.03
440	Copertura	18, 20	0	-68.65	6.51	26.42	-4.16	130.40	-87.30
			66	-68.65	6.51	23.67	-4.16	184.62	-77.00
			132	-68.65	6.51	20.93	-4.16	232.04	-66.70
441	Copertura	19, 21	0	68.38	4.82	-43.36	19.35	169.70	-30.78
			66	68.38	4.82	-30.59	19.35	188.31	-25.63
			132	68.38	4.82	-17.82	19.35	203.53	-20.48
442	Copertura	20, 22	0	-77.61	5.00	17.74	-11.45	169.32	-36.15
			66	-77.61	5.00	10.18	-11.45	189.78	-25.85
			132	-77.61	5.00	2.62	-11.45	203.44	-15.55
443	Copertura	21, 23	0	72.75	2.80	-18.87	10.08	157.42	-5.93
			66	72.75	2.80	-12.22	10.08	159.64	-0.78
			132	72.75	2.80	-5.57	10.08	158.46	4.37
444	Copertura	22, 24	0	-84.50	3.76	-0.16	-5.61	157.41	-9.27
			66	-84.50	3.76	-3.86	-5.61	160.14	1.03
			132	-84.50	3.76	-7.57	-5.61	156.06	11.33
445	Copertura	23, 25	0	75.42	0.33	-6.69	2.77	128.48	-5.70
			66	75.42	0.33	-4.86	2.77	130.54	-0.55
			132	75.42	0.33	-3.03	2.77	129.21	4.60
446	Copertura	24, 26	0	-89.38	2.60	-10.18	-0.48	127.47	5.28
			66	-89.38	2.60	-10.50	-0.48	120.59	15.58
			132	-89.38	2.60	-10.81	-0.48	106.90	25.89
447	Copertura	25, 28	0	76.71	0.20	-4.28	6.90	112.18	26.19
			85	76.71	0.20	1.58	6.90	85.91	35.62
			170	76.71	0.20	7.45	6.90	51.63	45.04
448	Copertura	26, 27	0	-95.07	1.54	-15.26	-3.24	89.09	-16.54
			66	-95.07	1.54	-17.40	-3.24	96.61	-6.24
			132	-95.07	1.54	-19.53	-3.24	97.33	4.06
449	Copertura	27, 29	0	-93.00	-0.26	-23.57	-0.97	90.47	24.14
			66	-93.00	-0.26	-24.21	-0.97	71.14	34.44

			132	-93.00	-0.26	-24.85	-0.97	45.01	44.74
450	Copertura	28, 30	0	78.90	1.52	0.57	12.75	44.89	-2.02
			73	78.90	1.52	9.87	12.75	43.96	4.57
			146	78.90	1.52	19.18	12.75	38.22	11.16
451	Copertura	29, 31	0	-90.04	-0.42	-32.38	3.37	43.66	8.60
			66	-90.04	-0.42	-30.15	3.37	34.58	18.91
			132	-90.04	-0.42	-27.93	3.37	18.70	29.21
452	Copertura	30, 32	0	79.77	0.65	9.96	9.60	36.99	7.23
			69	79.77	0.65	16.54	9.60	30.11	12.88
			137	79.77	0.65	23.12	9.60	19.35	18.52
453	Copertura	31, 33	0	-85.75	-0.26	-35.41	10.65	20.90	0.13
			66	-85.75	-0.26	-28.38	10.65	17.41	10.43
			132	-85.75	-0.26	-21.35	10.65	7.12	20.74
454	Copertura	32, 34	0	80.69	-0.22	13.15	6.14	21.40	4.52
			69	80.69	-0.22	17.38	6.14	16.30	10.27
			138	80.69	-0.22	21.62	6.14	7.23	16.02
455	Copertura	33, 35	0	-81.56	-0.33	-29.98	8.61	10.66	-3.82
			66	-81.56	-0.33	-24.29	8.61	9.78	6.48
			132	-81.56	-0.33	-18.61	8.61	2.10	16.78
456	Copertura	34, 36	0	81.71	-0.45	10.89	6.94	10.97	0.51
			69	81.71	-0.45	15.68	6.94	8.63	6.26
			138	81.71	-0.45	20.47	6.94	2.33	12.01
457	Copertura	35, 37	0	-76.57	-0.47	-27.46	11.88	6.58	-5.75
			66	-76.57	-0.47	-19.63	11.88	6.98	4.55
			132	-76.57	-0.47	-11.79	11.88	0.57	14.85
458	Copertura	36, 38	0	82.78	-0.30	9.08	13.16	6.92	-0.27
			69	82.78	-0.30	18.16	13.16	5.12	5.48
			138	82.78	-0.30	27.24	13.16	-0.64	11.22
459	Copertura	37, 39	0	-71.30	-1.16	-21.15	5.83	5.58	-2.69
			66	-71.30	-1.16	-17.30	5.83	3.95	7.62
			132	-71.30	-1.16	-13.45	5.83	-4.48	17.92
460	Copertura	38, 40	0	84.03	0.91	15.14	20.54	4.39	-1.93
			69	84.03	0.91	29.21	20.54	3.78	3.72
			137	84.03	0.91	43.29	20.54	-0.70	9.36
461	Copertura	39, 41	0	-66.25	-1.85	-23.03	10.10	0.89	16.99
			66	-66.25	-1.85	-16.36	10.10	-13.72	27.29
			132	-66.25	-1.85	-9.70	10.10	-35.13	37.59
462	Copertura	40, 42	0	86.01	3.12	30.35	18.70	4.38	-21.83
			69	86.01	3.12	43.25	18.70	17.46	-16.08
			138	86.01	3.12	56.16	18.70	26.57	-10.33
463	Copertura	41, 44	0	-51.49	-0.21	-16.09	6.90	-30.23	-76.32
			66	-51.49	-0.21	-11.54	6.90	16.74	-66.01
			132	-51.49	-0.21	-6.99	6.90	56.90	-55.71
464	Copertura	42, 43	0	83.27	-0.66	41.79	5.00	32.50	41.78
			23	83.27	-0.66	42.94	5.00	22.86	42.00
			46	83.27	-0.66	44.09	5.00	13.18	42.22
465	Copertura	43, 45	0	82.20	-3.97	43.28	-10.12	20.38	-50.98
			66	82.20	-3.97	36.60	-10.12	52.33	-45.83
			132	82.20	-3.97	29.92	-10.12	80.87	-40.68
466	Copertura	44, 46	0	-57.33	0.25	-14.24	0.03	63.21	-24.83
			66	-57.33	0.25	-14.22	0.03	76.19	-14.53
			132	-57.33	0.25	-14.20	0.03	82.38	-4.22
467	Copertura	45, 47	0	80.53	-2.84	29.27	-22.44	94.28	-33.41
			66	80.53	-2.84	14.46	-22.44	114.63	-28.26
			132	80.53	-2.84	-0.35	-22.44	131.58	-23.11
468	Copertura	46, 48	0	-58.44	-1.24	-17.47	4.15	94.62	-35.84
			66	-58.44	-1.24	-14.73	4.15	114.87	-25.53
			132	-58.44	-1.24	-11.99	4.15	128.32	-15.23
469	Copertura	47, 49	0	77.61	-2.97	-1.08	-23.55	156.21	-15.15
			66	77.61	-2.97	-16.62	-23.55	164.51	-10.00
			132	77.61	-2.97	-32.17	-23.55	169.41	-4.85
470	Copertura	48, 50	0	-58.56	-2.78	-15.44	11.28	153.04	-22.27
			66	-58.56	-2.78	-7.99	11.28	164.33	-11.97
			132	-58.56	-2.78	-0.54	11.28	168.83	-1.66
471	Copertura	49, 51	0	72.88	-4.25	-33.09	-25.92	210.60	15.25
			66	72.88	-4.25	-50.19	-25.92	198.83	20.40
			132	72.88	-4.25	-67.30	-25.92	183.67	25.55
472	Copertura	50, 52	0	-56.71	-5.01	-3.50	19.83	208.08	8.75
			66	-56.71	-5.01	9.58	19.83	198.91	19.05
			132	-56.71	-5.01	22.67	19.83	182.93	29.36
473	Copertura	51, 53	0	65.93	-6.41	-68.48	-7.72	244.83	72.62
			66	65.93	-6.41	-73.58	-7.72	195.20	77.77

			132	65.93	-6.41	-78.67	-7.72	142.17	82.92
474	Copertura	52, 54	0	-52.55	-5.75	19.86	18.37	243.91	66.71
			66	-52.55	-5.75	31.99	18.37	196.48	77.01
			132	-52.55	-5.75	44.11	18.37	142.25	87.32
475	Copertura	53, 55	0	56.70	-7.46	-80.32	24.50	223.08	165.33
			66	56.70	-7.46	-64.15	24.50	112.27	170.48
			132	56.70	-7.46	-47.98	24.50	-1.95	175.63
476	Copertura	54, 56	0	-45.31	-2.74	42.65	-8.75	219.94	155.85
			66	-45.31	-2.74	36.88	-8.75	113.68	166.15
			132	-45.31	-2.74	31.10	-8.75	0.62	176.45
477	Copertura	55, 57	0	45.86	-5.92	-50.41	43.48	89.66	281.73
			80	45.86	-5.92	-15.85	43.48	-137.45	289.61
			159	45.86	-5.92	18.72	43.48	-370.80	297.42
478	Copertura	56, 70	0	-37.41	10.75	29.52	-20.45	89.59	269.26
			80	-37.41	10.75	13.26	-20.45	-130.74	285.02
			159	-37.41	10.75	-3.00	-20.45	-363.55	300.63
479	Copertura	57, 58	0	225.96	-9.33	-81.32	-354.34	-365.69	-59.85
			83	225.96	-9.33	-375.86	-354.34	-315.94	-59.85
			166	225.96	-9.33	-670.39	-354.34	-266.20	-59.85
480	Copertura	58, 59	0	144.54	-19.35	-673.94	157.99	-265.95	-45.21
			69	144.54	-19.35	-564.93	157.99	-234.76	-45.21
			138	144.54	-19.35	-455.92	157.99	-203.56	-45.21
481	Copertura	59, 60	0	141.79	-5.88	-461.80	245.39	-203.32	-40.58
			69	141.79	-5.88	-292.48	245.39	-175.32	-40.58
			138	141.79	-5.88	-123.17	245.39	-147.32	-40.58
482	Copertura	60, 61	0	138.87	3.90	-129.42	175.47	-147.39	-35.49
			69	138.87	3.90	-8.35	175.47	-122.90	-35.49
			138	138.87	3.90	112.73	175.47	-98.41	-35.49
483	Copertura	61, 62	0	56.86	10.38	107.14	-282.95	-98.73	-30.99
			69	56.86	10.38	-88.10	-282.95	-77.35	-30.99
			138	56.86	10.38	-283.34	-282.95	-55.96	-30.99
484	Copertura	62, 63	0	-21.87	14.08	-289.00	124.18	-56.62	-28.27
			69	-21.87	14.08	-203.31	124.18	-37.11	-28.27
			138	-21.87	14.08	-117.63	124.18	-17.61	-28.27
485	Copertura	63, 64	0	-24.90	15.15	-124.15	183.04	-18.10	-27.31
			69	-24.90	15.15	2.14	183.04	0.75	-27.31
			138	-24.90	15.15	128.44	183.04	19.59	-27.31
486	Copertura	64, 65	0	-27.91	14.04	121.94	124.35	19.10	-28.24
			69	-27.91	14.04	207.74	124.35	38.59	-28.24
			138	-27.91	14.04	293.54	124.35	58.07	-28.24
487	Copertura	65, 66	0	-105.23	10.17	287.94	-278.52	57.41	-30.99
			69	-105.23	10.17	95.76	-278.52	78.80	-30.99
			138	-105.23	10.17	-96.42	-278.52	100.18	-30.99
488	Copertura	66, 67	0	-186.31	3.20	-101.92	175.84	99.87	-35.64
			69	-186.31	3.20	19.41	175.84	124.46	-35.64
			138	-186.31	3.20	140.73	175.84	149.05	-35.64
489	Copertura	67, 68	0	-189.18	-7.37	134.61	239.17	149.01	-40.79
			69	-189.18	-7.37	299.64	239.17	177.16	-40.79
			138	-189.18	-7.37	464.67	239.17	205.30	-40.79
490	Copertura	68, 69	0	-191.85	-20.53	458.97	137.43	205.61	-44.49
			69	-191.85	-20.53	553.79	137.43	236.30	-44.49
			138	-191.85	-20.53	648.62	137.43	267.00	-44.49
491	Copertura	69, 70	0	-268.23	-5.51	645.07	-373.76	267.38	-57.52
			83	-268.23	-5.51	334.39	-373.76	315.20	-57.52
			166	-268.23	-5.51	23.72	-373.76	363.01	-57.52
492	Copertura	1	0	230.70	-4.67	1.28	-0.42	72.37	2.79
			220	230.70	-4.67	0.36	-0.42	45.68	25.35
			440	230.70	-4.67	-0.55	-0.42	-56.29	71.24
493	Copertura	2	0	-287.38	-0.56	-25.33	5.96	4.98	2.29
			220	-287.38	-0.56	-12.22	5.96	-0.06	2.29
			440	-287.38	-0.56	0.88	5.96	-5.10	2.29
494	Copertura	3	0	-82.86	-0.25	-13.64	4.54	5.90	2.75
			220	-82.86	-0.25	-3.66	4.54	-0.15	2.75
			440	-82.86	-0.25	6.33	4.54	-6.20	2.75
495	Copertura	4	0	-1.11	0.06	-10.00	5.10	6.08	2.77
			220	-1.11	0.06	1.22	5.10	-0.01	2.77
			440	-1.11	0.06	12.44	5.10	-6.10	2.77
496	Copertura	5	0	73.81	0.30	-6.74	4.35	6.47	3.01
			220	73.81	0.30	2.84	4.35	-0.14	3.01
			440	73.81	0.30	12.42	4.35	-6.76	3.01
497	Copertura	6	0	187.33	0.44	-3.85	2.83	5.65	2.49
			220	187.33	0.44	2.38	2.83	0.18	2.49

			440	187.33	0.44	8.61	2.83	-5.29	2.49
498	Copertura	7	0	-189.02	0.50	-0.92	0.79	5.62	2.47
			220	-189.02	0.50	0.83	0.79	0.18	2.47
			440	-189.02	0.50	2.58	0.79	-5.27	2.47
499	Copertura	8	0	-12.38	0.50	1.12	-1.05	6.65	3.16
			220	-12.38	0.50	-1.18	-1.05	-0.30	3.16
			440	-12.38	0.50	-3.48	-1.05	-7.24	3.16
500	Copertura	9	0	167.30	0.44	3.43	-2.87	5.56	2.45
			220	167.30	0.44	-2.89	-2.87	0.17	2.45
			440	167.30	0.44	-9.22	-2.87	-5.22	2.45
501	Copertura	10	0	-196.68	0.30	7.02	-4.69	5.50	2.43
			220	-196.68	0.30	-3.29	-4.69	0.16	2.43
			440	-196.68	0.30	-13.60	-4.69	-5.17	2.43
502	Copertura	11	0	-55.89	0.05	10.66	-5.39	6.16	2.88
			220	-55.89	0.05	-1.20	-5.39	-0.18	2.88
			440	-55.89	0.05	-13.05	-5.39	-6.51	2.88
503	Copertura	12	0	108.08	-0.29	13.57	-4.07	5.74	2.69
			220	108.08	-0.29	4.61	-4.07	-0.16	2.69
			440	108.08	-0.29	-4.35	-4.07	-6.07	2.69
504	Copertura	13	0	312.21	-0.61	21.65	-3.46	4.81	2.21
			220	312.21	-0.61	14.04	-3.46	-0.05	2.21
			440	312.21	-0.61	6.43	-3.46	-4.91	2.21
505	Copertura	57	0	225.90	4.55	4.02	-1.95	74.72	3.69
			220	225.90	4.55	-0.27	-1.95	46.06	26.25
			440	225.90	4.55	-4.55	-1.95	-57.90	72.14
506	Copertura	58	0	-294.96	0.54	25.56	-6.35	5.00	2.30
			220	-294.96	0.54	11.60	-6.35	-0.06	2.30
			440	-294.96	0.54	-2.36	-6.35	-5.11	2.30
507	Copertura	59	0	-87.40	0.24	13.47	-4.63	5.88	2.75
			220	-87.40	0.24	3.28	-4.63	-0.16	2.75
			440	-87.40	0.24	-6.91	-4.63	-6.20	2.75
508	Copertura	60	0	69.92	-0.07	9.79	-5.08	6.26	2.92
			220	69.92	-0.07	-1.40	-5.08	-0.17	2.92
			440	69.92	-0.07	-12.58	-5.08	-6.60	2.92
509	Copertura	61	0	204.78	-0.30	6.48	-4.33	5.59	2.47
			220	204.78	-0.30	-3.04	-4.33	0.17	2.47
			440	204.78	-0.30	-12.57	-4.33	-5.26	2.47
510	Copertura	62	0	-164.06	-0.43	3.21	-2.65	5.66	2.49
			220	-164.06	-0.43	-2.62	-2.65	0.18	2.49
			440	-164.06	-0.43	-8.45	-2.65	-5.30	2.49
511	Copertura	63	0	-58.86	-0.49	1.06	-0.96	6.52	3.03
			220	-58.86	-0.49	-1.05	-0.96	-0.14	3.03
			440	-58.86	-0.49	-3.17	-0.96	-6.79	3.03
512	Copertura	64	0	58.69	-0.49	-1.11	0.93	6.50	3.02
			220	58.69	-0.49	0.94	0.93	-0.14	3.02
			440	58.69	-0.49	2.98	0.93	-6.77	3.02
513	Copertura	65	0	164.22	-0.43	-3.38	2.68	5.61	2.47
			220	164.22	-0.43	2.52	2.68	0.18	2.47
			440	164.22	-0.43	8.42	2.68	-5.24	2.47
514	Copertura	66	0	-203.57	-0.29	-6.96	4.47	5.50	2.42
			220	-203.57	-0.29	2.87	4.47	0.16	2.42
			440	-203.57	-0.29	12.69	4.47	-5.17	2.42
515	Copertura	67	0	-63.34	-0.04	-10.57	5.16	6.13	2.87
			220	-63.34	-0.04	0.77	5.16	-0.18	2.87
			440	-63.34	-0.04	12.12	5.16	-6.48	2.87
516	Copertura	68	0	101.74	0.30	-13.16	3.69	5.70	2.67
			220	101.74	0.30	-5.03	3.69	-0.16	2.67
			440	101.74	0.30	3.09	3.69	-6.03	2.67
517	Copertura	69	0	307.36	0.62	-19.38	2.31	4.77	2.19
			220	307.36	0.62	-14.30	2.31	-0.05	2.19
			440	307.36	0.62	-9.22	2.31	-4.87	2.19
518	Primo Impalcato	1, 74	0	-229.77	0.03	0.00	0.00	-0.38	-0.03
			118	-229.77	0.03	0.00	0.00	-0.35	-0.03
			235	-229.77	0.03	0.00	0.00	-0.32	-0.03
519	Copertura	74, 2	0	183.70	-0.17	0.00	0.00	1.45	0.21
			118	183.70	-0.17	0.00	0.00	1.20	0.21
			235	183.70	-0.17	0.00	0.00	0.96	0.21
520	Primo Impalcato	6, 71	0	-260.31	0.07	0.00	0.00	0.16	-0.14
			115	-260.31	0.07	0.00	0.00	0.32	-0.14
			231	-260.31	0.07	0.00	0.00	0.47	-0.14

521	Copertura	71, 7	0	259.80	0.05	0.00	0.00	-0.51	-0.02
			115	259.80	0.05	0.00	0.00	-0.49	-0.02
			231	259.80	0.05	0.00	0.00	-0.47	-0.02
522	Primo Impalcato	9, 72	0	-260.59	0.04	0.00	0.00	0.60	0.08
			115	-260.59	0.04	0.00	0.00	0.51	0.08
			231	-260.59	0.04	0.00	0.00	0.42	0.08
523	Copertura	72, 10	0	250.58	0.06	0.00	0.00	-0.36	-0.18
			115	250.58	0.06	0.00	0.00	-0.15	-0.18
			231	250.58	0.06	0.00	0.00	0.06	-0.18
524	Copertura	73, 13	0	-170.67	-0.19	0.00	0.00	1.47	0.07
			118	-170.67	-0.19	0.00	0.00	1.39	0.07
			235	-170.67	-0.19	0.00	0.00	1.31	0.07
525	Primo Impalcato	14, 73	0	219.57	0.10	0.00	0.00	0.01	0.03
			118	219.57	0.10	0.00	0.00	-0.03	0.03
			235	219.57	0.10	0.00	0.00	-0.08	0.03
526	Primo Impalcato	57, 75	0	-232.37	-0.03	0.00	0.00	0.56	0.13
			118	-232.37	-0.03	0.00	0.00	0.41	0.13
			235	-232.37	-0.03	0.00	0.00	0.25	0.13
527	Copertura	75, 58	0	183.79	0.17	0.00	0.00	-1.37	-0.19
			118	183.79	0.17	0.00	0.00	-1.14	-0.19
			235	183.79	0.17	0.00	0.00	-0.91	-0.19
528	Copertura	77, 61	0	-254.75	-0.06	0.00	0.00	0.36	0.17
			115	-254.75	-0.06	0.00	0.00	0.16	0.17
			231	-254.75	-0.06	0.00	0.00	-0.03	0.17
529	Primo Impalcato	62, 77	0	265.82	-0.04	0.00	0.00	-0.57	-0.07
			115	265.82	-0.04	0.00	0.00	-0.49	-0.07
			231	265.82	-0.04	0.00	0.00	-0.41	-0.07
530	Primo Impalcato	65, 78	0	-262.84	-0.04	0.00	0.00	-0.57	-0.07
			115	-262.84	-0.04	0.00	0.00	-0.49	-0.07
			231	-262.84	-0.04	0.00	0.00	-0.40	-0.07
531	Copertura	78, 66	0	250.11	-0.06	0.00	0.00	0.36	0.18
			115	250.11	-0.06	0.00	0.00	0.16	0.18
			231	250.11	-0.06	0.00	0.00	-0.04	0.18
532	Primo Impalcato	69, 76	0	-170.08	0.19	0.00	0.00	1.36	-0.08
			118	-170.08	0.19	0.00	0.00	1.46	-0.08
			235	-170.08	0.19	0.00	0.00	1.56	-0.08
533	Copertura	76, 70	0	217.89	-0.10	0.00	0.00	-0.17	-0.21
			118	217.89	-0.10	0.00	0.00	0.08	-0.21
			235	217.89	-0.10	0.00	0.00	0.34	-0.21
534	Copertura	1, 74	0	183.70	-0.18	0.00	0.00	0.92	-0.22
			118	183.70	-0.18	0.00	0.00	1.18	-0.22
			235	183.70	-0.18	0.00	0.00	1.44	-0.22
535	Copertura	74, 2	0	-229.77	0.03	0.00	0.00	-0.30	-0.46
			118	-229.77	0.03	0.00	0.00	0.24	-0.46
			235	-229.77	0.03	0.00	0.00	0.78	-0.46
536	Copertura	6, 71	0	259.80	0.05	0.00	0.00	-0.28	0.10
			115	259.80	0.05	0.00	0.00	-0.39	0.10
			231	259.80	0.05	0.00	0.00	-0.50	0.10
537	Copertura	71, 7	0	-260.31	0.07	0.00	0.00	0.47	-0.03
			115	-260.31	0.07	0.00	0.00	0.50	-0.03
			231	-260.31	0.07	0.00	0.00	0.53	-0.03
538	Copertura	9, 72	0	250.58	0.07	0.00	0.00	-0.55	-0.08
			115	250.58	0.07	0.00	0.00	-0.46	-0.08
			231	250.58	0.07	0.00	0.00	-0.37	-0.08
539	Copertura	72, 10	0	-260.59	0.02	0.00	0.00	0.42	0.18
			115	-260.59	0.02	0.00	0.00	0.21	0.18
			231	-260.59	0.02	0.00	0.00	0.00	0.18
540	Copertura	73, 13	0	219.57	0.04	0.00	0.00	-0.03	-0.26
			118	219.57	0.04	0.00	0.00	0.28	-0.26
			235	219.57	0.04	0.00	0.00	0.59	-0.26
541	Copertura	14, 73	0	-170.67	-0.17	0.00	0.00	0.86	-0.23
			118	-170.67	-0.17	0.00	0.00	1.13	-0.23
			235	-170.67	-0.17	0.00	0.00	1.40	-0.23
542	Copertura	15, 125	0	33.07	2.35	32.67	-81.83	90.78	12.17
			75	33.07	2.35	-28.71	-81.83	81.65	12.17
			150	33.07	2.35	-90.08	-81.83	72.52	12.17
543	Copertura	127, 16	0	-52.92	1.64	-36.78	-2.73	-73.45	9.82

			75	-52.92	1.64	-38.83	-2.73	-80.82	9.82
			150	-52.92	1.64	-40.88	-2.73	-88.19	9.82
544	Copertura	17, 129	0	137.29	2.12	45.33	-172.56	80.95	11.11
			75	137.29	2.12	-84.08	-172.56	72.62	11.11
			150	137.29	2.12	-213.50	-172.56	64.29	11.11
545	Copertura	130, 18	0	-154.28	2.07	51.78	-75.48	-64.41	10.60
			75	-154.28	2.07	-4.83	-75.48	-72.36	10.60
			150	-154.28	2.07	-61.44	-75.48	-80.31	10.60
546	Copertura	19, 135	0	259.21	1.66	52.92	-266.21	63.08	8.67
			75	259.21	1.66	-146.74	-266.21	56.58	8.67
			150	259.21	1.66	-346.39	-266.21	50.07	8.67
547	Copertura	134, 20	0	-275.97	1.34	184.46	-171.36	-50.50	7.42
			75	-275.97	1.34	55.94	-171.36	-56.07	7.42
			150	-275.97	1.34	-72.58	-171.36	-61.63	7.42
548	Copertura	21, 136	0	349.73	1.13	58.36	-335.17	44.62	6.12
			75	349.73	1.13	-193.02	-335.17	40.02	6.12
			150	349.73	1.13	-444.40	-335.17	35.43	6.12
549	Copertura	138, 22	0	-364.32	1.26	283.73	-241.40	-35.31	6.15
			75	-364.32	1.26	102.68	-241.40	-39.93	6.15
			150	-364.32	1.26	-78.37	-241.40	-44.54	6.15
550	Copertura	23, 141	0	415.66	0.71	62.81	-379.83	29.06	3.92
			75	415.66	0.71	-222.06	-379.83	26.11	3.92
			150	415.66	0.71	-506.94	-379.83	23.17	3.92
551	Copertura	142, 24	0	-417.67	0.59	352.40	-289.42	-23.34	3.26
			75	-417.67	0.59	135.33	-289.42	-25.78	3.26
			150	-417.67	0.59	-81.73	-289.42	-28.23	3.26
552	Copertura	25, 145	0	409.37	0.33	66.60	-396.84	16.59	2.18
			75	409.37	0.33	-231.03	-396.84	14.96	2.18
			150	409.37	0.33	-528.67	-396.84	13.32	2.18
553	Copertura	146, 26	0	-478.24	0.63	388.99	-315.43	-13.37	2.52
			75	-478.24	0.63	152.42	-315.43	-15.26	2.52
			150	-478.24	0.63	-84.15	-315.43	-17.15	2.52
554	Copertura	150, 27	0	-428.48	0.27	410.06	-330.86	-5.82	0.73
			75	-428.48	0.27	161.91	-330.86	-6.36	0.73
			150	-428.48	0.27	-86.23	-330.86	-6.90	0.73
555	Copertura	28, 149	0	488.53	-0.09	65.34	-404.36	6.49	0.76
			75	488.53	-0.09	-237.93	-404.36	5.93	0.76
			150	488.53	-0.09	-541.20	-404.36	5.36	0.76
556	Copertura	154, 29	0	-488.05	0.38	416.47	-333.31	-0.59	0.46
			75	-488.05	0.38	166.49	-333.31	-0.93	0.46
			150	-488.05	0.38	-83.49	-333.31	-1.28	0.46
557	Copertura	30, 153	0	449.81	-0.31	65.76	-417.48	1.11	-0.05
			75	449.81	-0.31	-247.35	-417.48	1.14	-0.05
			150	449.81	-0.31	-560.47	-417.48	1.18	-0.05
558	Copertura	158, 31	0	-480.46	0.26	414.58	-331.81	1.87	-0.12
			75	-480.46	0.26	165.72	-331.81	1.96	-0.12
			150	-480.46	0.26	-83.13	-331.81	2.05	-0.12
559	Copertura	32, 157	0	459.23	-0.43	64.53	-420.12	-2.02	-0.55
			75	459.23	-0.43	-250.56	-420.12	-1.61	-0.55
			150	459.23	-0.43	-565.65	-420.12	-1.20	-0.55
560	Copertura	162, 33	0	-472.14	0.32	409.04	-327.89	3.24	-0.15
			75	-472.14	0.32	163.12	-327.89	3.35	-0.15
			150	-472.14	0.32	-82.80	-327.89	3.46	-0.15
561	Copertura	34, 161	0	456.89	-0.51	63.38	-415.71	-3.65	-0.81
			75	456.89	-0.51	-248.40	-415.71	-3.04	-0.81
			150	456.89	-0.51	-560.18	-415.71	-2.43	-0.81
562	Copertura	166, 35	0	-464.96	0.30	401.12	-322.09	3.89	-0.30
			75	-464.96	0.30	159.55	-322.09	4.11	-0.30
			150	-464.96	0.30	-82.02	-322.09	4.34	-0.30
563	Copertura	36, 165	0	448.11	-0.55	62.44	-409.10	-4.48	-0.95
			75	448.11	-0.55	-244.39	-409.10	-3.76	-0.95
			150	448.11	-0.55	-551.21	-409.10	-3.05	-0.95
564	Copertura	170, 37	0	-454.37	0.31	392.50	-316.22	4.34	-0.34
			75	-454.37	0.31	155.33	-316.22	4.60	-0.34
			150	-454.37	0.31	-81.83	-316.22	4.85	-0.34
565	Copertura	38, 169	0	442.87	-0.58	60.47	-402.55	-4.94	-1.01
			75	442.87	-0.58	-241.44	-402.55	-4.18	-1.01
			150	442.87	-0.58	-543.35	-402.55	-3.43	-1.01
566	Copertura	175, 39	0	-433.09	0.31	383.14	-309.62	4.57	-0.41
			75	-433.09	0.31	150.93	-309.62	4.87	-0.41
			150	-433.09	0.31	-81.29	-309.62	5.18	-0.41
567	Copertura	40, 173	0	457.16	-0.56	57.31	-403.21	-5.10	-0.93

			75	457.16	-0.56	-245.10	-403.21	-4.40	-0.93
			150	457.16	-0.56	-547.51	-403.21	-3.70	-0.93
568	Copertura	178, 41	0	-543.77	0.25	380.17	-305.23	4.09	-0.45
			75	-543.77	0.25	151.25	-305.23	4.43	-0.45
			150	-543.77	0.25	-77.67	-305.23	4.77	-0.45
569	Copertura	42, 177	0	368.58	-0.64	56.88	-423.16	-5.87	-1.10
			75	368.58	-0.64	-260.49	-423.16	-5.04	-1.10
			150	368.58	-0.64	-577.86	-423.16	-4.22	-1.10
570	Copertura	43, 181	0	512.48	-0.25	57.32	-422.19	-6.90	-0.98
			75	512.48	-0.25	-259.32	-422.19	-6.16	-0.98
			150	512.48	-0.25	-575.96	-422.19	-5.43	-0.98
571	Copertura	182, 44	0	-401.77	0.09	378.07	-307.93	5.02	-0.71
			75	-401.77	0.09	147.12	-307.93	5.56	-0.71
			150	-401.77	0.09	-83.83	-307.93	6.09	-0.71
572	Copertura	45, 185	0	404.00	-0.42	59.42	-390.48	-12.84	-1.91
			75	404.00	-0.42	-233.44	-390.48	-11.41	-1.91
			150	404.00	-0.42	-526.29	-390.48	-9.98	-1.91
573	Copertura	186, 46	0	-447.24	-0.05	355.80	-292.03	10.39	-1.21
			75	-447.24	-0.05	136.77	-292.03	11.30	-1.21
			150	-447.24	-0.05	-82.26	-292.03	12.20	-1.21
574	Copertura	47, 189	0	379.80	-0.66	59.32	-360.43	-23.80	-3.30
			75	379.80	-0.66	-211.01	-360.43	-21.32	-3.30
			150	379.80	-0.66	-481.33	-360.43	-18.85	-3.30
575	Copertura	190, 48	0	-401.00	-0.52	321.20	-267.89	18.99	-3.26
			75	-401.00	-0.52	120.28	-267.89	21.43	-3.26
			150	-401.00	-0.52	-80.63	-267.89	23.88	-3.26
576	Copertura	49, 193	0	331.59	-1.11	56.86	-320.40	-39.83	-5.48
			75	331.59	-1.11	-183.43	-320.40	-35.72	-5.48
			150	331.59	-1.11	-423.73	-320.40	-31.61	-5.48
577	Copertura	195, 50	0	-346.42	-0.60	264.75	-228.10	32.15	-4.39
			75	-346.42	-0.60	93.67	-228.10	35.44	-4.39
			150	-346.42	-0.60	-77.41	-228.10	38.74	-4.39
578	Copertura	51, 197	0	247.67	-1.62	52.83	-257.59	-59.14	-8.15
			75	247.67	-1.62	-140.36	-257.59	-53.03	-8.15
			150	247.67	-1.62	-333.55	-257.59	-46.91	-8.15
579	Copertura	199, 52	0	-262.72	-1.43	169.46	-160.96	47.06	-7.99
			75	-262.72	-1.43	48.74	-160.96	53.05	-7.99
			150	-262.72	-1.43	-71.98	-160.96	59.05	-7.99
580	Copertura	53, 201	0	133.36	-2.17	45.00	-168.80	-78.26	-10.76
			75	133.36	-2.17	-81.60	-168.80	-70.19	-10.76
			150	133.36	-2.17	-208.19	-168.80	-62.12	-10.76
581	Copertura	202, 54	0	-150.00	-1.44	48.03	-72.68	62.91	-9.02
			75	-150.00	-1.44	-6.48	-72.68	69.68	-9.02
			150	-150.00	-1.44	-60.99	-72.68	76.44	-9.02
582	Copertura	55, 205	0	27.07	-2.38	33.12	-79.98	-88.85	-11.94
			75	27.07	-2.38	-26.87	-79.98	-79.89	-11.94
			150	27.07	-2.38	-86.86	-79.98	-70.94	-11.94
583	Copertura	206, 56	0	-51.73	-1.72	-42.83	0.45	71.67	-10.47
			75	-51.73	-1.72	-42.49	0.45	79.52	-10.47
			150	-51.73	-1.72	-42.15	0.45	87.37	-10.47
584	Copertura	57, 75	0	183.79	0.18	0.00	0.00	-1.12	0.10
			118	183.79	0.18	0.00	0.00	-1.24	0.10
			235	183.79	0.18	0.00	0.00	-1.35	0.10
585	Copertura	75, 58	0	-232.37	-0.03	0.00	0.00	0.23	0.42
			118	-232.37	-0.03	0.00	0.00	-0.26	0.42
			235	-232.37	-0.03	0.00	0.00	-0.75	0.42
586	Copertura	77, 61	0	265.82	-0.02	0.00	0.00	-0.41	-0.17
			115	265.82	-0.02	0.00	0.00	-0.21	-0.17
			231	265.82	-0.02	0.00	0.00	-0.01	-0.17
587	Copertura	62, 77	0	-254.75	-0.07	0.00	0.00	0.54	0.07
			115	-254.75	-0.07	0.00	0.00	0.45	0.07
			231	-254.75	-0.07	0.00	0.00	0.37	0.07
588	Copertura	65, 78	0	250.11	-0.07	0.00	0.00	0.54	0.07
			115	250.11	-0.07	0.00	0.00	0.45	0.07
			231	250.11	-0.07	0.00	0.00	0.37	0.07
589	Copertura	78, 66	0	-262.84	-0.02	0.00	0.00	-0.40	-0.18
			115	-262.84	-0.02	0.00	0.00	-0.20	-0.18
			231	-262.84	-0.02	0.00	0.00	0.01	-0.18
590	Copertura	69, 76	0	217.89	-0.04	0.00	0.00	0.56	0.29
			118	217.89	-0.04	0.00	0.00	0.22	0.29
			235	217.89	-0.04	0.00	0.00	-0.12	0.29
591	Copertura	76, 70	0	-170.08	0.18	0.00	0.00	1.48	0.42

			118	-170.08	0.18	0.00	0.00	0.99	0.42
			235	-170.08	0.18	0.00	0.00	0.50	0.42
592	Copertura	79, 81	0	-0.98	-0.04	-2.87	3.48	-10.28	-10.43
			80	-0.98	-0.04	-0.10	3.48	-1.98	-10.43
			159	-0.98	-0.04	2.67	3.48	6.31	-10.43
593	Copertura	80, 82	0	-2.47	0.60	-1.89	2.73	2.37	-1.64
			66	-2.47	0.60	-0.09	2.73	3.45	-1.64
			132	-2.47	0.60	1.71	2.73	4.53	-1.64
594	Copertura	83, 84	0	0.08	0.42	-1.38	2.05	1.37	-0.65
			66	0.08	0.42	-0.02	2.05	1.80	-0.65
			132	0.08	0.42	1.33	2.05	2.23	-0.65
595	Copertura	85, 86	0	2.23	0.18	-1.15	1.56	1.16	-0.04
			66	2.23	0.18	-0.13	1.56	1.19	-0.04
			132	2.23	0.18	0.90	1.56	1.22	-0.04
596	Copertura	87, 88	0	3.86	0.03	-0.23	0.07	0.76	0.10
			66	3.86	0.03	-0.18	0.07	0.70	0.10
			132	3.86	0.03	-0.13	0.07	0.63	0.10
597	Copertura	89, 90	0	1.06	-0.02	0.64	-1.06	0.32	0.14
			66	1.06	-0.02	-0.06	-1.06	0.23	0.14
			132	1.06	-0.02	-0.76	-1.06	0.14	0.14
598	Copertura	91, 92	0	0.24	-0.04	0.91	-1.43	0.14	0.12
			66	0.24	-0.04	-0.03	-1.43	0.06	0.12
			132	0.24	-0.04	-0.98	-1.43	-0.02	0.12
599	Copertura	93, 94	0	-4.12	-0.03	0.35	-0.26	-0.04	-0.04
			66	-4.12	-0.03	0.18	-0.26	-0.02	-0.04
			132	-4.12	-0.03	0.01	-0.26	0.01	-0.04
600	Copertura	95, 96	0	-4.91	-0.08	-0.77	1.45	0.63	-0.02
			66	-4.91	-0.08	0.19	1.45	0.65	-0.02
			132	-4.91	-0.08	1.15	1.45	0.66	-0.02
601	Copertura	97, 106	0	-0.35	-0.24	-2.01	3.02	1.63	0.21
			66	-0.35	-0.24	-0.02	3.02	1.49	0.21
			132	-0.35	-0.24	1.97	3.02	1.35	0.21
602	Copertura	98, 99	0	-0.34	0.36	-2.06	3.01	0.15	-3.15
			66	-0.34	0.36	-0.08	3.01	2.23	-3.15
			132	-0.34	0.36	1.91	3.01	4.31	-3.15
603	Copertura	100, 101	0	0.47	0.18	-2.02	3.09	0.62	-1.56
			66	0.47	0.18	0.01	3.09	1.65	-1.56
			132	0.47	0.18	2.05	3.09	2.67	-1.56
604	Copertura	102, 103	0	4.02	0.06	-2.11	3.03	0.66	-0.44
			66	4.02	0.06	-0.10	3.03	0.95	-0.44
			132	4.02	0.06	1.90	3.03	1.24	-0.44
605	Copertura	104, 105	0	1.02	-0.01	-1.76	2.74	0.48	0.16
			66	1.02	-0.01	0.05	2.74	0.38	0.16
			132	1.02	-0.01	1.86	2.74	0.28	0.16
606	Copertura	107, 108	0	-0.82	-0.54	-2.21	3.32	2.81	0.76
			66	-0.82	-0.54	-0.02	3.32	2.31	0.76
			132	-0.82	-0.54	2.17	3.32	1.81	0.76
607	Copertura	109, 110	0	-2.66	-0.52	-0.64	0.80	6.21	11.27
			80	-2.66	-0.52	-0.01	0.80	-2.76	11.27
			159	-2.66	-0.52	0.63	0.80	-11.72	11.27
608	Copertura	111, 112	0	0.25	-0.08	-1.88	2.94	0.29	0.28
			66	0.25	-0.08	0.06	2.94	0.10	0.28
			132	0.25	-0.08	2.00	2.94	-0.08	0.28
609	Copertura	113, 114	0	-0.21	-0.03	-2.08	3.08	0.14	0.23
			66	-0.21	-0.03	-0.05	3.08	-0.02	0.23
			132	-0.21	-0.03	1.98	3.08	-0.17	0.23
610	Copertura	115, 116	0	-8.20	-0.01	-2.40	3.98	0.10	-0.18
			66	-8.20	-0.01	0.23	3.98	0.22	-0.18
			132	-8.20	-0.01	2.86	3.98	0.34	-0.18
611	Copertura	117, 118	0	-0.49	-0.09	-3.39	5.03	1.63	0.66
			66	-0.49	-0.09	-0.07	5.03	1.19	0.66
			132	-0.49	-0.09	3.26	5.03	0.76	0.66
612	Copertura	119, 120	0	0.10	-0.26	-3.42	5.11	3.46	2.15
			66	0.10	-0.26	-0.04	5.11	2.04	2.15
			132	0.10	-0.26	3.33	5.11	0.62	2.15
613	Copertura	121, 122	0	-1.42	-0.27	-2.92	4.20	5.26	4.24
			66	-1.42	-0.27	-0.16	4.20	2.46	4.24
			132	-1.42	-0.27	2.61	4.20	-0.34	4.24
614	Copertura	124, 125	0	-122.37	0.54	-9.16	6.17	0.27	-2.28
			99	-122.37	0.54	-3.04	6.17	2.53	-2.28
			198	-122.37	0.54	3.08	6.17	4.80	-2.28
615	Copertura	125, 127	0	-55.37	-0.39	-87.01	2.97	76.50	9.89

			775	-55.37	-0.39	-63.99	2.97	-0.12	9.89
			1550	-55.37	-0.39	-40.98	2.97	-76.75	9.89
616	Copertura	126, 127	0	1.89	0.62	7.54	-5.91	3.95	0.06
			99	1.89	0.62	1.67	-5.91	3.88	0.06
			198	1.89	0.62	-4.20	-5.91	3.82	0.06
617	Copertura	128, 129	0	-276.10	0.47	-16.62	10.77	-0.24	-2.34
			99	-276.10	0.47	-5.94	10.77	2.09	-2.34
			198	-276.10	0.47	4.75	10.77	4.41	-2.34
618	Copertura	129, 130	0	-64.31	-0.41	-208.75	16.41	67.93	8.77
			775	-64.31	-0.41	-81.60	16.41	-0.02	8.77
			1550	-64.31	-0.41	45.56	16.41	-67.98	8.77
619	Copertura	131, 130	0	128.17	0.47	14.64	-10.51	0.68	-1.84
			99	128.17	0.47	4.21	-10.51	2.50	-1.84
			198	128.17	0.47	-6.23	-10.51	4.32	-1.84
620	Copertura	132, 135	0	-439.64	0.37	-24.25	15.38	-0.23	-1.84
			99	-439.64	0.37	-8.99	15.38	1.59	-1.84
			198	-439.64	0.37	6.27	15.38	3.41	-1.84
621	Copertura	133, 134	0	295.05	0.40	22.33	-15.17	1.80	-0.59
			99	295.05	0.40	7.28	-15.17	2.38	-0.59
			198	295.05	0.40	-7.78	-15.17	2.97	-0.59
622	Copertura	135, 134	0	-62.94	-0.30	-340.12	33.34	52.90	6.83
			775	-62.94	-0.30	-81.72	33.34	-0.05	6.83
			1550	-62.94	-0.30	176.68	33.34	-53.01	6.83
623	Copertura	137, 136	0	-560.20	0.27	-29.90	18.79	-0.16	-1.29
			99	-560.20	0.27	-11.25	18.79	1.12	-1.29
			198	-560.20	0.27	7.39	18.79	2.40	-1.29
624	Copertura	136, 138	0	-61.30	-0.24	-437.01	45.92	37.42	4.83
			775	-61.30	-0.24	-81.12	45.92	0.00	4.83
			1550	-61.30	-0.24	274.78	45.92	-37.42	4.83
625	Copertura	139, 138	0	417.17	0.24	28.11	-18.67	-0.05	-1.32
			99	417.17	0.24	9.58	-18.67	1.26	-1.32
			198	417.17	0.24	-8.95	-18.67	2.58	-1.32
626	Copertura	140, 141	0	-638.51	0.18	-33.65	21.09	-0.03	-0.77
			99	-638.51	0.18	-12.72	21.09	0.74	-0.77
			198	-638.51	0.18	8.21	21.09	1.50	-0.77
627	Copertura	141, 142	0	-53.04	-0.14	-498.73	54.29	24.43	3.15
			775	-53.04	-0.14	-78.00	54.29	-0.02	3.15
			1550	-53.04	-0.14	342.72	54.29	-24.47	3.15
628	Copertura	143, 142	0	500.65	0.19	31.86	-20.93	1.13	-0.10
			99	500.65	0.19	11.09	-20.93	1.23	-0.10
			198	500.65	0.19	-9.68	-20.93	1.33	-0.10
629	Copertura	144, 145	0	-668.78	0.11	-35.44	22.26	0.11	-0.35
			99	-668.78	0.11	-13.35	22.26	0.45	-0.35
			198	-668.78	0.11	8.75	22.26	0.80	-0.35
630	Copertura	145, 146	0	-81.44	-0.11	-519.92	57.98	14.00	1.83
			775	-81.44	-0.11	-70.56	57.98	-0.16	1.83
			1550	-81.44	-0.11	378.80	57.98	-14.33	1.83
631	Copertura	147, 146	0	544.41	0.07	34.08	-22.31	-0.18	-0.70
			99	544.41	0.07	11.95	-22.31	0.52	-0.70
			198	544.41	0.07	-10.19	-22.31	1.21	-0.70
632	Copertura	148, 149	0	-682.65	0.07	-36.55	22.99	-0.04	-0.01
			99	-682.65	0.07	-13.73	22.99	-0.03	-0.01
			198	-682.65	0.07	9.09	22.99	-0.02	-0.01
633	Copertura	149, 150	0	-12.28	-0.02	-532.11	60.10	5.39	0.75
			775	-12.28	-0.02	-66.18	60.10	-0.41	0.75
			1550	-12.28	-0.02	399.74	60.10	-6.20	0.75
634	Copertura	151, 150	0	570.57	0.03	35.06	-22.86	0.53	0.02
			99	570.57	0.03	12.37	-22.86	0.51	0.02
			198	570.57	0.03	-10.32	-22.86	0.48	0.02
635	Copertura	152, 153	0	-704.89	0.05	-37.10	23.24	-0.08	0.17
			99	-704.89	0.05	-14.03	23.24	-0.25	0.17
			198	-704.89	0.05	9.03	23.24	-0.41	0.17
636	Copertura	153, 154	0	-67.65	0.00	-551.43	61.74	0.89	0.12
			775	-67.65	0.00	-72.71	61.74	-0.04	0.12
			1551	-67.65	0.00	406.00	61.74	-0.98	0.12
637	Copertura	155, 154	0	576.42	-0.03	35.59	-23.20	-0.12	-0.34
			99	576.42	-0.03	12.56	-23.20	0.21	-0.34
			198	576.42	-0.03	-10.47	-23.20	0.55	-0.34
638	Copertura	156, 157	0	-709.21	0.03	-37.19	23.27	0.01	0.34
			99	-709.21	0.03	-14.10	23.27	-0.32	0.34
			198	-709.21	0.03	9.00	23.27	-0.65	0.34
639	Copertura	157, 158	0	-61.47	0.02	-556.65	61.95	-1.67	-0.22

			775	-61.47	0.02	-76.26	61.95	0.00	-0.22
			1551	-61.47	0.02	404.13	61.95	1.67	-0.22
640	Copertura	159, 158	0	574.51	-0.05	35.51	-23.16	0.12	-0.09
			99	574.51	-0.05	12.53	-23.16	0.21	-0.09
			198	574.51	-0.05	-10.45	-23.16	0.30	-0.09
641	Copertura	160, 161	0	-701.62	0.03	-36.86	23.07	0.05	0.43
			99	-701.62	0.03	-13.96	23.07	-0.37	0.43
			198	-701.62	0.03	8.94	23.07	-0.79	0.43
642	Copertura	161, 162	0	-58.21	0.03	-551.24	61.24	-3.01	-0.39
			776	-58.21	0.03	-76.30	61.24	0.00	-0.39
			1551	-58.21	0.03	398.63	61.24	3.01	-0.39
643	Copertura	163, 162	0	567.65	-0.07	35.18	-22.97	-0.12	-0.24
			99	567.65	-0.07	12.39	-22.97	0.12	-0.24
			198	567.65	-0.07	-10.41	-22.97	0.36	-0.24
644	Copertura	164, 165	0	-690.21	0.02	-36.35	22.77	0.07	0.48
			99	-690.21	0.02	-13.75	22.77	-0.41	0.48
			198	-690.21	0.02	8.85	22.77	-0.88	0.48
645	Copertura	165, 166	0	-58.56	0.04	-542.36	60.15	-3.70	-0.48
			776	-58.56	0.04	-75.77	60.15	0.00	-0.48
			1551	-58.56	0.04	390.81	60.15	3.71	-0.48
646	Copertura	167, 166	0	557.46	-0.07	34.74	-22.69	-0.05	-0.18
			99	557.46	-0.07	12.22	-22.69	0.13	-0.18
			198	557.46	-0.07	-10.31	-22.69	0.31	-0.18
647	Copertura	168, 169	0	-678.97	0.02	-35.83	22.45	0.02	0.47
			99	-678.97	0.02	-13.55	22.45	-0.45	0.47
			198	-678.97	0.02	8.73	22.45	-0.92	0.47
648	Copertura	169, 170	0	-55.52	0.05	-534.62	59.10	-4.11	-0.53
			776	-55.52	0.05	-76.17	59.10	0.02	-0.53
			1552	-55.52	0.05	382.27	59.10	4.15	-0.53
649	Copertura	171, 170	0	547.21	-0.08	34.25	-22.41	-0.06	-0.19
			99	547.21	-0.08	12.01	-22.41	0.13	-0.19
			198	547.21	-0.08	-10.23	-22.41	0.32	-0.19
650	Copertura	172, 173	0	-679.64	0.02	-35.69	22.31	-0.19	0.36
			99	-679.64	0.02	-13.55	22.31	-0.55	0.36
			198	-679.64	0.02	8.59	22.31	-0.91	0.36
651	Copertura	173, 175	0	-41.82	0.05	-538.91	58.77	-4.38	-0.57
			776	-41.82	0.05	-82.95	58.77	0.01	-0.57
			1552	-41.82	0.05	373.01	58.77	4.40	-0.57
652	Copertura	174, 175	0	536.95	-0.08	33.80	-22.13	-0.02	-0.16
			99	536.95	-0.08	11.83	-22.13	0.14	-0.16
			198	536.95	-0.08	-10.13	-22.13	0.30	-0.16
653	Copertura	176, 177	0	-713.01	0.02	-35.82	22.14	-0.04	0.52
			99	-713.01	0.02	-13.84	22.14	-0.55	0.52
			198	-713.01	0.02	8.13	22.14	-1.07	0.52
654	Copertura	177, 178	0	-155.73	0.07	-569.73	60.54	-5.01	-0.58
			776	-155.73	0.07	-99.91	60.54	-0.51	-0.58
			1552	-155.73	0.07	369.91	60.54	3.99	-0.58
655	Copertura	179, 178	0	532.80	-0.07	33.93	-22.26	-0.06	-0.13
			99	532.80	-0.07	11.84	-22.26	0.06	-0.13
			198	532.80	-0.07	-10.26	-22.26	0.19	-0.13
656	Copertura	180, 181	0	-711.13	-0.03	-35.95	22.25	0.11	0.29
			99	-711.13	-0.03	-13.86	22.25	-0.17	0.29
			198	-711.13	-0.03	8.22	22.25	-0.45	0.29
657	Copertura	181, 182	0	-10.34	0.03	-567.73	60.37	-5.79	-0.70
			775	-10.34	0.03	-99.87	60.37	-0.37	-0.70
			1550	-10.34	0.03	368.00	60.37	5.06	-0.70
658	Copertura	183, 182	0	537.01	-0.07	33.52	-21.96	0.04	0.02
			99	537.01	-0.07	11.73	-21.96	0.03	0.02
			198	537.01	-0.07	-10.07	-21.96	0.01	0.02
659	Copertura	184, 185	0	-656.76	-0.06	-34.14	21.30	0.25	0.53
			99	-656.76	-0.06	-13.00	21.30	-0.28	0.53
			198	-656.76	-0.06	8.14	21.30	-0.81	0.53
660	Copertura	185, 186	0	-78.36	0.06	-518.16	55.75	-10.62	-1.38
			775	-78.36	0.06	-86.09	55.75	0.03	-1.38
			1550	-78.36	0.06	345.97	55.75	10.69	-1.38
661	Copertura	187, 186	0	506.53	-0.12	32.30	-21.23	-0.63	-0.17
			99	506.53	-0.12	11.24	-21.23	-0.47	-0.17
			198	506.53	-0.12	-9.83	-21.23	-0.30	-0.17
662	Copertura	188, 189	0	-604.57	-0.13	-31.95	20.04	0.09	0.73
			99	-604.57	-0.13	-12.07	20.04	-0.64	0.73
			198	-604.57	-0.13	7.82	20.04	-1.36	0.73
663	Copertura	189, 190	0	-63.94	0.13	-473.51	50.67	-19.96	-2.58

			775	-63.94	0.13	-80.85	50.67	0.01	-2.58
			1550	-63.94	0.13	311.81	50.67	19.97	-2.58
664	Copertura	191, 190	0	463.35	-0.15	30.26	-19.98	0.19	0.68
			99	463.35	-0.15	10.43	-19.98	-0.49	0.68
			198	463.35	-0.15	-9.39	-19.98	-1.17	0.68
665	Copertura	192, 193	0	-534.61	-0.22	-28.72	18.08	0.08	1.16
			99	-534.61	-0.22	-10.77	18.08	-1.07	1.16
			198	-534.61	-0.22	7.17	18.08	-2.22	1.16
666	Copertura	193, 195	0	-60.56	0.18	-416.56	43.40	-33.43	-4.32
			775	-60.56	0.18	-80.25	43.40	0.03	-4.32
			1550	-60.56	0.18	256.06	43.40	33.50	-4.32
667	Copertura	194, 195	0	393.84	-0.29	26.94	-17.95	-1.38	0.08
			99	393.84	-0.29	9.13	-17.95	-1.45	0.08
			198	393.84	-0.29	-8.69	-17.95	-1.53	0.08
668	Copertura	196, 197	0	-424.23	-0.33	-23.54	14.96	0.16	1.75
			99	-424.23	-0.33	-8.69	14.96	-1.58	1.75
			198	-424.23	-0.33	6.15	14.96	-3.32	1.75
669	Copertura	197, 199	0	-63.12	0.31	-327.40	31.56	-49.63	-6.40
			775	-63.12	0.31	-82.80	31.56	-0.01	-6.40
			1550	-63.12	0.31	161.79	31.56	49.62	-6.40
670	Copertura	198, 199	0	276.92	-0.36	21.64	-14.77	0.08	1.59
			99	276.92	-0.36	6.98	-14.77	-1.49	1.59
			198	276.92	-0.36	-7.67	-14.77	-3.07	1.59
671	Copertura	200, 201	0	-269.70	-0.44	-16.31	10.59	0.17	2.28
			99	-269.70	-0.44	-5.81	10.59	-2.09	2.28
			198	-269.70	-0.44	4.70	10.59	-4.35	2.28
672	Copertura	201, 202	0	-63.51	0.35	-203.50	15.83	-65.69	-8.48
			775	-63.51	0.35	-80.78	15.83	0.06	-8.48
			1550	-63.51	0.35	41.93	15.83	65.80	-8.48
673	Copertura	203, 202	0	123.33	-0.54	14.23	-10.24	-2.30	0.53
			99	123.33	-0.54	4.06	-10.24	-2.83	0.53
			198	123.33	-0.54	-6.10	-10.24	-3.36	0.53
674	Copertura	204, 205	0	-118.73	-0.51	-8.98	6.07	-0.32	2.27
			99	-118.73	-0.51	-2.96	6.07	-2.57	2.27
			198	-118.73	-0.51	3.06	6.07	-4.82	2.27
675	Copertura	205, 206	0	-58.68	0.40	-83.80	2.36	-74.91	-9.67
			775	-58.68	0.40	-65.48	2.36	0.06	-9.67
			1550	-58.68	0.40	-47.17	2.36	75.03	-9.67
676	Copertura	207, 206	0	-4.00	-0.60	7.57	-6.00	-2.36	0.79
			99	-4.00	-0.60	1.61	-6.00	-3.14	0.79
			198	-4.00	-0.60	-4.34	-6.00	-3.93	0.79
677	Copertura	79	0	-237.98	-7.00	2.48	-3.69	74.36	12.53
			125	-237.98	-7.00	-2.13	-3.69	27.24	62.87
			250	-237.98	-7.00	-6.75	-3.69	-82.81	113.20
678	Copertura	124	0	-16.44	-2.23	-0.43	0.20	145.04	-35.21
			155	-16.44	-2.23	-0.12	0.20	154.35	23.21
			310	-16.44	-2.23	0.18	0.20	73.10	81.63
679	Copertura	80	0	5.10	-1.42	0.15	-4.73	229.60	35.49
			45	5.10	-1.42	-1.98	-4.73	206.00	69.41
			90	5.10	-1.42	-4.11	-4.73	167.13	103.34
680	Copertura	128	0	-43.23	-2.59	-0.18	-0.19	252.74	-6.96
			155	-43.23	-2.59	-0.48	-0.19	221.35	47.47
			310	-43.23	-2.59	-0.79	-0.19	105.59	101.90
681	Copertura	82	0	36.28	-5.82	-0.74	0.07	305.24	45.70
			43	36.28	-5.82	-0.71	0.07	279.35	75.66
			85	36.28	-5.82	-0.69	0.07	240.69	105.62
682	Copertura	132	0	-41.98	-2.06	0.04	-0.35	361.74	30.23
			155	-41.98	-2.06	-0.50	-0.35	272.69	84.66
			310	-41.98	-2.06	-1.04	-0.35	99.28	139.09
683	Copertura	83	0	41.59	-2.40	-0.19	-1.70	331.14	82.90
			43	41.59	-2.40	-0.91	-1.70	289.39	112.86
			85	41.59	-2.40	-1.64	-1.70	234.86	142.82
684	Copertura	137	0	-36.65	-1.44	0.22	-0.45	442.55	57.29
			155	-36.65	-1.44	-0.48	-0.45	311.57	111.72
			310	-36.65	-1.44	-1.17	-0.45	96.22	166.15
685	Copertura	84	0	39.04	-2.98	-0.17	-1.68	348.47	112.23
			43	39.04	-2.98	-0.88	-1.68	294.21	142.19
			85	39.04	-2.98	-1.60	-1.68	227.17	172.15
686	Copertura	140	0	-46.98	-0.82	0.35	-0.49	496.03	73.64
			155	-46.98	-0.82	-0.41	-0.49	339.70	128.07
			310	-46.98	-0.82	-1.17	-0.49	99.02	182.50
687	Copertura	85	0	50.69	-0.90	-0.93	0.04	360.75	130.40

			43	50.69	-0.90	-0.92	0.04	298.74	160.36
			85	50.69	-0.90	-0.90	0.04	223.95	190.32
688	Copertura	144	0	-62.11	-0.29	0.44	-0.54	524.14	71.57
			155	-62.11	-0.29	-0.39	-0.54	366.27	132.13
			310	-62.11	-0.29	-1.22	-0.54	114.53	192.70
689	Copertura	86	0	59.26	-1.30	0.48	-2.07	370.81	140.28
			43	59.26	-1.30	-0.40	-2.07	304.59	170.24
			85	59.26	-1.30	-1.29	-2.07	225.58	200.20
690	Copertura	87	0	60.80	-0.01	-1.38	2.40	373.37	145.98
			43	60.80	-0.01	-0.36	2.40	304.71	175.94
			85	60.80	-0.01	0.67	2.40	223.27	205.91
691	Copertura	148	0	-65.95	-0.23	-3.72	1.70	538.38	71.53
			155	-65.95	-0.23	-1.09	1.70	378.72	134.47
			310	-65.95	-0.23	1.54	1.70	121.51	197.41
692	Copertura	88	0	54.73	-0.34	1.01	-1.66	376.77	147.35
			43	54.73	-0.34	0.30	-1.66	307.52	177.31
			85	54.73	-0.34	-0.41	-1.66	225.50	207.27
693	Copertura	152	0	-58.60	-0.15	-5.44	2.65	546.80	82.71
			155	-58.60	-0.15	-1.34	2.65	373.90	140.39
			310	-58.60	-0.15	2.77	2.65	111.61	198.06
694	Copertura	89	0	58.47	0.24	-0.59	2.22	377.41	146.55
			43	58.47	0.24	0.36	2.22	308.51	176.51
			85	58.47	0.24	1.30	2.22	226.82	206.48
695	Copertura	156	0	-58.49	0.05	-6.07	3.02	547.34	86.34
			155	-58.49	0.05	-1.39	3.02	369.85	142.67
			310	-58.49	0.05	3.30	3.02	105.06	199.00
696	Copertura	90	0	59.30	0.08	0.08	1.13	376.19	145.14
			43	59.30	0.08	0.56	1.13	307.89	175.11
			85	59.30	0.08	1.04	1.13	226.81	205.07
697	Copertura	160	0	-62.04	0.15	-6.72	3.39	542.46	84.60
			155	-62.04	0.15	-1.45	3.39	367.54	141.10
			310	-62.04	0.15	3.81	3.39	105.04	197.60
698	Copertura	91	0	61.25	0.28	-0.35	2.20	374.13	143.09
			43	61.25	0.28	0.59	2.20	306.70	173.05
			85	61.25	0.28	1.53	2.20	226.50	203.01
699	Copertura	164	0	-66.38	0.18	-7.30	3.72	535.25	81.71
			155	-66.38	0.18	-1.53	3.72	364.81	138.21
			310	-66.38	0.18	4.25	3.72	106.79	194.71
700	Copertura	92	0	60.63	0.21	-0.20	2.04	372.30	140.86
			43	60.63	0.21	0.67	2.04	305.82	170.83
			85	60.63	0.21	1.54	2.04	226.56	200.79
701	Copertura	168	0	-66.48	0.12	-7.86	4.03	527.62	79.51
			155	-66.48	0.12	-1.61	4.03	360.72	135.84
			310	-66.48	0.12	4.64	4.03	106.51	192.17
702	Copertura	93	0	57.84	0.25	1.10	-1.22	372.06	138.34
			43	57.84	0.25	0.57	-1.22	306.66	168.30
			85	57.84	0.25	0.05	-1.22	228.48	198.26
703	Copertura	172	0	-56.92	-0.15	-8.45	4.36	524.71	83.85
			155	-56.92	-0.15	-1.70	4.36	351.09	140.18
			310	-56.92	-0.15	5.05	4.36	90.15	196.51
704	Copertura	94	0	59.50	0.13	-1.55	2.86	372.13	137.40
			43	59.50	0.13	-0.33	2.86	307.13	167.36
			85	59.50	0.13	0.88	2.86	229.35	197.33
705	Copertura	176	0	-46.84	0.04	-9.64	5.07	526.07	110.57
			155	-46.84	0.04	-1.79	5.07	326.08	147.49
			310	-46.84	0.04	6.07	5.07	68.85	184.42
706	Copertura	180	0	-45.26	0.37	0.36	-0.37	523.99	110.48
			155	-45.26	0.37	-0.20	-0.37	324.93	146.37
			310	-45.26	0.37	-0.77	-0.37	70.24	182.26
707	Copertura	95	0	69.77	0.49	1.18	-3.25	370.88	137.51
			43	69.77	0.49	-0.21	-3.25	305.83	167.47
			85	69.77	0.49	-1.59	-3.25	228.00	197.44
708	Copertura	184	0	-43.43	0.72	0.33	-0.30	503.68	81.62
			155	-43.43	0.72	-0.13	-0.30	334.98	136.05
			310	-43.43	0.72	-0.59	-0.30	81.91	190.48
709	Copertura	96	0	48.05	0.45	-1.88	1.94	364.18	131.47
			43	48.05	0.45	-1.05	1.94	301.71	161.43
			85	48.05	0.45	-0.23	1.94	226.45	191.40
710	Copertura	188	0	-49.56	0.81	0.42	-0.34	472.29	66.52
			155	-49.56	0.81	-0.11	-0.34	326.99	120.95
			310	-49.56	0.81	-0.64	-0.34	97.33	175.38
711	Copertura	97	0	45.55	1.75	-0.17	-2.56	356.47	122.44

			43	45.55	1.75	-1.26	-2.56	297.85	152.40
			85	45.55	1.75	-2.35	-2.56	226.45	182.36
712	Copertura	192	0	-41.03	1.27	0.56	-0.42	425.77	51.00
			155	-41.03	1.27	-0.09	-0.42	304.55	105.43
			310	-41.03	1.27	-0.73	-0.42	98.95	159.85
713	Copertura	106	0	32.76	1.39	-0.42	-2.02	344.89	105.98
			43	32.76	1.39	-1.28	-2.02	293.30	135.94
			85	32.76	1.39	-2.15	-2.02	228.92	165.90
714	Copertura	196	0	-49.76	1.92	0.78	-0.55	351.46	26.58
			155	-49.76	1.92	-0.07	-0.55	268.08	81.01
			310	-49.76	1.92	-0.93	-0.55	100.33	135.44
715	Copertura	107	0	34.82	3.94	-0.08	-3.17	329.20	79.81
			43	34.82	3.94	-1.43	-3.17	288.76	109.78
			85	34.82	3.94	-2.78	-3.17	235.55	139.74
716	Copertura	200	0	-48.05	2.49	1.03	-0.74	248.30	-8.36
			155	-48.05	2.49	-0.11	-0.74	219.07	46.07
			310	-48.05	2.49	-1.26	-0.74	105.48	100.50
717	Copertura	108	0	42.07	2.61	-0.55	-1.84	303.93	43.37
			43	42.07	2.61	-1.34	-1.84	279.04	73.33
			85	42.07	2.61	-2.12	-1.84	241.37	103.29
718	Copertura	204	0	-21.35	2.18	1.31	-1.17	142.55	-36.11
			155	-21.35	2.18	-0.50	-1.17	153.25	22.31
			310	-21.35	2.18	-2.31	-1.17	73.40	80.73
719	Copertura	109	0	17.47	5.97	0.48	-3.02	222.55	33.48
			43	17.47	5.97	-0.81	-3.02	201.41	65.64
			85	17.47	5.97	-2.09	-3.02	166.55	97.80
720	Copertura	110	0	-234.31	11.92	-1.68	0.83	3.88	83.52
			43	-234.31	11.92	-1.33	0.83	-35.41	100.69
			85	-234.31	11.92	-0.97	0.83	-82.03	117.87
721	Copertura	14	0	-234.49	3.28	4.76	-2.71	32.39	-34.15
			95	-234.49	3.28	2.19	-2.71	61.96	-25.09
			190	-234.49	3.28	-0.39	-2.71	74.32	2.09
722	Copertura	15	0	68.36	-2.79	2.05	-2.09	-34.66	-134.95
			65	68.36	-2.79	0.70	-2.09	52.45	-132.13
			130	68.36	-2.79	-0.66	-2.09	135.88	-123.65
723	Copertura	16	0	-1.45	-0.84	3.01	-3.21	-53.38	-141.74
			65	-1.45	-0.84	0.92	-3.21	37.52	-136.09
			130	-1.45	-0.84	-1.17	-3.21	121.08	-119.13
724	Copertura	17	0	145.73	-2.72	2.60	-2.54	-44.14	-219.09
			65	145.73	-2.72	0.95	-2.54	97.71	-216.46
			130	145.73	-2.72	-0.69	-2.54	236.12	-208.56
725	Copertura	18	0	-55.25	-2.28	1.23	-0.32	-65.59	-224.68
			65	-55.25	-2.28	1.02	-0.32	79.31	-219.41
			130	-55.25	-2.28	0.81	-0.32	217.37	-203.61
726	Copertura	19	0	257.57	-2.13	2.45	-2.19	-51.14	-302.46
			65	257.57	-2.13	1.03	-2.19	144.89	-299.83
			130	257.57	-2.13	-0.39	-2.19	337.49	-291.92
727	Copertura	20	0	-164.06	-1.09	1.85	-1.54	-71.06	-306.51
			65	-164.06	-1.09	0.85	-1.54	127.03	-301.25
			130	-164.06	-1.09	-0.15	-1.54	318.27	-285.44
728	Copertura	21	0	344.44	-1.49	2.18	-1.74	-56.34	-364.28
			65	344.44	-1.49	1.05	-1.74	179.87	-361.64
			130	344.44	-1.49	-0.09	-1.74	412.65	-353.74
729	Copertura	22	0	-247.24	-1.49	1.52	-0.74	-77.13	-370.59
			65	-247.24	-1.49	1.04	-0.74	162.61	-365.33
			130	-247.24	-1.49	0.56	-0.74	395.51	-349.52
730	Copertura	23	0	387.13	-0.92	1.83	-1.26	-60.33	-405.60
			65	387.13	-0.92	1.01	-1.26	202.73	-402.96
			130	387.13	-0.92	0.19	-1.26	462.38	-395.06
731	Copertura	24	0	-294.55	-0.36	2.02	-1.62	-80.57	-411.62
			65	-294.55	-0.36	0.96	-1.62	185.84	-406.35
			130	-294.55	-0.36	-0.09	-1.62	445.40	-390.54
732	Copertura	25	0	392.72	-0.44	1.58	-0.89	-66.47	-430.96
			65	392.72	-0.44	1.00	-0.89	213.02	-428.03
			130	392.72	-0.44	0.42	-0.89	488.70	-419.24
733	Copertura	26	0	-312.67	-0.66	3.81	-3.17	-83.09	-435.81
			65	-312.67	-0.66	1.75	-3.17	199.05	-430.54
			130	-312.67	-0.66	-0.30	-3.17	474.33	-414.74
734	Copertura	27	0	-333.13	0.05	5.54	-6.00	-84.42	-448.48
			65	-333.13	0.05	1.64	-6.00	205.95	-443.21
			130	-333.13	0.05	-2.26	-6.00	489.47	-427.41
735	Copertura	28	0	398.51	-0.25	8.13	-8.60	-66.65	-441.36

			65	398.51	-0.25	2.54	-8.60	219.57	-438.31
			130	398.51	-0.25	-3.05	-8.60	501.83	-429.17
736	Copertura	29	0	-337.65	-0.08	9.49	-10.29	-83.31	-451.73
			65	-337.65	-0.08	2.80	-10.29	209.17	-446.46
			130	-337.65	-0.08	-3.89	-10.29	494.81	-430.66
737	Copertura	30	0	420.63	-0.12	10.75	-11.72	-64.87	-445.71
			65	420.63	-0.12	3.13	-11.72	224.24	-442.91
			130	420.63	-0.12	-4.49	-11.72	509.71	-434.54
738	Copertura	31	0	-339.09	0.15	9.79	-10.63	-83.26	-451.14
			65	-339.09	0.15	2.88	-10.63	208.84	-445.88
			130	-339.09	0.15	-4.04	-10.63	494.10	-430.07
739	Copertura	32	0	423.58	0.02	11.53	-12.68	-63.65	-445.03
			65	423.58	0.02	3.29	-12.68	225.03	-442.31
			130	423.58	0.02	-4.95	-12.68	510.17	-434.13
740	Copertura	33	0	-325.85	0.07	11.12	-12.02	-82.69	-447.30
			65	-325.85	0.07	3.31	-12.02	206.91	-442.03
			130	-325.85	0.07	-4.50	-12.02	489.66	-426.23
741	Copertura	34	0	414.91	0.09	12.38	-13.71	-63.13	-441.15
			65	414.91	0.09	3.47	-13.71	223.03	-438.41
			130	414.91	0.09	-5.45	-13.71	505.63	-430.21
742	Copertura	35	0	-325.36	0.14	11.62	-12.63	-81.83	-442.09
			65	-325.36	0.14	3.41	-12.63	204.39	-436.82
			130	-325.36	0.14	-4.80	-12.63	483.76	-421.02
743	Copertura	36	0	402.88	0.11	13.17	-14.68	-62.56	-435.56
			65	402.88	0.11	3.63	-14.68	219.96	-432.82
			130	402.88	0.11	-5.92	-14.68	498.93	-424.62
744	Copertura	37	0	-310.18	0.15	12.36	-13.48	-81.09	-436.44
			65	-310.18	0.15	3.60	-13.48	201.45	-431.17
			130	-310.18	0.15	-5.17	-13.48	477.15	-415.37
745	Copertura	38	0	395.16	0.09	13.97	-15.68	-61.66	-429.39
			65	395.16	0.09	3.78	-15.68	216.85	-426.66
			130	395.16	0.09	-6.41	-15.68	491.82	-418.49
746	Copertura	39	0	-313.89	0.19	12.78	-14.06	-80.54	-431.74
			65	-313.89	0.19	3.64	-14.06	198.95	-426.47
			130	-313.89	0.19	-5.49	-14.06	471.59	-410.67
747	Copertura	40	0	405.06	-0.02	14.85	-16.84	-59.49	-425.58
			65	405.06	-0.02	3.91	-16.84	216.55	-422.86
			130	405.06	-0.02	-7.04	-16.84	489.04	-414.68
748	Copertura	41	0	-302.02	0.13	9.75	-10.95	-79.23	-429.26
			65	-302.02	0.13	2.63	-10.95	198.64	-423.99
			130	-302.02	0.13	-4.49	-10.95	469.67	-408.19
749	Copertura	42	0	436.86	0.06	16.37	-18.76	-53.07	-420.35
			65	436.86	0.06	4.17	-18.76	219.77	-418.56
			130	436.86	0.06	-8.02	-18.76	490.29	-413.20
750	Copertura	43	0	437.30	0.30	0.56	-0.08	-54.02	-419.28
			65	437.30	0.30	0.51	-0.08	218.14	-417.55
			130	437.30	0.30	0.46	-0.08	488.04	-412.34
751	Copertura	44	0	-301.07	0.21	7.16	-6.55	-84.29	-432.65
			65	-301.07	0.21	2.91	-6.55	195.79	-427.38
			130	-301.07	0.21	-1.35	-6.55	469.03	-411.58
752	Copertura	45	0	402.80	0.56	0.23	0.24	-60.55	-411.27
			65	402.80	0.56	0.39	0.24	206.21	-408.64
			130	402.80	0.56	0.54	0.24	469.54	-400.74
753	Copertura	46	0	-296.16	0.03	3.31	-2.32	-80.77	-415.62
			65	-296.16	0.03	1.81	-2.32	188.24	-410.36
			130	-296.16	0.03	0.30	-2.32	450.41	-394.55
754	Copertura	47	0	361.54	0.83	0.07	0.39	-59.19	-387.76
			65	361.54	0.83	0.32	0.39	192.28	-385.12
			130	361.54	0.83	0.57	0.39	440.33	-377.22
755	Copertura	48	0	-275.02	0.84	3.97	-3.38	-79.09	-393.96
			65	-275.02	0.84	1.77	-3.38	175.85	-388.70
			130	-275.02	0.84	-0.43	-3.38	423.93	-372.89
756	Copertura	49	0	322.77	1.35	-0.19	0.74	-55.58	-351.69
			65	322.77	1.35	0.30	0.74	172.45	-349.06
			130	322.77	1.35	0.78	0.74	397.05	-341.16
757	Copertura	50	0	-236.65	0.51	3.56	-2.54	-75.18	-356.84
			65	-236.65	0.51	1.91	-2.54	155.63	-351.57
			130	-236.65	0.51	0.25	-2.54	379.58	-335.77
758	Copertura	51	0	239.39	2.02	-0.43	1.20	-50.68	-294.75
			65	239.39	2.02	0.35	1.20	140.34	-292.11
			130	239.39	2.02	1.13	1.20	327.92	-284.21
759	Copertura	52	0	-159.50	1.92	4.24	-3.83	-71.24	-300.07

			65	-159.50	1.92	1.75	-3.83	122.66	-294.80
			130	-159.50	1.92	-0.74	-3.83	309.72	-279.00
760	Copertura	53	0	136.58	2.65	-0.53	1.54	-43.95	-215.77
			65	136.58	2.65	0.47	1.54	95.73	-213.13
			130	136.58	2.65	1.47	1.54	231.98	-205.23
761	Copertura	54	0	-45.56	1.25	2.90	-1.78	-64.00	-218.53
			65	-45.56	1.25	1.75	-1.78	76.90	-213.27
			130	-45.56	1.25	0.59	-1.78	210.96	-197.46
762	Copertura	55	0	61.00	2.76	0.06	1.10	-34.66	-133.17
			65	61.00	2.76	0.77	1.10	51.29	-130.34
			130	61.00	2.76	1.49	1.10	133.57	-121.86
763	Copertura	56	0	12.16	1.60	3.31	-2.57	-55.64	-144.54
			65	12.16	1.60	1.64	-2.57	37.08	-138.88
			130	12.16	1.60	-0.03	-2.57	122.46	-121.92
764	Copertura	70	0	-235.11	0.20	4.19	-1.83	34.11	-30.32
			95	-235.11	0.20	2.45	-1.83	60.05	-21.26
			190	-235.11	0.20	0.71	-1.83	68.77	5.92
765	Copertura	81	0	7.74	-3.76	1.72	-2.17	187.95	-86.78
			80	7.74	-3.76	-0.01	-2.17	233.24	-26.46
			160	7.74	-3.76	-1.75	-2.17	230.29	33.85
766	Copertura	126	0	4.26	2.55	0.95	-3.15	128.62	-121.57
			30	4.26	2.55	0.00	-3.15	161.70	-98.96
			60	4.26	2.55	-0.94	-3.15	187.99	-76.34
767	Copertura	98	0	33.64	-1.31	1.67	-2.50	287.19	-68.34
			82	33.64	-1.31	-0.39	-2.50	319.64	-10.50
			165	33.64	-1.31	-2.45	-2.50	304.48	47.34
768	Copertura	99	0	43.64	-3.77	1.36	-1.78	371.77	-33.42
			82	43.64	-3.77	-0.10	-1.78	375.48	24.41
			165	43.64	-3.77	-1.57	-1.78	331.56	82.25
769	Copertura	100	0	36.99	-0.75	1.13	-1.60	438.69	-2.80
			82	36.99	-0.75	-0.18	-1.60	417.18	55.04
			165	36.99	-0.75	-1.50	-1.60	348.05	112.87
770	Copertura	101	0	52.25	-2.06	1.52	-2.19	480.35	14.68
			82	52.25	-2.06	-0.28	-2.19	444.45	72.51
			165	52.25	-2.06	-2.09	-2.19	360.93	130.35
771	Copertura	102	0	57.70	-0.08	-0.69	0.16	506.48	24.65
			82	57.70	-0.08	-0.56	0.16	462.37	82.48
			165	57.70	-0.08	-0.42	0.16	370.64	140.32
772	Copertura	103	0	60.87	-0.78	0.78	-1.45	518.73	30.41
			82	60.87	-0.78	-0.41	-1.45	469.88	88.24
			165	60.87	-0.78	-1.61	-1.45	373.40	146.08
773	Copertura	104	0	54.66	0.29	-2.48	2.20	523.99	31.58
			82	54.66	0.29	-0.67	2.20	474.18	89.41
			165	54.66	0.29	1.14	2.20	376.74	147.25
774	Copertura	105	0	57.41	-0.07	-1.86	1.16	523.72	31.01
			82	57.41	-0.07	-0.90	1.16	474.37	88.85
			165	57.41	-0.07	0.05	1.16	377.39	146.69
775	Copertura	111	0	60.36	0.22	-2.66	2.19	518.17	32.96
			80	60.36	0.22	-0.91	2.19	469.54	88.98
			160	60.36	0.22	0.84	2.19	376.22	145.01
776	Copertura	112	0	59.82	0.14	-2.68	1.97	514.69	27.53
			82	59.82	0.14	-1.06	1.97	468.21	85.37
			165	59.82	0.14	0.56	1.97	374.09	143.21
777	Copertura	113	0	62.07	0.19	-2.97	2.28	508.87	25.07
			82	62.07	0.19	-1.09	2.28	464.41	82.91
			165	62.07	0.19	0.78	2.28	372.33	140.75
778	Copertura	114	0	57.57	0.29	-3.31	2.89	504.53	22.62
			82	57.57	0.29	-0.93	2.89	462.09	80.46
			165	57.57	0.29	1.45	2.89	372.03	138.30
779	Copertura	115	0	59.76	0.14	0.51	-1.26	503.27	21.77
			82	59.76	0.14	-0.52	-1.26	461.53	79.61
			165	59.76	0.14	-1.56	-1.26	372.16	137.45
780	Copertura	116	0	71.22	-0.14	-2.33	1.66	501.98	21.82
			82	71.22	-0.14	-0.96	1.66	460.20	79.66
			165	71.22	-0.14	0.41	1.66	370.80	137.49
781	Copertura	117	0	46.60	1.11	1.87	-2.97	485.56	15.81
			82	46.60	1.11	-0.58	-2.97	448.72	73.65
			165	46.60	1.11	-3.03	-2.97	364.26	131.49
782	Copertura	118	0	48.56	0.12	1.45	-2.21	462.96	6.97
			82	48.56	0.12	-0.37	-2.21	433.40	64.81
			165	48.56	0.12	-2.18	-2.21	356.22	122.65
783	Copertura	131	0	36.64	-1.46	0.90	-2.16	232.01	-113.63

			30	36.64	-1.46	0.25	-2.16	262.94	-92.56
			60	36.64	-1.46	-0.39	-2.16	287.55	-71.49
784	Copertura	133	0	40.64	0.54	0.73	-2.12	340.61	-72.41
			30	40.64	0.54	0.09	-2.12	359.17	-51.34
			60	40.64	0.54	-0.54	-2.12	371.41	-30.27
785	Copertura	139	0	40.08	-1.37	0.35	-2.06	423.61	-46.50
			30	40.08	-1.37	-0.27	-2.06	434.40	-25.43
			60	40.08	-1.37	-0.89	-2.06	438.87	-4.36
786	Copertura	143	0	49.16	0.62	0.51	-1.73	477.26	-25.91
			30	49.16	0.62	-0.01	-1.73	481.88	-4.84
			60	49.16	0.62	-0.53	-1.73	480.17	16.23
787	Copertura	147	0	60.74	-0.74	-0.47	-3.86	508.42	-17.94
			30	60.74	-0.74	-1.63	-3.86	510.64	3.13
			60	60.74	-0.74	-2.79	-3.86	506.54	24.20
788	Copertura	151	0	57.83	0.47	-2.66	2.57	524.53	-11.29
			30	57.83	0.47	-1.89	2.57	524.76	9.78
			60	57.83	0.47	-1.12	2.57	518.67	30.85
789	Copertura	155	0	57.40	-0.19	-4.95	1.18	530.38	-10.41
			30	57.40	-0.19	-4.59	1.18	530.34	10.66
			60	57.40	-0.19	-4.24	1.18	523.98	31.73
790	Copertura	159	0	54.67	0.20	-5.02	2.18	529.60	-11.29
			30	54.67	0.20	-4.36	2.18	529.82	9.79
			60	54.67	0.20	-3.71	2.18	523.72	30.86
791	Copertura	119	0	29.74	2.74	1.51	-2.37	424.07	-9.91
			82	29.74	2.74	-0.44	-2.37	408.42	47.93
			165	29.74	2.74	-2.39	-2.37	345.14	105.77
792	Copertura	120	0	38.13	1.13	1.57	-2.34	366.10	-35.11
			82	38.13	1.13	-0.36	-2.34	371.19	22.73
			165	38.13	1.13	-2.29	-2.34	328.66	80.57
793	Copertura	121	0	38.75	4.42	1.67	-2.67	279.39	-73.06
			82	38.75	4.42	-0.52	-2.67	315.74	-15.22
			165	38.75	4.42	-2.72	-2.67	304.47	42.61
794	Copertura	122	0	18.27	-0.24	0.42	-0.35	193.51	-79.40
			82	18.27	-0.24	0.13	-0.35	233.33	-17.32
			165	18.27	-0.24	-0.16	-0.35	222.03	44.76
795	Copertura	123	0	-235.11	0.20	0.71	-1.83	68.77	5.92
			82	-235.11	0.20	-0.80	-1.83	50.24	39.08
			165	-235.11	0.20	-2.31	-1.83	4.40	72.24
796	Copertura	163	0	63.28	-0.06	-5.73	1.82	524.83	-12.53
			33	63.28	-0.06	-5.14	1.82	525.18	10.35
			65	63.28	-0.06	-4.54	1.82	518.08	33.24
797	Copertura	167	0	56.89	0.05	-6.08	2.34	518.47	-14.89
			30	56.89	0.05	-5.38	2.34	519.78	6.18
			60	56.89	0.05	-4.68	2.34	514.76	27.25
798	Copertura	171	0	65.14	0.05	-6.54	2.48	511.38	-16.84
			30	65.14	0.05	-5.79	2.48	513.27	4.23
			60	65.14	0.05	-5.05	2.48	508.84	25.30
799	Copertura	174	0	54.50	0.12	-6.91	2.69	505.36	-19.75
			30	54.50	0.12	-6.10	2.69	508.12	1.32
			60	54.50	0.12	-5.29	2.69	504.57	22.39
800	Copertura	179	0	63.75	0.04	-6.05	6.94	503.57	-20.55
			30	63.75	0.04	-3.97	6.94	506.57	0.52
			60	63.75	0.04	-1.88	6.94	503.26	21.59
801	Copertura	183	0	67.24	0.20	-1.27	-6.53	502.55	-20.15
			30	67.24	0.20	-3.23	-6.53	505.43	0.93
			60	67.24	0.20	-5.19	-6.53	501.99	22.00
802	Copertura	187	0	51.63	-0.52	-0.03	-2.49	482.71	-25.67
			30	51.63	-0.52	-0.77	-2.49	487.25	-4.60
			60	51.63	-0.52	-1.52	-2.49	485.47	16.47
803	Copertura	191	0	43.53	0.88	-0.19	-2.70	454.19	-35.83
			30	43.53	0.88	-1.00	-2.70	461.78	-14.76
			60	43.53	0.88	-1.81	-2.70	463.05	6.31
804	Copertura	194	0	34.85	-0.72	-0.43	-2.47	406.52	-49.90
			30	34.85	-0.72	-1.17	-2.47	418.33	-28.83
			60	34.85	-0.72	-1.91	-2.47	423.82	-7.76
805	Copertura	198	0	33.02	1.75	-0.42	-2.24	331.36	-79.40
			30	33.02	1.75	-1.09	-2.24	352.01	-58.33
			60	33.02	1.75	-1.76	-2.24	366.35	-37.26
806	Copertura	203	0	42.95	-0.84	-0.51	-1.24	225.19	-110.97
			30	42.95	-0.84	-0.88	-1.24	255.31	-89.90
			60	42.95	-0.84	-1.25	-1.24	279.12	-68.82
807	Copertura	207	0	14.07	-0.58	-1.12	-1.78	130.02	-128.87

			30	14.07	-0.58	-1.66	-1.78	165.29	-106.25
			60	14.07	-0.58	-2.19	-1.78	193.78	-83.64

1.1.10.2 Piastre SLU

Tabella 20.I

Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	-4.392	-0.678	-0.720	913.452	133.901	-103.022	-11.385	2.496
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	-5.233	-1.057	-1.031	1121.632	264.081	154.517	-14.686	-4.817
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	-4.177	-0.465	0.752	829.385	115.079	-130.399	-10.688	2.696

1.1.11 Risultati Condizioni (Vento (+Y)).

1.1.11.1 Sollecitazioni SLU

Tabella 21.I

Sollecitazioni									
Asta	Imp.	Fili	X [cm]	N [daN]	Mt [daNm]	Mxz [daNm]	Txz [daN]	Mxy [daNm]	Txy [daN]
1	Fondazione	1, 2	0	-38.60	-28.08	-8.82	216.72	19.08	38.69
			42	-38.46	-28.07	60.22	118.74	3.00	39.00
			83	-38.44	-28.05	91.58	34.99	-13.61	41.27
2	Fondazione	1, 2	0	-17.61	117.77	90.67	23.27	-13.63	-42.58
			42	-17.72	117.78	84.86	-48.95	3.26	-38.40
			83	-17.96	117.79	50.89	-112.77	18.03	-32.33
3	Fondazione	1, 15	0	-57.34	65.43	-9.70	307.13	1.30	-0.70
			40	-48.94	65.43	92.35	219.29	1.55	-0.61
			80	-40.56	65.42	164.54	156.35	1.80	-0.64
4	Fondazione	1, 15	0	-7.62	73.66	127.53	114.14	1.78	-9.35
			40	0.75	73.65	162.27	72.32	5.52	-9.51
			80	9.11	73.65	183.83	46.94	9.35	-9.76
5	Fondazione	2, 3	0	-27.54	-11.97	112.66	-53.44	20.61	60.01
			35	-27.48	-11.96	85.66	-102.68	-0.62	63.07
			69	-27.42	-11.95	41.86	-151.18	-22.91	66.12
6	Fondazione	2, 3	0	-20.88	245.37	98.94	-154.79	-22.92	-73.01
			35	-20.84	245.39	37.08	-204.03	1.75	-70.01
			69	-20.80	245.40	-42.08	-255.22	25.40	-67.11
7	Fondazione	3, 4	0	-12.88	-75.65	15.84	36.30	29.47	80.49

			35	-12.85	-75.63	19.22	-17.05	1.21	83.36
			69	-12.83	-75.62	3.79	-72.82	-28.05	86.25
8	Fondazio ne	3, 4	0	-10.89	266.64	55.93	-119.75	-28.05	-84.86
			35	-10.86	266.66	4.60	-178.33	0.73	-82.00
			69	-10.85	266.68	-67.50	-240.15	28.54	-79.22
9	Fondazio ne	4, 5	0	-5.92	-128.60	-24.98	97.35	31.52	86.58
			35	-5.91	-128.58	-2.48	32.68	1.17	89.34
			69	-5.89	-128.56	-2.72	-34.50	-30.13	92.14
10	Fondazio ne	4, 5	0	-3.21	266.59	33.61	-80.58	-30.13	-89.42
			35	-3.20	266.61	-6.15	-150.34	0.24	-86.63
			69	-3.19	266.63	-70.44	-222.80	29.65	-83.92
11	Fondazio ne	5, 6	0	0.02	-168.88	-39.68	135.92	31.81	88.24
			35	0.03	-168.86	-5.61	61.30	0.90	90.94
			69	0.04	-168.84	2.42	-14.99	-30.95	93.69
12	Fondazio ne	5, 6	0	-0.12	264.27	26.38	-59.32	-30.95	-84.56
			35	-0.11	264.29	-7.49	-137.34	-2.25	-81.82
			69	-0.10	264.31	-68.59	-217.17	25.52	-79.15
13	Fondazio ne	6, 7	0	-0.99	-205.77	-50.25	170.14	36.56	96.61
			35	-0.98	-205.75	-5.51	89.09	2.78	99.26
			69	-0.97	-205.73	11.14	7.33	-31.93	101.96
14	Fondazio ne	6, 7	0	-0.86	253.66	23.19	-34.80	-31.93	-101.46
			35	-0.85	253.68	-3.03	-117.34	2.61	-98.77
			69	-0.85	253.71	-57.89	-200.83	36.23	-96.14
15	Fondazio ne	7, 8	0	0.89	-230.08	-59.15	191.15	26.76	81.52
			35	0.90	-230.06	-7.68	107.24	-1.82	84.16
			69	0.91	-230.03	14.86	23.46	-31.32	86.87
16	Fondazio ne	7, 8	0	-3.88	234.52	20.54	-22.43	-31.32	-93.04
			35	-3.87	234.54	-1.64	-106.16	0.31	-90.34
			69	-3.86	234.57	-52.72	-189.99	31.02	-87.69
17	Fondazio ne	8, 9	0	5.11	-247.68	-68.83	208.89	30.48	84.25
			35	5.11	-247.65	-11.19	125.44	0.95	86.89
			69	5.12	-247.63	17.84	43.02	-29.49	89.60
18	Fondazio ne	8, 9	0	-11.40	199.60	9.01	11.58	-29.49	-81.29
			35	-11.39	199.62	-1.06	-69.84	-1.91	-78.57
			69	-11.39	199.65	-39.07	-150.36	24.74	-75.91
19	Fondazio ne	9, 10	0	4.91	-260.25	-61.92	205.84	32.64	86.71
			35	4.91	-260.22	-4.62	126.60	2.27	89.36
			69	4.91	-260.20	25.64	49.14	-29.02	92.07
20	Fondazio ne	9, 10	0	-13.51	157.83	4.39	10.00	-29.02	-95.07
			35	-13.51	157.85	-5.29	-65.82	3.31	-92.35
			69	-13.51	157.87	-40.85	-140.04	34.70	-89.66
21	Fondazio ne	10, 11	0	0.96	-270.28	-77.69	233.61	23.46	73.59
			35	0.95	-270.26	-9.61	161.47	-2.39	76.30
			69	0.95	-270.24	34.04	92.07	-29.19	79.08
22	Fondazio ne	10, 11	0	-12.53	117.23	-2.71	35.30	-29.19	-89.97
			35	-12.54	117.25	-2.12	-31.47	1.37	-87.17
			69	-12.55	117.27	-24.13	-95.68	30.96	-84.41
23	Fondazio ne	11, 12	0	-10.42	-264.57	-70.63	238.56	27.90	77.45
			35	-10.44	-264.55	1.00	177.26	0.70	80.23
			69	-10.46	-264.53	52.06	119.30	-27.47	83.10
24	Fondazio ne	11, 12	0	-20.69	64.99	1.83	69.12	-27.47	-84.88
			35	-20.72	65.00	16.12	14.16	1.32	-81.99
			69	-20.76	65.02	11.91	-38.14	29.11	-79.11
25	Fondazio ne	12, 13	0	-25.28	-243.06	-42.67	249.23	25.03	66.32
			35	-25.32	-243.04	34.66	199.40	1.65	69.23

			69	-25.38	-243.03	95.20	151.85	-22.75	72.24
26	Fondazio ne	12, 13	0	-37.97	11.43	39.77	132.95	-22.74	-67.22
			35	-38.04	11.45	77.63	86.56	-0.08	-64.16
			69	-38.12	11.46	99.50	39.94	21.53	-61.09
27	Fondazio ne	13, 14	0	-15.93	-125.05	47.76	109.12	19.06	34.01
			42	-15.72	-125.04	81.04	49.44	3.60	40.10
			83	-15.63	-125.03	88.13	-17.39	-14.01	44.31
28	Fondazio ne	13, 14	0	-40.76	17.79	77.88	-15.33	-13.99	-40.67
			42	-40.79	17.80	56.06	-92.25	2.37	-38.36
			83	-40.96	17.81	-0.26	-181.72	18.17	-37.99
29	Fondazio ne	14, 16	0	-54.38	-53.71	7.84	248.70	-0.78	1.66
			40	-46.03	-53.71	88.29	168.51	-1.41	1.54
			80	-37.71	-53.70	141.39	110.64	-2.03	1.56
30	Fondazio ne	14, 16	0	-10.73	-64.67	119.98	84.85	-2.00	8.36
			40	-2.42	-64.67	143.72	45.83	-5.35	8.50
			80	5.88	-64.67	155.01	21.47	-8.78	8.75
31	Fondazio ne	15, 17	0	-38.83	-11.95	172.67	-108.23	7.17	12.46
			33	-31.90	-11.96	133.35	-120.59	3.10	12.21
			66	-24.97	-11.96	90.84	-127.99	-0.88	11.94
32	Fondazio ne	15, 17	0	-18.35	14.87	86.11	-158.60	-0.88	-4.66
			33	-11.43	14.87	31.59	-163.02	0.70	-4.93
			66	-4.52	14.87	-24.05	-165.50	2.37	-5.21
33	Fondazio ne	16, 18	0	-35.74	9.10	147.11	-82.87	-6.90	-12.05
			33	-28.85	9.11	116.18	-95.24	-2.96	-11.80
			66	-21.97	9.11	81.98	-103.03	0.88	-11.53
34	Fondazio ne	16, 18	0	-18.75	-17.19	74.74	-125.80	0.89	5.26
			33	-11.88	-17.19	30.97	-130.73	-0.90	5.55
			66	-5.01	-17.19	-14.09	-133.76	-2.78	5.84
35	Fondazio ne	17, 19	0	-74.87	18.43	-23.14	90.92	1.51	2.36
			33	-67.96	18.43	5.32	90.23	0.78	2.07
			66	-61.09	18.43	33.86	91.44	0.15	1.79
36	Fondazio ne	17, 19	0	-48.79	23.15	12.92	82.89	0.15	0.63
			33	-41.93	23.15	39.32	85.70	-0.02	0.35
			66	-35.09	23.15	66.86	89.60	-0.09	0.08
37	Fondazio ne	18, 20	0	-64.26	-14.23	-16.19	76.93	-2.02	-3.44
			33	-57.40	-14.23	7.55	75.59	-0.93	-3.13
			66	-50.56	-14.23	31.14	75.97	0.05	-2.83
38	Fondazio ne	18, 20	0	-42.68	-22.00	13.54	68.25	0.05	0.33
			33	-35.86	-22.00	34.96	70.06	-0.11	0.63
			66	-29.06	-22.00	57.15	72.81	-0.37	0.94
39	Fondazio ne	19, 21	0	-91.87	8.69	67.72	-98.98	-0.15	-0.82
			33	-85.05	8.68	34.37	-94.90	0.16	-1.08
			66	-78.26	8.68	2.29	-91.51	0.56	-1.35
40	Fondazio ne	19, 21	0	-61.66	5.02	-0.63	-88.48	0.57	1.22
			33	-54.90	5.02	-30.76	-86.08	0.20	0.97
			66	-48.16	5.02	-60.23	-84.42	-0.07	0.72
41	Fondazio ne	20, 22	0	-80.36	-7.24	58.19	-83.26	-0.26	-0.25
			33	-73.58	-7.24	29.84	-80.35	-0.23	0.05
			66	-66.81	-7.24	2.38	-78.03	-0.29	0.35
42	Fondazio ne	20, 22	0	-54.40	-5.84	-0.32	-75.34	-0.29	-0.43
			33	-47.66	-5.84	-26.27	-73.88	-0.20	-0.14
			66	-40.94	-5.84	-51.85	-73.06	-0.20	0.15
43	Fondazio ne	21, 23	0	-102.73	21.29	-55.90	91.59	0.00	-0.50
			33	-96.02	21.29	-26.75	93.29	0.20	-0.74
			66	-89.34	21.29	3.07	95.71	0.48	-0.97

44	Fondazio ne	21, 23	0	-68.10	16.05	-11.74	106.62	0.49	1.17
			33	-61.45	16.05	22.64	110.03	0.14	0.95
			66	-54.82	16.05	58.31	114.28	-0.14	0.74
45	Fondazio ne	22, 24	0	-88.90	-16.72	-48.31	82.76	-0.27	-0.37
			33	-82.20	-16.72	-22.21	83.58	-0.19	-0.09
			66	-75.53	-16.72	4.25	85.02	-0.21	0.19
46	Fondazio ne	22, 24	0	-59.59	-14.63	-7.39	89.10	-0.21	-0.32
			33	-52.94	-14.63	21.03	91.34	-0.15	-0.06
			66	-46.32	-14.63	50.31	94.23	-0.17	0.20
47	Fondazio ne	23, 25	0	-112.76	-2.29	67.31	-120.40	-0.08	-0.66
			33	-106.16	-2.29	26.99	-116.00	0.17	-0.87
			66	-99.60	-2.29	-11.95	-112.20	0.49	-1.06
48	Fondazio ne	23, 25	0	-78.54	-4.17	-8.97	-105.49	0.49	-2.98
			33	-72.01	-4.17	-44.56	-102.44	1.51	-3.16
			66	-65.50	-4.17	-79.22	-99.67	2.58	-3.32
49	Fondazio ne	24, 26	0	-94.24	2.70	57.56	-90.70	-0.20	-0.28
			33	-87.64	2.70	26.80	-87.78	-0.15	-0.02
			66	-81.07	2.70	-3.08	-85.50	-0.18	0.22
50	Fondazio ne	24, 26	0	-65.53	5.27	1.28	-77.90	-0.19	3.03
			33	-58.99	5.27	-25.48	-76.50	-1.22	3.26
			66	-52.46	5.27	-51.89	-75.75	-2.33	3.48
51	Fondazio ne	25, 26	0	8.21	-7.41	-5.49	12.59	7.16	18.63
			49	7.99	-7.41	1.70	16.65	0.41	9.09
			97	7.77	-7.41	10.72	20.12	-1.71	-0.36
52	Fondazio ne	25, 26	0	11.65	-3.30	1.13	-2.57	-1.68	6.48
			49	11.44	-3.30	0.60	0.07	-2.55	-2.89
			97	11.24	-3.30	1.12	1.76	1.12	-12.21
53	Fondazio ne	25, 26	0	12.43	-3.83	-2.60	-1.11	1.13	9.45
			49	12.24	-3.83	-2.88	-0.38	-1.21	0.17
			97	12.06	-3.83	-3.02	-0.47	0.96	-9.08
54	Fondazio ne	25, 26	0	14.61	-1.87	-3.34	1.39	0.97	9.02
			49	14.44	-1.87	-2.80	0.63	-1.17	-0.21
			97	14.28	-1.87	-2.75	-0.62	1.17	-9.41
55	Fondazio ne	25, 26	0	16.85	-0.69	-2.37	2.21	1.17	9.06
			49	16.71	-0.69	-1.64	0.62	-1.00	-0.13
			97	16.57	-0.69	-1.75	-1.19	1.29	-9.31
56	Fondazio ne	25, 26	0	19.13	-0.15	-1.38	2.31	1.30	9.10
			49	19.01	-0.15	-0.70	0.36	-0.90	-0.07
			97	18.91	-0.16	-0.99	-1.66	1.36	-9.23
57	Fondazio ne	25, 26	0	21.10	0.04	-0.76	2.20	1.36	9.12
			49	21.02	0.04	-0.17	0.14	-0.84	-0.05
			97	20.94	0.04	-0.59	-1.93	1.41	-9.20
58	Fondazio ne	25, 26	0	22.68	0.08	-0.48	2.10	1.41	9.09
			49	22.62	0.08	0.05	0.04	-0.79	-0.07
			97	22.59	0.08	-0.42	-2.01	1.48	-9.23
59	Fondazio ne	25, 26	0	23.78	0.09	-0.39	2.08	1.48	9.28
			49	23.76	0.09	0.13	0.05	-0.81	0.12
			97	23.76	0.09	-0.33	-1.96	1.36	-9.03
60	Fondazio ne	25, 26	0	24.24	-0.23	-0.33	1.96	1.36	9.00
			49	24.26	-0.23	0.14	-0.02	-0.80	-0.16
			97	24.30	-0.23	-0.36	-1.98	1.51	-9.32
61	Fondazio ne	25, 26	0	24.64	-0.04	-0.50	2.03	1.51	9.26
			49	24.70	-0.04	0.00	0.10	-0.77	0.10
			97	24.77	-0.04	-0.43	-1.79	1.42	-9.07
62	Fondazio	25, 26	0	24.34	-0.10	-0.47	1.96	1.42	9.17

	ne								
			49	24.43	-0.10	0.02	0.11	-0.81	0.00
			97	24.55	-0.10	-0.39	-1.68	1.42	-9.18
63	Fondazio ne	25, 26	0	23.53	-0.09	-0.50	1.85	1.42	9.25
			49	23.66	-0.09	-0.05	0.12	-0.85	0.06
			97	23.81	-0.09	-0.43	-1.54	1.36	-9.13
64	Fondazio ne	25, 26	0	22.10	-0.07	-0.60	1.68	1.36	9.28
			49	22.27	-0.07	-0.21	0.10	-0.92	0.08
			97	22.46	-0.07	-0.56	-1.37	1.28	-9.13
65	Fondazio ne	25, 26	0	19.94	0.00	-0.82	1.51	1.28	9.30
			49	20.15	0.00	-0.46	0.15	-1.01	0.08
			97	20.37	0.00	-0.73	-1.05	1.20	-9.15
66	Fondazio ne	25, 26	0	17.22	0.13	-1.06	0.96	1.20	9.42
			49	17.46	0.13	-0.90	-0.06	-1.14	0.16
			97	17.71	0.13	-1.17	-0.84	1.04	-9.11
67	Fondazio ne	25, 26	0	14.12	0.24	-1.78	1.04	1.03	9.13
			49	14.38	0.24	-1.46	0.56	-1.15	-0.18
			97	14.65	0.24	-1.28	0.47	1.21	-9.52
68	Fondazio ne	25, 26	0	10.93	0.30	0.48	3.74	1.20	11.34
			49	11.22	0.30	2.31	4.08	-2.04	1.96
			97	11.51	0.30	4.40	4.81	-0.70	-7.47
69	Fondazio ne	25, 26	0	7.86	1.82	8.81	-18.27	-0.72	2.61
			49	8.16	1.82	0.07	-17.38	0.32	-6.89
			97	8.47	1.82	-8.24	-16.50	6.01	-16.47
70	Fondazio ne	25, 28	0	-127.62	19.56	-65.90	72.57	-4.55	-6.37
			43	-119.29	19.56	-35.78	77.40	-1.81	-6.55
			85	-111.04	19.56	-2.97	85.39	1.01	-6.71
71	Fondazio ne	25, 28	0	-84.07	18.67	-12.11	92.94	1.01	1.61
			43	-75.87	18.67	28.14	104.87	0.36	1.45
			85	-67.73	18.67	74.27	120.36	-0.22	1.31
72	Fondazio ne	26, 27	0	-87.24	-7.20	-43.12	71.87	3.68	5.68
			33	-80.74	-7.20	-20.59	72.60	1.77	5.89
			66	-74.28	-7.20	2.26	73.86	-0.21	6.08
73	Fondazio ne	26, 27	0	-55.28	-5.94	-3.93	78.15	-0.21	-0.05
			33	-48.83	-5.94	20.88	80.13	-0.22	0.14
			66	-42.41	-5.94	46.44	82.65	-0.30	0.32
74	Fondazio ne	27, 29	0	-84.92	7.85	57.81	-92.39	-0.27	-0.64
			33	-78.52	7.84	26.47	-89.91	-0.09	-0.47
			66	-72.14	7.84	-4.16	-88.15	0.04	-0.30
75	Fondazio ne	27, 29	0	-52.65	8.31	3.45	-86.04	0.03	0.10
			33	-46.29	8.31	-26.05	-85.23	-0.02	0.25
			66	-39.96	8.31	-55.41	-85.13	-0.13	0.40
76	Fondazio ne	28, 30	0	-149.33	-2.24	86.16	-103.67	-0.19	0.78
			37	-142.38	-2.24	49.61	-88.91	-0.46	0.67
			73	-135.50	-2.24	18.46	-74.41	-0.68	0.57
77	Fondazio ne	28, 30	0	-118.62	-13.12	23.05	-49.32	-0.68	-0.54
			37	-111.79	-13.12	6.17	-35.91	-0.47	-0.63
			73	-105.01	-13.12	-6.06	-23.95	-0.22	-0.72
78	Fondazio ne	29, 31	0	-80.51	-5.01	-44.40	74.20	-0.11	-0.45
			33	-74.19	-5.01	-21.18	74.24	0.01	-0.32
			66	-67.91	-5.01	2.13	74.79	0.10	-0.19
79	Fondazio ne	29, 31	0	-47.71	-5.48	-3.59	74.03	0.09	0.21
			33	-41.45	-5.48	19.77	75.28	0.00	0.33
			66	-35.20	-5.48	43.65	77.07	-0.12	0.44
80	Fondazio ne	30, 32	0	-102.94	-11.02	15.30	-39.91	-0.23	-0.19

			34	-96.62	-11.02	2.09	-30.06	-0.15	-0.28
			69	-90.34	-11.02	-7.98	-21.65	-0.04	-0.36
81	Fondazio ne	30, 32	0	-84.27	-10.01	-1.14	-24.07	-0.04	0.07
			34	-78.02	-10.01	-9.40	-17.05	-0.05	-0.01
			69	-71.80	-10.01	-15.46	-11.31	-0.03	-0.09
82	Fondazio ne	31, 33	0	-75.94	6.60	54.95	-88.50	-0.13	-0.53
			33	-69.71	6.60	24.81	-86.73	0.03	-0.43
			66	-63.50	6.60	-4.85	-85.61	0.16	-0.34
83	Fondazio ne	31, 33	0	-43.69	7.71	2.09	-83.01	0.16	0.42
			33	-37.50	7.71	-26.47	-82.74	0.00	0.51
			66	-31.33	7.71	-55.06	-83.10	-0.18	0.58
84	Fondazio ne	32, 34	0	-74.49	-7.04	4.12	-18.27	-0.04	0.02
			35	-68.26	-7.04	-2.59	-13.59	-0.04	-0.06
			69	-62.05	-7.04	-7.86	-9.95	0.00	-0.15
85	Fondazio ne	32, 34	0	-57.53	-6.20	-3.24	-10.20	0.00	0.03
			35	-51.34	-6.20	-7.51	-7.52	0.00	-0.05
			69	-45.18	-6.20	-11.00	-5.68	0.03	-0.13
86	Fondazio ne	33, 35	0	-71.11	-5.98	-45.17	74.61	-0.16	-0.60
			33	-64.96	-5.98	-21.84	74.30	0.02	-0.53
			66	-58.82	-5.98	1.48	74.62	0.19	-0.48
87	Fondazio ne	33, 35	0	-38.53	-6.49	-4.50	72.81	0.19	0.45
			33	-32.42	-6.49	18.47	73.96	0.03	0.49
			66	-26.32	-6.49	41.95	75.80	-0.14	0.54
88	Fondazio ne	34, 36	0	-49.74	-5.04	5.58	-9.33	0.03	0.17
			35	-43.59	-5.04	1.35	-8.19	-0.01	0.08
			69	-37.46	-5.04	-2.61	-7.76	-0.03	0.00
89	Fondazio ne	34, 36	0	-34.59	-5.25	0.57	-7.98	-0.03	-0.04
			35	-28.48	-5.25	-3.43	-8.26	0.00	-0.13
			69	-22.37	-5.25	-7.65	-9.22	0.06	-0.21
90	Fondazio ne	35, 37	0	-66.56	4.81	52.75	-85.71	-0.13	-0.48
			33	-60.47	4.81	23.59	-83.71	0.02	-0.45
			66	-54.41	4.81	-4.98	-82.17	0.17	-0.42
91	Fondazio ne	35, 37	0	-34.86	6.29	0.12	-80.71	0.16	0.33
			33	-28.81	6.29	-27.56	-79.80	0.05	0.34
			66	-22.77	6.29	-55.01	-79.26	-0.06	0.35
92	Fondazio ne	36, 38	0	-26.19	-5.22	8.46	-4.69	0.06	0.16
			35	-20.10	-5.22	5.37	-6.26	0.02	0.08
			69	-14.01	-5.22	1.63	-8.53	0.01	0.00
93	Fondazio ne	36, 38	0	-10.80	-5.99	5.05	-8.92	0.01	-0.06
			35	-4.72	-5.99	0.26	-11.98	0.04	-0.15
			69	1.36	-5.99	-5.74	-15.86	0.11	-0.23
94	Fondazio ne	37, 39	0	-63.57	-9.30	-46.71	81.60	-0.03	-0.23
			33	-57.54	-9.30	-20.87	82.44	0.04	-0.23
			66	-51.54	-9.30	5.39	84.16	0.12	-0.24
95	Fondazio ne	37, 39	0	-32.53	-8.61	-1.77	83.18	0.12	-0.09
			33	-26.54	-8.61	24.91	85.95	0.15	-0.10
			66	-20.56	-8.61	52.65	89.54	0.19	-0.12
96	Fondazio ne	38, 40	0	-1.67	-7.40	11.31	-5.85	0.11	0.15
			34	4.36	-7.40	7.32	-10.53	0.07	0.07
			69	10.40	-7.40	1.58	-16.16	0.06	-0.01
97	Fondazio ne	38, 40	0	15.02	-8.37	6.52	-16.64	0.06	-0.12
			34	21.06	-8.37	-1.50	-23.33	0.12	-0.20
			69	27.11	-8.37	-12.00	-31.11	0.20	-0.28
98	Fondazio ne	39, 41	0	-63.14	3.72	61.76	-71.03	0.16	-0.29
			33	-57.18	3.72	37.75	-67.31	0.26	-0.31

			66	-51.24	3.72	14.88	-64.27	0.37	-0.35
99	Fondazio ne	39, 41	0	-36.31	13.02	21.07	-45.72	0.37	0.36
			33	-30.38	13.02	5.14	-43.86	0.25	0.33
			66	-24.47	13.02	-10.39	-43.38	0.15	0.29
100	Fondazio ne	40, 42	0	26.69	-10.16	7.10	-15.14	0.19	0.15
			35	32.80	-10.16	-0.84	-24.01	0.15	0.07
			69	38.92	-10.16	-12.03	-33.93	0.14	0.00
101	Fondazio ne	40, 42	0	49.29	-7.08	-6.04	-45.76	0.14	-0.99
			35	55.43	-7.08	-24.90	-56.61	0.49	-1.06
			69	61.58	-7.08	-47.62	-68.04	0.87	-1.12
102	Fondazio ne	41, 44	0	-17.22	12.29	9.27	-43.40	0.08	0.72
			33	-11.31	12.29	-6.34	-44.33	-0.15	0.68
			66	-5.41	12.29	-22.49	-46.64	-0.37	0.63
103	Fondazio ne	41, 44	0	8.42	5.87	-16.33	-61.41	-0.37	3.67
			33	14.32	5.87	-38.32	-64.85	-1.57	3.63
			66	20.23	5.87	-61.56	-68.91	-2.76	3.57
104	Fondazio ne	42, 43	0	66.31	2.24	-31.84	-35.76	0.82	-5.51
			23	70.43	2.24	-41.77	-43.38	2.09	-5.55
			46	74.56	2.24	-53.43	-50.73	3.37	-5.59
105	Fondazio ne	43, 44	0	-2.00	-10.98	-7.41	36.88	5.89	15.67
			49	-2.06	-10.98	7.21	23.76	0.39	6.94
			97	-2.13	-10.98	16.36	14.39	-0.88	-1.71
106	Fondazio ne	43, 44	0	1.85	-6.09	11.42	5.27	-0.86	6.29
			49	1.79	-6.09	12.37	-0.96	-1.84	-2.29
			97	1.72	-6.09	10.91	-4.77	1.36	-10.83
107	Fondazio ne	43, 44	0	2.85	-2.28	8.30	0.04	1.37	8.93
			49	2.79	-2.28	7.78	-1.99	-0.91	0.43
			97	2.73	-2.28	6.59	-2.75	0.95	-8.03
108	Fondazio ne	43, 44	0	3.11	-0.83	5.59	-1.77	0.96	8.22
			49	3.05	-0.83	4.74	-1.65	-0.99	-0.20
			97	3.00	-0.83	4.10	-0.96	1.15	-8.60
109	Fondazio ne	43, 44	0	1.96	-0.21	3.14	-2.34	1.16	8.40
			49	1.90	-0.21	2.25	-1.33	-0.89	0.03
			97	1.85	-0.21	1.90	-0.14	1.13	-8.31
110	Fondazio ne	43, 44	0	0.69	0.02	1.37	-1.97	1.13	8.30
			49	0.64	0.02	0.73	-0.72	-0.88	-0.02
			97	0.59	0.02	0.68	0.51	1.15	-8.32
111	Fondazio ne	43, 44	0	-0.56	0.09	0.46	-1.52	1.16	8.27
			49	-0.61	0.09	0.02	-0.33	-0.85	-0.01
			97	-0.66	0.09	0.15	0.80	1.17	-8.29
112	Fondazio ne	43, 44	0	-1.70	0.08	0.08	-1.18	1.17	8.27
			49	-1.75	0.08	-0.22	-0.10	-0.84	0.01
			97	-1.81	0.08	-0.01	0.91	1.16	-8.24
113	Fondazio ne	43, 44	0	-2.67	0.03	0.00	-1.01	1.16	8.19
			49	-2.72	0.03	-0.24	-0.04	-0.82	-0.06
			97	-2.78	0.03	-0.02	0.89	1.22	-8.30
114	Fondazio ne	43, 44	0	-3.55	0.05	0.05	-0.88	1.22	8.34
			49	-3.61	0.05	-0.15	0.03	-0.84	0.11
			97	-3.68	0.05	0.10	0.91	1.12	-8.13
115	Fondazio ne	43, 44	0	-3.89	-0.08	0.05	-0.79	1.12	8.15
			49	-3.95	-0.08	-0.11	0.08	-0.85	-0.08
			97	-4.02	-0.08	0.15	0.93	1.20	-8.32
116	Fondazio ne	43, 44	0	-4.10	-0.13	0.17	-0.79	1.20	8.29
			49	-4.18	-0.13	0.00	0.04	-0.83	0.04
			97	-4.25	-0.13	0.24	0.86	1.15	-8.21

117	Fondazio ne	43, 44	0	-3.95	-0.21	0.24	-0.74	1.15	8.27
			49	-4.03	-0.21	0.09	0.05	-0.87	0.01
			97	-4.11	-0.21	0.32	0.82	1.14	-8.26
118	Fondazio ne	43, 44	0	-3.39	-0.31	0.36	-0.64	1.14	8.31
			49	-3.48	-0.31	0.24	0.09	-0.89	0.02
			97	-3.56	-0.31	0.47	0.76	1.12	-8.29
119	Fondazio ne	43, 44	0	-2.41	-0.47	0.59	-0.40	1.12	8.35
			49	-2.50	-0.47	0.56	0.19	-0.92	0.02
			97	-2.59	-0.47	0.80	0.68	1.10	-8.33
120	Fondazio ne	43, 44	0	-1.00	-0.70	1.18	0.01	1.09	8.46
			49	-1.09	-0.70	1.29	0.35	-0.99	0.08
			97	-1.19	-0.70	1.52	0.48	1.01	-8.33
121	Fondazio ne	43, 44	0	0.65	-0.48	2.54	0.76	1.00	8.03
			49	0.56	-0.48	2.90	0.58	-0.85	-0.41
			97	0.46	-0.48	3.08	-0.04	1.41	-8.89
122	Fondazio ne	43, 44	0	1.76	1.44	5.67	0.92	1.40	10.61
			49	1.67	1.44	5.86	-0.35	-1.70	2.09
			97	1.58	1.44	5.21	-2.58	-0.63	-6.47
123	Fondazio ne	43, 44	0	1.21	3.55	12.75	-19.07	-0.66	1.98
			49	1.12	3.55	2.68	-22.62	0.48	-6.65
			97	1.03	3.55	-9.52	-27.85	5.83	-15.34
124	Fondazio ne	43, 45	0	29.00	19.88	-46.13	100.23	-2.55	-4.57
			33	34.94	19.88	-15.86	90.70	-1.03	-4.60
			66	40.89	19.87	11.53	82.82	0.49	-4.62
125	Fondazio ne	43, 45	0	61.14	12.10	-4.92	109.84	0.49	1.11
			33	67.11	12.10	29.07	103.69	0.13	1.10
			66	73.10	12.10	61.28	99.00	-0.23	1.10
126	Fondazio ne	44, 46	0	-16.69	-12.80	-55.20	90.85	2.97	4.99
			33	-10.78	-12.79	-27.05	87.00	1.33	4.92
			66	-4.87	-12.79	-0.04	84.07	-0.28	4.85
127	Fondazio ne	44, 46	0	16.23	-12.84	-13.28	98.00	-0.28	-0.04
			33	22.14	-12.84	17.55	96.28	-0.26	-0.12
			66	28.05	-12.84	48.02	95.68	-0.20	-0.21
128	Fondazio ne	45, 47	0	17.50	-3.18	70.53	-91.47	-0.20	-0.52
			33	23.51	-3.18	38.47	-95.49	-0.03	-0.51
			66	29.53	-3.18	5.07	-99.73	0.13	-0.48
129	Fondazio ne	45, 47	0	53.46	-3.24	9.23	-105.00	0.14	0.30
			33	59.50	-3.24	-27.41	-109.87	0.03	0.34
			66	65.55	-3.24	-65.75	-115.18	-0.09	0.39
130	Fondazio ne	46, 48	0	-21.23	3.16	56.91	-92.75	-0.20	-0.79
			33	-15.31	3.16	25.11	-92.79	0.07	-0.88
			66	-9.40	3.16	-6.71	-92.94	0.38	-0.98
131	Fondazio ne	46, 48	0	13.35	0.48	-0.39	-80.24	0.38	1.28
			33	19.26	0.48	-28.12	-80.68	-0.02	1.18
			66	25.18	0.48	-56.01	-81.14	-0.39	1.06
132	Fondazio ne	47, 49	0	16.25	15.91	-54.94	104.50	-0.02	-0.11
			33	22.32	15.91	-22.52	99.49	0.00	-0.05
			66	28.40	15.91	8.40	95.44	0.01	0.02
133	Fondazio ne	47, 49	0	50.27	17.00	-3.66	91.86	0.01	-0.18
			33	56.36	17.00	24.92	88.94	0.06	-0.10
			66	62.47	17.00	52.69	86.92	0.07	-0.01
134	Fondazio ne	48, 50	0	-25.06	-14.86	-52.06	91.94	-0.40	-1.19
			33	-19.14	-14.86	-22.90	92.16	0.02	-1.31
			66	-13.23	-14.86	6.54	93.69	0.47	-1.44
135	Fondazio	48, 50	0	6.15	-19.30	-4.99	94.31	0.47	0.94

	ne								
			33	12.06	-19.30	25.41	97.34	0.18	0.81
			66	17.98	-19.30	57.03	101.65	-0.07	0.67
136	Fondazio ne	49, 51	0	14.02	2.86	59.07	-86.14	0.16	0.28
			33	20.15	2.86	29.13	-87.92	0.05	0.39
			66	26.28	2.86	-1.47	-90.19	-0.09	0.51
137	Fondazio ne	49, 51	0	46.99	4.38	-1.04	-92.33	-0.09	-0.61
			33	53.14	4.38	-33.22	-95.34	0.09	-0.48
			66	59.31	4.38	-66.48	-98.78	0.22	-0.33
138	Fondazio ne	50, 52	0	-32.81	-4.96	60.88	-64.22	-0.06	-0.92
			33	-26.90	-4.97	39.30	-59.34	0.27	-1.07
			66	-21.00	-4.97	19.32	-54.73	0.64	-1.21
139	Fondazio ne	50, 52	0	-10.53	2.05	18.79	-33.94	0.64	0.98
			33	-4.63	2.05	7.07	-30.12	0.34	0.83
			66	1.26	2.05	-3.56	-27.34	0.09	0.68
140	Fondazio ne	51, 53	0	9.80	19.19	-62.68	86.59	0.22	-0.12
			33	15.98	19.19	-35.87	83.55	0.24	0.04
			66	22.17	19.19	-9.87	81.76	0.20	0.21
141	Fondazio ne	51, 53	0	41.17	16.79	-25.91	86.72	0.20	1.08
			33	47.36	16.79	1.40	86.63	-0.19	1.26
			66	53.58	16.80	28.99	88.41	-0.64	1.47
142	Fondazio ne	52, 54	0	0.02	2.37	10.02	-38.44	0.20	0.64
			33	5.92	2.37	-3.53	-36.76	0.01	0.49
			66	11.82	2.37	-16.72	-36.20	-0.13	0.34
143	Fondazio ne	52, 54	0	14.58	5.66	-16.06	-30.42	-0.13	-1.03
			33	20.48	5.66	-27.32	-30.80	0.24	-1.18
			66	26.39	5.66	-38.81	-31.72	0.66	-1.33
144	Fondazio ne	53, 55	0	-0.60	9.64	30.91	-136.60	-1.07	-3.41
			33	5.62	9.64	-14.89	-133.17	0.02	-3.20
			66	11.85	9.64	-59.31	-128.17	1.03	-2.97
145	Fondazio ne	53, 55	0	27.48	-1.68	-63.58	-117.31	1.04	6.53
			33	33.71	-1.68	-102.43	-110.07	-1.16	6.77
			66	39.95	-1.68	-138.33	-99.13	-3.43	7.02
146	Fondazio ne	54, 56	0	22.66	-5.58	-27.36	-63.57	1.10	3.57
			33	28.58	-5.58	-49.68	-64.49	-0.05	3.42
			66	34.51	-5.58	-72.21	-64.66	-1.16	3.28
147	Fondazio ne	54, 56	0	39.40	-0.90	-76.77	-70.03	-1.16	-6.33
			33	45.35	-0.90	-100.86	-68.36	0.95	-6.47
			66	51.30	-0.90	-123.90	-63.28	3.11	-6.61
148	Fondazio ne	55, 57	0	-4.55	56.86	-142.42	52.25	-4.62	-6.52
			40	2.98	56.86	-119.31	73.39	-2.09	-6.21
			80	10.51	56.87	-85.46	106.97	0.32	-5.92
149	Fondazio ne	55, 57	0	37.95	52.95	-111.86	114.48	0.31	-0.96
			40	45.50	52.96	-58.65	163.84	0.64	-0.69
			80	53.07	52.96	17.76	231.48	0.87	-0.44
150	Fondazio ne	56, 70	0	4.13	-51.51	-130.47	53.03	4.01	4.93
			40	11.32	-51.51	-108.48	66.53	2.08	4.77
			80	18.52	-51.51	-78.95	91.53	0.21	4.65
151	Fondazio ne	56, 70	0	41.37	-47.19	-100.69	98.97	0.22	2.09
			40	48.58	-47.19	-55.48	138.49	-0.60	2.01
			80	55.82	-47.20	8.72	194.84	-1.39	1.97
152	Fondazio ne	57, 58	0	12.37	-35.75	30.09	-189.76	12.08	27.57
			42	12.44	-35.74	-32.79	-115.03	1.35	24.22
			83	12.58	-35.73	-67.05	-51.87	-8.20	21.92
153	Fondazio ne	57, 58	0	-8.43	42.13	-54.77	-43.13	-8.20	-18.83

			42	-8.23	42.14	-61.27	10.16	-0.07	-20.11
			83	-7.99	42.15	-47.31	55.73	8.38	-20.40
154	Fondazio ne	58, 59	0	-10.01	-23.90	-58.27	-6.77	9.67	31.97
			35	-9.80	-23.89	-54.74	27.03	-1.15	30.78
			69	-9.59	-23.89	-39.93	58.82	-11.57	29.62
155	Fondazio ne	58, 59	0	-15.03	120.21	-59.77	67.26	-11.57	-34.32
			35	-14.83	120.22	-31.27	98.07	0.47	-35.49
			69	-14.63	120.23	7.81	128.76	12.92	-36.69
156	Fondazio ne	59, 60	0	-16.95	-44.79	-13.13	-30.65	14.93	43.59
			35	-16.76	-44.78	-18.42	0.27	0.09	42.40
			69	-16.58	-44.77	-12.96	31.72	-14.34	41.24
157	Fondazio ne	59, 60	0	-19.95	135.38	-35.97	69.78	-14.34	-40.95
			35	-19.77	135.39	-6.38	102.16	-0.01	-42.11
			69	-19.60	135.40	34.59	135.79	14.72	-43.29
158	Fondazio ne	60, 61	0	-20.25	-73.68	11.03	-52.82	16.11	46.35
			35	-20.09	-73.67	-1.26	-18.08	0.33	45.17
			69	-19.93	-73.66	-1.40	17.64	-15.06	44.02
159	Fondazio ne	60, 61	0	-21.51	131.02	-17.68	37.39	-15.05	-38.70
			35	-21.37	131.03	1.50	74.17	-1.51	-39.84
			69	-21.23	131.04	33.57	112.12	12.44	-41.01
160	Fondazio ne	61, 62	0	-21.04	-91.13	21.38	-73.60	18.12	50.13
			35	-20.91	-91.12	2.65	-34.75	1.03	48.96
			69	-20.79	-91.11	-2.57	4.77	-15.67	47.82
161	Fondazio ne	61, 62	0	-20.50	130.62	-12.08	22.27	-15.67	-47.57
			35	-20.39	130.63	2.49	62.49	0.94	-48.70
			69	-20.29	130.64	31.08	103.46	17.94	-49.86
162	Fondazio ne	62, 63	0	-20.74	-108.46	25.09	-86.53	13.72	43.64
			35	-20.65	-108.44	2.36	-45.06	-1.14	42.48
			69	-20.56	-108.43	-6.02	-3.35	-15.60	41.37
163	Fondazio ne	62, 63	0	-20.24	122.42	-9.92	14.19	-15.60	-44.24
			35	-20.16	122.43	2.20	56.20	-0.15	-45.36
			69	-20.09	122.44	28.87	98.56	15.70	-46.50
164	Fondazio ne	63, 64	0	-19.67	-118.02	27.86	-95.84	15.90	46.78
			35	-19.60	-118.00	2.11	-53.38	-0.04	45.64
			69	-19.55	-117.99	-9.02	-11.08	-15.60	44.53
165	Fondazio ne	63, 64	0	-18.11	114.40	-8.26	7.14	-15.60	-44.64
			35	-18.06	114.41	1.47	49.35	-0.01	-45.75
			69	-18.02	114.42	25.77	91.53	15.97	-46.88
166	Fondazio ne	64, 65	0	-17.00	-125.04	29.14	-101.55	15.67	46.35
			35	-16.96	-125.02	1.35	-59.62	-0.12	45.21
			69	-16.94	-125.01	-12.07	-18.20	-15.53	44.12
167	Fondazio ne	64, 65	0	-14.57	104.87	-6.86	-0.14	-15.53	-41.52
			35	-14.55	104.88	0.17	40.86	-1.02	-42.62
			69	-14.54	104.89	21.29	81.53	13.88	-43.75
168	Fondazio ne	65, 66	0	-13.78	-131.15	28.89	-100.78	17.93	49.58
			35	-13.77	-131.14	1.06	-60.63	1.02	48.45
			69	-13.76	-131.13	-13.04	-21.24	-15.51	47.35
169	Fondazio ne	65, 66	0	-12.22	87.59	-2.54	-1.52	-15.51	-47.72
			35	-12.22	87.60	3.63	37.20	1.14	-48.82
			69	-12.23	87.61	23.05	75.27	18.18	-49.94
170	Fondazio ne	66, 67	0	-11.33	-133.33	35.83	-112.77	12.48	40.43
			35	-11.34	-133.32	3.37	-75.61	-1.27	39.31
			69	-11.35	-133.31	-16.48	-39.67	-14.65	38.24
171	Fondazio ne	66, 67	0	-10.77	63.98	0.61	-19.51	-14.65	-42.93
			35	-10.79	63.99	-0.08	15.29	0.35	-44.00

			69	-10.81	64.00	11.05	48.99	15.71	-45.10
172	Fondazio ne	67, 68	0	-5.75	-128.42	28.91	-114.63	14.21	41.26
			35	-5.77	-128.41	-4.99	-82.15	0.16	40.17
			69	-5.80	-128.40	-27.92	-51.03	-13.51	39.12
173	Fondazio ne	67, 68	0	-5.51	40.41	-6.45	-34.51	-13.51	-39.64
			35	-5.54	40.42	-13.14	-4.49	0.35	-40.69
			69	-5.57	40.43	-9.63	24.70	14.57	-41.76
174	Fondazio ne	68, 69	0	0.46	-112.75	9.71	-117.08	12.54	35.28
			35	0.42	-112.74	-25.73	-88.52	0.56	34.22
			69	0.39	-112.73	-51.40	-60.31	-11.08	33.21
175	Fondazio ne	68, 69	0	1.75	21.54	-32.30	-60.00	-11.07	-29.73
			35	1.72	21.55	-48.09	-31.42	-0.64	-30.73
			69	1.68	21.56	-53.83	-1.59	10.13	-31.73
176	Fondazio ne	69, 70	0	-2.20	-43.43	-41.79	-46.63	9.00	21.19
			42	-2.24	-43.42	-53.21	-7.06	0.17	21.17
			83	-2.22	-43.42	-46.97	38.66	-8.46	20.17
177	Fondazio ne	69, 70	0	13.06	30.82	-58.52	44.66	-8.45	-21.40
			42	13.14	30.83	-29.19	98.39	0.82	-23.38
			83	13.27	30.83	24.41	161.61	11.12	-26.38
178	Primo Impalcato	1, 2	0	-65.77	17.02	28.50	-38.40	-256.31	-226.73
			83	-68.11	17.02	-3.42	-38.40	-84.84	-183.64
			166	-71.16	17.02	-35.35	-38.40	45.30	-127.29
179	Primo Impalcato	1, 15	0	-396.70	1.17	266.59	-196.76	239.47	145.04
			80	-396.70	1.17	110.17	-196.76	124.16	145.04
			159	-396.70	1.17	-46.26	-196.76	8.86	145.04
180	Primo Impalcato	2, 3	0	-54.45	17.33	-31.12	20.40	43.79	-46.05
			69	-54.45	17.33	-17.04	20.40	60.82	-3.33
			138	-54.45	17.33	-2.96	20.40	48.39	39.38
181	Primo Impalcato	3, 4	0	-54.50	16.03	-1.90	1.87	49.50	-26.39
			69	-54.50	16.03	-0.61	1.87	52.97	16.33
			138	-54.50	16.03	0.68	1.87	26.96	59.05
182	Primo Impalcato	4, 5	0	-54.50	13.26	1.63	-2.54	29.72	-38.07
			69	-54.50	13.26	-0.12	-2.54	41.25	4.65
			138	-54.50	13.26	-1.87	-2.54	23.31	47.37
183	Primo Impalcato	5, 6	0	-54.50	9.45	-1.10	-1.61	25.99	-42.86
			69	-54.50	9.45	-2.21	-1.61	40.82	-0.14
			138	-54.50	9.45	-3.31	-1.61	26.18	42.58
184	Primo Impalcato	6, 7	0	-50.23	4.73	-2.96	1.47	26.06	-46.40
			69	-50.23	4.73	-1.95	1.47	43.34	-3.69
			138	-50.23	4.73	-0.93	1.47	31.14	39.03
185	Primo Impalcato	7, 8	0	-53.81	-0.20	-0.97	-2.65	33.07	-45.27
			69	-53.81	-0.20	-2.79	-2.65	49.57	-2.55
			138	-53.81	-0.20	-4.62	-2.65	36.60	40.16
186	Primo Impalcato	8, 9	0	-53.78	-5.52	-5.12	7.27	35.93	-38.41
			69	-53.78	-5.52	-0.11	7.27	47.70	4.31
			138	-53.78	-5.52	4.90	7.27	29.98	47.03
187	Primo Impalcato	9, 10	0	-47.61	-9.84	4.18	-8.35	26.47	-38.71
			69	-47.61	-9.84	-1.58	-8.35	38.44	4.01
			138	-47.61	-9.84	-7.34	-8.35	20.93	46.73
188	Primo Impalcato	10, 11	0	-49.38	-13.87	-8.41	8.87	20.91	-48.55
			69	-49.38	-13.87	-2.29	8.87	39.67	-5.83
			138	-49.38	-13.87	3.83	8.87	28.96	36.89
189	Primo Impalcato	11, 12	0	-49.34	-16.50	2.38	-3.24	26.06	-55.35
			69	-49.34	-16.50	0.14	-3.24	49.51	-12.63
			138	-49.34	-16.50	-2.09	-3.24	43.49	30.09

190	Primo Impalcato	12, 13	0	-49.26	-17.71	-3.60	-19.84	42.11	-34.72
			69	-49.26	-17.71	-17.29	-19.84	51.33	7.99
			138	-49.26	-17.71	-30.98	-19.84	31.08	50.71
191	Primo Impalcato	13, 14	0	-72.04	-15.43	-35.57	49.09	31.24	110.41
			83	-68.99	-15.43	5.23	49.09	-84.87	166.76
			166	-66.65	-15.43	46.03	49.09	-242.31	209.85
192	Primo Impalcato	14, 16	0	-318.22	-1.36	138.28	-91.47	-216.48	-129.89
			80	-318.22	-1.36	65.55	-91.47	-113.22	-129.89
			159	-318.22	-1.36	-7.17	-91.47	-9.95	-129.89
193	Primo Impalcato	15, 17	0	-342.21	-0.70	76.10	-129.33	10.32	23.15
			66	-342.21	-0.70	-9.26	-129.33	-4.96	23.15
			132	-342.21	-0.70	-94.62	-129.33	-20.25	23.15
194	Primo Impalcato	16, 18	0	-268.44	0.61	59.91	-97.40	-11.68	-21.36
			66	-268.44	0.61	-4.38	-97.40	2.42	-21.36
			132	-268.44	0.61	-68.66	-97.40	16.52	-21.36
195	Primo Impalcato	17, 19	0	-284.79	-0.19	26.76	-28.19	-19.08	-9.87
			66	-284.79	-0.19	8.15	-28.19	-12.56	-9.87
			132	-284.79	-0.19	-10.45	-28.19	-6.05	-9.87
196	Primo Impalcato	18, 20	0	-268.04	0.19	16.42	-8.06	16.40	7.84
			66	-268.04	0.19	11.10	-8.06	11.22	7.84
			132	-268.04	0.19	5.78	-8.06	6.05	7.84
197	Primo Impalcato	19, 21	0	-223.68	0.02	113.69	-168.83	-6.37	-5.37
			66	-223.68	0.02	2.26	-168.83	-2.82	-5.37
			132	-223.68	0.02	-109.16	-168.83	0.72	-5.37
198	Primo Impalcato	20, 22	0	-225.95	0.00	75.78	-114.13	5.66	4.55
			66	-225.95	0.00	0.46	-114.13	2.66	4.55
			132	-225.95	0.00	-74.87	-114.13	-0.35	4.55
199	Primo Impalcato	21, 23	0	-160.03	0.01	15.71	-22.60	0.05	-0.83
			66	-160.03	0.01	0.79	-22.60	0.59	-0.83
			132	-160.03	0.01	-14.13	-22.60	1.14	-0.83
200	Primo Impalcato	22, 24	0	-192.59	0.02	-0.46	3.12	-0.20	0.43
			66	-192.59	0.02	1.59	3.12	-0.48	0.43
			132	-192.59	0.02	3.65	3.12	-0.76	0.43
201	Primo Impalcato	23, 25	0	-102.34	0.01	110.89	-168.50	0.52	0.15
			66	-102.34	0.01	-0.33	-168.50	0.42	0.15
			132	-102.34	0.01	-111.54	-168.50	0.33	0.15
202	Primo Impalcato	24, 26	0	-155.37	-0.01	74.52	-112.97	-0.69	-0.02
			66	-155.37	-0.01	-0.03	-112.97	-0.67	-0.02
			132	-155.37	-0.01	-74.59	-112.97	-0.66	-0.02
203	Primo Impalcato	25, 28	0	4.21	-0.03	13.18	-21.53	-0.28	-0.49
			85	4.21	-0.03	-5.12	-21.53	0.13	-0.49
			170	4.21	-0.03	-23.42	-21.53	0.55	-0.49
204	Primo Impalcato	26, 27	0	-121.73	0.07	-1.24	2.45	-0.72	-0.81
			66	-121.73	0.07	0.38	2.45	-0.19	-0.81
			132	-121.73	0.07	2.00	2.45	0.35	-0.81
205	Primo Impalcato	27, 29	0	-86.74	0.01	73.46	-111.80	0.31	0.11
			66	-86.74	0.01	-0.32	-111.80	0.23	0.11
			132	-86.74	0.01	-74.11	-111.80	0.16	0.11
206	Primo Impalcato	28, 30	0	105.45	0.00	99.50	-119.02	-0.04	-0.25
			73	105.45	0.00	12.61	-119.02	0.14	-0.25
			146	105.45	0.00	-74.27	-119.02	0.32	-0.25
207	Primo Impalcato	29, 31	0	-54.03	0.03	-1.47	1.79	0.14	0.04
			66	-54.03	0.03	-0.29	1.79	0.12	0.04
			132	-54.03	0.03	0.89	1.79	0.09	0.04
208	Primo	30, 32	0	65.99	0.01	52.98	-84.42	-0.24	-0.33

	Impalcato								
			69	65.99	0.01	-4.85	-84.42	-0.01	-0.33
			137	65.99	0.01	-62.68	-84.42	0.21	-0.33
209	Primo Impalcato	31, 33	0	-22.75	0.00	73.66	-111.93	0.08	0.22
			66	-22.75	0.00	-0.21	-111.93	-0.07	0.22
			132	-22.75	0.00	-74.08	-111.93	-0.21	0.22
210	Primo Impalcato	32, 34	0	26.45	0.00	63.24	-91.59	-0.34	-0.34
			69	26.45	0.00	0.04	-91.59	-0.10	-0.34
			138	26.45	0.00	-63.16	-91.59	0.13	-0.34
211	Primo Impalcato	33, 35	0	9.76	0.04	-1.57	2.36	-0.23	-0.21
			66	9.76	0.04	-0.01	2.36	-0.10	-0.21
			132	9.76	0.04	1.55	2.36	0.04	-0.21
212	Primo Impalcato	34, 36	0	-13.13	0.01	62.72	-91.06	-0.43	-0.50
			69	-13.13	0.01	-0.11	-91.06	-0.08	-0.50
			138	-13.13	0.01	-62.94	-91.06	0.27	-0.50
213	Primo Impalcato	35, 37	0	41.75	0.01	72.75	-109.74	0.02	0.06
			66	41.75	0.01	0.32	-109.74	-0.01	0.06
			132	41.75	0.01	-72.11	-109.74	-0.05	0.06
214	Primo Impalcato	36, 38	0	-52.75	0.01	62.89	-91.42	-0.30	-0.45
			69	-52.75	0.01	-0.19	-91.42	0.01	-0.45
			138	-52.75	0.01	-63.27	-91.42	0.32	-0.45
215	Primo Impalcato	37, 39	0	78.11	0.04	-2.26	-2.49	-0.08	-0.72
			66	78.11	0.04	-3.90	-2.49	0.39	-0.72
			132	78.11	0.04	-5.54	-2.49	0.87	-0.72
216	Primo Impalcato	38, 40	0	-92.41	0.02	62.53	-86.87	-0.24	-0.71
			69	-92.41	0.02	3.02	-86.87	0.25	-0.71
			137	-92.41	0.02	-56.48	-86.87	0.73	-0.71
217	Primo Impalcato	39, 41	0	113.49	-0.04	63.69	-75.91	0.82	-0.38
			66	113.49	-0.04	13.59	-75.91	1.07	-0.38
			132	113.49	-0.04	-36.51	-75.91	1.32	-0.38
218	Primo Impalcato	40, 42	0	-132.10	0.01	70.15	-107.69	0.19	-0.51
			69	-132.10	0.01	-4.16	-107.69	0.54	-0.51
			138	-132.10	0.01	-78.46	-107.69	0.90	-0.51
219	Primo Impalcato	41, 44	0	60.87	-0.18	40.03	-82.04	1.40	2.09
			66	60.87	-0.18	-14.12	-82.04	0.03	2.09
			132	60.87	-0.18	-68.27	-82.04	-1.35	2.09
220	Primo Impalcato	42, 43	0	-172.16	-0.21	46.74	-284.14	0.49	3.21
			23	-172.16	-0.21	-18.61	-284.14	-0.24	3.21
			46	-172.16	-0.21	-83.97	-284.14	-0.98	3.21
221	Primo Impalcato	43, 45	0	-113.87	0.00	38.69	-46.59	-1.37	-0.67
			66	-113.87	0.00	7.94	-46.59	-0.93	-0.67
			132	-113.87	0.00	-22.81	-46.59	-0.49	-0.67
222	Primo Impalcato	44, 46	0	94.58	-0.01	2.66	2.02	-1.24	-0.24
			66	94.58	-0.01	3.99	2.02	-1.09	-0.24
			132	94.58	-0.01	5.33	2.02	-0.93	-0.24
223	Primo Impalcato	45, 47	0	-56.80	0.06	102.03	-158.71	-1.04	-0.59
			66	-56.80	0.06	-2.72	-158.71	-0.65	-0.59
			132	-56.80	0.06	-107.47	-158.71	-0.26	-0.59
224	Primo Impalcato	46, 48	0	130.31	0.04	77.30	-118.48	-0.96	-0.94
			66	130.31	0.04	-0.90	-118.48	-0.34	-0.94
			132	130.31	0.04	-79.09	-118.48	0.28	-0.94
225	Primo Impalcato	47, 49	0	-1.49	0.05	16.69	-25.50	-0.86	-0.77
			66	-1.49	0.05	-0.14	-25.50	-0.35	-0.77
			132	-1.49	0.05	-16.97	-25.50	0.15	-0.77
226	Primo Impalcato	48, 50	0	161.55	0.07	-5.65	3.17	0.30	0.25

			66	161.55	0.07	-3.56	3.17	0.13	0.25
			132	161.55	0.07	-1.47	3.17	-0.03	0.25
227	Primo Impalcato	49, 51	0	57.54	0.06	107.11	-164.96	-0.48	-3.21
			66	57.54	0.06	-1.77	-164.96	1.63	-3.21
			132	57.54	0.06	-110.64	-164.96	3.75	-3.21
228	Primo Impalcato	50, 52	0	202.55	0.06	67.38	-90.36	0.02	2.28
			66	202.55	0.06	7.75	-90.36	-1.48	2.28
			132	202.55	0.06	-51.89	-90.36	-2.98	2.28
229	Primo Impalcato	51, 53	0	113.31	-0.08	12.76	-29.21	3.31	-5.60
			66	113.31	-0.08	-6.52	-29.21	7.01	-5.60
			132	113.31	-0.08	-25.80	-29.21	10.70	-5.60
230	Primo Impalcato	52, 54	0	147.66	0.11	24.33	-41.83	-2.78	3.94
			66	147.66	0.11	-3.28	-41.83	-5.39	3.94
			132	147.66	0.11	-30.89	-41.83	-7.99	3.94
231	Primo Impalcato	53, 55	0	166.15	-0.35	95.30	-125.95	11.09	11.92
			66	166.15	-0.35	12.17	-125.95	3.23	11.92
			132	166.15	-0.35	-70.96	-125.95	-4.64	11.92
232	Primo Impalcato	54, 56	0	103.05	0.33	39.83	-79.35	-8.94	-13.32
			66	103.05	0.33	-12.54	-79.35	-0.15	-13.32
			132	103.05	0.33	-64.92	-79.35	8.65	-13.32
233	Primo Impalcato	55, 57	0	223.07	0.58	52.18	-195.17	-3.99	80.36
			80	223.07	0.58	-102.98	-195.17	-67.87	80.36
			159	223.07	0.58	-258.14	-195.17	-131.76	80.36
234	Primo Impalcato	56, 70	0	113.91	-0.73	20.63	-80.62	5.61	-64.30
			80	113.91	-0.73	-43.47	-80.62	56.72	-64.30
			159	113.91	-0.73	-107.56	-80.62	107.84	-64.30
235	Primo Impalcato	57, 58	0	39.67	10.20	5.64	5.80	-141.23	-128.23
			83	40.83	10.20	10.47	5.80	-43.14	-106.69
			166	42.36	10.20	15.29	5.80	34.29	-78.52
236	Primo Impalcato	58, 59	0	39.39	8.32	13.69	-10.33	32.39	-19.40
			69	39.39	8.32	6.56	-10.33	38.41	1.96
			138	39.39	8.32	-0.57	-10.33	29.69	23.31
237	Primo Impalcato	59, 60	0	39.41	7.61	-0.71	-0.12	30.10	-9.71
			69	39.41	7.61	-0.79	-0.12	29.43	11.65
			138	39.41	7.61	-0.88	-0.12	14.02	33.00
238	Primo Impalcato	60, 61	0	39.38	6.29	-1.10	1.65	15.38	-16.74
			69	39.38	6.29	0.04	1.65	19.56	4.62
			138	39.38	6.29	1.18	1.65	9.00	25.98
239	Primo Impalcato	61, 62	0	36.78	4.36	1.04	-0.51	9.13	-23.25
			69	36.78	4.36	0.69	-0.51	17.81	-1.89
			138	36.78	4.36	0.34	-0.51	11.75	19.46
240	Primo Impalcato	62, 63	0	37.43	2.28	0.35	0.48	13.24	-24.01
			69	37.43	2.28	0.68	0.48	22.43	-2.65
			138	37.43	2.28	1.02	0.48	16.89	18.71
241	Primo Impalcato	63, 64	0	37.41	-0.27	1.19	0.42	17.10	-21.52
			69	37.41	-0.27	1.49	0.42	24.58	-0.16
			138	37.41	-0.27	1.78	0.42	17.33	21.19
242	Primo Impalcato	64, 65	0	37.38	-2.83	2.19	-3.93	16.99	-19.06
			69	37.38	-2.83	-0.53	-3.93	22.78	2.29
			138	37.38	-2.83	-3.24	-3.93	13.83	23.65
243	Primo Impalcato	65, 66	0	34.15	-4.90	-2.79	4.93	12.17	-19.51
			69	34.15	-4.90	0.61	4.93	18.27	1.84
			138	34.15	-4.90	4.02	4.93	9.63	23.20
244	Primo Impalcato	66, 67	0	34.78	-6.85	4.61	-5.10	9.51	-24.74
			69	34.78	-6.85	1.09	-5.10	19.21	-3.38

			138	34.78	-6.85	-2.43	-5.10	14.18	17.97
245	Primo Impalcato	67, 68	0	34.76	-8.12	-1.66	1.31	12.73	-28.91
			69	34.76	-8.12	-0.75	1.31	25.31	-7.55
			138	34.76	-8.12	0.15	1.31	23.15	13.80
246	Primo Impalcato	68, 69	0	34.71	-8.72	0.86	8.66	22.51	-18.80
			69	34.71	-8.72	6.83	8.66	28.11	2.56
			138	34.71	-8.72	12.80	8.66	18.97	23.91
247	Primo Impalcato	69, 70	0	42.41	-8.75	14.91	-16.26	19.50	60.86
			83	40.88	-8.75	1.40	-16.26	-43.25	89.03
			166	39.71	-8.75	-12.12	-16.26	-126.66	110.57
248	Primo Impalcato	1	0	406.16	-19.47	44.98	-52.85	-62.76	-36.30
			188	406.16	-19.47	-10.77	-2.26	5.48	-36.30
			376	406.16	-19.47	52.26	73.53	73.71	-36.30
249	Primo Impalcato	2	0	-141.65	-5.35	-56.85	53.62	-1.04	-0.36
			188	-141.65	-5.35	129.05	152.35	-0.37	-0.36
			376	-141.65	-5.35	546.82	300.28	0.30	-0.36
250	Primo Impalcato	3	0	14.21	-4.08	-153.75	175.34	-0.44	-0.23
			188	14.21	-4.08	258.89	271.64	-0.01	-0.23
			376	14.21	-4.08	897.69	415.93	0.41	-0.23
251	Primo Impalcato	4	0	-4.64	-2.98	-125.23	223.76	-0.43	-0.24
			188	-4.64	-2.98	378.45	320.06	0.02	-0.24
			376	-4.64	-2.98	1108.28	464.35	0.46	-0.24
252	Primo Impalcato	5	0	-14.96	-2.16	-58.77	241.14	-0.36	-0.19
			188	-14.96	-2.16	477.59	337.44	0.00	-0.19
			376	-14.96	-2.16	1240.09	481.73	0.35	-0.19
253	Primo Impalcato	6	0	-14.76	-1.34	-1.74	248.40	-0.17	-0.09
			188	-14.76	-1.34	548.26	344.70	0.00	-0.09
			376	-14.76	-1.34	1324.41	488.99	0.17	-0.09
254	Primo Impalcato	7	0	-18.81	-0.47	21.73	254.73	-0.01	0.00
			188	-18.81	-0.47	583.63	351.03	0.00	0.00
			376	-18.81	-0.47	1371.69	495.32	0.01	0.00
255	Primo Impalcato	8	0	-22.42	0.55	20.16	254.72	0.20	0.10
			188	-22.42	0.55	582.04	351.02	0.02	0.10
			376	-22.42	0.55	1370.07	495.31	-0.17	0.10
256	Primo Impalcato	9	0	-32.00	1.52	-9.81	248.65	0.29	0.16
			188	-32.00	1.52	540.66	344.95	-0.01	0.16
			376	-32.00	1.52	1317.28	489.24	-0.30	0.16
257	Primo Impalcato	10	0	-3.18	2.28	-57.32	234.79	0.43	0.24
			188	-3.18	2.28	467.09	331.09	-0.01	0.24
			376	-3.18	2.28	1217.66	475.38	-0.45	0.24
258	Primo Impalcato	11	0	0.76	3.07	-129.00	217.81	0.61	0.33
			188	0.76	3.07	363.48	314.11	-0.01	0.33
			376	0.76	3.07	1082.11	458.40	-0.63	0.33
259	Primo Impalcato	12	0	20.71	4.09	-164.05	171.03	0.60	0.32
			188	20.71	4.09	240.48	267.33	0.00	0.32
			376	20.71	4.09	871.17	411.62	-0.59	0.32
260	Primo Impalcato	13	0	-124.71	5.14	-90.09	59.95	1.24	0.47
			188	-124.71	5.14	107.71	158.68	0.35	0.47
			376	-124.71	5.14	537.37	306.61	-0.53	0.47
261	Primo Impalcato	14	0	327.12	18.06	32.23	-48.42	53.33	33.12
			188	327.12	18.06	-15.20	2.16	-8.93	33.12
			376	327.12	18.06	56.15	77.95	-71.19	33.12
262	Primo Impalcato	15	0	32.64	1.22	-17.27	9.04	118.66	72.23
			188	32.64	1.22	-0.28	9.04	-17.13	72.23
			376	32.64	1.22	16.71	9.04	-152.92	72.23

263	Primo Impalcato	16	0	89.50	-0.98	-14.38	7.57	-105.52	-66.68
			188	89.50	-0.98	-0.14	7.57	19.83	-66.68
			376	89.50	-0.98	14.09	7.57	145.19	-66.68
264	Primo Impalcato	17	0	174.86	0.90	-16.65	9.19	32.95	19.47
			188	174.86	0.90	0.61	9.19	-3.66	19.47
			376	174.86	0.90	17.88	9.19	-40.26	19.47
265	Primo Impalcato	18	0	154.07	-0.83	-14.43	7.95	-31.41	-20.94
			188	154.07	-0.83	0.52	7.95	7.96	-20.94
			376	154.07	-0.83	15.46	7.95	47.33	-20.94
266	Primo Impalcato	19	0	-65.47	0.10	-17.80	9.72	-4.83	-3.27
			188	-65.47	0.10	0.48	9.72	1.31	-3.27
			376	-65.47	0.10	18.75	9.72	7.46	-3.27
267	Primo Impalcato	20	0	-44.05	-0.12	-16.01	8.65	3.77	0.36
			188	-44.05	-0.12	0.26	8.65	3.08	0.36
			376	-44.05	-0.12	16.53	8.65	2.40	0.36
268	Primo Impalcato	21	0	29.17	-0.07	-17.90	9.74	-4.70	-3.24
			188	29.17	-0.07	0.41	9.74	1.39	-3.24
			376	29.17	-0.07	18.71	9.74	7.48	-3.24
269	Primo Impalcato	22	0	35.07	0.05	-15.84	8.56	4.58	1.03
			188	35.07	0.05	0.26	8.56	2.64	1.03
			376	35.07	0.05	16.35	8.56	0.71	1.03
270	Primo Impalcato	23	0	-117.07	-0.04	-17.80	9.67	-0.73	-1.71
			188	-117.07	-0.04	0.37	9.67	2.48	-1.71
			376	-117.07	-0.04	18.54	9.67	5.69	-1.71
271	Primo Impalcato	24	0	-81.01	0.02	-15.84	8.53	0.58	-0.35
			188	-81.01	0.02	0.20	8.53	1.24	-0.35
			376	-81.01	0.02	16.23	8.53	1.90	-0.35
272	Primo Impalcato	25	0	32.38	-0.01	-17.53	9.49	1.18	-0.43
			188	32.38	-0.01	0.32	9.49	1.99	-0.43
			376	32.38	-0.01	18.17	9.49	2.81	-0.43
273	Primo Impalcato	26	0	33.31	-0.02	-15.67	8.44	0.45	-0.63
			188	33.31	-0.02	0.20	8.44	1.63	-0.63
			376	33.31	-0.02	16.08	8.44	2.81	-0.63
274	Primo Impalcato	27	0	-64.87	-0.03	-15.59	8.40	-0.14	-0.03
			188	-64.87	-0.03	0.19	8.40	-0.08	-0.03
			376	-64.87	-0.03	15.98	8.40	-0.02	-0.03
275	Primo Impalcato	28	0	-114.26	0.00	-16.55	9.09	2.29	-1.09
			188	-114.26	0.00	0.53	9.09	4.33	-1.09
			376	-114.26	0.00	17.61	9.09	6.38	-1.09
276	Primo Impalcato	29	0	47.13	-0.02	-15.45	8.33	0.96	0.34
			188	47.13	-0.02	0.21	8.33	0.31	0.34
			376	47.13	-0.02	15.87	8.33	-0.34	0.34
277	Primo Impalcato	30	0	-23.28	0.01	-19.15	10.32	3.11	-0.38
			188	-23.28	0.01	0.24	10.32	3.82	-0.38
			376	-23.28	0.01	19.64	10.32	4.52	-0.38
278	Primo Impalcato	31	0	-56.37	-0.01	-15.35	8.28	1.20	0.92
			188	-56.37	-0.01	0.21	8.28	-0.53	0.92
			376	-56.37	-0.01	15.77	8.28	-2.27	0.92
279	Primo Impalcato	32	0	-10.23	0.01	-18.48	10.04	3.02	0.03
			188	-10.23	0.01	0.40	10.04	2.95	0.03
			376	-10.23	0.01	19.28	10.04	2.89	0.03
280	Primo Impalcato	33	0	48.44	-0.01	-15.29	8.24	1.72	0.91
			188	48.44	-0.01	0.21	8.24	0.00	0.91
			376	48.44	-0.01	15.71	8.24	-1.72	0.91
281	Primo	34	0	-7.62	0.00	-18.46	10.01	3.08	0.36

	Impalcato								
			188	-7.62	0.00	0.37	10.01	2.41	0.36
			376	-7.62	0.00	19.19	10.01	1.74	0.36
282	Primo Impalcato	35	0	-56.56	-0.02	-15.28	8.24	1.58	1.47
			188	-56.56	-0.02	0.20	8.24	-1.19	1.47
			376	-56.56	-0.02	15.69	8.24	-3.96	1.47
283	Primo Impalcato	36	0	6.66	0.00	-18.41	9.99	3.01	0.67
			188	6.66	0.00	0.36	9.99	1.76	0.67
			376	6.66	0.00	19.14	9.99	0.51	0.67
284	Primo Impalcato	37	0	57.09	-0.02	-15.36	8.26	2.37	1.81
			188	57.09	-0.02	0.18	8.26	-1.03	1.81
			376	57.09	-0.02	15.71	8.26	-4.43	1.81
285	Primo Impalcato	38	0	14.19	0.00	-18.36	9.97	3.28	1.16
			188	14.19	0.00	0.39	9.97	1.10	1.16
			376	14.19	0.00	19.14	9.97	-1.08	1.16
286	Primo Impalcato	39	0	-61.26	0.00	-14.93	8.12	1.75	2.25
			188	-61.26	0.00	0.33	8.12	-2.47	2.25
			376	-61.26	0.00	15.59	8.12	-6.69	2.25
287	Primo Impalcato	40	0	24.45	0.01	-18.73	10.12	2.91	1.42
			188	24.45	0.01	0.29	10.12	0.24	1.42
			376	24.45	0.01	19.32	10.12	-2.43	1.42
288	Primo Impalcato	41	0	-0.26	0.07	-17.32	9.21	-0.18	0.51
			188	-0.26	0.07	-0.01	9.21	-1.14	0.51
			376	-0.26	0.07	17.30	9.21	-2.10	0.51
289	Primo Impalcato	42	0	95.73	0.05	-17.74	9.63	-0.49	0.08
			188	95.73	0.05	0.35	9.63	-0.64	0.08
			376	95.73	0.05	18.45	9.63	-0.80	0.08
290	Primo Impalcato	43	0	33.43	0.04	-16.53	9.05	3.05	1.19
			188	33.43	0.04	0.49	9.05	0.82	1.19
			376	33.43	0.04	17.51	9.05	-1.41	1.19
291	Primo Impalcato	44	0	72.22	0.07	-15.05	8.19	2.68	-0.14
			188	72.22	0.07	0.35	8.19	2.95	-0.14
			376	72.22	0.07	15.74	8.19	3.21	-0.14
292	Primo Impalcato	45	0	-44.24	-0.01	-17.62	9.50	-0.52	-1.25
			188	-44.24	-0.01	0.24	9.50	1.82	-1.25
			376	-44.24	-0.01	18.11	9.50	4.17	-1.25
293	Primo Impalcato	46	0	-58.05	0.00	-15.67	8.43	0.79	-0.78
			188	-58.05	0.00	0.17	8.43	2.26	-0.78
			376	-58.05	0.00	16.01	8.43	3.73	-0.78
294	Primo Impalcato	47	0	104.16	-0.05	-17.22	9.36	0.02	-0.28
			188	104.16	-0.05	0.38	9.36	0.54	-0.28
			376	104.16	-0.05	17.98	9.36	1.07	-0.28
295	Primo Impalcato	48	0	81.83	-0.02	-15.68	8.44	-1.09	-1.43
			188	81.83	-0.02	0.19	8.44	1.60	-1.43
			376	81.83	-0.02	16.06	8.44	4.29	-1.43
296	Primo Impalcato	49	0	-35.48	-0.08	-17.21	9.36	2.51	0.93
			188	-35.48	-0.08	0.39	9.36	0.76	0.93
			376	-35.48	-0.08	17.99	9.36	-0.99	0.93
297	Primo Impalcato	50	0	-50.20	-0.01	-15.38	8.35	-2.53	-0.93
			188	-50.20	-0.01	0.33	8.35	-0.78	-0.93
			376	-50.20	-0.01	16.03	8.35	0.98	-0.93
298	Primo Impalcato	51	0	67.59	0.03	-16.99	9.27	2.70	1.54
			188	67.59	0.03	0.44	9.27	-0.20	1.54
			376	67.59	0.03	17.87	9.27	-3.10	1.54
299	Primo Impalcato	52	0	-18.29	-0.10	-17.06	9.18	-2.12	-0.08

			188	-18.29	-0.10	0.21	9.18	-1.96	-0.08
			376	-18.29	-0.10	17.48	9.18	-1.80	-0.08
300	Primo Impalcato	53	0	-139.03	0.47	-15.95	8.78	-17.44	-10.61
			188	-139.03	0.47	0.55	8.78	2.50	-10.61
			376	-139.03	0.47	17.06	8.78	22.45	-10.61
301	Primo Impalcato	54	0	-66.61	-0.44	-16.55	8.92	17.30	11.18
			188	-66.61	-0.44	0.22	8.92	-3.72	11.18
			376	-66.61	-0.44	16.99	8.92	-24.74	11.18
302	Primo Impalcato	55	0	23.77	0.68	-17.09	8.94	-66.30	-40.24
			188	23.77	0.68	-0.28	8.94	9.36	-40.24
			376	23.77	0.68	16.53	8.94	85.01	-40.24
303	Primo Impalcato	56	0	-25.41	-0.45	-13.83	7.44	54.09	34.24
			188	-25.41	-0.45	0.16	7.44	-10.28	34.24
			376	-25.41	-0.45	14.15	7.44	-74.65	34.24
304	Primo Impalcato	57	0	-353.76	-10.62	23.01	-24.30	32.24	16.77
			188	-353.76	-10.62	-0.88	0.98	0.70	16.77
			376	-353.76	-10.62	34.61	38.87	-30.83	16.77
305	Primo Impalcato	58	0	66.72	-2.82	1.95	22.72	0.20	0.01
			188	66.72	-2.82	87.20	72.08	0.19	0.01
			376	66.72	-2.82	288.37	146.04	0.18	0.01
306	Primo Impalcato	59	0	-14.96	-2.00	-63.88	91.58	0.05	0.02
			188	-14.96	-2.00	149.79	139.72	0.01	0.02
			376	-14.96	-2.00	476.51	211.86	-0.04	0.02
307	Primo Impalcato	60	0	-4.65	-1.39	-51.96	115.43	0.12	0.07
			188	-4.65	-1.39	206.54	163.57	-0.01	0.07
			376	-4.65	-1.39	578.11	235.71	-0.14	0.07
308	Primo Impalcato	61	0	3.74	-1.00	-16.84	121.82	0.09	0.05
			188	3.74	-1.00	253.67	169.96	0.00	0.05
			376	3.74	-1.00	637.25	242.10	-0.10	0.05
309	Primo Impalcato	62	0	9.11	-0.65	5.83	127.12	0.02	0.01
			188	9.11	-0.65	286.32	175.27	0.00	0.01
			376	9.11	-0.65	679.88	247.40	-0.02	0.01
310	Primo Impalcato	63	0	8.89	-0.20	17.79	129.89	-0.06	-0.03
			188	8.89	-0.20	303.48	178.03	0.00	-0.03
			376	8.89	-0.20	702.23	250.17	0.06	-0.03
311	Primo Impalcato	64	0	11.44	0.30	16.38	129.57	-0.17	-0.09
			188	11.44	0.30	301.47	177.72	-0.01	-0.09
			376	11.44	0.30	699.63	249.85	0.15	-0.09
312	Primo Impalcato	65	0	17.30	0.77	1.82	126.01	-0.17	-0.10
			188	17.30	0.77	280.21	174.15	0.01	-0.10
			376	17.30	0.77	671.67	246.29	0.19	-0.10
313	Primo Impalcato	66	0	-0.73	1.13	-21.97	119.11	-0.24	-0.13
			188	-0.73	1.13	243.46	167.26	0.01	-0.13
			376	-0.73	1.13	621.96	239.39	0.26	-0.13
314	Primo Impalcato	67	0	-4.58	1.51	-58.12	111.10	-0.33	-0.18
			188	-4.58	1.51	192.25	159.25	0.01	-0.18
			376	-4.58	1.51	555.68	231.38	0.34	-0.18
315	Primo Impalcato	68	0	-14.39	2.03	-74.90	87.77	-0.27	-0.14
			188	-14.39	2.03	131.61	135.91	0.00	-0.14
			376	-14.39	2.03	451.18	208.05	0.27	-0.14
316	Primo Impalcato	69	0	60.67	2.61	-32.25	29.59	-0.46	-0.15
			188	60.67	2.61	65.94	78.95	-0.17	-0.15
			376	60.67	2.61	280.03	152.91	0.11	-0.15
317	Primo Impalcato	70	0	-265.14	9.14	4.83	-17.51	-23.29	-14.19
			188	-265.14	9.14	-6.30	7.77	3.38	-14.19

			376	-265.14	9.14	41.95	45.66	30.05	-14.19
318	Fondazio ne	1, 71	0	240.22	-0.03	0.00	0.00	-1.95	-0.86
			102	240.22	-0.03	0.00	0.00	-1.07	-0.86
			204	240.22	-0.03	0.00	0.00	-0.19	-0.86
319	Fondazio ne	1, 92	0	126.13	-0.34	0.00	0.00	0.41	5.79
			103	126.13	-0.34	0.00	0.00	-5.55	5.79
			206	126.13	-0.34	0.00	0.00	-11.50	5.79
320	Primo Impalcato	92, 2	0	-119.31	-0.62	0.00	0.00	6.10	6.95
			103	-119.31	-0.62	0.00	0.00	-1.05	6.95
			206	-119.31	-0.62	0.00	0.00	-8.20	6.95
321	Fondazio ne	6, 89	0	-0.79	0.71	0.00	0.00	-30.11	-7.44
			100	-0.79	0.71	0.00	0.00	-22.66	-7.44
			200	-0.79	0.71	0.00	0.00	-15.21	-7.44
322	Primo Impalcato	89, 7	0	-9.16	-0.86	0.00	0.00	-12.89	9.13
			100	-9.16	-0.86	0.00	0.00	-22.03	9.13
			200	-9.16	-0.86	0.00	0.00	-31.18	9.13
323	Fondazio ne	9, 90	0	-22.29	0.88	0.00	0.00	-29.78	-9.79
			100	-22.29	0.88	0.00	0.00	-19.98	-9.79
			200	-22.29	0.88	0.00	0.00	-10.18	-9.79
324	Primo Impalcato	90, 10	0	11.96	-0.56	0.00	0.00	-15.03	6.25
			100	11.96	-0.56	0.00	0.00	-21.29	6.25
			200	11.96	-0.56	0.00	0.00	-27.55	6.25
325	Fondazio ne	13, 91	0	-130.96	0.59	0.00	0.00	-7.93	-6.78
			103	-130.96	0.59	0.00	0.00	-0.96	-6.78
			206	-130.96	0.59	0.00	0.00	6.01	-6.78
326	Primo Impalcato	88, 14	0	212.56	0.03	0.00	0.00	-0.25	0.73
			102	212.56	0.03	0.00	0.00	-1.00	0.73
			204	212.56	0.03	0.00	0.00	-1.74	0.73
327	Primo Impalcato	91, 14	0	133.35	0.32	0.00	0.00	-10.78	-5.36
			103	133.35	0.32	0.00	0.00	-5.28	-5.36
			206	133.35	0.32	0.00	0.00	0.23	-5.36
328	Primo Impalcato	71, 15	0	-201.04	-0.09	0.00	0.00	1.82	2.19
			102	-201.04	-0.09	0.00	0.00	-0.42	2.19
			204	-201.04	-0.09	0.00	0.00	-2.66	2.19
329	Fondazio ne	16, 88	0	-171.34	0.09	0.00	0.00	-2.48	-2.06
			102	-171.34	0.09	0.00	0.00	-0.38	-2.06
			204	-171.34	0.09	0.00	0.00	1.73	-2.06
330	Fondazio ne	17, 72	0	302.89	0.02	0.00	0.00	-0.19	-0.20
			100	302.89	0.02	0.00	0.00	0.01	-0.20
			199	302.89	0.02	0.00	0.00	0.20	-0.20
331	Primo Impalcato	87, 18	0	263.80	-0.02	0.00	0.00	0.16	0.22
			100	263.80	-0.02	0.00	0.00	-0.06	0.22
			199	263.80	-0.02	0.00	0.00	-0.27	0.22
332	Primo Impalcato	72, 19	0	-291.12	0.02	0.00	0.00	-0.35	-0.26
			100	-291.12	0.02	0.00	0.00	-0.09	-0.26
			199	-291.12	0.02	0.00	0.00	0.16	-0.26
333	Fondazio ne	20, 87	0	-251.58	-0.01	0.00	0.00	0.06	0.22
			100	-251.58	-0.01	0.00	0.00	-0.16	0.22
			199	-251.58	-0.01	0.00	0.00	-0.37	0.22
334	Fondazio ne	21, 73	0	294.09	0.00	0.00	0.00	0.04	0.02
			100	294.09	0.00	0.00	0.00	0.01	0.02
			199	294.09	0.00	0.00	0.00	-0.01	0.02
335	Primo Impalcato	86, 22	0	256.61	0.00	0.00	0.00	-0.04	0.00
			100	256.61	0.00	0.00	0.00	-0.04	0.00
			199	256.61	0.00	0.00	0.00	-0.04	0.00

336	Primo Impalcato	73, 23	0	-311.52	0.00	0.00	0.00	0.05	-0.01
			100	-311.52	0.00	0.00	0.00	0.06	-0.01
			199	-311.52	0.00	0.00	0.00	0.07	-0.01
337	Fondazione	24, 86	0	-267.93	0.00	0.00	0.00	0.00	0.00
			100	-267.93	0.00	0.00	0.00	0.00	0.00
			199	-267.93	0.00	0.00	0.00	0.01	0.00
338	Fondazione	25, 74	0	342.98	0.00	0.00	0.00	0.00	-0.02
			103	342.98	0.00	0.00	0.00	0.01	-0.02
			206	342.98	0.00	0.00	0.00	0.03	-0.02
339	Primo Impalcato	85, 26	0	254.85	0.00	0.00	0.00	0.01	0.02
			100	254.85	0.00	0.00	0.00	-0.01	0.02
			199	254.85	0.00	0.00	0.00	-0.04	0.02
340	Fondazione	27, 85	0	-262.47	0.00	0.00	0.00	0.01	0.01
			100	-262.47	0.00	0.00	0.00	-0.01	0.01
			199	-262.47	0.00	0.00	0.00	-0.02	0.01
341	Primo Impalcato	74, 28	0	-355.45	0.00	0.00	0.00	0.03	-0.02
			103	-355.45	0.00	0.00	0.00	0.05	-0.02
			206	-355.45	0.00	0.00	0.00	0.08	-0.02
342	Primo Impalcato	84, 29	0	253.85	0.00	0.00	0.00	0.01	0.01
			100	253.85	0.00	0.00	0.00	0.00	0.01
			199	253.85	0.00	0.00	0.00	0.00	0.01
343	Fondazione	31, 84	0	-256.54	0.00	0.00	0.00	0.03	0.02
			100	-256.54	0.00	0.00	0.00	0.01	0.02
			199	-256.54	0.00	0.00	0.00	-0.01	0.02
344	Primo Impalcato	83, 33	0	252.58	0.00	0.00	0.00	0.02	0.00
			100	252.58	0.00	0.00	0.00	0.01	0.00
			199	252.58	0.00	0.00	0.00	0.01	0.00
345	Fondazione	35, 83	0	-253.80	0.00	0.00	0.00	0.04	0.02
			100	-253.80	0.00	0.00	0.00	0.02	0.02
			199	-253.80	0.00	0.00	0.00	-0.01	0.02
346	Primo Impalcato	82, 37	0	252.63	0.00	0.00	0.00	0.02	-0.01
			100	252.63	0.00	0.00	0.00	0.03	-0.01
			199	252.63	0.00	0.00	0.00	0.03	-0.01
347	Fondazione	39, 82	0	-251.86	0.00	0.00	0.00	0.08	0.04
			100	-251.86	0.00	0.00	0.00	0.04	0.04
			199	-251.86	0.00	0.00	0.00	0.00	0.04
348	Primo Impalcato	78, 43	0	292.64	0.00	0.00	0.00	-0.03	-0.02
			100	292.64	0.00	0.00	0.00	-0.01	-0.02
			199	292.64	0.00	0.00	0.00	0.02	-0.02
349	Primo Impalcato	81, 44	0	257.08	0.00	0.00	0.00	-0.03	0.01
			100	257.08	0.00	0.00	0.00	-0.05	0.01
			199	257.08	0.00	0.00	0.00	-0.06	0.01
350	Fondazione	45, 78	0	-296.50	0.00	0.00	0.00	-0.06	-0.04
			100	-296.50	0.00	0.00	0.00	-0.03	-0.04
			199	-296.50	0.00	0.00	0.00	0.01	-0.04
351	Fondazione	46, 81	0	-252.93	0.00	0.00	0.00	-0.03	-0.01
			100	-252.93	0.00	0.00	0.00	-0.02	-0.01
			199	-252.93	0.00	0.00	0.00	0.00	-0.01
352	Primo Impalcato	77, 47	0	298.55	0.00	0.00	0.00	0.03	0.01
			100	298.55	0.00	0.00	0.00	0.02	0.01
			199	298.55	0.00	0.00	0.00	0.01	0.01
353	Primo Impalcato	80, 48	0	261.49	0.00	0.00	0.00	0.00	0.03
			100	261.49	0.00	0.00	0.00	-0.03	0.03
			199	261.49	0.00	0.00	0.00	-0.06	0.03
354	Fondazione	49, 77	0	-287.48	0.00	0.00	0.00	-0.02	0.01

	ne								
			100	-287.48	0.00	0.00	0.00	-0.03	0.01
			199	-287.48	0.00	0.00	0.00	-0.04	0.01
355	Fondazio ne	50, 80	0	-253.24	0.00	0.00	0.00	0.01	0.01
			100	-253.24	0.00	0.00	0.00	0.00	0.01
			199	-253.24	0.00	0.00	0.00	-0.01	0.01
356	Primo Impalcato	76, 51	0	279.17	0.01	0.00	0.00	-0.19	-0.14
			100	279.17	0.01	0.00	0.00	-0.05	-0.14
			199	279.17	0.01	0.00	0.00	0.09	-0.14
357	Fondazio ne	53, 76	0	-288.31	0.01	0.00	0.00	-0.12	-0.11
			100	-288.31	0.01	0.00	0.00	-0.01	-0.11
			199	-288.31	0.01	0.00	0.00	0.09	-0.11
358	Primo Impalcato	75, 55	0	218.33	-0.05	0.00	0.00	0.96	1.18
			102	218.33	-0.05	0.00	0.00	-0.24	1.18
			204	218.33	-0.05	0.00	0.00	-1.44	1.18
359	Fondazio ne	56, 79	0	201.15	0.05	0.00	0.00	-1.24	-1.04
			102	201.15	0.05	0.00	0.00	-0.18	-1.04
			204	201.15	0.05	0.00	0.00	0.88	-1.04
360	Fondazio ne	57, 75	0	-247.82	-0.02	0.00	0.00	-1.15	-0.52
			102	-247.82	-0.02	0.00	0.00	-0.62	-0.52
			204	-247.82	-0.02	0.00	0.00	-0.09	-0.52
361	Fondazio ne	57, 93	0	-53.64	-0.17	0.00	0.00	0.05	3.09
			103	-53.64	-0.17	0.00	0.00	-3.12	3.09
			206	-53.64	-0.17	0.00	0.00	-6.29	3.09
362	Primo Impalcato	93, 58	0	32.85	-0.33	0.00	0.00	2.92	3.63
			103	32.85	-0.33	0.00	0.00	-0.81	3.63
			206	32.85	-0.33	0.00	0.00	-4.54	3.63
363	Fondazio ne	61, 95	0	-0.93	0.31	0.00	0.00	-14.42	-3.31
			100	-0.93	0.31	0.00	0.00	-11.10	-3.31
			200	-0.93	0.31	0.00	0.00	-7.79	-3.31
364	Primo Impalcato	95, 62	0	5.06	-0.45	0.00	0.00	-5.69	4.85
			100	5.06	-0.45	0.00	0.00	-10.54	4.85
			200	5.06	-0.45	0.00	0.00	-15.39	4.85
365	Primo Impalcato	96, 65	0	12.41	0.45	0.00	0.00	5.34	-4.92
			100	12.41	0.45	0.00	0.00	10.27	-4.92
			200	12.41	0.45	0.00	0.00	15.19	-4.92
366	Fondazio ne	66, 96	0	-7.33	-0.29	0.00	0.00	14.07	3.16
			100	-7.33	-0.29	0.00	0.00	10.91	3.16
			200	-7.33	-0.29	0.00	0.00	7.75	3.16
367	Fondazio ne	69, 94	0	50.08	0.30	0.00	0.00	-4.33	-3.46
			103	50.08	0.30	0.00	0.00	-0.77	-3.46
			206	50.08	0.30	0.00	0.00	2.79	-3.46
368	Primo Impalcato	79, 70	0	-231.26	0.02	0.00	0.00	-0.15	0.39
			102	-231.26	0.02	0.00	0.00	-0.54	0.39
			204	-231.26	0.02	0.00	0.00	-0.93	0.39
369	Primo Impalcato	94, 70	0	-62.66	0.15	0.00	0.00	-5.50	-2.58
			103	-62.66	0.15	0.00	0.00	-2.86	-2.58
			206	-62.66	0.15	0.00	0.00	-0.21	-2.58
370	Primo Impalcato	1, 71	0	-201.04	-0.65	0.00	0.00	6.29	2.33
			102	-201.04	-0.65	0.00	0.00	3.91	2.33
			204	-201.04	-0.65	0.00	0.00	1.53	2.33
371	Primo Impalcato	1, 92	0	-119.31	-0.15	0.00	0.00	1.93	-1.97
			103	-119.31	-0.15	0.00	0.00	3.96	-1.97
			206	-119.31	-0.15	0.00	0.00	5.99	-1.97
372	Primo Impalcato	92, 2	0	126.13	-0.73	0.00	0.00	-11.78	-3.13

			103	126.13	-0.73	0.00	0.00	-8.56	-3.13
			206	126.13	-0.73	0.00	0.00	-5.34	-3.13
373	Primo Impalcato	6, 89	0	-9.16	-0.48	0.00	0.00	4.42	8.82
			100	-9.16	-0.48	0.00	0.00	-4.40	8.82
			200	-9.16	-0.48	0.00	0.00	-13.23	8.82
374	Primo Impalcato	89, 7	0	-0.79	0.20	0.00	0.00	-15.20	-7.75
			100	-0.79	0.20	0.00	0.00	-7.43	-7.75
			200	-0.79	0.20	0.00	0.00	0.33	-7.75
375	Primo Impalcato	9, 90	0	11.96	0.01	0.00	0.00	-0.99	6.90
			100	11.96	0.01	0.00	0.00	-7.91	6.90
			200	11.96	0.01	0.00	0.00	-14.82	6.90
376	Primo Impalcato	90, 10	0	-22.29	0.58	0.00	0.00	-10.71	-9.14
			100	-22.29	0.58	0.00	0.00	-1.56	-9.14
			200	-22.29	0.58	0.00	0.00	7.58	-9.14
377	Primo Impalcato	13, 91	0	133.35	0.73	0.00	0.00	-4.20	3.34
			103	133.35	0.73	0.00	0.00	-7.63	3.34
			206	133.35	0.73	0.00	0.00	-11.06	3.34
378	Primo Impalcato	88, 14	0	-171.34	0.60	0.00	0.00	1.47	-2.15
			102	-171.34	0.60	0.00	0.00	3.66	-2.15
			204	-171.34	0.60	0.00	0.00	5.85	-2.15
379	Primo Impalcato	91, 14	0	-130.96	0.11	0.00	0.00	5.89	1.91
			103	-130.96	0.11	0.00	0.00	3.92	1.91
			206	-130.96	0.11	0.00	0.00	1.96	1.91
380	Primo Impalcato	71, 15	0	240.22	0.16	0.00	0.00	0.42	-0.73
			102	240.22	0.16	0.00	0.00	1.16	-0.73
			204	240.22	0.16	0.00	0.00	1.90	-0.73
381	Primo Impalcato	16, 88	0	212.56	-0.14	0.00	0.00	1.62	0.65
			102	212.56	-0.14	0.00	0.00	0.96	0.65
			204	212.56	-0.14	0.00	0.00	0.30	0.65
382	Primo Impalcato	17, 72	0	-291.12	0.07	0.00	0.00	-0.20	0.07
			100	-291.12	0.07	0.00	0.00	-0.26	0.07
			199	-291.12	0.07	0.00	0.00	-0.33	0.07
383	Primo Impalcato	87, 18	0	-251.58	-0.06	0.00	0.00	-0.36	-0.10
			100	-251.58	-0.06	0.00	0.00	-0.26	-0.10
			199	-251.58	-0.06	0.00	0.00	-0.16	-0.10
384	Primo Impalcato	72, 19	0	302.89	-0.01	0.00	0.00	0.15	0.13
			100	302.89	-0.01	0.00	0.00	0.03	0.13
			199	302.89	-0.01	0.00	0.00	-0.09	0.13
385	Primo Impalcato	20, 87	0	263.80	0.01	0.00	0.00	-0.08	-0.10
			100	263.80	0.01	0.00	0.00	0.02	-0.10
			199	263.80	0.01	0.00	0.00	0.12	-0.10
386	Primo Impalcato	21, 73	0	-311.52	0.00	0.00	0.00	-0.03	-0.04
			100	-311.52	0.00	0.00	0.00	0.01	-0.04
			199	-311.52	0.00	0.00	0.00	0.06	-0.04
387	Primo Impalcato	86, 22	0	-267.93	0.00	0.00	0.00	0.01	0.02
			100	-267.93	0.00	0.00	0.00	-0.01	0.02
			199	-267.93	0.00	0.00	0.00	-0.04	0.02
388	Primo Impalcato	73, 23	0	294.09	0.00	0.00	0.00	-0.01	-0.01
			100	294.09	0.00	0.00	0.00	0.00	-0.01
			199	294.09	0.00	0.00	0.00	0.01	-0.01
389	Primo Impalcato	24, 86	0	256.61	0.00	0.00	0.00	0.01	0.03
			100	256.61	0.00	0.00	0.00	-0.01	0.03
			199	256.61	0.00	0.00	0.00	-0.04	0.03
390	Primo Impalcato	25, 74	0	-355.45	0.00	0.00	0.00	-0.01	-0.02
			103	-355.45	0.00	0.00	0.00	0.01	-0.02

			206	-355.45	0.00	0.00	0.00	0.03	-0.02
391	Primo Impalcato	85, 26	0	-262.47	0.00	0.00	0.00	-0.02	0.00
			100	-262.47	0.00	0.00	0.00	-0.02	0.00
			199	-262.47	0.00	0.00	0.00	-0.02	0.00
392	Primo Impalcato	27, 85	0	254.85	0.00	0.00	0.00	0.02	0.01
			100	254.85	0.00	0.00	0.00	0.02	0.01
			199	254.85	0.00	0.00	0.00	0.01	0.01
393	Primo Impalcato	74, 28	0	342.98	0.00	0.00	0.00	0.02	-0.01
			103	342.98	0.00	0.00	0.00	0.04	-0.01
			206	342.98	0.00	0.00	0.00	0.05	-0.01
394	Primo Impalcato	84, 29	0	-256.54	0.00	0.00	0.00	-0.01	0.01
			100	-256.54	0.00	0.00	0.00	-0.01	0.01
			199	-256.54	0.00	0.00	0.00	-0.02	0.01
395	Primo Impalcato	31, 84	0	253.85	0.00	0.00	0.00	0.00	0.00
			100	253.85	0.00	0.00	0.00	0.00	0.00
			199	253.85	0.00	0.00	0.00	0.01	0.00
396	Primo Impalcato	83, 33	0	-253.80	0.00	0.00	0.00	0.00	0.01
			100	-253.80	0.00	0.00	0.00	-0.02	0.01
			199	-253.80	0.00	0.00	0.00	-0.03	0.01
397	Primo Impalcato	35, 83	0	252.58	0.00	0.00	0.00	0.00	-0.01
			100	252.58	0.00	0.00	0.00	0.01	-0.01
			199	252.58	0.00	0.00	0.00	0.02	-0.01
398	Primo Impalcato	82, 37	0	-251.86	0.00	0.00	0.00	0.01	0.02
			100	-251.86	0.00	0.00	0.00	-0.02	0.02
			199	-251.86	0.00	0.00	0.00	-0.04	0.02
399	Primo Impalcato	39, 82	0	252.63	0.00	0.00	0.00	-0.01	-0.02
			100	252.63	0.00	0.00	0.00	0.00	-0.02
			199	252.63	0.00	0.00	0.00	0.02	-0.02
400	Primo Impalcato	78, 43	0	-296.50	0.00	0.00	0.00	0.01	0.00
			100	-296.50	0.00	0.00	0.00	0.01	0.00
			199	-296.50	0.00	0.00	0.00	0.00	0.00
401	Primo Impalcato	81, 44	0	-252.93	0.01	0.00	0.00	0.00	0.00
			100	-252.93	0.01	0.00	0.00	0.00	0.00
			199	-252.93	0.01	0.00	0.00	0.01	0.00
402	Primo Impalcato	45, 78	0	292.64	0.00	0.00	0.00	0.01	0.02
			100	292.64	0.00	0.00	0.00	0.00	0.02
			199	292.64	0.00	0.00	0.00	-0.02	0.02
403	Primo Impalcato	46, 81	0	257.08	0.00	0.00	0.00	0.01	0.02
			100	257.08	0.00	0.00	0.00	-0.01	0.02
			199	257.08	0.00	0.00	0.00	-0.03	0.02
404	Primo Impalcato	77, 47	0	-287.48	0.00	0.00	0.00	-0.04	-0.02
			100	-287.48	0.00	0.00	0.00	-0.02	-0.02
			199	-287.48	0.00	0.00	0.00	0.00	-0.02
405	Primo Impalcato	80, 48	0	-253.24	0.00	0.00	0.00	-0.01	0.01
			100	-253.24	0.00	0.00	0.00	-0.01	0.01
			199	-253.24	0.00	0.00	0.00	-0.02	0.01
406	Primo Impalcato	49, 77	0	298.55	0.00	0.00	0.00	0.00	-0.02
			100	298.55	0.00	0.00	0.00	0.01	-0.02
			199	298.55	0.00	0.00	0.00	0.03	-0.02
407	Primo Impalcato	50, 80	0	261.49	0.00	0.00	0.00	0.05	0.03
			100	261.49	0.00	0.00	0.00	0.02	0.03
			199	261.49	0.00	0.00	0.00	0.00	0.03
408	Primo Impalcato	76, 51	0	-288.31	-0.01	0.00	0.00	0.07	0.06
			100	-288.31	-0.01	0.00	0.00	0.00	0.06
			199	-288.31	-0.01	0.00	0.00	-0.06	0.06

409	Primo Impalcato	53, 76	0	279.17	0.04	0.00	0.00	-0.11	0.03
			100	279.17	0.04	0.00	0.00	-0.14	0.03
			199	279.17	0.04	0.00	0.00	-0.17	0.03
410	Primo Impalcato	75, 55	0	-247.82	0.09	0.00	0.00	0.24	-0.41
			102	-247.82	0.09	0.00	0.00	0.65	-0.41
			204	-247.82	0.09	0.00	0.00	1.06	-0.41
411	Primo Impalcato	56, 79	0	-231.26	-0.07	0.00	0.00	0.82	0.34
			102	-231.26	-0.07	0.00	0.00	0.47	0.34
			204	-231.26	-0.07	0.00	0.00	0.13	0.34
412	Primo Impalcato	57, 75	0	218.33	-0.36	0.00	0.00	3.44	1.29
			102	218.33	-0.36	0.00	0.00	2.12	1.29
			204	218.33	-0.36	0.00	0.00	0.81	1.29
413	Primo Impalcato	57, 93	0	32.85	-0.10	0.00	0.00	1.34	-0.74
			103	32.85	-0.10	0.00	0.00	2.10	-0.74
			206	32.85	-0.10	0.00	0.00	2.86	-0.74
414	Primo Impalcato	93, 58	0	-53.64	-0.37	0.00	0.00	-6.43	-1.29
			103	-53.64	-0.37	0.00	0.00	-5.11	-1.29
			206	-53.64	-0.37	0.00	0.00	-3.78	-1.29
415	Primo Impalcato	61, 95	0	5.06	-0.28	0.00	0.00	3.26	4.59
			100	5.06	-0.28	0.00	0.00	-1.34	4.59
			200	5.06	-0.28	0.00	0.00	-5.94	4.59
416	Primo Impalcato	95, 62	0	-0.93	0.02	0.00	0.00	-7.70	-3.57
			100	-0.93	0.02	0.00	0.00	-4.13	-3.57
			200	-0.93	0.02	0.00	0.00	-0.56	-3.57
417	Primo Impalcato	96, 65	0	-7.33	0.00	0.00	0.00	7.64	3.48
			100	-7.33	0.00	0.00	0.00	4.16	3.48
			200	-7.33	0.00	0.00	0.00	0.67	3.48
418	Primo Impalcato	66, 96	0	12.41	0.29	0.00	0.00	-3.61	-4.60
			100	12.41	0.29	0.00	0.00	1.00	-4.60
			200	12.41	0.29	0.00	0.00	5.61	-4.60
419	Primo Impalcato	69, 94	0	-62.66	0.37	0.00	0.00	-2.68	1.43
			103	-62.66	0.37	0.00	0.00	-4.16	1.43
			206	-62.66	0.37	0.00	0.00	-5.63	1.43
420	Primo Impalcato	79, 70	0	201.15	0.30	0.00	0.00	0.75	-1.08
			102	201.15	0.30	0.00	0.00	1.85	-1.08
			204	201.15	0.30	0.00	0.00	2.96	-1.08
421	Primo Impalcato	94, 70	0	50.08	0.06	0.00	0.00	2.71	0.54
			103	50.08	0.06	0.00	0.00	2.15	0.54
			206	50.08	0.06	0.00	0.00	1.59	0.54
422	Copertura	1, 2	0	-1681.74	66.19	-14.93	108.20	-2553.47	-911.33
			83	-1682.57	66.19	75.01	108.20	-1802.32	-895.93
			166	-1683.44	66.19	164.94	108.20	-1064.19	-880.00
423	Copertura	15, 1	0	-756.86	-5.75	515.22	-152.91	223.32	1745.51
			80	-756.86	-5.75	393.65	-152.91	-1164.36	1745.51
			159	-756.86	-5.75	272.09	-152.91	-2552.04	1745.51
424	Copertura	2, 3	0	-1702.74	100.23	169.37	-62.14	-1068.46	-668.42
			69	-1702.74	100.23	126.49	-62.14	-611.42	-656.33
			138	-1702.74	100.23	83.61	-62.14	-162.72	-644.25
425	Copertura	3, 4	0	-1702.46	151.04	84.21	-57.81	-167.91	-499.98
			69	-1702.46	151.04	44.32	-57.81	172.91	-487.89
			138	-1702.46	151.04	4.43	-57.81	505.39	-475.81
426	Copertura	4, 5	0	-1702.23	156.72	4.95	-48.76	499.64	-348.61
			69	-1702.23	156.72	-28.69	-48.76	736.02	-336.53
			138	-1702.23	156.72	-62.34	-48.76	964.05	-324.44
427	Copertura	5, 6	0	-1702.04	123.09	-61.93	-34.73	959.22	-221.52
			69	-1702.04	123.09	-85.90	-34.73	1107.90	-209.44
			138	-1702.04	123.09	-109.87	-34.73	1248.24	-197.35
428	Copertura	6, 7	0	-1698.63	62.75	-109.67	-7.38	1242.32	-112.04
			69	-1698.63	62.75	-114.77	-7.38	1315.46	-99.95
			138	-1698.63	62.75	-119.86	-7.38	1380.25	-87.87

429	Copertura	7, 8	0	-1699.76	-4.99	-119.90	9.22	1380.50	-11.93
			69	-1699.76	-4.99	-113.53	9.22	1384.56	0.16
			138	-1699.76	-4.99	-107.17	9.22	1380.28	12.24
430	Copertura	8, 9	0	-1699.89	-69.22	-107.46	21.73	1381.49	89.93
			69	-1699.89	-69.22	-92.46	21.73	1315.27	102.01
			138	-1699.89	-69.22	-77.47	21.73	1240.72	114.10
431	Copertura	9, 10	0	-1705.95	-126.57	-77.92	6.81	1243.89	198.63
			69	-1705.95	-126.57	-73.22	6.81	1102.67	210.71
			138	-1705.95	-126.57	-68.52	6.81	953.11	222.80
432	Copertura	10, 11	0	-1716.48	-164.51	-69.17	65.01	961.49	327.48
			69	-1716.48	-164.51	-24.31	65.01	731.36	339.56
			138	-1716.48	-164.51	20.54	65.01	492.90	351.65
433	Copertura	11, 12	0	-1716.85	-158.05	19.73	76.36	498.87	479.91
			69	-1716.85	-158.05	72.42	76.36	163.56	491.99
			138	-1716.85	-158.05	125.10	76.36	-180.08	504.08
434	Copertura	12, 13	0	-1717.25	-102.86	124.25	72.26	-174.62	651.70
			69	-1717.25	-102.86	174.11	72.26	-628.47	663.79
			138	-1717.25	-102.86	223.97	72.26	-1090.65	675.87
435	Copertura	13, 14	0	-1697.12	-40.23	220.79	-126.66	-1085.77	902.81
			83	-1696.26	-40.23	115.51	-126.66	-1842.85	918.74
			166	-1695.42	-40.23	10.22	-126.66	-2612.96	934.14
436	Copertura	16, 14	0	-789.34	6.39	415.02	-169.87	-206.41	-1762.69
			80	-789.34	6.39	279.98	-169.87	1194.93	-1762.69
			159	-789.34	6.39	144.93	-169.87	2596.27	-1762.69
437	Copertura	15, 17	0	-708.17	7.35	621.47	-167.80	-222.71	-99.69
			66	-708.17	7.35	510.72	-167.80	-156.92	-99.69
			132	-708.17	7.35	399.97	-167.80	-91.12	-99.69
438	Copertura	16, 18	0	-766.64	-7.19	460.10	-98.69	191.09	81.88
			66	-766.64	-7.19	394.96	-98.69	137.05	81.88
			132	-766.64	-7.19	329.82	-98.69	83.00	81.88
439	Copertura	17, 19	0	-659.26	3.96	507.15	-168.65	-97.09	-81.27
			66	-659.26	3.96	395.83	-168.65	-43.46	-81.27
			132	-659.26	3.96	284.52	-168.65	10.18	-81.27
440	Copertura	18, 20	0	-710.33	-3.93	404.87	-83.74	76.22	64.83
			66	-710.33	-3.93	349.61	-83.74	33.43	64.83
			132	-710.33	-3.93	294.34	-83.74	-9.35	64.83
441	Copertura	19, 21	0	-609.55	0.51	393.36	-247.91	2.95	-2.80
			66	-609.55	0.51	229.75	-247.91	4.80	-2.80
			132	-609.55	0.51	66.13	-247.91	6.64	-2.80
442	Copertura	20, 22	0	-657.24	-0.51	368.15	-211.72	-15.42	-11.99
			66	-657.24	-0.51	228.41	-211.72	-7.51	-11.99
			132	-657.24	-0.51	88.68	-211.72	0.40	-11.99
443	Copertura	21, 23	0	-559.51	-0.50	175.76	-128.88	-0.29	-3.74
			66	-559.51	-0.50	90.70	-128.88	2.17	-3.74
			132	-559.51	-0.50	5.64	-128.88	4.64	-3.74
444	Copertura	22, 24	0	-599.04	0.56	167.35	-78.27	-6.58	-9.12
			66	-599.04	0.56	115.70	-78.27	-0.56	-9.12
			132	-599.04	0.56	64.04	-78.27	5.47	-9.12
445	Copertura	23, 25	0	-509.36	-0.01	115.57	-143.00	-2.20	-13.03
			66	-509.36	-0.01	21.19	-143.00	6.41	-13.03
			132	-509.36	-0.01	-73.19	-143.00	15.01	-13.03
446	Copertura	24, 26	0	-541.90	-0.03	142.16	-156.83	-1.49	1.88
			66	-541.90	-0.03	38.65	-156.83	-2.73	1.88
			132	-541.90	-0.03	-64.87	-156.83	-3.97	1.88
447	Copertura	25, 28	0	-459.22	-0.23	36.76	2.04	8.52	6.81
			85	-459.22	-0.23	38.49	2.04	2.73	6.81
			170	-459.22	-0.23	40.23	2.04	-3.06	6.81
448	Copertura	26, 27	0	-483.39	0.48	14.43	-24.46	-10.78	-15.38
			66	-483.39	0.48	-1.72	-24.46	-0.63	-15.38
			132	-483.39	0.48	-17.86	-24.46	9.52	-15.38
449	Copertura	27, 29	0	-425.84	-0.15	60.95	-119.46	2.78	-1.94
			66	-425.84	-0.15	-17.90	-119.46	4.06	-1.94
			132	-425.84	-0.15	-96.74	-119.46	5.34	-1.94
450	Copertura	28, 30	0	-409.05	0.10	149.92	-98.85	-9.33	-6.71
			73	-409.05	0.10	77.75	-98.85	-4.43	-6.71
			146	-409.05	0.10	5.59	-98.85	0.48	-6.71
451	Copertura	29, 31	0	-367.68	0.06	-17.70	-4.42	-1.32	-2.22
			66	-367.68	0.06	-20.62	-4.42	0.15	-2.22
			132	-367.68	0.06	-23.54	-4.42	1.61	-2.22
452	Copertura	30, 32	0	-358.53	-0.02	116.35	-110.36	-6.02	-6.38
			69	-358.53	-0.02	40.75	-110.36	-1.65	-6.38
			137	-358.53	-0.02	-34.84	-110.36	2.73	-6.38

453	Copertura	31, 33	0	-309.63	-0.15	55.30	-106.27	-5.10	-5.29
			66	-309.63	-0.15	-14.83	-106.27	-1.61	-5.29
			132	-309.63	-0.15	-84.97	-106.27	1.89	-5.29
454	Copertura	32, 34	0	-308.27	0.07	75.61	-93.44	-3.88	-4.34
			69	-308.27	0.07	11.14	-93.44	-0.89	-4.34
			138	-308.27	0.07	-53.34	-93.44	2.10	-4.34
455	Copertura	33, 35	0	-254.70	0.14	-8.14	3.98	-4.98	-5.45
			66	-254.70	0.14	-5.51	3.98	-1.38	-5.45
			132	-254.70	0.14	-2.89	3.98	2.21	-5.45
456	Copertura	34, 36	0	-257.91	-0.07	57.13	-86.79	-4.62	-4.95
			69	-257.91	-0.07	-2.75	-86.79	-1.20	-4.95
			138	-257.91	-0.07	-62.63	-86.79	2.22	-4.95
457	Copertura	35, 37	0	-193.40	-0.15	79.20	-100.14	-4.75	-5.96
			66	-193.40	-0.15	13.11	-100.14	-0.81	-5.96
			132	-193.40	-0.15	-52.98	-100.14	3.12	-5.96
458	Copertura	36, 38	0	-207.49	0.07	47.84	-93.91	-4.62	-6.80
			69	-207.49	0.07	-16.96	-93.91	0.07	-6.80
			138	-207.49	0.07	-81.75	-93.91	4.76	-6.80
459	Copertura	37, 39	0	-135.41	0.19	25.81	8.79	-3.92	-9.46
			66	-135.41	0.19	31.61	8.79	2.33	-9.46
			132	-135.41	0.19	37.41	8.79	8.58	-9.46
460	Copertura	38, 40	0	-157.18	-0.03	28.75	-113.43	-2.11	-5.30
			69	-157.18	-0.03	-48.96	-113.43	1.53	-5.30
			137	-157.18	-0.03	-126.66	-113.43	5.16	-5.30
461	Copertura	39, 41	0	-76.09	-0.07	116.80	-127.62	1.76	-28.71
			66	-76.09	-0.07	32.57	-127.62	20.70	-28.71
			132	-76.09	-0.07	-51.65	-127.62	39.65	-28.71
462	Copertura	40, 42	0	-107.35	0.26	-16.00	-118.30	-1.53	9.87
			69	-107.35	0.26	-97.63	-118.30	-8.34	9.87
			138	-107.35	0.26	-179.25	-118.30	-15.15	9.87
463	Copertura	41, 44	0	-21.95	-0.67	27.11	-85.09	33.71	52.22
			66	-21.95	-0.67	-29.05	-85.09	-0.76	52.22
			132	-21.95	-0.67	-85.21	-85.09	-35.22	52.22
464	Copertura	42, 43	0	-53.04	-1.07	-68.97	-39.12	-21.82	-78.76
			23	-53.04	-1.07	-77.97	-39.12	-3.71	-78.76
			46	-53.04	-1.07	-86.97	-39.12	14.41	-78.76
465	Copertura	43, 45	0	-3.36	0.05	22.23	-29.45	7.62	6.59
			66	-3.36	0.05	2.79	-29.45	3.26	6.59
			132	-3.36	0.05	-16.64	-29.45	-1.09	6.59
466	Copertura	44, 46	0	35.87	0.22	-7.02	-40.94	-41.27	-27.02
			66	35.87	0.22	-34.04	-40.94	-23.43	-27.02
			132	35.87	0.22	-61.06	-40.94	-5.60	-27.02
467	Copertura	45, 47	0	46.82	0.08	93.18	-148.62	-8.36	-6.58
			66	46.82	0.08	-4.91	-148.62	-4.02	-6.58
			132	46.82	0.08	-103.00	-148.62	0.32	-6.58
468	Copertura	46, 48	0	92.55	0.16	16.12	-69.19	-12.90	-11.38
			66	92.55	0.16	-29.54	-69.19	-5.39	-11.38
			132	92.55	0.16	-75.20	-69.19	2.12	-11.38
469	Copertura	47, 49	0	96.95	-0.25	6.71	-114.50	-7.38	-7.85
			66	96.95	-0.25	-68.86	-114.50	-2.20	-7.85
			132	96.95	-0.25	-144.43	-114.50	2.98	-7.85
470	Copertura	48, 50	0	149.67	0.41	2.24	-70.95	-5.72	-9.28
			66	149.67	0.41	-44.59	-70.95	0.40	-9.28
			132	149.67	0.41	-91.42	-70.95	6.52	-9.28
471	Copertura	49, 51	0	147.05	0.37	-34.87	-221.17	-4.85	-6.44
			66	147.05	0.37	-180.84	-221.17	-0.59	-6.44
			132	147.05	0.37	-326.82	-221.17	3.66	-6.44
472	Copertura	50, 52	0	205.99	-0.17	-14.65	-138.11	-1.35	-10.50
			66	205.99	-0.17	-105.80	-138.11	5.58	-10.50
			132	205.99	-0.17	-196.95	-138.11	12.51	-10.50
473	Copertura	51, 53	0	196.88	2.27	-217.84	-152.69	-4.13	-44.04
			66	196.88	2.27	-318.61	-152.69	24.94	-44.04
			132	196.88	2.27	-419.38	-152.69	54.01	-44.04
474	Copertura	52, 54	0	262.68	-2.21	-120.20	-202.08	5.16	26.43
			66	262.68	-2.21	-253.57	-202.08	-12.28	26.43
			132	262.68	-2.21	-386.95	-202.08	-29.73	26.43
475	Copertura	53, 55	0	246.08	4.22	-311.68	-180.39	47.15	-52.72
			66	246.08	4.22	-430.74	-180.39	81.94	-52.72
			132	246.08	4.22	-549.80	-180.39	116.74	-52.72
476	Copertura	54, 56	0	313.18	-3.62	-316.18	-69.82	-36.36	35.66
			66	313.18	-3.62	-362.26	-69.82	-59.89	35.66
			132	313.18	-3.62	-408.34	-69.82	-83.42	35.66

477	Copertura	55, 57	0	295.27	-1.90	-442.48	92.50	113.65	834.10
			80	295.27	-1.90	-368.93	92.50	-549.46	834.10
			159	295.27	-1.90	-295.39	92.50	-1212.57	834.10
478	Copertura	56, 70	0	367.80	2.48	-335.89	121.74	-92.40	-856.70
			80	367.80	2.48	-239.11	121.74	588.68	-856.70
			159	367.80	2.48	-142.33	121.74	1269.76	-856.70
479	Copertura	57, 58	0	814.20	60.35	39.23	-53.26	-1213.64	-429.24
			83	814.61	60.35	-5.04	-53.26	-860.03	-421.53
			166	815.05	60.35	-49.31	-53.26	-512.94	-413.57
480	Copertura	58, 59	0	824.69	50.57	-52.79	12.63	-514.62	-322.52
			69	824.69	50.57	-44.07	12.63	-294.17	-316.47
			138	824.69	50.57	-35.36	12.63	-77.89	-310.43
481	Copertura	59, 60	0	824.65	72.40	-35.45	17.38	-80.30	-242.09
			69	824.65	72.40	-23.46	17.38	84.66	-236.04
			138	824.65	72.40	-11.47	17.38	245.44	-230.00
482	Copertura	60, 61	0	824.60	75.39	-11.56	20.26	242.70	-168.78
			69	824.60	75.39	2.42	20.26	357.07	-162.74
			138	824.60	75.39	16.40	20.26	467.28	-156.70
483	Copertura	61, 62	0	823.59	56.47	16.35	13.37	463.41	-107.22
			69	823.59	56.47	25.58	13.37	535.31	-101.17
			138	823.59	56.47	34.81	13.37	603.03	-95.13
484	Copertura	62, 63	0	824.43	27.85	34.84	4.69	601.74	-55.22
			69	824.43	27.85	38.08	4.69	637.76	-49.18
			138	824.43	27.85	41.32	4.69	669.61	-43.14
485	Copertura	63, 64	0	824.48	-3.70	41.44	-4.14	669.20	-5.90
			69	824.48	-3.70	38.59	-4.14	671.19	0.14
			138	824.48	-3.70	35.73	-4.14	669.01	6.18
486	Copertura	64, 65	0	824.59	-35.11	35.96	-11.22	669.64	43.77
			69	824.59	-35.11	28.22	-11.22	637.36	49.81
			138	824.59	-35.11	20.48	-11.22	600.90	55.86
487	Copertura	65, 66	0	828.33	-63.24	20.76	-0.69	602.51	96.69
			69	828.33	-63.24	20.29	-0.69	533.71	102.74
			138	828.33	-63.24	19.81	-0.69	460.73	108.78
488	Copertura	66, 67	0	834.23	-81.84	20.17	-31.38	464.90	159.65
			69	834.23	-81.84	-1.49	-31.38	352.66	165.69
			138	834.23	-81.84	-23.14	-31.38	236.25	171.73
489	Copertura	67, 68	0	834.43	-78.61	-22.72	-33.22	239.20	234.41
			69	834.43	-78.61	-45.64	-33.22	75.38	240.45
			138	834.43	-78.61	-68.55	-33.22	-92.62	246.50
490	Copertura	68, 69	0	834.62	-53.01	-68.14	-26.17	-89.95	318.23
			69	834.62	-53.01	-86.20	-26.17	-311.61	324.27
			138	834.62	-53.01	-104.25	-26.17	-537.44	330.31
491	Copertura	69, 70	0	824.62	-34.18	-101.95	64.55	-535.14	436.61
			83	824.19	-34.18	-48.29	64.55	-901.38	444.57
			166	823.77	-34.18	5.37	64.55	-1274.13	452.27
492	Copertura	1	0	-190.20	-0.84	-201.18	58.05	16.85	9.71
			220	-190.20	-0.84	-33.46	102.01	-4.50	9.71
			440	-190.20	-0.84	281.01	191.45	-25.85	9.71
493	Copertura	2	0	103.42	-2.75	40.84	-119.08	-0.96	-0.54
			220	103.42	-2.75	-143.03	-33.29	0.23	-0.54
			440	103.42	-2.75	-40.54	141.25	1.41	-0.54
494	Copertura	3	0	-4.33	-5.19	50.82	-144.27	-0.60	-0.28
			220	-4.33	-5.19	-190.43	-60.62	0.02	-0.28
			440	-4.33	-5.19	-152.45	109.57	0.63	-0.28
495	Copertura	4	0	-9.05	-5.74	5.67	-127.19	-0.53	-0.24
			220	-9.05	-5.74	-198.00	-43.54	0.00	-0.24
			440	-9.05	-5.74	-122.46	126.64	0.53	-0.24
496	Copertura	5	0	-14.02	-4.84	-33.63	-102.92	-0.40	-0.19
			220	-14.02	-4.84	-183.90	-19.27	0.00	-0.19
			440	-14.02	-4.84	-54.95	150.92	0.41	-0.19
497	Copertura	6	0	-16.76	-3.10	-53.26	-86.10	-0.19	-0.09
			220	-16.76	-3.10	-166.53	-2.45	0.00	-0.09
			440	-16.76	-3.10	-0.57	167.74	0.19	-0.09
498	Copertura	7	0	-13.07	-0.96	-64.05	-76.91	0.04	0.02
			220	-13.07	-0.96	-157.10	6.74	0.00	0.02
			440	-13.07	-0.96	29.06	176.92	-0.04	0.02
499	Copertura	8	0	-12.51	1.21	-64.23	-77.69	0.29	0.13
			220	-12.51	1.21	-158.98	5.96	-0.01	0.13
			440	-12.51	1.21	25.47	176.15	-0.30	0.13
500	Copertura	9	0	-3.75	3.27	-56.04	-85.24	0.46	0.20
			220	-3.75	3.27	-167.42	-1.59	0.01	0.20
			440	-3.75	3.27	0.43	168.60	-0.44	0.20

501	Copertura	10	0	-25.55	5.04	-29.91	-104.87	0.65	0.29
			220	-25.55	5.04	-184.47	-21.22	0.01	0.29
			440	-25.55	5.04	-59.80	148.97	-0.63	0.29
502	Copertura	11	0	-11.35	5.97	6.46	-128.26	0.82	0.38
			220	-11.35	5.97	-199.57	-44.61	-0.01	0.38
			440	-11.35	5.97	-126.37	125.57	-0.84	0.38
503	Copertura	12	0	4.10	5.46	55.19	-147.62	0.85	0.40
			220	4.10	5.46	-193.44	-63.97	-0.03	0.40
			440	4.10	5.46	-162.84	106.21	-0.90	0.40
504	Copertura	13	0	131.17	3.17	71.98	-134.24	1.18	0.65
			220	131.17	3.17	-145.24	-48.45	-0.25	0.65
			440	131.17	3.17	-76.11	126.09	-1.68	0.65
505	Copertura	57	0	108.38	0.89	-226.39	84.47	-37.45	-16.03
			220	108.38	0.89	-20.54	106.45	-2.19	-16.03
			440	108.38	0.89	258.68	151.17	33.06	-16.03
506	Copertura	58	0	-35.85	-1.06	-7.85	-45.67	0.24	0.15
			220	-35.85	-1.06	-69.28	-2.78	-0.08	0.15
			440	-35.85	-1.06	12.44	84.47	-0.40	0.15
507	Copertura	59	0	-4.75	-2.41	21.83	-68.35	0.09	0.04
			220	-4.75	-2.41	-90.46	-26.53	0.00	0.04
			440	-4.75	-2.41	-63.16	58.56	-0.09	0.04
508	Copertura	60	0	-2.88	-2.75	2.99	-61.22	0.09	0.04
			220	-2.88	-2.75	-93.62	-19.40	0.00	0.04
			440	-2.88	-2.75	-50.64	65.68	-0.10	0.04
509	Copertura	61	0	3.70	-2.30	-15.12	-49.64	0.04	0.02
			220	3.70	-2.30	-86.25	-7.82	0.00	0.02
			440	3.70	-2.30	-17.80	77.26	-0.05	0.02
510	Copertura	62	0	6.05	-1.42	-27.79	-40.32	-0.04	-0.02
			220	6.05	-1.42	-78.43	1.50	0.00	-0.02
			440	6.05	-1.42	10.53	86.58	0.03	-0.02
511	Copertura	63	0	8.83	-0.41	-31.55	-37.24	-0.12	-0.06
			220	8.83	-0.41	-75.41	4.58	0.00	-0.06
			440	8.83	-0.41	20.33	89.66	0.12	-0.06
512	Copertura	64	0	7.08	0.64	-31.41	-37.59	-0.23	-0.11
			220	7.08	0.64	-76.03	4.23	0.01	-0.11
			440	7.08	0.64	18.94	89.31	0.24	-0.11
513	Copertura	65	0	1.00	1.64	-27.52	-41.22	-0.28	-0.13
			220	1.00	1.64	-80.12	0.60	-0.01	-0.13
			440	1.00	1.64	6.86	85.69	0.27	-0.13
514	Copertura	66	0	12.42	2.51	-14.62	-50.99	-0.36	-0.16
			220	12.42	2.51	-88.73	-9.17	0.00	-0.16
			440	12.42	2.51	-23.26	75.91	0.35	-0.16
515	Copertura	67	0	1.83	2.95	3.23	-62.68	-0.42	-0.20
			220	1.83	2.95	-96.61	-20.86	0.01	-0.20
			440	1.83	2.95	-56.85	64.22	0.44	-0.20
516	Copertura	68	0	-7.05	2.67	25.60	-71.73	-0.42	-0.19
			220	-7.05	2.67	-94.14	-29.91	0.01	-0.19
			440	-7.05	2.67	-74.30	55.17	0.44	-0.19
517	Copertura	69	0	-58.65	1.49	23.16	-60.98	-0.54	-0.29
			220	-58.65	1.49	-71.95	-18.09	0.10	-0.29
			440	-58.65	1.49	-23.90	69.17	0.74	-0.29
518	Primo Impalcato	1, 74	0	71.53	-0.65	0.00	0.00	-14.60	-7.15
			118	71.53	-0.65	0.00	0.00	-6.19	-7.15
			235	71.53	-0.65	0.00	0.00	2.22	-7.15
519	Copertura	74, 2	0	-75.80	-0.06	0.00	0.00	-3.24	-6.01
			118	-75.80	-0.06	0.00	0.00	3.83	-6.01
			235	-75.80	-0.06	0.00	0.00	10.89	-6.01
520	Primo Impalcato	6, 71	0	-3.70	-0.22	0.00	0.00	0.38	-0.50
			115	-3.70	-0.22	0.00	0.00	0.96	-0.50
			231	-3.70	-0.22	0.00	0.00	1.53	-0.50
521	Copertura	71, 7	0	-11.11	-0.29	0.00	0.00	5.75	1.25
			115	-11.11	-0.29	0.00	0.00	4.30	1.25
			231	-11.11	-0.29	0.00	0.00	2.86	1.25
522	Primo Impalcato	9, 72	0	-34.21	0.53	0.00	0.00	5.40	-1.22
			115	-34.21	0.53	0.00	0.00	6.80	-1.22
			231	-34.21	0.53	0.00	0.00	8.21	-1.22
523	Copertura	72, 10	0	19.56	0.52	0.00	0.00	-0.49	-0.32
			115	19.56	0.52	0.00	0.00	-0.12	-0.32
			231	19.56	0.52	0.00	0.00	0.25	-0.32
524	Copertura	73, 13	0	-69.48	0.08	0.00	0.00	1.55	5.60

			118	-69.48	0.08	0.00	0.00	-5.03	5.60
			235	-69.48	0.08	0.00	0.00	-11.61	5.60
525	Primo Impalcato	14, 73	0	72.42	0.76	0.00	0.00	9.98	4.40
			118	72.42	0.76	0.00	0.00	4.80	4.40
			235	72.42	0.76	0.00	0.00	-0.37	4.40
526	Primo Impalcato	57, 75	0	-32.12	-0.23	0.00	0.00	-11.65	-6.12
			118	-32.12	-0.23	0.00	0.00	-4.46	-6.12
			235	-32.12	-0.23	0.00	0.00	2.73	-6.12
527	Copertura	75, 58	0	39.96	-0.02	0.00	0.00	-3.08	-3.36
			118	39.96	-0.02	0.00	0.00	0.87	-3.36
			235	39.96	-0.02	0.00	0.00	4.82	-3.36
528	Copertura	77, 61	0	2.76	-0.23	0.00	0.00	0.18	0.08
			115	2.76	-0.23	0.00	0.00	0.09	0.08
			231	2.76	-0.23	0.00	0.00	0.00	0.08
529	Primo Impalcato	62, 77	0	3.34	-0.24	0.00	0.00	-2.25	0.64
			115	3.34	-0.24	0.00	0.00	-2.99	0.64
			231	3.34	-0.24	0.00	0.00	-3.73	0.64
530	Primo Impalcato	65, 78	0	19.16	0.26	0.00	0.00	2.53	-0.64
			115	19.16	0.26	0.00	0.00	3.26	-0.64
			231	19.16	0.26	0.00	0.00	4.00	-0.64
531	Copertura	78, 66	0	-12.09	0.26	0.00	0.00	-0.34	-0.13
			115	-12.09	0.26	0.00	0.00	-0.18	-0.13
			231	-12.09	0.26	0.00	0.00	-0.03	-0.13
532	Primo Impalcato	69, 76	0	39.65	0.04	0.00	0.00	5.60	2.98
			118	39.65	0.04	0.00	0.00	2.10	2.98
			235	39.65	0.04	0.00	0.00	-1.40	2.98
533	Copertura	76, 70	0	-34.28	0.34	0.00	0.00	0.87	3.40
			118	-34.28	0.34	0.00	0.00	-3.12	3.40
			235	-34.28	0.34	0.00	0.00	-7.12	3.40
534	Copertura	1, 74	0	-75.80	0.86	0.00	0.00	3.96	2.60
			118	-75.80	0.86	0.00	0.00	0.90	2.60
			235	-75.80	0.86	0.00	0.00	-2.16	2.60
535	Copertura	74, 2	0	71.53	-0.63	0.00	0.00	0.80	1.46
			118	71.53	-0.63	0.00	0.00	-0.91	1.46
			235	71.53	-0.63	0.00	0.00	-2.63	1.46
536	Copertura	6, 71	0	-11.11	-0.58	0.00	0.00	7.60	0.78
			115	-11.11	-0.58	0.00	0.00	6.70	0.78
			231	-11.11	-0.58	0.00	0.00	5.80	0.78
537	Copertura	71, 7	0	-3.70	0.04	0.00	0.00	1.65	-0.97
			115	-3.70	0.04	0.00	0.00	2.77	-0.97
			231	-3.70	0.04	0.00	0.00	3.89	-0.97
538	Copertura	9, 72	0	19.56	0.30	0.00	0.00	1.28	0.71
			115	19.56	0.30	0.00	0.00	0.47	0.71
			231	19.56	0.30	0.00	0.00	-0.35	0.71
539	Copertura	72, 10	0	-34.21	0.79	0.00	0.00	8.22	-0.19
			115	-34.21	0.79	0.00	0.00	8.44	-0.19
			231	-34.21	0.79	0.00	0.00	8.66	-0.19
540	Copertura	73, 13	0	72.42	0.66	0.00	0.00	1.01	-0.89
			118	72.42	0.66	0.00	0.00	2.06	-0.89
			235	72.42	0.66	0.00	0.00	3.10	-0.89
541	Copertura	14, 73	0	-69.48	-0.76	0.00	0.00	1.17	0.31
			118	-69.48	-0.76	0.00	0.00	0.81	0.31
			235	-69.48	-0.76	0.00	0.00	0.44	0.31
542	Copertura	15, 125	0	1789.28	4.18	-51.13	88.31	-1.68	1.85
			75	1789.28	4.18	15.10	88.31	-3.07	1.85
			150	1789.28	4.18	81.34	88.31	-4.46	1.85
543	Copertura	127, 16	0	1799.48	-0.96	71.64	-79.92	-10.13	2.41
			75	1799.48	-0.96	11.71	-79.92	-11.94	2.41
			150	1799.48	-0.96	-48.23	-79.92	-13.75	2.41
544	Copertura	17, 129	0	-23.46	4.61	4.68	15.96	4.42	2.41
			75	-23.46	4.61	16.65	15.96	2.61	2.41
			150	-23.46	4.61	28.62	15.96	0.81	2.41
545	Copertura	130, 18	0	-16.49	-2.79	21.33	-10.43	-8.38	-0.86
			75	-16.49	-2.79	13.51	-10.43	-7.74	-0.86
			150	-16.49	-2.79	5.69	-10.43	-7.10	-0.86
546	Copertura	19, 135	0	-80.49	4.63	1.83	0.74	5.84	2.25
			75	-80.49	4.63	2.39	0.74	4.15	2.25
			150	-80.49	4.63	2.94	0.74	2.47	2.25

547	Copertura	134, 20	0	-75.44	-2.80	-3.61	3.00	-7.55	-0.73
			75	-75.44	-2.80	-1.36	3.00	-7.00	-0.73
			150	-75.44	-2.80	0.89	3.00	-6.45	-0.73
548	Copertura	21, 136	0	2.42	4.62	3.82	-3.07	5.63	2.16
			75	2.42	4.62	1.52	-3.07	4.01	2.16
			150	2.42	4.62	-0.79	-3.07	2.39	2.16
549	Copertura	138, 22	0	9.62	-2.83	-8.33	8.75	-7.85	-0.52
			75	9.62	-2.83	-1.77	8.75	-7.46	-0.52
			150	9.62	-2.83	4.79	8.75	-7.07	-0.52
550	Copertura	23, 141	0	6.55	4.63	-1.29	2.80	5.52	2.16
			75	6.55	4.63	0.81	2.80	3.89	2.16
			150	6.55	4.63	2.91	2.80	2.27	2.16
551	Copertura	142, 24	0	10.69	-2.82	-3.06	0.14	-7.81	-0.50
			75	10.69	-2.82	-2.95	0.14	-7.44	-0.50
			150	10.69	-2.82	-2.84	0.14	-7.06	-0.50
552	Copertura	25, 145	0	-18.16	4.63	4.55	-1.16	5.19	2.13
			75	-18.16	4.63	3.68	-1.16	3.59	2.13
			150	-18.16	4.63	2.81	-1.16	1.99	2.13
553	Copertura	146, 26	0	-11.09	-2.88	-5.13	6.60	-7.87	-0.62
			75	-11.09	-2.88	-0.17	6.60	-7.41	-0.62
			150	-11.09	-2.88	4.78	6.60	-6.95	-0.62
554	Copertura	150, 27	0	1.43	-2.86	3.42	-11.68	-7.80	-0.61
			75	1.43	-2.86	-5.34	-11.68	-7.34	-0.61
			150	1.43	-2.86	-14.10	-11.68	-6.89	-0.61
555	Copertura	28, 149	0	23.66	4.60	13.88	-8.56	4.97	2.09
			75	23.66	4.60	7.46	-8.56	3.40	2.09
			150	23.66	4.60	1.03	-8.56	1.83	2.09
556	Copertura	154, 29	0	-10.02	-2.86	2.15	-8.81	-7.69	-0.60
			75	-10.02	-2.86	-4.46	-8.81	-7.24	-0.60
			150	-10.02	-2.86	-11.07	-8.81	-6.80	-0.60
557	Copertura	30, 153	0	18.15	4.64	23.71	-16.64	5.17	2.13
			75	18.15	4.64	11.24	-16.64	3.57	2.13
			150	18.15	4.64	-1.24	-16.64	1.97	2.13
558	Copertura	158, 31	0	-20.50	-2.84	5.50	-16.37	-7.71	-0.58
			75	-20.50	-2.84	-6.78	-16.37	-7.28	-0.58
			150	-20.50	-2.84	-19.06	-16.37	-6.84	-0.58
559	Copertura	32, 157	0	19.73	4.63	26.65	-19.85	5.28	2.13
			75	19.73	4.63	11.76	-19.85	3.68	2.13
			150	19.73	4.63	-3.13	-19.85	2.08	2.13
560	Copertura	162, 33	0	-13.17	-2.79	3.60	-11.75	-7.76	-0.49
			75	-13.17	-2.79	-5.21	-11.75	-7.39	-0.49
			150	-13.17	-2.79	-14.02	-11.75	-7.03	-0.49
561	Copertura	34, 161	0	24.57	4.63	29.24	-22.08	5.39	2.15
			75	24.57	4.63	12.69	-22.08	3.78	2.15
			150	24.57	4.63	-3.87	-22.08	2.17	2.15
562	Copertura	166, 35	0	-22.75	-2.92	8.13	-20.97	-8.01	-0.63
			75	-22.75	-2.92	-7.60	-20.97	-7.54	-0.63
			150	-22.75	-2.92	-23.32	-20.97	-7.07	-0.63
563	Copertura	36, 165	0	28.67	4.64	31.38	-24.83	5.50	2.15
			75	28.67	4.64	12.76	-24.83	3.89	2.15
			150	28.67	4.64	-5.86	-24.83	2.27	2.15
564	Copertura	170, 37	0	-21.01	-2.82	6.27	-15.97	-7.96	-0.53
			75	-21.01	-2.82	-5.70	-15.97	-7.56	-0.53
			150	-21.01	-2.82	-17.68	-15.97	-7.16	-0.53
565	Copertura	38, 169	0	27.68	4.62	34.06	-27.20	5.53	2.16
			75	27.68	4.62	13.66	-27.20	3.91	2.16
			150	27.68	4.62	-6.74	-27.20	2.29	2.16
566	Copertura	175, 39	0	-45.69	-2.84	11.36	-25.22	-7.80	-0.57
			75	-45.69	-2.84	-7.56	-25.22	-7.38	-0.57
			150	-45.69	-2.84	-26.47	-25.22	-6.95	-0.57
567	Copertura	40, 173	0	17.66	4.62	36.78	-30.77	5.35	2.14
			75	17.66	4.62	13.70	-30.77	3.75	2.14
			150	17.66	4.62	-9.38	-30.77	2.15	2.14
568	Copertura	178, 41	0	55.90	-2.81	11.84	-24.46	-6.79	-0.52
			75	55.90	-2.81	-6.50	-24.46	-6.41	-0.52
			150	55.90	-2.81	-24.84	-24.46	-6.02	-0.52
569	Copertura	42, 177	0	125.48	4.60	41.02	-36.47	5.29	2.11
			75	125.48	4.60	13.67	-36.47	3.71	2.11
			150	125.48	4.60	-13.69	-36.47	2.12	2.11
570	Copertura	43, 181	0	-87.35	4.63	0.80	3.65	5.43	2.16
			75	-87.35	4.63	3.54	3.65	3.81	2.16
			150	-87.35	4.63	6.27	3.65	2.19	2.16

571	Copertura	182, 44	0	-73.09	-2.82	-7.80	7.62	-6.89	-0.53
			75	-73.09	-2.82	-2.08	7.62	-6.49	-0.53
			150	-73.09	-2.82	3.64	7.62	-6.10	-0.53
572	Copertura	45, 185	0	7.18	4.64	-4.00	6.08	5.93	2.24
			75	7.18	4.64	0.56	6.08	4.25	2.24
			150	7.18	4.64	5.12	6.08	2.58	2.24
573	Copertura	186, 46	0	17.55	-2.79	-4.41	2.35	-8.11	-0.47
			75	17.55	-2.79	-2.65	2.35	-7.76	-0.47
			150	17.55	-2.79	-0.89	2.35	-7.41	-0.47
574	Copertura	47, 189	0	0.79	4.65	1.10	0.59	6.35	2.28
			75	0.79	4.65	1.54	0.59	4.64	2.28
			150	0.79	4.65	1.98	0.59	2.93	2.28
575	Copertura	190, 48	0	3.44	-2.77	-1.69	1.34	-8.50	-0.39
			75	3.44	-2.77	-0.69	1.34	-8.20	-0.39
			150	3.44	-2.77	0.31	1.34	-7.90	-0.39
576	Copertura	49, 193	0	-5.05	4.64	-3.51	4.72	6.48	2.29
			75	-5.05	4.64	0.03	4.72	4.76	2.29
			150	-5.05	4.64	3.57	4.72	3.05	2.29
577	Copertura	195, 50	0	-3.02	-2.75	2.22	-2.96	-8.51	-0.38
			75	-3.02	-2.75	0.00	-2.96	-8.23	-0.38
			150	-3.02	-2.75	-2.22	-2.96	-7.95	-0.38
578	Copertura	51, 197	0	38.92	4.63	-0.25	-0.47	6.40	2.31
			75	38.92	4.63	-0.60	-0.47	4.67	2.31
			150	38.92	4.63	-0.96	-0.47	2.94	2.31
579	Copertura	199, 52	0	32.98	-2.79	2.67	-4.72	-8.26	-0.51
			75	32.98	-2.79	-0.86	-4.72	-7.88	-0.51
			150	32.98	-2.79	-4.40	-4.72	-7.50	-0.51
580	Copertura	53, 201	0	10.18	4.60	-3.44	-7.28	5.40	2.36
			75	10.18	4.60	-8.90	-7.28	3.63	2.36
			150	10.18	4.60	-14.37	-7.28	1.86	2.36
581	Copertura	202, 54	0	12.85	-2.74	-13.80	9.99	-8.33	-0.80
			75	12.85	-2.74	-6.30	9.99	-7.72	-0.80
			150	12.85	-2.74	1.19	9.99	-7.12	-0.80
582	Copertura	55, 205	0	-854.88	4.42	27.47	-50.47	1.87	2.01
			75	-854.88	4.42	-10.38	-50.47	0.36	2.01
			150	-854.88	4.42	-48.23	-50.47	-1.15	2.01
583	Copertura	206, 56	0	-867.48	-2.50	-35.53	40.55	-9.44	-0.38
			75	-867.48	-2.50	-5.11	40.55	-9.16	-0.38
			150	-867.48	-2.50	25.30	40.55	-8.88	-0.38
584	Copertura	57, 75	0	39.96	0.51	0.00	0.00	6.89	4.02
			118	39.96	0.51	0.00	0.00	2.16	4.02
			235	39.96	0.51	0.00	0.00	-2.57	4.02
585	Copertura	75, 58	0	-32.12	-0.30	0.00	0.00	2.00	1.27
			118	-32.12	-0.30	0.00	0.00	0.50	1.27
			235	-32.12	-0.30	0.00	0.00	-0.99	1.27
586	Copertura	77, 61	0	3.34	-0.36	0.00	0.00	-3.74	0.15
			115	3.34	-0.36	0.00	0.00	-3.92	0.15
			231	3.34	-0.36	0.00	0.00	-4.10	0.15
587	Copertura	62, 77	0	2.76	-0.13	0.00	0.00	-0.83	-0.41
			115	2.76	-0.13	0.00	0.00	-0.36	-0.41
			231	2.76	-0.13	0.00	0.00	0.11	-0.41
588	Copertura	65, 78	0	-12.09	0.15	0.00	0.00	0.60	0.38
			115	-12.09	0.15	0.00	0.00	0.17	0.38
			231	-12.09	0.15	0.00	0.00	-0.27	0.38
589	Copertura	78, 66	0	19.16	0.39	0.00	0.00	4.00	-0.13
			115	19.16	0.39	0.00	0.00	4.15	-0.13
			231	19.16	0.39	0.00	0.00	4.29	-0.13
590	Copertura	69, 76	0	-34.28	0.33	0.00	0.00	-1.45	-0.69
			118	-34.28	0.33	0.00	0.00	-0.64	-0.69
			235	-34.28	0.33	0.00	0.00	0.17	-0.69
591	Copertura	76, 70	0	39.65	-0.41	0.00	0.00	-0.86	-1.11
			118	39.65	-0.41	0.00	0.00	0.44	-1.11
			235	39.65	-0.41	0.00	0.00	1.75	-1.11
592	Copertura	79, 81	0	-58.25	0.06	57.47	-72.75	-26.10	-12.01
			80	-58.25	0.06	-0.37	-72.75	-16.56	-12.01
			159	-58.25	0.06	-58.20	-72.75	-7.01	-12.01
593	Copertura	80, 82	0	-43.91	-0.02	55.54	-82.64	-2.53	-3.66
			66	-43.91	-0.02	0.97	-82.64	-0.12	-3.66
			132	-43.91	-0.02	-53.61	-82.64	2.29	-3.66
594	Copertura	83, 84	0	-6.99	0.00	50.65	-76.83	0.53	0.37
			66	-6.99	0.00	-0.06	-76.83	0.29	0.37
			132	-6.99	0.00	-50.77	-76.83	0.04	0.37

595	Copertura	85, 86	0	-3.60	0.00	50.81	-77.11	-0.02	0.10
			66	-3.60	0.00	-0.09	-77.11	-0.08	0.10
			132	-3.60	0.00	-50.98	-77.11	-0.15	0.10
596	Copertura	87, 88	0	-1.87	0.00	50.96	-77.28	0.08	0.06
			66	-1.87	0.00	-0.05	-77.28	0.04	0.06
			132	-1.87	0.00	-51.05	-77.28	0.00	0.06
597	Copertura	89, 90	0	2.18	0.00	51.31	-77.90	0.04	0.08
			66	2.18	0.00	-0.10	-77.90	-0.02	0.08
			132	2.18	0.00	-51.51	-77.90	-0.07	0.08
598	Copertura	91, 92	0	4.09	0.00	49.83	-75.68	0.03	0.05
			66	4.09	0.00	-0.12	-75.68	0.00	0.05
			132	4.09	0.00	-50.07	-75.68	-0.04	0.05
599	Copertura	93, 94	0	-2.17	0.00	50.42	-76.57	0.17	-0.04
			66	-2.17	0.00	-0.12	-76.57	0.20	-0.04
			132	-2.17	0.00	-50.66	-76.57	0.23	-0.04
600	Copertura	95, 96	0	0.62	0.00	48.74	-73.84	-0.26	-0.07
			66	0.62	0.00	0.01	-73.84	-0.21	-0.07
			132	0.62	0.00	-48.73	-73.84	-0.16	-0.07
601	Copertura	97, 106	0	4.09	0.01	48.49	-73.20	0.02	0.02
			66	4.09	0.01	0.18	-73.20	0.01	0.02
			132	4.09	0.01	-48.13	-73.20	-0.01	0.02
602	Copertura	98, 99	0	-7.09	-0.08	68.97	-105.60	1.03	0.30
			66	-7.09	-0.08	-0.73	-105.60	0.84	0.30
			132	-7.09	-0.08	-70.42	-105.60	0.64	0.30
603	Copertura	100, 101	0	-2.01	0.01	72.60	-110.26	0.15	0.25
			66	-2.01	0.01	-0.17	-110.26	-0.02	0.25
			132	-2.01	0.01	-72.94	-110.26	-0.19	0.25
604	Copertura	102, 103	0	-1.12	0.00	73.24	-111.07	-0.01	0.02
			66	-1.12	0.00	-0.07	-111.07	-0.02	0.02
			132	-1.12	0.00	-73.38	-111.07	-0.03	0.02
605	Copertura	104, 105	0	-0.18	0.00	73.13	-110.79	0.13	0.18
			66	-0.18	0.00	0.01	-110.79	0.01	0.18
			132	-0.18	0.00	-73.11	-110.79	-0.11	0.18
606	Copertura	107, 108	0	7.43	-0.01	49.61	-75.18	-0.51	0.14
			66	7.43	-0.01	-0.01	-75.18	-0.60	0.14
			132	7.43	-0.01	-49.62	-75.18	-0.69	0.14
607	Copertura	109, 110	0	41.06	-0.03	42.93	-54.32	3.33	-7.06
			80	41.06	-0.03	-0.26	-54.32	8.94	-7.06
			159	41.06	-0.03	-43.44	-54.32	14.55	-7.06
608	Copertura	111, 112	0	10.62	0.00	73.09	-110.63	0.10	0.15
			66	10.62	0.00	0.02	-110.63	0.00	0.15
			132	10.62	0.00	-73.05	-110.63	-0.10	0.15
609	Copertura	113, 114	0	0.75	0.00	73.00	-110.53	0.11	0.11
			66	0.75	0.00	0.06	-110.53	0.04	0.11
			132	0.75	0.00	-72.89	-110.53	-0.03	0.11
610	Copertura	115, 116	0	0.88	-0.01	73.54	-111.16	0.58	0.88
			66	0.88	-0.01	0.18	-111.16	0.00	0.88
			132	0.88	-0.01	-73.19	-111.16	-0.58	0.88
611	Copertura	117, 118	0	0.99	0.01	72.83	-110.19	0.04	0.15
			66	0.99	0.01	0.10	-110.19	-0.06	0.15
			132	0.99	0.01	-72.63	-110.19	-0.16	0.15
612	Copertura	119, 120	0	0.87	0.00	72.13	-109.13	0.12	0.27
			66	0.87	0.00	0.10	-109.13	-0.06	0.27
			132	0.87	0.00	-71.92	-109.13	-0.23	0.27
613	Copertura	121, 122	0	9.67	-0.05	69.13	-103.24	-0.92	-1.20
			66	9.67	-0.05	0.98	-103.24	-0.13	-1.20
			132	9.67	-0.05	-67.16	-103.24	0.67	-1.20
614	Copertura	124, 125	0	137.47	-1.03	-1.44	1.48	3.16	-1.27
			99	137.47	-1.03	0.03	1.48	4.42	-1.27
			198	137.47	-1.03	1.50	1.48	5.68	-1.27
615	Copertura	125, 127	0	1894.14	-0.32	82.83	-0.60	-0.85	0.59
			775	1894.14	-0.32	78.16	-0.60	-5.40	0.59
			1550	1894.14	-0.32	73.48	-0.60	-9.95	0.59
616	Copertura	126, 127	0	123.47	0.37	-2.24	2.05	-4.17	-1.82
			99	123.47	0.37	-0.20	2.05	-2.36	-1.82
			198	123.47	0.37	1.84	2.05	-0.55	-1.82
617	Copertura	128, 129	0	24.75	-1.02	0.65	-0.27	2.75	-1.71
			99	24.75	-1.02	0.38	-0.27	4.44	-1.71
			198	24.75	-1.02	0.11	-0.27	6.14	-1.71
618	Copertura	129, 130	0	-4.94	-0.18	28.72	-0.46	4.78	0.71
			775	-4.94	-0.18	25.15	-0.46	-0.69	0.71
			1550	-4.94	-0.18	21.58	-0.46	-6.16	0.71

619	Copertura	131, 130	0	15.26	0.52	0.19	0.03	-0.29	1.56
			99	15.26	0.52	0.22	0.03	-1.84	1.56
			198	15.26	0.52	0.25	0.03	-3.39	1.56
620	Copertura	132, 135	0	1.46	-1.01	0.28	-0.28	3.22	-1.49
			99	1.46	-1.01	0.00	-0.28	4.70	-1.49
			198	1.46	-1.01	-0.28	-0.28	6.18	-1.49
621	Copertura	133, 134	0	-5.37	0.53	-0.08	-0.12	-0.42	1.50
			99	-5.37	0.53	-0.20	-0.12	-1.91	1.50
			198	-5.37	0.53	-0.32	-0.12	-3.39	1.50
622	Copertura	135, 134	0	-79.57	-0.18	2.66	-0.42	6.47	0.76
			775	-79.57	-0.18	-0.63	-0.42	0.57	0.76
			1550	-79.57	-0.18	-3.92	-0.42	-5.34	0.76
623	Copertura	137, 136	0	-3.78	-1.01	-0.05	0.16	3.41	-1.38
			99	-3.78	-1.01	0.11	0.16	4.79	-1.38
			198	-3.78	-1.01	0.27	0.16	6.16	-1.38
624	Copertura	136, 138	0	-0.33	-0.18	-0.52	-0.48	6.38	0.77
			775	-0.33	-0.18	-4.22	-0.48	0.39	0.77
			1550	-0.33	-0.18	-7.93	-0.48	-5.61	0.77
625	Copertura	139, 138	0	-13.56	0.54	-0.50	0.46	-0.86	1.30
			99	-13.56	0.54	-0.05	0.46	-2.15	1.30
			198	-13.56	0.54	0.40	0.46	-3.44	1.30
626	Copertura	140, 141	0	4.71	-1.02	0.20	-0.14	3.40	-1.40
			99	4.71	-1.02	0.06	-0.14	4.79	-1.40
			198	4.71	-1.02	-0.08	-0.14	6.17	-1.40
627	Copertura	141, 142	0	10.02	-0.18	2.83	-0.39	6.27	0.76
			775	10.02	-0.18	-0.20	-0.39	0.35	0.76
			1550	10.02	-0.18	-3.23	-0.39	-5.58	0.76
628	Copertura	143, 142	0	-0.86	0.54	-0.10	-0.03	-0.90	1.27
			99	-0.86	0.54	-0.13	-0.03	-2.16	1.27
			198	-0.86	0.54	-0.17	-0.03	-3.42	1.27
629	Copertura	144, 145	0	-0.87	-1.02	0.10	0.11	3.41	-1.38
			99	-0.87	-1.02	0.20	0.11	4.78	-1.38
			198	-0.87	-1.02	0.31	0.11	6.15	-1.38
630	Copertura	145, 146	0	-18.75	-0.17	3.13	-0.51	5.98	0.75
			775	-18.75	-0.17	-0.82	-0.51	0.20	0.75
			1550	-18.75	-0.17	-4.76	-0.51	-5.58	0.75
631	Copertura	147, 146	0	-10.45	0.54	-0.34	0.36	-0.80	1.36
			99	-10.45	0.54	0.01	0.36	-2.15	1.36
			198	-10.45	0.54	0.37	0.36	-3.50	1.36
632	Copertura	148, 149	0	-12.70	-1.02	-0.81	0.48	3.41	-1.36
			99	-12.70	-1.02	-0.34	0.48	4.76	-1.36
			198	-12.70	-1.02	0.14	0.48	6.11	-1.36
633	Copertura	149, 150	0	14.38	-0.17	1.18	0.12	5.79	0.73
			775	14.38	-0.17	2.12	0.12	0.13	0.73
			1550	14.38	-0.17	3.06	0.12	-5.53	0.73
634	Copertura	151, 150	0	17.52	0.54	0.51	-0.44	-0.82	1.34
			99	17.52	0.54	0.07	-0.44	-2.15	1.34
			198	17.52	0.54	-0.36	-0.44	-3.47	1.34
635	Copertura	152, 153	0	-24.63	-1.02	-1.31	0.92	3.40	-1.40
			99	-24.63	-1.02	-0.40	0.92	4.78	-1.40
			198	-24.63	-1.02	0.52	0.92	6.17	-1.40
636	Copertura	153, 154	0	0.14	-0.17	-0.72	0.19	5.97	0.73
			775	0.14	-0.17	0.78	0.19	0.27	0.73
			1551	0.14	-0.17	2.28	0.19	-5.42	0.73
637	Copertura	155, 154	0	13.58	0.54	0.43	-0.15	-0.84	1.33
			99	13.58	0.54	0.28	-0.15	-2.16	1.33
			198	13.58	0.54	0.13	-0.15	-3.48	1.33
638	Copertura	156, 157	0	-29.78	-1.02	-1.54	1.10	3.39	-1.39
			99	-29.78	-1.02	-0.44	1.10	4.77	-1.39
			198	-29.78	-1.02	0.65	1.10	6.15	-1.39
639	Copertura	157, 158	0	-2.05	-0.17	-2.47	0.48	6.06	0.74
			775	-2.05	-0.17	1.27	0.48	0.30	0.74
			1551	-2.05	-0.17	5.02	0.48	-5.45	0.74
640	Copertura	159, 158	0	24.98	0.54	0.82	-0.66	-0.84	1.32
			99	24.98	0.54	0.17	-0.66	-2.15	1.32
			198	24.98	0.54	-0.48	-0.66	-3.46	1.32
641	Copertura	160, 161	0	-32.97	-1.02	-1.72	1.22	3.39	-1.39
			99	-32.97	-1.02	-0.51	1.22	4.77	-1.39
			198	-32.97	-1.02	0.70	1.22	6.15	-1.39
642	Copertura	161, 162	0	0.45	-0.17	-3.17	0.44	6.15	0.76
			776	0.45	-0.17	0.24	0.44	0.29	0.76
			1551	0.45	-0.17	3.65	0.44	-5.57	0.76

643	Copertura	163, 162	0	18.27	0.54	0.63	-0.29	-0.90	1.24
			99	18.27	0.54	0.34	-0.29	-2.14	1.24
			198	18.27	0.54	0.05	-0.29	-3.37	1.24
644	Copertura	164, 165	0	-37.58	-1.02	-1.96	1.36	3.39	-1.38
			99	-37.58	-1.02	-0.60	1.36	4.77	-1.38
			198	-37.58	-1.02	0.75	1.36	6.14	-1.38
645	Copertura	165, 166	0	1.16	-0.16	-5.11	0.82	6.25	0.77
			776	1.16	-0.16	1.24	0.82	0.29	0.77
			1551	1.16	-0.16	7.59	0.82	-5.66	0.77
646	Copertura	167, 166	0	32.33	0.55	1.06	-0.81	-0.82	1.40
			99	32.33	0.55	0.26	-0.81	-2.20	1.40
			198	32.33	0.55	-0.54	-0.81	-3.59	1.40
647	Copertura	168, 169	0	-41.03	-1.02	-2.14	1.47	3.39	-1.38
			99	-41.03	-1.02	-0.68	1.47	4.77	-1.38
			198	-41.03	-1.02	0.78	1.47	6.14	-1.38
648	Copertura	169, 170	0	-2.36	-0.17	-5.95	0.79	6.27	0.77
			776	-2.36	-0.17	0.15	0.79	0.28	0.77
			1552	-2.36	-0.17	6.26	0.79	-5.72	0.77
649	Copertura	171, 170	0	25.06	0.54	0.87	-0.45	-0.85	1.30
			99	25.06	0.54	0.43	-0.45	-2.14	1.30
			198	25.06	0.54	-0.02	-0.45	-3.43	1.30
650	Copertura	172, 173	0	-46.99	-1.02	-2.36	1.63	3.39	-1.39
			99	-46.99	-1.02	-0.74	1.63	4.76	-1.39
			198	-46.99	-1.02	0.87	1.63	6.14	-1.39
651	Copertura	173, 175	0	-16.78	-0.17	-8.51	1.23	6.12	0.75
			776	-16.78	-0.17	1.07	1.23	0.29	0.75
			1552	-16.78	-0.17	10.65	1.23	-5.54	0.75
652	Copertura	174, 175	0	39.17	0.54	1.39	-1.06	-0.84	1.32
			99	39.17	0.54	0.34	-1.06	-2.15	1.32
			198	39.17	0.54	-0.72	-1.06	-3.45	1.32
653	Copertura	176, 177	0	-55.52	-1.02	-3.04	2.19	3.30	-1.43
			99	-55.52	-1.02	-0.86	2.19	4.71	-1.43
			198	-55.52	-1.02	1.32	2.19	6.13	-1.43
654	Copertura	177, 178	0	84.96	-0.18	-12.37	1.55	6.09	0.69
			776	84.96	-0.18	-0.34	1.55	0.76	0.69
			1552	84.96	-0.18	11.69	1.55	-4.56	0.69
655	Copertura	179, 178	0	38.99	0.53	1.09	-0.63	-1.02	1.21
			99	38.99	0.53	0.47	-0.63	-2.22	1.21
			198	38.99	0.53	-0.15	-0.63	-3.42	1.21
656	Copertura	180, 181	0	6.51	-1.01	0.56	-0.36	3.28	-1.46
			99	6.51	-1.01	0.20	-0.36	4.72	-1.46
			198	6.51	-1.01	-0.16	-0.36	6.17	-1.46
657	Copertura	181, 182	0	-82.67	-0.18	6.11	-0.89	6.19	0.70
			775	-82.67	-0.18	-0.80	-0.89	0.77	0.70
			1550	-82.67	-0.18	-7.72	-0.89	-4.64	0.70
658	Copertura	183, 182	0	-12.81	0.52	-0.25	0.16	-0.99	1.23
			99	-12.81	0.52	-0.08	0.16	-2.21	1.23
			198	-12.81	0.52	0.08	0.16	-3.43	1.23
659	Copertura	184, 185	0	9.80	-1.01	0.34	-0.34	3.37	-1.43
			99	9.80	-1.01	0.00	-0.34	4.78	-1.43
			198	9.80	-1.01	-0.34	-0.34	6.20	-1.43
660	Copertura	185, 186	0	14.36	-0.18	4.78	-0.59	6.60	0.81
			775	14.36	-0.18	0.18	-0.59	0.34	0.81
			1550	14.36	-0.18	-4.41	-0.59	-5.92	0.81
661	Copertura	187, 186	0	-4.34	0.53	-0.26	0.13	-0.83	1.28
			99	-4.34	0.53	-0.13	0.13	-2.10	1.28
			198	-4.34	0.53	0.00	0.13	-3.36	1.28
662	Copertura	188, 189	0	1.26	-1.01	0.07	0.00	3.39	-1.42
			99	1.26	-1.01	0.07	0.00	4.80	-1.42
			198	1.26	-1.01	0.07	0.00	6.21	-1.42
663	Copertura	189, 190	0	1.74	-0.18	2.05	-0.24	6.96	0.86
			775	1.74	-0.18	0.19	-0.24	0.32	0.86
			1550	1.74	-0.18	-1.66	-0.24	-6.33	0.86
664	Copertura	191, 190	0	-2.31	0.53	-0.13	0.08	-0.85	1.25
			99	-2.31	0.53	-0.05	0.08	-2.09	1.25
			198	-2.31	0.53	0.03	0.08	-3.33	1.25
665	Copertura	192, 193	0	7.03	-1.01	0.23	-0.26	3.39	-1.42
			99	7.03	-1.01	-0.03	-0.26	4.80	-1.42
			198	7.03	-1.01	-0.29	-0.26	6.21	-1.42
666	Copertura	193, 195	0	0.09	-0.19	3.28	-0.08	7.08	0.87
			775	0.09	-0.19	2.67	-0.08	0.36	0.87
			1550	0.09	-0.19	2.06	-0.08	-6.36	0.87

667	Copertura	194, 195	0	4.23	0.53	0.12	-0.14	-0.84	1.24
			99	4.23	0.53	-0.03	-0.14	-2.07	1.24
			198	4.23	0.53	-0.17	-0.14	-3.31	1.24
668	Copertura	196, 197	0	-0.85	-1.00	-0.13	0.17	3.28	-1.47
			99	-0.85	-1.00	0.04	0.17	4.74	-1.47
			198	-0.85	-1.00	0.20	0.17	6.20	-1.47
669	Copertura	197, 199	0	38.38	-0.19	-0.75	0.21	6.97	0.84
			775	38.38	-0.19	0.87	0.21	0.45	0.84
			1550	38.38	-0.19	2.50	0.21	-6.06	0.84
670	Copertura	198, 199	0	7.31	0.53	0.19	-0.18	-0.69	1.35
			99	7.31	0.53	0.00	-0.18	-2.03	1.35
			198	7.31	0.53	-0.18	-0.18	-3.36	1.35
671	Copertura	200, 201	0	-11.14	-1.01	-0.26	0.06	3.01	-1.58
			99	-11.14	-1.01	-0.20	0.06	4.58	-1.58
			198	-11.14	-1.01	-0.14	0.06	6.15	-1.58
672	Copertura	201, 202	0	1.80	-0.19	-14.51	0.06	5.84	0.78
			775	1.80	-0.19	-14.04	0.06	-0.18	0.78
			1550	1.80	-0.19	-13.57	0.06	-6.20	0.78
673	Copertura	203, 202	0	-14.86	0.53	-0.30	0.27	-0.14	1.58
			99	-14.86	0.53	-0.04	0.27	-1.71	1.58
			198	-14.86	0.53	0.23	0.27	-3.28	1.58
674	Copertura	204, 205	0	-78.71	-1.02	0.33	-0.38	3.18	-1.36
			99	-78.71	-1.02	-0.05	-0.38	4.53	-1.36
			198	-78.71	-1.02	-0.42	-0.38	5.88	-1.36
675	Copertura	205, 206	0	-914.61	-0.20	-48.65	0.80	2.62	0.66
			775	-914.61	-0.20	-42.44	0.80	-2.46	0.66
			1550	-914.61	-0.20	-36.23	0.80	-7.54	0.66
676	Copertura	207, 206	0	-61.65	0.49	0.95	-0.83	-0.90	1.03
			99	-61.65	0.49	0.12	-0.83	-1.92	1.03
			198	-61.65	0.49	-0.70	-0.83	-2.95	1.03
677	Copertura	79	0	-158.78	-8.28	-45.06	27.69	16.06	6.65
			125	-158.78	-8.28	20.21	76.74	7.75	6.65
			250	-158.78	-8.28	146.78	125.78	-0.57	6.65
678	Copertura	124	0	321.32	0.64	-44.04	48.10	-33.22	-48.93
			155	321.32	0.64	30.53	48.10	42.63	-48.93
			310	321.32	0.64	105.09	48.10	118.48	-48.93
679	Copertura	80	0	279.35	-0.01	16.18	40.57	-67.90	41.21
			45	279.35	-0.01	34.44	40.57	-86.45	41.21
			90	279.35	-0.01	52.70	40.57	-104.99	41.21
680	Copertura	128	0	1.31	-0.14	-44.70	48.20	-8.50	-13.48
			155	1.31	-0.14	30.01	48.20	12.40	-13.48
			310	1.31	-0.14	104.72	48.20	33.30	-13.48
681	Copertura	82	0	6.03	-0.82	-6.88	90.88	-24.73	8.17
			43	6.03	-0.82	31.88	90.88	-28.22	8.17
			85	6.03	-0.82	70.65	90.88	-31.70	8.17
682	Copertura	132	0	79.68	0.38	-45.39	48.95	-1.28	1.10
			155	79.68	0.38	30.47	48.95	-2.99	1.10
			310	79.68	0.38	106.34	48.95	-4.70	1.10
683	Copertura	83	0	98.79	0.30	7.97	53.95	1.23	-2.83
			43	98.79	0.30	30.98	53.95	2.44	-2.83
			85	98.79	0.30	54.00	53.95	3.64	-2.83
684	Copertura	137	0	-118.55	0.61	-45.76	49.27	-0.83	1.26
			155	-118.55	0.61	30.61	49.27	-2.79	1.26
			310	-118.55	0.61	106.97	49.27	-4.75	1.26
685	Copertura	84	0	-100.50	-0.11	4.00	63.96	2.01	-3.07
			43	-100.50	-0.11	31.28	63.96	3.32	-3.07
			85	-100.50	-0.11	58.57	63.96	4.63	-3.07
686	Copertura	140	0	14.51	0.59	-45.90	49.39	-2.97	-0.73
			155	14.51	0.59	30.66	49.39	-1.84	-0.73
			310	14.51	0.59	107.21	49.39	-0.72	-0.73
687	Copertura	85	0	45.03	-0.05	7.00	56.31	-0.16	-0.83
			43	45.03	-0.05	31.02	56.31	0.19	-0.83
			85	45.03	-0.05	55.04	56.31	0.54	-0.83
688	Copertura	144	0	-144.53	0.60	-45.92	49.39	-2.25	-1.09
			155	-144.53	0.60	30.63	49.39	-0.56	-1.09
			310	-144.53	0.60	107.19	49.39	1.13	-1.09
689	Copertura	86	0	-98.93	0.04	5.01	61.74	-0.67	-1.42
			43	-98.93	0.04	31.35	61.74	-0.06	-1.42
			85	-98.93	0.04	57.69	61.74	0.55	-1.42
690	Copertura	87	0	61.34	0.00	6.55	57.82	0.54	0.89
			43	61.34	0.00	31.21	57.82	0.16	0.89
			85	61.34	0.00	55.87	57.82	-0.22	0.89

691	Copertura	148	0	100.77	0.62	-45.96	49.14	-0.24	-0.84
			155	100.77	0.62	30.20	49.14	1.06	-0.84
			310	100.77	0.62	106.37	49.14	2.36	-0.84
692	Copertura	88	0	-81.34	-0.01	5.49	60.60	1.24	0.28
			43	-81.34	-0.01	31.34	60.60	1.12	0.28
			85	-81.34	-0.01	57.19	60.60	1.00	0.28
693	Copertura	152	0	11.31	0.57	-46.23	49.78	1.71	-0.45
			155	11.31	0.57	30.93	49.78	2.41	-0.45
			310	11.31	0.57	108.10	49.78	3.12	-0.45
694	Copertura	89	0	69.44	0.00	5.31	61.09	2.12	1.10
			43	69.44	0.00	31.37	61.09	1.65	1.10
			85	69.44	0.00	57.43	61.09	1.18	1.10
695	Copertura	156	0	-17.40	0.56	-46.26	49.58	3.08	0.02
			155	-17.40	0.56	30.59	49.58	3.05	0.02
			310	-17.40	0.56	107.44	49.58	3.01	0.02
696	Copertura	90	0	-76.75	0.00	6.20	59.81	2.22	0.50
			43	-76.75	0.00	31.71	59.81	2.00	0.50
			85	-76.75	0.00	57.23	59.81	1.79	0.50
697	Copertura	160	0	-7.09	0.56	-46.31	49.59	3.70	0.20
			155	-7.09	0.56	30.56	49.59	3.40	0.20
			310	-7.09	0.56	107.42	49.59	3.09	0.20
698	Copertura	91	0	69.66	-0.01	4.81	59.91	3.03	1.74
			43	69.66	-0.01	30.36	59.91	2.29	1.74
			85	69.66	-0.01	55.92	59.91	1.54	1.74
699	Copertura	164	0	6.30	0.56	-46.37	49.61	5.25	0.72
			155	6.30	0.56	30.53	49.61	4.13	0.72
			310	6.30	0.56	107.42	49.61	3.01	0.72
700	Copertura	92	0	-73.30	-0.01	7.29	55.33	3.34	1.06
			43	-73.30	-0.01	30.89	55.33	2.89	1.06
			85	-73.30	-0.01	54.49	55.33	2.44	1.06
701	Copertura	168	0	18.74	0.56	-46.43	49.63	6.06	0.89
			155	18.74	0.56	30.51	49.63	4.67	0.89
			310	18.74	0.56	107.44	49.63	3.28	0.89
702	Copertura	93	0	103.69	0.06	6.17	56.42	3.89	2.60
			43	103.69	0.06	30.24	56.42	2.78	2.60
			85	103.69	0.06	54.31	56.42	1.67	2.60
703	Copertura	172	0	3.63	0.56	-46.52	49.81	7.94	1.62
			155	3.63	0.56	30.69	49.81	5.42	1.62
			310	3.63	0.56	107.90	49.81	2.91	1.62
704	Copertura	94	0	-6.39	-0.01	6.48	61.82	2.22	2.98
			43	-6.39	-0.01	32.85	61.82	0.95	2.98
			85	-6.39	-0.01	59.22	61.82	-0.32	2.98
705	Copertura	176	0	-80.73	0.45	-46.55	49.68	11.06	3.80
			155	-80.73	0.45	30.45	49.68	5.17	3.80
			310	-80.73	0.45	107.46	49.68	-0.71	3.80
706	Copertura	180	0	-8.78	0.44	-45.70	48.98	-5.07	-2.69
			155	-8.78	0.44	30.21	48.98	-0.90	-2.69
			310	-8.78	0.44	106.13	48.98	3.27	-2.69
707	Copertura	95	0	-82.37	-0.03	6.17	58.26	0.74	-2.47
			43	-82.37	-0.03	31.02	58.26	1.80	-2.47
			85	-82.37	-0.03	55.87	58.26	2.85	-2.47
708	Copertura	184	0	119.77	0.53	-45.82	49.37	-4.16	-1.19
			155	119.77	0.53	30.70	49.37	-2.32	-1.19
			310	119.77	0.53	107.22	49.37	-0.48	-1.19
709	Copertura	96	0	64.01	0.03	6.95	57.85	-0.46	-1.51
			43	64.01	0.03	31.63	57.85	0.19	-1.51
			85	64.01	0.03	56.30	57.85	0.83	-1.51
710	Copertura	188	0	-33.89	0.55	-45.83	49.28	-1.46	-0.47
			155	-33.89	0.55	30.56	49.28	-0.72	-0.47
			310	-33.89	0.55	106.94	49.28	0.01	-0.47
711	Copertura	97	0	-35.47	-0.05	5.66	61.09	-1.24	-0.23
			43	-35.47	-0.05	31.71	61.09	-1.14	-0.23
			85	-35.47	-0.05	57.77	61.09	-1.04	-0.23
712	Copertura	192	0	106.75	0.56	-45.75	49.23	-2.08	-1.49
			155	106.75	0.56	30.56	49.23	0.22	-1.49
			310	106.75	0.56	106.86	49.23	2.53	-1.49
713	Copertura	106	0	103.00	-0.08	7.43	53.97	-1.68	1.06
			43	103.00	-0.08	30.45	53.97	-2.13	1.06
			85	103.00	-0.08	53.47	53.97	-2.59	1.06
714	Copertura	196	0	-68.69	0.44	-45.47	48.99	0.18	-0.78
			155	-68.69	0.44	30.47	48.99	1.40	-0.78
			310	-68.69	0.44	106.41	48.99	2.62	-0.78

715	Copertura	107	0	30.23	-0.30	4.50	64.08	-0.72	1.58
			43	30.23	-0.30	31.83	64.08	-1.39	1.58
			85	30.23	-0.30	59.16	64.08	-2.07	1.58
716	Copertura	200	0	27.64	0.15	-44.95	48.42	3.71	6.88
			155	27.64	0.15	30.10	48.42	-6.95	6.88
			310	27.64	0.15	105.15	48.42	-17.61	6.88
717	Copertura	108	0	-104.13	0.51	8.50	53.53	12.33	-6.09
			43	-104.13	0.51	31.33	53.53	14.93	-6.09
			85	-104.13	0.51	54.17	53.53	17.53	-6.09
718	Copertura	204	0	-273.69	0.52	-44.43	48.54	19.85	27.80
			155	-273.69	0.52	30.81	48.54	-23.23	27.80
			310	-273.69	0.52	106.04	48.54	-66.32	27.80
719	Copertura	109	0	-239.68	2.21	-2.22	86.66	39.76	-16.40
			43	-239.68	2.21	34.74	86.66	46.76	-16.40
			85	-239.68	2.21	71.71	86.66	53.75	-16.40
720	Copertura	110	0	94.88	-10.40	49.75	46.24	-9.32	-2.78
			43	94.88	-10.40	71.26	54.61	-8.13	-2.78
			85	94.88	-10.40	96.34	62.98	-6.95	-2.78
721	Copertura	14	0	-231.53	17.82	-106.13	50.62	5.95	-5.36
			95	-231.53	17.82	-55.25	59.45	11.04	-5.36
			190	-231.53	17.82	12.41	85.94	16.13	-5.36
722	Copertura	15	0	232.40	-1.07	-102.07	46.84	38.04	55.92
			65	232.40	-1.07	-71.63	46.84	1.69	55.92
			130	232.40	-1.07	-41.18	46.84	-34.66	55.92
723	Copertura	16	0	188.64	-1.58	-44.12	25.11	-34.65	-45.09
			65	188.64	-1.58	-27.80	25.11	-5.34	-45.09
			130	188.64	-1.58	-11.48	25.11	23.97	-45.09
724	Copertura	17	0	-15.11	-1.55	-102.57	46.49	-1.30	5.04
			65	-15.11	-1.55	-72.35	46.49	-4.57	5.04
			130	-15.11	-1.55	-42.13	46.49	-7.85	5.04
725	Copertura	18	0	-25.39	0.31	-72.26	55.46	2.43	0.57
			65	-25.39	0.31	-36.21	55.46	2.06	0.57
			130	-25.39	0.31	-0.17	55.46	1.69	0.57
726	Copertura	19	0	78.51	-1.39	-104.21	47.46	1.62	2.02
			65	78.51	-1.39	-73.37	47.46	0.31	2.02
			130	78.51	-1.39	-42.52	47.46	-1.00	2.02
727	Copertura	20	0	130.98	0.38	-71.00	52.35	-2.52	1.38
			65	130.98	0.38	-36.97	52.35	-3.42	1.38
			130	130.98	0.38	-2.94	52.35	-4.32	1.38
728	Copertura	21	0	-115.95	-1.31	-105.01	47.89	-2.81	-1.49
			65	-115.95	-1.31	-73.89	47.89	-1.84	-1.49
			130	-115.95	-1.31	-42.76	47.89	-0.88	-1.49
729	Copertura	22	0	-124.70	0.09	-75.84	57.68	3.71	6.76
			65	-124.70	0.09	-38.35	57.68	-0.68	6.76
			130	-124.70	0.09	-0.86	57.68	-5.07	6.76
730	Copertura	23	0	11.32	-1.32	-105.30	47.99	0.79	2.74
			65	11.32	-1.32	-74.10	47.99	-0.99	2.74
			130	11.32	-1.32	-42.90	47.99	-2.77	2.74
731	Copertura	24	0	78.71	0.10	-75.30	56.64	-2.25	-0.31
			65	78.71	0.10	-38.48	56.64	-2.05	-0.31
			130	78.71	0.10	-1.66	56.64	-1.85	-0.31
732	Copertura	25	0	-143.88	-1.31	-105.33	48.01	-4.33	-1.68
			65	-143.88	-1.31	-74.12	48.01	-3.24	-1.68
			130	-143.88	-1.31	-42.92	48.01	-2.15	-1.68
733	Copertura	26	0	-125.77	0.14	-76.41	57.90	4.28	6.16
			65	-125.77	0.14	-38.78	57.90	0.27	6.16
			130	-125.77	0.14	-1.14	57.90	-3.73	6.16
734	Copertura	27	0	83.32	0.15	-75.67	56.97	-13.42	-11.99
			65	83.32	0.15	-38.64	56.97	-5.63	-11.99
			130	83.32	0.15	-1.61	56.97	2.17	-11.99
735	Copertura	28	0	109.46	-1.30	-104.81	47.59	-14.11	-10.09
			65	109.46	-1.30	-73.88	47.59	-7.55	-10.09
			130	109.46	-1.30	-42.94	47.59	-0.99	-10.09
736	Copertura	29	0	-123.85	0.13	-75.87	57.29	-11.19	-9.72
			65	-123.85	0.13	-38.64	57.29	-4.88	-9.72
			130	-123.85	0.13	-1.40	57.29	1.44	-9.72
737	Copertura	30	0	28.14	-1.32	-105.45	47.88	-23.46	-18.41
			65	28.14	-1.32	-74.32	47.88	-11.49	-18.41
			130	28.14	-1.32	-43.20	47.88	0.48	-18.41
738	Copertura	31	0	85.47	0.13	-75.42	56.84	-18.75	-17.40
			65	85.47	0.13	-38.47	56.84	-7.44	-17.40
			130	85.47	0.13	-1.53	56.84	3.87	-17.40

739	Copertura	32	0	2.94	-1.33	-105.00	47.52	-26.58	-21.71
			65	2.94	-1.33	-74.11	47.52	-12.47	-21.71
			130	2.94	-1.33	-43.23	47.52	1.63	-21.71
740	Copertura	33	0	-122.00	0.16	-73.57	54.00	-14.21	-12.99
			65	-122.00	0.16	-38.47	54.00	-5.77	-12.99
			130	-122.00	0.16	-3.37	54.00	2.67	-12.99
741	Copertura	34	0	15.42	-1.33	-104.85	47.38	-28.94	-23.86
			65	15.42	-1.33	-74.05	47.38	-13.43	-23.86
			130	15.42	-1.33	-43.26	47.38	2.08	-23.86
742	Copertura	35	0	83.15	0.12	-78.30	59.82	-22.91	-22.19
			65	83.15	0.12	-39.41	59.82	-8.48	-22.19
			130	83.15	0.12	-0.53	59.82	5.94	-22.19
743	Copertura	36	0	31.94	-1.34	-104.67	47.20	-31.33	-26.72
			65	31.94	-1.34	-73.99	47.20	-13.96	-26.72
			130	31.94	-1.34	-43.31	47.20	3.40	-26.72
744	Copertura	37	0	-124.89	0.12	-75.26	56.60	-17.88	-17.47
			65	-124.89	0.12	-38.46	56.60	-6.53	-17.47
			130	-124.89	0.12	-1.67	56.60	4.83	-17.47
745	Copertura	38	0	46.73	-1.34	-104.50	47.03	-33.75	-29.07
			65	46.73	-1.34	-73.93	47.03	-14.85	-29.07
			130	46.73	-1.34	-43.35	47.03	4.04	-29.07
746	Copertura	39	0	111.18	0.13	-75.41	56.78	-26.08	-26.37
			65	111.18	0.13	-38.50	56.78	-8.93	-26.37
			130	111.18	0.13	-1.60	56.78	8.21	-26.37
747	Copertura	40	0	35.64	-1.34	-104.45	46.94	-36.84	-32.73
			65	35.64	-1.34	-73.94	46.94	-15.56	-32.73
			130	35.64	-1.34	-43.43	46.94	5.71	-32.73
748	Copertura	41	0	-66.98	0.07	-74.80	56.22	-24.09	-25.06
			65	-66.98	0.07	-38.26	56.22	-7.80	-25.06
			130	-66.98	0.07	-1.71	56.22	8.49	-25.06
749	Copertura	42	0	-42.71	-1.37	-103.77	46.37	-39.43	-36.61
			65	-42.71	-1.37	-73.63	46.37	-15.63	-36.61
			130	-42.71	-1.37	-43.49	46.37	8.17	-36.61
750	Copertura	43	0	-13.32	-1.37	-104.57	47.52	-1.91	2.00
			65	-13.32	-1.37	-73.68	47.52	-3.21	2.00
			130	-13.32	-1.37	-42.79	47.52	-4.51	2.00
751	Copertura	44	0	-36.53	0.06	-75.37	57.29	2.75	6.15
			65	-36.53	0.06	-38.13	57.29	-1.25	6.15
			130	-36.53	0.06	-0.89	57.29	-5.24	6.15
752	Copertura	45	0	113.09	-1.35	-105.18	47.94	3.97	5.99
			65	113.09	-1.35	-74.02	47.94	0.07	5.99
			130	113.09	-1.35	-42.85	47.94	-3.82	5.99
753	Copertura	46	0	30.60	0.10	-74.39	56.21	-0.83	1.91
			65	30.60	0.10	-37.86	56.21	-2.07	1.91
			130	30.60	0.10	-1.33	56.21	-3.31	1.91
754	Copertura	47	0	-34.71	-1.35	-105.06	47.86	-0.77	0.48
			65	-34.71	-1.35	-73.95	47.86	-1.08	0.48
			130	-34.71	-1.35	-42.85	47.86	-1.39	0.48
755	Copertura	48	0	3.10	0.06	-74.67	56.73	0.06	1.34
			65	3.10	0.06	-37.80	56.73	-0.80	1.34
			130	3.10	0.06	-0.92	56.73	-1.67	1.34
756	Copertura	49	0	101.95	-1.35	-104.92	47.81	2.89	3.65
			65	101.95	-1.35	-73.84	47.81	0.52	3.65
			130	101.95	-1.35	-42.76	47.81	-1.85	3.65
757	Copertura	50	0	64.19	0.08	-74.01	55.94	-1.64	-1.80
			65	64.19	0.08	-37.65	55.94	-0.47	-1.80
			130	64.19	0.08	-1.29	55.94	0.70	-1.80
758	Copertura	51	0	-68.01	-1.38	-104.35	47.53	-1.66	-1.32
			65	-68.01	-1.38	-73.46	47.53	-0.80	-1.32
			130	-68.01	-1.38	-42.56	47.53	0.06	-1.32
759	Copertura	52	0	59.25	0.15	-73.96	56.18	-2.36	-3.95
			65	59.25	0.15	-37.44	56.18	0.21	-3.95
			130	59.25	0.15	-0.93	56.18	2.78	-3.95
760	Copertura	53	0	34.98	-1.46	-103.10	46.83	1.49	-1.50
			65	34.98	-1.46	-72.66	46.83	2.47	-1.50
			130	34.98	-1.46	-42.21	46.83	3.44	-1.50
761	Copertura	54	0	-122.26	0.49	-68.03	49.70	2.61	3.63
			65	-122.26	0.49	-35.72	49.70	0.25	3.63
			130	-122.26	0.49	-3.41	49.70	-2.11	3.63
762	Copertura	55	0	-222.43	-1.22	-102.91	47.18	-21.34	-31.94
			65	-222.43	-1.22	-72.24	47.18	-0.58	-31.94
			130	-222.43	-1.22	-41.57	47.18	20.17	-31.94

763	Copertura	56	0	-151.00	-0.10	-69.94	54.24	19.20	24.88
			65	-151.00	-0.10	-34.69	54.24	3.03	24.88
			130	-151.00	-0.10	0.56	54.24	-13.14	24.88
764	Copertura	70	0	149.19	4.14	-106.13	37.35	5.89	4.28
			95	149.19	4.14	-69.25	41.76	1.82	4.28
			190	149.19	4.14	-23.99	55.00	-2.24	4.28
765	Copertura	81	0	195.21	2.52	-58.72	81.53	-7.94	37.55
			80	195.21	2.52	6.50	81.53	-37.98	37.55
			160	195.21	2.52	71.72	81.53	-68.02	37.55
766	Copertura	126	0	267.96	-4.49	-14.49	23.28	21.73	49.56
			30	267.96	-4.49	-7.50	23.28	6.87	49.56
			60	267.96	-4.49	-0.52	23.28	-8.00	49.56
767	Copertura	98	0	90.18	1.47	-35.51	49.93	-5.32	11.82
			82	90.18	1.47	5.61	49.93	-15.06	11.82
			165	90.18	1.47	46.73	49.93	-24.79	11.82
768	Copertura	99	0	21.96	-0.23	-41.73	60.94	-2.82	-2.46
			82	21.96	-0.23	8.45	60.94	-0.80	-2.46
			165	21.96	-0.23	58.62	60.94	1.23	-2.46
769	Copertura	100	0	-23.66	-0.07	-39.05	56.97	-3.66	-3.45
			82	-23.66	-0.07	7.86	56.97	-0.83	-3.45
			165	-23.66	-0.07	54.77	56.97	2.01	-3.45
770	Copertura	101	0	-32.09	-0.04	-40.86	59.91	-1.36	-0.72
			82	-32.09	-0.04	8.47	59.91	-0.76	-0.72
			165	-32.09	-0.04	57.81	59.91	-0.16	-0.72
771	Copertura	102	0	-21.81	-0.11	-39.76	58.14	-3.17	-1.52
			82	-21.81	-0.11	8.12	58.14	-1.92	-1.52
			165	-21.81	-0.11	55.99	58.14	-0.67	-1.52
772	Copertura	103	0	-15.95	-0.08	-40.79	59.69	2.10	0.95
			82	-15.95	-0.08	8.36	59.69	1.32	0.95
			165	-15.95	-0.08	57.51	59.69	0.54	0.95
773	Copertura	104	0	-4.06	-0.01	-40.16	58.72	1.60	0.22
			82	-4.06	-0.01	8.19	58.72	1.42	0.22
			165	-4.06	-0.01	56.54	58.72	1.24	0.22
774	Copertura	105	0	-8.46	-0.03	-40.38	58.90	4.06	1.18
			82	-8.46	-0.03	8.12	58.90	3.09	1.18
			165	-8.46	-0.03	56.63	58.90	2.12	1.18
775	Copertura	111	0	1.15	-0.06	-41.18	61.99	2.90	0.43
			80	1.15	-0.06	8.27	61.99	2.56	0.43
			160	1.15	-0.06	57.71	61.99	2.22	0.43
776	Copertura	112	0	-6.03	-0.04	-37.30	55.83	5.98	1.79
			82	-6.03	-0.04	8.67	55.83	4.51	1.79
			165	-6.03	-0.04	54.63	55.83	3.03	1.79
777	Copertura	113	0	2.39	-0.05	-40.48	59.41	4.99	1.00
			82	2.39	-0.05	8.45	59.41	4.17	1.00
			165	2.39	-0.05	57.37	59.41	3.34	1.00
778	Copertura	114	0	27.11	-0.12	-39.90	58.59	8.10	2.55
			82	27.11	-0.12	8.35	58.59	5.99	2.55
			165	27.11	-0.12	56.60	58.59	3.89	2.55
779	Copertura	115	0	70.19	0.22	-41.11	59.65	7.20	3.02
			82	70.19	0.22	8.01	59.65	4.71	3.02
			165	70.19	0.22	57.13	59.65	2.22	3.02
780	Copertura	116	0	-156.21	0.23	-40.01	57.64	-3.44	-2.54
			82	-156.21	0.23	7.45	57.64	-1.35	-2.54
			165	-156.21	0.23	54.91	57.64	0.75	-2.54
781	Copertura	117	0	137.85	-0.13	-40.61	58.47	-2.82	-1.43
			82	137.85	-0.13	7.54	58.47	-1.64	-1.43
			165	137.85	-0.13	55.68	58.47	-0.46	-1.43
782	Copertura	118	0	-108.67	-0.07	-39.72	57.00	-1.58	-0.21
			82	-108.67	-0.07	7.22	57.00	-1.40	-0.21
			165	-108.67	-0.07	54.15	57.00	-1.23	-0.21
783	Copertura	131	0	-15.42	0.44	-0.75	57.02	1.87	12.12
			30	-15.42	0.44	16.36	57.02	-1.76	12.12
			60	-15.42	0.44	33.46	57.02	-5.40	12.12
784	Copertura	133	0	127.56	0.41	-3.62	53.85	-4.40	-2.75
			30	127.56	0.41	12.53	53.85	-3.57	-2.75
			60	127.56	0.41	28.69	53.85	-2.74	-2.75
785	Copertura	139	0	-133.92	-0.21	-1.83	58.97	-5.57	-3.19
			30	-133.92	-0.21	15.86	58.97	-4.61	-3.19
			60	-133.92	-0.21	33.55	58.97	-3.66	-3.19
786	Copertura	143	0	78.17	-0.23	-2.66	57.91	-1.95	-0.98
			30	78.17	-0.23	14.71	57.91	-1.66	-0.98
			60	78.17	-0.23	32.08	57.91	-1.36	-0.98

787	Copertura	147	0	-132.88	-0.11	-2.08	59.26	-4.07	-1.50
			30	-132.88	-0.11	15.70	59.26	-3.62	-1.50
			60	-132.88	-0.11	33.48	59.26	-3.17	-1.50
788	Copertura	151	0	95.12	-0.11	-2.56	58.57	2.66	0.93
			30	95.12	-0.11	15.01	58.57	2.38	0.93
			60	95.12	-0.11	32.58	58.57	2.10	0.93
789	Copertura	155	0	-114.85	-0.14	-2.37	58.90	1.84	0.40
			30	-114.85	-0.14	15.30	58.90	1.72	0.40
			60	-114.85	-0.14	32.97	58.90	1.60	0.40
790	Copertura	159	0	102.33	-0.15	-2.51	58.73	4.66	1.00
			30	102.33	-0.15	15.11	58.73	4.36	1.00
			60	102.33	-0.15	32.72	58.73	4.06	1.00
791	Copertura	119	0	176.20	-0.09	-40.06	58.06	0.03	1.04
			82	176.20	-0.09	7.75	58.06	-0.83	1.04
			165	176.20	-0.09	55.56	58.06	-1.69	1.04
792	Copertura	120	0	-44.95	0.21	-39.19	56.65	2.09	1.72
			82	-44.95	0.21	7.46	56.65	0.68	1.72
			165	-44.95	0.21	54.11	56.65	-0.73	1.72
793	Copertura	121	0	-28.95	-0.18	-42.26	60.95	2.10	-6.22
			82	-28.95	-0.18	7.93	60.95	7.22	-6.22
			165	-28.95	-0.18	58.12	60.95	12.35	-6.22
794	Copertura	122	0	-294.00	-1.12	-34.39	45.60	1.10	-23.45
			82	-294.00	-1.12	3.16	45.60	20.42	-23.45
			165	-294.00	-1.12	40.70	45.60	39.73	-23.45
795	Copertura	123	0	149.19	4.14	-23.99	55.00	-2.24	4.28
			82	149.19	4.14	27.95	71.15	-5.76	4.28
			165	149.19	4.14	93.19	87.31	-9.29	4.28
796	Copertura	163	0	-109.81	-0.16	-4.39	55.71	3.27	0.58
			33	-109.81	-0.16	13.76	55.71	3.08	0.58
			65	-109.81	-0.16	31.91	55.71	2.89	0.58
797	Copertura	167	0	104.93	-0.14	-1.52	62.11	6.97	1.64
			30	104.93	-0.14	17.12	62.11	6.47	1.64
			60	104.93	-0.14	35.75	62.11	5.98	1.64
798	Copertura	171	0	-108.14	-0.16	-2.67	58.66	5.66	1.11
			30	-108.14	-0.16	14.93	58.66	5.33	1.11
			60	-108.14	-0.16	32.53	58.66	4.99	1.11
799	Copertura	174	0	137.64	-0.15	-2.61	59.35	9.56	2.45
			30	137.64	-0.15	15.19	59.35	8.83	2.45
			60	137.64	-0.15	33.00	59.35	8.09	2.45
800	Copertura	179	0	-40.98	-0.36	-2.83	58.77	9.53	3.90
			30	-40.98	-0.36	14.80	58.77	8.36	3.90
			60	-40.98	-0.36	32.43	58.77	7.19	3.90
801	Copertura	183	0	-45.05	-0.35	-1.94	58.52	-5.49	-3.42
			30	-45.05	-0.35	15.62	58.52	-4.46	-3.42
			60	-45.05	-0.35	33.18	58.52	-3.44	-3.42
802	Copertura	187	0	27.66	-0.17	-2.27	57.48	-3.58	-1.28
			30	27.66	-0.17	14.97	57.48	-3.19	-1.28
			60	27.66	-0.17	32.22	57.48	-2.81	-1.28
803	Copertura	191	0	1.53	-0.23	-1.88	57.98	-1.80	-0.36
			30	1.53	-0.23	15.51	57.98	-1.69	-0.36
			60	1.53	-0.23	32.91	57.98	-1.59	-0.36
804	Copertura	194	0	67.08	-0.21	-2.24	57.18	0.82	1.31
			30	67.08	-0.21	14.91	57.18	0.42	1.31
			60	67.08	-0.21	32.07	57.18	0.03	1.31
805	Copertura	198	0	64.18	-0.02	-1.78	57.53	2.96	1.45
			30	64.18	-0.02	15.48	57.53	2.53	1.45
			60	64.18	-0.02	32.73	57.53	2.09	1.45
806	Copertura	203	0	-132.20	0.74	-3.91	51.28	-2.41	-7.43
			30	-132.20	0.74	11.48	51.28	-0.18	-7.43
			60	-132.20	0.74	26.86	51.28	2.04	-7.43
807	Copertura	207	0	-190.75	-0.46	-0.40	55.27	-12.19	-22.25
			30	-190.75	-0.46	16.19	55.27	-5.52	-22.25
			60	-190.75	-0.46	32.77	55.27	1.16	-22.25

1.1.11.2 Piastre SLU

Tabella 22.I

Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
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1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	-0.309	-2.133	-0.617	-21.930	-70.077	34.846	1.700	-2.389
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	-0.408	2.166	0.871	-136.065	-533.377	89.162	-3.135	6.742
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	-1.603	-4.592	0.920	381.168	1116.593	-165.693	12.140	13.966

1.1.12 Risultati Condizioni (Vento (-Y)).

1.1.12.1 Sollecitazioni SLU

Tabella 23.I

Sollecitazioni									
Asta	Imp.	Fili	X [cm]	N [daN]	Mt [daNm]	Mxz [daNm]	Txz [daN]	Mxy [daNm]	Txy [daN]
1	Fondazio ne	1, 2	0	12.43	37.33	28.33	-191.34	-11.90	-26.84
			42	12.46	37.32	-35.30	-117.09	-1.47	-23.53
			83	12.55	37.31	-70.49	-54.34	7.80	-21.26
2	Fondazio ne	1, 2	0	-6.86	-43.42	-52.03	-43.00	7.80	18.17
			42	-6.71	-43.42	-58.53	10.04	-0.05	19.43
			83	-6.51	-43.43	-44.64	55.44	-8.21	19.69
3	Fondazio ne	1, 15	0	51.79	-54.15	21.61	-243.07	0.69	0.42
			40	44.26	-54.14	-59.50	-175.88	0.49	0.62
			80	36.75	-54.14	-117.60	-126.95	0.20	0.86
4	Fondazio ne	1, 15	0	8.10	-55.48	-84.52	-108.56	0.20	5.73
			40	0.61	-55.48	-119.08	-75.31	-2.13	5.99
			80	-6.89	-55.48	-143.00	-54.39	-4.56	6.26
5	Fondazio ne	2, 3	0	-10.68	21.41	-63.53	4.75	-9.51	-31.69
			35	-10.50	21.40	-56.04	38.44	1.22	-30.52
			69	-10.33	21.39	-37.29	70.17	11.55	-29.37
6	Fondazio ne	2, 3	0	-14.28	-119.50	-59.25	70.62	11.55	34.44
			35	-14.11	-119.51	-29.60	101.41	-0.53	35.59
			69	-13.95	-119.52	10.65	132.11	-13.01	36.77
7	Fondazio ne	3, 4	0	-18.68	48.79	-13.35	-27.87	-15.03	-43.68
			35	-18.52	48.78	-17.68	3.05	-0.16	-42.50
			69	-18.38	48.77	-11.25	34.46	14.30	-41.35
8	Fondazio ne	3, 4	0	-19.83	-133.15	-33.68	59.75	14.30	40.79
			35	-19.69	-133.16	-7.55	92.03	0.03	41.94
			69	-19.56	-133.17	29.91	125.51	-14.64	43.12
9	Fondazio ne	4, 5	0	-22.52	72.64	11.51	-55.30	-16.05	-46.53
			35	-22.40	72.63	-1.66	-20.73	-0.20	-45.35
			69	-22.29	72.62	-2.74	14.81	15.25	-44.21
10	Fondazio	4, 5	0	-24.00	-133.62	-18.57	39.26	15.25	42.86

	ne								
			35	-23.90	-133.63	1.23	75.88	0.26	44.00
			69	-23.81	-133.64	33.88	113.68	-15.12	45.16
11	Fondazio ne	5, 6	0	-25.68	90.60	20.36	-73.26	-16.12	-47.07
			35	-25.60	90.58	1.73	-34.53	-0.08	-45.91
			69	-25.52	90.57	-3.42	4.92	15.56	-44.78
12	Fondazio ne	5, 6	0	-25.52	-132.92	-13.90	27.65	15.56	40.16
			35	-25.46	-132.93	2.54	67.85	1.51	41.29
			69	-25.40	-132.94	32.99	108.89	-12.93	42.44
13	Fondazio ne	6, 7	0	-25.46	107.11	24.86	-87.22	-18.52	-51.19
			35	-25.42	107.09	1.93	-45.63	-1.06	-50.03
			69	-25.38	107.08	-6.60	-3.73	16.01	-48.90
14	Fondazio ne	6, 7	0	-25.23	-128.27	-11.95	17.74	16.01	48.67
			35	-25.21	-128.28	1.44	60.02	-0.98	49.80
			69	-25.19	-128.30	29.51	102.75	-18.35	50.96
15	Fondazio ne	7, 8	0	-26.29	118.16	30.74	-98.97	-13.48	-43.39
			35	-26.29	118.15	4.00	-56.05	1.29	-42.24
			69	-26.29	118.14	-7.95	-13.22	15.67	-41.12
16	Fondazio ne	7, 8	0	-23.53	-118.98	-10.44	10.26	15.67	44.32
			35	-23.54	-118.99	0.48	53.03	0.18	45.44
			69	-23.57	-119.00	26.16	95.84	-15.69	46.59
17	Fondazio ne	8, 9	0	-27.62	125.99	34.49	-106.54	-15.40	-44.81
			35	-27.66	125.98	5.10	-63.95	-0.14	-43.66
			69	-27.70	125.96	-9.68	-21.88	14.73	-42.54
18	Fondazio ne	8, 9	0	-18.76	-102.35	-5.46	-6.17	14.73	38.37
			35	-18.81	-102.37	-0.40	35.40	1.30	39.49
			69	-18.88	-102.38	18.94	76.54	-12.52	40.65
19	Fondazio ne	9, 10	0	-26.81	131.11	29.87	-103.40	-16.57	-46.22
			35	-26.88	131.10	1.23	-62.86	-0.83	-45.06
			69	-26.97	131.09	-13.57	-23.14	14.52	-43.91
20	Fondazio ne	9, 10	0	-17.13	-82.75	-3.90	-3.18	14.52	45.35
			35	-17.22	-82.76	1.77	35.79	-1.32	46.50
			69	-17.32	-82.77	20.76	74.07	-17.56	47.67
21	Fondazio ne	10, 11	0	-24.42	135.37	38.09	-119.72	-11.87	-39.60
			35	-24.53	135.36	3.29	-82.37	1.59	-38.43
			69	-24.64	135.35	-18.84	-46.24	14.65	-37.29
22	Fondazio ne	10, 11	0	-17.03	-63.90	-2.11	-16.66	14.65	42.81
			35	-17.15	-63.91	-1.77	18.32	-0.31	43.96
			69	-17.28	-63.92	10.46	52.26	-15.68	45.13
23	Fondazio ne	11, 12	0	-17.49	131.12	31.62	-123.56	-14.17	-41.77
			35	-17.63	131.11	-5.29	-90.79	0.03	-40.60
			69	-17.77	131.11	-31.11	-59.31	13.84	-39.45
24	Fondazio ne	11, 12	0	-11.68	-40.57	-9.05	-33.18	13.84	40.25
			35	-11.83	-40.58	-15.19	-2.72	-0.24	41.40
			69	-11.99	-40.59	-10.95	27.03	-14.73	42.58
25	Fondazio ne	12, 13	0	-8.80	116.74	12.04	-128.03	-12.70	-36.23
			35	-8.96	116.74	-27.04	-98.74	-0.41	-35.05
			69	-9.12	116.73	-56.05	-69.64	11.49	-33.90
26	Fondazio ne	12, 13	0	-2.06	-18.84	-34.42	-59.15	11.49	30.64
			35	-2.22	-18.85	-49.71	-29.47	0.72	31.78
			69	-2.39	-18.86	-54.52	1.72	-10.45	32.94
27	Fondazio ne	13, 14	0	-4.95	48.43	-38.86	-58.04	-9.28	-21.38
			42	-5.14	48.42	-54.59	-16.49	-0.41	-21.14
			83	-5.28	48.41	-51.77	31.58	8.15	-19.91
28	Fondazio ne	13, 14	0	13.56	-27.74	-57.74	37.08	8.15	20.80

			42	13.48	-27.75	-30.96	93.60	-0.92	23.03
			83	13.47	-27.76	21.34	160.11	-11.14	26.30
29	Fondazio ne	14, 16	0	49.49	43.10	7.62	-195.41	-1.16	-1.31
			40	42.00	43.10	-56.02	-135.19	-0.60	-1.50
			80	34.54	43.09	-98.94	-90.85	0.04	-1.72
30	Fondazio ne	14, 16	0	10.75	47.19	-77.82	-81.10	0.03	-4.92
			40	3.30	47.19	-102.05	-50.37	2.04	-5.17
			80	-4.15	47.18	-116.28	-30.32	4.15	-5.45
31	Fondazio ne	15, 17	0	37.75	3.48	-136.30	96.25	-3.35	-6.63
			33	31.53	3.48	-101.38	107.09	-1.20	-6.41
			66	25.33	3.48	-63.53	114.28	0.88	-6.19
32	Fondazio ne	15, 17	0	8.40	-8.98	-60.93	132.48	0.87	2.47
			33	2.20	-8.98	-15.10	137.47	0.02	2.67
			66	-4.00	-8.98	32.12	140.95	-0.89	2.87
33	Fondazio ne	16, 18	0	33.27	-1.25	-112.27	71.86	3.20	6.45
			33	27.09	-1.25	-85.41	82.78	1.11	6.22
			66	20.92	-1.25	-55.53	90.38	-0.90	5.99
34	Fondazio ne	16, 18	0	8.39	11.11	-50.93	102.49	-0.90	-3.00
			33	2.22	11.11	-14.91	108.03	0.12	-3.22
			66	-3.94	11.11	22.68	112.08	1.22	-3.43
35	Fondazio ne	17, 19	0	52.12	-17.28	29.03	-89.37	-0.42	-1.03
			33	45.93	-17.28	1.14	-87.49	-0.12	-0.84
			66	39.75	-17.28	-26.44	-87.44	0.13	-0.67
36	Fondazio ne	17, 19	0	19.25	-18.40	-9.72	-81.94	0.13	-0.39
			33	13.09	-18.40	-35.75	-83.53	0.23	-0.23
			66	6.93	-18.40	-62.52	-86.31	0.29	-0.09
37	Fondazio ne	18, 20	0	42.05	13.52	22.22	-76.03	0.85	1.98
			33	35.90	13.52	-1.16	-73.47	0.23	1.77
			66	29.75	13.52	-23.98	-72.55	-0.32	1.57
38	Fondazio ne	18, 20	0	14.34	17.49	-10.14	-67.33	-0.31	-0.41
			33	8.20	17.49	-31.19	-67.87	-0.15	-0.60
			66	2.07	17.49	-52.60	-69.46	0.08	-0.78
39	Fondazio ne	19, 21	0	54.31	-3.95	-65.73	95.37	0.31	0.60
			33	48.16	-3.95	-33.55	92.23	0.09	0.73
			66	42.04	-3.95	-2.35	89.57	-0.18	0.86
40	Fondazio ne	19, 21	0	20.48	-1.19	-2.41	87.85	-0.18	-0.70
			33	14.36	-1.19	27.47	85.99	0.03	-0.58
			66	8.25	-1.19	56.85	84.71	0.21	-0.48
41	Fondazio ne	20, 22	0	43.09	2.83	-56.25	79.66	0.03	0.26
			33	36.97	2.83	-29.06	77.74	-0.03	0.09
			66	30.86	2.83	-2.45	76.22	-0.03	-0.08
42	Fondazio ne	20, 22	0	13.25	2.14	-2.54	74.66	-0.03	0.03
			33	7.15	2.13	23.15	73.80	-0.01	-0.13
			66	1.05	2.13	48.66	73.42	0.06	-0.27
43	Fondazio ne	21, 23	0	55.36	-16.63	50.45	-84.04	0.17	0.52
			33	49.26	-16.63	23.72	-85.43	-0.02	0.61
			66	43.18	-16.63	-3.58	-87.58	-0.23	0.70
44	Fondazio ne	21, 23	0	18.40	-12.73	8.55	-96.41	-0.24	-0.92
			33	12.32	-12.73	-22.54	-99.53	0.05	-0.84
			66	6.26	-12.73	-54.80	-103.45	0.32	-0.78
45	Fondazio ne	22, 24	0	41.77	12.39	43.14	-75.87	0.10	0.33
			33	35.67	12.39	19.26	-76.35	0.01	0.19
			66	29.59	12.39	-4.89	-77.47	-0.03	0.06
46	Fondazio ne	22, 24	0	9.86	11.43	4.37	-79.98	-0.03	0.12
			33	3.78	11.43	-21.10	-81.89	-0.04	0.00

			66	-2.29	11.43	-47.31	-84.42	-0.02	-0.12
47	Fondazio ne	23, 25	0	56.34	3.94	-64.80	116.05	0.28	0.77
			33	50.28	3.94	-25.97	111.99	0.01	0.83
			66	44.25	3.94	11.60	108.52	-0.27	0.87
48	Fondazio ne	23, 25	0	19.70	4.90	8.01	104.01	-0.27	4.46
			33	13.67	4.90	43.07	101.27	-1.75	4.49
			66	7.65	4.90	77.28	98.79	-3.23	4.51
49	Fondazio ne	24, 26	0	38.28	-4.32	-55.46	87.29	-0.01	0.17
			33	32.22	-4.32	-25.88	84.73	-0.05	0.06
			66	26.16	-4.32	2.95	82.81	-0.06	-0.03
50	Fondazio ne	24, 26	0	7.30	-6.03	-1.96	76.96	-0.05	-4.65
			33	1.26	-6.03	24.45	75.89	1.50	-4.74
			66	-4.79	-6.03	50.62	75.46	3.07	-4.81
51	Fondazio ne	25, 26	0	-1.41	6.94	5.59	-12.74	-7.44	-18.07
			49	-1.39	6.93	-1.53	-16.43	-0.80	-9.22
			97	-1.38	6.93	-10.34	-19.67	1.56	-0.47
52	Fondazio ne	25, 26	0	-2.67	3.00	-1.08	2.14	1.53	-5.95
			49	-2.65	3.00	-0.70	-0.42	2.31	2.72
			97	-2.64	3.00	-1.37	-2.19	-1.11	11.31
53	Fondazio ne	25, 26	0	-1.27	3.57	2.31	1.12	-1.12	-8.77
			49	-1.26	3.57	2.59	0.16	1.06	-0.22
			97	-1.25	3.57	2.57	-0.11	-0.90	8.29
54	Fondazio ne	25, 26	0	-1.45	1.71	3.01	-1.06	-0.91	-8.35
			49	-1.44	1.71	2.55	-0.77	1.09	0.11
			97	-1.44	1.71	2.32	-0.09	-1.02	8.54
55	Fondazio ne	25, 26	0	-1.92	0.59	2.07	-1.67	-1.03	-8.33
			49	-1.91	0.59	1.48	-0.72	0.98	0.07
			97	-1.91	0.59	1.39	0.38	-1.09	8.45
56	Fondazio ne	25, 26	0	-2.75	0.09	1.12	-1.63	-1.10	-8.33
			49	-2.75	0.09	0.61	-0.45	0.92	0.03
			97	-2.76	0.09	0.69	0.77	-1.12	8.36
57	Fondazio ne	25, 26	0	-3.67	-0.08	0.52	-1.43	-1.13	-8.31
			49	-3.67	-0.08	0.12	-0.21	0.89	0.01
			97	-3.68	-0.08	0.31	0.98	-1.14	8.32
58	Fondazio ne	25, 26	0	-4.53	-0.11	0.24	-1.25	-1.14	-8.23
			49	-4.54	-0.11	-0.08	-0.08	0.85	0.07
			97	-4.56	-0.11	0.16	1.06	-1.21	8.36
59	Fondazio ne	25, 26	0	-5.26	-0.09	0.14	-1.15	-1.21	-8.46
			49	-5.28	-0.09	-0.14	-0.04	0.89	-0.17
			97	-5.30	-0.09	0.11	1.04	-1.04	8.11
60	Fondazio ne	25, 26	0	-5.57	0.11	0.11	-1.04	-1.04	-8.07
			49	-5.59	0.11	-0.13	0.02	0.87	0.21
			97	-5.62	0.11	0.14	1.06	-1.25	8.50
61	Fondazio ne	25, 26	0	-6.17	0.04	0.22	-1.05	-1.24	-8.40
			49	-6.21	0.04	-0.03	-0.03	0.83	-0.11
			97	-6.25	0.04	0.20	0.96	-1.14	8.19
62	Fondazio ne	25, 26	0	-6.35	0.10	0.22	-1.00	-1.14	-8.30
			49	-6.39	0.10	-0.01	-0.03	0.88	0.01
			97	-6.44	0.10	0.21	0.91	-1.15	8.33
63	Fondazio ne	25, 26	0	-6.32	0.12	0.26	-0.93	-1.15	-8.38
			49	-6.38	0.12	0.04	-0.02	0.90	-0.04
			97	-6.44	0.12	0.26	0.85	-1.11	8.31
64	Fondazio ne	25, 26	0	-6.00	0.13	0.34	-0.82	-1.11	-8.40
			49	-6.07	0.13	0.15	0.00	0.95	-0.03
			97	-6.14	0.13	0.36	0.77	-1.08	8.37

65	Fondazio ne	25, 26	0	-5.32	0.10	0.48	-0.73	-1.08	-8.45
			49	-5.39	0.10	0.32	-0.03	0.99	-0.02
			97	-5.47	0.10	0.47	0.58	-1.06	8.43
66	Fondazio ne	25, 26	0	-4.42	0.03	0.66	-0.30	-1.05	-8.57
			49	-4.50	0.03	0.65	0.19	1.06	-0.09
			97	-4.59	0.03	0.85	0.53	-0.97	8.44
67	Fondazio ne	25, 26	0	-3.38	-0.03	1.29	-0.47	-0.96	-8.30
			49	-3.47	-0.03	1.13	-0.32	1.00	0.27
			97	-3.56	-0.03	0.97	-0.44	-1.23	8.89
68	Fondazio ne	25, 26	0	-2.37	0.00	-0.82	-3.19	-1.22	-10.56
			49	-2.46	0.00	-2.45	-3.61	1.81	-1.89
			97	-2.56	0.00	-4.33	-4.24	0.61	6.85
69	Fondazio ne	25, 26	0	-1.48	-1.39	-8.63	17.97	0.63	-1.65
			49	-1.58	-1.38	-0.03	17.33	-0.71	7.16
			97	-1.68	-1.38	8.31	16.85	-6.36	16.05
70	Fondazio ne	25, 28	0	65.55	-18.79	63.90	-70.63	4.19	5.87
			43	57.82	-18.79	34.57	-75.05	1.69	5.87
			85	50.12	-18.79	2.77	-82.51	-0.80	5.85
71	Fondazio ne	25, 28	0	21.98	-18.13	11.63	-89.50	-0.80	-1.26
			43	14.31	-18.13	-27.13	-100.77	-0.26	-1.29
			85	6.64	-18.13	-71.45	-115.50	0.30	-1.33
72	Fondazio ne	26, 27	0	26.23	6.65	41.61	-69.76	-3.29	-4.98
			33	20.18	6.65	19.74	-70.15	-1.64	-5.04
			66	14.15	6.65	-2.33	-71.05	0.03	-5.08
73	Fondazio ne	26, 27	0	-5.99	5.61	3.54	-74.75	0.03	-0.22
			33	-12.02	5.61	-20.16	-76.33	0.11	-0.26
			66	-18.06	5.61	-44.48	-78.41	0.20	-0.29
74	Fondazio ne	27, 29	0	20.84	-7.57	-55.52	88.78	0.18	0.40
			33	14.80	-7.57	-25.37	86.75	0.05	0.37
			66	8.76	-7.57	4.22	85.43	-0.07	0.35
75	Fondazio ne	27, 29	0	-11.88	-7.85	-3.08	83.91	-0.07	-0.25
			33	-17.91	-7.85	25.73	83.51	0.02	-0.26
			66	-23.95	-7.85	54.53	83.80	0.10	-0.26
76	Fondazio ne	28, 30	0	82.99	1.93	-82.83	99.38	0.26	-0.53
			37	76.42	1.93	-47.79	85.33	0.46	-0.58
			73	69.89	1.93	-17.89	71.49	0.69	-0.64
77	Fondazio ne	28, 30	0	52.03	12.42	-22.15	47.38	0.69	0.69
			37	45.52	12.42	-5.93	34.60	0.45	0.62
			73	39.03	12.42	5.87	23.19	0.23	0.56
78	Fondazio ne	29, 31	0	14.89	5.21	43.94	-74.05	0.09	0.30
			33	8.85	5.21	20.78	-73.71	-0.01	0.31
			66	2.81	5.21	-2.35	-73.89	-0.12	0.32
79	Fondazio ne	29, 31	0	-18.25	5.60	3.45	-73.15	-0.11	-0.37
			33	-24.29	5.60	-19.61	-74.03	0.00	-0.35
			66	-30.34	5.60	-43.06	-75.46	0.11	-0.31
80	Fondazio ne	30, 32	0	35.86	10.44	-14.79	38.22	0.24	0.34
			34	29.79	10.44	-2.13	28.83	0.14	0.28
			69	23.73	10.43	7.54	20.81	0.05	0.21
81	Fondazio ne	30, 32	0	16.86	9.53	1.07	23.15	0.05	0.09
			34	10.80	9.52	9.02	16.48	0.03	0.02
			69	4.75	9.52	14.91	11.03	0.04	-0.04
82	Fondazio ne	31, 33	0	8.47	-6.40	-54.14	86.94	0.12	0.36
			33	2.42	-6.40	-24.49	85.52	-0.01	0.40
			66	-3.64	-6.40	4.80	84.74	-0.15	0.45
83	Fondazio	31, 33	0	-24.03	-7.45	-1.99	82.44	-0.15	-0.56

	ne								
			33	-30.09	-7.45	26.42	82.50	0.03	-0.50
			66	-36.16	-7.45	54.95	83.15	0.18	-0.44
84	Fondazio ne	32, 34	0	6.72	6.73	-4.23	17.61	0.05	0.13
			35	0.63	6.73	2.26	13.17	0.01	0.07
			69	-5.46	6.73	7.40	9.74	0.00	0.00
85	Fondazio ne	32, 34	0	-10.45	6.01	2.96	9.91	0.00	0.12
			35	-16.55	6.01	7.14	7.41	-0.03	0.05
			69	-22.65	6.01	10.60	5.71	-0.03	-0.01
86	Fondazio ne	33, 35	0	3.61	6.14	45.21	-75.40	0.17	0.47
			33	-2.46	6.14	21.65	-74.81	0.00	0.55
			66	-8.54	6.14	-1.81	-74.87	-0.19	0.63
87	Fondazio ne	33, 35	0	-29.13	6.57	4.25	-73.13	-0.19	-0.60
			33	-35.21	6.57	-18.79	-74.03	-0.01	-0.51
			66	-41.30	6.57	-42.25	-75.62	0.14	-0.41
88	Fondazio ne	34, 36	0	-18.30	4.97	-5.84	9.08	-0.03	-0.02
			35	-24.41	4.97	-1.68	8.07	-0.01	-0.09
			69	-30.53	4.97	2.25	7.76	0.03	-0.15
89	Fondazio ne	34, 36	0	-33.40	5.26	-0.91	7.97	0.03	0.19
			35	-39.53	5.26	3.11	8.37	-0.03	0.13
			69	-45.67	5.26	7.39	9.44	-0.06	0.07
90	Fondazio ne	35, 37	0	-1.26	-4.89	-53.14	86.15	0.14	0.34
			33	-7.36	-4.89	-23.79	84.40	0.01	0.45
			66	-13.47	-4.89	5.05	83.10	-0.16	0.56
91	Fondazio ne	35, 37	0	-33.04	-6.31	-0.10	81.92	-0.16	-0.46
			33	-39.15	-6.31	28.03	81.26	-0.02	-0.34
			66	-45.28	-6.31	56.03	80.97	0.07	-0.21
92	Fondazio ne	36, 38	0	-41.62	5.36	-8.84	4.62	-0.06	-0.03
			35	-47.78	5.36	-5.74	6.31	-0.04	-0.09
			69	-53.96	5.36	-1.93	8.73	0.00	-0.14
93	Fondazio ne	36, 38	0	-56.78	6.23	-5.47	9.09	0.00	0.20
			35	-62.98	6.23	-0.57	12.31	-0.06	0.14
			69	-69.21	6.23	5.61	16.39	-0.10	0.08
94	Fondazio ne	37, 39	0	-2.78	9.46	47.61	-83.90	0.04	0.13
			33	-8.92	9.46	21.07	-84.49	-0.03	0.26
			66	-15.06	9.46	-5.80	-86.00	-0.14	0.41
95	Fondazio ne	37, 39	0	-33.80	8.70	1.47	-85.06	-0.14	-0.05
			33	-39.95	8.70	-25.76	-87.63	-0.14	0.10
			66	-46.11	8.70	-53.99	-91.03	-0.20	0.26
96	Fondazio ne	38, 40	0	-65.50	7.80	-11.83	6.01	-0.10	-0.02
			34	-71.71	7.80	-7.72	10.92	-0.09	-0.08
			69	-77.95	7.80	-1.75	16.82	-0.05	-0.14
97	Fondazio ne	38, 40	0	-81.84	8.87	-6.98	17.24	-0.05	0.25
			34	-88.11	8.87	1.34	24.25	-0.12	0.18
			69	-94.41	8.87	12.27	32.41	-0.17	0.12
98	Fondazio ne	39, 41	0	-2.00	-4.11	-63.48	72.66	-0.17	0.18
			33	-8.17	-4.11	-38.86	69.14	-0.26	0.34
			66	-14.35	-4.11	-15.30	66.33	-0.40	0.52
99	Fondazio ne	39, 41	0	-28.65	-13.68	-21.84	47.32	-0.40	-0.45
			33	-34.83	-13.68	-5.29	45.74	-0.28	-0.28
			66	-41.02	-13.68	10.98	45.60	-0.22	-0.09
100	Fondazio ne	40, 42	0	-92.98	10.84	-7.51	15.80	-0.16	-0.10
			35	-99.36	10.84	0.79	25.12	-0.12	-0.16
			69	-105.78	10.84	12.51	35.53	-0.05	-0.23
101	Fondazio ne	40, 42	0	-115.32	7.66	6.06	47.75	-0.05	1.17

			35	-121.79	7.66	25.77	59.15	-0.44	1.09
			69	-128.30	7.67	49.55	71.19	-0.80	1.01
102	Fondazio ne	41, 44	0	-47.43	-13.03	-9.57	44.93	-0.15	-0.76
			33	-53.64	-13.03	6.68	46.25	0.07	-0.58
			66	-59.87	-13.03	23.60	49.01	0.23	-0.39
103	Fondazio ne	41, 44	0	-73.25	-6.28	17.05	64.60	0.23	-4.85
			33	-79.50	-6.28	40.24	68.52	1.80	-4.66
			66	-85.78	-6.29	64.85	73.08	3.31	-4.47
104	Fondazio ne	42, 43	0	-132.24	-1.98	32.99	38.46	-0.75	7.03
			23	-136.62	-1.98	43.64	46.50	-2.36	6.98
			46	-141.01	-1.98	56.11	54.26	-3.96	6.91
105	Fondazio ne	43, 44	0	9.12	11.11	7.90	-38.93	-5.74	-16.21
			49	8.98	11.11	-7.48	-25.07	-0.11	-6.91
			97	8.85	11.11	-17.11	-15.23	1.00	2.32
106	Fondazio ne	43, 44	0	7.09	5.97	-11.99	-5.62	0.99	-6.73
			49	6.96	5.97	-13.01	0.84	2.03	2.44
			97	6.85	5.97	-11.55	4.68	-1.38	11.56
107	Fondazio ne	43, 44	0	7.86	2.03	-8.85	0.10	-1.39	-9.51
			49	7.75	2.03	-8.25	2.00	1.03	-0.42
			97	7.64	2.03	-7.09	2.47	-0.97	8.64
108	Fondazio ne	43, 44	0	9.52	0.59	-6.05	2.18	-0.98	-8.75
			49	9.42	0.59	-5.06	1.66	1.07	0.29
			97	9.33	0.59	-4.50	0.49	-1.26	9.30
109	Fondazio ne	43, 44	0	12.34	-0.01	-3.50	2.92	-1.27	-8.99
			49	12.26	-0.01	-2.43	1.34	0.92	0.01
			97	12.18	-0.01	-2.19	-0.46	-1.27	8.99
110	Fondazio ne	43, 44	0	15.08	-0.20	-1.64	2.62	-1.28	-8.92
			49	15.01	-0.20	-0.81	0.72	0.88	0.06
			97	14.96	-0.20	-0.92	-1.21	-1.33	9.02
111	Fondazio ne	43, 44	0	17.50	-0.22	-0.69	2.24	-1.33	-8.92
			49	17.46	-0.22	-0.06	0.32	0.83	0.04
			97	17.43	-0.22	-0.35	-1.56	-1.37	8.99
112	Fondazio ne	43, 44	0	19.48	-0.17	-0.29	1.93	-1.37	-8.94
			49	19.47	-0.17	0.20	0.09	0.80	0.01
			97	19.47	-0.17	-0.19	-1.70	-1.38	8.95
113	Fondazio ne	43, 44	0	20.94	-0.06	-0.21	1.83	-1.38	-8.87
			49	20.96	-0.06	0.25	0.07	0.76	0.07
			97	21.00	-0.06	-0.15	-1.66	-1.45	9.01
114	Fondazio ne	43, 44	0	21.99	-0.09	-0.25	1.68	-1.45	-9.05
			49	22.04	-0.09	0.14	-0.03	0.78	-0.11
			97	22.12	-0.09	-0.30	-1.71	-1.34	8.82
115	Fondazio ne	43, 44	0	22.11	0.14	-0.19	1.55	-1.34	-8.86
			49	22.20	0.14	0.14	-0.11	0.80	0.08
			97	22.31	0.14	-0.34	-1.75	-1.41	9.01
116	Fondazio ne	43, 44	0	21.82	0.22	-0.36	1.58	-1.41	-8.99
			49	21.94	0.22	-0.01	-0.04	0.79	-0.06
			97	22.09	0.22	-0.44	-1.62	-1.36	8.88
117	Fondazio ne	43, 44	0	20.79	0.34	-0.44	1.50	-1.36	-8.98
			49	20.95	0.34	-0.12	-0.04	0.84	-0.04
			97	21.12	0.34	-0.54	-1.53	-1.32	8.91
118	Fondazio ne	43, 44	0	19.02	0.48	-0.58	1.34	-1.32	-9.01
			49	19.21	0.48	-0.31	-0.08	0.89	-0.06
			97	19.42	0.48	-0.72	-1.41	-1.26	8.90
119	Fondazio ne	43, 44	0	16.51	0.67	-0.86	1.02	-1.26	-9.04
			49	16.72	0.67	-0.71	-0.19	0.96	-0.07

			97	16.96	0.67	-1.12	-1.25	-1.19	8.91
120	Fondazio ne	43, 44	0	13.32	0.93	-1.53	0.49	-1.19	-9.14
			49	13.56	0.93	-1.56	-0.35	1.07	-0.15
			97	13.82	0.93	-1.92	-0.90	-1.05	8.87
121	Fondazio ne	43, 44	0	9.80	0.68	-3.02	-0.43	-1.04	-8.64
			49	10.07	0.68	-3.34	-0.58	0.96	0.40
			97	10.34	0.68	-3.60	-0.14	-1.44	9.47
122	Fondazio ne	43, 44	0	6.86	-1.32	-6.29	-0.70	-1.43	-11.41
			49	7.14	-1.32	-6.43	0.53	1.91	-2.31
			97	7.42	-1.32	-5.70	2.91	0.82	6.83
123	Fondazio ne	43, 44	0	5.24	-3.58	-13.57	20.15	0.84	-2.48
			49	5.53	-3.58	-2.94	24.06	-0.19	6.72
			97	5.82	-3.58	10.06	29.90	-5.71	15.98
124	Fondazio ne	43, 45	0	-91.73	-20.56	48.19	-104.78	1.81	3.33
			33	-98.07	-20.56	16.60	-94.68	0.72	3.23
			66	-104.45	-20.56	-11.93	-86.27	-0.32	3.11
125	Fondazio ne	43, 45	0	-122.03	-12.86	5.23	-113.71	-0.33	-0.96
			33	-128.44	-12.86	-29.87	-107.10	0.01	-1.09
			66	-134.91	-12.86	-63.04	-101.99	0.40	-1.24
126	Fondazio ne	44, 46	0	-44.79	13.48	58.12	-96.15	-2.31	-3.86
			33	-51.09	13.48	28.39	-91.83	-1.07	-3.65
			66	-57.42	13.48	-0.07	-88.49	0.10	-3.43
127	Fondazio ne	44, 46	0	-75.98	13.72	13.88	-102.57	0.10	-0.12
			33	-82.32	13.72	-18.32	-100.51	0.11	0.11
			66	-88.70	13.72	-50.05	-99.65	0.03	0.35
128	Fondazio ne	45, 47	0	-74.07	2.47	-72.38	92.14	0.36	0.69
			33	-80.58	2.47	-39.94	96.55	0.16	0.53
			66	-87.11	2.47	-6.03	101.18	0.01	0.35
129	Fondazio ne	45, 47	0	-108.17	1.61	-9.53	108.63	0.01	-0.13
			33	-114.73	1.61	28.48	113.90	0.08	-0.32
			66	-121.34	1.61	68.34	119.64	0.22	-0.52
130	Fondazio ne	46, 48	0	-33.70	-2.33	-59.10	94.71	0.03	0.56
			33	-40.10	-2.33	-26.51	94.97	-0.19	0.80
			66	-46.52	-2.33	6.16	95.31	-0.50	1.06
131	Fondazio ne	46, 48	0	-66.81	1.24	0.46	83.81	-0.50	-1.44
			33	-73.25	1.24	29.50	84.43	-0.06	-1.18
			66	-79.71	1.24	58.77	85.06	0.28	-0.92
132	Fondazio ne	47, 49	0	-64.95	-19.27	58.45	-115.26	0.14	0.09
			33	-71.59	-19.27	22.66	-109.83	0.14	-0.12
			66	-78.25	-19.27	-11.49	-105.42	0.22	-0.34
133	Fondazio ne	47, 49	0	-96.71	-21.64	3.09	-100.16	0.22	0.45
			33	-103.41	-21.64	-28.05	-96.90	0.11	0.21
			66	-110.14	-21.64	-58.27	-94.52	0.08	-0.03
134	Fondazio ne	48, 50	0	-21.15	18.53	56.14	-103.55	0.31	1.30
			33	-27.63	18.53	23.28	-103.66	-0.17	1.57
			66	-34.12	18.53	-9.83	-105.16	-0.73	1.85
135	Fondazio ne	48, 50	0	-50.17	24.34	4.52	-104.35	-0.73	-1.26
			33	-56.68	24.34	-29.07	-107.42	-0.36	-0.98
			66	-63.20	24.34	-63.91	-111.79	-0.09	-0.69
136	Fondazio ne	49, 51	0	-54.17	-6.69	-62.69	86.28	-0.04	-0.45
			33	-60.93	-6.69	-32.51	88.50	0.15	-0.70
			66	-67.72	-6.69	-1.49	91.37	0.42	-0.96
137	Fondazio ne	49, 51	0	-83.51	-9.07	0.94	94.64	0.42	0.94
			33	-90.33	-9.07	34.14	98.44	0.16	0.67
			66	-97.17	-9.07	68.72	102.88	-0.02	0.39

138	Fondazio ne	50, 52	0	-3.96	8.94	-65.58	63.60	-0.07	1.13
			33	-10.50	8.94	-44.09	58.73	-0.49	1.42
			66	-17.04	8.94	-24.16	54.27	-1.01	1.71
139	Fondazio ne	50, 52	0	-22.11	1.90	-20.69	32.75	-1.01	-1.31
			33	-28.66	1.90	-9.17	29.32	-0.62	-1.02
			66	-35.22	1.90	1.42	27.19	-0.33	-0.73
140	Fondazio ne	51, 53	0	-36.95	-23.75	67.62	-90.45	0.03	0.20
			33	-43.82	-23.75	39.86	-86.24	0.01	-0.08
			66	-50.71	-23.76	13.32	-83.19	0.08	-0.37
141	Fondazio ne	51, 53	0	-62.38	-17.75	33.20	-90.92	0.08	-2.24
			33	-69.29	-17.76	4.85	-89.56	0.87	-2.54
			66	-76.22	-17.76	-23.35	-90.15	1.76	-2.84
142	Fondazio ne	52, 54	0	-26.58	0.58	-10.43	44.17	-0.51	-0.85
			33	-33.15	0.58	5.30	43.45	-0.27	-0.58
			66	-39.73	0.58	21.03	44.14	-0.13	-0.31
143	Fondazio ne	52, 54	0	-34.14	-6.69	22.92	35.62	-0.13	2.32
			33	-40.74	-6.68	36.27	37.48	-0.94	2.58
			66	-47.34	-6.68	50.37	40.00	-1.83	2.83
144	Fondazio ne	53, 55	0	-8.30	-15.33	-22.92	160.36	2.59	5.79
			33	-15.25	-15.33	31.04	157.91	0.72	5.49
			66	-22.20	-15.34	83.87	153.47	-1.04	5.20
145	Fondazio ne	53, 55	0	-28.47	9.80	90.60	132.02	-1.04	-12.19
			33	-35.44	9.80	134.43	124.56	3.03	-12.47
			66	-42.41	9.79	175.05	112.07	7.19	-12.75
146	Fondazio ne	54, 56	0	-33.77	11.57	40.43	81.93	-2.69	-6.18
			33	-40.39	11.57	69.20	84.35	-0.69	-5.95
			66	-47.03	11.58	98.63	85.65	1.24	-5.74
147	Fondazio ne	54, 56	0	-41.77	-6.76	105.88	81.84	1.23	12.12
			33	-48.42	-6.76	134.10	80.51	-2.80	12.30
			66	-55.09	-6.76	161.17	74.43	-6.89	12.46
148	Fondazio ne	55, 57	0	6.50	-75.03	182.98	-44.98	9.35	9.98
			40	-1.91	-75.03	162.17	-70.59	5.45	9.69
			80	-10.32	-75.03	128.06	-112.74	1.64	9.50
149	Fondazio ne	55, 57	0	-41.12	-64.31	154.95	-135.43	1.66	0.69
			40	-49.55	-64.32	91.01	-198.76	1.40	0.61
			80	-58.00	-64.32	-2.94	-286.96	1.15	0.67
150	Fondazio ne	56, 70	0	-3.49	70.11	172.17	-47.12	-8.66	-8.21
			40	-11.54	70.11	152.04	-64.53	-5.42	-8.08
			80	-19.59	70.11	122.04	-97.60	-2.22	-8.07
151	Fondazio ne	56, 70	0	-45.94	58.98	143.57	-120.43	-2.24	-2.21
			40	-54.01	58.98	87.51	-173.55	-1.34	-2.33
			80	-62.12	58.99	5.75	-250.19	-0.37	-2.61
152	Fondazio ne	57, 58	0	-40.21	26.28	-9.57	213.57	-19.24	-39.45
			42	-40.11	26.26	58.10	115.24	-2.86	-39.72
			83	-40.15	26.25	87.94	31.17	14.04	-41.94
153	Fondazio ne	57, 58	0	-12.80	-118.27	91.10	29.94	14.06	43.26
			42	-12.96	-118.28	88.02	-42.50	-3.12	39.11
			83	-13.24	-118.29	56.70	-106.47	-18.19	33.08
154	Fondazio ne	58, 59	0	-30.25	16.79	103.03	-33.93	-20.76	-60.14
			35	-30.22	16.78	82.75	-83.32	0.51	-63.18
			69	-30.20	16.77	45.62	-131.92	22.83	-66.20
155	Fondazio ne	58, 59	0	-19.30	-247.43	98.96	-147.44	22.84	72.70
			35	-19.29	-247.45	39.63	-196.74	-1.73	69.72
			69	-19.29	-247.46	-37.01	-247.95	-25.28	66.84
156	Fondazio	59, 60	0	-15.04	67.76	14.95	42.14	-29.34	-80.49

	ne								
			35	-15.05	67.74	20.34	-11.28	-1.08	-83.34
			69	-15.06	67.73	6.89	-67.18	28.17	-86.21
157	Fondazio ne	59, 60	0	-8.69	-270.47	60.11	-139.48	28.18	85.23
			35	-8.71	-270.49	1.94	-198.29	-0.74	82.39
			69	-8.73	-270.51	-77.09	-260.44	-28.68	79.62
158	Fondazio ne	60, 61	0	-7.76	131.17	-24.58	92.68	-31.63	-86.25
			35	-7.78	131.15	-3.74	27.67	-1.41	-88.99
			69	-7.81	131.13	-5.76	-39.84	29.78	-91.78
159	Fondazio ne	60, 61	0	-5.09	-261.15	30.91	-76.69	29.78	81.36
			35	-5.12	-261.17	-7.54	-146.71	2.19	78.58
			69	-5.15	-261.19	-70.61	-219.35	-24.45	75.88
160	Fondazio ne	61, 62	0	-5.93	170.55	-43.11	139.96	-35.68	-94.20
			35	-5.96	170.53	-7.65	65.30	-2.72	-96.87
			69	-5.99	170.51	1.79	-10.87	31.17	-99.59
161	Fondazio ne	61, 62	0	-6.17	-259.39	23.28	-44.38	31.17	99.03
			35	-6.20	-259.41	-5.38	-122.07	-2.53	96.32
			69	-6.24	-259.44	-61.12	-201.37	-35.30	93.68
162	Fondazio ne	62, 63	0	-5.80	207.95	-47.03	163.75	-27.21	-81.96
			35	-5.85	207.92	-4.37	83.35	1.52	-84.62
			69	-5.89	207.90	10.44	2.33	31.18	-87.33
163	Fondazio ne	62, 63	0	-5.75	-242.97	20.07	-31.46	31.18	92.76
			35	-5.80	-242.99	-4.85	-113.19	-0.35	90.05
			69	-5.84	-243.02	-58.11	-195.76	-30.96	87.40
164	Fondazio ne	63, 64	0	-5.80	229.48	-54.65	185.59	-31.43	-88.18
			35	-5.86	229.45	-4.91	102.72	-0.56	-90.82
			69	-5.91	229.43	16.27	20.05	31.24	-93.53
165	Fondazio ne	63, 64	0	-7.75	-225.65	15.63	-16.04	31.24	93.66
			35	-7.81	-225.68	-4.13	-98.61	-0.60	90.95
			69	-7.87	-225.70	-52.39	-181.19	-31.53	88.30
166	Fondazio ne	64, 65	0	-8.80	245.85	-58.77	199.56	-30.95	-87.32
			35	-8.87	245.83	-4.10	117.45	-0.37	-89.98
			69	-8.93	245.81	22.41	36.32	31.14	-92.70
167	Fondazio ne	64, 65	0	-12.35	-204.52	11.68	0.33	31.14	87.61
			35	-12.42	-204.54	-2.07	-79.96	1.39	84.88
			69	-12.50	-204.56	-43.39	-159.53	-27.43	82.20
168	Fondazio ne	65, 66	0	-13.04	260.29	-59.52	200.18	-35.34	-93.55
			35	-13.13	260.27	-4.02	121.74	-2.60	-96.23
			69	-13.21	260.25	24.70	44.92	31.07	-98.98
169	Fondazio ne	65, 66	0	-14.76	-167.46	2.00	6.45	31.07	99.68
			35	-14.85	-167.48	-8.79	-68.88	-2.85	96.92
			69	-14.95	-167.50	-45.32	-142.70	-35.82	94.19
170	Fondazio ne	66, 67	0	-15.93	266.40	-73.14	220.54	-24.57	-75.30
			35	-16.03	266.37	-9.50	148.75	1.88	-78.06
			69	-16.14	266.35	29.84	79.64	29.30	-80.90
171	Fondazio ne	66, 67	0	-15.87	-117.20	-7.45	41.12	29.30	90.13
			35	-15.99	-117.22	-4.78	-25.38	-1.30	87.27
			69	-16.11	-117.24	-24.61	-89.25	-30.92	84.43
172	Fondazio ne	67, 68	0	-24.91	259.89	-64.67	222.50	-27.85	-76.54
			35	-25.04	259.87	1.51	161.58	-0.95	-79.41
			69	-25.18	259.85	47.26	104.05	26.95	-82.36
173	Fondazio ne	67, 68	0	-24.84	-63.73	-1.85	72.26	26.94	83.60
			35	-24.99	-63.75	13.63	17.79	-1.39	80.61
			69	-25.15	-63.77	10.80	-33.90	-28.68	77.62
174	Fondazio ne	68, 69	0	-36.63	236.98	-37.05	230.54	-24.60	-64.45

			35	-36.80	236.96	33.97	181.46	-1.85	-67.49
			69	-36.98	236.95	88.50	134.80	21.97	-70.63
175	Fondazio ne	68, 69	0	-39.91	-14.25	37.28	135.24	21.96	65.28
			35	-40.11	-14.26	76.14	89.91	-0.01	62.07
			69	-40.33	-14.27	99.41	44.59	-20.87	58.84
176	Fondazio ne	69, 70	0	-19.79	118.09	53.25	93.19	-18.43	-33.28
			42	-19.73	118.07	80.31	35.36	-3.22	-39.59
			83	-19.79	118.06	82.02	-29.34	14.22	-44.04
177	Fondazio ne	69, 70	0	-40.24	-21.70	79.43	-25.22	14.20	41.14
			42	-40.43	-21.72	54.03	-99.69	-2.30	38.58
			83	-40.75	-21.73	-4.77	-186.30	-18.14	37.95
178	Primo Impalcato	1, 2	0	39.30	-10.20	5.61	5.89	141.64	128.48
			83	40.47	-10.20	10.51	5.89	43.34	106.94
			166	41.99	-10.20	15.41	5.89	-34.29	78.76
179	Primo Impalcato	1, 15	0	226.84	-0.56	-258.33	195.74	-132.15	-80.50
			80	226.84	-0.56	-102.72	195.74	-68.15	-80.50
			159	226.84	-0.56	52.89	195.74	-4.16	-80.50
180	Primo Impalcato	2, 3	0	38.95	-8.33	13.81	-10.34	-32.36	19.27
			69	38.95	-8.33	6.67	-10.34	-38.29	-2.09
			138	38.95	-8.33	-0.47	-10.34	-29.49	-23.44
181	Primo Impalcato	3, 4	0	38.97	-7.63	-0.60	-0.21	-29.87	9.80
			69	38.97	-7.63	-0.74	-0.21	-29.26	-11.56
			138	38.97	-7.63	-0.88	-0.21	-13.92	-32.92
182	Primo Impalcato	4, 5	0	38.94	-6.26	-1.08	1.45	-15.25	18.01
			69	38.94	-6.26	-0.08	1.45	-20.31	-3.35
			138	38.94	-6.26	0.92	1.45	-10.63	-24.70
183	Primo Impalcato	5, 6	0	38.91	-4.42	0.78	-0.43	-11.93	21.43
			69	38.91	-4.42	0.48	-0.43	-19.34	0.07
			138	38.91	-4.42	0.19	-0.43	-12.02	-21.29
184	Primo Impalcato	6, 7	0	35.69	-2.15	0.19	0.88	-12.06	23.34
			69	35.69	-2.15	0.79	0.88	-20.79	1.99
			138	35.69	-2.15	1.40	0.88	-14.80	-19.37
185	Primo Impalcato	7, 8	0	36.66	0.24	1.57	0.22	-15.61	22.73
			69	36.66	0.24	1.72	0.22	-23.92	1.37
			138	36.66	0.24	1.87	0.22	-17.50	-19.98
186	Primo Impalcato	8, 9	0	36.63	2.80	2.30	-4.14	-17.15	19.19
			69	36.63	2.80	-0.56	-4.14	-23.02	-2.16
			138	36.63	2.80	-3.41	-4.14	-14.16	-23.52
187	Primo Impalcato	9, 10	0	33.52	4.89	-2.94	4.99	-12.49	19.37
			69	33.52	4.89	0.50	4.99	-18.49	-1.99
			138	33.52	4.89	3.95	4.99	-9.75	-23.34
188	Primo Impalcato	10, 11	0	34.09	6.84	4.55	-5.24	-9.63	24.69
			69	34.09	6.84	0.93	-5.24	-19.30	3.33
			138	34.09	6.84	-2.69	-5.24	-14.23	-18.02
189	Primo Impalcato	11, 12	0	34.07	8.11	-1.93	1.12	-12.78	29.04
			69	34.07	8.11	-1.16	1.12	-25.45	7.69
			138	34.07	8.11	-0.39	1.12	-23.39	-13.67
190	Primo Impalcato	12, 13	0	34.02	8.72	0.26	9.36	-22.75	19.15
			69	34.02	8.72	6.71	9.36	-28.59	-2.21
			138	34.02	8.72	13.17	9.36	-19.70	-23.57
191	Primo Impalcato	13, 14	0	42.96	8.60	15.18	-16.01	-20.24	-60.60
			83	41.43	8.60	1.87	-16.01	42.30	-88.77
			166	40.27	8.60	-11.43	-16.01	125.49	-110.31
192	Primo Impalcato	14, 16	0	154.85	0.74	-134.90	94.18	112.26	67.39
			80	154.85	0.74	-60.03	94.18	58.68	67.39

			159	154.85	0.74	14.84	94.18	5.11	67.39
193	Primo Impalcato	15, 17	0	172.80	0.38	-70.24	124.78	-4.82	-12.09
			66	172.80	0.38	12.11	124.78	3.15	-12.09
			132	172.80	0.38	94.47	124.78	11.13	-12.09
194	Primo Impalcato	16, 18	0	110.25	-0.29	-53.67	91.12	6.01	10.86
			66	110.25	-0.29	6.47	91.12	-1.16	10.86
			132	110.25	-0.29	66.61	91.12	-8.33	10.86
195	Primo Impalcato	17, 19	0	122.31	0.11	-26.63	30.52	10.73	5.74
			66	122.31	0.11	-6.49	30.52	6.94	5.74
			132	122.31	0.11	13.66	30.52	3.15	5.74
196	Primo Impalcato	18, 20	0	106.91	-0.11	-13.68	8.30	-8.25	-3.92
			66	106.91	-0.11	-8.20	8.30	-5.66	-3.92
			132	106.91	-0.11	-2.73	8.30	-3.07	-3.92
197	Primo Impalcato	19, 21	0	68.96	-0.02	-109.72	163.54	3.59	3.14
			66	68.96	-0.02	-1.78	163.54	1.52	3.14
			132	68.96	-0.02	106.15	163.54	-0.55	3.14
198	Primo Impalcato	20, 22	0	74.66	0.00	-73.01	109.49	-2.87	-2.35
			66	74.66	0.00	-0.75	109.49	-1.32	-2.35
			132	74.66	0.00	71.51	109.49	0.23	-2.35
199	Primo Impalcato	21, 23	0	11.93	0.00	-17.90	25.75	0.07	0.65
			66	11.93	0.00	-0.91	25.75	-0.36	0.65
			132	11.93	0.00	16.08	25.75	-0.79	0.65
200	Primo Impalcato	22, 24	0	44.54	-0.02	-0.83	-0.47	0.16	-0.20
			66	44.54	-0.02	-1.14	-0.47	0.29	-0.20
			132	44.54	-0.02	-1.45	-0.47	0.42	-0.20
201	Primo Impalcato	23, 25	0	-40.96	-0.01	-108.27	164.97	-0.20	0.02
			66	-40.96	-0.01	0.61	164.97	-0.22	0.02
			132	-40.96	-0.01	109.49	164.97	-0.23	0.02
202	Primo Impalcato	24, 26	0	14.03	0.01	-72.79	109.89	0.38	-0.14
			66	14.03	0.01	-0.27	109.89	0.48	-0.14
			132	14.03	0.01	72.26	109.89	0.57	-0.14
203	Primo Impalcato	25, 28	0	-141.17	0.03	-14.61	22.92	0.37	0.55
			85	-141.17	0.03	4.87	22.92	-0.09	0.55
			170	-141.17	0.03	24.36	22.92	-0.56	0.55
204	Primo Impalcato	26, 27	0	-18.05	-0.07	0.52	-0.81	0.63	0.74
			66	-18.05	-0.07	-0.01	-0.81	0.14	0.74
			132	-18.05	-0.07	-0.55	-0.81	-0.35	0.74
205	Primo Impalcato	27, 29	0	-48.24	-0.01	-72.65	110.05	-0.30	-0.12
			66	-48.24	-0.01	-0.01	110.05	-0.22	-0.12
			132	-48.24	-0.01	72.62	110.05	-0.14	-0.12
206	Primo Impalcato	28, 30	0	-238.48	0.00	-98.19	117.75	0.04	0.26
			73	-238.48	0.00	-12.23	117.75	-0.14	0.26
			146	-238.48	0.00	73.73	117.75	-0.33	0.26
207	Primo Impalcato	29, 31	0	-81.29	-0.03	1.33	-1.07	-0.13	-0.03
			66	-81.29	-0.03	0.62	-1.07	-0.11	-0.03
			132	-81.29	-0.03	-0.09	-1.07	-0.09	-0.03
208	Primo Impalcato	30, 32	0	-198.78	-0.01	-53.15	84.42	0.24	0.33
			69	-198.78	-0.01	4.68	84.42	0.01	0.33
			137	-198.78	-0.01	62.51	84.42	-0.22	0.33
209	Primo Impalcato	31, 33	0	-109.36	0.00	-73.71	111.47	-0.07	-0.22
			66	-109.36	0.00	-0.14	111.47	0.07	-0.22
			132	-109.36	0.00	73.44	111.47	0.21	-0.22
210	Primo Impalcato	32, 34	0	-159.10	0.00	-63.21	91.49	0.34	0.34
			69	-159.10	0.00	-0.08	91.49	0.10	0.34
			138	-159.10	0.00	63.04	91.49	-0.13	0.34

211	Primo Impalcato	33, 35	0	-144.00	-0.04	2.01	-2.56	0.24	0.21
			66	-144.00	-0.04	0.32	-2.56	0.10	0.21
			132	-144.00	-0.04	-1.37	-2.56	-0.04	0.21
212	Primo Impalcato	34, 36	0	-119.49	-0.01	-62.78	91.07	0.43	0.50
			69	-119.49	-0.01	0.06	91.07	0.08	0.50
			138	-119.49	-0.01	62.90	91.07	-0.27	0.50
213	Primo Impalcato	35, 37	0	-174.55	-0.01	-73.66	110.59	-0.02	-0.06
			66	-174.55	-0.01	-0.67	110.59	0.02	-0.06
			132	-174.55	-0.01	72.32	110.59	0.06	-0.06
214	Primo Impalcato	36, 38	0	-79.93	-0.01	-63.03	91.55	0.29	0.45
			69	-79.93	-0.01	0.14	91.55	-0.01	0.45
			138	-79.93	-0.01	63.31	91.55	-0.32	0.45
215	Primo Impalcato	37, 39	0	-214.83	-0.05	3.31	1.56	0.09	0.72
			66	-214.83	-0.05	4.34	1.56	-0.39	0.72
			132	-214.83	-0.05	5.37	1.56	-0.87	0.72
216	Primo Impalcato	38, 40	0	-40.43	-0.02	-62.74	87.05	0.24	0.71
			69	-40.43	-0.02	-3.11	87.05	-0.25	0.71
			137	-40.43	-0.02	56.51	87.05	-0.74	0.71
217	Primo Impalcato	39, 41	0	-250.66	0.04	-65.12	76.70	-0.82	0.37
			66	-250.66	0.04	-14.49	76.70	-1.06	0.37
			132	-250.66	0.04	36.13	76.70	-1.31	0.37
218	Primo Impalcato	40, 42	0	-1.00	-0.02	-70.52	108.23	-0.20	0.50
			69	-1.00	-0.02	4.16	108.23	-0.55	0.50
			138	-1.00	-0.02	78.84	108.23	-0.89	0.50
219	Primo Impalcato	41, 44	0	-200.67	0.18	-40.02	83.71	-1.39	-2.07
			66	-200.67	0.18	15.23	83.71	-0.02	-2.07
			132	-200.67	0.18	70.48	83.71	1.35	-2.07
220	Primo Impalcato	42, 43	0	38.71	0.21	-46.89	287.83	-0.50	-3.23
			23	38.71	0.21	19.32	287.83	0.25	-3.23
			46	38.71	0.21	85.52	287.83	0.99	-3.23
221	Primo Impalcato	43, 45	0	-22.95	0.00	-37.64	44.67	1.38	0.61
			66	-22.95	0.00	-8.15	44.67	0.98	0.61
			132	-22.95	0.00	21.33	44.67	0.58	0.61
222	Primo Impalcato	44, 46	0	-236.26	0.01	-1.94	-4.30	1.24	0.31
			66	-236.26	0.01	-4.78	-4.30	1.04	0.31
			132	-236.26	0.01	-7.62	-4.30	0.84	0.31
223	Primo Impalcato	45, 47	0	-84.76	-0.06	-104.17	162.38	1.14	0.43
			66	-84.76	-0.06	2.99	162.38	0.85	0.43
			132	-84.76	-0.06	110.16	162.38	0.57	0.43
224	Primo Impalcato	46, 48	0	-279.86	-0.04	-79.30	122.67	0.86	1.11
			66	-279.86	-0.04	1.66	122.67	0.12	1.11
			132	-279.86	-0.04	82.62	122.67	-0.61	1.11
225	Primo Impalcato	47, 49	0	-145.14	-0.05	-14.71	22.28	1.21	0.95
			66	-145.14	-0.05	-0.01	22.28	0.58	0.95
			132	-145.14	-0.05	14.70	22.28	-0.05	0.95
226	Primo Impalcato	48, 50	0	-314.56	-0.06	7.29	-6.25	-0.64	-0.48
			66	-314.56	-0.06	3.16	-6.25	-0.32	-0.48
			132	-314.56	-0.06	-0.96	-6.25	-0.01	-0.48
227	Primo Impalcato	49, 51	0	-211.05	-0.06	-110.24	170.45	0.64	5.43
			66	-211.05	-0.06	2.26	170.45	-2.94	5.43
			132	-211.05	-0.06	114.76	170.45	-6.53	5.43
228	Primo Impalcato	50, 52	0	-365.93	-0.06	-69.52	94.08	-0.11	-4.73
			66	-365.93	-0.06	-7.43	94.08	3.02	-4.73
			132	-365.93	-0.06	54.66	94.08	6.14	-4.73
229	Primo	51, 53	0	-274.79	0.16	-9.45	26.74	-6.20	9.70

	Impalcato								
			66	-274.79	0.16	8.19	26.74	-12.61	9.70
			132	-274.79	0.16	25.84	26.74	-19.01	9.70
230	Primo Impalcato	52, 54	0	-308.24	-0.19	-24.53	42.78	5.73	-7.71
			66	-308.24	-0.19	3.71	42.78	10.82	-7.71
			132	-308.24	-0.19	31.94	42.78	15.91	-7.71
231	Primo Impalcato	53, 55	0	-334.78	0.67	-95.58	130.61	-20.17	-22.92
			66	-334.78	0.67	-9.38	130.61	-5.05	-22.92
			132	-334.78	0.67	76.82	130.61	10.08	-22.92
232	Primo Impalcato	54, 56	0	-268.32	-0.67	-38.42	88.22	17.78	25.94
			66	-268.32	-0.67	19.80	88.22	0.66	25.94
			132	-268.32	-0.67	78.02	88.22	-16.46	25.94
233	Primo Impalcato	55, 57	0	-392.57	-1.18	-45.60	196.32	8.64	-144.95
			80	-392.57	-1.18	110.48	196.32	123.88	-144.95
			159	-392.57	-1.18	266.56	196.32	239.12	-144.95
234	Primo Impalcato	56, 70	0	-260.52	1.36	-16.77	77.25	-10.64	124.51
			80	-260.52	1.36	44.65	77.25	-109.62	124.51
			159	-260.52	1.36	106.07	77.25	-208.61	124.51
235	Primo Impalcato	57, 58	0	-66.39	-17.02	28.05	-38.13	255.93	226.60
			83	-68.73	-17.02	-3.65	-38.13	84.56	183.51
			166	-71.78	-17.02	-35.35	-38.13	-45.47	127.16
236	Primo Impalcato	58, 59	0	-55.08	-17.31	-31.16	20.62	-43.99	46.29
			69	-55.08	-17.31	-16.93	20.62	-61.19	3.57
			138	-55.08	-17.31	-2.71	20.62	-48.92	-39.15
237	Primo Impalcato	59, 60	0	-55.14	-15.99	-1.67	2.15	-50.06	26.17
			69	-55.14	-15.99	-0.19	2.15	-53.38	-16.55
			138	-55.14	-15.99	1.29	2.15	-27.22	-59.27
238	Primo Impalcato	60, 61	0	-55.14	-13.33	2.25	-5.47	-30.03	35.54
			69	-55.14	-13.33	-1.52	-5.47	-39.81	-7.18
			138	-55.14	-13.33	-5.29	-5.47	-20.11	-49.90
239	Primo Impalcato	61, 62	0	-51.69	-9.31	-4.66	4.19	-20.15	46.51
			69	-51.69	-9.31	-1.77	4.19	-37.51	3.79
			138	-51.69	-9.31	1.12	4.19	-25.38	-38.93
240	Primo Impalcato	62, 63	0	-55.95	-5.01	1.38	-3.31	-28.71	47.64
			69	-55.95	-5.01	-0.91	-3.31	-46.84	4.92
			138	-55.95	-5.01	-3.19	-3.31	-35.49	-37.80
241	Primo Impalcato	63, 64	0	-55.94	0.27	-3.22	-0.43	-35.98	42.88
			69	-55.94	0.27	-3.51	-0.43	-50.83	0.16
			138	-55.94	0.27	-3.81	-0.43	-36.21	-42.56
242	Primo Impalcato	64, 65	0	-55.92	5.56	-4.37	6.78	-35.59	38.17
			69	-55.92	5.56	0.31	6.78	-47.19	-4.55
			138	-55.92	5.56	4.99	6.78	-29.31	-47.27
243	Primo Impalcato	65, 66	0	-49.59	9.86	4.26	-8.65	-25.82	39.02
			69	-49.59	9.86	-1.71	-8.65	-38.01	-3.70
			138	-49.59	9.86	-7.68	-8.65	-20.72	-46.42
244	Primo Impalcato	66, 67	0	-51.57	13.89	-8.76	8.99	-20.70	48.72
			69	-51.57	13.89	-2.56	8.99	-39.57	6.00
			138	-51.57	13.89	3.64	8.99	-28.97	-36.72
245	Primo Impalcato	67, 68	0	-51.53	16.51	2.13	-3.47	-26.08	55.21
			69	-51.53	16.51	-0.26	-3.47	-49.44	12.49
			138	-51.53	16.51	-2.65	-3.47	-43.32	-30.23
246	Primo Impalcato	68, 69	0	-51.46	17.72	-4.27	-18.90	-41.94	34.10
			69	-51.46	17.72	-17.31	-18.90	-50.74	-8.62
			138	-51.46	17.72	-30.35	-18.90	-30.05	-51.34
247	Primo Impalcato	69, 70	0	-72.93	15.62	-35.07	49.42	-30.22	-111.57

			83	-69.87	15.62	6.01	49.42	86.85	-167.92
			166	-67.54	15.62	47.09	49.42	245.26	-211.00
248	Primo Impalcato	1	0	-351.32	10.63	-23.86	24.77	32.55	16.90
			188	-351.32	10.63	0.91	-0.52	0.78	16.90
			376	-351.32	10.63	-33.72	-38.41	-30.99	16.90
249	Primo Impalcato	2	0	67.39	2.83	-2.35	-22.49	0.20	0.01
			188	67.39	2.83	-87.17	-71.85	0.19	0.01
			376	67.39	2.83	-287.90	-145.80	0.18	0.01
250	Primo Impalcato	3	0	-13.89	2.01	64.21	-91.76	0.04	0.02
			188	-13.89	2.01	-149.79	-139.90	0.01	0.02
			376	-13.89	2.01	-476.86	-212.04	-0.03	0.02
251	Primo Impalcato	4	0	-4.39	1.40	53.39	-116.32	0.12	0.07
			188	-4.39	1.40	-206.79	-164.46	-0.01	0.07
			376	-4.39	1.40	-580.02	-236.60	-0.14	0.07
252	Primo Impalcato	5	0	4.65	1.00	20.18	-123.58	0.09	0.05
			188	4.65	1.00	-253.64	-171.72	0.00	0.05
			376	4.65	1.00	-640.52	-243.86	-0.10	0.05
253	Primo Impalcato	6	0	9.44	0.61	-7.87	-126.25	0.03	0.02
			188	9.44	0.61	-286.71	-174.39	0.00	0.02
			376	9.44	0.61	-678.61	-246.53	-0.03	0.02
254	Primo Impalcato	7	0	8.28	0.20	-18.99	-128.88	-0.05	-0.02
			188	8.28	0.20	-302.79	-177.03	0.00	-0.02
			376	8.28	0.20	-699.65	-249.16	0.05	-0.02
255	Primo Impalcato	8	0	12.58	-0.29	-17.51	-128.71	-0.17	-0.09
			188	12.58	-0.29	-300.99	-176.86	-0.01	-0.09
			376	12.58	-0.29	-697.53	-248.99	0.15	-0.09
256	Primo Impalcato	9	0	17.84	-0.76	-2.06	-125.74	-0.18	-0.10
			188	17.84	-0.76	-279.95	-173.88	0.01	-0.10
			376	17.84	-0.76	-670.90	-246.02	0.20	-0.10
257	Primo Impalcato	10	0	-2.28	-1.12	22.10	-119.14	-0.24	-0.14
			188	-2.28	-1.12	-243.37	-167.28	0.01	-0.14
			376	-2.28	-1.12	-621.90	-239.42	0.26	-0.14
258	Primo Impalcato	11	0	-7.28	-1.51	58.33	-111.21	-0.32	-0.17
			188	-7.28	-1.51	-192.24	-159.36	0.01	-0.17
			376	-7.28	-1.51	-555.88	-231.49	0.33	-0.17
259	Primo Impalcato	12	0	-19.61	-2.03	75.10	-87.90	-0.24	-0.13
			188	-19.61	-2.03	-131.65	-136.04	0.00	-0.13
			376	-19.61	-2.03	-451.45	-208.18	0.24	-0.13
260	Primo Impalcato	13	0	51.64	-2.62	31.81	-29.42	-0.41	-0.13
			188	51.64	-2.62	-66.04	-78.78	-0.17	-0.13
			376	51.64	-2.62	-279.81	-152.74	0.07	-0.13
261	Primo Impalcato	14	0	-276.77	-9.41	-11.71	20.56	-24.04	-14.20
			188	-276.77	-9.41	5.15	-4.72	2.66	-14.20
			376	-276.77	-9.41	-37.37	-42.61	29.36	-14.20
262	Primo Impalcato	15	0	21.13	-0.69	16.72	-8.75	-66.33	-40.10
			188	21.13	-0.69	0.28	-8.75	9.06	-40.10
			376	21.13	-0.69	-16.17	-8.75	84.45	-40.10
263	Primo Impalcato	16	0	-32.80	0.49	13.94	-7.34	54.77	35.14
			188	-32.80	0.49	0.14	-7.34	-11.28	35.14
			376	-32.80	0.49	-13.65	-7.34	-77.34	35.14
264	Primo Impalcato	17	0	-137.72	-0.49	15.57	-8.58	-17.63	-10.27
			188	-137.72	-0.49	-0.56	-8.58	1.68	-10.27
			376	-137.72	-0.49	-16.68	-8.58	21.00	-10.27
265	Primo Impalcato	18	0	-119.06	0.42	13.56	-7.44	15.77	11.32
			188	-119.06	0.42	-0.43	-7.44	-5.51	11.32

			376	-119.06	0.42	-14.42	-7.44	-26.78	11.32
266	Primo Impalcato	19	0	66.50	-0.05	16.60	-9.06	2.80	2.34
			188	66.50	-0.05	-0.44	-9.06	-1.60	2.34
			376	66.50	-0.05	-17.48	-9.06	-6.00	2.34
267	Primo Impalcato	20	0	45.11	0.06	14.84	-8.02	-1.99	0.26
			188	45.11	0.06	-0.24	-8.02	-2.47	0.26
			376	45.11	0.06	-15.33	-8.02	-2.95	0.26
268	Primo Impalcato	21	0	-31.06	0.04	16.82	-9.16	2.48	2.08
			188	-31.06	0.04	-0.40	-9.16	-1.44	2.08
			376	-31.06	0.04	-17.62	-9.16	-5.35	2.08
269	Primo Impalcato	22	0	-36.56	-0.03	14.90	-8.05	-2.34	0.01
			188	-36.56	-0.03	-0.24	-8.05	-2.36	0.01
			376	-36.56	-0.03	-15.38	-8.05	-2.37	0.01
270	Primo Impalcato	23	0	106.30	0.02	16.94	-9.20	0.37	1.45
			188	106.30	0.02	-0.36	-9.20	-2.37	1.45
			376	106.30	0.02	-17.66	-9.20	-5.10	1.45
271	Primo Impalcato	24	0	71.25	-0.01	15.03	-8.10	-0.15	0.55
			188	71.25	-0.01	-0.20	-8.10	-1.18	0.55
			376	71.25	-0.01	-15.44	-8.10	-2.21	0.55
272	Primo Impalcato	25	0	-34.72	0.01	16.79	-9.10	-1.01	0.46
			188	-34.72	0.01	-0.33	-9.10	-1.87	0.46
			376	-34.72	0.01	-17.44	-9.10	-2.73	0.46
273	Primo Impalcato	26	0	-36.11	0.02	15.06	-8.12	-0.60	0.56
			188	-36.11	0.02	-0.20	-8.12	-1.66	0.56
			376	-36.11	0.02	-15.46	-8.12	-2.72	0.56
274	Primo Impalcato	27	0	60.86	0.03	15.09	-8.13	0.01	0.01
			188	60.86	0.03	-0.20	-8.13	-0.01	0.01
			376	60.86	0.03	-15.49	-8.13	-0.04	0.01
275	Primo Impalcato	28	0	109.57	0.00	16.05	-8.82	-2.17	1.06
			188	109.57	0.00	-0.53	-8.82	-4.16	1.06
			376	109.57	0.00	-17.11	-8.82	-6.15	1.06
276	Primo Impalcato	29	0	-46.74	0.02	15.15	-8.16	-1.03	-0.34
			188	-46.74	0.02	-0.20	-8.16	-0.39	-0.34
			376	-46.74	0.02	-15.55	-8.16	0.24	-0.34
277	Primo Impalcato	30	0	21.93	-0.01	18.74	-10.10	-3.06	0.34
			188	21.93	-0.01	-0.25	-10.10	-3.70	0.34
			376	21.93	-0.01	-19.24	-10.10	-4.34	0.34
278	Primo Impalcato	31	0	55.88	0.01	15.15	-8.17	-1.23	-0.90
			188	55.88	0.01	-0.22	-8.17	0.45	-0.90
			376	55.88	0.01	-15.59	-8.17	2.14	-0.90
279	Primo Impalcato	32	0	9.76	-0.01	18.25	-9.92	-2.99	-0.05
			188	9.76	-0.01	-0.40	-9.92	-2.89	-0.05
			376	9.76	-0.01	-19.05	-9.92	-2.79	-0.05
280	Primo Impalcato	33	0	-47.88	0.01	15.28	-8.24	-1.75	-0.89
			188	-47.88	0.01	-0.21	-8.24	-0.07	-0.89
			376	-47.88	0.01	-15.70	-8.24	1.61	-0.89
281	Primo Impalcato	34	0	7.17	0.00	18.40	-9.98	-3.06	-0.37
			188	7.17	0.00	-0.37	-9.98	-2.37	-0.37
			376	7.17	0.00	-19.13	-9.98	-1.68	-0.37
282	Primo Impalcato	35	0	57.56	0.02	15.39	-8.30	-1.59	-1.45
			188	57.56	0.02	-0.21	-8.30	1.13	-1.45
			376	57.56	0.02	-15.81	-8.30	3.86	-1.45
283	Primo Impalcato	36	0	-7.07	0.00	18.52	-10.05	-3.00	-0.67
			188	-7.07	0.00	-0.36	-10.05	-1.73	-0.67
			376	-7.07	0.00	-19.25	-10.05	-0.46	-0.67

284	Primo Impalcato	37	0	-57.85	0.02	15.66	-8.42	-2.39	-1.79
			188	-57.85	0.02	-0.17	-8.42	0.97	-1.79
			376	-57.85	0.02	-16.00	-8.42	4.32	-1.79
285	Primo Impalcato	38	0	-14.66	0.00	18.64	-10.12	-3.26	-1.17
			188	-14.66	0.00	-0.39	-10.12	-1.05	-1.17
			376	-14.66	0.00	-19.42	-10.12	1.16	-1.17
286	Primo Impalcato	39	0	63.22	0.00	15.32	-8.33	-1.77	-2.23
			188	63.22	0.00	-0.34	-8.33	2.43	-2.23
			376	63.22	0.00	-16.01	-8.33	6.63	-2.23
287	Primo Impalcato	40	0	-25.29	-0.02	19.18	-10.36	-2.86	-1.44
			188	-25.29	-0.02	-0.29	-10.36	-0.15	-1.44
			376	-25.29	-0.02	-19.77	-10.36	2.57	-1.44
288	Primo Impalcato	41	0	-0.91	-0.07	18.01	-9.56	0.12	-0.49
			188	-0.91	-0.07	0.03	-9.56	1.05	-0.49
			376	-0.91	-0.07	-17.96	-9.56	1.98	-0.49
289	Primo Impalcato	42	0	-98.87	-0.05	18.34	-9.94	0.57	-0.12
			188	-98.87	-0.05	-0.35	-9.94	0.79	-0.12
			376	-98.87	-0.05	-19.04	-9.94	1.01	-0.12
290	Primo Impalcato	43	0	-37.28	-0.05	17.14	-9.38	-2.93	-1.21
			188	-37.28	-0.05	-0.49	-9.38	-0.66	-1.21
			376	-37.28	-0.05	-18.11	-9.38	1.61	-1.21
291	Primo Impalcato	44	0	-77.12	-0.07	15.72	-8.56	-2.80	0.14
			188	-77.12	-0.07	-0.36	-8.56	-3.07	0.14
			376	-77.12	-0.07	-16.45	-8.56	-3.33	0.14
292	Primo Impalcato	45	0	41.76	0.02	18.41	-9.92	0.68	1.27
			188	41.76	0.02	-0.24	-9.92	-1.71	1.27
			376	41.76	0.02	-18.88	-9.92	-4.10	1.27
293	Primo Impalcato	46	0	56.72	-0.01	16.61	-8.92	-0.94	0.72
			188	56.72	-0.01	-0.15	-8.92	-2.30	0.72
			376	56.72	-0.01	-16.92	-8.92	-3.66	0.72
294	Primo Impalcato	47	0	-114.92	0.07	18.14	-9.85	-0.39	0.04
			188	-114.92	0.07	-0.38	-9.85	-0.46	0.04
			376	-114.92	0.07	-18.90	-9.85	-0.53	0.04
295	Primo Impalcato	48	0	-92.86	0.00	16.68	-8.98	1.56	1.66
			188	-92.86	0.00	-0.20	-8.98	-1.56	1.66
			376	-92.86	0.00	-17.09	-8.98	-4.68	1.66
296	Primo Impalcato	49	0	33.80	0.11	18.33	-9.96	-4.73	-2.06
			188	33.80	0.11	-0.40	-9.96	-0.85	-2.06
			376	33.80	0.11	-19.13	-9.96	3.02	-2.06
297	Primo Impalcato	50	0	49.65	-0.02	16.64	-9.03	4.94	2.05
			188	49.65	-0.02	-0.34	-9.03	1.08	2.05
			376	49.65	-0.02	-17.31	-9.03	-2.78	2.05
298	Primo Impalcato	51	0	-66.69	-0.08	18.24	-9.95	-4.71	-2.42
			188	-66.69	-0.08	-0.47	-9.95	-0.16	-2.42
			376	-66.69	-0.08	-19.18	-9.95	4.40	-2.42
299	Primo Impalcato	52	0	26.14	0.17	18.51	-9.98	3.71	0.60
			188	26.14	0.17	-0.25	-9.98	2.57	0.60
			376	26.14	0.17	-19.01	-9.98	1.44	0.60
300	Primo Impalcato	53	0	175.97	-0.88	17.07	-9.41	32.70	19.83
			188	175.97	-0.88	-0.61	-9.41	-4.58	19.83
			376	175.97	-0.88	-18.30	-9.41	-41.85	19.83
301	Primo Impalcato	54	0	96.87	0.86	18.05	-9.73	-34.08	-21.31
			188	96.87	0.86	-0.24	-9.73	5.99	-21.31
			376	96.87	0.86	-18.54	-9.73	46.06	-21.31
302	Primo	55	0	29.14	-1.20	17.69	-9.26	118.69	72.44

	Impalcato								
			188	29.14	-1.20	0.29	-9.26	-17.50	72.44
			376	29.14	-1.20	-17.12	-9.26	-153.68	72.44
303	Primo Impalcato	56	0	81.25	0.90	14.13	-7.65	-104.70	-65.70
			188	81.25	0.90	-0.26	-7.65	18.81	-65.70
			376	81.25	0.90	-14.65	-7.65	142.32	-65.70
304	Primo Impalcato	57	0	408.95	19.46	-44.01	52.31	-62.23	-35.98
			188	408.95	19.46	10.74	1.73	5.41	-35.98
			376	408.95	19.46	-53.29	-74.06	73.04	-35.98
305	Primo Impalcato	58	0	-139.55	5.34	57.25	-53.84	-1.02	-0.35
			188	-139.55	5.34	-129.06	-152.57	-0.37	-0.35
			376	-139.55	5.34	-547.24	-300.50	0.29	-0.35
306	Primo Impalcato	59	0	16.20	4.06	153.09	-174.94	-0.42	-0.22
			188	16.20	4.06	-258.80	-271.24	-0.01	-0.22
			376	16.20	4.06	-896.84	-415.53	0.40	-0.22
307	Primo Impalcato	60	0	-2.49	2.96	122.46	-221.99	-0.43	-0.23
			188	-2.49	2.96	-377.89	-318.29	0.01	-0.23
			376	-2.49	2.96	-1104.40	-462.58	0.45	-0.23
308	Primo Impalcato	61	0	-9.74	2.16	51.87	-237.51	-0.28	-0.15
			188	-9.74	2.16	-477.66	-333.81	0.01	-0.15
			376	-9.74	2.16	-1233.34	-478.10	0.29	-0.15
309	Primo Impalcato	62	0	-24.08	1.42	6.18	-250.31	-0.12	-0.06
			188	-24.08	1.42	-547.41	-346.61	0.00	-0.06
			376	-24.08	1.42	-1327.15	-490.90	0.12	-0.06
310	Primo Impalcato	63	0	-17.12	0.47	-19.36	-256.75	0.00	0.00
			188	-17.12	0.47	-585.06	-353.05	-0.01	0.00
			376	-17.12	0.47	-1376.92	-497.34	-0.01	0.00
311	Primo Impalcato	64	0	-19.63	-0.57	-17.94	-256.44	0.24	0.12
			188	-19.63	-0.57	-583.05	-352.74	0.01	0.12
			376	-19.63	-0.57	-1374.32	-497.03	-0.22	0.12
312	Primo Impalcato	65	0	-32.19	-1.54	10.23	-249.21	0.29	0.16
			188	-32.19	-1.54	-541.28	-345.51	-0.01	0.16
			376	-32.19	-1.54	-1318.94	-489.80	-0.30	0.16
313	Primo Impalcato	66	0	-5.11	-2.29	57.02	-234.79	0.45	0.24
			188	-5.11	-2.29	-467.40	-331.09	-0.01	0.24
			376	-5.11	-2.29	-1217.96	-475.38	-0.47	0.24
314	Primo Impalcato	67	0	-2.30	-3.08	128.55	-217.64	0.65	0.35
			188	-2.30	-3.08	-363.63	-313.94	-0.01	0.35
			376	-2.30	-3.08	-1081.95	-458.23	-0.66	0.35
315	Primo Impalcato	68	0	14.95	-4.09	163.45	-170.73	0.66	0.35
			188	14.95	-4.09	-240.52	-267.03	0.01	0.35
			376	14.95	-4.09	-870.64	-411.32	-0.65	0.35
316	Primo Impalcato	69	0	-134.76	-5.13	89.93	-59.80	1.31	0.51
			188	-134.76	-5.13	-107.60	-158.53	0.35	0.51
			376	-134.76	-5.13	-536.99	-306.47	-0.60	0.51
317	Primo Impalcato	70	0	318.30	-17.60	-23.86	44.71	52.10	32.98
			188	318.30	-17.60	16.60	-5.87	-9.90	32.98
			376	318.30	-17.60	-61.74	-81.66	-71.89	32.98
318	Fondazione	1, 71	0	-241.34	0.01	0.00	0.00	1.15	0.52
			102	-241.34	0.01	0.00	0.00	0.62	0.52
			204	-241.34	0.01	0.00	0.00	0.08	0.52
319	Fondazione	1, 92	0	-53.68	0.17	0.00	0.00	-0.08	-3.11
			103	-53.68	0.17	0.00	0.00	3.11	-3.11
			206	-53.68	0.17	0.00	0.00	6.31	-3.11
320	Primo Impalcato	92, 2	0	33.32	0.33	0.00	0.00	-2.93	-3.63

			103	33.32	0.33	0.00	0.00	0.80	-3.63
			206	33.32	0.33	0.00	0.00	4.52	-3.63
321	Fondazio ne	6, 89	0	2.84	-0.37	0.00	0.00	15.43	3.80
			100	2.84	-0.37	0.00	0.00	11.63	3.80
			200	2.84	-0.37	0.00	0.00	7.83	3.80
322	Primo Impalcato	89, 7	0	2.54	0.44	0.00	0.00	6.79	-4.55
			100	2.54	0.44	0.00	0.00	11.35	-4.55
			200	2.54	0.44	0.00	0.00	15.91	-4.55
323	Fondazio ne	9, 90	0	12.71	-0.45	0.00	0.00	15.18	4.91
			100	12.71	-0.45	0.00	0.00	10.26	4.91
			200	12.71	-0.45	0.00	0.00	5.34	4.91
324	Primo Impalcato	90, 10	0	-7.94	0.29	0.00	0.00	7.73	-3.17
			100	-7.94	0.29	0.00	0.00	10.90	-3.17
			200	-7.94	0.29	0.00	0.00	14.07	-3.17
325	Fondazio ne	13, 91	0	45.78	-0.30	0.00	0.00	4.30	3.49
			103	45.78	-0.30	0.00	0.00	0.72	3.49
			206	45.78	-0.30	0.00	0.00	-2.87	3.49
326	Primo Impalcato	88, 14	0	-214.16	-0.02	0.00	0.00	0.14	-0.41
			102	-214.16	-0.02	0.00	0.00	0.55	-0.41
			204	-214.16	-0.02	0.00	0.00	0.97	-0.41
327	Primo Impalcato	91, 14	0	-61.90	-0.15	0.00	0.00	5.60	2.67
			103	-61.90	-0.15	0.00	0.00	2.86	2.67
			206	-61.90	-0.15	0.00	0.00	0.11	2.67
328	Primo Impalcato	71, 15	0	211.82	0.05	0.00	0.00	-0.96	-1.18
			102	211.82	0.05	0.00	0.00	0.24	-1.18
			204	211.82	0.05	0.00	0.00	1.44	-1.18
329	Fondazio ne	16, 88	0	182.72	-0.05	0.00	0.00	1.29	1.06
			102	182.72	-0.05	0.00	0.00	0.20	1.06
			204	182.72	-0.05	0.00	0.00	-0.88	1.06
330	Fondazio ne	17, 72	0	-282.14	-0.01	0.00	0.00	0.10	0.11
			100	-282.14	-0.01	0.00	0.00	-0.01	0.11
			199	-282.14	-0.01	0.00	0.00	-0.12	0.11
331	Primo Impalcato	87, 18	0	-244.82	0.01	0.00	0.00	-0.07	-0.12
			100	-244.82	0.01	0.00	0.00	0.05	-0.12
			199	-244.82	0.01	0.00	0.00	0.17	-0.12
332	Primo Impalcato	72, 19	0	273.21	-0.01	0.00	0.00	0.19	0.15
			100	273.21	-0.01	0.00	0.00	0.04	0.15
			199	273.21	-0.01	0.00	0.00	-0.11	0.15
333	Fondazio ne	20, 87	0	235.13	0.01	0.00	0.00	-0.02	-0.11
			100	235.13	0.01	0.00	0.00	0.09	-0.11
			199	235.13	0.01	0.00	0.00	0.20	-0.11
334	Fondazio ne	21, 73	0	-281.27	0.00	0.00	0.00	-0.03	-0.01
			100	-281.27	0.00	0.00	0.00	-0.01	-0.01
			199	-281.27	0.00	0.00	0.00	0.00	-0.01
335	Primo Impalcato	86, 22	0	-245.22	0.00	0.00	0.00	0.02	-0.01
			100	-245.22	0.00	0.00	0.00	0.03	-0.01
			199	-245.22	0.00	0.00	0.00	0.04	-0.01
336	Primo Impalcato	73, 23	0	293.63	0.00	0.00	0.00	-0.04	0.01
			100	293.63	0.00	0.00	0.00	-0.05	0.01
			199	293.63	0.00	0.00	0.00	-0.06	0.01
337	Fondazio ne	24, 86	0	251.71	0.00	0.00	0.00	0.01	0.00
			100	251.71	0.00	0.00	0.00	0.01	0.00
			199	251.71	0.00	0.00	0.00	0.01	0.00
338	Fondazio ne	25, 74	0	-334.18	0.00	0.00	0.00	0.00	0.01
			103	-334.18	0.00	0.00	0.00	-0.01	0.01

			206	-334.18	0.00	0.00	0.00	-0.03	0.01
339	Primo Impalcato	85, 26	0	-248.18	0.00	0.00	0.00	-0.01	-0.02
			100	-248.18	0.00	0.00	0.00	0.01	-0.02
			199	-248.18	0.00	0.00	0.00	0.03	-0.02
340	Fondazione	27, 85	0	251.80	0.00	0.00	0.00	-0.01	-0.01
			100	251.80	0.00	0.00	0.00	0.01	-0.01
			199	251.80	0.00	0.00	0.00	0.02	-0.01
341	Primo Impalcato	74, 28	0	341.18	0.00	0.00	0.00	-0.03	0.02
			103	341.18	0.00	0.00	0.00	-0.05	0.02
			206	341.18	0.00	0.00	0.00	-0.08	0.02
342	Primo Impalcato	84, 29	0	-251.31	0.00	0.00	0.00	-0.01	-0.01
			100	-251.31	0.00	0.00	0.00	0.00	-0.01
			199	-251.31	0.00	0.00	0.00	0.00	-0.01
343	Fondazione	31, 84	0	251.15	0.00	0.00	0.00	-0.03	-0.02
			100	251.15	0.00	0.00	0.00	-0.01	-0.02
			199	251.15	0.00	0.00	0.00	0.01	-0.02
344	Primo Impalcato	83, 33	0	-254.67	0.00	0.00	0.00	-0.02	0.00
			100	-254.67	0.00	0.00	0.00	-0.01	0.00
			199	-254.67	0.00	0.00	0.00	-0.01	0.00
345	Fondazione	35, 83	0	253.33	0.00	0.00	0.00	-0.04	-0.02
			100	253.33	0.00	0.00	0.00	-0.02	-0.02
			199	253.33	0.00	0.00	0.00	0.01	-0.02
346	Primo Impalcato	82, 37	0	-259.54	0.00	0.00	0.00	-0.02	0.00
			100	-259.54	0.00	0.00	0.00	-0.03	0.00
			199	-259.54	0.00	0.00	0.00	-0.03	0.00
347	Fondazione	39, 82	0	256.10	0.00	0.00	0.00	-0.08	-0.04
			100	256.10	0.00	0.00	0.00	-0.04	-0.04
			199	256.10	0.00	0.00	0.00	0.00	-0.04
348	Primo Impalcato	78, 43	0	-305.56	0.00	0.00	0.00	0.02	0.02
			100	-305.56	0.00	0.00	0.00	0.00	0.02
			199	-305.56	0.00	0.00	0.00	-0.02	0.02
349	Primo Impalcato	81, 44	0	-271.81	0.00	0.00	0.00	0.03	-0.01
			100	-271.81	0.00	0.00	0.00	0.05	-0.01
			199	-271.81	0.00	0.00	0.00	0.06	-0.01
350	Fondazione	45, 78	0	305.55	0.00	0.00	0.00	0.06	0.04
			100	305.55	0.00	0.00	0.00	0.02	0.04
			199	305.55	0.00	0.00	0.00	-0.01	0.04
351	Fondazione	46, 81	0	263.71	0.00	0.00	0.00	0.03	0.01
			100	263.71	0.00	0.00	0.00	0.02	0.01
			199	263.71	0.00	0.00	0.00	0.00	0.01
352	Primo Impalcato	77, 47	0	-317.13	0.00	0.00	0.00	-0.04	-0.01
			100	-317.13	0.00	0.00	0.00	-0.03	-0.01
			199	-317.13	0.00	0.00	0.00	-0.02	-0.01
353	Primo Impalcato	80, 48	0	-281.97	0.00	0.00	0.00	0.01	-0.03
			100	-281.97	0.00	0.00	0.00	0.04	-0.03
			199	-281.97	0.00	0.00	0.00	0.07	-0.03
354	Fondazione	49, 77	0	301.05	0.00	0.00	0.00	0.01	-0.02
			100	301.05	0.00	0.00	0.00	0.03	-0.02
			199	301.05	0.00	0.00	0.00	0.05	-0.02
355	Fondazione	50, 80	0	268.73	0.00	0.00	0.00	-0.01	0.00
			100	268.73	0.00	0.00	0.00	0.00	0.00
			199	268.73	0.00	0.00	0.00	0.00	0.00
356	Primo Impalcato	76, 51	0	-297.71	-0.01	0.00	0.00	0.35	0.24
			100	-297.71	-0.01	0.00	0.00	0.11	0.24
			199	-297.71	-0.01	0.00	0.00	-0.13	0.24

357	Fondazio ne	53, 76	0	309.66	-0.02	0.00	0.00	0.21	0.19
			100	309.66	-0.02	0.00	0.00	0.01	0.19
			199	309.66	-0.02	0.00	0.00	-0.18	0.19
358	Primo Impalcato	75, 55	0	-208.62	0.09	0.00	0.00	-1.82	-2.19
			102	-208.62	0.09	0.00	0.00	0.42	-2.19
			204	-208.62	0.09	0.00	0.00	2.66	-2.19
359	Fondazio ne	56, 79	0	-193.24	-0.09	0.00	0.00	2.41	2.02
			102	-193.24	-0.09	0.00	0.00	0.34	2.02
			204	-193.24	-0.09	0.00	0.00	-1.72	2.02
360	Fondazio ne	57, 75	0	247.68	0.03	0.00	0.00	1.95	0.86
			102	247.68	0.03	0.00	0.00	1.07	0.86
			204	247.68	0.03	0.00	0.00	0.19	0.86
361	Fondazio ne	57, 93	0	125.44	0.34	0.00	0.00	-0.37	-5.77
			103	125.44	0.34	0.00	0.00	5.56	-5.77
			206	125.44	0.34	0.00	0.00	11.48	-5.77
362	Primo Impalcato	93, 58	0	-117.80	0.62	0.00	0.00	-6.08	-6.95
			103	-117.80	0.62	0.00	0.00	1.06	-6.95
			206	-117.80	0.62	0.00	0.00	8.21	-6.95
363	Fondazio ne	61, 95	0	4.57	-0.58	0.00	0.00	27.90	6.39
			100	4.57	-0.58	0.00	0.00	21.50	6.39
			200	4.57	-0.58	0.00	0.00	15.10	6.39
364	Primo Impalcato	95, 62	0	-14.63	0.88	0.00	0.00	10.53	-9.73
			100	-14.63	0.88	0.00	0.00	20.27	-9.73
			200	-14.63	0.88	0.00	0.00	30.02	-9.73
365	Primo Impalcato	96, 65	0	-22.80	-0.88	0.00	0.00	-10.17	9.81
			100	-22.80	-0.88	0.00	0.00	-20.00	9.81
			200	-22.80	-0.88	0.00	0.00	-29.82	9.81
366	Fondazio ne	66, 96	0	11.84	0.56	0.00	0.00	-27.55	-6.23
			100	11.84	0.56	0.00	0.00	-21.31	-6.23
			200	11.84	0.56	0.00	0.00	-15.06	-6.23
367	Fondazio ne	69, 94	0	-135.76	-0.58	0.00	0.00	7.94	6.74
			103	-135.76	-0.58	0.00	0.00	1.02	6.74
			206	-135.76	-0.58	0.00	0.00	-5.90	6.74
368	Primo Impalcato	79, 70	0	233.77	-0.03	0.00	0.00	0.28	-0.69
			102	233.77	-0.03	0.00	0.00	0.98	-0.69
			204	233.77	-0.03	0.00	0.00	1.68	-0.69
369	Primo Impalcato	94, 70	0	134.63	-0.32	0.00	0.00	10.66	5.25
			103	134.63	-0.32	0.00	0.00	5.26	5.25
			206	134.63	-0.32	0.00	0.00	-0.13	5.25
370	Primo Impalcato	1, 71	0	211.82	0.36	0.00	0.00	-3.44	-1.29
			102	211.82	0.36	0.00	0.00	-2.12	-1.29
			204	211.82	0.36	0.00	0.00	-0.80	-1.29
371	Primo Impalcato	1, 92	0	33.32	0.10	0.00	0.00	-1.30	0.77
			103	33.32	0.10	0.00	0.00	-2.09	0.77
			206	33.32	0.10	0.00	0.00	-2.87	0.77
372	Primo Impalcato	92, 2	0	-53.68	0.37	0.00	0.00	6.44	1.29
			103	-53.68	0.37	0.00	0.00	5.12	1.29
			206	-53.68	0.37	0.00	0.00	3.80	1.29
373	Primo Impalcato	6, 89	0	2.54	0.24	0.00	0.00	-1.90	-4.42
			100	2.54	0.24	0.00	0.00	2.53	-4.42
			200	2.54	0.24	0.00	0.00	6.95	-4.42
374	Primo Impalcato	89, 7	0	2.84	-0.11	0.00	0.00	7.83	3.93
			100	2.84	-0.11	0.00	0.00	3.90	3.93
			200	2.84	-0.11	0.00	0.00	-0.04	3.93
375	Primo	9, 90	0	-7.94	0.00	0.00	0.00	0.67	-3.48

	Impalcato								
			100	-7.94	0.00	0.00	0.00	4.15	-3.48
			200	-7.94	0.00	0.00	0.00	7.63	-3.48
376	Primo Impalcato	90, 10	0	12.71	-0.29	0.00	0.00	5.61	4.60
			100	12.71	-0.29	0.00	0.00	1.00	4.60
			200	12.71	-0.29	0.00	0.00	-3.60	4.60
377	Primo Impalcato	13, 91	0	-61.90	-0.37	0.00	0.00	2.63	-1.51
			103	-61.90	-0.37	0.00	0.00	4.18	-1.51
			206	-61.90	-0.37	0.00	0.00	5.73	-1.51
378	Primo Impalcato	88, 14	0	182.72	-0.31	0.00	0.00	-0.75	1.13
			102	182.72	-0.31	0.00	0.00	-1.91	1.13
			204	182.72	-0.31	0.00	0.00	-3.06	1.13
379	Primo Impalcato	91, 14	0	45.78	-0.07	0.00	0.00	-2.79	-0.69
			103	45.78	-0.07	0.00	0.00	-2.08	-0.69
			206	45.78	-0.07	0.00	0.00	-1.37	-0.69
380	Primo Impalcato	71, 15	0	-241.34	-0.09	0.00	0.00	-0.24	0.41
			102	-241.34	-0.09	0.00	0.00	-0.66	0.41
			204	-241.34	-0.09	0.00	0.00	-1.08	0.41
381	Primo Impalcato	16, 88	0	-214.16	0.07	0.00	0.00	-0.83	-0.34
			102	-214.16	0.07	0.00	0.00	-0.49	-0.34
			204	-214.16	0.07	0.00	0.00	-0.15	-0.34
382	Primo Impalcato	17, 72	0	273.21	-0.04	0.00	0.00	0.12	-0.03
			100	273.21	-0.04	0.00	0.00	0.15	-0.03
			199	273.21	-0.04	0.00	0.00	0.17	-0.03
383	Primo Impalcato	87, 18	0	235.13	0.03	0.00	0.00	0.19	0.05
			100	235.13	0.03	0.00	0.00	0.14	0.05
			199	235.13	0.03	0.00	0.00	0.09	0.05
384	Primo Impalcato	72, 19	0	-282.14	0.00	0.00	0.00	-0.09	-0.07
			100	-282.14	0.00	0.00	0.00	-0.02	-0.07
			199	-282.14	0.00	0.00	0.00	0.05	-0.07
385	Primo Impalcato	20, 87	0	-244.82	0.00	0.00	0.00	0.04	0.04
			100	-244.82	0.00	0.00	0.00	-0.01	0.04
			199	-244.82	0.00	0.00	0.00	-0.05	0.04
386	Primo Impalcato	21, 73	0	293.63	0.00	0.00	0.00	0.02	0.03
			100	293.63	0.00	0.00	0.00	-0.01	0.03
			199	293.63	0.00	0.00	0.00	-0.04	0.03
387	Primo Impalcato	86, 22	0	251.71	0.00	0.00	0.00	0.00	-0.01
			100	251.71	0.00	0.00	0.00	0.01	-0.01
			199	251.71	0.00	0.00	0.00	0.02	-0.01
388	Primo Impalcato	73, 23	0	-281.27	0.00	0.00	0.00	0.00	0.00
			100	-281.27	0.00	0.00	0.00	0.00	0.00
			199	-281.27	0.00	0.00	0.00	-0.01	0.00
389	Primo Impalcato	24, 86	0	-245.22	0.00	0.00	0.00	-0.01	-0.02
			100	-245.22	0.00	0.00	0.00	0.01	-0.02
			199	-245.22	0.00	0.00	0.00	0.03	-0.02
390	Primo Impalcato	25, 74	0	341.18	0.00	0.00	0.00	0.01	0.02
			103	341.18	0.00	0.00	0.00	-0.01	0.02
			206	341.18	0.00	0.00	0.00	-0.03	0.02
391	Primo Impalcato	85, 26	0	251.80	0.00	0.00	0.00	0.02	0.00
			100	251.80	0.00	0.00	0.00	0.02	0.00
			199	251.80	0.00	0.00	0.00	0.02	0.00
392	Primo Impalcato	27, 85	0	-248.18	0.00	0.00	0.00	-0.02	-0.01
			100	-248.18	0.00	0.00	0.00	-0.01	-0.01
			199	-248.18	0.00	0.00	0.00	-0.01	-0.01
393	Primo Impalcato	74, 28	0	-334.18	0.00	0.00	0.00	-0.02	0.01

			103	-334.18	0.00	0.00	0.00	-0.03	0.01
			206	-334.18	0.00	0.00	0.00	-0.05	0.01
394	Primo Impalcato	84, 29	0	251.15	0.00	0.00	0.00	0.01	-0.01
			100	251.15	0.00	0.00	0.00	0.02	-0.01
			199	251.15	0.00	0.00	0.00	0.02	-0.01
395	Primo Impalcato	31, 84	0	-251.31	0.00	0.00	0.00	0.00	0.00
			100	-251.31	0.00	0.00	0.00	0.00	0.00
			199	-251.31	0.00	0.00	0.00	-0.01	0.00
396	Primo Impalcato	83, 33	0	253.33	0.00	0.00	0.00	0.00	-0.01
			100	253.33	0.00	0.00	0.00	0.02	-0.01
			199	253.33	0.00	0.00	0.00	0.03	-0.01
397	Primo Impalcato	35, 83	0	-254.67	0.00	0.00	0.00	0.00	0.01
			100	-254.67	0.00	0.00	0.00	-0.01	0.01
			199	-254.67	0.00	0.00	0.00	-0.01	0.01
398	Primo Impalcato	82, 37	0	256.10	0.00	0.00	0.00	0.00	-0.02
			100	256.10	0.00	0.00	0.00	0.02	-0.02
			199	256.10	0.00	0.00	0.00	0.04	-0.02
399	Primo Impalcato	39, 82	0	-259.54	0.00	0.00	0.00	0.01	0.02
			100	-259.54	0.00	0.00	0.00	0.00	0.02
			199	-259.54	0.00	0.00	0.00	-0.02	0.02
400	Primo Impalcato	78, 43	0	305.55	0.00	0.00	0.00	-0.01	0.00
			100	305.55	0.00	0.00	0.00	-0.01	0.00
			199	305.55	0.00	0.00	0.00	-0.01	0.00
401	Primo Impalcato	81, 44	0	263.71	-0.01	0.00	0.00	0.00	0.00
			100	263.71	-0.01	0.00	0.00	0.00	0.00
			199	263.71	-0.01	0.00	0.00	0.00	0.00
402	Primo Impalcato	45, 78	0	-305.56	0.00	0.00	0.00	-0.02	-0.02
			100	-305.56	0.00	0.00	0.00	0.00	-0.02
			199	-305.56	0.00	0.00	0.00	0.02	-0.02
403	Primo Impalcato	46, 81	0	-271.81	0.00	0.00	0.00	-0.01	-0.02
			100	-271.81	0.00	0.00	0.00	0.01	-0.02
			199	-271.81	0.00	0.00	0.00	0.03	-0.02
404	Primo Impalcato	77, 47	0	301.05	0.00	0.00	0.00	0.05	0.02
			100	301.05	0.00	0.00	0.00	0.03	0.02
			199	301.05	0.00	0.00	0.00	0.01	0.02
405	Primo Impalcato	80, 48	0	268.73	0.00	0.00	0.00	-0.01	-0.01
			100	268.73	0.00	0.00	0.00	0.01	-0.01
			199	268.73	0.00	0.00	0.00	0.02	-0.01
406	Primo Impalcato	49, 77	0	-317.13	0.01	0.00	0.00	0.02	0.03
			100	-317.13	0.01	0.00	0.00	-0.02	0.03
			199	-317.13	0.01	0.00	0.00	-0.05	0.03
407	Primo Impalcato	50, 80	0	-281.97	0.00	0.00	0.00	-0.07	-0.04
			100	-281.97	0.00	0.00	0.00	-0.03	-0.04
			199	-281.97	0.00	0.00	0.00	0.02	-0.04
408	Primo Impalcato	76, 51	0	309.66	0.01	0.00	0.00	-0.13	-0.12
			100	309.66	0.01	0.00	0.00	-0.01	-0.12
			199	309.66	0.01	0.00	0.00	0.11	-0.12
409	Primo Impalcato	53, 76	0	-297.71	-0.07	0.00	0.00	0.19	-0.07
			100	-297.71	-0.07	0.00	0.00	0.26	-0.07
			199	-297.71	-0.07	0.00	0.00	0.33	-0.07
410	Primo Impalcato	75, 55	0	247.68	-0.16	0.00	0.00	-0.41	0.72
			102	247.68	-0.16	0.00	0.00	-1.15	0.72
			204	247.68	-0.16	0.00	0.00	-1.89	0.72
411	Primo Impalcato	56, 79	0	233.77	0.13	0.00	0.00	-1.59	-0.65
			102	233.77	0.13	0.00	0.00	-0.92	-0.65

			204	233.77	0.13	0.00	0.00	-0.26	-0.65
412	Primo Impalcato	57, 75	0	-208.62	0.65	0.00	0.00	-6.29	-2.33
			102	-208.62	0.65	0.00	0.00	-3.91	-2.33
			204	-208.62	0.65	0.00	0.00	-1.53	-2.33
413	Primo Impalcato	57, 93	0	-117.80	0.15	0.00	0.00	-1.97	1.95
			103	-117.80	0.15	0.00	0.00	-3.97	1.95
			206	-117.80	0.15	0.00	0.00	-5.97	1.95
414	Primo Impalcato	93, 58	0	125.44	0.73	0.00	0.00	11.76	3.13
			103	125.44	0.73	0.00	0.00	8.54	3.13
			206	125.44	0.73	0.00	0.00	5.32	3.13
415	Primo Impalcato	61, 95	0	-14.63	0.57	0.00	0.00	-7.23	-9.13
			100	-14.63	0.57	0.00	0.00	1.91	-9.13
			200	-14.63	0.57	0.00	0.00	11.05	-9.13
416	Primo Impalcato	95, 62	0	4.57	-0.01	0.00	0.00	14.91	6.99
			100	4.57	-0.01	0.00	0.00	7.90	6.99
			200	4.57	-0.01	0.00	0.00	0.90	6.99
417	Primo Impalcato	96, 65	0	11.84	-0.02	0.00	0.00	-14.85	-6.91
			100	11.84	-0.02	0.00	0.00	-7.93	-6.91
			200	11.84	-0.02	0.00	0.00	-1.01	-6.91
418	Primo Impalcato	66, 96	0	-22.80	-0.58	0.00	0.00	7.58	9.14
			100	-22.80	-0.58	0.00	0.00	-1.56	9.14
			200	-22.80	-0.58	0.00	0.00	-10.71	9.14
419	Primo Impalcato	69, 94	0	134.63	-0.74	0.00	0.00	4.29	-3.23
			103	134.63	-0.74	0.00	0.00	7.61	-3.23
			206	134.63	-0.74	0.00	0.00	10.93	-3.23
420	Primo Impalcato	79, 70	0	-193.24	-0.58	0.00	0.00	-1.47	2.06
			102	-193.24	-0.58	0.00	0.00	-3.57	2.06
			204	-193.24	-0.58	0.00	0.00	-5.67	2.06
421	Primo Impalcato	94, 70	0	-135.76	-0.09	0.00	0.00	-5.78	-1.75
			103	-135.76	-0.09	0.00	0.00	-3.98	-1.75
			206	-135.76	-0.09	0.00	0.00	-2.19	-1.75
422	Copertura	1, 2	0	814.12	-60.34	39.56	-53.00	1214.81	429.34
			83	814.54	-60.34	-4.50	-53.00	861.12	421.64
			166	814.97	-60.34	-48.56	-53.00	513.93	413.68
423	Copertura	15, 1	0	294.90	1.97	-439.68	90.09	-111.98	-833.81
			80	294.90	1.97	-368.06	90.09	550.90	-833.81
			159	294.90	1.97	-296.43	90.09	1213.78	-833.81
424	Copertura	2, 3	0	824.64	-50.22	-52.03	12.15	515.61	322.80
			69	824.64	-50.22	-43.65	12.15	294.96	316.76
			138	824.64	-50.22	-35.27	12.15	78.49	310.71
425	Copertura	3, 4	0	824.61	-71.86	-35.35	15.90	80.89	242.33
			69	824.61	-71.86	-24.38	15.90	-84.24	236.29
			138	824.61	-71.86	-13.41	15.90	-245.19	230.25
426	Copertura	4, 5	0	824.57	-74.76	-13.49	18.64	-242.46	168.74
			69	824.57	-74.76	-0.63	18.64	-356.80	162.70
			138	824.57	-74.76	12.23	18.64	-466.98	156.65
427	Copertura	5, 6	0	824.55	-58.29	12.19	15.86	-464.68	107.20
			69	824.55	-58.29	23.14	15.86	-536.56	101.16
			138	824.55	-58.29	34.08	15.86	-604.27	95.12
428	Copertura	6, 7	0	824.54	-28.76	34.12	10.03	-601.47	54.38
			69	824.54	-28.76	41.04	10.03	-636.90	48.34
			138	824.54	-28.76	47.96	10.03	-668.17	42.30
429	Copertura	7, 8	0	826.91	4.29	48.09	-7.56	-668.38	5.97
			69	826.91	4.29	42.87	-7.56	-670.42	-0.07
			138	826.91	4.29	37.66	-7.56	-668.29	-6.11
430	Copertura	8, 9	0	827.02	35.54	37.90	-15.78	-668.94	-43.48
			69	827.02	35.54	27.01	-15.78	-636.85	-49.52
			138	827.02	35.54	16.13	-15.78	-600.60	-55.56
431	Copertura	9, 10	0	830.94	63.43	16.42	-4.69	-602.22	-96.40
			69	830.94	63.43	13.18	-4.69	-533.62	-102.45
			138	830.94	63.43	9.94	-4.69	-460.84	-108.49
432	Copertura	10, 11	0	836.92	81.87	10.30	-34.71	-465.01	-159.42
			69	836.92	81.87	-13.65	-34.71	-352.93	-165.46

			138	836.92	81.87	-37.60	-34.71	-236.68	-171.50
433	Copertura	11, 12	0	837.11	78.52	-37.19	-33.80	-239.63	-234.26
			69	837.11	78.52	-60.51	-33.80	-75.91	-240.30
			138	837.11	78.52	-83.83	-33.80	91.98	-246.34
434	Copertura	12, 13	0	837.29	52.73	-83.44	-22.43	89.31	-318.16
			69	837.29	52.73	-98.92	-22.43	310.93	-324.20
			138	837.29	52.73	-114.39	-22.43	536.71	-330.25
435	Copertura	13, 14	0	827.35	34.25	-112.14	73.17	534.41	-436.70
			83	826.92	34.25	-51.31	73.17	900.73	-444.66
			166	826.50	34.25	9.51	73.17	1273.56	-452.36
436	Copertura	16, 14	0	335.15	-2.46	-340.23	112.10	94.05	854.63
			80	335.15	-2.46	-251.11	112.10	-585.38	854.63
			159	335.15	-2.46	-161.99	112.10	-1264.81	854.63
437	Copertura	15, 17	0	245.59	-4.31	-547.32	181.27	114.59	52.39
			66	245.59	-4.31	-427.68	181.27	80.02	52.39
			132	245.59	-4.31	-308.04	181.27	45.44	52.39
438	Copertura	16, 18	0	303.39	4.07	-394.20	115.56	-83.75	-34.33
			66	303.39	4.07	-317.93	115.56	-61.09	-34.33
			132	303.39	4.07	-241.66	115.56	-38.44	-34.33
439	Copertura	17, 19	0	196.29	-2.06	-416.12	154.95	51.64	43.16
			66	196.29	-2.06	-313.85	154.95	23.15	43.16
			132	196.29	-2.06	-211.59	154.95	-5.33	43.16
440	Copertura	18, 20	0	246.77	1.98	-317.65	71.49	-31.92	-27.16
			66	246.77	1.98	-270.46	71.49	-14.00	-27.16
			132	246.77	1.98	-223.28	71.49	3.93	-27.16
441	Copertura	19, 21	0	146.37	-0.33	-320.94	221.23	1.65	4.90
			66	146.37	-0.33	-174.93	221.23	-1.59	4.90
			132	146.37	-0.33	-28.91	221.23	-4.82	4.90
442	Copertura	20, 22	0	191.99	0.32	-298.81	186.84	10.37	9.51
			66	191.99	0.32	-175.50	186.84	4.09	9.51
			132	191.99	0.32	-52.19	186.84	-2.19	9.51
443	Copertura	21, 23	0	96.21	0.32	-138.84	112.59	2.07	5.16
			66	96.21	0.32	-64.54	112.59	-1.34	5.16
			132	96.21	0.32	9.77	112.59	-4.74	5.16
444	Copertura	22, 24	0	134.01	-0.38	-130.84	62.59	4.75	7.47
			66	134.01	-0.38	-89.53	62.59	-0.19	7.47
			132	134.01	-0.38	-48.22	62.59	-5.12	7.47
445	Copertura	23, 25	0	45.97	-0.06	-100.36	132.09	2.07	12.87
			66	45.97	-0.06	-13.18	132.09	-6.42	12.87
			132	45.97	-0.06	74.00	132.09	-14.92	12.87
446	Copertura	24, 26	0	76.19	0.10	-126.97	146.22	1.76	-1.79
			66	76.19	0.10	-30.46	146.22	2.94	-1.79
			132	76.19	0.10	66.04	146.22	4.13	-1.79
447	Copertura	25, 28	0	-4.22	0.22	-36.07	-2.52	-8.45	-6.82
			85	-4.22	0.22	-38.22	-2.52	-2.66	-6.82
			170	-4.22	0.22	-40.37	-2.52	3.14	-6.82
448	Copertura	26, 27	0	18.06	-0.46	-12.96	21.93	10.90	15.37
			66	18.06	-0.46	1.51	21.93	0.76	15.37
			132	18.06	-0.46	15.99	21.93	-9.38	15.37
449	Copertura	27, 29	0	-40.02	0.14	-63.28	118.18	-2.66	1.97
			66	-40.02	0.14	14.72	118.18	-3.96	1.97
			132	-40.02	0.14	92.71	118.18	-5.26	1.97
450	Copertura	28, 30	0	-54.43	-0.09	-150.16	97.71	9.38	6.71
			73	-54.43	-0.09	-78.83	97.71	4.49	6.71
			146	-54.43	-0.09	-7.50	97.71	-0.41	6.71
451	Copertura	29, 31	0	-97.73	-0.07	14.05	5.36	1.39	2.24
			66	-97.73	-0.07	17.58	5.36	-0.09	2.24
			132	-97.73	-0.07	21.12	5.36	-1.56	2.24
452	Copertura	30, 32	0	-104.97	0.02	-118.30	109.31	6.08	6.39
			69	-104.97	0.02	-43.42	109.31	1.70	6.39
			137	-104.97	0.02	31.45	109.31	-2.68	6.39
453	Copertura	31, 33	0	-156.24	0.15	-58.10	106.51	5.14	5.30
			66	-156.24	0.15	12.20	106.51	1.64	5.30
			132	-156.24	0.15	82.49	106.51	-1.86	5.30
454	Copertura	32, 34	0	-155.24	-0.07	-79.03	92.97	3.92	4.35
			69	-155.24	-0.07	-14.88	92.97	0.92	4.35
			138	-155.24	-0.07	49.27	92.97	-2.08	4.35
455	Copertura	33, 35	0	-210.69	-0.14	6.09	-4.11	5.01	5.45
			66	-210.69	-0.14	3.38	-4.11	1.41	5.45
			132	-210.69	-0.14	0.67	-4.11	-2.19	5.45
456	Copertura	34, 36	0	-205.61	0.07	-61.21	86.65	4.64	4.96
			69	-205.61	0.07	-1.42	86.65	1.22	4.96

			138	-205.61	0.07	58.37	86.65	-2.20	4.96
457	Copertura	35, 37	0	-272.40	0.15	-81.72	99.98	4.77	5.96
			66	-272.40	0.15	-15.74	99.98	0.83	5.96
			132	-272.40	0.15	50.25	99.98	-3.10	5.96
458	Copertura	36, 38	0	-256.02	-0.08	-52.09	94.06	4.65	6.81
			69	-256.02	-0.08	12.81	94.06	-0.05	6.81
			138	-256.02	-0.08	77.71	94.06	-4.75	6.81
459	Copertura	37, 39	0	-329.81	-0.19	-28.03	-10.28	3.94	9.46
			66	-329.81	-0.19	-34.81	-10.28	-2.30	9.46
			132	-329.81	-0.19	-41.60	-10.28	-8.54	9.46
460	Copertura	38, 40	0	-306.32	0.03	-32.76	114.00	2.12	5.29
			69	-306.32	0.03	45.33	114.00	-1.50	5.29
			137	-306.32	0.03	123.42	114.00	-5.13	5.29
461	Copertura	39, 41	0	-389.49	0.08	-121.23	128.87	-1.72	28.77
			66	-389.49	0.08	-36.18	128.87	-20.71	28.77
			132	-389.49	0.08	48.88	128.87	-39.70	28.77
462	Copertura	40, 42	0	-356.13	-0.27	12.81	119.35	1.57	-9.92
			69	-356.13	-0.27	95.17	119.35	8.42	-9.92
			138	-356.13	-0.27	177.52	119.35	15.26	-9.92
463	Copertura	41, 44	0	-442.97	0.67	-29.27	86.80	-33.74	-52.34
			66	-442.97	0.67	28.02	86.80	0.80	-52.34
			132	-442.97	0.67	85.31	86.80	35.35	-52.34
464	Copertura	42, 43	0	-410.42	1.06	67.32	40.17	21.94	78.91
			23	-410.42	1.06	76.56	40.17	3.79	78.91
			46	-410.42	1.06	85.80	40.17	-14.36	78.91
465	Copertura	43, 45	0	-460.05	-0.03	-23.30	31.42	-7.55	-6.55
			66	-460.05	-0.03	-2.57	31.42	-3.23	-6.55
			132	-460.05	-0.03	18.17	31.42	1.10	-6.55
466	Copertura	44, 46	0	-501.10	-0.24	6.97	41.33	41.39	27.01
			66	-501.10	-0.24	34.25	41.33	23.56	27.01
			132	-501.10	-0.24	61.53	41.33	5.73	27.01
467	Copertura	45, 47	0	-510.18	-0.02	-91.54	159.67	8.39	6.71
			66	-510.18	-0.02	13.85	159.67	3.96	6.71
			132	-510.18	-0.02	119.23	159.67	-0.47	6.71
468	Copertura	46, 48	0	-557.00	-0.24	-14.89	78.52	13.07	11.32
			66	-557.00	-0.24	36.93	78.52	5.60	11.32
			132	-557.00	-0.24	88.76	78.52	-1.87	11.32
469	Copertura	47, 49	0	-560.22	0.43	9.71	130.42	7.23	6.41
			66	-560.22	0.43	95.79	130.42	3.00	6.41
			132	-560.22	0.43	181.87	130.42	-1.23	6.41
470	Copertura	48, 50	0	-614.30	-0.61	11.34	83.96	6.02	10.90
			66	-614.30	-0.61	66.75	83.96	-1.18	10.90
			132	-614.30	-0.61	122.16	83.96	-8.37	10.90
471	Copertura	49, 51	0	-610.20	-0.56	72.61	247.63	6.62	4.31
			66	-610.20	-0.56	236.04	247.63	3.77	4.31
			132	-610.20	-0.56	399.47	247.63	0.93	4.31
472	Copertura	50, 52	0	-669.56	0.40	46.49	164.63	-0.47	13.08
			66	-669.56	0.40	155.15	164.63	-9.10	13.08
			132	-669.56	0.40	263.80	164.63	-17.73	13.08
473	Copertura	51, 53	0	-659.82	-4.19	291.00	166.06	8.94	82.13
			66	-659.82	-4.19	400.60	166.06	-45.27	82.13
			132	-659.82	-4.19	510.20	166.06	-99.48	82.13
474	Copertura	52, 54	0	-726.14	4.24	187.55	222.87	-10.63	-64.21
			66	-726.14	4.24	334.64	222.87	31.75	-64.21
			132	-726.14	4.24	481.74	222.87	74.13	-64.21
475	Copertura	53, 55	0	-708.63	-7.19	403.40	167.03	-92.85	100.27
			66	-708.63	-7.19	513.64	167.03	-159.03	100.27
			132	-708.63	-7.19	623.88	167.03	-225.20	100.27
476	Copertura	54, 56	0	-773.12	6.51	414.67	55.80	80.38	-84.67
			66	-773.12	6.51	451.50	55.80	136.27	-84.67
			132	-773.12	6.51	488.33	55.80	192.15	-84.67
477	Copertura	55, 57	0	-757.21	5.65	517.90	-155.20	-225.32	-1746.13
			80	-757.21	5.65	394.51	-155.20	1162.86	-1746.13
			159	-757.21	5.65	271.13	-155.20	2551.03	-1746.13
478	Copertura	56, 70	0	-826.74	-6.26	418.00	-187.11	204.58	1766.85
			80	-826.74	-6.26	269.25	-187.11	-1200.07	1766.85
			159	-826.74	-6.26	120.49	-187.11	-2604.72	1766.85
479	Copertura	57, 58	0	-1682.60	-66.24	-15.01	106.66	2552.50	911.24
			83	-1683.43	-66.24	73.65	106.66	1801.42	895.84
			166	-1684.30	-66.24	162.31	106.66	1063.36	879.91
480	Copertura	58, 59	0	-1703.86	-100.86	166.73	-63.74	1067.65	668.08
			69	-1703.86	-100.86	122.75	-63.74	610.84	656.00

			138	-1703.86	-100.86	78.77	-63.74	162.37	643.91
481	Copertura	59, 60	0	-1703.58	-152.09	79.36	-61.47	167.58	499.70
			69	-1703.58	-152.09	36.94	-61.47	-173.05	487.62
			138	-1703.58	-152.09	-5.47	-61.47	-505.34	475.53
482	Copertura	60, 61	0	-1703.35	-158.04	-4.95	-51.37	-499.57	348.88
			69	-1703.35	-158.04	-40.39	-51.37	-736.13	336.80
			138	-1703.35	-158.04	-75.84	-51.37	-964.35	324.71
483	Copertura	61, 62	0	-1697.35	-119.40	-75.48	-13.92	-956.26	221.57
			69	-1697.35	-119.40	-85.08	-13.92	-1104.98	209.49
			138	-1697.35	-119.40	-94.68	-13.92	-1245.36	197.40
484	Copertura	62, 63	0	-1695.71	-61.01	-94.53	-10.25	-1242.52	113.84
			69	-1695.71	-61.01	-101.60	-10.25	-1316.91	101.76
			138	-1695.71	-61.01	-108.68	-10.25	-1382.95	89.67
485	Copertura	63, 64	0	-1695.72	3.72	-108.72	3.99	-1381.99	11.91
			69	-1695.72	3.72	-105.97	3.99	-1386.04	-0.17
			138	-1695.72	3.72	-103.22	3.99	-1381.75	-12.26
486	Copertura	64, 65	0	-1695.86	68.30	-103.52	16.41	-1382.94	-90.38
			69	-1695.86	68.30	-92.20	16.41	-1316.41	-102.46
			138	-1695.86	68.30	-80.88	16.41	-1241.55	-114.55
487	Copertura	65, 66	0	-1701.90	126.16	-81.34	1.30	-1244.70	-199.05
			69	-1701.90	126.16	-80.44	1.30	-1103.19	-211.14
			138	-1701.90	126.16	-79.55	1.30	-953.33	-223.22
488	Copertura	66, 67	0	-1712.55	164.39	-80.20	61.78	-961.71	-327.77
			69	-1712.55	164.39	-37.58	61.78	-731.38	-339.86
			138	-1712.55	164.39	5.05	61.78	-492.71	-351.94
489	Copertura	67, 68	0	-1712.94	158.09	4.21	76.54	-498.68	-480.06
			69	-1712.94	158.09	57.02	76.54	-163.27	-492.15
			138	-1712.94	158.09	109.83	76.54	180.48	-504.23
490	Copertura	68, 69	0	-1713.36	103.14	108.94	77.02	175.02	-651.67
			69	-1713.36	103.14	162.08	77.02	628.84	-663.75
			138	-1713.36	103.14	215.22	77.02	1091.00	-675.84
491	Copertura	69, 70	0	-1693.27	40.43	211.96	-117.17	1086.11	-902.35
			83	-1692.41	40.43	114.56	-117.17	1842.82	-918.27
			166	-1691.57	40.43	17.16	-117.17	2612.54	-933.68
492	Copertura	1	0	105.88	-0.93	227.40	-84.94	-37.84	-16.18
			220	105.88	-0.93	20.52	-106.92	-2.24	-16.18
			440	105.88	-0.93	-259.72	-151.63	33.35	-16.18
493	Copertura	2	0	-35.16	1.05	8.21	45.50	0.24	0.14
			220	-35.16	1.05	69.27	2.61	-0.08	0.14
			440	-35.16	1.05	-12.84	-84.65	-0.40	0.14
494	Copertura	3	0	-3.75	2.40	-21.65	68.38	0.08	0.04
			220	-3.75	2.40	90.73	26.56	0.00	0.04
			440	-3.75	2.40	63.51	-58.52	-0.08	0.04
495	Copertura	4	0	-2.74	2.74	-2.89	61.51	0.08	0.04
			220	-2.74	2.74	94.36	19.69	0.00	0.04
			440	-2.74	2.74	52.01	-65.39	-0.08	0.04
496	Copertura	5	0	2.78	2.30	16.47	49.46	0.04	0.02
			220	2.78	2.30	87.20	7.64	0.00	0.02
			440	2.78	2.30	18.34	-77.45	-0.05	0.02
497	Copertura	6	0	5.76	1.45	26.11	41.16	-0.03	-0.01
			220	5.76	1.45	78.60	-0.66	0.00	-0.01
			440	5.76	1.45	-8.51	-85.74	0.03	-0.01
498	Copertura	7	0	10.23	0.41	31.18	36.84	-0.13	-0.06
			220	10.23	0.41	74.16	-4.98	0.00	-0.06
			440	10.23	0.41	-22.46	-90.06	0.12	-0.06
499	Copertura	8	0	8.22	-0.65	31.24	37.37	-0.24	-0.11
			220	8.22	-0.65	75.38	-4.45	0.01	-0.11
			440	8.22	-0.65	-20.08	-89.54	0.26	-0.11
500	Copertura	9	0	0.97	-1.65	27.29	41.22	-0.29	-0.13
			220	0.97	-1.65	79.89	-0.60	0.00	-0.13
			440	0.97	-1.65	-7.10	-85.69	0.29	-0.13
501	Copertura	10	0	11.47	-2.51	14.46	51.06	-0.36	-0.16
			220	11.47	-2.51	88.71	9.24	0.00	-0.16
			440	11.47	-2.51	23.38	-75.85	0.36	-0.16
502	Copertura	11	0	-0.92	-2.95	-3.34	62.76	-0.41	-0.19
			220	-0.92	-2.95	96.65	20.94	0.01	-0.19
			440	-0.92	-2.95	57.06	-64.14	0.44	-0.19
503	Copertura	12	0	-11.37	-2.67	-25.79	71.82	-0.39	-0.18
			220	-11.37	-2.67	94.15	30.00	0.01	-0.18
			440	-11.37	-2.67	74.49	-55.08	0.41	-0.18
504	Copertura	13	0	-63.32	-1.48	-23.35	60.97	-0.50	-0.27
			220	-63.32	-1.48	71.75	18.08	0.10	-0.27

			440	-63.32	-1.48	23.69	-69.17	0.70	-0.27
505	Copertura	57	0	-191.63	0.88	200.20	-57.59	16.84	9.68
			220	-191.63	0.88	33.48	-101.55	-4.46	9.68
			440	-191.63	0.88	-279.98	-191.00	-25.76	9.68
506	Copertura	58	0	104.15	2.76	-41.26	119.26	-0.95	-0.53
			220	104.15	2.76	143.01	33.47	0.22	-0.53
			440	104.15	2.76	40.93	-141.06	1.40	-0.53
507	Copertura	59	0	-2.27	5.20	-51.22	144.21	-0.59	-0.27
			220	-2.27	5.20	189.88	60.56	0.02	-0.27
			440	-2.27	5.20	151.77	-109.63	0.62	-0.27
508	Copertura	60	0	-10.10	5.77	-5.95	126.65	-0.52	-0.24
			220	-10.10	5.77	196.53	43.00	0.01	-0.24
			440	-10.10	5.77	119.79	-127.18	0.53	-0.24
509	Copertura	61	0	-18.86	4.83	30.80	103.36	-0.36	-0.16
			220	-18.86	4.83	182.03	19.71	0.00	-0.16
			440	-18.86	4.83	54.05	-150.48	0.35	-0.16
510	Copertura	62	0	-8.70	3.04	56.83	84.31	-0.15	-0.07
			220	-8.70	3.04	166.16	0.66	0.00	-0.07
			440	-8.70	3.04	-3.72	-169.52	0.14	-0.07
511	Copertura	63	0	-14.24	0.96	64.73	77.76	0.04	0.02
			220	-14.24	0.96	159.66	-5.89	0.01	0.02
			440	-14.24	0.96	-24.64	-176.07	-0.03	0.02
512	Copertura	64	0	-12.42	-1.19	64.57	78.12	0.30	0.14
			220	-12.42	-1.19	160.28	-5.53	-0.01	0.14
			440	-12.42	-1.19	-23.23	-175.72	-0.32	0.14
513	Copertura	65	0	-3.49	-3.26	56.52	85.22	0.46	0.20
			220	-3.49	-3.26	167.86	1.57	0.01	0.20
			440	-3.49	-3.26	-0.02	-168.61	-0.44	0.20
514	Copertura	66	0	-27.46	-5.04	30.21	104.74	0.66	0.30
			220	-27.46	-5.04	184.48	21.09	0.01	0.30
			440	-27.46	-5.04	59.53	-149.10	-0.64	0.30
515	Copertura	67	0	-14.76	-5.97	-6.31	128.12	0.84	0.39
			220	-14.76	-5.97	199.42	44.47	-0.01	0.39
			440	-14.76	-5.97	125.92	-125.71	-0.86	0.39
516	Copertura	68	0	-0.48	-5.46	-54.94	147.43	0.90	0.42
			220	-0.48	-5.46	193.26	63.78	-0.03	0.42
			440	-0.48	-5.46	162.24	-106.40	-0.95	0.42
517	Copertura	69	0	126.44	-3.19	-71.61	134.06	1.24	0.68
			220	126.44	-3.19	145.22	48.27	-0.25	0.68
			440	126.44	-3.19	75.69	-126.27	-1.73	0.68
518	Primo Impalcato	1, 74	0	-32.06	0.23	0.00	0.00	11.69	6.14
			118	-32.06	0.23	0.00	0.00	4.47	6.14
			235	-32.06	0.23	0.00	0.00	-2.75	6.14
519	Copertura	74, 2	0	39.79	0.02	0.00	0.00	3.11	3.37
			118	39.79	0.02	0.00	0.00	-0.85	3.37
			235	39.79	0.02	0.00	0.00	-4.81	3.37
520	Primo Impalcato	6, 71	0	7.72	0.10	0.00	0.00	-0.05	0.29
			115	7.72	0.10	0.00	0.00	-0.39	0.29
			231	7.72	0.10	0.00	0.00	-0.73	0.29
521	Copertura	71, 7	0	0.07	0.14	0.00	0.00	-2.66	-0.65
			115	0.07	0.14	0.00	0.00	-1.92	-0.65
			231	0.07	0.14	0.00	0.00	-1.17	-0.65
522	Primo Impalcato	9, 72	0	19.44	-0.26	0.00	0.00	-2.52	0.64
			115	19.44	-0.26	0.00	0.00	-3.26	0.64
			231	19.44	-0.26	0.00	0.00	-4.00	0.64
523	Copertura	72, 10	0	-12.63	-0.26	0.00	0.00	0.34	0.14
			115	-12.63	-0.26	0.00	0.00	0.18	0.14
			231	-12.63	-0.26	0.00	0.00	0.02	0.14
524	Copertura	73, 13	0	35.26	-0.04	0.00	0.00	-1.39	-2.96
			118	35.26	-0.04	0.00	0.00	2.08	-2.96
			235	35.26	-0.04	0.00	0.00	5.56	-2.96
525	Primo Impalcato	14, 73	0	-34.50	-0.34	0.00	0.00	-7.00	-3.36
			118	-34.50	-0.34	0.00	0.00	-3.05	-3.36
			235	-34.50	-0.34	0.00	0.00	0.90	-3.36
526	Primo Impalcato	57, 75	0	70.82	0.65	0.00	0.00	14.56	7.13
			118	70.82	0.65	0.00	0.00	6.18	7.13
			235	70.82	0.65	0.00	0.00	-2.21	7.13
527	Copertura	75, 58	0	-75.07	0.06	0.00	0.00	3.22	6.00

			118	-75.07	0.06	0.00	0.00	-3.84	6.00
			235	-75.07	0.06	0.00	0.00	-10.91	6.00
528	Copertura	77, 61	0	5.28	0.50	0.00	0.00	-0.31	-0.25
			115	5.28	0.50	0.00	0.00	-0.02	-0.25
			231	5.28	0.50	0.00	0.00	0.27	-0.25
529	Primo Impalcato	62, 77	0	-19.49	0.50	0.00	0.00	5.13	-1.22
			115	-19.49	0.50	0.00	0.00	6.53	-1.22
			231	-19.49	0.50	0.00	0.00	7.94	-1.22
530	Primo Impalcato	65, 78	0	-34.61	-0.53	0.00	0.00	-5.41	1.21
			115	-34.61	-0.53	0.00	0.00	-6.81	1.21
			231	-34.61	-0.53	0.00	0.00	-8.20	1.21
531	Copertura	78, 66	0	19.49	-0.53	0.00	0.00	0.48	0.31
			115	19.49	-0.53	0.00	0.00	0.12	0.31
			231	19.49	-0.53	0.00	0.00	-0.23	0.31
532	Primo Impalcato	69, 76	0	-74.56	-0.08	0.00	0.00	-11.64	-5.61
			118	-74.56	-0.08	0.00	0.00	-5.04	-5.61
			235	-74.56	-0.08	0.00	0.00	1.56	-5.61
533	Copertura	76, 70	0	72.42	-0.77	0.00	0.00	-0.32	-4.46
			118	72.42	-0.77	0.00	0.00	4.92	-4.46
			235	72.42	-0.77	0.00	0.00	10.17	-4.46
534	Copertura	1, 74	0	39.79	-0.51	0.00	0.00	-6.92	-4.04
			118	39.79	-0.51	0.00	0.00	-2.16	-4.04
			235	39.79	-0.51	0.00	0.00	2.59	-4.04
535	Copertura	74, 2	0	-32.06	0.29	0.00	0.00	-2.01	-1.27
			118	-32.06	0.29	0.00	0.00	-0.52	-1.27
			235	-32.06	0.29	0.00	0.00	0.98	-1.27
536	Copertura	6, 71	0	0.07	0.27	0.00	0.00	-3.67	-0.43
			115	0.07	0.27	0.00	0.00	-3.18	-0.43
			231	0.07	0.27	0.00	0.00	-2.69	-0.43
537	Copertura	71, 7	0	7.72	-0.03	0.00	0.00	-0.78	0.52
			115	7.72	-0.03	0.00	0.00	-1.38	0.52
			231	7.72	-0.03	0.00	0.00	-1.97	0.52
538	Copertura	9, 72	0	-12.63	-0.16	0.00	0.00	-0.59	-0.37
			115	-12.63	-0.16	0.00	0.00	-0.16	-0.37
			231	-12.63	-0.16	0.00	0.00	0.27	-0.37
539	Copertura	72, 10	0	19.44	-0.39	0.00	0.00	-4.00	0.13
			115	19.44	-0.39	0.00	0.00	-4.15	0.13
			231	19.44	-0.39	0.00	0.00	-4.29	0.13
540	Copertura	73, 13	0	-34.50	-0.32	0.00	0.00	0.21	0.71
			118	-34.50	-0.32	0.00	0.00	-0.63	0.71
			235	-34.50	-0.32	0.00	0.00	-1.47	0.71
541	Copertura	14, 73	0	35.26	0.41	0.00	0.00	1.76	1.11
			118	35.26	0.41	0.00	0.00	0.45	1.11
			235	35.26	0.41	0.00	0.00	-0.86	1.11
542	Copertura	15, 125	0	-854.09	-4.37	27.57	-50.78	-1.40	-1.97
			75	-854.09	-4.37	-10.52	-50.78	0.08	-1.97
			150	-854.09	-4.37	-48.61	-50.78	1.56	-1.97
543	Copertura	127, 16	0	-865.55	1.69	-36.82	41.69	8.08	-1.04
			75	-865.55	1.69	-5.55	41.69	8.86	-1.04
			150	-865.55	1.69	25.71	41.69	9.65	-1.04
544	Copertura	17, 129	0	12.18	-4.60	-3.54	-8.76	-4.76	-2.27
			75	12.18	-4.60	-10.11	-8.76	-3.05	-2.27
			150	12.18	-4.60	-16.68	-8.76	-1.34	-2.27
545	Copertura	130, 18	0	4.60	2.80	-8.63	2.81	7.87	0.74
			75	4.60	2.80	-6.52	2.81	7.31	0.74
			150	4.60	2.80	-4.42	2.81	6.75	0.74
546	Copertura	19, 135	0	41.01	-4.63	-0.01	-2.13	-5.62	-2.21
			75	41.01	-4.63	-1.61	-2.13	-3.97	-2.21
			150	41.01	-4.63	-3.21	-2.13	-2.31	-2.21
547	Copertura	134, 20	0	36.30	2.80	3.02	-1.34	7.63	0.63
			75	36.30	2.80	2.01	-1.34	7.16	0.63
			150	36.30	2.80	1.01	-1.34	6.69	0.63
548	Copertura	21, 136	0	-1.30	-4.64	-3.34	1.83	-5.57	-2.17
			75	-1.30	-4.64	-1.97	1.83	-3.95	-2.17
			150	-1.30	-4.64	-0.60	1.83	-2.32	-2.17
549	Copertura	138, 22	0	-8.05	2.84	6.44	-7.16	7.84	0.53
			75	-8.05	2.84	1.07	-7.16	7.44	0.53
			150	-8.05	2.84	-4.30	-7.16	7.04	0.53
550	Copertura	23, 141	0	-4.95	-4.64	1.28	-2.92	-5.49	-2.17
			75	-4.95	-4.64	-0.91	-2.92	-3.86	-2.17

			150	-4.95	-4.64	-3.11	-2.92	-2.24	-2.17
551	Copertura	142, 24	0	-8.72	2.85	2.45	0.26	7.80	0.54
			75	-8.72	2.85	2.65	0.26	7.39	0.54
			150	-8.72	2.85	2.84	0.26	6.99	0.54
552	Copertura	25, 145	0	18.17	-4.63	-4.30	1.07	-5.16	-2.13
			75	18.17	-4.63	-3.50	1.07	-3.56	-2.13
			150	18.17	-4.63	-2.70	1.07	-1.97	-2.13
553	Copertura	146, 26	0	11.23	2.87	5.04	-6.42	7.84	0.61
			75	11.23	2.87	0.23	-6.42	7.38	0.61
			150	11.23	2.87	-4.59	-6.42	6.92	0.61
554	Copertura	150, 27	0	-1.32	2.87	-3.37	11.70	7.80	0.62
			75	-1.32	2.87	5.40	11.70	7.33	0.62
			150	-1.32	2.87	14.18	11.70	6.86	0.62
555	Copertura	28, 149	0	-23.79	-4.60	-13.93	8.74	-4.95	-2.09
			75	-23.79	-4.60	-7.37	8.74	-3.38	-2.09
			150	-23.79	-4.60	-0.82	8.74	-1.82	-2.09
556	Copertura	154, 29	0	10.00	2.85	-2.09	8.79	7.67	0.59
			75	10.00	2.85	4.50	8.79	7.23	0.59
			150	10.00	2.85	11.09	8.79	6.79	0.59
557	Copertura	30, 153	0	-18.22	-4.64	-23.72	16.71	-5.16	-2.13
			75	-18.22	-4.64	-11.18	16.71	-3.56	-2.13
			150	-18.22	-4.64	1.35	16.71	-1.97	-2.13
558	Copertura	158, 31	0	20.51	2.85	-5.45	16.37	7.72	0.59
			75	20.51	2.85	6.83	16.37	7.28	0.59
			150	20.51	2.85	19.10	16.37	6.83	0.59
559	Copertura	32, 157	0	-19.76	-4.64	-26.64	19.89	-5.27	-2.13
			75	-19.76	-4.64	-11.73	19.89	-3.67	-2.13
			150	-19.76	-4.64	3.19	19.89	-2.07	-2.13
560	Copertura	162, 33	0	13.05	2.78	-3.51	11.63	7.75	0.48
			75	13.05	2.78	5.21	11.63	7.39	0.48
			150	13.05	2.78	13.93	11.63	7.03	0.48
561	Copertura	34, 161	0	-24.56	-4.63	-29.24	22.09	-5.39	-2.15
			75	-24.56	-4.63	-12.67	22.09	-3.78	-2.15
			150	-24.56	-4.63	3.90	22.09	-2.17	-2.15
562	Copertura	166, 35	0	22.77	2.93	-8.09	20.98	8.03	0.64
			75	22.77	2.93	7.64	20.98	7.55	0.64
			150	22.77	2.93	23.38	20.98	7.07	0.64
563	Copertura	36, 165	0	-28.68	-4.64	-31.37	24.84	-5.51	-2.15
			75	-28.68	-4.64	-12.74	24.84	-3.89	-2.15
			150	-28.68	-4.64	5.89	24.84	-2.28	-2.15
564	Copertura	170, 37	0	20.84	2.81	-6.16	15.79	7.95	0.51
			75	20.84	2.81	5.68	15.79	7.56	0.51
			150	20.84	2.81	17.52	15.79	7.17	0.51
565	Copertura	38, 169	0	-27.66	-4.62	-34.04	27.20	-5.54	-2.16
			75	-27.66	-4.62	-13.64	27.20	-3.92	-2.16
			150	-27.66	-4.62	6.76	27.20	-2.30	-2.16
566	Copertura	175, 39	0	45.86	2.84	-11.37	25.32	7.81	0.57
			75	45.86	2.84	7.61	25.32	7.38	0.57
			150	45.86	2.84	26.60	25.32	6.95	0.57
567	Copertura	40, 173	0	-17.64	-4.62	-36.74	30.81	-5.36	-2.14
			75	-17.64	-4.62	-13.64	30.81	-3.76	-2.14
			150	-17.64	-4.62	9.46	30.81	-2.16	-2.14
568	Copertura	178, 41	0	-56.24	2.79	-11.73	24.29	6.78	0.50
			75	-56.24	2.79	6.49	24.29	6.41	0.50
			150	-56.24	2.79	24.71	24.29	6.03	0.50
569	Copertura	42, 177	0	-125.69	-4.60	-40.99	36.53	-5.31	-2.12
			75	-125.69	-4.60	-13.59	36.53	-3.72	-2.12
			150	-125.69	-4.60	13.81	36.53	-2.13	-2.12
570	Copertura	43, 181	0	87.42	-4.62	-0.79	-3.55	-5.44	-2.16
			75	87.42	-4.62	-3.46	-3.55	-3.82	-2.16
			150	87.42	-4.62	-6.12	-3.55	-2.20	-2.16
571	Copertura	182, 44	0	73.13	2.82	7.92	-7.74	6.90	0.54
			75	73.13	2.82	2.12	-7.74	6.50	0.54
			150	73.13	2.82	-3.69	-7.74	6.10	0.54
572	Copertura	45, 185	0	-7.12	-4.64	4.22	-6.17	-5.95	-2.24
			75	-7.12	-4.64	-0.41	-6.17	-4.27	-2.24
			150	-7.12	-4.64	-5.03	-6.17	-2.59	-2.24
573	Copertura	186, 46	0	-17.38	2.76	4.36	-2.17	8.10	0.44
			75	-17.38	2.76	2.73	-2.17	7.77	0.44
			150	-17.38	2.76	1.10	-2.17	7.44	0.44
574	Copertura	47, 189	0	0.82	-4.64	-1.12	-0.74	-6.36	-2.27
			75	0.82	-4.64	-1.67	-0.74	-4.66	-2.27

			150	0.82	-4.64	-2.23	-0.74	-2.95	-2.27
575	Copertura	190, 48	0	-1.58	2.76	1.13	-1.00	8.52	0.39
			75	-1.58	2.76	0.38	-1.00	8.23	0.39
			150	-1.58	2.76	-0.36	-1.00	7.94	0.39
576	Copertura	49, 193	0	6.23	-4.62	4.01	-6.01	-6.51	-2.27
			75	6.23	-4.62	-0.49	-6.01	-4.81	-2.27
			150	6.23	-4.62	-5.00	-6.01	-3.10	-2.27
577	Copertura	195, 50	0	4.80	2.71	-4.24	4.72	8.47	0.33
			75	4.80	2.71	-0.70	4.72	8.22	0.33
			150	4.80	2.71	2.84	4.72	7.97	0.33
578	Copertura	51, 197	0	-78.32	-4.63	2.08	-1.01	-6.59	-2.35
			75	-78.32	-4.63	1.32	-1.01	-4.83	-2.35
			150	-78.32	-4.63	0.57	-1.01	-3.07	-2.35
579	Copertura	199, 52	0	-72.18	2.80	-3.05	6.41	8.15	0.57
			75	-72.18	2.80	1.76	6.41	7.72	0.57
			150	-72.18	2.80	6.57	6.41	7.30	0.57
580	Copertura	53, 201	0	-21.45	-4.60	4.54	14.23	-5.06	-2.50
			75	-21.45	-4.60	15.22	14.23	-3.19	-2.50
			150	-21.45	-4.60	25.89	14.23	-1.32	-2.50
581	Copertura	202, 54	0	-26.33	2.77	27.73	-18.61	8.89	1.18
			75	-26.33	2.77	13.77	-18.61	8.01	1.18
			150	-26.33	2.77	-0.18	-18.61	7.13	1.18
582	Copertura	55, 205	0	1790.58	-4.25	-50.96	88.01	1.21	-1.88
			75	1790.58	-4.25	15.05	88.01	2.62	-1.88
			150	1790.58	-4.25	81.06	88.01	4.03	-1.88
583	Copertura	206, 56	0	1802.48	2.24	69.16	-78.62	12.08	0.04
			75	1802.48	2.24	10.20	-78.62	12.05	0.04
			150	1802.48	2.24	-48.76	-78.62	12.02	0.04
584	Copertura	57, 75	0	-75.07	-0.86	0.00	0.00	-3.93	-2.58
			118	-75.07	-0.86	0.00	0.00	-0.90	-2.58
			235	-75.07	-0.86	0.00	0.00	2.14	-2.58
585	Copertura	75, 58	0	70.82	0.63	0.00	0.00	-0.78	-1.46
			118	70.82	0.63	0.00	0.00	0.93	-1.46
			235	70.82	0.63	0.00	0.00	2.64	-1.46
586	Copertura	77, 61	0	-19.49	0.76	0.00	0.00	7.96	-0.22
			115	-19.49	0.76	0.00	0.00	8.21	-0.22
			231	-19.49	0.76	0.00	0.00	8.46	-0.22
587	Copertura	62, 77	0	5.28	0.27	0.00	0.00	1.55	0.75
			115	5.28	0.27	0.00	0.00	0.68	0.75
			231	5.28	0.27	0.00	0.00	-0.18	0.75
588	Copertura	65, 78	0	19.49	-0.30	0.00	0.00	-1.31	-0.72
			115	19.49	-0.30	0.00	0.00	-0.49	-0.72
			231	19.49	-0.30	0.00	0.00	0.34	-0.72
589	Copertura	78, 66	0	-34.61	-0.79	0.00	0.00	-8.22	0.19
			115	-34.61	-0.79	0.00	0.00	-8.44	0.19
			231	-34.61	-0.79	0.00	0.00	-8.65	0.19
590	Copertura	69, 76	0	72.42	-0.66	0.00	0.00	3.07	0.85
			118	72.42	-0.66	0.00	0.00	2.07	0.85
			235	72.42	-0.66	0.00	0.00	1.07	0.85
591	Copertura	76, 70	0	-74.56	0.76	0.00	0.00	0.44	-0.30
			118	-74.56	0.76	0.00	0.00	0.79	-0.30
			235	-74.56	0.76	0.00	0.00	1.15	-0.30
592	Copertura	79, 81	0	42.93	-0.04	-60.87	76.43	13.04	5.92
			80	42.93	-0.04	-0.11	76.43	8.33	5.92
			159	42.93	-0.04	60.65	76.43	3.62	5.92
593	Copertura	80, 82	0	32.05	0.02	-54.59	81.53	1.30	1.83
			66	32.05	0.02	-0.74	81.53	0.09	1.83
			132	32.05	0.02	53.10	81.53	-1.12	1.83
594	Copertura	83, 84	0	3.15	0.00	-50.81	76.98	-0.29	-0.22
			66	3.15	0.00	0.00	76.98	-0.14	-0.22
			132	3.15	0.00	50.80	76.98	0.00	-0.22
595	Copertura	85, 86	0	0.35	0.00	-50.94	77.20	0.00	-0.10
			66	0.35	0.00	0.01	77.20	0.06	-0.10
			132	0.35	0.00	50.96	77.20	0.13	-0.10
596	Copertura	87, 88	0	-1.28	0.00	-51.03	77.29	-0.08	-0.06
			66	-1.28	0.00	-0.02	77.29	-0.04	-0.06
			132	-1.28	0.00	50.99	77.29	0.00	-0.06
597	Copertura	89, 90	0	-5.30	0.00	-51.35	77.86	-0.04	-0.08
			66	-5.30	0.00	0.03	77.86	0.02	-0.08
			132	-5.30	0.00	51.42	77.86	0.07	-0.08
598	Copertura	91, 92	0	-7.18	0.00	-49.83	75.60	-0.03	-0.05
			66	-7.18	0.00	0.06	75.60	0.01	-0.05

			132	-7.18	0.00	49.95	75.60	0.04	-0.05
599	Copertura	93, 94	0	-0.84	0.00	-50.40	76.45	-0.17	0.04
			66	-0.84	0.00	0.06	76.45	-0.20	0.04
			132	-0.84	0.00	50.51	76.45	-0.23	0.04
600	Copertura	95, 96	0	-3.77	0.00	-48.59	73.52	0.26	0.08
			66	-3.77	0.00	-0.07	73.52	0.21	0.08
			132	-3.77	0.00	48.45	73.52	0.15	0.08
601	Copertura	97, 106	0	-7.54	-0.01	-48.24	72.69	-0.06	-0.06
			66	-7.54	-0.01	-0.26	72.69	-0.02	-0.06
			132	-7.54	-0.01	47.71	72.69	0.01	-0.06
602	Copertura	98, 99	0	4.47	0.04	-70.27	107.22	-0.55	-0.23
			66	4.47	0.04	0.50	107.22	-0.40	-0.23
			132	4.47	0.04	71.26	107.22	-0.25	-0.23
603	Copertura	100, 101	0	0.59	0.00	-72.98	110.70	-0.14	-0.22
			66	0.59	0.00	0.07	110.70	0.01	-0.22
			132	0.59	0.00	73.13	110.70	0.16	-0.22
604	Copertura	102, 103	0	-0.23	0.00	-73.41	111.21	0.00	-0.03
			66	-0.23	0.00	-0.01	111.21	0.02	-0.03
			132	-0.23	0.00	73.39	111.21	0.03	-0.03
605	Copertura	104, 105	0	-1.14	0.00	-73.22	110.80	-0.13	-0.18
			66	-1.14	0.00	-0.09	110.80	-0.01	-0.18
			132	-1.14	0.00	73.04	110.80	0.11	-0.18
606	Copertura	107, 108	0	-12.72	0.03	-49.42	74.84	1.07	-0.26
			66	-12.72	0.03	-0.03	74.84	1.23	-0.26
			132	-12.72	0.03	49.37	74.84	1.40	-0.26
607	Copertura	109, 110	0	-66.86	0.07	-44.14	56.27	-6.36	13.98
			80	-66.86	0.07	0.59	56.27	-17.47	13.98
			159	-66.86	0.07	45.32	56.27	-28.59	13.98
608	Copertura	111, 112	0	-11.92	0.00	-73.11	110.53	-0.10	-0.15
			66	-11.92	0.00	-0.10	110.53	0.00	-0.15
			132	-11.92	0.00	72.91	110.53	0.10	-0.15
609	Copertura	113, 114	0	-2.06	0.00	-72.94	110.31	-0.11	-0.10
			66	-2.06	0.00	-0.13	110.31	-0.04	-0.10
			132	-2.06	0.00	72.67	110.31	0.02	-0.10
610	Copertura	115, 116	0	-2.28	0.01	-73.42	110.85	-0.58	-0.88
			66	-2.28	0.01	-0.26	110.85	0.00	-0.88
			132	-2.28	0.01	72.90	110.85	0.58	-0.88
611	Copertura	117, 118	0	-2.41	-0.01	-72.59	109.69	-0.05	-0.15
			66	-2.41	-0.01	-0.19	109.69	0.04	-0.15
			132	-2.41	-0.01	72.20	109.69	0.14	-0.15
612	Copertura	119, 120	0	-2.46	0.00	-71.59	108.13	-0.11	-0.37
			66	-2.46	0.00	-0.22	108.13	0.13	-0.37
			132	-2.46	0.00	71.14	108.13	0.37	-0.37
613	Copertura	121, 122	0	-14.61	0.10	-67.26	99.70	2.04	2.45
			66	-14.61	0.10	-1.46	99.70	0.43	2.45
			132	-14.61	0.10	64.34	99.70	-1.19	2.45
614	Copertura	124, 125	0	-79.10	1.03	0.30	-0.37	-3.18	1.37
			99	-79.10	1.03	-0.06	-0.37	-4.55	1.37
			198	-79.10	1.03	-0.42	-0.37	-5.91	1.37
615	Copertura	125, 127	0	-914.10	0.27	-49.03	0.74	-2.23	-0.60
			775	-914.10	0.27	-43.26	0.74	2.43	-0.60
			1550	-914.10	0.27	-37.49	0.74	7.09	-0.60
616	Copertura	126, 127	0	-63.50	-0.43	1.02	-0.86	2.56	0.44
			99	-63.50	-0.43	0.17	-0.86	2.12	0.44
			198	-63.50	-0.43	-0.68	-0.86	1.68	0.44
617	Copertura	128, 129	0	-14.00	1.02	-0.39	0.14	-3.02	1.57
			99	-14.00	1.02	-0.25	0.14	-4.58	1.57
			198	-14.00	1.02	-0.12	0.14	-6.13	1.57
618	Copertura	129, 130	0	1.69	0.18	-16.80	0.51	-5.31	-0.71
			775	1.69	0.18	-12.84	0.51	0.16	-0.71
			1550	1.69	0.18	-8.88	0.51	5.64	-0.71
619	Copertura	131, 130	0	-3.70	-0.52	0.08	-0.17	0.52	-1.45
			99	-3.70	-0.52	-0.09	-0.17	1.96	-1.45
			198	-3.70	-0.52	-0.26	-0.17	3.40	-1.45
620	Copertura	132, 135	0	-3.60	1.01	-0.26	0.24	-3.30	1.45
			99	-3.60	1.01	-0.02	0.24	-4.74	1.45
			198	-3.60	1.01	0.23	0.24	-6.17	1.45
621	Copertura	133, 134	0	2.77	-0.53	0.08	0.10	0.64	-1.38
			99	2.77	-0.53	0.17	0.10	2.02	-1.38
			198	2.77	-0.53	0.27	0.10	3.39	-1.38
622	Copertura	135, 134	0	38.46	0.18	-2.99	0.40	-6.31	-0.76
			775	38.46	0.18	0.15	0.40	-0.45	-0.76

			1550	38.46	0.18	3.29	0.40	5.42	-0.76
623	Copertura	137, 136	0	1.97	1.02	-0.01	-0.12	-3.40	1.40
			99	1.97	1.02	-0.12	-0.12	-4.79	1.40
			198	1.97	1.02	-0.24	-0.12	-6.18	1.40
624	Copertura	136, 138	0	0.11	0.18	-0.84	0.45	-6.32	-0.77
			775	0.11	0.18	2.61	0.45	-0.37	-0.77
			1550	0.11	0.18	6.07	0.45	5.59	-0.77
625	Copertura	139, 138	0	11.15	-0.54	0.42	-0.40	0.86	-1.30
			99	11.15	-0.54	0.03	-0.40	2.15	-1.30
			198	11.15	-0.54	-0.37	-0.40	3.45	-1.30
626	Copertura	140, 141	0	-4.85	1.02	-0.20	0.14	-3.40	1.41
			99	-4.85	1.02	-0.06	0.14	-4.79	1.41
			198	-4.85	1.02	0.09	0.14	-6.19	1.41
627	Copertura	141, 142	0	-8.52	0.18	-3.02	0.36	-6.24	-0.76
			775	-8.52	0.18	-0.19	0.36	-0.35	-0.76
			1550	-8.52	0.18	2.63	0.36	5.54	-0.76
628	Copertura	143, 142	0	0.22	-0.54	0.08	0.05	0.87	-1.30
			99	0.22	-0.54	0.13	0.05	2.17	-1.30
			198	0.22	-0.54	0.18	0.05	3.46	-1.30
629	Copertura	144, 145	0	0.77	1.02	-0.10	-0.09	-3.41	1.38
			99	0.77	1.02	-0.19	-0.09	-4.79	1.38
			198	0.77	1.02	-0.29	-0.09	-6.16	1.38
630	Copertura	145, 146	0	18.68	0.18	-2.98	0.50	-5.95	-0.74
			775	18.68	0.18	0.86	0.50	-0.20	-0.74
			1550	18.68	0.18	4.69	0.50	5.56	-0.74
631	Copertura	147, 146	0	10.16	-0.54	0.33	-0.34	0.81	-1.35
			99	10.16	-0.54	-0.01	-0.34	2.15	-1.35
			198	10.16	-0.54	-0.35	-0.34	3.49	-1.35
632	Copertura	148, 149	0	12.98	1.02	0.83	-0.49	-3.41	1.36
			99	12.98	1.02	0.34	-0.49	-4.77	1.36
			198	12.98	1.02	-0.15	-0.49	-6.12	1.36
633	Copertura	149, 150	0	-14.30	0.17	-0.97	-0.13	-5.77	-0.73
			775	-14.30	0.17	-1.98	-0.13	-0.13	-0.73
			1550	-14.30	0.17	-3.00	-0.13	5.51	-0.73
634	Copertura	151, 150	0	-17.55	-0.54	-0.51	0.44	0.81	-1.35
			99	-17.55	-0.54	-0.07	0.44	2.15	-1.35
			198	-17.55	-0.54	0.36	0.44	3.49	-1.35
635	Copertura	152, 153	0	24.75	1.02	1.32	-0.93	-3.40	1.40
			99	24.75	1.02	0.40	-0.93	-4.79	1.40
			198	24.75	1.02	-0.52	-0.93	-6.17	1.40
636	Copertura	153, 154	0	-0.12	0.17	0.83	-0.20	-5.96	-0.73
			775	-0.12	0.17	-0.69	-0.20	-0.27	-0.73
			1551	-0.12	0.17	-2.21	-0.20	5.41	-0.73
637	Copertura	155, 154	0	-13.53	-0.54	-0.43	0.16	0.85	-1.32
			99	-13.53	-0.54	-0.27	0.16	2.15	-1.32
			198	-13.53	-0.54	-0.12	0.16	3.46	-1.32
638	Copertura	156, 157	0	29.83	1.02	1.54	-1.10	-3.39	1.39
			99	29.83	1.02	0.44	-1.10	-4.77	1.39
			198	29.83	1.02	-0.65	-1.10	-6.15	1.39
639	Copertura	157, 158	0	2.06	0.16	2.53	-0.48	-6.05	-0.74
			775	2.06	0.16	-1.22	-0.48	-0.30	-0.74
			1551	2.06	0.16	-4.97	-0.48	5.45	-0.74
640	Copertura	159, 158	0	-24.98	-0.54	-0.82	0.65	0.83	-1.33
			99	-24.98	-0.54	-0.17	0.65	2.15	-1.33
			198	-24.98	-0.54	0.48	0.65	3.48	-1.33
641	Copertura	160, 161	0	32.99	1.02	1.72	-1.22	-3.39	1.39
			99	32.99	1.02	0.51	-1.22	-4.77	1.39
			198	32.99	1.02	-0.70	-1.22	-6.15	1.39
642	Copertura	161, 162	0	-0.43	0.17	3.20	-0.44	-6.15	-0.76
			776	-0.43	0.17	-0.18	-0.44	-0.29	-0.76
			1551	-0.43	0.17	-3.56	-0.44	5.57	-0.76
643	Copertura	163, 162	0	-18.08	-0.54	-0.63	0.29	0.91	-1.23
			99	-18.08	-0.54	-0.34	0.29	2.13	-1.23
			198	-18.08	-0.54	-0.05	0.29	3.35	-1.23
644	Copertura	164, 165	0	37.61	1.02	1.96	-1.36	-3.39	1.38
			99	37.61	1.02	0.61	-1.36	-4.77	1.38
			198	37.61	1.02	-0.75	-1.36	-6.14	1.38
645	Copertura	165, 166	0	-1.15	0.15	5.14	-0.82	-6.25	-0.77
			776	-1.15	0.15	-1.20	-0.82	-0.29	-0.77
			1551	-1.15	0.15	-7.55	-0.82	5.67	-0.77
646	Copertura	167, 166	0	-32.35	-0.55	-1.06	0.81	0.81	-1.41
			99	-32.35	-0.55	-0.26	0.81	2.21	-1.41

			198	-32.35	-0.55	0.54	0.81	3.60	-1.41
647	Copertura	168, 169	0	41.04	1.02	2.14	-1.47	-3.39	1.39
			99	41.04	1.02	0.68	-1.47	-4.77	1.39
			198	41.04	1.02	-0.78	-1.47	-6.14	1.39
648	Copertura	169, 170	0	2.39	0.17	5.98	-0.78	-6.27	-0.77
			776	2.39	0.17	-0.08	-0.78	-0.27	-0.77
			1552	2.39	0.17	-6.15	-0.78	5.72	-0.77
649	Copertura	171, 170	0	-24.79	-0.54	-0.87	0.44	0.85	-1.29
			99	-24.79	-0.54	-0.43	0.44	2.13	-1.29
			198	-24.79	-0.54	0.01	0.44	3.41	-1.29
650	Copertura	172, 173	0	47.05	1.02	2.36	-1.63	-3.38	1.38
			99	47.05	1.02	0.74	-1.63	-4.76	1.38
			198	47.05	1.02	-0.87	-1.63	-6.13	1.38
651	Copertura	173, 175	0	16.85	0.17	8.59	-1.24	-6.13	-0.75
			776	16.85	0.17	-1.03	-1.24	-0.29	-0.75
			1552	16.85	0.17	-10.65	-1.24	5.55	-0.75
652	Copertura	174, 175	0	-39.32	-0.54	-1.39	1.07	0.83	-1.33
			99	-39.32	-0.54	-0.34	1.07	2.15	-1.33
			198	-39.32	-0.54	0.72	1.07	3.46	-1.33
653	Copertura	176, 177	0	55.62	1.02	3.04	-2.20	-3.29	1.43
			99	55.62	1.02	0.86	-2.20	-4.71	1.43
			198	55.62	1.02	-1.32	-2.20	-6.13	1.43
654	Copertura	177, 178	0	-85.10	0.18	12.49	-1.55	-6.10	-0.69
			776	-85.10	0.18	0.46	-1.55	-0.76	-0.69
			1552	-85.10	0.18	-11.58	-1.55	4.57	-0.69
655	Copertura	179, 178	0	-38.74	-0.52	-1.09	0.63	1.03	-1.19
			99	-38.74	-0.52	-0.47	0.63	2.21	-1.19
			198	-38.74	-0.52	0.15	0.63	3.39	-1.19
656	Copertura	180, 181	0	-6.37	1.01	-0.56	0.36	-3.27	1.46
			99	-6.37	1.01	-0.20	0.36	-4.72	1.46
			198	-6.37	1.01	0.16	0.36	-6.16	1.46
657	Copertura	181, 182	0	82.84	0.18	-5.96	0.89	-6.20	-0.70
			775	82.84	0.18	0.94	0.89	-0.77	-0.70
			1550	82.84	0.18	7.84	0.89	4.65	-0.70
658	Copertura	183, 182	0	12.99	-0.52	0.25	-0.17	0.98	-1.24
			99	12.99	-0.52	0.08	-0.17	2.21	-1.24
			198	12.99	-0.52	-0.08	-0.17	3.44	-1.24
659	Copertura	184, 185	0	-9.90	1.01	-0.34	0.35	-3.37	1.43
			99	-9.90	1.01	0.01	0.35	-4.78	1.43
			198	-9.90	1.01	0.36	0.35	-6.20	1.43
660	Copertura	185, 186	0	-14.38	0.18	-4.67	0.58	-6.61	-0.81
			775	-14.38	0.18	-0.14	0.58	-0.34	-0.81
			1550	-14.38	0.18	4.38	0.58	5.94	-0.81
661	Copertura	187, 186	0	4.07	-0.53	0.26	-0.12	0.84	-1.25
			99	4.07	-0.53	0.14	-0.12	2.08	-1.25
			198	4.07	-0.53	0.02	-0.12	3.32	-1.25
662	Copertura	188, 189	0	-1.46	1.01	-0.07	0.01	-3.39	1.41
			99	-1.46	1.01	-0.07	0.01	-4.80	1.41
			198	-1.46	1.01	-0.06	0.01	-6.20	1.41
663	Copertura	189, 190	0	-0.28	0.18	-2.29	0.22	-6.98	-0.86
			775	-0.28	0.18	-0.59	0.22	-0.31	-0.86
			1550	-0.28	0.18	1.11	0.22	6.35	-0.86
664	Copertura	191, 190	0	1.78	-0.53	0.11	-0.07	0.85	-1.25
			99	1.78	-0.53	0.04	-0.07	2.09	-1.25
			198	1.78	-0.53	-0.02	-0.07	3.32	-1.25
665	Copertura	192, 193	0	-8.89	1.00	-0.29	0.30	-3.40	1.40
			99	-8.89	1.00	0.01	0.30	-4.80	1.40
			198	-8.89	1.00	0.32	0.30	-6.19	1.40
666	Copertura	193, 195	0	-0.29	0.19	-4.68	0.04	-7.12	-0.87
			775	-0.29	0.19	-4.36	0.04	-0.38	-0.87
			1550	-0.29	0.19	-4.03	0.04	6.36	-0.87
667	Copertura	194, 195	0	-6.91	-0.53	-0.20	0.21	0.86	-1.20
			99	-6.91	-0.53	0.00	0.21	2.05	-1.20
			198	-6.91	-0.53	0.21	0.21	3.25	-1.20
668	Copertura	196, 197	0	-1.45	1.00	0.14	-0.20	-3.21	1.51
			99	-1.45	1.00	-0.06	-0.20	-4.70	1.51
			198	-1.45	1.00	-0.25	-0.20	-6.20	1.51
669	Copertura	197, 199	0	-79.55	0.19	0.31	-0.21	-7.10	-0.84
			775	-79.55	0.19	-1.29	-0.21	-0.58	-0.84
			1550	-79.55	0.19	-2.89	-0.21	5.95	-0.84
670	Copertura	198, 199	0	-9.90	-0.53	-0.19	0.17	0.57	-1.41
			99	-9.90	-0.53	-0.02	0.17	1.97	-1.41

			198	-9.90	-0.53	0.15	0.17	3.37	-1.41
671	Copertura	200, 201	0	21.38	1.01	0.50	-0.18	-2.74	1.72
			99	21.38	1.01	0.32	-0.18	-4.44	1.72
			198	21.38	1.01	0.14	-0.18	-6.15	1.72
672	Copertura	201, 202	0	-5.42	0.19	26.03	0.09	-5.30	-0.78
			775	-5.42	0.19	26.76	0.09	0.72	-0.78
			1550	-5.42	0.19	27.48	0.09	6.75	-0.78
673	Copertura	203, 202	0	28.06	-0.54	0.61	-0.44	-0.57	-1.95
			99	28.06	-0.54	0.18	-0.44	1.37	-1.95
			198	28.06	-0.54	-0.25	-0.44	3.31	-1.95
674	Copertura	204, 205	0	137.25	1.02	-1.46	1.49	-3.17	1.24
			99	137.25	1.02	0.02	1.49	-4.40	1.24
			198	137.25	1.02	1.50	1.49	-5.62	1.24
675	Copertura	205, 206	0	1895.27	0.21	82.56	-0.75	0.45	-0.65
			775	1895.27	0.21	76.75	-0.75	5.46	-0.65
			1550	1895.27	0.21	70.93	-0.75	10.47	-0.65
676	Copertura	207, 206	0	121.12	-0.48	-2.06	1.93	1.19	-0.69
			99	121.12	-0.48	-0.14	1.93	1.87	-0.69
			198	121.12	-0.48	1.77	1.93	2.55	-0.69
677	Copertura	79	0	75.86	4.52	42.15	-44.74	-4.28	1.61
			125	75.86	4.52	-29.10	-69.26	-6.30	1.61
			250	75.86	4.52	-131.01	-93.78	-8.32	1.61
678	Copertura	124	0	-272.11	-0.53	44.59	-48.71	20.15	27.90
			155	-272.11	-0.53	-30.91	-48.71	-23.10	27.90
			310	-272.11	-0.53	-106.41	-48.71	-66.35	27.90
679	Copertura	80	0	-233.11	-0.02	-13.03	-46.15	35.54	-21.06
			45	-233.11	-0.02	-33.80	-46.15	45.01	-21.06
			90	-233.11	-0.02	-54.57	-46.15	54.49	-21.06
680	Copertura	128	0	25.81	-0.17	45.10	-48.59	5.53	7.53
			155	25.81	-0.17	-30.21	-48.59	-6.14	7.53
			310	25.81	-0.17	-105.53	-48.59	-17.80	7.53
681	Copertura	82	0	19.97	0.39	3.23	-81.99	12.96	-3.42
			43	19.97	0.39	-31.75	-81.99	14.42	-3.42
			85	19.97	0.39	-66.72	-81.99	15.88	-3.42
682	Copertura	132	0	-66.69	-0.47	45.62	-49.16	2.11	-0.19
			155	-66.69	-0.47	-30.58	-49.16	2.41	-0.19
			310	-66.69	-0.47	-106.78	-49.16	2.71	-0.19
683	Copertura	83	0	-84.69	-0.15	-6.93	-56.87	-0.39	1.79
			43	-84.69	-0.15	-31.19	-56.87	-1.15	1.79
			85	-84.69	-0.15	-55.44	-56.87	-1.91	1.79
684	Copertura	137	0	108.20	-0.59	45.89	-49.40	1.35	-0.38
			155	108.20	-0.59	-30.67	-49.40	1.93	-0.38
			310	108.20	-0.59	-107.24	-49.40	2.51	-0.38
685	Copertura	84	0	90.98	0.05	-5.14	-61.30	-0.55	2.15
			43	90.98	0.05	-31.29	-61.30	-1.47	2.15
			85	90.98	0.05	-57.44	-61.30	-2.39	2.15
686	Copertura	140	0	-19.87	-0.57	45.98	-49.48	2.88	0.82
			155	-19.87	-0.57	-30.72	-49.48	1.62	0.82
			310	-19.87	-0.57	-107.42	-49.48	0.35	0.82
687	Copertura	85	0	-49.77	0.03	-6.13	-58.83	0.42	0.62
			43	-49.77	0.03	-31.22	-58.83	0.16	0.62
			85	-49.77	0.03	-56.31	-58.83	-0.11	0.62
688	Copertura	144	0	134.12	-0.60	45.97	-49.45	2.14	1.00
			155	134.12	-0.60	-30.67	-49.45	0.59	1.00
			310	134.12	-0.60	-107.31	-49.45	-0.96	1.00
689	Copertura	86	0	90.77	-0.03	-5.96	-59.44	0.55	1.45
			43	90.77	-0.03	-31.32	-59.44	-0.07	1.45
			85	90.77	-0.03	-56.67	-59.44	-0.69	1.45
690	Copertura	87	0	-62.45	0.00	-5.68	-60.15	-0.63	-0.85
			43	-62.45	0.00	-31.34	-60.15	-0.27	-0.85
			85	-62.45	0.00	-57.00	-60.15	0.09	-0.85
691	Copertura	148	0	-100.10	-0.62	46.00	-49.19	0.10	0.76
			155	-100.10	-0.62	-30.25	-49.19	-1.07	0.76
			310	-100.10	-0.62	-106.49	-49.19	-2.24	0.76
692	Copertura	88	0	79.11	0.01	-6.40	-58.31	-1.28	-0.25
			43	79.11	0.01	-31.27	-58.31	-1.18	-0.25
			85	79.11	0.01	-56.14	-58.31	-1.07	-0.25
693	Copertura	152	0	-11.40	-0.58	46.25	-49.80	-1.78	0.42
			155	-11.40	-0.58	-30.94	-49.80	-2.42	0.42
			310	-11.40	-0.58	-108.13	-49.80	-3.07	0.42
694	Copertura	89	0	-68.70	0.00	-4.43	-63.35	-2.13	-1.09
			43	-68.70	0.00	-31.45	-63.35	-1.67	-1.09

			85	-68.70	0.00	-58.48	-63.35	-1.21	-1.09
695	Copertura	156	0	16.82	-0.56	46.27	-49.59	-3.11	-0.04
			155	16.82	-0.56	-30.60	-49.59	-3.05	-0.04
			310	16.82	-0.56	-107.47	-49.59	-2.98	-0.04
696	Copertura	90	0	77.12	0.00	-7.08	-57.52	-2.22	-0.48
			43	77.12	0.00	-31.61	-57.52	-2.02	-0.48
			85	77.12	0.00	-56.15	-57.52	-1.82	-0.48
697	Copertura	160	0	6.75	-0.56	46.31	-49.59	-3.71	-0.21
			155	6.75	-0.56	-30.56	-49.59	-3.39	-0.21
			310	6.75	-0.56	-107.43	-49.59	-3.07	-0.21
698	Copertura	91	0	-69.59	0.01	-3.92	-62.10	-3.04	-1.73
			43	-69.59	0.01	-30.41	-62.10	-2.30	-1.73
			85	-69.59	0.01	-56.90	-62.10	-1.56	-1.73
699	Copertura	164	0	-6.59	-0.56	46.37	-49.60	-5.27	-0.73
			155	-6.59	-0.56	-30.52	-49.60	-4.13	-0.73
			310	-6.59	-0.56	-107.41	-49.60	-2.99	-0.73
700	Copertura	92	0	74.77	0.01	-8.15	-52.98	-3.34	-1.02
			43	74.77	0.01	-30.75	-52.98	-2.90	-1.02
			85	74.77	0.01	-53.34	-52.98	-2.47	-1.02
701	Copertura	168	0	-19.16	-0.56	46.42	-49.62	-6.07	-0.91
			155	-19.16	-0.56	-30.50	-49.62	-4.66	-0.91
			310	-19.16	-0.56	-107.41	-49.62	-3.26	-0.91
702	Copertura	93	0	-106.52	-0.06	-5.28	-58.47	-3.91	-2.60
			43	-106.52	-0.06	-30.22	-58.47	-2.80	-2.60
			85	-106.52	-0.06	-55.16	-58.47	-1.69	-2.60
703	Copertura	172	0	-4.11	-0.55	46.50	-49.79	-7.98	-1.65
			155	-4.11	-0.55	-30.68	-49.79	-5.42	-1.65
			310	-4.11	-0.55	-107.85	-49.79	-2.86	-1.65
704	Copertura	94	0	6.10	0.01	-7.34	-59.56	-2.24	-2.94
			43	6.10	0.01	-32.74	-59.56	-0.99	-2.94
			85	6.10	0.01	-58.15	-59.56	0.27	-2.94
705	Copertura	176	0	80.74	-0.45	46.53	-49.65	-11.13	-3.85
			155	80.74	-0.45	-30.43	-49.65	-5.16	-3.85
			310	80.74	-0.45	-107.39	-49.65	0.80	-3.85
706	Copertura	180	0	7.86	-0.44	45.67	-48.93	4.98	2.62
			155	7.86	-0.44	-30.17	-48.93	0.92	2.62
			310	7.86	-0.44	-106.01	-48.93	-3.15	2.62
707	Copertura	95	0	83.70	0.03	-5.24	-60.32	-0.82	2.53
			43	83.70	0.03	-30.97	-60.32	-1.90	2.53
			85	83.70	0.03	-56.70	-60.32	-2.98	2.53
708	Copertura	184	0	-128.84	-0.54	45.78	-49.31	4.08	1.11
			155	-128.84	-0.54	-30.66	-49.31	2.36	1.11
			310	-128.84	-0.54	-107.10	-49.31	0.64	1.11
709	Copertura	96	0	-72.78	-0.02	-7.84	-55.35	0.34	1.55
			43	-72.78	-0.02	-31.45	-55.35	-0.32	1.55
			85	-72.78	-0.02	-55.06	-55.35	-0.98	1.55
710	Copertura	188	0	29.03	-0.56	45.75	-49.19	1.42	0.58
			155	29.03	-0.56	-30.49	-49.19	0.51	0.58
			310	29.03	-0.56	-106.74	-49.19	-0.39	0.58
711	Copertura	97	0	31.79	0.04	-4.66	-63.29	1.56	0.05
			43	31.79	0.04	-31.66	-63.29	1.54	0.05
			85	31.79	0.04	-58.66	-63.29	1.52	0.05
712	Copertura	192	0	-117.24	-0.58	45.62	-49.10	2.64	2.39
			155	-117.24	-0.58	-30.49	-49.10	-1.06	2.39
			310	-117.24	-0.58	-106.60	-49.10	-4.76	2.39
713	Copertura	106	0	-116.07	0.11	-8.37	-51.06	3.16	-2.16
			43	-116.07	0.11	-30.15	-51.06	4.08	-2.16
			85	-116.07	0.11	-51.93	-51.06	5.00	-2.16
714	Copertura	196	0	81.77	-0.35	45.24	-48.78	0.76	1.72
			155	81.77	-0.35	-30.36	-48.78	-1.91	1.72
			310	81.77	-0.35	-105.97	-48.78	-4.59	1.72
715	Copertura	107	0	-25.16	0.58	-2.95	-67.67	1.55	-2.37
			43	-25.16	0.58	-31.82	-67.67	2.56	-2.37
			85	-25.16	0.58	-60.68	-67.67	3.58	-2.37
716	Copertura	200	0	-1.06	0.16	44.55	-48.03	-6.36	-12.72
			155	-1.06	0.16	-29.90	-48.03	13.35	-12.72
			310	-1.06	0.16	-104.35	-48.03	33.06	-12.72
717	Copertura	108	0	142.31	-1.01	-9.95	-49.65	-24.03	12.34
			43	142.31	-1.01	-31.13	-49.65	-29.29	12.34
			85	142.31	-1.01	-52.31	-49.65	-34.56	12.34
718	Copertura	204	0	322.98	-0.64	43.88	-47.94	-32.99	-48.87
			155	322.98	-0.64	-30.43	-47.94	42.76	-48.87

			310	322.98	-0.64	-104.73	-47.94	118.52	-48.87
719	Copertura	109	0	285.60	-4.18	10.20	-106.51	-76.60	32.22
			43	285.60	-4.18	-35.23	-106.51	-90.34	32.22
			85	285.60	-4.18	-80.66	-106.51	-104.08	32.22
720	Copertura	110	0	-178.27	19.65	-52.21	-45.95	9.95	14.86
			43	-178.27	19.65	-75.38	-62.68	3.61	14.86
			85	-178.27	19.65	-105.68	-79.42	-2.73	14.86
721	Copertura	14	0	152.29	-8.52	125.49	-70.01	10.00	7.54
			95	152.29	-8.52	57.58	-74.43	2.84	7.54
			190	152.29	-8.52	-18.72	-87.67	-4.32	7.54
722	Copertura	15	0	-220.58	1.21	103.26	-47.34	-21.29	-32.11
			65	-220.58	1.21	72.50	-47.34	-0.42	-32.11
			130	-220.58	1.21	41.73	-47.34	20.45	-32.11
723	Copertura	16	0	-185.97	0.65	52.27	-32.81	19.19	23.40
			65	-185.97	0.65	30.95	-32.81	3.98	23.40
			130	-185.97	0.65	9.62	-32.81	-11.23	23.40
724	Copertura	17	0	35.08	1.44	103.48	-47.02	1.29	-2.96
			65	35.08	1.44	72.92	-47.02	3.22	-2.96
			130	35.08	1.44	42.35	-47.02	5.14	-2.96
725	Copertura	18	0	46.87	-0.23	73.18	-55.87	-2.33	-2.57
			65	46.87	-0.23	36.86	-55.87	-0.66	-2.57
			130	46.87	-0.23	0.54	-55.87	1.01	-2.57
726	Copertura	19	0	-64.15	1.36	104.73	-47.71	-1.72	-2.75
			65	-64.15	1.36	73.71	-47.71	0.06	-2.75
			130	-64.15	1.36	42.70	-47.71	1.85	-2.75
727	Copertura	20	0	-116.68	-0.25	72.73	-54.15	2.67	-0.37
			65	-116.68	-0.25	37.53	-54.15	2.91	-0.37
			130	-116.68	-0.25	2.33	-54.15	3.15	-0.37
728	Copertura	21	0	106.82	1.32	105.29	-48.00	2.69	1.04
			65	106.82	1.32	74.09	-48.00	2.01	1.04
			130	106.82	1.32	42.89	-48.00	1.34	1.04
729	Copertura	22	0	117.09	-0.10	75.80	-57.45	-3.60	-6.01
			65	117.09	-0.10	38.46	-57.45	0.31	-6.01
			130	117.09	-0.10	1.12	-57.45	4.22	-6.01
730	Copertura	23	0	-16.58	1.33	105.48	-48.08	-0.90	-2.76
			65	-16.58	1.33	74.23	-48.08	0.89	-2.76
			130	-16.58	1.33	42.98	-48.08	2.69	-2.76
731	Copertura	24	0	-83.37	-0.11	75.89	-57.28	2.36	0.54
			65	-83.37	-0.11	38.66	-57.28	2.01	0.54
			130	-83.37	-0.11	1.43	-57.28	1.65	0.54
732	Copertura	25	0	133.54	1.31	105.44	-48.06	4.02	1.52
			65	133.54	1.31	74.20	-48.06	3.03	1.52
			130	133.54	1.31	42.97	-48.06	2.05	1.52
733	Copertura	26	0	117.87	-0.15	76.13	-57.51	-4.02	-5.93
			65	117.87	-0.15	38.75	-57.51	-0.17	-5.93
			130	117.87	-0.15	1.36	-57.51	3.68	-5.93
734	Copertura	27	0	-84.55	-0.15	76.11	-57.49	13.51	12.06
			65	-84.55	-0.15	38.74	-57.49	5.67	12.06
			130	-84.55	-0.15	1.37	-57.49	-2.17	12.06
735	Copertura	28	0	-108.97	1.30	104.90	-47.63	14.15	10.21
			65	-108.97	1.30	73.94	-47.63	7.51	10.21
			130	-108.97	1.30	42.98	-47.63	0.87	10.21
736	Copertura	29	0	121.61	-0.14	75.51	-56.84	11.21	9.71
			65	121.61	-0.14	38.56	-56.84	4.90	9.71
			130	121.61	-0.14	1.62	-56.84	-1.42	9.71
737	Copertura	30	0	-28.31	1.32	105.49	-47.90	23.47	18.47
			65	-28.31	1.32	74.35	-47.90	11.46	18.47
			130	-28.31	1.32	43.22	-47.90	-0.54	18.47
738	Copertura	31	0	-84.78	-0.13	75.78	-57.29	18.78	17.42
			65	-84.78	-0.13	38.54	-57.29	7.46	17.42
			130	-84.78	-0.13	1.31	-57.29	-3.86	17.42
739	Copertura	32	0	-3.55	1.33	105.03	-47.53	26.58	21.72
			65	-3.55	1.33	74.13	-47.53	12.46	21.72
			130	-3.55	1.33	43.24	-47.53	-1.66	21.72
740	Copertura	33	0	122.24	-0.16	73.16	-53.53	14.13	12.88
			65	122.24	-0.16	38.36	-53.53	5.76	12.88
			130	122.24	-0.16	3.56	-53.53	-2.61	12.88
741	Copertura	34	0	-15.77	1.33	104.86	-47.38	28.93	23.86
			65	-15.77	1.33	74.06	-47.38	13.42	23.86
			130	-15.77	1.33	43.26	-47.38	-2.09	23.86
742	Copertura	35	0	-83.11	-0.11	78.59	-60.22	22.95	22.22
			65	-83.11	-0.11	39.45	-60.22	8.51	22.22

			130	-83.11	-0.11	0.31	-60.22	-5.93	22.22
743	Copertura	36	0	-32.24	1.34	104.66	-47.20	31.32	26.72
			65	-32.24	1.34	73.98	-47.20	13.95	26.72
			130	-32.24	1.34	43.30	-47.20	-3.42	26.72
744	Copertura	37	0	126.05	-0.13	74.76	-56.06	17.74	17.30
			65	126.05	-0.13	38.33	-56.06	6.49	17.30
			130	126.05	-0.13	1.89	-56.06	-4.76	17.30
745	Copertura	38	0	-47.15	1.34	104.47	-47.02	33.73	29.06
			65	-47.15	1.34	73.91	-47.02	14.84	29.06
			130	-47.15	1.34	43.35	-47.02	-4.05	29.06
746	Copertura	39	0	-113.83	-0.13	75.64	-57.12	26.19	26.48
			65	-113.83	-0.13	38.51	-57.12	8.98	26.48
			130	-113.83	-0.13	1.38	-57.12	-8.23	26.48
747	Copertura	40	0	-36.16	1.34	104.41	-46.92	36.81	32.74
			65	-36.16	1.34	73.91	-46.92	15.53	32.74
			130	-36.16	1.34	43.42	-46.92	-5.75	32.74
748	Copertura	41	0	66.36	-0.07	74.21	-55.59	23.96	24.92
			65	66.36	-0.07	38.07	-55.59	7.76	24.92
			130	66.36	-0.07	1.94	-55.59	-8.44	24.92
749	Copertura	42	0	42.65	1.37	103.70	-46.34	39.40	36.63
			65	42.65	1.37	73.58	-46.34	15.59	36.63
			130	42.65	1.37	43.46	-46.34	-8.22	36.63
750	Copertura	43	0	12.30	1.37	104.48	-47.47	1.89	-1.95
			65	12.30	1.37	73.62	-47.47	3.16	-1.95
			130	12.30	1.37	42.76	-47.47	4.43	-1.95
751	Copertura	44	0	37.73	-0.05	75.52	-57.59	-2.79	-6.22
			65	37.73	-0.05	38.09	-57.59	1.26	-6.22
			130	37.73	-0.05	0.65	-57.59	5.30	-6.22
752	Copertura	45	0	-122.08	1.34	105.06	-47.89	-4.24	-6.14
			65	-122.08	1.34	73.94	-47.89	-0.25	-6.14
			130	-122.08	1.34	42.81	-47.89	3.74	-6.14
753	Copertura	46	0	-39.36	-0.10	73.66	-55.46	1.10	-1.68
			65	-39.36	-0.10	37.61	-55.46	2.20	-1.68
			130	-39.36	-0.10	1.56	-55.46	3.29	-1.68
754	Copertura	47	0	29.99	1.34	104.88	-47.78	0.67	-0.52
			65	29.99	1.34	73.82	-47.78	1.01	-0.52
			130	29.99	1.34	42.77	-47.78	1.34	-0.52
755	Copertura	48	0	-6.43	-0.05	74.66	-56.92	0.01	-1.16
			65	-6.43	-0.05	37.66	-56.92	0.76	-1.16
			130	-6.43	-0.05	0.67	-56.92	1.52	-1.16
756	Copertura	49	0	-111.19	1.33	104.64	-47.70	-3.02	-4.13
			65	-111.19	1.33	73.64	-47.70	-0.33	-4.13
			130	-111.19	1.33	42.63	-47.70	2.35	-4.13
757	Copertura	50	0	-75.95	-0.07	72.95	-54.93	1.84	2.62
			65	-75.95	-0.07	37.25	-54.93	0.14	2.62
			130	-75.95	-0.07	1.55	-54.93	-1.56	2.62
758	Copertura	51	0	82.57	1.41	103.84	-47.27	1.55	0.50
			65	82.57	1.41	73.11	-47.27	1.23	0.50
			130	82.57	1.41	42.39	-47.27	0.90	0.50
759	Copertura	52	0	-51.84	-0.20	73.46	-56.00	2.72	5.11
			65	-51.84	-0.20	37.06	-56.00	-0.60	5.11
			130	-51.84	-0.20	0.66	-56.00	-3.92	5.11
760	Copertura	53	0	-15.20	1.56	102.20	-46.31	-1.54	3.32
			65	-15.20	1.56	72.09	-46.31	-3.70	3.32
			130	-15.20	1.56	41.99	-46.31	-5.86	3.32
761	Copertura	54	0	148.46	-0.87	64.30	-45.80	-2.45	-5.87
			65	148.46	-0.87	34.53	-45.80	1.37	-5.87
			130	148.46	-0.87	4.75	-45.80	5.18	-5.87
762	Copertura	55	0	234.22	1.09	101.74	-46.70	38.11	55.82
			65	234.22	1.09	71.38	-46.70	1.83	55.82
			130	234.22	1.09	41.02	-46.70	-34.45	55.82
763	Copertura	56	0	164.30	0.41	68.08	-53.58	-35.99	-49.04
			65	164.30	0.41	33.26	-53.58	-4.12	-49.04
			130	164.30	0.41	-1.57	-53.58	27.76	-49.04
764	Copertura	70	0	-234.54	-8.94	81.85	-12.87	13.02	0.88
			95	-234.54	-8.94	66.83	-21.70	12.18	0.88
			190	-234.54	-8.94	35.03	-48.18	11.34	0.88
765	Copertura	81	0	-150.49	-1.32	52.85	-75.29	4.84	-19.22
			80	-150.49	-1.32	-7.38	-75.29	20.22	-19.22
			160	-150.49	-1.32	-67.62	-75.29	35.60	-19.22
766	Copertura	126	0	-226.92	2.31	11.62	-32.37	-10.21	-25.15
			30	-226.92	2.31	1.91	-32.37	-2.67	-25.15

			60	-226.92	2.31	-7.80	-32.37	4.88	-25.15
767	Copertura	98	0	-62.65	-0.73	37.16	-52.85	4.34	-5.25
			82	-62.65	-0.73	-6.36	-52.85	8.66	-5.25
			165	-62.65	-0.73	-49.88	-52.85	12.98	-5.25
768	Copertura	99	0	-7.71	0.13	41.10	-60.01	2.19	1.57
			82	-7.71	0.13	-8.32	-60.01	0.90	1.57
			165	-7.71	0.13	-57.74	-60.01	-0.39	1.57
769	Copertura	100	0	14.00	0.06	39.83	-58.16	3.35	2.37
			82	14.00	0.06	-8.06	-58.16	1.40	2.37
			165	14.00	0.06	-55.95	-58.16	-0.55	2.37
770	Copertura	101	0	27.43	0.03	40.39	-59.18	1.28	0.52
			82	27.43	0.03	-8.34	-59.18	0.85	0.52
			165	27.43	0.03	-57.06	-59.18	0.42	0.52
771	Copertura	102	0	13.57	0.10	40.40	-59.09	3.10	1.55
			82	13.57	0.10	-8.26	-59.09	1.82	1.55
			165	13.57	0.10	-56.92	-59.09	0.54	1.55
772	Copertura	103	0	14.84	0.08	40.25	-58.88	-2.13	-0.91
			82	14.84	0.08	-8.23	-58.88	-1.38	-0.91
			165	14.84	0.08	-56.71	-58.88	-0.63	-0.91
773	Copertura	104	0	1.82	0.02	40.74	-59.58	-1.60	-0.19
			82	1.82	0.02	-8.32	-59.58	-1.44	-0.19
			165	1.82	0.02	-57.38	-59.58	-1.28	-0.19
774	Copertura	105	0	9.17	0.03	39.81	-58.05	-4.05	-1.17
			82	9.17	0.03	-7.99	-58.05	-3.09	-1.17
			165	9.17	0.03	-55.79	-58.05	-2.13	-1.17
775	Copertura	111	0	-0.74	0.07	41.71	-62.82	-2.86	-0.40
			80	-0.74	0.07	-8.39	-62.82	-2.54	-0.40
			160	-0.74	0.07	-58.50	-62.82	-2.22	-0.40
776	Copertura	112	0	6.01	0.04	36.69	-54.92	-5.97	-1.78
			82	6.01	0.04	-8.53	-54.92	-4.50	-1.78
			165	6.01	0.04	-53.76	-54.92	-3.04	-1.78
777	Copertura	113	0	-0.83	0.05	40.97	-60.16	-4.94	-0.97
			82	-0.83	0.05	-8.57	-60.16	-4.14	-0.97
			165	-0.83	0.05	-58.10	-60.16	-3.34	-0.97
778	Copertura	114	0	-30.08	0.12	39.24	-57.64	-8.11	-2.56
			82	-30.08	0.12	-8.22	-57.64	-6.01	-2.56
			165	-30.08	0.12	-55.68	-57.64	-3.91	-2.56
779	Copertura	115	0	-70.34	-0.22	41.61	-60.39	-7.16	-2.98
			82	-70.34	-0.22	-8.12	-60.39	-4.71	-2.98
			165	-70.34	-0.22	-57.85	-60.39	-2.25	-2.98
780	Copertura	116	0	157.22	-0.23	39.30	-56.55	3.47	2.61
			82	157.22	-0.23	-7.26	-56.55	1.32	2.61
			165	157.22	-0.23	-53.83	-56.55	-0.82	2.61
781	Copertura	117	0	-146.30	0.13	41.07	-59.12	2.76	1.47
			82	-146.30	0.13	-7.61	-59.12	1.55	1.47
			165	-146.30	0.13	-56.29	-59.12	0.35	1.47
782	Copertura	118	0	104.47	0.10	38.93	-55.76	1.53	-0.01
			82	104.47	0.10	-6.98	-55.76	1.54	-0.01
			165	104.47	0.10	-52.89	-55.76	1.54	-0.01
783	Copertura	131	0	44.58	-0.18	1.28	-57.32	1.09	-5.47
			30	44.58	-0.18	-15.92	-57.32	2.74	-5.47
			60	44.58	-0.18	-33.11	-57.32	4.38	-5.47
784	Copertura	133	0	-114.94	-0.11	3.16	-55.54	3.22	1.79
			30	-114.94	-0.11	-13.50	-55.54	2.69	1.79
			60	-114.94	-0.11	-30.17	-55.54	2.15	1.79
785	Copertura	139	0	124.70	0.20	2.10	-58.75	4.64	2.15
			30	124.70	0.20	-15.53	-58.75	4.00	2.15
			60	124.70	0.20	-33.15	-58.75	3.35	2.15
786	Copertura	143	0	-83.27	0.19	2.41	-58.58	1.73	0.74
			30	-83.27	0.19	-15.17	-58.58	1.51	0.74
			60	-83.27	0.19	-32.74	-58.58	1.29	0.74
787	Copertura	147	0	124.78	0.11	2.30	-58.87	4.02	1.52
			30	124.78	0.11	-15.36	-58.87	3.56	1.52
			60	124.78	0.11	-33.02	-58.87	3.10	1.52
788	Copertura	151	0	-96.38	0.11	2.33	-59.11	-2.66	-0.88
			30	-96.38	0.11	-15.41	-59.11	-2.39	-0.88
			60	-96.38	0.11	-33.14	-59.11	-2.13	-0.88
789	Copertura	155	0	112.62	0.15	2.59	-58.44	-1.82	-0.37
			30	112.62	0.15	-14.94	-58.44	-1.71	-0.37
			60	112.62	0.15	-32.48	-58.44	-1.59	-0.37
790	Copertura	159	0	-101.63	0.14	2.28	-59.19	-4.64	-0.98
			30	-101.63	0.14	-15.47	-59.19	-4.35	-0.98

			60	-101.63	0.14	-33.23	-59.19	-4.05	-0.98
791	Copertura	119	0	-188.76	0.12	40.42	-58.60	-0.28	-2.10
			82	-188.76	0.12	-7.83	-58.60	1.45	-2.10
			165	-188.76	0.12	-56.08	-58.60	3.18	-2.10
792	Copertura	120	0	49.68	-0.48	38.13	-54.95	-2.75	-2.63
			82	49.68	-0.48	-7.12	-54.95	-0.59	-2.63
			165	49.68	-0.48	-52.37	-54.95	1.58	-2.63
793	Copertura	121	0	67.47	0.39	43.39	-62.37	-3.33	12.59
			82	67.47	0.39	-7.96	-62.37	-13.69	12.59
			165	67.47	0.39	-59.32	-62.37	-24.06	12.59
794	Copertura	122	0	341.86	2.19	31.36	-39.65	-0.44	46.20
			82	341.86	2.19	-1.29	-39.65	-38.49	46.20
			165	341.86	2.19	-33.94	-39.65	-76.53	46.20
795	Copertura	123	0	-234.54	-8.94	35.03	-48.18	11.34	0.88
			82	-234.54	-8.94	-17.94	-80.49	10.61	0.88
			165	-234.54	-8.94	-97.53	-112.80	9.89	0.88
796	Copertura	163	0	110.18	0.17	4.59	-55.22	-3.21	-0.55
			33	110.18	0.17	-13.40	-55.22	-3.03	-0.55
			65	110.18	0.17	-31.39	-55.22	-2.85	-0.55
797	Copertura	167	0	-104.91	0.14	1.29	-62.52	-6.95	-1.63
			30	-104.91	0.14	-17.46	-62.52	-6.46	-1.63
			60	-104.91	0.14	-36.22	-62.52	-5.97	-1.63
798	Copertura	171	0	109.48	0.16	2.89	-58.09	-5.58	-1.07
			30	109.48	0.16	-14.54	-58.09	-5.26	-1.07
			60	109.48	0.16	-31.97	-58.09	-4.94	-1.07
799	Copertura	174	0	-140.39	0.14	2.39	-59.70	-9.59	-2.45
			30	-140.39	0.14	-15.52	-59.70	-8.85	-2.45
			60	-140.39	0.14	-33.43	-59.70	-8.11	-2.45
800	Copertura	179	0	40.51	0.36	3.06	-58.12	-9.47	-3.86
			30	40.51	0.36	-14.38	-58.12	-8.31	-3.86
			60	40.51	0.36	-31.81	-58.12	-7.15	-3.86
801	Copertura	183	0	46.36	0.35	1.69	-58.82	5.55	3.48
			30	46.36	0.35	-15.96	-58.82	4.51	3.48
			60	46.36	0.35	-33.60	-58.82	3.46	3.48
802	Copertura	187	0	-36.61	0.18	2.51	-56.71	3.54	1.32
			30	-36.61	0.18	-14.50	-56.71	3.15	1.32
			60	-36.61	0.18	-31.52	-56.71	2.75	1.32
803	Copertura	191	0	-5.22	0.25	1.62	-58.16	1.63	0.14
			30	-5.22	0.25	-15.83	-58.16	1.58	0.14
			60	-5.22	0.25	-33.27	-58.16	1.54	0.14
804	Copertura	194	0	-80.63	0.23	2.51	-56.13	-1.76	-2.47
			30	-80.63	0.23	-14.33	-56.13	-1.02	-2.47
			60	-80.63	0.23	-31.17	-56.13	-0.28	-2.47
805	Copertura	198	0	-58.45	-0.11	1.43	-57.42	-4.11	-2.26
			30	-58.45	-0.11	-15.79	-57.42	-3.43	-2.26
			60	-58.45	-0.11	-33.02	-57.42	-2.75	-2.26
806	Copertura	203	0	167.17	-1.66	4.79	-47.76	5.80	15.04
			30	167.17	-1.66	-9.54	-47.76	1.29	15.04
			60	167.17	-1.66	-23.86	-47.76	-3.23	15.04
807	Copertura	207	0	242.17	0.99	-0.42	-54.26	25.71	43.75
			30	242.17	0.99	-16.70	-54.26	12.58	43.75
			60	242.17	0.99	-32.98	-54.26	-0.54	43.75

1.1.12.2 Piastre SLU

Tabella 24.I

Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	-0.379	-2.306	0.723	20.866	73.222	-33.746	-1.634	2.307
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64,	-1.149	-4.520	-0.843	216.708	1043.669	-198.069	-6.118	-13.216

		65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44								
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	-0.446	2.203	0.648	-195.545	-569.381	-78.075	-6.209	-7.111

1.1.13 Risultati Condizioni (Neve).

1.1.13.1 Sollecitazioni SLU

Tabella 25.I

Sollecitazioni									
Asta	Imp.	Fili	X [cm]	N [daN]	Mt [daNm]	Mxz [daNm]	Txz [daN]	Mxy [daNm]	Txy [daN]
1	Fondazione	1, 2	0	-19.14	-23.55	-15.85	-75.21	2.38	0.73
			42	-19.13	-23.54	-37.88	-32.62	2.02	0.97
			83	-19.14	-23.54	-44.33	0.04	1.58	1.11
2	Fondazione	1, 2	0	-18.17	-23.90	-68.64	31.58	1.57	-1.53
			42	-18.18	-23.90	-50.19	55.90	2.19	-1.46
			83	-18.20	-23.90	-23.04	73.82	2.79	-1.45
3	Fondazione	1, 15	0	20.72	44.72	-29.34	-25.95	3.30	5.56
			40	20.46	44.72	-30.30	21.42	1.09	5.55
			80	20.20	44.73	-11.73	72.45	-1.10	5.44
4	Fondazione	1, 15	0	23.21	107.08	-57.31	77.88	-1.11	-6.24
			40	22.97	107.09	-15.43	133.46	1.40	-6.43
			80	22.73	107.09	49.61	194.48	4.01	-6.70
5	Fondazione	2, 3	0	-24.42	-19.57	-37.71	-7.14	2.28	3.04
			35	-24.45	-19.57	-38.16	3.93	1.23	3.02
			69	-24.49	-19.57	-35.29	12.32	0.20	2.97
6	Fondazione	2, 3	0	-14.81	-7.98	-43.75	40.81	0.19	-0.93
			35	-14.86	-7.98	-28.49	47.30	0.53	-0.99
			69	-14.91	-7.98	-11.22	52.60	0.88	-1.07
7	Fondazione	3, 4	0	-7.66	-7.06	-15.40	-2.71	0.75	0.91
			35	-7.72	-7.06	-15.53	1.82	0.45	0.82
			69	-7.78	-7.07	-14.17	5.91	0.18	0.72
8	Fondazione	3, 4	0	-1.58	-0.89	-15.11	18.30	0.18	-0.09
			35	-1.64	-0.89	-8.10	22.24	0.23	-0.20
			69	-1.70	-0.90	0.27	26.26	0.32	-0.32
9	Fondazione	4, 5	0	3.30	1.05	1.01	-11.04	0.27	0.28
			35	3.24	1.05	-2.07	-6.85	0.19	0.16
			69	3.17	1.05	-3.66	-2.45	0.16	0.03
10	Fondazione	4, 5	0	7.01	2.40	-1.77	3.72	0.16	0.19
			35	6.95	2.40	0.31	8.36	0.12	0.06
			69	6.90	2.40	4.05	13.27	0.12	-0.08
11	Fondazione	5, 6	0	9.72	2.73	5.98	-15.02	0.12	0.11
			35	9.67	2.73	1.69	-9.89	0.10	-0.03
			69	9.62	2.73	-0.81	-4.60	0.14	-0.17
12	Fondazione	5, 6	0	11.51	2.46	1.11	-1.07	0.14	0.22
			35	11.46	2.46	1.69	4.37	0.08	0.08
			69	11.42	2.46	4.16	9.92	0.08	-0.06
13	Fondazione	6, 7	0	14.79	2.12	5.69	-15.82	0.09	0.17

	ne								
			35	14.75	2.12	1.21	-10.19	0.06	0.03
			69	14.72	2.12	-1.33	-4.57	0.07	-0.12
14	Fondazio ne	6, 7	0	15.50	1.51	-0.14	-1.90	0.07	0.13
			35	15.48	1.51	0.18	3.73	0.05	-0.02
			69	15.46	1.51	2.44	9.37	0.09	-0.17
15	Fondazio ne	7, 8	0	14.47	0.70	3.11	-13.09	0.08	0.12
			35	14.46	0.70	-0.44	-7.47	0.07	-0.02
			69	14.45	0.70	-2.05	-1.89	0.10	-0.17
16	Fondazio ne	7, 8	0	14.48	-0.29	-2.19	0.45	0.10	0.14
			35	14.48	-0.29	-1.07	6.02	0.08	0.00
			69	14.48	-0.29	1.97	11.62	0.10	-0.15
17	Fondazio ne	8, 9	0	14.02	-1.54	1.27	-8.18	0.10	0.14
			35	14.03	-1.54	-0.59	-2.56	0.08	-0.01
			69	14.04	-1.54	-0.50	3.07	0.10	-0.15
18	Fondazio ne	8, 9	0	13.05	-2.61	-2.04	5.10	0.10	0.17
			35	13.07	-2.61	0.69	10.77	0.07	0.03
			69	13.10	-2.61	5.38	16.48	0.08	-0.11
19	Fondazio ne	9, 10	0	12.84	-3.21	3.51	-7.89	0.08	0.10
			35	12.88	-3.21	1.77	-2.19	0.07	-0.03
			69	12.91	-3.21	1.98	3.45	0.10	-0.17
20	Fondazio ne	9, 10	0	10.84	-3.30	-0.40	6.50	0.10	0.11
			35	10.88	-3.30	2.80	12.05	0.09	-0.02
			69	10.93	-3.30	7.89	17.48	0.12	-0.14
21	Fondazio ne	10, 11	0	4.89	-2.30	6.15	-15.79	0.12	0.00
			35	4.94	-2.30	1.59	-10.58	0.14	-0.12
			69	4.99	-2.30	-1.21	-5.67	0.20	-0.24
22	Fondazio ne	10, 11	0	1.34	-0.67	-2.94	0.85	0.20	-0.01
			35	1.40	-0.67	-1.86	5.47	0.23	-0.12
			69	1.45	-0.67	0.78	9.84	0.29	-0.22
23	Fondazio ne	11, 12	0	-3.51	0.89	0.37	-27.70	0.34	0.33
			35	-3.46	0.89	-8.47	-23.55	0.24	0.24
			69	-3.41	0.89	-15.92	-19.55	0.18	0.15
24	Fondazio ne	11, 12	0	-9.81	6.46	-14.95	-7.77	0.18	-0.90
			35	-9.76	6.46	-16.93	-3.66	0.50	-0.98
			69	-9.72	6.46	-17.44	0.89	0.85	-1.05
25	Fondazio ne	12, 13	0	-17.47	7.39	-13.69	-48.86	0.99	1.17
			35	-17.43	7.39	-29.66	-43.53	0.59	1.12
			69	-17.40	7.39	-43.60	-36.96	0.21	1.08
26	Fondazio ne	12, 13	0	-27.23	20.66	-35.98	-14.22	0.22	-2.96
			35	-27.21	20.66	-39.49	-5.67	1.24	-2.97
			69	-27.20	20.66	-39.60	5.62	2.27	-2.96
27	Fondazio ne	13, 14	0	-19.07	22.58	-24.83	-69.80	2.78	1.06
			42	-19.06	22.58	-50.23	-51.43	2.33	1.12
			83	-19.07	22.58	-66.69	-26.47	1.84	1.24
28	Fondazio ne	13, 14	0	-21.17	22.25	-38.02	-9.28	1.86	-0.86
			42	-21.18	22.25	-35.26	24.18	2.17	-0.66
			83	-21.21	22.25	-16.55	67.60	2.39	-0.35
29	Fondazio ne	14, 16	0	24.38	-46.07	-27.23	-34.37	-3.48	-5.33
			40	24.04	-46.08	-31.38	13.67	-1.36	-5.33
			80	23.72	-46.08	-15.78	65.15	0.75	-5.24
30	Fondazio ne	14, 16	0	24.46	-103.10	-52.80	61.78	0.76	5.64
			40	24.16	-103.11	-17.25	117.62	-1.51	5.81
			80	23.86	-103.11	41.53	178.74	-3.87	6.07
31	Fondazio ne	15, 17	0	28.58	29.33	1.99	-46.39	6.26	18.74

			33	28.40	29.34	-4.36	8.29	0.12	18.47
			66	28.22	29.34	7.92	66.53	-5.93	18.16
32	Fondazio ne	15, 17	0	26.52	121.94	-35.36	124.46	-5.94	-23.22
			33	26.36	121.95	15.85	186.35	1.78	-23.56
			66	26.20	121.95	88.10	251.92	9.62	-23.96
33	Fondazio ne	16, 18	0	29.41	-31.44	0.38	-43.90	-6.07	-18.02
			33	29.18	-31.45	-5.13	10.81	-0.16	-17.76
			66	28.95	-31.46	8.00	69.08	5.65	-17.46
34	Fondazio ne	16, 18	0	28.73	-119.28	-30.83	105.79	5.66	22.15
			33	28.52	-119.29	14.23	167.70	-1.71	22.50
			66	28.31	-119.30	80.33	233.28	-9.20	22.89
35	Fondazio ne	17, 19	0	43.90	-25.45	53.18	-147.57	11.06	28.83
			33	43.76	-25.44	15.74	-79.04	1.62	28.41
			66	43.63	-25.43	1.32	-8.18	-7.69	27.98
36	Fondazio ne	17, 19	0	37.21	85.43	-16.73	57.68	-7.69	-25.99
			33	37.10	85.44	14.32	130.76	0.96	-26.43
			66	37.01	85.45	69.85	206.01	9.76	-26.90
37	Fondazio ne	18, 20	0	43.71	20.28	51.64	-140.62	-10.70	-27.94
			33	43.52	20.27	16.51	-72.05	-1.55	-27.51
			66	43.34	20.26	4.41	-1.08	7.46	-27.08
38	Fondazio ne	18, 20	0	39.27	-86.94	-15.51	46.14	7.46	25.72
			33	39.11	-86.95	11.76	119.36	-1.10	26.17
			66	38.96	-86.96	63.57	194.81	-9.81	26.66
39	Fondazio ne	19, 21	0	24.36	-44.65	54.25	-168.81	8.63	25.49
			33	24.27	-44.64	11.20	-92.00	0.29	25.02
			66	24.19	-44.63	-6.33	-14.17	-7.89	24.55
40	Fondazio ne	19, 21	0	19.28	65.69	-13.21	38.41	-7.89	-23.91
			33	19.21	65.70	12.46	117.22	0.08	-24.38
			66	19.14	65.72	64.29	196.99	8.21	-24.88
41	Fondazio ne	20, 22	0	24.94	42.38	50.20	-163.16	-8.69	-25.64
			33	24.81	42.37	9.07	-86.03	-0.31	-25.14
			66	24.68	42.36	-6.40	-7.71	7.91	-24.66
42	Fondazio ne	20, 22	0	20.04	-67.84	-15.23	39.28	7.91	23.71
			33	19.92	-67.85	10.84	118.79	0.00	24.20
			66	19.81	-67.86	63.35	199.49	-8.07	24.72
43	Fondazio ne	21, 23	0	30.20	-58.46	61.65	-191.08	9.06	25.57
			33	30.15	-58.45	11.83	-110.93	0.71	25.07
			66	30.11	-58.44	-11.57	-30.98	-7.48	24.59
44	Fondazio ne	21, 23	0	25.31	49.69	-10.29	30.47	-7.48	-25.19
			33	25.28	49.70	12.94	110.21	0.91	-25.68
			66	25.26	49.72	62.44	189.71	9.46	-26.17
45	Fondazio ne	22, 24	0	31.24	54.05	58.97	-191.32	-8.93	-25.25
			33	31.14	54.04	9.27	-109.99	-0.68	-24.73
			66	31.05	54.03	-13.57	-28.55	7.39	-24.22
46	Fondazio ne	22, 24	0	26.36	-53.80	-14.02	20.28	7.39	24.60
			33	26.28	-53.81	6.15	101.86	-0.81	25.11
			66	26.21	-53.82	53.27	183.63	-9.18	25.63
47	Fondazio ne	23, 25	0	2.50	-78.69	71.73	-239.75	8.51	23.78
			33	2.48	-78.68	5.63	-161.10	0.74	23.29
			66	2.46	-78.67	-34.75	-83.85	-6.87	22.83
48	Fondazio ne	23, 25	0	-6.19	18.53	-18.43	-27.96	-6.86	-14.45
			33	-6.20	18.54	-15.07	48.09	-2.02	-14.90
			66	-6.23	18.55	13.23	123.27	2.97	-15.35
49	Fondazio ne	24, 26	0	5.28	65.71	56.00	-215.82	-8.24	-23.24
			33	5.21	65.70	-1.74	-134.29	-0.65	-22.73

			66	5.15	65.69	-32.68	-53.39	6.77	-22.23
50	Fondazio ne	24, 26	0	-2.14	-30.38	-28.42	-5.02	6.76	13.69
			33	-2.21	-30.39	-16.77	75.54	2.17	14.17
			66	-2.27	-30.40	21.47	156.17	-2.59	14.66
51	Fondazio ne	25, 26	0	42.26	8.99	-120.80	-91.33	-0.85	-1.07
			49	41.61	8.99	-141.50	-0.70	-0.34	-1.04
			97	41.00	8.99	-126.72	55.78	0.16	-1.01
52	Fondazio ne	25, 26	0	40.15	3.78	-131.10	-0.45	0.16	0.29
			49	39.57	3.78	-122.94	29.66	0.01	0.30
			97	39.02	3.78	-105.06	40.69	-0.14	0.30
53	Fondazio ne	25, 26	0	42.58	1.16	-93.82	31.97	-0.14	-0.16
			49	42.07	1.16	-78.14	30.36	-0.06	-0.17
			97	41.58	1.16	-65.28	21.16	0.03	-0.19
54	Fondazio ne	25, 26	0	45.12	0.94	-53.35	37.53	0.03	0.00
			49	44.67	0.94	-38.03	24.70	0.04	-0.03
			97	44.25	0.94	-29.27	10.95	0.06	-0.08
55	Fondazio ne	25, 26	0	46.99	0.45	-19.66	25.63	0.06	0.02
			49	46.61	0.45	-10.30	12.79	0.06	-0.03
			97	46.27	0.45	-6.77	1.79	0.09	-0.09
56	Fondazio ne	25, 26	0	48.15	0.23	-1.75	13.37	0.09	0.06
			49	47.85	0.23	2.60	4.64	0.08	-0.01
			97	47.58	0.23	3.25	-1.82	0.10	-0.09
57	Fondazio ne	25, 26	0	48.77	0.20	5.15	4.75	0.10	0.08
			49	48.54	0.20	6.36	0.37	0.08	-0.01
			97	48.35	0.20	5.88	-2.24	0.11	-0.10
58	Fondazio ne	25, 26	0	49.07	0.13	6.15	0.07	0.11	0.11
			49	48.91	0.13	5.87	-1.14	0.08	0.01
			97	48.80	0.13	5.27	-1.28	0.09	-0.09
59	Fondazio ne	25, 26	0	49.22	0.06	4.99	-1.54	0.09	0.06
			49	49.14	0.06	4.38	-0.94	0.09	-0.04
			97	49.10	0.06	4.17	0.14	0.13	-0.14
60	Fondazio ne	25, 26	0	49.49	0.00	4.06	-1.15	0.13	0.15
			49	49.48	0.00	3.81	0.16	0.08	0.05
			97	49.52	0.00	4.21	1.48	0.08	-0.05
61	Fondazio ne	25, 26	0	49.59	-0.06	4.43	-0.03	0.08	0.08
			49	49.67	-0.06	4.68	1.07	0.07	-0.02
			97	49.79	-0.06	5.36	1.69	0.10	-0.12
62	Fondazio ne	25, 26	0	49.73	-0.15	5.68	1.47	0.10	0.09
			49	49.88	-0.15	6.37	1.33	0.08	0.00
			97	50.08	-0.15	6.73	0.07	0.10	-0.09
63	Fondazio ne	25, 26	0	49.71	-0.28	6.50	2.47	0.11	0.08
			49	49.95	-0.28	7.06	-0.27	0.09	0.00
			97	50.22	-0.28	5.83	-4.89	0.11	-0.08
64	Fondazio ne	25, 26	0	49.38	-0.48	3.93	1.47	0.11	0.08
			49	49.69	-0.48	3.01	-5.40	0.09	0.01
			97	50.04	-0.48	-1.86	-14.72	0.10	-0.04
65	Fondazio ne	25, 26	0	48.50	-0.63	-7.08	-2.68	0.10	0.07
			49	48.89	-0.63	-11.23	-14.46	0.08	0.02
			97	49.31	-0.63	-21.65	-28.24	0.07	-0.01
66	Fondazio ne	25, 26	0	46.89	-0.33	-31.11	-12.05	0.07	0.05
			49	47.36	-0.33	-40.65	-26.81	0.06	0.03
			97	47.86	-0.33	-57.26	-40.61	0.04	0.03
67	Fondazio ne	25, 26	0	44.63	0.46	-70.69	-26.49	0.04	0.17
			49	45.17	0.46	-86.35	-36.42	-0.04	0.18
			97	45.74	0.46	-105.06	-38.11	-0.14	0.21

68	Fondazio ne	25, 26	0	41.53	1.13	-115.68	-34.93	-0.13	-0.48
			49	42.14	1.13	-130.56	-22.81	0.09	-0.44
			97	42.78	1.13	-134.81	10.05	0.29	-0.39
69	Fondazio ne	25, 26	0	43.87	1.50	-131.70	-67.66	0.30	0.83
			49	44.55	1.50	-151.20	-6.38	-0.12	0.90
			97	45.26	1.50	-132.30	91.53	-0.58	0.98
70	Fondazio ne	25, 28	0	8.91	-38.89	23.89	-177.11	4.92	14.64
			43	8.88	-38.88	-31.00	-81.48	-1.18	14.07
			85	8.86	-38.86	-45.49	13.20	-7.04	13.51
71	Fondazio ne	25, 28	0	10.98	68.68	-51.51	31.84	-7.04	-18.26
			43	10.97	68.70	-17.79	127.07	0.84	-18.84
			85	10.96	68.71	56.77	224.11	8.98	-19.47
72	Fondazio ne	26, 27	0	11.95	26.59	19.34	-154.88	-4.13	-16.52
			33	11.89	26.57	-18.44	-74.15	1.24	-16.02
			66	11.83	26.56	-29.56	6.75	6.44	-15.53
73	Fondazio ne	26, 27	0	14.94	-70.44	-36.43	52.11	6.45	22.95
			33	14.89	-70.45	-5.80	133.61	-1.21	23.46
			66	14.84	-70.46	51.87	216.05	-9.04	23.99
74	Fondazio ne	27, 29	0	0.86	46.93	46.06	-181.09	-8.13	-24.64
			33	0.81	46.92	0.01	-97.99	-0.09	-24.10
			66	0.77	46.91	-18.56	-14.57	7.78	-23.56
75	Fondazio ne	27, 29	0	1.44	-62.28	-23.62	28.81	7.78	22.76
			33	1.39	-62.29	-0.27	112.72	0.18	23.29
			66	1.35	-62.31	50.87	197.30	-7.60	23.85
76	Fondazio ne	28, 30	0	-4.46	-43.68	51.50	-188.98	7.92	22.83
			37	-4.46	-43.67	-2.07	-104.50	-0.31	22.28
			73	-4.47	-43.66	-24.71	-19.46	-8.34	21.75
77	Fondazio ne	28, 30	0	-1.72	68.15	-31.60	32.26	-8.35	-22.54
			37	-1.73	68.16	-4.18	118.19	-0.02	-23.08
			73	-1.73	68.17	54.84	205.39	8.50	-23.64
78	Fondazio ne	29, 31	0	15.45	52.65	49.05	-191.16	-8.54	-24.89
			33	15.41	52.64	-0.02	-106.24	-0.41	-24.33
			66	15.38	52.63	-21.06	-21.35	7.52	-23.78
79	Fondazio ne	29, 31	0	15.91	-57.81	-23.81	20.02	7.52	23.73
			33	15.88	-57.83	-3.17	105.08	-0.40	24.28
			66	15.86	-57.84	45.60	190.53	-8.51	24.85
80	Fondazio ne	30, 32	0	0.93	-48.90	49.47	-187.55	8.52	24.75
			34	0.92	-48.88	-0.63	-104.96	0.13	24.22
			69	0.91	-48.87	-22.39	-22.04	-8.07	23.69
81	Fondazio ne	30, 32	0	0.96	64.34	-27.99	38.10	-8.07	-23.65
			34	0.95	64.35	-0.66	121.59	0.12	-24.19
			69	0.95	64.36	55.40	205.90	8.50	-24.74
82	Fondazio ne	31, 33	0	-1.05	54.69	46.18	-190.32	-7.58	-23.87
			33	-1.07	54.68	-2.50	-104.77	0.21	-23.30
			66	-1.09	54.66	-22.98	-19.42	7.81	-22.75
83	Fondazio ne	31, 33	0	0.28	-55.87	-25.16	19.78	7.81	22.43
			33	0.26	-55.88	-4.55	105.16	0.31	22.98
			66	0.23	-55.89	44.29	190.83	-7.36	23.55
84	Fondazio ne	32, 34	0	2.02	-55.58	51.74	-201.17	8.51	24.82
			35	2.01	-55.57	-2.95	-115.85	0.04	24.26
			69	2.01	-55.55	-28.19	-30.51	-8.23	23.71
85	Fondazio ne	32, 34	0	1.33	61.15	-27.79	28.63	-8.23	-23.41
			35	1.32	61.17	-3.15	114.28	-0.06	-23.96
			69	1.32	61.18	51.14	200.54	8.30	-24.52
86	Fondazio	33, 35	0	12.75	55.44	46.13	-191.24	-8.29	-24.43

	ne								
			33	12.73	55.42	-2.83	-105.56	-0.32	-23.86
			66	12.72	55.41	-23.57	-20.15	7.46	-23.30
87	Fondazio ne	33, 35	0	14.58	-54.57	-25.28	18.27	7.46	23.50
			33	14.57	-54.58	-5.16	103.64	-0.38	24.06
			66	14.57	-54.60	43.15	189.22	-8.42	24.63
88	Fondazio ne	34, 36	0	2.34	-53.14	47.20	-196.57	8.31	24.29
			35	2.34	-53.13	-5.69	-110.06	0.03	23.72
			69	2.33	-53.12	-28.75	-23.62	-8.06	23.16
89	Fondazio ne	34, 36	0	2.10	59.98	-30.01	24.76	-8.06	-23.05
			35	2.10	59.99	-6.52	111.48	-0.01	-23.61
			69	2.09	60.01	46.99	198.82	8.24	-24.19
90	Fondazio ne	35, 37	0	-2.79	56.11	45.70	-190.06	-7.48	-23.75
			33	-2.79	56.10	-2.90	-104.52	0.26	-23.18
			66	-2.79	56.09	-23.32	-19.30	7.82	-22.63
91	Fondazio ne	35, 37	0	-0.64	-53.90	-24.55	20.50	7.82	22.56
			33	-0.65	-53.91	-3.74	105.63	0.28	23.11
			66	-0.65	-53.92	45.18	190.91	-7.44	23.68
92	Fondazio ne	36, 38	0	3.44	-51.71	43.81	-196.52	8.25	24.21
			35	3.44	-51.70	-8.86	-108.84	0.00	23.63
			69	3.44	-51.69	-31.28	-21.07	-8.06	23.07
93	Fondazio ne	36, 38	0	2.39	62.88	-33.58	26.13	-8.06	-22.85
			35	2.39	62.89	-9.36	114.40	-0.08	-23.42
			69	2.39	62.90	45.46	203.57	8.10	-24.01
94	Fondazio ne	37, 39	0	12.63	57.99	48.09	-191.70	-8.36	-24.62
			33	12.62	57.98	-1.11	-106.56	-0.33	-24.06
			66	12.63	57.97	-22.29	-21.88	7.52	-23.51
95	Fondazio ne	37, 39	0	14.26	-51.86	-22.07	21.29	7.52	23.90
			33	14.27	-51.87	-1.11	105.72	-0.46	24.44
			66	14.28	-51.88	47.70	190.09	-8.62	25.00
96	Fondazio ne	38, 40	0	5.64	-47.28	38.63	-190.81	8.12	23.83
			34	5.64	-47.27	-11.46	-101.61	0.05	23.25
			69	5.65	-47.26	-30.92	-11.92	-7.81	22.68
97	Fondazio ne	38, 40	0	3.22	67.19	-36.33	30.50	-7.81	-22.34
			34	3.22	67.20	-10.41	121.10	-0.06	-22.92
			69	3.23	67.21	46.77	213.06	7.89	-23.50
98	Fondazio ne	39, 41	0	-2.07	62.35	51.87	-200.71	-7.68	-23.96
			33	-2.06	62.33	-0.50	-116.73	0.13	-23.42
			66	-2.04	62.32	-25.27	-33.49	7.77	-22.89
99	Fondazio ne	39, 41	0	-1.30	-47.22	-21.94	10.42	7.77	24.14
			33	-1.29	-47.23	-4.85	93.12	-0.28	24.66
			66	-1.28	-47.24	39.48	175.53	-8.50	25.19
100	Fondazio ne	40, 42	0	7.68	-41.31	36.95	-181.53	7.90	24.30
			35	7.69	-41.30	-9.53	-87.75	-0.38	23.71
			69	7.70	-41.29	-23.50	6.98	-8.46	23.12
101	Fondazio ne	40, 42	0	8.16	82.11	-33.15	62.06	-8.46	-24.05
			35	8.17	82.12	4.78	158.10	-0.06	-24.64
			69	8.19	82.14	76.11	255.68	8.55	-25.24
102	Fondazio ne	41, 44	0	-4.72	66.69	44.96	-208.05	-8.49	-23.60
			33	-4.70	66.68	-10.17	-126.16	-0.79	-23.08
			66	-4.69	66.67	-38.39	-45.00	6.74	-22.58
103	Fondazio ne	41, 44	0	-9.09	-29.81	-34.54	5.10	6.74	13.90
			33	-9.08	-29.82	-19.52	85.94	2.07	14.38
			66	-9.07	-29.83	22.20	166.95	-2.76	14.87
104	Fondazio ne	42, 43	0	11.97	-36.78	64.47	-113.27	8.53	22.55

			23	11.99	-36.77	45.95	-47.66	3.39	22.14
			46	12.01	-36.76	42.54	18.01	-1.65	21.74
105	Fondazio ne	43, 44	0	63.98	9.54	-147.36	-134.44	-3.59	-4.64
			49	63.16	9.54	-182.90	-20.47	-1.32	-4.68
			97	62.38	9.54	-173.90	50.34	0.96	-4.71
106	Fondazio ne	43, 44	0	57.99	-0.02	-167.26	1.05	0.96	1.05
			49	57.26	-0.01	-156.23	38.90	0.46	1.02
			97	56.58	-0.01	-132.88	53.20	-0.03	0.99
107	Fondazio ne	43, 44	0	55.15	-0.53	-114.89	38.77	-0.03	-0.05
			49	54.51	-0.53	-95.67	37.63	0.00	-0.07
			97	53.91	-0.53	-79.49	27.26	0.04	-0.08
108	Fondazio ne	43, 44	0	55.19	-1.07	-61.96	41.80	0.04	0.06
			49	54.64	-1.07	-44.99	27.04	0.01	0.06
			97	54.13	-1.07	-35.60	11.11	-0.02	0.07
109	Fondazio ne	43, 44	0	55.29	-0.25	-23.67	30.12	-0.02	0.01
			49	54.82	-0.25	-12.62	15.19	-0.03	0.03
			97	54.39	-0.25	-8.36	2.38	-0.05	0.06
110	Fondazio ne	43, 44	0	55.37	-0.03	-2.00	15.68	-0.05	-0.02
			49	54.99	-0.03	3.12	5.53	-0.05	0.02
			97	54.65	-0.03	3.95	-1.97	-0.07	0.06
111	Fondazio ne	43, 44	0	55.24	-0.06	6.24	5.44	-0.06	-0.04
			49	54.94	-0.06	7.62	0.38	-0.06	0.01
			97	54.69	-0.06	7.05	-2.64	-0.07	0.07
112	Fondazio ne	43, 44	0	54.91	-0.07	7.29	-0.03	-0.07	-0.06
			49	54.70	-0.07	6.92	-1.42	-0.06	0.01
			97	54.53	-0.07	6.18	-1.60	-0.08	0.07
113	Fondazio ne	43, 44	0	54.47	-0.05	5.79	-1.86	-0.08	-0.07
			49	54.35	-0.05	5.04	-1.20	-0.06	0.00
			97	54.27	-0.05	4.75	0.00	-0.08	0.07
114	Fondazio ne	43, 44	0	53.97	0.01	4.51	-1.54	-0.08	-0.07
			49	53.93	0.01	4.11	-0.09	-0.06	0.01
			97	53.94	0.01	4.43	1.36	-0.09	0.09
115	Fondazio ne	43, 44	0	53.52	0.06	4.56	-0.20	-0.09	-0.09
			49	53.56	0.06	4.77	1.01	-0.06	-0.01
			97	53.65	0.06	5.44	1.73	-0.08	0.07
116	Fondazio ne	43, 44	0	52.94	0.15	5.73	1.32	-0.08	-0.07
			49	53.07	0.15	6.37	1.24	-0.06	0.00
			97	53.25	0.15	6.69	0.02	-0.08	0.08
117	Fondazio ne	43, 44	0	52.20	0.29	6.40	2.37	-0.08	-0.08
			49	52.41	0.29	6.92	-0.37	-0.06	-0.01
			97	52.66	0.29	5.64	-5.01	-0.08	0.06
118	Fondazio ne	43, 44	0	51.12	0.47	3.54	1.76	-0.08	-0.07
			49	51.42	0.47	2.76	-5.12	-0.06	-0.01
			97	51.75	0.47	-1.97	-14.46	-0.06	0.05
119	Fondazio ne	43, 44	0	49.57	0.58	-7.52	-1.92	-0.07	-0.07
			49	49.95	0.58	-11.31	-13.70	-0.05	-0.02
			97	50.36	0.58	-21.34	-27.45	-0.05	0.02
120	Fondazio ne	43, 44	0	47.48	0.73	-31.53	-10.34	-0.05	-0.10
			49	47.93	0.73	-40.23	-25.04	-0.01	-0.06
			97	48.42	0.73	-55.95	-38.77	0.01	-0.04
121	Fondazio ne	43, 44	0	45.11	0.33	-70.74	-25.13	0.01	0.11
			49	45.64	0.33	-85.72	-35.00	-0.05	0.13
			97	46.20	0.33	-103.72	-36.68	-0.11	0.14
122	Fondazio ne	43, 44	0	42.67	-0.24	-116.34	-37.95	-0.12	-0.74
			49	43.26	-0.24	-132.70	-25.90	0.24	-0.74

			97	43.90	-0.24	-138.47	6.90	0.60	-0.74
123	Fondazio ne	43, 44	0	43.93	2.26	-138.39	-57.57	0.60	0.71
			49	44.59	2.26	-152.96	3.81	0.26	0.70
			97	45.29	2.26	-129.01	102.19	-0.08	0.69
124	Fondazio ne	43, 45	0	21.80	-54.19	72.47	-269.93	2.86	15.63
			33	21.83	-54.18	-1.11	-176.14	-2.21	15.07
			66	21.87	-54.17	-43.89	-83.25	-7.09	14.51
125	Fondazio ne	43, 45	0	21.82	50.93	-20.77	15.85	-7.09	-23.53
			33	21.87	50.94	-0.31	108.13	0.77	-24.09
			66	21.92	50.95	50.54	200.05	8.81	-24.66
126	Fondazio ne	44, 46	0	8.70	27.72	19.85	-157.05	-3.78	-15.99
			33	8.71	27.71	-18.57	-75.82	1.42	-15.50
			66	8.72	27.70	-30.16	5.71	6.45	-15.02
127	Fondazio ne	44, 46	0	15.02	-76.49	-43.73	81.64	6.45	22.92
			33	15.03	-76.50	-3.25	163.92	-1.19	23.41
			66	15.05	-76.51	64.57	247.29	-9.00	23.93
128	Fondazio ne	45, 47	0	8.62	-69.96	55.34	-230.99	7.87	24.66
			33	8.68	-69.95	-5.83	-139.80	-0.17	24.09
			66	8.74	-69.94	-37.07	-49.66	-8.03	23.54
129	Fondazio ne	45, 47	0	11.71	48.12	-23.80	19.57	-8.03	-23.34
			33	11.78	48.13	-2.59	108.99	-0.24	-23.89
			66	11.85	48.14	48.06	197.95	7.74	-24.45
130	Fondazio ne	46, 48	0	2.85	53.61	55.47	-197.28	-8.09	-24.03
			33	2.87	53.60	4.22	-113.20	-0.25	-23.51
			66	2.90	53.58	-19.23	-28.89	7.43	-23.00
131	Fondazio ne	46, 48	0	9.10	-60.76	-18.86	30.59	7.43	21.80
			33	9.13	-60.78	5.19	115.27	0.15	22.32
			66	9.15	-60.79	57.26	200.42	-7.30	22.84
132	Fondazio ne	47, 49	0	28.90	-65.50	50.92	-201.08	8.65	25.02
			33	28.98	-65.49	-0.88	-112.91	0.49	24.46
			66	29.07	-65.47	-23.76	-25.85	-7.50	23.92
133	Fondazio ne	47, 49	0	33.52	45.55	-18.44	22.44	-7.50	-24.28
			33	33.62	45.56	3.17	108.57	0.60	-24.82
			66	33.73	45.57	53.08	193.91	8.88	-25.36
134	Fondazio ne	48, 50	0	25.24	60.37	60.59	-200.30	-8.24	-24.16
			33	25.28	60.35	8.55	-115.15	-0.35	-23.64
			66	25.32	60.34	-15.48	-30.51	7.36	-23.12
135	Fondazio ne	48, 50	0	31.71	-51.07	-14.65	29.25	7.36	24.35
			33	31.77	-51.08	8.89	113.43	-0.76	24.86
			66	31.83	-51.09	60.15	197.19	-9.04	25.38
136	Fondazio ne	49, 51	0	19.33	-73.96	62.76	-210.69	8.00	24.82
			33	19.45	-73.95	7.13	-126.57	-0.10	24.28
			66	19.58	-73.93	-21.02	-44.16	-8.02	23.77
137	Fondazio ne	49, 51	0	25.29	38.70	-10.34	6.11	-8.02	-24.80
			33	25.43	38.72	5.02	86.88	0.24	-25.30
			66	25.57	38.73	46.78	166.09	8.68	-25.81
138	Fondazio ne	50, 52	0	16.49	73.81	69.67	-216.55	-8.18	-25.18
			33	16.57	73.80	11.89	-133.76	0.04	-24.66
			66	16.65	73.79	-18.81	-52.52	8.10	-24.17
139	Fondazio ne	50, 52	0	23.38	-39.96	-8.14	11.00	8.09	25.74
			33	23.47	-39.97	8.66	90.68	-0.48	26.22
			66	23.56	-39.98	51.51	168.83	-9.22	26.71
140	Fondazio ne	51, 53	0	38.51	-90.61	63.74	-202.26	9.79	26.84
			33	38.67	-90.60	9.77	-125.04	1.02	26.34
			66	38.84	-90.59	-19.12	-50.33	-7.60	25.88

141	Fondazio ne	51, 53	0	44.22	18.86	2.35	2.38	-7.60	-27.52
			33	44.40	18.87	15.09	74.59	1.56	-27.97
			66	44.61	18.88	51.22	144.20	10.86	-28.40
142	Fondazio ne	52, 54	0	26.09	92.23	69.89	-214.70	-9.34	-26.54
			33	26.20	92.22	11.65	-138.58	-0.66	-26.06
			66	26.31	92.21	-21.90	-65.08	7.86	-25.61
143	Fondazio ne	52, 54	0	30.78	-19.46	0.59	-7.14	7.86	27.20
			33	30.90	-19.47	9.98	63.76	-1.19	27.64
			66	31.04	-19.48	42.33	132.01	-10.38	28.06
144	Fondazio ne	53, 55	0	27.56	-122.44	82.48	-240.74	9.41	23.42
			33	27.78	-122.43	14.06	-174.32	1.76	23.01
			66	28.00	-122.42	-33.07	-111.77	-5.78	22.66
145	Fondazio ne	53, 55	0	28.93	-33.03	7.41	-70.51	-5.77	-17.65
			33	29.16	-33.03	-6.10	-11.78	0.11	-17.96
			66	29.41	-33.02	-0.86	43.21	6.08	-18.23
146	Fondazio ne	54, 56	0	31.22	120.86	75.38	-233.33	-9.95	-24.19
			33	31.37	120.85	9.20	-168.20	-2.04	-23.79
			66	31.52	120.84	-36.09	-106.74	5.75	-23.44
147	Fondazio ne	54, 56	0	30.88	29.71	4.31	-59.27	5.75	17.70
			33	31.05	29.71	-5.63	-1.40	-0.15	18.01
			66	31.23	29.70	2.95	53.02	-6.14	18.29
148	Fondazio ne	55, 57	0	23.40	-105.05	41.86	-180.49	3.83	6.06
			40	23.71	-105.04	-17.58	-119.23	1.48	5.80
			80	24.04	-105.03	-53.78	-63.45	-0.78	5.62
149	Fondazio ne	55, 57	0	23.59	-46.95	-15.65	-66.15	-0.77	-5.22
			40	23.92	-46.94	-31.70	-14.94	1.32	-5.31
			80	24.27	-46.94	-28.14	32.65	3.44	-5.30
150	Fondazio ne	56, 70	0	24.36	103.83	46.38	-186.08	-3.85	-6.16
			40	24.59	103.82	-15.35	-125.21	-1.46	-5.88
			80	24.83	103.81	-53.95	-69.57	0.83	-5.69
151	Fondazio ne	56, 70	0	23.28	45.89	-14.34	-67.82	0.82	5.21
			40	23.54	45.89	-31.02	-16.55	-1.28	5.32
			80	23.80	45.88	-28.05	31.28	-3.40	5.34
152	Fondazio ne	57, 58	0	-20.92	23.06	-18.09	-65.35	-2.26	-0.18
			42	-20.89	23.06	-35.98	-22.50	-2.11	-0.50
			83	-20.87	23.06	-38.16	10.42	-1.86	-0.71
153	Fondazio ne	57, 58	0	-19.07	23.52	-67.13	27.88	-1.85	1.23
			42	-19.06	23.52	-50.19	52.34	-2.33	1.10
			83	-19.07	23.52	-24.51	70.26	-2.77	1.03
154	Fondazio ne	58, 59	0	-27.42	21.06	-39.63	-4.68	-2.26	-2.88
			35	-27.43	21.06	-39.26	6.28	-1.26	-2.90
			69	-27.45	21.06	-35.60	14.51	-0.27	-2.89
155	Fondazio ne	58, 59	0	-17.80	7.72	-43.52	37.03	-0.26	1.03
			35	-17.83	7.72	-29.61	43.31	-0.62	1.06
			69	-17.87	7.72	-13.76	48.36	-1.00	1.11
156	Fondazio ne	59, 60	0	-10.06	6.44	-17.89	0.09	-0.87	-1.06
			35	-10.11	6.45	-17.09	4.38	-0.51	-0.99
			69	-10.16	6.45	-14.89	8.25	-0.19	-0.91
157	Fondazio ne	59, 60	0	-3.47	1.06	-16.52	20.23	-0.18	0.17
			35	-3.52	1.06	-8.87	24.03	-0.26	0.26
			69	-3.58	1.06	0.10	27.99	-0.37	0.36
158	Fondazio ne	60, 61	0	1.95	-0.51	1.05	-9.50	-0.32	-0.30
			35	1.90	-0.51	-1.50	-5.27	-0.23	-0.19
			69	1.85	-0.51	-2.53	-0.75	-0.19	-0.07
159	Fondazio	60, 61	0	5.11	-2.23	-0.88	5.35	-0.18	-0.14

	ne								
			35	5.06	-2.22	1.81	10.19	-0.16	-0.02
			69	5.01	-2.22	6.21	15.34	-0.17	0.10
160	Fondazio ne	61, 62	0	10.85	-3.16	8.22	-17.46	-0.17	-0.20
			35	10.80	-3.16	3.13	-12.08	-0.12	-0.07
			69	10.76	-3.16	-0.08	-6.56	-0.12	0.06
161	Fondazio ne	61, 62	0	12.98	-3.07	2.08	-3.02	-0.12	-0.17
			35	12.94	-3.06	2.01	2.60	-0.08	-0.03
			69	12.91	-3.06	3.89	8.28	-0.10	0.11
162	Fondazio ne	62, 63	0	13.17	-2.68	5.77	-16.62	-0.10	-0.12
			35	13.15	-2.67	1.02	-10.94	-0.08	0.03
			69	13.13	-2.67	-1.77	-5.31	-0.12	0.18
163	Fondazio ne	62, 63	0	14.34	-1.76	-0.35	-3.38	-0.12	-0.18
			35	14.32	-1.76	-0.55	2.20	-0.08	-0.03
			69	14.31	-1.76	1.17	7.73	-0.10	0.12
164	Fondazio ne	63, 64	0	14.99	-0.58	1.92	-11.70	-0.10	-0.16
			35	14.99	-0.58	-1.17	-6.20	-0.07	-0.01
			69	14.99	-0.58	-2.37	-0.75	-0.09	0.14
165	Fondazio ne	63, 64	0	15.18	0.57	-2.37	0.65	-0.09	-0.15
			35	15.18	0.57	-1.21	6.11	-0.07	0.00
			69	15.20	0.57	1.84	11.59	-0.10	0.16
166	Fondazio ne	64, 65	0	14.89	1.74	1.12	-7.90	-0.09	-0.13
			35	14.91	1.74	-0.66	-2.38	-0.07	0.02
			69	14.94	1.74	-0.53	3.16	-0.11	0.17
167	Fondazio ne	64, 65	0	14.11	2.68	-1.96	5.10	-0.11	-0.19
			35	14.15	2.68	0.76	10.70	-0.07	-0.03
			69	14.18	2.68	5.42	16.35	-0.08	0.12
168	Fondazio ne	65, 66	0	14.03	3.08	3.54	-8.09	-0.08	-0.12
			35	14.07	3.08	1.72	-2.44	-0.06	0.03
			69	14.12	3.08	1.84	3.17	-0.10	0.17
169	Fondazio ne	65, 66	0	12.28	3.18	-0.35	6.91	-0.10	-0.12
			35	12.34	3.18	2.98	12.44	-0.08	0.03
			69	12.39	3.18	8.20	17.86	-0.11	0.17
170	Fondazio ne	66, 67	0	6.54	2.15	6.22	-15.79	-0.12	-0.05
			35	6.60	2.15	1.66	-10.59	-0.12	0.09
			69	6.66	2.15	-1.15	-5.67	-0.18	0.23
171	Fondazio ne	66, 67	0	3.10	0.60	-2.69	0.56	-0.18	-0.01
			35	3.17	0.60	-1.70	5.19	-0.20	0.12
			69	3.23	0.60	0.84	9.57	-0.26	0.25
172	Fondazio ne	67, 68	0	-1.68	-0.99	0.22	-26.98	-0.32	-0.36
			35	-1.61	-0.99	-8.38	-22.84	-0.21	-0.24
			69	-1.55	-0.99	-15.58	-18.82	-0.15	-0.12
173	Fondazio ne	67, 68	0	-7.86	-6.46	-14.66	-7.90	-0.15	0.86
			35	-7.80	-6.46	-16.69	-3.79	-0.47	0.96
			69	-7.73	-6.46	-17.25	0.74	-0.82	1.06
174	Fondazio ne	68, 69	0	-15.61	-7.36	-13.93	-47.54	-0.96	-1.15
			35	-15.55	-7.36	-29.46	-42.25	-0.57	-1.06
			69	-15.50	-7.36	-42.97	-35.71	-0.22	-1.00
175	Fondazio ne	68, 69	0	-24.99	-20.68	-35.57	-13.97	-0.22	2.77
			35	-24.94	-20.68	-39.01	-5.49	-1.19	2.82
			69	-24.91	-20.68	-39.07	5.71	-2.17	2.85
176	Fondazio ne	69, 70	0	-18.17	-22.20	-25.07	-69.84	-2.70	-1.07
			42	-18.14	-22.20	-50.52	-51.64	-2.26	-1.07
			83	-18.12	-22.20	-67.11	-26.91	-1.80	-1.13
177	Fondazio ne	69, 70	0	-20.91	-22.54	-39.78	-7.84	-1.81	1.02

			42	-20.90	-22.54	-36.47	25.36	-2.21	0.88
			83	-20.90	-22.54	-17.34	68.52	-2.53	0.65
178	Primo Impalcato	1, 2	0	108.90	0.08	20.36	-15.48	62.05	34.79
			83	108.90	0.08	7.49	-15.48	33.13	34.79
			166	108.90	0.08	-5.38	-15.48	4.21	34.79
179	Primo Impalcato	1, 15	0	25.37	4.34	-14.20	15.57	-73.77	-85.12
			80	25.37	4.34	-1.82	15.57	-6.10	-85.12
			159	25.37	4.34	10.56	15.57	61.57	-85.12
180	Primo Impalcato	2, 3	0	101.35	-0.09	-4.16	-1.60	5.22	6.89
			69	101.35	-0.09	-5.27	-1.60	0.47	6.89
			138	101.35	-0.09	-6.37	-1.60	-4.29	6.89
181	Primo Impalcato	3, 4	0	101.17	-0.11	-5.82	3.52	-4.04	-0.78
			69	101.17	-0.11	-3.39	3.52	-3.50	-0.78
			138	101.17	-0.11	-0.96	3.52	-2.96	-0.78
182	Primo Impalcato	4, 5	0	100.99	-0.05	-0.80	0.37	-2.87	-1.43
			69	100.99	-0.05	-0.54	0.37	-1.88	-1.43
			138	100.99	-0.05	-0.29	0.37	-0.90	-1.43
183	Primo Impalcato	5, 6	0	100.86	-0.01	-0.20	-0.23	-0.89	-0.64
			69	100.86	-0.01	-0.36	-0.23	-0.45	-0.64
			138	100.86	-0.01	-0.51	-0.23	-0.01	-0.64
184	Primo Impalcato	6, 7	0	104.37	0.00	-0.47	0.33	0.00	-0.14
			69	104.37	0.00	-0.24	0.33	0.09	-0.14
			138	104.37	0.00	0.00	0.33	0.19	-0.14
185	Primo Impalcato	7, 8	0	97.76	0.00	0.02	-0.45	0.18	0.00
			69	97.76	0.00	-0.29	-0.45	0.18	0.00
			138	97.76	0.00	-0.60	-0.45	0.18	0.00
186	Primo Impalcato	8, 9	0	97.78	0.00	-0.61	0.51	0.18	0.15
			69	97.78	0.00	-0.25	0.51	0.08	0.15
			138	97.78	0.00	0.10	0.51	-0.03	0.15
187	Primo Impalcato	9, 10	0	107.43	0.01	0.07	-0.41	0.00	0.65
			69	107.43	0.01	-0.21	-0.41	-0.45	0.65
			138	107.43	0.01	-0.50	-0.41	-0.89	0.65
188	Primo Impalcato	10, 11	0	104.49	0.05	-0.55	-0.19	-0.94	1.44
			69	104.49	0.05	-0.68	-0.19	-1.93	1.44
			138	104.49	0.05	-0.81	-0.19	-2.93	1.44
189	Primo Impalcato	11, 12	0	104.68	0.11	-0.95	-3.60	-3.02	0.74
			69	104.68	0.11	-3.43	-3.60	-3.53	0.74
			138	104.68	0.11	-5.92	-3.60	-4.04	0.74
190	Primo Impalcato	12, 13	0	104.86	0.10	-6.45	2.14	-4.29	-7.11
			69	104.86	0.10	-4.98	2.14	0.62	-7.11
			138	104.86	0.10	-3.50	2.14	5.52	-7.11
191	Primo Impalcato	13, 14	0	112.24	-0.09	-4.68	12.55	4.51	-35.47
			83	112.24	-0.09	5.75	12.55	33.99	-35.47
			166	112.24	-0.09	16.18	12.55	63.47	-35.47
192	Primo Impalcato	14, 16	0	23.62	-4.23	-14.67	15.71	67.77	79.46
			80	23.62	-4.23	-2.18	15.71	4.59	79.46
			159	23.62	-4.23	10.31	15.71	-58.58	79.46
193	Primo Impalcato	15, 17	0	-2.93	0.30	4.80	2.54	55.69	27.89
			66	-2.93	0.30	6.47	2.54	37.28	27.89
			132	-2.93	0.30	8.15	2.54	18.87	27.89
194	Primo Impalcato	16, 18	0	-5.24	-0.39	3.38	4.17	-52.76	-25.90
			66	-5.24	-0.39	6.14	4.17	-35.67	-25.90
			132	-5.24	-0.39	8.89	4.17	-18.57	-25.90
195	Primo Impalcato	17, 19	0	12.38	0.00	4.57	-0.35	17.41	13.76
			66	12.38	0.00	4.34	-0.35	8.33	13.76

			132	12.38	0.00	4.10	-0.35	-0.75	13.76
196	Primo Impalcato	18, 20	0	8.53	-0.01	5.22	-1.66	-18.91	-14.75
			66	8.53	-0.01	4.12	-1.66	-9.17	-14.75
			132	8.53	-0.01	3.03	-1.66	0.56	-14.75
197	Primo Impalcato	19, 21	0	-14.29	-0.05	2.31	1.07	0.05	1.07
			66	-14.29	-0.05	3.02	1.07	-0.65	1.07
			132	-14.29	-0.05	3.72	1.07	-1.36	1.07
198	Primo Impalcato	20, 22	0	-19.92	0.04	0.40	3.33	-0.19	-1.17
			66	-19.92	0.04	2.60	3.33	0.59	-1.17
			132	-19.92	0.04	4.80	3.33	1.36	-1.17
199	Primo Impalcato	21, 23	0	11.73	-0.01	3.23	-0.31	-1.66	-0.90
			66	11.73	-0.01	3.02	-0.31	-1.07	-0.90
			132	11.73	-0.01	2.82	-0.31	-0.47	-0.90
200	Primo Impalcato	22, 24	0	2.10	0.01	4.22	-2.04	1.80	0.94
			66	2.10	0.01	2.88	-2.04	1.18	0.94
			132	2.10	0.01	1.54	-2.04	0.56	0.94
201	Primo Impalcato	23, 25	0	-9.92	0.02	3.51	-4.87	0.03	0.16
			66	-9.92	0.02	0.30	-4.87	-0.07	0.16
			132	-9.92	0.02	-2.91	-4.87	-0.18	0.16
202	Primo Impalcato	24, 26	0	-21.03	-0.02	0.38	-1.01	0.07	-0.06
			66	-21.03	-0.02	-0.29	-1.01	0.10	-0.06
			132	-21.03	-0.02	-0.95	-1.01	0.14	-0.06
203	Primo Impalcato	25, 28	0	22.56	-0.01	-2.11	-0.83	-0.70	-0.22
			85	22.56	-0.01	-2.81	-0.83	-0.52	-0.22
			170	22.56	-0.01	-3.52	-0.83	-0.33	-0.22
204	Primo Impalcato	26, 27	0	0.93	0.02	-1.25	1.79	0.61	0.43
			66	0.93	0.02	-0.06	1.79	0.33	0.43
			132	0.93	0.02	1.12	1.79	0.05	0.43
205	Primo Impalcato	27, 29	0	-20.50	0.01	-2.28	3.04	-0.37	0.01
			66	-20.50	0.01	-0.27	3.04	-0.37	0.01
			132	-20.50	0.01	1.73	3.04	-0.38	0.01
206	Primo Impalcato	28, 30	0	-8.36	-0.01	-0.64	0.69	0.15	-0.04
			73	-8.36	-0.01	-0.14	0.69	0.18	-0.04
			146	-8.36	-0.01	0.37	0.69	0.20	-0.04
207	Primo Impalcato	29, 31	0	1.41	0.01	-0.03	1.65	0.07	-0.05
			66	1.41	0.01	1.06	1.65	0.11	-0.05
			132	1.41	0.01	2.14	1.65	0.14	-0.05
208	Primo Impalcato	30, 32	0	-11.86	0.00	4.42	-4.83	0.16	0.06
			69	-11.86	0.00	1.11	-4.83	0.12	0.06
			137	-11.86	0.00	-2.21	-4.83	0.08	0.06
209	Primo Impalcato	31, 33	0	-17.72	0.01	-2.32	3.16	-0.30	-0.05
			66	-17.72	0.01	-0.23	3.16	-0.27	-0.05
			132	-17.72	0.01	1.85	3.16	-0.24	-0.05
210	Primo Impalcato	32, 34	0	-15.64	0.01	2.62	-3.79	0.05	0.04
			69	-15.64	0.01	0.01	-3.79	0.02	0.04
			138	-15.64	0.01	-2.61	-3.79	0.00	0.04
211	Primo Impalcato	33, 35	0	8.31	0.01	-1.91	3.56	0.21	-0.01
			66	8.31	0.01	0.45	3.56	0.22	-0.01
			132	8.31	0.01	2.80	3.56	0.23	-0.01
212	Primo Impalcato	34, 36	0	-19.82	0.01	2.77	-4.27	-0.03	0.00
			69	-19.82	0.01	-0.18	-4.27	-0.03	0.00
			138	-19.82	0.01	-3.13	-4.27	-0.03	0.00
213	Primo Impalcato	35, 37	0	-9.79	0.01	-2.23	3.53	-0.23	-0.01
			66	-9.79	0.01	0.10	3.53	-0.22	-0.01
			132	-9.79	0.01	2.43	3.53	-0.21	-0.01

214	Primo Impalcato	36, 38	0	-24.46	0.01	2.69	-4.61	-0.07	-0.01
			69	-24.46	0.01	-0.49	-4.61	-0.06	-0.01
			138	-24.46	0.01	-3.67	-4.61	-0.05	-0.01
215	Primo Impalcato	37, 39	0	18.22	0.00	-2.00	1.37	0.24	0.01
			66	18.22	0.00	-1.09	1.37	0.24	0.01
			132	18.22	0.00	-0.18	1.37	0.23	0.01
216	Primo Impalcato	38, 40	0	-29.60	0.00	2.48	-4.38	-0.09	-0.15
			69	-29.60	0.00	-0.52	-4.38	0.01	-0.15
			137	-29.60	0.00	-3.52	-4.38	0.11	-0.15
217	Primo Impalcato	39, 41	0	-4.46	0.01	-3.50	7.31	-0.22	0.07
			66	-4.46	0.01	1.32	7.31	-0.27	0.07
			132	-4.46	0.01	6.15	7.31	-0.32	0.07
218	Primo Impalcato	40, 42	0	-35.18	-0.02	2.84	-0.10	0.07	-0.43
			69	-35.18	-0.02	2.77	-0.10	0.37	-0.43
			138	-35.18	-0.02	2.70	-0.10	0.67	-0.43
219	Primo Impalcato	41, 44	0	2.08	-0.02	2.30	-4.33	-0.36	-0.54
			66	2.08	-0.02	-0.56	-4.33	0.00	-0.54
			132	2.08	-0.02	-3.42	-4.33	0.36	-0.54
220	Primo Impalcato	42, 43	0	-41.17	0.05	10.44	-26.72	0.66	0.79
			23	-41.17	0.05	4.29	-26.72	0.48	0.79
			46	-41.17	0.05	-1.85	-26.72	0.30	0.79
221	Primo Impalcato	43, 45	0	-13.54	-0.01	-1.06	1.51	-0.14	0.03
			66	-13.54	-0.01	-0.07	1.51	-0.17	0.03
			132	-13.54	-0.01	0.92	1.51	-0.19	0.03
222	Primo Impalcato	44, 46	0	23.01	0.02	-3.88	4.35	0.78	0.52
			66	23.01	0.02	-1.01	4.35	0.43	0.52
			132	23.01	0.02	1.86	4.35	0.09	0.52
223	Primo Impalcato	45, 47	0	-35.38	0.00	1.81	-1.98	0.31	0.36
			66	-35.38	0.00	0.50	-1.98	0.07	0.36
			132	-35.38	0.00	-0.81	-1.98	-0.17	0.36
224	Primo Impalcato	46, 48	0	1.43	0.00	-1.45	3.29	-0.34	-0.32
			66	1.43	0.00	0.73	3.29	-0.13	-0.32
			132	1.43	0.00	2.90	3.29	0.09	-0.32
225	Primo Impalcato	47, 49	0	-7.08	0.01	0.30	2.65	-0.63	0.93
			66	-7.08	0.01	2.05	2.65	-1.24	0.93
			132	-7.08	0.01	3.79	2.65	-1.85	0.93
226	Primo Impalcato	48, 50	0	25.67	-0.02	3.06	-1.74	0.50	-1.02
			66	25.67	-0.02	1.91	-1.74	1.17	-1.02
			132	25.67	-0.02	0.77	-1.74	1.84	-1.02
227	Primo Impalcato	49, 51	0	-27.82	0.04	5.68	-4.89	-1.53	-1.11
			66	-27.82	0.04	2.45	-4.89	-0.79	-1.11
			132	-27.82	0.04	-0.77	-4.89	-0.06	-1.11
228	Primo Impalcato	50, 52	0	2.02	-0.04	1.80	2.82	1.57	1.33
			66	2.02	-0.04	3.66	2.82	0.69	1.33
			132	2.02	-0.04	5.52	2.82	-0.19	1.33
229	Primo Impalcato	51, 53	0	2.88	-0.01	2.16	2.18	-0.85	-13.74
			66	2.88	-0.01	3.60	2.18	8.22	-13.74
			132	2.88	-0.01	5.03	2.18	17.29	-13.74
230	Primo Impalcato	52, 54	0	1.44	0.00	7.68	-3.37	0.30	13.73
			66	1.44	0.00	5.46	-3.37	-8.76	13.73
			132	1.44	0.00	3.24	-3.37	-17.83	13.73
231	Primo Impalcato	53, 55	0	-9.57	-0.29	9.48	-4.70	18.74	-28.08
			66	-9.57	-0.29	6.38	-4.70	37.27	-28.08
			132	-9.57	-0.29	3.28	-4.70	55.81	-28.08
232	Primo	54, 56	0	-1.35	0.35	8.84	-5.47	-19.28	27.40

	Impalcato								
			66	-1.35	0.35	5.23	-5.47	-37.37	27.40
			132	-1.35	0.35	1.63	-5.47	-55.45	27.40
233	Primo Impalcato	55, 57	0	21.90	-4.35	9.84	-15.88	61.70	85.21
			80	21.90	-4.35	-2.78	-15.88	-6.04	85.21
			159	21.90	-4.35	-15.40	-15.88	-73.78	85.21
234	Primo Impalcato	56, 70	0	24.88	4.24	9.20	-14.11	-53.88	-74.38
			80	24.88	4.24	-2.02	-14.11	5.25	-74.38
			159	24.88	4.24	-13.24	-14.11	64.39	-74.38
235	Primo Impalcato	57, 58	0	109.60	-0.07	20.52	-15.62	-62.02	-34.74
			83	109.60	-0.07	7.53	-15.62	-33.14	-34.74
			166	109.60	-0.07	-5.46	-15.62	-4.26	-34.74
236	Primo Impalcato	58, 59	0	103.04	0.09	-4.24	-1.65	-5.26	-6.88
			69	103.04	0.09	-5.38	-1.65	-0.51	-6.88
			138	103.04	0.09	-6.52	-1.65	4.24	-6.88
237	Primo Impalcato	59, 60	0	102.88	0.11	-5.98	3.68	3.99	0.76
			69	102.88	0.11	-3.44	3.68	3.47	0.76
			138	102.88	0.11	-0.90	3.68	2.95	0.76
238	Primo Impalcato	60, 61	0	102.71	0.05	-0.76	0.15	2.85	1.42
			69	102.71	0.05	-0.66	0.15	1.88	1.42
			138	102.71	0.05	-0.56	0.15	0.90	1.42
239	Primo Impalcato	61, 62	0	106.15	0.01	-0.50	0.49	0.86	0.63
			69	106.15	0.01	-0.16	0.49	0.42	0.63
			138	106.15	0.01	0.18	0.49	-0.01	0.63
240	Primo Impalcato	62, 63	0	96.96	0.00	0.22	-0.52	0.02	0.15
			69	96.96	0.00	-0.14	-0.52	-0.09	0.15
			138	96.96	0.00	-0.50	-0.52	-0.19	0.15
241	Primo Impalcato	63, 64	0	96.95	0.00	-0.47	-0.01	-0.19	0.00
			69	96.95	0.00	-0.47	-0.01	-0.19	0.00
			138	96.95	0.00	-0.48	-0.01	-0.19	0.00
242	Primo Impalcato	64, 65	0	96.98	0.00	-0.50	0.48	-0.20	-0.16
			69	96.98	0.00	-0.17	0.48	-0.09	-0.16
			138	96.98	0.00	0.16	0.48	0.02	-0.16
243	Primo Impalcato	65, 66	0	107.03	-0.01	0.13	-0.47	-0.01	-0.66
			69	107.03	-0.01	-0.20	-0.47	0.45	-0.66
			138	107.03	-0.01	-0.52	-0.47	0.90	-0.66
244	Primo Impalcato	66, 67	0	104.35	-0.05	-0.57	-0.15	0.94	-1.49
			69	104.35	-0.05	-0.68	-0.15	1.97	-1.49
			138	104.35	-0.05	-0.78	-0.15	3.00	-1.49
245	Primo Impalcato	67, 68	0	104.55	-0.11	-0.92	-3.62	3.10	-0.81
			69	104.55	-0.11	-3.42	-3.62	3.66	-0.81
			138	104.55	-0.11	-5.93	-3.62	4.22	-0.81
246	Primo Impalcato	68, 69	0	104.74	-0.10	-6.46	2.09	4.48	7.19
			69	104.74	-0.10	-5.02	2.09	-0.48	7.19
			138	104.74	-0.10	-3.58	2.09	-5.45	7.19
247	Primo Impalcato	69, 70	0	112.47	0.07	-4.76	12.90	-4.39	36.28
			83	112.47	0.07	5.96	12.90	-34.55	36.28
			166	112.47	0.07	16.69	12.90	-64.70	36.28
248	Primo Impalcato	1	0	-81.01	-5.42	5.23	-2.34	-14.35	-12.28
			188	-81.01	-5.42	0.82	-2.34	8.75	-12.28
			376	-81.01	-5.42	-3.58	-2.34	31.84	-12.28
249	Primo Impalcato	2	0	-143.50	0.12	-23.58	13.92	-0.48	-0.24
			188	-143.50	0.12	2.58	13.92	-0.02	-0.24
			376	-143.50	0.12	28.74	13.92	0.43	-0.24
250	Primo Impalcato	3	0	-100.84	0.13	-8.31	5.60	-0.10	-0.03

			188	-100.84	0.13	2.22	5.60	-0.04	-0.03
			376	-100.84	0.13	12.76	5.60	0.02	-0.03
251	Primo Impalcato	4	0	-69.98	0.05	-0.32	0.96	0.09	0.06
			188	-69.98	0.05	1.48	0.96	-0.02	0.06
			376	-69.98	0.05	3.28	0.96	-0.13	0.06
252	Primo Impalcato	5	0	-48.23	0.01	1.47	-0.22	0.08	0.05
			188	-48.23	0.01	1.06	-0.22	-0.02	0.05
			376	-48.23	0.01	0.65	-0.22	-0.11	0.05
253	Primo Impalcato	6	0	-35.06	0.00	1.16	-0.15	0.04	0.03
			188	-35.06	0.00	0.89	-0.15	-0.01	0.03
			376	-35.06	0.00	0.62	-0.15	-0.06	0.03
254	Primo Impalcato	7	0	-31.75	0.00	0.78	0.03	0.01	0.00
			188	-31.75	0.00	0.83	0.03	0.00	0.00
			376	-31.75	0.00	0.88	0.03	-0.01	0.00
255	Primo Impalcato	8	0	-31.44	0.00	0.78	0.01	-0.02	-0.01
			188	-31.44	0.00	0.81	0.01	0.00	-0.01
			376	-31.44	0.00	0.84	0.01	0.02	-0.01
256	Primo Impalcato	9	0	-35.58	0.00	1.16	-0.16	-0.05	-0.03
			188	-35.58	0.00	0.87	-0.16	0.01	-0.03
			376	-35.58	0.00	0.58	-0.16	0.06	-0.03
257	Primo Impalcato	10	0	-45.74	-0.01	1.42	-0.20	-0.09	-0.06
			188	-45.74	-0.01	1.04	-0.20	0.01	-0.06
			376	-45.74	-0.01	0.66	-0.20	0.12	-0.06
258	Primo Impalcato	11	0	-68.74	-0.05	-0.40	0.99	-0.10	-0.07
			188	-68.74	-0.05	1.45	0.99	0.02	-0.07
			376	-68.74	-0.05	3.31	0.99	0.15	-0.07
259	Primo Impalcato	12	0	-101.54	-0.13	-8.53	5.72	0.09	0.03
			188	-101.54	-0.13	2.22	5.72	0.04	0.03
			376	-101.54	-0.13	12.96	5.72	-0.01	0.03
260	Primo Impalcato	13	0	-141.91	-0.12	-23.82	14.04	0.46	0.23
			188	-141.91	-0.12	2.57	14.04	0.02	0.23
			376	-141.91	-0.12	28.97	14.04	-0.42	0.23
261	Primo Impalcato	14	0	-84.40	5.59	6.04	-2.79	17.68	13.54
			188	-84.40	5.59	0.80	-2.79	-7.78	13.54
			376	-84.40	5.59	-4.44	-2.79	-33.24	13.54
262	Primo Impalcato	15	0	-304.32	-2.77	2.61	-1.26	46.39	70.83
			188	-304.32	-2.77	0.24	-1.26	-86.76	70.83
			376	-304.32	-2.77	-2.14	-1.26	-219.92	70.83
263	Primo Impalcato	16	0	-304.77	2.73	3.01	-1.48	-48.90	-71.22
			188	-304.77	2.73	0.23	-1.48	84.99	-71.22
			376	-304.77	2.73	-2.55	-1.48	218.89	-71.22
264	Primo Impalcato	17	0	-382.11	-0.40	1.56	-0.80	171.93	137.96
			188	-382.11	-0.40	0.07	-0.80	-87.44	137.96
			376	-382.11	-0.40	-1.43	-0.80	-346.81	137.96
265	Primo Impalcato	18	0	-385.68	0.46	2.03	-1.05	-170.51	-137.17
			188	-385.68	0.46	0.06	-1.05	87.36	-137.17
			376	-385.68	0.46	-1.91	-1.05	345.24	-137.17
266	Primo Impalcato	19	0	-411.81	0.13	0.67	-0.34	172.58	137.29
			188	-411.81	0.13	0.04	-0.34	-85.52	137.29
			376	-411.81	0.13	-0.59	-0.34	-343.61	137.29
267	Primo Impalcato	20	0	-413.60	-0.12	1.19	-0.61	-173.41	-137.63
			188	-413.60	-0.12	0.04	-0.61	85.34	-137.63
			376	-413.60	-0.12	-1.11	-0.61	344.09	-137.63
268	Primo Impalcato	21	0	-437.77	0.08	0.04	0.00	162.22	130.90
			188	-437.77	0.08	0.04	0.00	-83.87	130.90

			376	-437.77	0.08	0.05	0.00	-329.96	130.90
269	Primo Impalcato	22	0	-445.01	-0.08	0.65	-0.32	-162.61	-131.03
			188	-445.01	-0.08	0.04	-0.32	83.73	-131.03
			376	-445.01	-0.08	-0.56	-0.32	330.07	-131.03
270	Primo Impalcato	23	0	-464.54	0.02	-0.64	0.36	158.95	129.16
			188	-464.54	0.02	0.05	0.36	-83.87	129.16
			376	-464.54	0.02	0.73	0.36	-326.69	129.16
271	Primo Impalcato	24	0	-463.44	0.00	0.07	-0.02	-159.25	-129.15
			188	-463.44	0.00	0.02	-0.02	83.56	-129.15
			376	-463.44	0.00	-0.02	-0.02	326.37	-129.15
272	Primo Impalcato	25	0	-495.83	0.01	-0.66	0.37	159.55	130.76
			188	-495.83	0.01	0.03	0.37	-86.28	130.76
			376	-495.83	0.01	0.73	0.37	-332.11	130.76
273	Primo Impalcato	26	0	-480.47	0.00	0.20	-0.11	-160.05	-130.37
			188	-480.47	0.00	0.00	-0.11	85.05	-130.37
			376	-480.47	0.00	-0.20	-0.11	330.15	-130.37
274	Primo Impalcato	27	0	-460.34	0.02	0.31	-0.19	-159.98	-129.41
			188	-460.34	0.02	-0.05	-0.19	83.31	-129.41
			376	-460.34	0.02	-0.41	-0.19	326.60	-129.41
275	Primo Impalcato	28	0	-491.46	-0.03	0.14	-0.07	159.68	130.03
			188	-491.46	-0.03	0.01	-0.07	-84.78	130.03
			376	-491.46	-0.03	-0.12	-0.07	-329.24	130.03
276	Primo Impalcato	29	0	-449.75	0.00	0.32	-0.17	-160.66	-129.43
			188	-449.75	0.00	-0.01	-0.17	82.68	-129.43
			376	-449.75	0.00	-0.33	-0.17	326.02	-129.43
277	Primo Impalcato	30	0	-507.46	-0.02	0.14	-0.06	161.86	130.60
			188	-507.46	-0.02	0.03	-0.06	-83.66	130.60
			376	-507.46	-0.02	-0.08	-0.06	-329.19	130.60
278	Primo Impalcato	31	0	-445.51	0.01	0.12	-0.08	-160.90	-129.42
			188	-445.51	0.01	-0.02	-0.08	82.41	-129.42
			376	-445.51	0.01	-0.17	-0.08	325.73	-129.42
279	Primo Impalcato	32	0	-508.73	-0.01	-0.07	0.05	162.27	130.56
			188	-508.73	-0.01	0.02	0.05	-83.17	130.56
			376	-508.73	-0.01	0.11	0.05	-328.61	130.56
280	Primo Impalcato	33	0	-444.19	-0.01	0.16	-0.09	-161.00	-129.38
			188	-444.19	-0.01	-0.01	-0.09	82.23	-129.38
			376	-444.19	-0.01	-0.18	-0.09	325.47	-129.38
281	Primo Impalcato	34	0	-514.39	-0.01	-0.08	0.06	162.43	130.60
			188	-514.39	-0.01	0.03	0.06	-83.11	130.60
			376	-514.39	-0.01	0.14	0.06	-328.65	130.60
282	Primo Impalcato	35	0	-445.76	0.00	0.08	-0.05	-161.00	-129.33
			188	-445.76	0.00	-0.02	-0.05	82.15	-129.33
			376	-445.76	0.00	-0.12	-0.05	325.29	-129.33
283	Primo Impalcato	36	0	-522.73	-0.01	-0.01	0.02	162.55	130.62
			188	-522.73	-0.01	0.03	0.02	-83.01	130.62
			376	-522.73	-0.01	0.07	0.02	-328.57	130.62
284	Primo Impalcato	37	0	-444.61	-0.01	0.06	-0.04	-161.05	-129.34
			188	-444.61	-0.01	-0.01	-0.04	82.11	-129.34
			376	-444.61	-0.01	-0.09	-0.04	325.27	-129.34
285	Primo Impalcato	38	0	-525.84	-0.01	0.15	-0.07	162.88	130.64
			188	-525.84	-0.01	0.02	-0.07	-82.73	130.64
			376	-525.84	-0.01	-0.11	-0.07	-328.33	130.64
286	Primo Impalcato	39	0	-459.26	0.00	0.15	-0.05	-161.08	-129.45
			188	-459.26	0.00	0.05	-0.05	82.29	-129.45
			376	-459.26	0.00	-0.05	-0.05	325.67	-129.45

287	Primo Impalcato	40	0	-517.64	-0.01	0.35	-0.19	163.37	130.53
			188	-517.64	-0.01	0.00	-0.19	-82.03	130.53
			376	-517.64	-0.01	-0.35	-0.19	-327.43	130.53
288	Primo Impalcato	41	0	-501.01	-0.01	-0.06	0.04	-161.98	-130.14
			188	-501.01	-0.01	0.02	0.04	82.69	-130.14
			376	-501.01	-0.01	0.09	0.04	327.35	-130.14
289	Primo Impalcato	42	0	-476.62	0.01	-0.07	-0.01	162.51	129.14
			188	-476.62	0.01	-0.08	-0.01	-80.28	129.14
			376	-476.62	0.01	-0.10	-0.01	-323.06	129.14
290	Primo Impalcato	43	0	-463.39	0.02	-0.49	0.25	162.25	129.63
			188	-463.39	0.02	-0.02	0.25	-81.45	129.63
			376	-463.39	0.02	0.45	0.25	-325.15	129.63
291	Primo Impalcato	44	0	-491.43	-0.01	0.16	-0.10	-161.10	-130.50
			188	-491.43	-0.01	-0.04	-0.10	84.24	-130.50
			376	-491.43	-0.01	-0.23	-0.10	329.58	-130.50
292	Primo Impalcato	45	0	-467.14	0.01	-0.53	0.29	161.07	129.00
			188	-467.14	0.01	0.01	0.29	-81.45	129.00
			376	-467.14	0.01	0.55	0.29	-323.96	129.00
293	Primo Impalcato	46	0	-464.41	0.01	0.36	-0.22	-159.93	-128.80
			188	-464.41	0.01	-0.04	-0.22	82.21	-128.80
			376	-464.41	0.01	-0.45	-0.22	324.35	-128.80
294	Primo Impalcato	47	0	-465.00	0.02	-0.56	0.30	160.51	129.12
			188	-465.00	0.02	0.00	0.30	-82.23	129.12
			376	-465.00	0.02	0.56	0.30	-324.96	129.12
295	Primo Impalcato	48	0	-456.81	0.01	0.13	-0.07	-160.16	-128.81
			188	-456.81	0.01	-0.01	-0.07	82.01	-128.81
			376	-456.81	0.01	-0.14	-0.07	324.17	-128.81
296	Primo Impalcato	49	0	-457.99	-0.06	-0.93	0.47	162.87	130.85
			188	-457.99	-0.06	-0.04	0.47	-83.13	130.85
			376	-457.99	-0.06	0.85	0.47	-329.13	130.85
297	Primo Impalcato	50	0	-456.21	0.08	-0.36	0.20	-163.14	-130.78
			188	-456.21	0.08	0.02	0.20	82.73	-130.78
			376	-456.21	0.08	0.39	0.20	328.60	-130.78
298	Primo Impalcato	51	0	-422.71	-0.11	-1.39	0.71	172.85	137.23
			188	-422.71	-0.11	-0.05	0.71	-85.13	137.23
			376	-422.71	-0.11	1.28	0.71	-343.12	137.23
299	Primo Impalcato	52	0	-468.51	0.12	-1.08	0.57	-174.84	-138.02
			188	-468.51	0.12	-0.01	0.57	84.64	-138.02
			376	-468.51	0.12	1.06	0.57	344.12	-138.02
300	Primo Impalcato	53	0	-391.42	0.41	-2.13	1.10	172.28	138.13
			188	-391.42	0.41	-0.07	1.10	-87.39	138.13
			376	-391.42	0.41	1.99	1.10	-347.07	138.13
301	Primo Impalcato	54	0	-427.72	-0.43	-2.07	1.04	-173.36	-138.47
			188	-427.72	-0.43	-0.11	1.04	86.95	-138.47
			376	-427.72	-0.43	1.85	1.04	347.27	-138.47
302	Primo Impalcato	55	0	-304.18	2.77	-3.13	1.53	46.41	70.92
			188	-304.18	2.77	-0.25	1.53	-86.93	70.92
			376	-304.18	2.77	2.63	1.53	-220.27	70.92
303	Primo Impalcato	56	0	-317.44	-2.80	-2.88	1.39	-47.56	-70.66
			188	-317.44	-2.80	-0.26	1.39	85.29	-70.66
			376	-317.44	-2.80	2.36	1.39	218.14	-70.66
304	Primo Impalcato	57	0	-78.79	5.44	-6.05	2.80	-14.90	-12.55
			188	-78.79	5.44	-0.78	2.80	8.69	-12.55
			376	-78.79	5.44	4.49	2.80	32.27	-12.55
305	Primo	58	0	-141.60	-0.12	23.51	-13.75	-0.50	-0.25

	Impalcato								
			188	-141.60	-0.12	-2.34	-13.75	-0.02	-0.25
			376	-141.60	-0.12	-28.18	-13.75	0.45	-0.25
306	Primo Impalcato	59	0	-99.96	-0.13	8.39	-5.55	-0.10	-0.04
			188	-99.96	-0.13	-2.04	-5.55	-0.04	-0.04
			376	-99.96	-0.13	-12.46	-5.55	0.03	-0.04
307	Primo Impalcato	60	0	-67.92	-0.05	0.43	-0.93	0.09	0.06
			188	-67.92	-0.05	-1.31	-0.93	-0.02	0.06
			376	-67.92	-0.05	-3.06	-0.93	-0.14	0.06
308	Primo Impalcato	61	0	-45.34	-0.01	-1.33	0.21	0.08	0.05
			188	-45.34	-0.01	-0.92	0.21	-0.01	0.05
			376	-45.34	-0.01	-0.52	0.21	-0.10	0.05
309	Primo Impalcato	62	0	-36.05	0.00	-1.06	0.16	0.03	0.02
			188	-36.05	0.00	-0.76	0.16	0.00	0.02
			376	-36.05	0.00	-0.45	0.16	-0.04	0.02
310	Primo Impalcato	63	0	-32.17	0.00	-0.69	0.00	-0.01	0.00
			188	-32.17	0.00	-0.69	0.00	0.00	0.00
			376	-32.17	0.00	-0.68	0.00	0.01	0.00
311	Primo Impalcato	64	0	-32.29	0.00	-0.69	0.01	-0.02	-0.01
			188	-32.29	0.00	-0.68	0.01	0.00	-0.01
			376	-32.29	0.00	-0.66	0.01	0.02	-0.01
312	Primo Impalcato	65	0	-36.34	0.00	-1.07	0.18	-0.05	-0.03
			188	-36.34	0.00	-0.73	0.18	0.01	-0.03
			376	-36.34	0.00	-0.39	0.18	0.06	-0.03
313	Primo Impalcato	66	0	-45.66	0.01	-1.35	0.24	-0.10	-0.06
			188	-45.66	0.01	-0.89	0.24	0.01	-0.06
			376	-45.66	0.01	-0.43	0.24	0.13	-0.06
314	Primo Impalcato	67	0	-68.15	0.05	0.49	-0.95	-0.11	-0.07
			188	-68.15	0.05	-1.29	-0.95	0.02	-0.07
			376	-68.15	0.05	-3.08	-0.95	0.16	-0.07
315	Primo Impalcato	68	0	-100.57	0.13	8.83	-5.80	0.08	0.02
			188	-100.57	0.13	-2.07	-5.80	0.04	0.02
			376	-100.57	0.13	-12.97	-5.80	0.00	0.02
316	Primo Impalcato	69	0	-141.39	0.12	24.72	-14.45	0.45	0.23
			188	-141.39	0.12	-2.45	-14.45	0.02	0.23
			376	-141.39	0.12	-29.62	-14.45	-0.41	0.23
317	Primo Impalcato	70	0	-83.77	-5.65	-5.83	2.63	17.06	13.28
			188	-83.77	-5.65	-0.87	2.63	-7.90	13.28
			376	-83.77	-5.65	4.08	2.63	-32.87	13.28
318	Fondazio ne	1, 71	0	-73.13	-0.10	0.00	0.00	0.11	1.27
			102	-73.13	-0.10	0.00	0.00	-1.19	1.27
			204	-73.13	-0.10	0.00	0.00	-2.48	1.27
319	Fondazio ne	1, 92	0	18.24	-0.01	0.00	0.00	-0.55	-0.18
			103	18.24	-0.01	0.00	0.00	-0.36	-0.18
			206	18.24	-0.01	0.00	0.00	-0.17	-0.18
320	Primo Impalcato	92, 2	0	-59.98	-0.03	0.00	0.00	0.60	0.80
			103	-59.98	-0.03	0.00	0.00	-0.22	0.80
			206	-59.98	-0.03	0.00	0.00	-1.04	0.80
321	Fondazio ne	6, 89	0	-9.15	0.00	0.00	0.00	-0.02	0.00
			100	-9.15	0.00	0.00	0.00	-0.02	0.00
			200	-9.15	0.00	0.00	0.00	-0.03	0.00
322	Primo Impalcato	89, 7	0	-6.25	0.00	0.00	0.00	-0.01	0.00
			100	-6.25	0.00	0.00	0.00	-0.02	0.00
			200	-6.25	0.00	0.00	0.00	-0.02	0.00
323	Fondazio ne	9, 90	0	-5.55	0.00	0.00	0.00	0.00	0.01

			100	-5.55	0.00	0.00	0.00	-0.01	0.01
			200	-5.55	0.00	0.00	0.00	-0.02	0.01
324	Primo Impalcato	90, 10	0	-13.62	0.00	0.00	0.00	-0.03	-0.01
			100	-13.62	0.00	0.00	0.00	-0.02	-0.01
			200	-13.62	0.00	0.00	0.00	-0.01	-0.01
325	Fondazio ne	13, 91	0	-60.15	0.03	0.00	0.00	-1.05	-0.81
			103	-60.15	0.03	0.00	0.00	-0.21	-0.81
			206	-60.15	0.03	0.00	0.00	0.63	-0.81
326	Primo Impalcato	88, 14	0	-80.12	0.10	0.00	0.00	-2.44	-1.24
			102	-80.12	0.10	0.00	0.00	-1.18	-1.24
			204	-80.12	0.10	0.00	0.00	0.09	-1.24
327	Primo Impalcato	91, 14	0	18.53	0.01	0.00	0.00	-0.19	0.17
			103	18.53	0.01	0.00	0.00	-0.37	0.17
			206	18.53	0.01	0.00	0.00	-0.54	0.17
328	Primo Impalcato	71, 15	0	18.43	-0.15	0.00	0.00	1.70	1.65
			102	18.43	-0.15	0.00	0.00	0.02	1.65
			204	18.43	-0.15	0.00	0.00	-1.66	1.65
329	Fondazio ne	16, 88	0	24.94	0.14	0.00	0.00	-1.66	-1.64
			102	24.94	0.14	0.00	0.00	0.01	-1.64
			204	24.94	0.14	0.00	0.00	1.69	-1.64
330	Fondazio ne	17, 72	0	-81.17	0.07	0.00	0.00	-3.34	-1.31
			100	-81.17	0.07	0.00	0.00	-2.04	-1.31
			199	-81.17	0.07	0.00	0.00	-0.73	-1.31
331	Primo Impalcato	87, 18	0	-89.39	-0.06	0.00	0.00	-0.74	1.31
			100	-89.39	-0.06	0.00	0.00	-2.04	1.31
			199	-89.39	-0.06	0.00	0.00	-3.35	1.31
332	Primo Impalcato	72, 19	0	-45.72	-0.07	0.00	0.00	-0.75	1.24
			100	-45.72	-0.07	0.00	0.00	-1.99	1.24
			199	-45.72	-0.07	0.00	0.00	-3.22	1.24
333	Fondazio ne	20, 87	0	-38.43	0.07	0.00	0.00	-3.23	-1.25
			100	-38.43	0.07	0.00	0.00	-1.98	-1.25
			199	-38.43	0.07	0.00	0.00	-0.73	-1.25
334	Fondazio ne	21, 73	0	-66.44	0.07	0.00	0.00	-3.03	-1.15
			100	-66.44	0.07	0.00	0.00	-1.89	-1.15
			199	-66.44	0.07	0.00	0.00	-0.74	-1.15
335	Primo Impalcato	86, 22	0	-77.50	-0.06	0.00	0.00	-0.74	1.15
			100	-77.50	-0.06	0.00	0.00	-1.89	1.15
			199	-77.50	-0.06	0.00	0.00	-3.03	1.15
336	Primo Impalcato	73, 23	0	-77.86	-0.06	0.00	0.00	-0.79	1.12
			100	-77.86	-0.06	0.00	0.00	-1.91	1.12
			199	-77.86	-0.06	0.00	0.00	-3.02	1.12
337	Fondazio ne	24, 86	0	-67.97	0.06	0.00	0.00	-3.01	-1.12
			100	-67.97	0.06	0.00	0.00	-1.90	-1.12
			199	-67.97	0.06	0.00	0.00	-0.79	-1.12
338	Fondazio ne	25, 74	0	-68.77	0.08	0.00	0.00	-2.88	-1.05
			103	-68.77	0.08	0.00	0.00	-1.80	-1.05
			206	-68.77	0.08	0.00	0.00	-0.72	-1.05
339	Primo Impalcato	85, 26	0	-81.16	-0.06	0.00	0.00	-0.76	1.16
			100	-81.16	-0.06	0.00	0.00	-1.92	1.16
			199	-81.16	-0.06	0.00	0.00	-3.08	1.16
340	Fondazio ne	27, 85	0	-69.55	0.06	0.00	0.00	-2.99	-1.12
			100	-69.55	0.06	0.00	0.00	-1.88	-1.12
			199	-69.55	0.06	0.00	0.00	-0.77	-1.12
341	Primo Impalcato	74, 28	0	-78.06	-0.08	0.00	0.00	-0.72	1.02
			103	-78.06	-0.08	0.00	0.00	-1.77	1.02

			206	-78.06	-0.08	0.00	0.00	-2.82	1.02
342	Primo Impalcato	84, 29	0	-75.80	-0.06	0.00	0.00	-0.75	1.14
			100	-75.80	-0.06	0.00	0.00	-1.88	1.14
			199	-75.80	-0.06	0.00	0.00	-3.02	1.14
343	Fondazio ne	31, 84	0	-67.60	0.06	0.00	0.00	-3.01	-1.13
			100	-67.60	0.06	0.00	0.00	-1.88	-1.13
			199	-67.60	0.06	0.00	0.00	-0.75	-1.13
344	Primo Impalcato	83, 33	0	-74.04	-0.06	0.00	0.00	-0.74	1.14
			100	-74.04	-0.06	0.00	0.00	-1.88	1.14
			199	-74.04	-0.06	0.00	0.00	-3.01	1.14
345	Fondazio ne	35, 83	0	-68.38	0.06	0.00	0.00	-3.01	-1.13
			100	-68.38	0.06	0.00	0.00	-1.88	-1.13
			199	-68.38	0.06	0.00	0.00	-0.75	-1.13
346	Primo Impalcato	82, 37	0	-73.90	-0.06	0.00	0.00	-0.75	1.13
			100	-73.90	-0.06	0.00	0.00	-1.87	1.13
			199	-73.90	-0.06	0.00	0.00	-3.00	1.13
347	Fondazio ne	39, 82	0	-70.55	0.06	0.00	0.00	-3.01	-1.14
			100	-70.55	0.06	0.00	0.00	-1.88	-1.14
			199	-70.55	0.06	0.00	0.00	-0.75	-1.14
348	Primo Impalcato	78, 43	0	-66.34	0.06	0.00	0.00	0.73	-1.14
			100	-66.34	0.06	0.00	0.00	1.87	-1.14
			199	-66.34	0.06	0.00	0.00	3.00	-1.14
349	Primo Impalcato	81, 44	0	-83.19	-0.06	0.00	0.00	-0.75	1.17
			100	-83.19	-0.06	0.00	0.00	-1.91	1.17
			199	-83.19	-0.06	0.00	0.00	-3.07	1.17
350	Fondazio ne	45, 78	0	-82.99	-0.06	0.00	0.00	3.00	1.13
			100	-82.99	-0.06	0.00	0.00	1.87	1.13
			199	-82.99	-0.06	0.00	0.00	0.75	1.13
351	Fondazio ne	46, 81	0	-69.50	0.06	0.00	0.00	-2.97	-1.11
			100	-69.50	0.06	0.00	0.00	-1.87	-1.11
			199	-69.50	0.06	0.00	0.00	-0.77	-1.11
352	Primo Impalcato	77, 47	0	-62.66	0.06	0.00	0.00	0.77	-1.11
			100	-62.66	0.06	0.00	0.00	1.88	-1.11
			199	-62.66	0.06	0.00	0.00	2.99	-1.11
353	Primo Impalcato	80, 48	0	-70.55	-0.06	0.00	0.00	-0.78	1.11
			100	-70.55	-0.06	0.00	0.00	-1.88	1.11
			199	-70.55	-0.06	0.00	0.00	-2.99	1.11
354	Fondazio ne	49, 77	0	-85.32	-0.06	0.00	0.00	3.04	1.15
			100	-85.32	-0.06	0.00	0.00	1.89	1.15
			199	-85.32	-0.06	0.00	0.00	0.74	1.15
355	Fondazio ne	50, 80	0	-75.18	0.06	0.00	0.00	-3.03	-1.15
			100	-75.18	0.06	0.00	0.00	-1.88	-1.15
			199	-75.18	0.06	0.00	0.00	-0.73	-1.15
356	Primo Impalcato	76, 51	0	-37.51	0.07	0.00	0.00	0.75	-1.24
			100	-37.51	0.07	0.00	0.00	1.98	-1.24
			199	-37.51	0.07	0.00	0.00	3.21	-1.24
357	Fondazio ne	53, 76	0	-92.80	-0.07	0.00	0.00	3.35	1.31
			100	-92.80	-0.07	0.00	0.00	2.04	1.31
			199	-92.80	-0.07	0.00	0.00	0.73	1.31
358	Primo Impalcato	75, 55	0	26.38	0.15	0.00	0.00	-1.70	-1.65
			102	26.38	0.15	0.00	0.00	-0.02	-1.65
			204	26.38	0.15	0.00	0.00	1.66	-1.65
359	Fondazio ne	56, 79	0	21.10	-0.14	0.00	0.00	1.64	1.62
			102	21.10	-0.14	0.00	0.00	-0.01	1.62
			204	21.10	-0.14	0.00	0.00	-1.66	1.62

360	Fondazio ne	57, 75	0	-80.90	0.10	0.00	0.00	-0.11	-1.27
			102	-80.90	0.10	0.00	0.00	1.19	-1.27
			204	-80.90	0.10	0.00	0.00	2.49	-1.27
361	Fondazio ne	57, 93	0	19.39	0.01	0.00	0.00	0.53	0.17
			103	19.39	0.01	0.00	0.00	0.35	0.17
			206	19.39	0.01	0.00	0.00	0.18	0.17
362	Primo Impalcato	93, 58	0	-60.40	0.03	0.00	0.00	-0.61	-0.79
			103	-60.40	0.03	0.00	0.00	0.21	-0.79
			206	-60.40	0.03	0.00	0.00	1.02	-0.79
363	Fondazio ne	61, 95	0	-12.73	0.00	0.00	0.00	0.01	-0.01
			100	-12.73	0.00	0.00	0.00	0.02	-0.01
			200	-12.73	0.00	0.00	0.00	0.02	-0.01
364	Primo Impalcato	95, 62	0	-6.48	0.00	0.00	0.00	0.02	0.01
			100	-6.48	0.00	0.00	0.00	0.01	0.01
			200	-6.48	0.00	0.00	0.00	0.00	0.01
365	Primo Impalcato	96, 65	0	-5.26	0.00	0.00	0.00	-0.02	-0.01
			100	-5.26	0.00	0.00	0.00	-0.01	-0.01
			200	-5.26	0.00	0.00	0.00	0.00	-0.01
366	Fondazio ne	66, 96	0	-14.10	0.00	0.00	0.00	-0.01	0.01
			100	-14.10	0.00	0.00	0.00	-0.02	0.01
			200	-14.10	0.00	0.00	0.00	-0.02	0.01
367	Fondazio ne	69, 94	0	-59.62	-0.03	0.00	0.00	1.07	0.83
			103	-59.62	-0.03	0.00	0.00	0.22	0.83
			206	-59.62	-0.03	0.00	0.00	-0.63	0.83
368	Primo Impalcato	79, 70	0	-78.11	-0.10	0.00	0.00	2.43	1.23
			102	-78.11	-0.10	0.00	0.00	1.17	1.23
			204	-78.11	-0.10	0.00	0.00	-0.09	1.23
369	Primo Impalcato	94, 70	0	18.21	-0.01	0.00	0.00	0.18	-0.19
			103	18.21	-0.01	0.00	0.00	0.38	-0.19
			206	18.21	-0.01	0.00	0.00	0.57	-0.19
370	Primo Impalcato	1, 71	0	18.43	-0.05	0.00	0.00	0.45	-0.66
			102	18.43	-0.05	0.00	0.00	1.12	-0.66
			204	18.43	-0.05	0.00	0.00	1.80	-0.66
371	Primo Impalcato	1, 92	0	-59.98	-0.18	0.00	0.00	1.65	0.55
			103	-59.98	-0.18	0.00	0.00	1.09	0.55
			206	-59.98	-0.18	0.00	0.00	0.53	0.55
372	Primo Impalcato	92, 2	0	18.24	0.04	0.00	0.00	-0.02	-0.43
			103	18.24	0.04	0.00	0.00	0.42	-0.43
			206	18.24	0.04	0.00	0.00	0.87	-0.43
373	Primo Impalcato	6, 89	0	-6.25	0.00	0.00	0.00	-0.03	-0.01
			100	-6.25	0.00	0.00	0.00	-0.02	-0.01
			200	-6.25	0.00	0.00	0.00	-0.01	-0.01
374	Primo Impalcato	89, 7	0	-9.15	0.00	0.00	0.00	-0.03	-0.01
			100	-9.15	0.00	0.00	0.00	-0.02	-0.01
			200	-9.15	0.00	0.00	0.00	-0.02	-0.01
375	Primo Impalcato	9, 90	0	-13.62	0.00	0.00	0.00	-0.03	0.00
			100	-13.62	0.00	0.00	0.00	-0.03	0.00
			200	-13.62	0.00	0.00	0.00	-0.03	0.00
376	Primo Impalcato	90, 10	0	-5.55	0.00	0.00	0.00	-0.02	0.02
			100	-5.55	0.00	0.00	0.00	-0.04	0.02
			200	-5.55	0.00	0.00	0.00	-0.05	0.02
377	Primo Impalcato	13, 91	0	18.53	-0.04	0.00	0.00	0.88	0.45
			103	18.53	-0.04	0.00	0.00	0.42	0.45
			206	18.53	-0.04	0.00	0.00	-0.03	0.45
378	Primo	88, 14	0	24.94	0.06	0.00	0.00	1.78	0.62

	Impalcato								
			102	24.94	0.06	0.00	0.00	1.15	0.62
			204	24.94	0.06	0.00	0.00	0.51	0.62
379	Primo Impalcato	91, 14	0	-60.15	0.18	0.00	0.00	0.56	-0.54
			103	-60.15	0.18	0.00	0.00	1.12	-0.54
			206	-60.15	0.18	0.00	0.00	1.67	-0.54
380	Primo Impalcato	71, 15	0	-73.13	-0.09	0.00	0.00	-2.62	-1.04
			102	-73.13	-0.09	0.00	0.00	-1.56	-1.04
			204	-73.13	-0.09	0.00	0.00	-0.50	-1.04
381	Primo Impalcato	16, 88	0	-80.12	0.09	0.00	0.00	-0.47	1.03
			102	-80.12	0.09	0.00	0.00	-1.52	1.03
			204	-80.12	0.09	0.00	0.00	-2.56	1.03
382	Primo Impalcato	17, 72	0	-45.72	-0.02	0.00	0.00	1.90	1.35
			100	-45.72	-0.02	0.00	0.00	0.55	1.35
			199	-45.72	-0.02	0.00	0.00	-0.80	1.35
383	Primo Impalcato	87, 18	0	-38.43	0.03	0.00	0.00	-0.78	-1.36
			100	-38.43	0.03	0.00	0.00	0.57	-1.36
			199	-38.43	0.03	0.00	0.00	1.92	-1.36
384	Primo Impalcato	72, 19	0	-81.17	0.00	0.00	0.00	-0.72	-1.20
			100	-81.17	0.00	0.00	0.00	0.47	-1.20
			199	-81.17	0.00	0.00	0.00	1.66	-1.20
385	Primo Impalcato	20, 87	0	-89.39	0.00	0.00	0.00	1.67	1.21
			100	-89.39	0.00	0.00	0.00	0.47	1.21
			199	-89.39	0.00	0.00	0.00	-0.73	1.21
386	Primo Impalcato	21, 73	0	-77.86	0.02	0.00	0.00	1.46	1.14
			100	-77.86	0.02	0.00	0.00	0.32	1.14
			199	-77.86	0.02	0.00	0.00	-0.82	1.14
387	Primo Impalcato	86, 22	0	-67.97	-0.02	0.00	0.00	-0.81	-1.14
			100	-67.97	-0.02	0.00	0.00	0.33	-1.14
			199	-67.97	-0.02	0.00	0.00	1.46	-1.14
388	Primo Impalcato	73, 23	0	-66.44	-0.01	0.00	0.00	-0.77	-1.12
			100	-66.44	-0.01	0.00	0.00	0.35	-1.12
			199	-66.44	-0.01	0.00	0.00	1.47	-1.12
389	Primo Impalcato	24, 86	0	-77.50	0.01	0.00	0.00	1.47	1.12
			100	-77.50	0.01	0.00	0.00	0.35	1.12
			199	-77.50	0.01	0.00	0.00	-0.77	1.12
390	Primo Impalcato	25, 74	0	-78.06	0.02	0.00	0.00	1.36	1.02
			103	-78.06	0.02	0.00	0.00	0.30	1.02
			206	-78.06	0.02	0.00	0.00	-0.76	1.02
391	Primo Impalcato	85, 26	0	-69.55	-0.01	0.00	0.00	-0.79	-1.13
			100	-69.55	-0.01	0.00	0.00	0.34	-1.13
			199	-69.55	-0.01	0.00	0.00	1.46	-1.13
392	Primo Impalcato	27, 85	0	-81.16	0.01	0.00	0.00	1.49	1.15
			100	-81.16	0.01	0.00	0.00	0.35	1.15
			199	-81.16	0.01	0.00	0.00	-0.80	1.15
393	Primo Impalcato	74, 28	0	-68.77	-0.02	0.00	0.00	-0.76	-1.04
			103	-68.77	-0.02	0.00	0.00	0.31	-1.04
			206	-68.77	-0.02	0.00	0.00	1.38	-1.04
394	Primo Impalcato	84, 29	0	-67.60	-0.01	0.00	0.00	-0.78	-1.13
			100	-67.60	-0.01	0.00	0.00	0.36	-1.13
			199	-67.60	-0.01	0.00	0.00	1.49	-1.13
395	Primo Impalcato	31, 84	0	-75.80	0.01	0.00	0.00	1.49	1.14
			100	-75.80	0.01	0.00	0.00	0.36	1.14
			199	-75.80	0.01	0.00	0.00	-0.78	1.14
396	Primo Impalcato	83, 33	0	-68.38	-0.01	0.00	0.00	-0.77	-1.13

			100	-68.38	-0.01	0.00	0.00	0.36	-1.13
			199	-68.38	-0.01	0.00	0.00	1.49	-1.13
397	Primo Impalcato	35, 83	0	-74.04	0.01	0.00	0.00	1.49	1.13
			100	-74.04	0.01	0.00	0.00	0.36	1.13
			199	-74.04	0.01	0.00	0.00	-0.77	1.13
398	Primo Impalcato	82, 37	0	-70.55	-0.01	0.00	0.00	-0.77	-1.14
			100	-70.55	-0.01	0.00	0.00	0.36	-1.14
			199	-70.55	-0.01	0.00	0.00	1.49	-1.14
399	Primo Impalcato	39, 82	0	-73.90	0.01	0.00	0.00	1.49	1.13
			100	-73.90	0.01	0.00	0.00	0.36	1.13
			199	-73.90	0.01	0.00	0.00	-0.77	1.13
400	Primo Impalcato	78, 43	0	-82.99	0.01	0.00	0.00	0.78	1.14
			100	-82.99	0.01	0.00	0.00	-0.36	1.14
			199	-82.99	0.01	0.00	0.00	-1.50	1.14
401	Primo Impalcato	81, 44	0	-69.50	-0.01	0.00	0.00	-0.79	-1.13
			100	-69.50	-0.01	0.00	0.00	0.34	-1.13
			199	-69.50	-0.01	0.00	0.00	1.47	-1.13
402	Primo Impalcato	45, 78	0	-66.34	-0.01	0.00	0.00	-1.49	-1.13
			100	-66.34	-0.01	0.00	0.00	-0.37	-1.13
			199	-66.34	-0.01	0.00	0.00	0.76	-1.13
403	Primo Impalcato	46, 81	0	-83.19	0.01	0.00	0.00	1.49	1.14
			100	-83.19	0.01	0.00	0.00	0.36	1.14
			199	-83.19	0.01	0.00	0.00	-0.78	1.14
404	Primo Impalcato	77, 47	0	-85.32	0.01	0.00	0.00	0.77	1.13
			100	-85.32	0.01	0.00	0.00	-0.35	1.13
			199	-85.32	0.01	0.00	0.00	-1.48	1.13
405	Primo Impalcato	80, 48	0	-75.18	-0.01	0.00	0.00	-0.76	-1.13
			100	-75.18	-0.01	0.00	0.00	0.36	-1.13
			199	-75.18	-0.01	0.00	0.00	1.48	-1.13
406	Primo Impalcato	49, 77	0	-62.66	-0.02	0.00	0.00	-1.46	-1.13
			100	-62.66	-0.02	0.00	0.00	-0.33	-1.13
			199	-62.66	-0.02	0.00	0.00	0.80	-1.13
407	Primo Impalcato	50, 80	0	-70.55	0.02	0.00	0.00	1.46	1.14
			100	-70.55	0.02	0.00	0.00	0.33	1.14
			199	-70.55	0.02	0.00	0.00	-0.80	1.14
408	Primo Impalcato	76, 51	0	-92.80	0.00	0.00	0.00	0.73	1.20
			100	-92.80	0.00	0.00	0.00	-0.47	1.20
			199	-92.80	0.00	0.00	0.00	-1.66	1.20
409	Primo Impalcato	53, 76	0	-37.51	0.02	0.00	0.00	-1.90	-1.35
			100	-37.51	0.02	0.00	0.00	-0.55	-1.35
			199	-37.51	0.02	0.00	0.00	0.80	-1.35
410	Primo Impalcato	75, 55	0	-80.90	0.09	0.00	0.00	2.63	1.04
			102	-80.90	0.09	0.00	0.00	1.56	1.04
			204	-80.90	0.09	0.00	0.00	0.50	1.04
411	Primo Impalcato	56, 79	0	-78.11	-0.09	0.00	0.00	0.58	-0.96
			102	-78.11	-0.09	0.00	0.00	1.56	-0.96
			204	-78.11	-0.09	0.00	0.00	2.54	-0.96
412	Primo Impalcato	57, 75	0	26.38	0.05	0.00	0.00	-0.45	0.67
			102	26.38	0.05	0.00	0.00	-1.13	0.67
			204	26.38	0.05	0.00	0.00	-1.81	0.67
413	Primo Impalcato	57, 93	0	-60.40	0.18	0.00	0.00	-1.62	-0.52
			103	-60.40	0.18	0.00	0.00	-1.08	-0.52
			206	-60.40	0.18	0.00	0.00	-0.55	-0.52
414	Primo Impalcato	93, 58	0	19.39	-0.04	0.00	0.00	0.03	0.44
			103	19.39	-0.04	0.00	0.00	-0.42	0.44

			206	19.39	-0.04	0.00	0.00	-0.87	0.44
415	Primo Impalcato	61, 95	0	-6.48	0.00	0.00	0.00	0.05	0.02
			100	-6.48	0.00	0.00	0.00	0.03	0.02
			200	-6.48	0.00	0.00	0.00	0.02	0.02
416	Primo Impalcato	95, 62	0	-12.73	0.00	0.00	0.00	0.03	0.00
			100	-12.73	0.00	0.00	0.00	0.03	0.00
			200	-12.73	0.00	0.00	0.00	0.03	0.00
417	Primo Impalcato	96, 65	0	-14.10	0.00	0.00	0.00	-0.03	0.00
			100	-14.10	0.00	0.00	0.00	-0.03	0.00
			200	-14.10	0.00	0.00	0.00	-0.03	0.00
418	Primo Impalcato	66, 96	0	-5.26	0.00	0.00	0.00	-0.05	-0.02
			100	-5.26	0.00	0.00	0.00	-0.03	-0.02
			200	-5.26	0.00	0.00	0.00	-0.02	-0.02
419	Primo Impalcato	69, 94	0	18.21	0.04	0.00	0.00	-0.92	-0.46
			103	18.21	0.04	0.00	0.00	-0.45	-0.46
			206	18.21	0.04	0.00	0.00	0.02	-0.46
420	Primo Impalcato	79, 70	0	21.10	-0.07	0.00	0.00	-1.74	-0.57
			102	21.10	-0.07	0.00	0.00	-1.16	-0.57
			204	21.10	-0.07	0.00	0.00	-0.58	-0.57
421	Primo Impalcato	94, 70	0	-59.62	-0.18	0.00	0.00	-0.56	0.56
			103	-59.62	-0.18	0.00	0.00	-1.13	0.56
			206	-59.62	-0.18	0.00	0.00	-1.70	0.56
422	Copertura	1, 2	0	9.28	-8.19	134.15	-40.42	-9.62	-7.93
			83	9.28	-8.19	88.94	-68.35	-3.02	-7.93
			166	9.28	-8.19	20.52	-96.28	3.57	-7.93
423	Copertura	15, 1	0	-12.03	-117.81	320.56	-217.95	7.21	13.72
			80	-12.03	-117.81	147.30	-217.95	-3.69	13.72
			159	-12.03	-117.81	-25.97	-217.95	-14.60	13.72
424	Copertura	2, 3	0	14.78	2.32	20.68	-42.06	3.37	-0.64
			69	14.78	2.32	-16.34	-65.25	3.81	-0.64
			138	14.78	2.32	-69.36	-88.43	4.25	-0.64
425	Copertura	3, 4	0	14.98	3.10	-68.90	7.29	4.13	1.42
			69	14.98	3.10	-71.87	-15.90	3.15	1.42
			138	14.98	3.10	-90.83	-39.08	2.17	1.42
426	Copertura	4, 5	0	15.11	1.38	-90.54	34.06	2.12	1.12
			69	15.11	1.38	-75.04	10.87	1.35	1.12
			138	15.11	1.38	-75.53	-12.31	0.58	1.12
427	Copertura	5, 6	0	15.19	0.28	-75.34	36.52	0.57	0.54
			69	15.19	0.28	-58.14	13.33	0.20	0.54
			138	15.19	0.28	-56.94	-9.85	-0.18	0.54
428	Copertura	6, 7	0	18.67	-0.05	-56.83	36.93	-0.17	0.20
			69	18.67	-0.05	-39.35	13.75	-0.31	0.20
			138	18.67	-0.05	-37.86	-9.44	-0.45	0.20
429	Copertura	7, 8	0	17.26	-0.01	-37.83	25.28	-0.45	0.03
			69	17.26	-0.01	-28.38	2.09	-0.47	0.03
			138	17.26	-0.01	-34.94	-21.09	-0.49	0.03
430	Copertura	8, 9	0	17.25	0.02	-34.96	9.38	-0.49	-0.14
			69	17.25	0.02	-36.49	-13.80	-0.39	-0.14
			138	17.25	0.02	-54.01	-36.99	-0.30	-0.14
431	Copertura	9, 10	0	18.37	-0.30	-54.10	0.40	-0.30	-0.47
			69	18.37	-0.30	-61.82	-22.78	0.03	-0.47
			138	18.37	-0.30	-85.54	-45.96	0.35	-0.47
432	Copertura	10, 11	0	13.40	-1.42	-85.72	16.67	0.37	-1.06
			69	13.40	-1.42	-82.21	-6.51	1.10	-1.06
			138	13.40	-1.42	-94.70	-29.70	1.83	-1.06
433	Copertura	11, 12	0	13.28	-3.12	-95.00	42.45	1.88	-1.34
			69	13.28	-3.12	-73.70	19.27	2.80	-1.34
			138	13.28	-3.12	-68.40	-3.91	3.73	-1.34
434	Copertura	12, 13	0	13.08	-2.24	-68.86	91.89	3.84	0.79
			69	13.08	-2.24	-13.46	68.70	3.30	0.79
			138	13.08	-2.24	25.95	45.52	2.75	0.79
435	Copertura	13, 14	0	7.45	8.22	25.80	100.99	2.95	8.31
			83	7.45	8.22	98.13	73.06	-3.95	8.31
			166	7.45	8.22	147.25	45.13	-10.86	8.31
436	Copertura	16, 14	0	-14.22	117.07	308.44	-211.12	-19.72	-28.96
			80	-14.22	117.07	140.60	-211.12	3.30	-28.96

			159	-14.22	117.07	-27.24	-211.12	26.32	-28.96
437	Copertura	15, 17	0	-13.52	-10.01	317.23	35.41	-4.20	-5.31
			66	-13.52	-10.01	340.60	35.41	-0.70	-5.31
			132	-13.52	-10.01	363.97	35.41	2.81	-5.31
438	Copertura	16, 18	0	-16.76	10.85	305.85	34.40	8.26	6.83
			66	-16.76	10.85	328.56	34.40	3.75	6.83
			132	-16.76	10.85	351.26	34.40	-0.76	6.83
439	Copertura	17, 19	0	-14.50	-0.84	361.70	-51.46	3.25	2.10
			66	-14.50	-0.84	327.74	-51.46	1.86	2.10
			132	-14.50	-0.84	293.77	-51.46	0.47	2.10
440	Copertura	18, 20	0	-18.61	0.93	348.47	-52.04	-1.07	-0.46
			66	-18.61	0.93	314.13	-52.04	-0.77	-0.46
			132	-18.61	0.93	279.78	-52.04	-0.47	-0.46
441	Copertura	19, 21	0	-15.06	0.94	292.47	-79.62	0.49	0.81
			66	-15.06	0.94	239.92	-79.62	-0.04	0.81
			132	-15.06	0.94	187.38	-79.62	-0.57	0.81
442	Copertura	20, 22	0	-19.89	-1.00	278.17	-72.11	-0.29	-0.09
			66	-19.89	-1.00	230.58	-72.11	-0.23	-0.09
			132	-19.89	-1.00	182.99	-72.11	-0.17	-0.09
443	Copertura	21, 23	0	-15.30	0.40	186.85	-82.08	-0.52	0.06
			66	-15.30	0.40	132.68	-82.08	-0.57	0.06
			132	-15.30	0.40	78.51	-82.08	-0.61	0.06
444	Copertura	22, 24	0	-19.82	-0.43	182.82	-71.51	0.04	0.39
			66	-19.82	-0.43	135.62	-71.51	-0.22	0.39
			132	-19.82	-0.43	88.43	-71.51	-0.48	0.39
445	Copertura	23, 25	0	-15.30	0.06	78.48	-65.35	-0.54	0.04
			66	-15.30	0.06	35.35	-65.35	-0.56	0.04
			132	-15.30	0.06	-7.78	-65.35	-0.59	0.04
446	Copertura	24, 26	0	-19.78	-0.04	88.61	-51.67	-0.35	0.32
			66	-19.78	-0.04	54.51	-51.67	-0.57	0.32
			132	-19.78	-0.04	20.41	-51.67	-0.78	0.32
447	Copertura	25, 28	0	-15.26	-0.14	-7.69	-17.52	-0.57	0.01
			85	-15.26	-0.14	-22.59	-17.52	-0.57	0.01
			170	-15.26	-0.14	-37.48	-17.52	-0.58	0.01
448	Copertura	26, 27	0	-16.68	0.17	23.58	-22.43	-0.74	-0.01
			66	-16.68	0.17	8.77	-22.43	-0.73	-0.01
			132	-16.68	0.17	-6.03	-22.43	-0.72	-0.01
449	Copertura	27, 29	0	-19.50	0.24	-1.77	-4.90	-0.75	-0.23
			66	-19.50	0.24	-5.01	-4.90	-0.59	-0.23
			132	-19.50	0.24	-8.24	-4.90	-0.44	-0.23
450	Copertura	28, 30	0	-15.44	-0.22	-44.68	19.88	-0.55	-0.06
			73	-15.44	-0.22	-30.16	19.88	-0.50	-0.06
			146	-15.44	-0.22	-15.65	19.88	-0.45	-0.06
451	Copertura	29, 31	0	-19.50	0.13	1.17	-3.15	-0.46	-0.12
			66	-19.50	0.13	-0.91	-3.15	-0.38	-0.12
			132	-19.50	0.13	-2.98	-3.15	-0.30	-0.12
452	Copertura	30, 32	0	-15.66	-0.09	-25.49	17.62	-0.47	-0.17
			69	-15.66	-0.09	-13.41	17.62	-0.36	-0.17
			137	-15.66	-0.09	-1.34	17.62	-0.25	-0.17
453	Copertura	31, 33	0	-20.72	0.09	6.29	-6.95	-0.36	-0.17
			66	-20.72	0.09	1.70	-6.95	-0.24	-0.17
			132	-20.72	0.09	-2.88	-6.95	-0.13	-0.17
454	Copertura	32, 34	0	-15.84	-0.04	-12.05	10.02	-0.31	-0.15
			69	-15.84	-0.04	-5.14	10.02	-0.21	-0.15
			138	-15.84	-0.04	1.78	10.02	-0.11	-0.15
455	Copertura	33, 35	0	-20.92	0.10	8.43	-10.35	-0.18	-0.17
			66	-20.92	0.10	1.61	-10.35	-0.06	-0.17
			132	-20.92	0.10	-5.22	-10.35	0.05	-0.17
456	Copertura	34, 36	0	-16.03	-0.04	-10.04	9.54	-0.19	-0.18
			69	-16.03	-0.04	-3.45	9.54	-0.06	-0.18
			138	-16.03	-0.04	3.13	9.54	0.06	-0.18
457	Copertura	35, 37	0	-22.18	0.09	6.18	-14.50	-0.02	-0.30
			66	-22.18	0.09	-3.39	-14.50	0.18	-0.30
			132	-22.18	0.09	-12.97	-14.50	0.38	-0.30
458	Copertura	36, 38	0	-16.23	-0.06	-9.80	17.17	-0.02	-0.24
			69	-16.23	-0.06	2.05	17.17	0.15	-0.24
			138	-16.23	-0.06	13.90	17.17	0.32	-0.24
459	Copertura	37, 39	0	-23.01	0.10	-0.10	-12.35	0.35	-0.25
			66	-23.01	0.10	-8.25	-12.35	0.51	-0.25
			132	-23.01	0.10	-16.40	-12.35	0.68	-0.25
460	Copertura	38, 40	0	-16.45	-0.08	-0.14	27.28	0.27	-0.27
			69	-16.45	-0.08	18.55	27.28	0.46	-0.27

			137	-16.45	-0.08	37.24	27.28	0.64	-0.27
461	Copertura	39, 41	0	-24.34	-0.03	-3.24	-8.02	0.71	-0.05
			66	-24.34	-0.03	-8.53	-8.02	0.74	-0.05
			132	-24.34	-0.03	-13.83	-8.02	0.78	-0.05
462	Copertura	40, 42	0	-16.68	0.05	22.31	25.13	0.65	-0.27
			69	-16.68	0.05	39.65	25.13	0.84	-0.27
			138	-16.68	0.05	56.99	25.13	1.02	-0.27
463	Copertura	41, 44	0	-31.24	-0.43	-4.97	-6.87	0.88	0.24
			66	-31.24	-0.43	-9.51	-6.87	0.72	0.24
			132	-31.24	-0.43	-14.04	-6.87	0.55	0.24
464	Copertura	42, 43	0	-16.77	1.04	41.21	12.81	1.09	-0.09
			23	-16.77	1.04	44.15	12.81	1.11	-0.09
			46	-16.77	1.04	47.10	12.81	1.13	-0.09
465	Copertura	43, 45	0	-16.67	0.16	47.31	11.34	1.15	0.50
			66	-16.67	0.16	54.79	11.34	0.82	0.50
			132	-16.67	0.16	62.27	11.34	0.49	0.50
466	Copertura	44, 46	0	-25.15	-0.13	-8.01	24.72	0.67	0.13
			66	-25.15	-0.13	8.31	24.72	0.58	0.13
			132	-25.15	-0.13	24.63	24.72	0.50	0.13
467	Copertura	45, 47	0	-16.52	0.01	62.60	29.53	0.59	0.53
			66	-16.52	0.01	82.10	29.53	0.24	0.53
			132	-16.52	0.01	101.59	29.53	-0.11	0.53
468	Copertura	46, 48	0	-24.78	0.00	25.20	56.43	0.60	0.44
			66	-24.78	0.00	62.44	56.43	0.31	0.44
			132	-24.78	0.00	99.69	56.43	0.02	0.44
469	Copertura	47, 49	0	-16.28	-0.33	102.17	55.31	0.01	0.55
			66	-16.28	-0.33	138.67	55.31	-0.36	0.55
			132	-16.28	-0.33	175.18	55.31	-0.72	0.55
470	Copertura	48, 50	0	-23.86	0.32	100.76	74.02	0.14	0.23
			66	-23.86	0.32	149.62	74.02	-0.01	0.23
			132	-23.86	0.32	198.47	74.02	-0.16	0.23
471	Copertura	49, 51	0	-15.84	-0.92	176.23	64.81	-0.55	-0.32
			66	-15.84	-0.92	219.01	64.81	-0.33	-0.32
			132	-15.84	-0.92	261.78	64.81	-0.12	-0.32
472	Copertura	50, 52	0	-22.60	0.90	200.01	79.20	-0.19	0.46
			66	-22.60	0.90	252.28	79.20	-0.49	0.46
			132	-22.60	0.90	304.55	79.20	-0.79	0.46
473	Copertura	51, 53	0	-15.10	0.78	263.53	52.83	0.06	-1.75
			66	-15.10	0.78	298.40	52.83	1.22	-1.75
			132	-15.10	0.78	333.27	52.83	2.38	-1.75
474	Copertura	52, 54	0	-20.91	-0.85	307.06	39.58	-0.87	1.19
			66	-20.91	-0.85	333.18	39.58	-1.66	1.19
			132	-20.91	-0.85	359.30	39.58	-2.44	1.19
475	Copertura	53, 55	0	-13.98	9.84	335.89	-28.58	2.05	6.26
			66	-13.98	9.84	317.03	-28.58	-2.08	6.26
			132	-13.98	9.84	298.17	-28.58	-6.21	6.26
476	Copertura	54, 56	0	-17.90	-10.29	363.19	-42.10	-1.27	-7.52
			66	-17.90	-10.29	335.40	-42.10	3.69	-7.52
			132	-17.90	-10.29	307.62	-42.10	8.66	-7.52
477	Copertura	55, 57	0	-12.41	118.03	301.68	-206.51	-8.92	-15.33
			80	-12.41	118.03	137.51	-206.51	3.27	-15.33
			159	-12.41	118.03	-26.67	-206.51	15.45	-15.33
478	Copertura	56, 70	0	-14.13	-117.70	312.71	-214.94	12.09	20.26
			80	-14.13	-117.70	141.84	-214.94	-4.02	20.26
			159	-14.13	-117.70	-29.04	-214.94	-20.12	20.26
479	Copertura	57, 58	0	6.98	8.40	133.94	-39.64	10.44	8.22
			83	6.98	8.40	89.38	-67.56	3.60	8.22
			166	6.98	8.40	21.61	-95.49	-3.23	8.22
480	Copertura	58, 59	0	12.47	-2.21	21.75	-42.99	-3.03	0.78
			69	12.47	-2.21	-15.91	-66.17	-3.56	0.78
			138	12.47	-2.21	-69.57	-89.36	-4.10	0.78
481	Copertura	59, 60	0	12.67	-3.07	-69.12	5.27	-3.98	-1.32
			69	12.67	-3.07	-73.48	-17.91	-3.07	-1.32
			138	12.67	-3.07	-93.84	-41.10	-2.16	-1.32
482	Copertura	60, 61	0	12.78	-1.39	-93.56	30.36	-2.12	-1.05
			69	12.78	-1.39	-80.61	7.18	-1.40	-1.05
			138	12.78	-1.39	-83.66	-16.01	-0.67	-1.05
483	Copertura	61, 62	0	17.60	-0.28	-83.49	46.00	-0.66	-0.49
			69	17.60	-0.28	-59.75	22.81	-0.32	-0.49
			138	17.60	-0.28	-52.01	-0.37	0.01	-0.49
484	Copertura	62, 63	0	16.31	0.03	-51.93	37.72	0.01	-0.18
			69	16.31	0.03	-33.90	14.54	0.13	-0.18

			138	16.31	0.03	-31.87	-8.65	0.25	-0.18
485	Copertura	63, 64	0	16.32	0.01	-31.85	23.01	0.25	-0.03
			69	16.32	0.01	-23.97	-0.17	0.27	-0.03
			138	16.32	0.01	-32.09	-23.36	0.29	-0.03
486	Copertura	64, 65	0	16.30	-0.01	-32.13	8.45	0.29	0.13
			69	16.30	-0.01	-34.29	-14.73	0.20	0.13
			138	16.30	-0.01	-52.46	-37.92	0.12	0.13
487	Copertura	65, 66	0	17.26	0.31	-52.56	-0.50	0.12	0.44
			69	17.26	0.31	-60.90	-23.69	-0.18	0.44
			138	17.26	0.31	-85.25	-46.87	-0.49	0.44
488	Copertura	66, 67	0	12.07	1.47	-85.44	16.51	-0.50	1.02
			69	12.07	1.47	-82.04	-6.67	-1.21	1.02
			138	12.07	1.47	-94.64	-29.86	-1.91	1.02
489	Copertura	67, 68	0	11.94	3.22	-94.95	41.76	-1.96	1.29
			69	11.94	3.22	-74.13	18.58	-2.85	1.29
			138	11.94	3.22	-69.31	-4.61	-3.74	1.29
490	Copertura	68, 69	0	11.73	2.34	-69.78	90.25	-3.86	-0.92
			69	11.73	2.34	-15.51	67.06	-3.23	-0.92
			138	11.73	2.34	22.77	43.88	-2.60	-0.92
491	Copertura	69, 70	0	5.92	-8.76	22.63	97.53	-2.81	-8.81
			83	5.92	-8.76	92.09	69.60	4.52	-8.81
			166	5.92	-8.76	138.34	41.67	11.84	-8.81
492	Copertura	1	0	-133.68	4.57	9.49	-3.98	-15.64	-5.99
			220	-133.68	4.57	0.74	-3.98	-2.46	-5.99
			440	-133.68	4.57	-8.00	-3.98	10.72	-5.99
493	Copertura	2	0	-69.10	-0.12	11.30	-7.80	-0.62	-0.30
			220	-69.10	-0.12	-5.86	-7.80	0.05	-0.30
			440	-69.10	-0.12	-23.01	-7.80	0.72	-0.30
494	Copertura	3	0	-95.72	-0.12	0.78	-2.06	-0.46	-0.21
			220	-95.72	-0.12	-3.76	-2.06	0.00	-0.21
			440	-95.72	-0.12	-8.30	-2.06	0.45	-0.21
495	Copertura	4	0	-73.14	-0.04	-1.71	0.30	-0.30	-0.12
			220	-73.14	-0.04	-1.05	0.30	-0.03	-0.12
			440	-73.14	-0.04	-0.38	0.30	0.25	-0.12
496	Copertura	5	0	-48.83	0.00	-1.11	0.58	-0.19	-0.08
			220	-48.83	0.00	0.16	0.58	-0.02	-0.08
			440	-48.83	0.00	1.43	0.58	0.16	-0.08
497	Copertura	6	0	-35.81	0.01	-0.32	0.33	-0.11	-0.04
			220	-35.81	0.01	0.42	0.33	-0.01	-0.04
			440	-35.81	0.01	1.16	0.33	0.09	-0.04
498	Copertura	7	0	-30.16	0.00	0.03	0.17	-0.04	-0.02
			220	-30.16	0.00	0.40	0.17	0.00	-0.02
			440	-30.16	0.00	0.78	0.17	0.03	-0.02
499	Copertura	8	0	-30.47	0.00	0.03	0.17	0.02	0.01
			220	-30.47	0.00	0.41	0.17	0.00	0.01
			440	-30.47	0.00	0.78	0.17	-0.02	0.01
500	Copertura	9	0	-33.68	0.00	-0.31	0.33	0.09	0.04
			220	-33.68	0.00	0.41	0.33	0.01	0.04
			440	-33.68	0.00	1.14	0.33	-0.08	0.04
501	Copertura	10	0	-47.03	0.00	-1.09	0.56	0.18	0.07
			220	-47.03	0.00	0.15	0.56	0.02	0.07
			440	-47.03	0.00	1.39	0.56	-0.14	0.07
502	Copertura	11	0	-72.15	0.04	-1.70	0.28	0.29	0.12
			220	-72.15	0.04	-1.08	0.28	0.03	0.12
			440	-72.15	0.04	-0.46	0.28	-0.24	0.12
503	Copertura	12	0	-95.80	0.12	0.88	-2.13	0.46	0.21
			220	-95.80	0.12	-3.82	-2.13	0.00	0.21
			440	-95.80	0.12	-8.51	-2.13	-0.45	0.21
504	Copertura	13	0	-70.77	0.11	11.52	-7.91	0.61	0.30
			220	-70.77	0.11	-5.88	-7.91	-0.05	0.30
			440	-70.77	0.11	-23.28	-7.91	-0.70	0.30
505	Copertura	57	0	-124.40	-4.60	-9.97	4.16	-15.20	-5.80
			220	-124.40	-4.60	-0.83	4.16	-2.44	-5.80
			440	-124.40	-4.60	8.32	4.16	10.33	-5.80
506	Copertura	58	0	-67.42	0.12	-11.46	7.82	-0.61	-0.30
			220	-67.42	0.12	5.75	7.82	0.05	-0.30
			440	-67.42	0.12	22.96	7.82	0.71	-0.30
507	Copertura	59	0	-94.63	0.12	-0.86	2.10	-0.44	-0.20
			220	-94.63	0.12	3.75	2.10	0.00	-0.20
			440	-94.63	0.12	8.37	2.10	0.44	-0.20
508	Copertura	60	0	-71.46	0.04	1.68	-0.27	-0.28	-0.11
			220	-71.46	0.04	1.08	-0.27	-0.03	-0.11

			440	-71.46	0.04	0.49	-0.27	0.23	-0.11
509	Copertura	61	0	-46.87	0.00	1.07	-0.54	-0.17	-0.07
			220	-46.87	0.00	-0.11	-0.54	-0.02	-0.07
			440	-46.87	0.00	-1.30	-0.54	0.13	-0.07
510	Copertura	62	0	-33.88	0.00	0.31	-0.31	-0.08	-0.03
			220	-33.88	0.00	-0.36	-0.31	-0.01	-0.03
			440	-33.88	0.00	-1.04	-0.31	0.07	-0.03
511	Copertura	63	0	-31.66	0.00	-0.02	-0.15	-0.02	-0.01
			220	-31.66	0.00	-0.35	-0.15	0.00	-0.01
			440	-31.66	0.00	-0.69	-0.15	0.02	-0.01
512	Copertura	64	0	-31.81	0.00	-0.02	-0.15	0.04	0.02
			220	-31.81	0.00	-0.36	-0.15	0.00	0.02
			440	-31.81	0.00	-0.69	-0.15	-0.04	0.02
513	Copertura	65	0	-34.22	0.00	0.32	-0.31	0.10	0.04
			220	-34.22	0.00	-0.37	-0.31	0.01	0.04
			440	-34.22	0.00	-1.06	-0.31	-0.09	0.04
514	Copertura	66	0	-47.09	-0.01	1.12	-0.55	0.19	0.08
			220	-47.09	-0.01	-0.10	-0.55	0.02	0.08
			440	-47.09	-0.01	-1.32	-0.55	-0.16	0.08
515	Copertura	67	0	-71.62	-0.05	1.75	-0.27	0.30	0.13
			220	-71.62	-0.05	1.16	-0.27	0.03	0.13
			440	-71.62	-0.05	0.56	-0.27	-0.25	0.13
516	Copertura	68	0	-94.85	-0.12	-0.89	2.21	0.47	0.21
			220	-94.85	-0.12	3.97	2.21	0.00	0.21
			440	-94.85	-0.12	8.82	2.21	-0.46	0.21
517	Copertura	69	0	-69.50	-0.12	-11.99	8.22	0.63	0.31
			220	-69.50	-0.12	6.11	8.22	-0.05	0.31
			440	-69.50	-0.12	24.20	8.22	-0.72	0.31
518	Primo Impalcato	1, 74	0	15.91	0.14	0.00	0.00	1.54	0.52
			118	15.91	0.14	0.00	0.00	0.94	0.52
			235	15.91	0.14	0.00	0.00	0.33	0.52
519	Copertura	74, 2	0	-46.87	-0.05	0.00	0.00	0.23	-0.31
			118	-46.87	-0.05	0.00	0.00	0.59	-0.31
			235	-46.87	-0.05	0.00	0.00	0.95	-0.31
520	Primo Impalcato	6, 71	0	-4.78	0.00	0.00	0.00	-0.03	-0.01
			115	-4.78	0.00	0.00	0.00	-0.01	-0.01
			231	-4.78	0.00	0.00	0.00	0.00	-0.01
521	Copertura	71, 7	0	-11.49	0.00	0.00	0.00	-0.02	0.00
			115	-11.49	0.00	0.00	0.00	-0.02	0.00
			231	-11.49	0.00	0.00	0.00	-0.02	0.00
522	Primo Impalcato	9, 72	0	-16.36	0.00	0.00	0.00	-0.04	-0.01
			115	-16.36	0.00	0.00	0.00	-0.03	-0.01
			231	-16.36	0.00	0.00	0.00	-0.02	-0.01
523	Copertura	72, 10	0	-3.89	0.00	0.00	0.00	0.00	0.02
			115	-3.89	0.00	0.00	0.00	-0.02	0.02
			231	-3.89	0.00	0.00	0.00	-0.04	0.02
524	Copertura	73, 13	0	-46.79	0.05	0.00	0.00	-0.21	0.32
			118	-46.79	0.05	0.00	0.00	-0.59	0.32
			235	-46.79	0.05	0.00	0.00	-0.97	0.32
525	Primo Impalcato	14, 73	0	16.36	-0.15	0.00	0.00	-1.54	-0.50
			118	16.36	-0.15	0.00	0.00	-0.95	-0.50
			235	16.36	-0.15	0.00	0.00	-0.36	-0.50
526	Primo Impalcato	57, 75	0	15.95	-0.14	0.00	0.00	-1.56	-0.52
			118	15.95	-0.14	0.00	0.00	-0.94	-0.52
			235	15.95	-0.14	0.00	0.00	-0.33	-0.52
527	Copertura	75, 58	0	-45.40	0.05	0.00	0.00	-0.23	0.31
			118	-45.40	0.05	0.00	0.00	-0.59	0.31
			235	-45.40	0.05	0.00	0.00	-0.95	0.31
528	Copertura	77, 61	0	-4.42	0.00	0.00	0.00	0.00	0.02
			115	-4.42	0.00	0.00	0.00	-0.02	0.02
			231	-4.42	0.00	0.00	0.00	-0.04	0.02
529	Primo Impalcato	62, 77	0	-15.86	0.00	0.00	0.00	-0.03	-0.01
			115	-15.86	0.00	0.00	0.00	-0.02	-0.01
			231	-15.86	0.00	0.00	0.00	-0.01	-0.01
530	Primo Impalcato	65, 78	0	-17.08	0.00	0.00	0.00	0.03	0.01
			115	-17.08	0.00	0.00	0.00	0.02	0.01

			231	-17.08	0.00	0.00	0.00	0.01	0.01
531	Copertura	78, 66	0	-3.35	0.00	0.00	0.00	0.00	-0.02
			115	-3.35	0.00	0.00	0.00	0.02	-0.02
			231	-3.35	0.00	0.00	0.00	0.04	-0.02
532	Primo Impalcato	69, 76	0	-47.49	-0.05	0.00	0.00	-1.00	-0.32
			118	-47.49	-0.05	0.00	0.00	-0.62	-0.32
			235	-47.49	-0.05	0.00	0.00	-0.24	-0.32
533	Copertura	76, 70	0	16.94	0.15	0.00	0.00	-0.34	0.55
			118	16.94	0.15	0.00	0.00	-0.99	0.55
			235	16.94	0.15	0.00	0.00	-1.64	0.55
534	Copertura	1, 74	0	-46.87	0.01	0.00	0.00	-1.12	-0.53
			118	-46.87	0.01	0.00	0.00	-0.50	-0.53
			235	-46.87	0.01	0.00	0.00	0.13	-0.53
535	Copertura	74, 2	0	15.91	0.03	0.00	0.00	0.36	0.29
			118	15.91	0.03	0.00	0.00	0.02	0.29
			235	15.91	0.03	0.00	0.00	-0.32	0.29
536	Copertura	6, 71	0	-11.49	0.00	0.00	0.00	0.00	0.01
			115	-11.49	0.00	0.00	0.00	-0.01	0.01
			231	-11.49	0.00	0.00	0.00	-0.02	0.01
537	Copertura	71, 7	0	-4.78	0.00	0.00	0.00	0.00	0.00
			115	-4.78	0.00	0.00	0.00	0.00	0.00
			231	-4.78	0.00	0.00	0.00	0.00	0.00
538	Copertura	9, 72	0	-3.89	0.00	0.00	0.00	0.00	0.00
			115	-3.89	0.00	0.00	0.00	0.00	0.00
			231	-3.89	0.00	0.00	0.00	0.00	0.00
539	Copertura	72, 10	0	-16.36	0.00	0.00	0.00	-0.02	-0.02
			115	-16.36	0.00	0.00	0.00	0.01	-0.02
			231	-16.36	0.00	0.00	0.00	0.04	-0.02
540	Copertura	73, 13	0	16.36	-0.03	0.00	0.00	-0.39	-0.31
			118	16.36	-0.03	0.00	0.00	-0.03	-0.31
			235	16.36	-0.03	0.00	0.00	0.33	-0.31
541	Copertura	14, 73	0	-46.79	-0.02	0.00	0.00	1.11	0.52
			118	-46.79	-0.02	0.00	0.00	0.50	0.52
			235	-46.79	-0.02	0.00	0.00	-0.11	0.52
542	Copertura	15, 125	0	489.42	-0.75	-65.85	-40.96	-1.78	-1.49
			75	489.42	-0.75	-113.85	-87.04	-0.66	-1.49
			150	489.42	-0.75	-196.41	-133.12	0.45	-1.49
543	Copertura	127, 16	0	502.70	2.19	-212.86	142.48	2.76	6.17
			75	502.70	2.19	-123.28	96.40	-1.87	6.17
			150	502.70	2.19	-68.26	50.32	-6.49	6.17
544	Copertura	17, 129	0	420.21	-0.17	27.45	-2.93	-0.24	-0.24
			75	420.21	-0.17	9.59	-44.69	-0.06	-0.24
			150	420.21	-0.17	-39.59	-86.45	0.13	-0.24
545	Copertura	130, 18	0	420.05	0.18	-39.97	86.23	0.28	0.26
			75	420.05	0.18	9.04	44.47	0.08	0.26
			150	420.05	0.18	26.74	2.71	-0.11	0.26
546	Copertura	19, 135	0	431.13	-0.04	35.48	-5.69	-0.05	0.03
			75	431.13	-0.04	15.55	-47.45	-0.08	0.03
			150	431.13	-0.04	-35.70	-89.21	-0.10	0.03
547	Copertura	134, 20	0	430.06	0.05	-34.33	88.45	0.14	-0.01
			75	430.06	0.05	16.35	46.69	0.15	-0.01
			150	430.06	0.05	35.70	4.93	0.16	-0.01
548	Copertura	21, 136	0	432.49	-0.01	37.74	-11.34	-0.08	0.02
			75	432.49	-0.01	13.57	-53.10	-0.09	0.02
			150	432.49	-0.01	-41.91	-94.86	-0.10	0.02
549	Copertura	138, 22	0	432.17	-0.01	-41.43	94.63	0.07	-0.07
			75	432.17	-0.01	13.88	52.87	0.12	-0.07
			150	432.17	-0.01	37.88	11.11	0.18	-0.07
550	Copertura	23, 141	0	432.59	0.00	37.97	-13.24	-0.07	-0.01
			75	432.59	0.00	12.38	-55.00	-0.07	-0.01
			150	432.59	0.00	-44.53	-96.76	-0.07	-0.01
551	Copertura	142, 24	0	432.59	-0.02	-44.41	96.78	0.05	-0.03
			75	432.59	-0.02	12.52	55.02	0.07	-0.03
			150	432.59	-0.02	38.12	13.26	0.10	-0.03
552	Copertura	25, 145	0	433.74	0.01	38.79	-14.33	-0.03	0.00
			75	433.74	0.01	12.39	-56.09	-0.03	0.00
			150	433.74	0.01	-45.34	-97.85	-0.03	0.00
553	Copertura	146, 26	0	432.61	-0.10	-44.44	96.91	-0.07	-0.08
			75	432.61	-0.10	12.59	55.15	-0.01	-0.08
			150	432.61	-0.10	38.30	13.39	0.05	-0.08
554	Copertura	150, 27	0	432.02	-0.20	-44.23	96.11	-0.14	-0.09

			75	432.02	-0.20	12.19	54.35	-0.07	-0.09
			150	432.02	-0.20	37.30	12.59	0.00	-0.09
555	Copertura	28, 149	0	432.78	-0.30	37.55	-13.23	-0.04	-0.19
			75	432.78	-0.30	11.96	-54.99	0.10	-0.19
			150	432.78	-0.30	-44.94	-96.75	0.24	-0.19
556	Copertura	154, 29	0	431.13	-0.39	-43.65	94.68	-0.34	-0.24
			75	431.13	-0.39	11.70	52.92	-0.16	-0.24
			150	431.13	-0.39	35.73	11.16	0.02	-0.24
557	Copertura	30, 153	0	430.92	-0.40	35.51	-10.97	-0.01	-0.24
			75	430.92	-0.40	11.62	-52.73	0.17	-0.24
			150	430.92	-0.40	-43.59	-94.49	0.35	-0.24
558	Copertura	158, 31	0	430.74	-0.39	-43.25	94.28	-0.37	-0.23
			75	430.74	-0.39	11.80	52.52	-0.19	-0.23
			150	430.74	-0.39	35.53	10.76	-0.02	-0.23
559	Copertura	32, 157	0	430.46	-0.44	35.15	-10.50	0.02	-0.26
			75	430.46	-0.44	11.62	-52.26	0.21	-0.26
			150	430.46	-0.44	-43.23	-94.02	0.40	-0.26
560	Copertura	162, 33	0	430.27	-0.47	-43.11	93.83	-0.45	-0.29
			75	430.27	-0.47	11.60	52.07	-0.23	-0.29
			150	430.27	-0.47	35.00	10.31	-0.01	-0.29
561	Copertura	34, 161	0	430.55	-0.48	35.01	-10.53	0.03	-0.28
			75	430.55	-0.48	11.45	-52.29	0.24	-0.28
			150	430.55	-0.48	-43.43	-94.05	0.45	-0.28
562	Copertura	166, 35	0	430.05	-0.48	-43.02	93.62	-0.45	-0.28
			75	430.05	-0.48	11.53	51.86	-0.24	-0.28
			150	430.05	-0.48	34.77	10.10	-0.02	-0.28
563	Copertura	36, 165	0	430.64	-0.53	34.83	-10.58	0.02	-0.31
			75	430.64	-0.53	11.24	-52.34	0.26	-0.31
			150	430.64	-0.53	-43.68	-94.10	0.49	-0.31
564	Copertura	170, 37	0	429.97	-0.54	-43.17	93.47	-0.48	-0.33
			75	429.97	-0.54	11.27	51.71	-0.23	-0.33
			150	429.97	-0.54	34.39	9.95	0.01	-0.33
565	Copertura	38, 169	0	430.36	-0.57	34.44	-10.28	-0.01	-0.34
			75	430.36	-0.57	11.07	-52.04	0.25	-0.34
			150	430.36	-0.57	-43.62	-93.80	0.51	-0.34
566	Copertura	175, 39	0	430.19	-0.55	-43.32	93.40	-0.45	-0.35
			75	430.19	-0.55	11.06	51.64	-0.19	-0.35
			150	430.19	-0.55	34.13	9.88	0.08	-0.35
567	Copertura	40, 173	0	429.61	-0.61	33.56	-9.38	-0.06	-0.37
			75	429.61	-0.61	10.86	-51.14	0.21	-0.37
			150	429.61	-0.61	-43.15	-92.90	0.49	-0.37
568	Copertura	178, 41	0	431.16	-0.43	-44.41	94.42	-0.26	-0.25
			75	431.16	-0.43	10.75	52.66	-0.07	-0.25
			150	431.16	-0.43	34.59	10.90	0.12	-0.25
569	Copertura	42, 177	0	428.65	-0.65	32.01	-8.74	-0.13	-0.39
			75	428.65	-0.65	9.79	-50.50	0.16	-0.39
			150	428.65	-0.65	-43.75	-92.26	0.45	-0.39
570	Copertura	43, 181	0	430.98	0.02	38.06	-11.24	-0.03	0.00
			75	430.98	0.02	13.97	-53.00	-0.03	0.00
			150	430.98	0.02	-41.43	-94.76	-0.03	0.00
571	Copertura	182, 44	0	432.57	-0.20	-42.95	96.04	-0.17	-0.19
			75	432.57	-0.20	13.42	54.28	-0.03	-0.19
			150	432.57	-0.20	38.47	12.52	0.11	-0.19
572	Copertura	45, 185	0	432.20	0.02	37.93	-12.17	-0.10	-0.01
			75	432.20	0.02	13.14	-53.93	-0.09	-0.01
			150	432.20	0.02	-42.97	-95.69	-0.09	-0.01
573	Copertura	186, 46	0	432.67	-0.02	-43.29	96.08	0.06	-0.02
			75	432.67	-0.02	13.12	54.32	0.08	-0.02
			150	432.67	-0.02	38.20	12.56	0.09	-0.02
574	Copertura	47, 189	0	432.72	0.03	38.31	-12.89	-0.13	-0.01
			75	432.72	0.03	12.98	-54.65	-0.12	-0.01
			150	432.72	0.03	-43.66	-96.41	-0.12	-0.01
575	Copertura	190, 48	0	431.67	-0.04	-42.71	95.55	0.07	-0.04
			75	431.67	-0.04	13.29	53.79	0.10	-0.04
			150	431.67	-0.04	37.98	12.03	0.12	-0.04
576	Copertura	49, 193	0	433.10	0.03	38.18	-11.60	-0.15	-0.04
			75	433.10	0.03	13.81	-53.36	-0.13	-0.04
			150	433.10	0.03	-41.87	-95.12	-0.10	-0.04
577	Copertura	195, 50	0	431.56	-0.03	-40.22	93.93	0.08	0.03
			75	431.56	-0.03	14.57	52.17	0.05	0.03
			150	431.56	-0.03	38.03	10.41	0.03	0.03
578	Copertura	51, 197	0	431.81	0.05	36.04	-6.17	-0.15	-0.05

			75	431.81	0.05	15.75	-47.93	-0.11	-0.05
			150	431.81	0.05	-35.86	-89.69	-0.08	-0.05
579	Copertura	199, 52	0	429.24	-0.07	-33.61	87.58	0.01	0.03
			75	429.24	-0.07	16.41	45.82	-0.01	0.03
			150	429.24	-0.07	35.12	4.06	-0.03	0.03
580	Copertura	53, 201	0	419.91	0.19	27.75	-3.10	0.13	0.23
			75	419.91	0.19	9.76	-44.86	-0.04	0.23
			150	419.91	0.19	-39.54	-86.62	-0.22	0.23
581	Copertura	202, 54	0	419.00	-0.35	-38.72	85.91	-0.40	-0.70
			75	419.00	-0.35	10.06	44.15	0.13	-0.70
			150	419.00	-0.35	27.51	2.39	0.65	-0.70
582	Copertura	55, 205	0	492.97	0.68	-66.02	-41.69	1.48	1.48
			75	492.97	0.68	-114.56	-87.77	0.37	1.48
			150	492.97	0.68	-197.67	-133.85	-0.74	1.48
583	Copertura	206, 56	0	500.03	-0.80	-205.76	139.06	-0.72	-1.82
			75	500.03	-0.80	-118.74	92.98	0.65	-1.82
			150	500.03	-0.80	-66.28	46.90	2.01	-1.82
584	Copertura	57, 75	0	-45.40	-0.02	0.00	0.00	1.14	0.54
			118	-45.40	-0.02	0.00	0.00	0.51	0.54
			235	-45.40	-0.02	0.00	0.00	-0.13	0.54
585	Copertura	75, 58	0	15.95	-0.03	0.00	0.00	-0.36	-0.29
			118	15.95	-0.03	0.00	0.00	-0.02	-0.29
			235	15.95	-0.03	0.00	0.00	0.32	-0.29
586	Copertura	77, 61	0	-15.86	0.00	0.00	0.00	-0.01	-0.02
			115	-15.86	0.00	0.00	0.00	0.01	-0.02
			231	-15.86	0.00	0.00	0.00	0.04	-0.02
587	Copertura	62, 77	0	-4.42	0.00	0.00	0.00	0.00	0.00
			115	-4.42	0.00	0.00	0.00	0.00	0.00
			231	-4.42	0.00	0.00	0.00	0.00	0.00
588	Copertura	65, 78	0	-3.35	0.00	0.00	0.00	0.00	0.00
			115	-3.35	0.00	0.00	0.00	0.00	0.00
			231	-3.35	0.00	0.00	0.00	0.00	0.00
589	Copertura	78, 66	0	-17.08	0.00	0.00	0.00	0.01	0.02
			115	-17.08	0.00	0.00	0.00	-0.01	0.02
			231	-17.08	0.00	0.00	0.00	-0.04	0.02
590	Copertura	69, 76	0	16.94	0.03	0.00	0.00	0.34	0.30
			118	16.94	0.03	0.00	0.00	-0.02	0.30
			235	16.94	0.03	0.00	0.00	-0.38	0.30
591	Copertura	76, 70	0	-47.49	0.02	0.00	0.00	-0.14	-0.57
			118	-47.49	0.02	0.00	0.00	0.53	-0.57
			235	-47.49	0.02	0.00	0.00	1.20	-0.57
592	Copertura	79, 81	0	1.17	0.53	-5.10	6.38	18.14	21.31
			80	1.17	0.53	-0.02	6.38	1.20	21.31
			159	1.17	0.53	5.05	6.38	-15.74	21.31
593	Copertura	80, 82	0	0.06	0.13	-2.67	3.81	-6.53	-2.73
			66	0.06	0.13	-0.15	3.81	-4.73	-2.73
			132	0.06	0.13	2.36	3.81	-2.93	-2.73
594	Copertura	83, 84	0	-0.78	-0.01	-0.74	1.02	-0.14	-0.26
			66	-0.78	-0.01	-0.07	1.02	0.03	-0.26
			132	-0.78	-0.01	0.60	1.02	0.20	-0.26
595	Copertura	85, 86	0	-3.26	0.00	-0.26	0.57	0.03	0.02
			66	-3.26	0.00	0.12	0.57	0.02	0.02
			132	-3.26	0.00	0.50	0.57	0.00	0.02
596	Copertura	87, 88	0	-5.52	0.00	-1.55	2.69	-0.03	0.01
			66	-5.52	0.00	0.22	2.69	-0.03	0.01
			132	-5.52	0.00	2.00	2.69	-0.04	0.01
597	Copertura	89, 90	0	-2.38	0.00	-2.98	4.64	-0.03	-0.01
			66	-2.38	0.00	0.08	4.64	-0.02	-0.01
			132	-2.38	0.00	3.15	4.64	-0.02	-0.01
598	Copertura	91, 92	0	-1.56	0.00	-3.56	5.47	-0.02	-0.01
			66	-1.56	0.00	0.05	5.47	-0.02	-0.01
			132	-1.56	0.00	3.66	5.47	-0.01	-0.01
599	Copertura	93, 94	0	4.97	0.00	-3.17	4.40	-0.03	0.00
			66	4.97	0.00	-0.26	4.40	-0.02	0.00
			132	4.97	0.00	2.64	4.40	-0.02	0.00
600	Copertura	95, 96	0	7.36	0.00	-1.50	1.87	0.04	0.00
			66	7.36	0.00	-0.26	1.87	0.04	0.00
			132	7.36	0.00	0.98	1.87	0.04	0.00
601	Copertura	97, 106	0	0.49	0.00	0.45	-0.73	0.10	-0.02
			66	0.49	0.00	-0.03	-0.73	0.11	-0.02
			132	0.49	0.00	-0.52	-0.73	0.12	-0.02
602	Copertura	98, 99	0	-0.30	0.01	-2.09	2.96	-1.03	-0.66

			66	-0.30	0.01	-0.14	2.96	-0.60	-0.66
			132	-0.30	0.01	1.81	2.96	-0.17	-0.66
603	Copertura	100, 101	0	-0.66	-0.01	-0.05	-0.08	0.05	0.00
			66	-0.66	-0.01	-0.11	-0.08	0.05	0.00
			132	-0.66	-0.01	-0.16	-0.08	0.06	0.00
604	Copertura	102, 103	0	-5.39	0.00	0.36	-0.35	0.00	0.00
			66	-5.39	0.00	0.13	-0.35	0.01	0.00
			132	-5.39	0.00	-0.10	-0.35	0.01	0.00
605	Copertura	104, 105	0	-1.55	0.00	-0.46	0.60	-0.05	-0.06
			66	-1.55	0.00	-0.06	0.60	-0.01	-0.06
			132	-1.55	0.00	0.34	0.60	0.03	-0.06
606	Copertura	107, 108	0	-0.81	0.00	2.00	-3.21	-0.39	0.79
			66	-0.81	0.00	-0.12	-3.21	-0.91	0.79
			132	-0.81	0.00	-2.24	-3.21	-1.43	0.79
607	Copertura	109, 110	0	1.84	0.49	3.70	-4.67	-11.20	-16.90
			80	1.84	0.49	-0.01	-4.67	2.24	-16.90
			159	1.84	0.49	-3.72	-4.67	15.67	-16.90
608	Copertura	111, 112	0	-1.25	0.06	-0.71	0.97	-0.05	-0.07
			66	-1.25	0.06	-0.07	0.97	-0.01	-0.07
			132	-1.25	0.06	0.56	0.97	0.04	-0.07
609	Copertura	113, 114	0	-0.14	0.00	-0.72	1.21	-0.05	-0.08
			66	-0.14	0.00	0.08	1.21	0.01	-0.08
			132	-0.14	0.00	0.88	1.21	0.06	-0.08
610	Copertura	115, 116	0	11.45	0.00	-0.53	0.26	-0.06	-0.10
			66	11.45	0.00	-0.35	0.26	0.00	-0.10
			132	11.45	0.00	-0.18	0.26	0.06	-0.10
611	Copertura	117, 118	0	0.81	0.00	0.68	-0.94	0.01	-0.01
			66	0.81	0.00	0.06	-0.94	0.01	-0.01
			132	0.81	0.00	-0.56	-0.94	0.02	-0.01
612	Copertura	119, 120	0	-0.28	0.02	1.62	-2.63	0.16	0.26
			66	-0.28	0.02	-0.11	-2.63	-0.02	0.26
			132	-0.28	0.02	-1.85	-2.63	-0.19	0.26
613	Copertura	121, 122	0	0.01	-0.27	4.28	-6.70	-1.63	1.16
			66	0.01	-0.27	-0.15	-6.70	-2.39	1.16
			132	0.01	-0.27	-4.57	-6.70	-3.15	1.16
614	Copertura	124, 125	0	-893.52	0.09	-45.50	30.46	2.04	1.45
			99	-893.52	0.09	-15.27	30.46	0.61	1.45
			198	-893.52	0.09	14.96	30.46	-0.83	1.45
615	Copertura	125, 127	0	-165.86	-0.14	-181.45	475.09	-0.11	-0.04
			775	-165.86	-0.14	1655.36	-1.07	0.21	-0.04
			1550	-165.86	-0.14	-198.07	-477.23	0.53	-0.04
616	Copertura	126, 127	0	-911.09	-0.30	-45.66	30.45	-9.11	-6.21
			99	-911.09	-0.30	-15.44	30.45	-2.95	-6.21
			198	-911.09	-0.30	14.79	30.45	3.22	-6.21
617	Copertura	128, 129	0	-756.96	0.03	-42.22	29.36	0.24	0.24
			99	-756.96	0.03	-13.08	29.36	0.01	0.24
			198	-756.96	0.03	16.07	29.36	-0.23	0.24
618	Copertura	129, 130	0	-132.59	0.00	-23.52	431.49	-0.02	-0.01
			775	-132.59	0.00	1648.41	-0.03	0.04	-0.01
			1550	-132.59	0.00	-23.93	-431.55	0.11	-0.01
619	Copertura	131, 130	0	-756.74	-0.03	-42.18	29.33	-0.29	-0.27
			99	-756.74	-0.03	-13.07	29.33	-0.02	-0.27
			198	-756.74	-0.03	16.05	29.33	0.25	-0.27
620	Copertura	132, 135	0	-760.99	0.01	-42.53	29.68	-0.13	-0.04
			99	-760.99	0.01	-13.07	29.68	-0.09	-0.04
			198	-760.99	0.01	16.39	29.68	-0.05	-0.04
621	Copertura	133, 134	0	-759.56	-0.01	-42.49	29.67	0.05	-0.01
			99	-759.56	-0.01	-13.04	29.67	0.05	-0.01
			198	-759.56	-0.01	16.40	29.67	0.06	-0.01
622	Copertura	135, 134	0	-124.50	0.00	-19.31	431.61	-0.13	-0.01
			775	-124.50	0.00	1653.52	0.09	-0.01	-0.01
			1550	-124.50	0.00	-17.93	-431.43	0.11	-0.01
623	Copertura	137, 136	0	-769.32	0.00	-42.78	29.85	-0.08	-0.03
			99	-769.32	0.00	-13.16	29.85	-0.05	-0.03
			198	-769.32	0.00	16.47	29.85	-0.02	-0.03
624	Copertura	136, 138	0	-129.33	0.00	-25.45	431.55	-0.11	-0.01
			775	-129.33	0.00	1646.94	0.03	-0.01	-0.01
			1550	-129.33	0.00	-24.96	-431.49	0.09	-0.01
625	Copertura	139, 138	0	-768.89	0.00	-42.77	29.85	0.09	0.06
			99	-768.89	0.00	-13.15	29.85	0.03	0.06
			198	-768.89	0.00	16.47	29.85	-0.02	0.06
626	Copertura	140, 141	0	-772.13	0.00	-42.85	29.90	-0.01	0.00

			99	-772.13	0.00	-13.17	29.90	-0.01	0.00
			198	-772.13	0.00	16.50	29.90	0.00	0.00
627	Copertura	141, 142	0	-131.32	0.00	-28.03	431.53	-0.07	-0.01
			775	-131.32	0.00	1644.18	0.01	0.00	-0.01
			1550	-131.32	0.00	-27.90	-431.51	0.07	-0.01
628	Copertura	143, 142	0	-772.13	0.00	-42.85	29.90	0.02	0.02
			99	-772.13	0.00	-13.17	29.90	0.00	0.02
			198	-772.13	0.00	16.51	29.90	-0.03	0.02
629	Copertura	144, 145	0	-773.79	0.00	-42.91	29.97	-0.01	0.00
			99	-773.79	0.00	-13.16	29.97	0.00	0.00
			198	-773.79	0.00	16.58	29.97	0.00	0.00
630	Copertura	145, 146	0	-131.38	0.01	-28.76	431.58	-0.03	0.00
			775	-131.38	0.01	1643.81	0.06	0.00	0.00
			1550	-131.38	0.01	-27.90	-431.46	0.03	0.00
631	Copertura	147, 146	0	-772.25	0.01	-42.85	29.92	0.00	0.08
			99	-772.25	0.01	-13.16	29.92	-0.08	0.08
			198	-772.25	0.01	16.53	29.92	-0.15	0.08
632	Copertura	148, 149	0	-772.28	0.02	-42.89	29.95	0.05	0.19
			99	-772.28	0.02	-13.16	29.95	-0.14	0.19
			198	-772.28	0.02	16.56	29.95	-0.33	0.19
633	Copertura	149, 150	0	-131.21	-0.07	-28.38	431.67	0.01	0.00
			775	-131.21	-0.07	1644.93	0.04	0.00	0.00
			1550	-131.21	-0.07	-27.72	-431.59	-0.01	0.00
634	Copertura	151, 150	0	-771.23	0.01	-42.84	29.90	0.01	0.10
			99	-771.23	0.01	-13.17	29.90	-0.09	0.10
			198	-771.23	0.01	16.51	29.90	-0.18	0.10
635	Copertura	152, 153	0	-769.00	0.03	-42.82	29.87	0.05	0.25
			99	-769.00	0.03	-13.18	29.87	-0.20	0.25
			198	-769.00	0.03	16.46	29.87	-0.44	0.25
636	Copertura	153, 154	0	-130.64	-0.09	-27.13	431.72	0.04	0.01
			775	-130.64	-0.09	1646.57	0.00	0.00	0.01
			1551	-130.64	-0.09	-27.17	-431.73	-0.04	0.01
637	Copertura	155, 154	0	-769.29	0.03	-42.83	29.88	0.07	0.25
			99	-769.29	0.03	-13.18	29.88	-0.18	0.25
			198	-769.29	0.03	16.48	29.88	-0.42	0.25
638	Copertura	156, 157	0	-768.35	0.03	-42.82	29.86	0.05	0.26
			99	-768.35	0.03	-13.18	29.86	-0.21	0.26
			198	-768.35	0.03	16.46	29.86	-0.48	0.26
639	Copertura	157, 158	0	-130.62	-0.10	-26.78	431.76	0.07	0.01
			775	-130.62	-0.10	1647.26	0.00	0.00	0.01
			1551	-130.62	-0.10	-26.78	-431.76	-0.07	0.01
640	Copertura	159, 158	0	-768.74	0.03	-42.82	29.87	0.06	0.24
			99	-768.74	0.03	-13.18	29.87	-0.18	0.24
			198	-768.74	0.03	16.47	29.87	-0.41	0.24
641	Copertura	160, 161	0	-768.48	0.04	-42.84	29.89	0.05	0.29
			99	-768.48	0.04	-13.18	29.89	-0.24	0.29
			198	-768.48	0.04	16.48	29.89	-0.52	0.29
642	Copertura	161, 162	0	-130.61	-0.11	-26.94	431.84	0.08	0.01
			776	-130.61	-0.11	1647.66	0.02	0.00	0.01
			1551	-130.61	-0.11	-26.64	-431.80	-0.09	0.01
643	Copertura	163, 162	0	-768.10	0.04	-42.82	29.87	0.08	0.30
			99	-768.10	0.04	-13.17	29.87	-0.21	0.30
			198	-768.10	0.04	16.47	29.87	-0.51	0.30
644	Copertura	164, 165	0	-768.65	0.04	-42.87	29.92	0.06	0.32
			99	-768.65	0.04	-13.18	29.92	-0.26	0.32
			198	-768.65	0.04	16.51	29.92	-0.57	0.32
645	Copertura	165, 166	0	-130.63	-0.12	-27.17	431.92	0.08	0.01
			776	-130.63	-0.12	1648.06	0.04	0.00	0.01
			1551	-130.63	-0.12	-26.55	-431.84	-0.09	0.01
646	Copertura	167, 166	0	-767.84	0.04	-42.83	29.88	0.08	0.29
			99	-767.84	0.04	-13.18	29.88	-0.22	0.29
			198	-767.84	0.04	16.48	29.88	-0.51	0.29
647	Copertura	168, 169	0	-768.25	0.04	-42.89	29.93	0.07	0.35
			99	-768.25	0.04	-13.18	29.93	-0.28	0.35
			198	-768.25	0.04	16.53	29.93	-0.62	0.35
648	Copertura	169, 170	0	-130.59	-0.13	-27.09	431.97	0.06	0.01
			776	-130.59	-0.13	1648.54	0.03	0.00	0.01
			1552	-130.59	-0.13	-26.67	-431.92	-0.07	0.01
649	Copertura	171, 170	0	-767.70	0.04	-42.85	29.90	0.09	0.34
			99	-767.70	0.04	-13.17	29.90	-0.24	0.34
			198	-767.70	0.04	16.50	29.90	-0.58	0.34
650	Copertura	172, 173	0	-766.93	0.05	-42.86	29.91	0.08	0.37

			99	-766.93	0.05	-13.18	29.91	-0.29	0.37
			198	-766.93	0.05	16.50	29.91	-0.67	0.37
651	Copertura	173, 175	0	-130.37	-0.14	-26.65	431.99	0.02	0.00
			776	-130.37	-0.14	1649.14	-0.01	0.00	0.00
			1552	-130.37	-0.14	-26.81	-432.01	-0.03	0.00
652	Copertura	174, 175	0	-767.71	0.04	-42.87	29.92	0.11	0.35
			99	-767.71	0.04	-13.18	29.92	-0.24	0.35
			198	-767.71	0.04	16.51	29.92	-0.59	0.35
653	Copertura	176, 177	0	-766.07	0.05	-42.84	29.87	0.07	0.38
			99	-766.07	0.05	-13.19	29.87	-0.31	0.38
			198	-766.07	0.05	16.46	29.87	-0.69	0.38
654	Copertura	177, 178	0	-130.70	-0.16	-27.29	432.04	-0.04	0.00
			776	-130.70	-0.16	1648.86	-0.04	-0.01	0.00
			1552	-130.70	-0.16	-27.91	-432.12	0.02	0.00
655	Copertura	179, 178	0	-769.44	0.02	-42.90	29.92	0.10	0.25
			99	-769.44	0.02	-13.20	29.92	-0.15	0.25
			198	-769.44	0.02	16.50	29.92	-0.39	0.25
656	Copertura	180, 181	0	-768.99	0.00	-42.77	29.84	-0.01	-0.01
			99	-768.99	0.00	-13.15	29.84	0.00	-0.01
			198	-768.99	0.00	16.47	29.84	0.00	-0.01
657	Copertura	181, 182	0	-130.59	0.02	-24.97	431.43	-0.03	-0.01
			775	-130.59	0.02	1646.45	-0.09	0.01	-0.01
			1550	-130.59	0.02	-26.40	-431.61	0.05	-0.01
658	Copertura	183, 182	0	-771.15	0.02	-42.83	29.91	0.06	0.18
			99	-771.15	0.02	-13.14	29.91	-0.12	0.18
			198	-771.15	0.02	16.54	29.91	-0.30	0.18
659	Copertura	184, 185	0	-770.49	0.00	-42.80	29.87	0.00	0.00
			99	-770.49	0.00	-13.15	29.87	0.01	0.00
			198	-770.49	0.00	16.50	29.87	0.01	0.00
660	Copertura	185, 186	0	-130.49	0.01	-26.47	431.50	-0.08	-0.01
			775	-130.49	0.01	1645.53	-0.02	0.00	-0.01
			1550	-130.49	0.01	-26.76	-431.54	0.08	-0.01
661	Copertura	187, 186	0	-771.12	0.00	-42.80	29.89	-0.01	0.01
			99	-771.12	0.00	-13.14	29.89	-0.02	0.01
			198	-771.12	0.00	16.53	29.89	-0.04	0.01
662	Copertura	188, 189	0	-771.67	-0.01	-42.84	29.91	0.01	-0.01
			99	-771.67	-0.01	-13.16	29.91	0.02	-0.01
			198	-771.67	-0.01	16.53	29.91	0.02	-0.01
663	Copertura	189, 190	0	-130.83	0.01	-27.14	431.58	-0.10	-0.01
			775	-130.83	0.01	1645.46	0.06	0.00	-0.01
			1550	-130.83	0.01	-26.22	-431.46	0.11	-0.01
664	Copertura	191, 190	0	-770.24	0.00	-42.78	29.86	-0.01	0.02
			99	-770.24	0.00	-13.14	29.86	-0.04	0.02
			198	-770.24	0.00	16.49	29.86	-0.06	0.02
665	Copertura	192, 193	0	-769.80	-0.01	-42.81	29.88	0.08	0.03
			99	-769.80	-0.01	-13.15	29.88	0.06	0.03
			198	-769.80	-0.01	16.50	29.88	0.03	0.03
666	Copertura	193, 195	0	-129.07	0.01	-25.37	431.63	-0.08	-0.01
			775	-129.07	0.01	1647.59	0.10	0.01	-0.01
			1550	-129.07	0.01	-23.74	-431.42	0.11	-0.01
667	Copertura	194, 195	0	-767.72	0.00	-42.73	29.83	-0.13	-0.04
			99	-767.72	0.00	-13.12	29.83	-0.09	-0.04
			198	-767.72	0.00	16.48	29.83	-0.04	-0.04
668	Copertura	196, 197	0	-761.75	-0.01	-42.56	29.72	0.14	0.04
			99	-761.75	-0.01	-13.06	29.72	0.10	0.04
			198	-761.75	-0.01	16.43	29.72	0.06	0.04
669	Copertura	197, 199	0	-124.36	0.00	-19.42	431.66	-0.04	-0.01
			775	-124.36	0.00	1653.79	0.14	0.02	-0.01
			1550	-124.36	0.00	-17.27	-431.38	0.07	-0.01
670	Copertura	198, 199	0	-758.24	0.01	-42.42	29.60	-0.16	-0.04
			99	-758.24	0.01	-13.04	29.60	-0.13	-0.04
			198	-758.24	0.01	16.34	29.60	-0.09	-0.04
671	Copertura	200, 201	0	-757.32	-0.04	-42.23	29.38	-0.23	-0.23
			99	-757.32	-0.04	-13.07	29.38	0.00	-0.23
			198	-757.32	-0.04	16.09	29.38	0.23	-0.23
672	Copertura	201, 202	0	-133.15	0.02	-23.46	431.57	-0.07	0.00
			775	-133.15	0.02	1649.09	0.05	-0.06	0.00
			1550	-133.15	0.02	-22.64	-431.47	-0.05	0.00
673	Copertura	203, 202	0	-756.10	0.05	-42.19	29.36	0.89	0.70
			99	-756.10	0.05	-13.06	29.36	0.19	0.70
			198	-756.10	0.05	16.08	29.36	-0.51	0.70
674	Copertura	204, 205	0	-895.39	-0.10	-45.59	30.52	-2.06	-1.49

			99	-895.39	-0.10	-15.30	30.52	-0.58	-1.49
			198	-895.39	-0.10	15.00	30.52	0.90	-1.49
675	Copertura	205, 206	0	-163.67	0.01	-182.67	475.64	-0.12	-0.01
			775	-163.67	0.01	1658.40	-0.52	-0.04	-0.01
			1550	-163.67	0.01	-190.77	-476.68	0.05	-0.01
676	Copertura	207, 206	0	-904.82	0.11	-45.82	30.63	2.48	1.81
			99	-904.82	0.11	-15.42	30.63	0.68	1.81
			198	-904.82	0.11	14.99	30.63	-1.11	1.81
677	Copertura	79	0	-128.59	3.08	3.92	-4.73	-7.93	-1.91
			125	-128.59	3.08	-1.99	-4.73	-5.55	-1.91
			250	-128.59	3.08	-7.90	-4.73	-3.16	-1.91
678	Copertura	124	0	-384.71	2.84	1.32	-1.44	615.05	184.88
			155	-384.71	2.84	-0.92	-1.44	328.49	184.88
			310	-384.71	2.84	-3.15	-1.44	41.92	184.88
679	Copertura	80	0	-390.10	-2.83	-0.47	-3.83	-204.51	-177.61
			45	-390.10	-2.83	-2.19	-3.83	-124.59	-177.61
			90	-390.10	-2.83	-3.91	-3.83	-44.66	-177.61
680	Copertura	128	0	-428.14	0.40	1.00	-0.97	561.49	125.18
			155	-428.14	0.40	-0.50	-0.97	367.46	125.18
			310	-428.14	0.40	-2.01	-0.97	173.42	125.18
681	Copertura	82	0	-427.78	1.46	0.14	-2.08	-280.60	-127.37
			43	-427.78	1.46	-0.75	-2.08	-226.27	-127.37
			85	-427.78	1.46	-1.64	-2.08	-171.94	-127.37
682	Copertura	132	0	-486.98	-0.13	0.58	-0.55	564.06	125.80
			155	-486.98	-0.13	-0.27	-0.55	369.08	125.80
			310	-486.98	-0.13	-1.12	-0.55	174.09	125.80
683	Copertura	83	0	-492.95	0.08	0.07	-1.77	-281.81	-125.26
			43	-492.95	0.08	-0.68	-1.77	-228.37	-125.26
			85	-492.95	0.08	-1.44	-1.77	-174.94	-125.26
684	Copertura	137	0	-512.61	-0.08	0.24	-0.22	566.86	130.07
			155	-512.61	-0.08	-0.11	-0.22	365.25	130.07
			310	-512.61	-0.08	-0.46	-0.22	163.64	130.07
685	Copertura	84	0	-514.50	-0.05	-0.08	0.17	-274.99	-130.07
			43	-514.50	-0.05	0.00	0.17	-219.51	-130.07
			85	-514.50	-0.05	0.07	0.17	-164.03	-130.07
686	Copertura	140	0	-531.78	-0.01	0.04	0.01	567.55	131.35
			155	-531.78	-0.01	0.05	0.01	363.97	131.35
			310	-531.78	-0.01	0.06	0.01	160.38	131.35
687	Copertura	85	0	-535.53	0.01	1.10	-2.57	-272.66	-131.28
			43	-535.53	0.01	0.01	-2.57	-216.67	-131.28
			85	-535.53	0.01	-1.09	-2.57	-160.67	-131.28
688	Copertura	144	0	-562.92	-0.01	-0.01	0.05	568.13	131.41
			155	-562.92	-0.01	0.06	0.05	364.44	131.41
			310	-562.92	-0.01	0.14	0.05	160.76	131.41
689	Copertura	86	0	-543.29	0.00	-0.92	0.97	-273.18	-131.02
			43	-543.29	0.00	-0.51	0.97	-217.29	-131.02
			85	-543.29	0.00	-0.09	0.97	-161.40	-131.02
690	Copertura	87	0	-535.67	-0.04	1.74	-5.65	-273.13	-130.97
			43	-535.67	-0.04	-0.67	-5.65	-217.27	-130.97
			85	-535.67	-0.04	-3.08	-5.65	-161.40	-130.97
691	Copertura	148	0	-552.60	0.04	-4.78	2.51	567.82	131.25
			155	-552.60	0.04	-0.88	2.51	364.38	131.25
			310	-552.60	0.04	3.01	2.51	160.94	131.25
692	Copertura	88	0	-514.92	0.02	-1.71	0.31	-273.51	-130.64
			43	-514.92	0.02	-1.58	0.31	-217.79	-130.64
			85	-514.92	0.02	-1.45	0.31	-162.06	-130.64
693	Copertura	152	0	-512.98	0.03	-6.49	3.44	567.02	130.69
			155	-512.98	0.03	-1.15	3.44	364.45	130.69
			310	-512.98	0.03	4.19	3.44	161.88	130.69
694	Copertura	89	0	-515.52	-0.03	0.83	-6.06	-273.69	-130.56
			43	-515.52	-0.03	-1.76	-6.06	-218.00	-130.56
			85	-515.52	-0.03	-4.34	-6.06	-162.31	-130.56
695	Copertura	156	0	-507.68	0.02	-7.11	3.83	566.96	130.54
			155	-507.68	0.02	-1.18	3.83	364.62	130.54
			310	-507.68	0.02	4.76	3.83	162.28	130.54
696	Copertura	90	0	-508.30	0.02	-0.64	-3.47	-273.72	-130.48
			43	-508.30	0.02	-2.12	-3.47	-218.06	-130.48
			85	-508.30	0.02	-3.60	-3.47	-162.41	-130.48
697	Copertura	160	0	-514.88	0.02	-7.87	4.25	567.18	130.56
			155	-514.88	0.02	-1.29	4.25	364.80	130.56
			310	-514.88	0.02	5.29	4.25	162.43	130.56
698	Copertura	91	0	-515.65	-0.03	0.58	-6.48	-273.71	-130.47

			43	-515.65	-0.03	-2.18	-6.48	-218.06	-130.47
			85	-515.65	-0.03	-4.95	-6.48	-162.41	-130.47
699	Copertura	164	0	-523.07	0.02	-8.63	4.66	567.41	130.60
			155	-523.07	0.02	-1.41	4.66	364.98	130.60
			310	-523.07	0.02	5.81	4.66	162.54	130.60
700	Copertura	92	0	-513.33	0.02	-0.38	-4.68	-273.75	-130.45
			43	-513.33	0.02	-2.37	-4.68	-218.10	-130.45
			85	-513.33	0.02	-4.37	-4.68	-162.46	-130.45
701	Copertura	168	0	-525.60	0.03	-9.39	5.06	567.44	130.50
			155	-525.60	0.03	-1.55	5.06	365.16	130.50
			310	-525.60	0.03	6.30	5.06	162.88	130.50
702	Copertura	93	0	-523.04	-0.03	-1.59	-1.85	-273.84	-130.52
			43	-523.04	-0.03	-2.38	-1.85	-218.16	-130.52
			85	-523.04	-0.03	-3.17	-1.85	-162.49	-130.52
703	Copertura	172	0	-513.36	0.03	-10.04	5.40	567.13	130.25
			155	-513.36	0.03	-1.66	5.40	365.24	130.25
			310	-513.36	0.03	6.71	5.40	163.36	130.25
704	Copertura	94	0	-512.65	0.02	1.62	-6.50	-273.56	-130.76
			43	-512.65	0.02	-1.15	-6.50	-217.78	-130.76
			85	-512.65	0.02	-3.92	-6.50	-162.00	-130.76
705	Copertura	176	0	-503.23	0.01	-10.87	5.98	566.71	130.37
			155	-503.23	0.01	-1.60	5.98	364.64	130.37
			310	-503.23	0.01	7.66	5.98	162.57	130.37
706	Copertura	180	0	-513.48	-0.02	-0.05	0.11	566.62	130.00
			155	-513.48	-0.02	0.12	0.11	365.12	130.00
			310	-513.48	-0.02	0.29	0.11	163.61	130.00
707	Copertura	95	0	-548.34	0.04	-2.01	2.00	-273.84	-130.57
			43	-548.34	0.04	-1.15	2.00	-218.15	-130.57
			85	-548.34	0.04	-0.30	2.00	-162.45	-130.57
708	Copertura	184	0	-533.21	0.00	-0.12	0.16	566.91	130.46
			155	-533.21	0.00	0.12	0.16	364.70	130.46
			310	-533.21	0.00	0.36	0.16	162.49	130.46
709	Copertura	96	0	-543.95	-0.04	2.33	-6.19	-272.94	-130.78
			43	-543.95	-0.04	-0.31	-6.19	-217.15	-130.78
			85	-543.95	-0.04	-2.95	-6.19	-161.36	-130.78
710	Copertura	188	0	-540.88	0.00	-0.25	0.25	567.43	130.81
			155	-540.88	0.00	0.15	0.25	364.68	130.81
			310	-540.88	0.00	0.54	0.25	161.92	130.81
711	Copertura	97	0	-532.78	0.07	-0.21	0.59	-273.02	-130.63
			43	-532.78	0.07	0.04	0.59	-217.30	-130.63
			85	-532.78	0.07	0.29	0.59	-161.58	-130.63
712	Copertura	192	0	-524.65	0.08	-0.45	0.46	567.11	129.94
			155	-524.65	0.08	0.26	0.46	365.70	129.94
			310	-524.65	0.08	0.96	0.46	164.28	129.94
713	Copertura	106	0	-518.21	-0.12	0.27	0.48	-275.09	-129.57
			43	-518.21	-0.12	0.48	0.48	-219.82	-129.57
			85	-518.21	-0.12	0.68	0.48	-164.55	-129.57
714	Copertura	196	0	-503.20	0.13	-0.77	0.75	564.33	125.79
			155	-503.20	0.13	0.39	0.75	369.35	125.79
			310	-503.20	0.13	1.55	0.75	174.37	125.79
715	Copertura	107	0	-474.70	-0.37	0.09	1.16	-281.96	-125.62
			43	-474.70	-0.37	0.58	1.16	-228.37	-125.62
			85	-474.70	-0.37	1.07	1.16	-174.79	-125.62
716	Copertura	200	0	-433.69	-0.40	-1.15	1.12	561.71	125.14
			155	-433.69	-0.40	0.58	1.12	367.75	125.14
			310	-433.69	-0.40	2.32	1.12	173.78	125.14
717	Copertura	108	0	-429.82	1.03	0.27	3.82	-279.49	-124.80
			43	-429.82	1.03	1.90	3.82	-226.26	-124.80
			85	-429.82	1.03	3.53	3.82	-173.02	-124.80
718	Copertura	204	0	-389.87	-2.85	-1.45	1.57	616.23	185.26
			155	-389.87	-2.85	0.99	1.57	329.08	185.26
			310	-389.87	-2.85	3.43	1.57	41.93	185.26
719	Copertura	109	0	-398.03	-4.68	-0.08	5.59	-191.09	-173.40
			43	-398.03	-4.68	2.30	5.59	-117.13	-173.40
			85	-398.03	-4.68	4.69	5.59	-43.16	-173.40
720	Copertura	110	0	-133.51	-7.83	3.59	3.51	-11.18	-8.00
			43	-133.51	-7.83	5.09	3.51	-7.77	-8.00
			85	-133.51	-7.83	6.58	3.51	-4.36	-8.00
721	Copertura	14	0	-122.21	-15.05	10.03	-5.90	29.46	19.40
			95	-122.21	-15.05	4.43	-5.90	11.03	19.40
			190	-122.21	-15.05	-1.17	-5.90	-7.40	19.40
722	Copertura	15	0	223.50	1.24	2.58	0.01	-41.96	-470.39

			65	223.50	1.24	2.58	0.01	263.80	-470.39
			130	223.50	1.24	2.59	0.01	569.55	-470.39
723	Copertura	16	0	227.04	-4.96	0.39	3.63	37.97	466.91
			65	227.04	-4.96	2.75	3.63	-265.52	466.91
			130	227.04	-4.96	5.10	3.63	-569.02	466.91
724	Copertura	17	0	89.81	0.20	2.10	-0.74	-36.62	-427.62
			65	89.81	0.20	1.62	-0.74	241.33	-427.62
			130	89.81	0.20	1.14	-0.74	519.28	-427.62
725	Copertura	18	0	89.16	-0.20	2.60	-1.59	36.66	427.35
			65	89.16	-0.20	1.57	-1.59	-241.12	427.35
			130	89.16	-0.20	0.53	-1.59	-518.89	427.35
726	Copertura	19	0	33.85	-0.03	1.26	-0.59	-37.25	-429.83
			65	33.85	-0.03	0.88	-0.59	242.14	-429.83
			130	33.85	-0.03	0.49	-0.59	521.53	-429.83
727	Copertura	20	0	24.99	0.02	1.56	-1.28	37.63	429.70
			65	24.99	0.02	0.72	-1.28	-241.67	429.70
			130	24.99	0.02	-0.11	-1.28	-520.97	429.70
728	Copertura	21	0	13.80	-0.02	0.52	-0.25	-37.20	-431.75
			65	13.80	-0.02	0.35	-0.25	243.44	-431.75
			130	13.80	-0.02	0.18	-0.25	524.08	-431.75
729	Copertura	22	0	10.52	0.04	0.18	0.00	37.31	431.69
			65	10.52	0.04	0.18	0.00	-243.29	431.69
			130	10.52	0.04	0.18	0.00	-523.88	431.69
730	Copertura	23	0	-3.50	0.00	0.03	0.00	-37.63	-432.57
			65	-3.50	0.00	0.03	0.00	243.54	-432.57
			130	-3.50	0.00	0.03	0.00	524.71	-432.57
731	Copertura	24	0	-6.58	0.02	-0.17	0.00	37.73	432.66
			65	-6.58	0.02	-0.17	0.00	-243.49	432.66
			130	-6.58	0.02	-0.16	0.00	-524.72	432.66
732	Copertura	25	0	-33.49	0.00	-0.08	0.05	-38.60	-433.71
			65	-33.49	0.00	-0.05	0.05	243.31	-433.71
			130	-33.49	0.00	-0.02	0.05	525.22	-433.71
733	Copertura	26	0	-15.84	-0.01	-3.06	3.02	38.08	432.95
			65	-15.84	-0.01	-1.10	3.02	-243.34	432.95
			130	-15.84	-0.01	0.86	3.02	-524.75	432.95
734	Copertura	27	0	-4.94	-0.02	-4.83	5.96	37.23	432.14
			65	-4.94	-0.02	-0.95	5.96	-243.67	432.14
			130	-4.94	-0.02	2.92	5.96	-524.56	432.14
735	Copertura	28	0	-24.18	-0.02	7.66	-8.88	-37.46	-432.62
			65	-24.18	-0.02	1.89	-8.88	243.74	-432.62
			130	-24.18	-0.02	-3.88	-8.88	524.94	-432.62
736	Copertura	29	0	9.40	-0.04	-10.03	11.87	35.84	430.86
			65	9.40	-0.04	-2.32	11.87	-244.22	430.86
			130	9.40	-0.04	5.40	11.87	-524.27	430.86
737	Copertura	30	0	13.23	-0.03	10.44	-12.08	-35.64	-430.66
			65	13.23	-0.03	2.58	-12.08	244.29	-430.66
			130	13.23	-0.03	-5.27	-12.08	524.22	-430.66
738	Copertura	31	0	14.56	-0.03	-9.98	11.82	35.56	430.60
			65	14.56	-0.03	-2.30	11.82	-244.33	430.60
			130	14.56	-0.03	5.39	11.82	-524.22	430.60
739	Copertura	32	0	18.10	-0.04	11.36	-13.19	-35.20	-430.28
			65	18.10	-0.04	2.79	-13.19	244.48	-430.28
			130	18.10	-0.04	-5.78	-13.19	524.16	-430.28
740	Copertura	33	0	13.70	-0.04	-12.04	14.16	34.99	430.03
			65	13.70	-0.04	-2.84	14.16	-244.53	430.03
			130	13.70	-0.04	6.36	14.16	-524.05	430.03
741	Copertura	34	0	11.01	-0.05	12.53	-14.56	-35.01	-430.28
			65	11.01	-0.05	3.06	-14.56	244.67	-430.28
			130	11.01	-0.05	-6.40	-14.56	524.36	-430.28
742	Copertura	35	0	14.26	-0.04	-12.22	14.48	34.76	429.89
			65	14.26	-0.04	-2.81	14.48	-244.67	429.89
			130	14.26	-0.04	6.61	14.48	-524.10	429.89
743	Copertura	36	0	2.95	-0.05	13.70	-15.94	-34.81	-430.28
			65	2.95	-0.05	3.34	-15.94	244.88	-430.28
			130	2.95	-0.05	-7.02	-15.94	524.56	-430.28
744	Copertura	37	0	7.79	-0.04	-13.72	16.26	34.38	429.59
			65	7.79	-0.04	-3.15	16.26	-244.85	429.59
			130	7.79	-0.04	7.42	16.26	-524.08	429.59
745	Copertura	38	0	0.17	-0.05	14.86	-17.31	-34.41	-430.00
			65	0.17	-0.05	3.61	-17.31	245.09	-430.00
			130	0.17	-0.05	-7.64	-17.31	524.58	-430.00
746	Copertura	39	0	5.54	-0.04	-14.08	16.90	34.25	429.61

			65	5.54	-0.04	-3.10	16.90	-244.99	429.61
			130	5.54	-0.04	7.89	16.90	-524.23	429.61
747	Copertura	40	0	11.52	-0.06	15.77	-18.42	-33.68	-429.22
			65	11.52	-0.06	3.80	-18.42	245.31	-429.22
			130	11.52	-0.06	-8.17	-18.42	524.30	-429.22
748	Copertura	41	0	9.75	-0.02	-10.03	12.88	34.98	430.41
			65	9.75	-0.02	-1.66	12.88	-244.79	430.41
			130	9.75	-0.02	6.71	12.88	-524.56	430.41
749	Copertura	42	0	21.07	-0.07	16.62	-19.61	-32.99	-428.39
			65	21.07	-0.07	3.88	-19.61	245.47	-428.39
			130	21.07	-0.07	-8.87	-19.61	523.92	-428.39
750	Copertura	43	0	12.71	-0.01	-0.18	0.10	-37.18	-431.57
			65	12.71	-0.01	-0.12	0.10	243.33	-431.57
			130	12.71	-0.01	-0.05	0.10	523.85	-431.57
751	Copertura	44	0	-19.07	0.00	-5.84	5.90	38.17	432.69
			65	-19.07	0.00	-2.00	5.90	-243.08	432.69
			130	-19.07	0.00	1.84	5.90	-524.33	432.69
752	Copertura	45	0	-6.02	0.00	-0.31	0.15	-37.78	-432.23
			65	-6.02	0.00	-0.22	0.15	243.16	-432.23
			130	-6.02	0.00	-0.12	0.15	524.11	-432.23
753	Copertura	46	0	-19.15	0.00	-0.55	0.35	38.07	432.36
			65	-19.15	0.00	-0.32	0.35	-242.96	432.36
			130	-19.15	0.00	-0.09	0.35	-523.99	432.36
754	Copertura	47	0	-12.89	-0.01	-0.56	0.25	-37.97	-432.74
			65	-12.89	-0.01	-0.40	0.25	243.31	-432.74
			130	-12.89	-0.01	-0.23	0.25	524.59	-432.74
755	Copertura	48	0	-5.56	0.00	-1.04	0.88	37.66	431.87
			65	-5.56	0.00	-0.46	0.88	-243.06	431.87
			130	-5.56	0.00	0.11	0.88	-523.78	431.87
756	Copertura	49	0	2.10	0.02	-1.02	0.48	-37.59	-432.22
			65	2.10	0.02	-0.70	0.48	243.36	-432.22
			130	2.10	0.02	-0.39	0.48	524.30	-432.22
757	Copertura	50	0	5.23	-0.06	-1.51	1.29	37.45	431.33
			65	5.23	-0.06	-0.67	1.29	-242.91	431.33
			130	5.23	-0.06	0.17	1.29	-523.28	431.33
758	Copertura	51	0	18.15	0.03	-1.70	0.79	-37.73	-430.38
			65	18.15	0.03	-1.18	0.79	242.02	-430.38
			130	18.15	0.03	-0.67	0.79	521.76	-430.38
759	Copertura	52	0	43.68	-0.05	-2.44	1.72	36.87	428.51
			65	43.68	-0.05	-1.32	1.72	-241.66	428.51
			130	43.68	-0.05	-0.20	1.72	-520.19	428.51
760	Copertura	53	0	84.51	-0.20	-2.43	0.89	-36.81	-427.91
			65	84.51	-0.20	-1.85	0.89	241.33	-427.91
			130	84.51	-0.20	-1.28	0.89	519.48	-427.91
761	Copertura	54	0	84.07	0.52	-3.53	2.31	36.95	427.71
			65	84.07	0.52	-2.03	2.31	-241.06	427.71
			130	84.07	0.52	-0.53	2.31	-519.07	427.71
762	Copertura	55	0	219.62	-1.23	-2.83	0.08	-42.17	-471.39
			65	219.62	-1.23	-2.78	0.08	264.23	-471.39
			130	219.62	-1.23	-2.72	0.08	570.64	-471.39
763	Copertura	56	0	219.75	1.42	-4.30	1.94	41.12	472.24
			65	219.75	1.42	-3.03	1.94	-265.83	472.24
			130	219.75	1.42	-1.77	1.94	-572.79	472.24
764	Copertura	70	0	-128.84	7.84	-11.69	5.36	19.90	8.90
			95	-128.84	7.84	-6.60	5.36	11.45	8.90
			190	-128.84	7.84	-1.51	5.36	2.99	8.90
765	Copertura	81	0	-386.29	3.70	2.87	-3.75	-493.15	-180.34
			80	-386.29	3.70	-0.13	-3.75	-348.88	-180.34
			160	-386.29	3.70	-3.13	-3.75	-204.61	-180.34
766	Copertura	126	0	-392.67	-12.04	-0.63	-2.58	-614.67	-201.65
			30	-392.67	-12.04	-1.41	-2.58	-554.18	-201.65
			60	-392.67	-12.04	-2.18	-2.58	-493.68	-201.65
767	Copertura	98	0	-431.58	-1.47	1.34	-2.16	-485.91	-124.64
			82	-431.58	-1.47	-0.44	-2.16	-383.27	-124.64
			165	-431.58	-1.47	-2.22	-2.16	-280.63	-124.64
768	Copertura	99	0	-491.93	0.21	0.96	-0.99	-488.53	-125.52
			82	-491.93	0.21	0.15	-0.99	-385.17	-125.52
			165	-491.93	0.21	-0.67	-0.99	-281.82	-125.52
769	Copertura	100	0	-515.52	0.16	0.33	-0.61	-488.76	-129.81
			82	-515.52	0.16	-0.18	-0.61	-381.87	-129.81
			165	-515.52	0.16	-0.68	-0.61	-274.98	-129.81
770	Copertura	101	0	-534.96	-0.02	-0.30	0.69	-488.83	-131.25

			82	-534.96	-0.02	0.27	0.69	-380.75	-131.25
			165	-534.96	-0.02	0.84	0.69	-272.66	-131.25
771	Copertura	102	0	-543.87	0.01	2.35	-2.29	-488.98	-131.04
			82	-543.87	0.01	0.47	-2.29	-381.08	-131.04
			165	-543.87	0.01	-1.42	-2.29	-273.18	-131.04
772	Copertura	103	0	-532.99	-0.01	0.39	-0.12	-488.81	-130.96
			82	-532.99	-0.01	0.29	-0.12	-380.97	-130.96
			165	-532.99	-0.01	0.19	-0.12	-273.13	-130.96
773	Copertura	104	0	-517.61	-0.01	4.88	-5.22	-488.67	-130.64
			82	-517.61	-0.01	0.59	-5.22	-381.09	-130.64
			165	-517.61	-0.01	-3.71	-5.22	-273.51	-130.64
774	Copertura	105	0	-510.88	0.00	3.92	-3.68	-488.71	-130.56
			82	-510.88	0.00	0.88	-3.68	-381.20	-130.56
			165	-510.88	0.00	-2.15	-3.68	-273.69	-130.56
775	Copertura	111	0	-512.94	0.00	5.54	-5.85	-481.84	-130.47
			80	-512.94	0.00	0.88	-5.85	-377.78	-130.47
			160	-512.94	0.00	-3.79	-5.85	-273.72	-130.47
776	Copertura	112	0	-510.18	0.00	5.12	-4.91	-488.60	-130.48
			82	-510.18	0.00	1.07	-4.91	-381.16	-130.48
			165	-510.18	0.00	-2.98	-4.91	-273.71	-130.48
777	Copertura	113	0	-518.80	0.01	6.24	-6.24	-488.58	-130.44
			82	-518.80	0.01	1.10	-6.24	-381.16	-130.44
			165	-518.80	0.01	-4.04	-6.24	-273.75	-130.44
778	Copertura	114	0	-518.65	0.00	6.49	-6.83	-488.80	-130.53
			82	-518.65	0.00	0.86	-6.83	-381.32	-130.53
			165	-518.65	0.00	-4.76	-6.83	-273.84	-130.53
779	Copertura	115	0	-517.05	0.00	1.50	-1.52	-488.90	-130.75
			82	-517.05	0.00	0.24	-1.52	-381.23	-130.75
			165	-517.05	0.00	-1.01	-1.52	-273.56	-130.75
780	Copertura	116	0	-546.47	0.00	5.33	-5.36	-488.87	-130.57
			82	-546.47	0.00	0.91	-5.36	-381.36	-130.57
			165	-546.47	0.00	-3.50	-5.36	-273.84	-130.57
781	Copertura	117	0	-545.83	0.00	-0.57	1.17	-488.32	-130.78
			82	-545.83	0.00	0.39	1.17	-380.63	-130.78
			165	-545.83	0.00	1.36	1.17	-272.94	-130.78
782	Copertura	118	0	-533.51	-0.03	0.08	0.10	-488.18	-130.64
			82	-533.51	-0.03	0.16	0.10	-380.60	-130.64
			165	-533.51	-0.03	0.24	0.10	-273.02	-130.64
783	Copertura	131	0	-428.62	-0.44	0.36	-1.86	-561.08	-125.30
			30	-428.62	-0.44	-0.20	-1.86	-523.49	-125.30
			60	-428.62	-0.44	-0.75	-1.86	-485.90	-125.30
784	Copertura	133	0	-494.89	0.05	-0.07	-1.29	-563.46	-124.86
			30	-494.89	0.05	-0.46	-1.29	-526.00	-124.86
			60	-494.89	0.05	-0.85	-1.29	-488.54	-124.86
785	Copertura	139	0	-515.61	0.10	0.24	0.06	-566.65	-129.81
			30	-515.61	0.10	0.26	0.06	-527.71	-129.81
			60	-515.61	0.10	0.27	0.06	-488.76	-129.81
786	Copertura	143	0	-534.88	0.04	-0.15	0.03	-567.57	-131.25
			30	-534.88	0.04	-0.14	0.03	-528.19	-131.25
			60	-534.88	0.04	-0.14	0.03	-488.82	-131.25
787	Copertura	147	0	-544.22	0.00	0.85	3.10	-567.60	-131.04
			30	-544.22	0.00	1.78	3.10	-528.29	-131.04
			60	-544.22	0.00	2.71	3.10	-488.98	-131.04
788	Copertura	151	0	-532.63	-0.01	3.80	-5.51	-567.39	-130.96
			30	-532.63	-0.01	2.14	-5.51	-528.11	-130.96
			60	-532.63	-0.01	0.49	-5.51	-488.82	-130.96
789	Copertura	155	0	-517.01	0.03	6.62	-3.67	-567.08	-130.70
			30	-517.01	0.03	5.52	-3.67	-527.87	-130.70
			60	-517.01	0.03	4.42	-3.67	-488.66	-130.70
790	Copertura	159	0	-511.48	0.03	6.72	-5.23	-567.02	-130.51
			30	-511.48	0.03	5.15	-5.23	-527.87	-130.51
			60	-511.48	0.03	3.58	-5.23	-488.72	-130.51
791	Copertura	119	0	-517.48	0.00	-0.80	0.97	-488.45	-129.55
			82	-517.48	0.00	0.00	0.97	-381.77	-129.55
			165	-517.48	0.00	0.79	0.97	-275.09	-129.55
792	Copertura	120	0	-477.91	0.02	-1.15	1.97	-487.54	-124.83
			82	-477.91	0.02	0.47	1.97	-384.75	-124.83
			165	-477.91	0.02	2.09	1.97	-281.96	-124.83
793	Copertura	121	0	-426.61	-0.41	-2.46	3.02	-486.33	-125.59
			82	-426.61	-0.41	0.02	3.02	-382.91	-125.59
			165	-426.61	-0.41	2.51	3.02	-279.49	-125.59
794	Copertura	122	0	-402.70	6.52	-2.55	3.75	-504.01	-190.30

			82	-402.70	6.52	0.53	3.75	-347.31	-190.30
			165	-402.70	6.52	3.62	3.75	-190.61	-190.30
795	Copertura	123	0	-128.84	7.84	-1.51	5.36	2.99	8.90
			82	-128.84	7.84	2.90	5.36	-4.34	8.90
			165	-128.84	7.84	7.31	5.36	-11.67	8.90
796	Copertura	163	0	-511.93	0.05	7.85	-4.63	-566.85	-130.54
			33	-511.93	0.05	6.34	-4.63	-524.32	-130.54
			65	-511.93	0.05	4.83	-4.63	-481.79	-130.54
797	Copertura	167	0	-511.20	0.04	8.23	-6.12	-566.90	-130.41
			30	-511.20	0.04	6.39	-6.12	-527.77	-130.41
			60	-511.20	0.04	4.55	-6.12	-488.65	-130.41
798	Copertura	171	0	-517.59	0.05	9.18	-6.11	-566.89	-130.53
			30	-517.59	0.05	7.35	-6.11	-527.73	-130.53
			60	-517.59	0.05	5.52	-6.11	-488.58	-130.53
799	Copertura	174	0	-519.86	0.06	9.78	-6.96	-567.07	-130.44
			30	-519.86	0.06	7.70	-6.96	-527.93	-130.44
			60	-519.86	0.06	5.61	-6.96	-488.80	-130.44
800	Copertura	179	0	-516.79	0.07	8.75	-12.97	-567.41	-130.85
			30	-516.79	0.07	4.86	-12.97	-528.15	-130.85
			60	-516.79	0.07	0.97	-12.97	-488.90	-130.85
801	Copertura	183	0	-546.73	0.06	1.86	6.09	-567.15	-130.47
			30	-546.73	0.06	3.68	6.09	-528.01	-130.47
			60	-546.73	0.06	5.51	6.09	-488.87	-130.47
802	Copertura	187	0	-546.77	0.00	-0.11	0.36	-566.80	-130.80
			30	-546.77	0.00	0.00	0.36	-527.56	-130.80
			60	-546.77	0.00	0.11	0.36	-488.32	-130.80
803	Copertura	191	0	-532.57	-0.01	0.10	0.91	-566.55	-130.63
			30	-532.57	-0.01	0.37	0.91	-527.36	-130.63
			60	-532.57	-0.01	0.64	0.91	-488.18	-130.63
804	Copertura	194	0	-520.11	-0.15	0.08	1.25	-566.01	-129.29
			30	-520.11	-0.15	0.45	1.25	-527.22	-129.29
			60	-520.11	-0.15	0.82	1.25	-488.43	-129.29
805	Copertura	198	0	-475.28	-0.17	-0.32	1.69	-562.61	-125.09
			30	-475.28	-0.17	0.19	1.69	-525.09	-125.09
			60	-475.28	-0.17	0.69	1.69	-487.56	-125.09
806	Copertura	203	0	-433.31	1.22	0.01	3.01	-561.27	-124.44
			30	-433.31	1.22	0.91	3.01	-523.93	-124.44
			60	-433.31	1.22	1.82	3.01	-486.60	-124.44
807	Copertura	207	0	-396.00	3.37	-0.23	3.75	-618.61	-191.46
			30	-396.00	3.37	0.89	3.75	-561.17	-191.46
			60	-396.00	3.37	2.02	3.75	-503.74	-191.46

1.1.13.2 Piastre SLU

Tabella 26.I

Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	1.330	0.386	-0.256	-338.179	-80.391	-43.905	2.695	-1.413
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	1.397	0.821	0.392	-337.163	-87.136	-95.422	3.817	1.758
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10,	1.405	0.823	0.363	-311.568	-57.704	-95.180	2.886	-1.861

		9, 8, 7, 6, 5, 4, 3, 2								
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1.2 Inviluppi.

Gli effetti relativi alle varie combinazioni sono considerati utilizzando la tecnica dell'involuppo, in modo da considerare i massimi effetti relativi allo stato limite in esame.

Tale tecnica è stata utilizzata per:

- Cinematismi nodali;
- Sforzo Normale;
- Momento Torcente;
- Momento Flettente X-Z;
- Taglio X-Z;
- Momento Flettente X-Y;
- Taglio X-Y;

1.2.1 Inviluppi dei Cinematismi nodali.

I dati seguenti riportano i valori dei cinematismi nodali dei nodi che definiscono la struttura ed in modo particolare:

Nodo	: numerazione interna del nodo.
X	: distanza dal nodo iniziale misurata lungo l'asse dell'asta.
Cinematismi nodali	: valore dello spostamento. Per le azioni sismiche è riferito allo spettro elastico:
Vx	: traslazione X rispetto al sistema di riferimento globale.
Vy	: traslazione Y rispetto al sistema di riferimento globale.
Vz	: Traslazione Z rispetto al sistema di riferimento globale.
Rx	: rotazione X rispetto al sistema di riferimento globale.
Ry	: rotazione Y rispetto al sistema di riferimento globale.
Rz	: rotazione Z rispetto al sistema di riferimento globale.
Max	: valore massimo (rispetto al sistema di riferimento globale) dell'involuppo.
Min	: valore minimo (rispetto al sistema di riferimento globale) dell'involuppo.

1.2.1.1 Inviluppi SLO.

Tabella 26.I

STATO LIMITE DI OPERATIVITA'												
Nodo	Spostamenti						Rotazioni					
	Vx [cm]		Vy [cm]		Vz [cm]		Rx [rad]		Ry [rad]		Rz [rad]	
	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min
1	0.011	-0.011	0.012	-0.013	-0.020	-0.078	1.5E-4	-1.5E-4	2.1E-4	-5.0E-5	4.5E-6	-6.7E-6
2	0.011	-0.011	0.012	-0.012	-0.026	-0.052	8.0E-5	-1.1E-4	1.1E-4	-3.7E-5	4.6E-6	-5.5E-6
3	0.011	-0.011	0.012	-0.012	-0.029	-0.043	5.1E-5	-9.5E-5	3.8E-5	-2.1E-5	4.7E-6	-5.1E-6
4	0.011	-0.011	0.011	-0.011	-0.032	-0.040	3.7E-5	-8.8E-5	1.7E-5	-2.1E-5	4.7E-6	-4.9E-6
5	0.011	-0.011	0.011	-0.011	-0.033	-0.040	2.9E-5	-8.0E-5	8.0E-6	-1.6E-5	4.6E-6	-4.7E-6
6	0.011	-0.011	0.011	-0.011	-0.034	-0.040	2.1E-5	-7.1E-5	5.9E-6	-1.0E-5	4.5E-6	-4.6E-6
7	0.011	-0.011	0.011	-0.011	-0.034	-0.041	1.9E-5	-6.6E-5	6.5E-6	-5.5E-6	4.6E-6	-4.6E-6
8	0.011	-0.011	0.011	-0.011	-0.035	-0.040	1.4E-5	-6.0E-5	9.2E-6	-9.3E-6	4.5E-6	-4.5E-6
9	0.011	-0.011	0.011	-0.011	-0.035	-0.041	6.8E-6	-5.6E-5	5.8E-6	-5.8E-6	4.5E-6	-4.4E-6
10	0.011	-0.011	0.011	-0.011	-0.035	-0.040	5.4E-7	-5.4E-5	1.2E-5	-4.6E-6	4.6E-6	-4.5E-6
11	0.011	-0.011	0.011	-0.011	-0.034	-0.040	-4.5E-6	-4.8E-5	2.3E-5	-1.6E-5	4.7E-6	-4.4E-6
12	0.011	-0.011	0.011	-0.011	-0.031	-0.042	2.2E-6	-4.8E-5	1.6E-5	-3.2E-5	4.8E-6	-4.3E-6
13	0.011	-0.011	0.011	-0.011	-0.031	-0.047	1.5E-5	-4.0E-5	-1.0E-6	-7.3E-5	5.1E-6	-4.1E-6
14	0.011	-0.011	0.011	-0.012	-0.036	-0.063	3.1E-5	-3.3E-5	-6.6E-6	-1.6E-4	6.2E-6	-3.8E-6
15	0.011	-0.011	0.012	-0.013	-0.039	-0.064	1.0E-4	-5.3E-5	2.2E-4	4.4E-5	4.4E-6	-5.9E-6
16	0.011	-0.011	0.011	-0.012	-0.038	-0.066	5.2E-5	-2.1E-6	-5.2E-5	-2.1E-4	5.6E-6	-4.0E-6
17	0.010	-0.011	0.012	-0.013	-0.042	-0.069	6.3E-5	-1.7E-5	2.9E-4	6.9E-5	4.6E-6	-5.6E-6
18	0.011	-0.010	0.011	-0.012	-0.040	-0.071	5.1E-5	-4.1E-6	-7.6E-5	-2.8E-4	5.4E-6	-4.4E-6
19	0.010	-0.011	0.012	-0.012	-0.043	-0.072	4.2E-5	-1.8E-5	3.3E-4	6.8E-5	4.8E-6	-5.1E-6
20	0.011	-0.010	0.011	-0.012	-0.041	-0.075	3.9E-5	-1.4E-5	-6.8E-5	-3.3E-4	5.0E-6	-4.7E-6
21	0.010	-0.011	0.012	-0.012	-0.043	-0.074	2.6E-5	-2.8E-5	3.6E-4	5.5E-5	4.8E-6	-5.0E-6

22	0.011	-0.010	0.011	-0.012	-0.041	-0.076	2.8E-5	-2.5E-5	-5.3E-5	-3.7E-4	5.0E-6	-4.8E-6
23	0.010	-0.011	0.012	-0.012	-0.040	-0.075	9.9E-6	-3.7E-5	3.8E-4	3.6E-5	5.1E-6	-4.7E-6
24	0.011	-0.010	0.011	-0.012	-0.039	-0.077	1.6E-5	-3.2E-5	-3.3E-5	-3.9E-4	4.8E-6	-5.0E-6
25	0.010	-0.010	0.012	-0.012	-0.037	-0.074	1.4E-5	-3.2E-5	3.6E-4	2.4E-5	5.0E-6	-5.1E-6
26	0.010	-0.010	0.011	-0.012	-0.037	-0.078	2.3E-5	-2.1E-5	-1.7E-5	-3.9E-4	5.1E-6	-4.9E-6
27	0.010	-0.010	0.011	-0.012	-0.036	-0.082	3.6E-5	-1.2E-5	1.1E-5	-4.4E-4	5.0E-6	-4.8E-6
28	0.010	-0.010	0.012	-0.012	-0.034	-0.079	4.3E-5	-1.6E-5	4.1E-4	-1.8E-5	4.8E-6	-4.9E-6
29	0.010	-0.010	0.011	-0.012	-0.036	-0.084	2.9E-5	-1.4E-5	2.7E-5	-4.6E-4	5.0E-6	-4.7E-6
30	0.010	-0.010	0.012	-0.012	-0.035	-0.082	4.0E-5	-2.0E-5	4.4E-4	-3.2E-5	4.7E-6	-4.9E-6
31	0.010	-0.010	0.011	-0.012	-0.035	-0.086	2.1E-5	-1.6E-5	4.0E-5	-4.8E-4	4.7E-6	-4.7E-6
32	0.009	-0.010	0.012	-0.012	-0.035	-0.083	3.0E-5	-2.1E-5	4.6E-4	-3.9E-5	4.6E-6	-4.8E-6
33	0.010	-0.009	0.011	-0.011	-0.036	-0.086	1.7E-5	-1.6E-5	4.1E-5	-4.8E-4	4.7E-6	-4.6E-6
34	0.009	-0.010	0.012	-0.012	-0.036	-0.083	2.3E-5	-1.9E-5	4.6E-4	-4.2E-5	4.6E-6	-4.6E-6
35	0.010	-0.009	0.011	-0.011	-0.036	-0.085	1.7E-5	-1.8E-5	4.1E-5	-4.8E-4	4.4E-6	-4.5E-6
36	0.009	-0.010	0.012	-0.012	-0.036	-0.083	2.1E-5	-1.8E-5	4.7E-4	-4.0E-5	4.5E-6	-4.5E-6
37	0.010	-0.009	0.011	-0.011	-0.036	-0.085	1.5E-5	-2.1E-5	4.0E-5	-4.7E-4	4.5E-6	-4.5E-6
38	0.009	-0.010	0.012	-0.012	-0.036	-0.084	2.5E-5	-1.9E-5	4.8E-4	-4.1E-5	4.6E-6	-4.6E-6
39	0.010	-0.010	0.011	-0.011	-0.036	-0.083	1.4E-5	-3.0E-5	3.2E-5	-4.7E-4	4.6E-6	-4.8E-6
40	0.010	-0.010	0.012	-0.012	-0.036	-0.086	3.0E-5	-1.9E-5	4.9E-4	-3.6E-5	4.7E-6	-4.7E-6
41	0.010	-0.010	0.011	-0.011	-0.036	-0.081	2.1E-5	-4.2E-5	1.8E-5	-4.5E-4	4.6E-6	-4.8E-6
42	0.010	-0.010	0.012	-0.012	-0.036	-0.087	2.3E-5	-1.0E-5	5.1E-4	-2.5E-5	4.6E-6	-4.8E-6
43	0.010	-0.010	0.012	-0.012	-0.036	-0.087	2.2E-5	-3.2E-5	4.8E-4	-1.0E-5	5.3E-6	-4.8E-6
44	0.010	-0.010	0.011	-0.011	-0.036	-0.079	2.7E-5	-2.2E-5	-3.2E-6	-4.1E-4	4.7E-6	-4.7E-6
45	0.010	-0.010	0.012	-0.012	-0.038	-0.084	2.3E-5	-2.8E-5	4.6E-4	2.5E-6	4.9E-6	-4.8E-6
46	0.010	-0.010	0.011	-0.011	-0.039	-0.079	3.6E-5	-1.2E-5	-3.9E-6	-4.3E-4	4.9E-6	-4.8E-6
47	0.010	-0.011	0.012	-0.012	-0.040	-0.082	2.2E-5	-2.9E-5	4.3E-4	2.0E-5	4.8E-6	-4.8E-6
48	0.011	-0.010	0.011	-0.011	-0.041	-0.079	2.8E-5	-2.0E-5	-2.2E-5	-4.1E-4	5.0E-6	-4.9E-6
49	0.010	-0.011	0.013	-0.012	-0.042	-0.078	1.9E-5	-3.7E-5	3.9E-4	4.2E-5	4.9E-6	-4.6E-6
50	0.011	-0.010	0.012	-0.011	-0.043	-0.077	1.7E-5	-3.2E-5	-4.4E-5	-3.8E-4	4.9E-6	-5.1E-6
51	0.011	-0.011	0.013	-0.012	-0.042	-0.075	1.3E-5	-4.6E-5	3.5E-4	6.0E-5	5.0E-6	-4.6E-6
52	0.011	-0.010	0.012	-0.011	-0.043	-0.073	1.3E-5	-4.8E-5	-5.9E-5	-3.5E-4	4.8E-6	-5.2E-6
53	0.011	-0.011	0.013	-0.012	-0.040	-0.071	1.3E-5	-6.4E-5	3.0E-4	6.1E-5	5.6E-6	-4.5E-6
54	0.011	-0.011	0.012	-0.011	-0.041	-0.069	5.2E-6	-5.4E-5	-6.3E-5	-2.9E-4	4.5E-6	-5.4E-6
55	0.011	-0.012	0.013	-0.012	-0.035	-0.068	5.1E-5	-1.0E-4	2.3E-4	3.5E-5	6.0E-6	-4.4E-6
56	0.011	-0.011	0.012	-0.011	-0.038	-0.065	1.8E-6	-4.9E-5	-4.0E-5	-2.2E-4	4.1E-6	-5.6E-6
57	0.012	-0.012	0.013	-0.012	-0.017	-0.081	1.5E-4	-1.5E-4	2.2E-4	-5.3E-5	7.0E-6	-4.5E-6
58	0.012	-0.012	0.012	-0.012	-0.024	-0.054	1.1E-4	-8.0E-5	1.1E-4	-4.1E-5	5.7E-6	-4.7E-6
59	0.012	-0.012	0.012	-0.012	-0.028	-0.044	9.6E-5	-5.0E-5	4.3E-5	-2.7E-5	5.2E-6	-4.7E-6
60	0.012	-0.012	0.011	-0.012	-0.032	-0.041	8.9E-5	-3.6E-5	1.8E-5	-2.6E-5	4.9E-6	-4.7E-6
61	0.012	-0.012	0.011	-0.011	-0.033	-0.040	8.2E-5	-2.8E-5	6.8E-6	-1.4E-5	4.8E-6	-4.6E-6
62	0.012	-0.012	0.011	-0.011	-0.034	-0.040	7.6E-5	-2.6E-5	8.4E-6	-7.5E-6	4.7E-6	-4.6E-6
63	0.012	-0.012	0.011	-0.011	-0.034	-0.040	6.6E-5	-2.1E-5	1.3E-5	-1.0E-5	4.6E-6	-4.6E-6
64	0.012	-0.012	0.011	-0.011	-0.034	-0.040	5.8E-5	-1.3E-5	1.0E-5	-1.2E-5	4.6E-6	-4.6E-6
65	0.012	-0.012	0.011	-0.011	-0.034	-0.040	5.7E-5	-7.4E-6	7.4E-6	-8.5E-6	4.5E-6	-4.6E-6
66	0.012	-0.012	0.011	-0.011	-0.035	-0.040	5.3E-5	1.5E-7	1.2E-5	-5.4E-6	4.6E-6	-4.6E-6
67	0.012	-0.012	0.011	-0.011	-0.034	-0.040	4.7E-5	5.6E-6	2.3E-5	-1.5E-5	4.5E-6	-4.7E-6
68	0.012	-0.012	0.011	-0.011	-0.031	-0.041	4.7E-5	-1.0E-6	1.4E-5	-3.0E-5	4.5E-6	-4.9E-6
69	0.012	-0.012	0.011	-0.011	-0.032	-0.046	4.1E-5	-1.5E-5	2.6E-6	-7.6E-5	4.3E-6	-5.2E-6
70	0.012	-0.012	0.012	-0.011	-0.034	-0.064	3.5E-5	-3.2E-5	1.3E-6	-1.6E-4	3.8E-6	-6.2E-6
71	0.067	-0.073	0.192	-0.190	-0.015	-0.092	9.1E-4	-7.8E-4	1.6E-4	-1.8E-4	6.5E-4	-2.8E-3
72	0.068	-0.076	0.590	-0.496	-0.036	-0.064	2.9E-3	-2.8E-3	9.3E-5	-1.3E-5	2.1E-3	-1.7E-3
73	0.069	-0.076	0.684	-0.647	-0.038	-0.054	2.9E-3	-2.8E-3	4.9E-5	-1.7E-5	1.0E-3	-6.8E-4
74	0.070	-0.075	0.650	-0.646	-0.039	-0.050	2.8E-3	-2.8E-3	1.8E-5	-1.1E-5	1.1E-3	-9.6E-4
75	0.070	-0.074	0.629	-0.636	-0.040	-0.048	2.7E-3	-2.7E-3	3.6E-5	-2.9E-5	4.3E-4	-4.1E-4
76	0.071	-0.073	0.541	-0.547	-0.039	-0.049	2.5E-3	-2.5E-3	3.1E-5	-2.6E-5	1.2E-3	-1.2E-3
77	0.072	-0.072	0.506	-0.512	-0.040	-0.048	2.2E-3	-2.2E-3	2.6E-5	-2.9E-5	9.1E-4	-9.1E-4
78	0.072	-0.071	0.448	-0.454	-0.042	-0.048	1.9E-3	-1.9E-3	5.1E-5	-5.1E-5	9.5E-4	-9.5E-4
79	0.073	-0.071	0.360	-0.367	-0.039	-0.048	1.6E-3	-1.6E-3	2.9E-5	-2.8E-5	1.3E-3	-1.3E-3
80	0.074	-0.069	0.325	-0.332	-0.040	-0.048	1.3E-3	-1.3E-3	2.9E-5	-3.5E-5	6.4E-4	-6.6E-4
81	0.074	-0.069	0.251	-0.248	-0.042	-0.048	1.1E-3	-1.0E-3	3.0E-5	-4.1E-5	1.2E-3	-1.3E-3
82	0.075	-0.068	0.237	-0.199	-0.039	-0.053	8.9E-4	-8.1E-4	1.9E-5	-5.2E-5	7.9E-4	-1.2E-3
83	0.075	-0.066	0.215	-0.121	-0.038	-0.061	6.8E-4	-5.7E-4	-7.3E-6	-7.3E-5	6.3E-4	-9.7E-4
84	0.069	-0.063	0.037	-0.039	-0.038	-0.069	1.7E-4	-5.2E-5	1.7E-4	-1.6E-4	2.2E-3	5.2E-5
85	-0.050	-0.479	0.191	-0.188	-0.046	-0.077	8.6E-5	-9.4E-6	1.6E-3	1.2E-4	-2.3E-4	-2.5E-3
86	0.500	0.023	0.037	-0.039	-0.043	-0.080	7.8E-5	-1.5E-6	-1.0E-4	-1.6E-3	2.6E-3	1.3E-4
87	-0.017	-0.703	0.190	-0.187	-0.049	-0.083	1.7E-4	-1.1E-4	2.2E-3	-2.6E-4	8.9E-4	-1.4E-3
88	0.729	-0.012	0.037	-0.039	-0.047	-0.086	6.6E-5	-8.6E-6	2.7E-4	-2.2E-3	1.4E-3	-8.8E-4
89	0.091	-0.824	0.190	-0.186	-0.050	-0.088	1.2E-4	-9.0E-5	2.7E-3	-7.3E-4	1.2E-3	-1.1E-3
90	0.837	-0.103	0.037	-0.039	-0.048	-0.091	5.2E-5	-2.1E-5	7.4E-4	-2.7E-3	1.2E-3	-1.3E-3
91	0.213	-0.934	0.190	-0.186	-0.051	-0.090	9.7E-5	-8.9E-5	3.1E-3	-1.2E-3	1.3E-3	-1.2E-3
92	0.941	-0.219	0.037	-0.039	-0.050	-0.092	4.4E-5	-3.1E-5	1.2E-3	-3.1E-3	1.1E-3	-1.2E-3
93	0.329	-1.044	0.190	-0.187	-0.048	-0.092	7.9E-5	-9.1E-5	3.5E-3	-1.6E-3	1.2E-3	-1.2E-3

94	1.039	-0.322	0.038	-0.039	-0.048	-0.094	3.1E-5	-3.7E-5	1.6E-3	-3.5E-3	1.1E-3	-1.1E-3
95	0.426	-1.139	0.191	-0.187	-0.046	-0.093	9.3E-5	-8.8E-5	3.8E-3	-1.9E-3	1.0E-3	-1.0E-3
96	1.134	-0.416	0.038	-0.039	-0.046	-0.096	3.4E-5	-3.2E-5	1.9E-3	-3.8E-3	1.1E-3	-1.1E-3
97	1.211	-0.492	0.038	-0.040	-0.043	-0.099	3.4E-5	-2.4E-5	2.2E-3	-4.1E-3	1.1E-3	-1.0E-3
98	0.503	-1.218	0.194	-0.190	-0.042	-0.099	1.4E-4	-1.2E-4	4.1E-3	-2.2E-3	9.0E-4	-9.2E-4
99	1.284	-0.564	0.038	-0.040	-0.043	-0.101	3.7E-5	-2.5E-5	2.4E-3	-4.3E-3	8.2E-4	-8.3E-4
100	0.566	-1.284	0.197	-0.193	-0.043	-0.101	6.5E-5	-4.1E-5	4.3E-3	-2.4E-3	7.5E-4	-7.7E-4
101	1.323	-0.603	0.038	-0.040	-0.042	-0.103	2.6E-5	-2.6E-5	2.6E-3	-4.5E-3	7.5E-4	-7.4E-4
102	0.584	-1.303	0.199	-0.195	-0.044	-0.102	8.6E-5	-7.4E-5	4.5E-3	-2.6E-3	7.5E-4	-6.6E-4
103	1.332	-0.613	0.038	-0.040	-0.043	-0.102	2.7E-5	-2.7E-5	2.6E-3	-4.5E-3	5.8E-4	-5.9E-4
104	0.616	-1.336	0.201	-0.196	-0.046	-0.102	8.3E-5	-7.4E-5	4.5E-3	-2.6E-3	5.2E-4	-5.2E-4
105	1.331	-0.612	0.039	-0.040	-0.043	-0.103	2.5E-5	-3.1E-5	2.6E-3	-4.5E-3	4.5E-4	-4.5E-4
106	0.607	-1.329	0.201	-0.197	-0.046	-0.102	8.2E-5	-7.4E-5	4.5E-3	-2.6E-3	5.3E-4	-5.4E-4
107	1.320	-0.602	0.039	-0.041	-0.044	-0.101	2.5E-5	-3.3E-5	2.6E-3	-4.5E-3	6.4E-4	-6.6E-4
108	0.608	-1.332	0.201	-0.198	-0.045	-0.104	8.3E-5	-7.4E-5	4.5E-3	-2.6E-3	6.0E-4	-6.1E-4
109	1.314	-0.596	0.040	-0.041	-0.044	-0.101	3.1E-5	-3.2E-5	2.5E-3	-4.4E-3	6.3E-4	-6.2E-4
110	0.596	-1.323	0.200	-0.197	-0.045	-0.105	6.1E-5	-5.2E-5	4.5E-3	-2.5E-3	6.4E-4	-6.6E-4
111	1.282	-0.564	0.040	-0.042	-0.044	-0.100	3.4E-5	-4.8E-5	2.4E-3	-4.3E-3	6.9E-4	-7.0E-4
112	0.538	-1.266	0.198	-0.196	-0.044	-0.105	7.9E-5	-1.0E-4	4.3E-3	-2.4E-3	8.7E-4	-8.7E-4
113	0.522	-1.249	0.198	-0.195	-0.045	-0.103	1.2E-4	-1.3E-4	4.2E-3	-2.3E-3	9.1E-4	-8.9E-4
114	1.233	-0.517	0.041	-0.042	-0.045	-0.097	3.4E-5	-4.0E-5	2.3E-3	-4.2E-3	9.2E-4	-9.3E-4
115	0.471	-1.196	0.196	-0.193	-0.047	-0.100	7.1E-5	-7.4E-5	4.0E-3	-2.1E-3	9.5E-4	-9.3E-4
116	1.195	-0.479	0.041	-0.042	-0.048	-0.096	4.1E-5	-3.0E-5	2.1E-3	-4.0E-3	9.3E-4	-9.2E-4
117	0.373	-1.096	0.195	-0.192	-0.047	-0.099	8.7E-5	-9.5E-5	3.6E-3	-1.7E-3	1.2E-3	-1.1E-3
118	1.104	-0.387	0.041	-0.042	-0.050	-0.095	3.4E-5	-2.9E-5	1.7E-3	-3.6E-3	1.2E-3	-1.2E-3
119	0.261	-0.986	0.194	-0.192	-0.050	-0.094	8.1E-5	-1.0E-4	3.2E-3	-1.3E-3	1.2E-3	-1.3E-3
120	0.978	-0.257	0.042	-0.042	-0.051	-0.093	3.1E-5	-3.9E-5	1.3E-3	-3.2E-3	1.4E-3	-1.3E-3
121	0.142	-0.878	0.194	-0.191	-0.049	-0.091	8.2E-5	-1.2E-4	2.8E-3	-8.8E-4	1.3E-3	-1.3E-3
122	0.874	-0.140	0.042	-0.042	-0.052	-0.090	2.0E-5	-5.2E-5	8.7E-4	-2.8E-3	1.3E-3	-1.2E-3
123	0.041	-0.763	0.194	-0.192	-0.046	-0.087	1.1E-4	-1.7E-4	2.3E-3	-3.9E-4	1.6E-3	-1.1E-3
124	0.739	-0.020	0.043	-0.043	-0.050	-0.085	-2.4E-6	-6.8E-5	3.9E-4	-2.3E-3	1.0E-3	-1.5E-3
125	-0.002	-0.527	0.195	-0.192	-0.042	-0.082	6.8E-6	-8.8E-5	1.7E-3	4.7E-5	2.7E-3	4.3E-5
126	0.505	0.019	0.043	-0.042	-0.045	-0.079	-6.3E-6	-8.0E-5	-2.7E-5	-1.7E-3	-2.1E-4	-2.6E-3
127	0.073	-0.079	0.196	-0.194	-0.011	-0.095	7.8E-4	-9.0E-4	1.7E-4	-1.9E-4	2.8E-3	-5.8E-4
128	0.073	-0.081	0.488	-0.578	-0.034	-0.066	2.8E-3	-2.9E-3	1.0E-4	-2.0E-5	1.7E-3	-2.0E-3
129	0.074	-0.081	0.639	-0.674	-0.036	-0.055	2.9E-3	-2.9E-3	5.6E-5	-2.4E-5	5.4E-4	-9.0E-4
130	0.075	-0.080	0.644	-0.646	-0.039	-0.050	2.8E-3	-2.8E-3	4.3E-5	-3.3E-5	7.3E-4	-8.7E-4
131	0.076	-0.080	0.628	-0.620	-0.039	-0.049	2.7E-3	-2.7E-3	3.8E-5	-3.2E-5	4.2E-4	-4.4E-4
132	0.077	-0.079	0.554	-0.546	-0.038	-0.050	2.5E-3	-2.5E-3	3.0E-5	-3.1E-5	1.0E-3	-9.9E-4
133	0.078	-0.078	0.506	-0.499	-0.041	-0.048	2.2E-3	-2.2E-3	3.1E-5	-3.3E-5	8.5E-4	-8.4E-4
134	0.079	-0.077	0.446	-0.439	-0.041	-0.048	1.9E-3	-1.9E-3	3.3E-5	-3.1E-5	8.5E-4	-8.5E-4
135	0.079	-0.076	0.362	-0.353	-0.039	-0.049	1.6E-3	-1.6E-3	3.0E-5	-2.9E-5	1.1E-3	-1.1E-3
136	0.080	-0.075	0.314	-0.305	-0.040	-0.048	1.3E-3	-1.3E-3	2.9E-5	-3.6E-5	6.5E-4	-6.3E-4
137	0.080	-0.074	0.236	-0.237	-0.042	-0.048	1.0E-3	-1.0E-3	3.0E-5	-4.0E-5	1.1E-3	-9.8E-4
138	0.081	-0.073	0.180	-0.217	-0.039	-0.052	7.9E-4	-8.6E-4	1.6E-5	-4.9E-5	1.1E-3	-6.7E-4
139	0.081	-0.072	0.104	-0.199	-0.039	-0.060	5.2E-4	-6.3E-4	-5.0E-6	-7.5E-5	8.5E-4	-4.9E-4
140	0.074	-0.068	0.043	-0.042	-0.036	-0.071	3.7E-5	-1.6E-4	1.9E-4	-1.7E-4	-4.8E-5	-2.3E-3
141	0.011	-0.109	0.087	-0.093	-0.031	-0.077	5.7E-4	-4.2E-4	8.1E-4	-4.8E-5	-2.2E-4	-1.1E-3
142	0.007	-0.303	0.092	-0.091	-0.047	-0.078	5.4E-4	-4.3E-4	2.4E-3	-5.4E-5	3.7E-4	-4.2E-4
143	0.086	-0.375	0.093	-0.092	-0.046	-0.082	5.3E-4	-4.3E-4	3.0E-3	-7.7E-4	4.7E-4	-4.5E-4
144	0.156	-0.441	0.095	-0.093	-0.040	-0.086	5.2E-4	-3.9E-4	3.6E-3	-1.4E-3	4.4E-4	-4.5E-4
145	0.023	-0.121	0.096	-0.088	-0.029	-0.079	4.3E-4	-5.7E-4	8.8E-4	-1.1E-4	1.2E-3	1.1E-4
146	0.035	-0.332	0.095	-0.093	-0.045	-0.081	4.5E-4	-5.4E-4	2.6E-3	-2.4E-4	5.0E-4	-4.5E-4
147	0.106	-0.398	0.096	-0.095	-0.045	-0.088	4.5E-4	-5.3E-4	3.2E-3	-9.1E-4	4.1E-4	-4.1E-4
148	0.163	-0.459	0.098	-0.097	-0.042	-0.094	4.5E-4	-5.3E-4	3.7E-3	-1.5E-3	3.3E-4	-3.2E-4
149	0.115	-0.017	0.023	-0.015	-0.039	-0.069	1.5E-4	-9.5E-5	9.1E-5	-8.5E-4	-1.8E-4	-1.1E-3
150	0.395	-0.105	0.019	-0.019	-0.046	-0.086	7.6E-5	-1.6E-4	9.2E-4	-3.2E-3	4.8E-4	-4.7E-4
151	0.452	-0.163	0.019	-0.019	-0.042	-0.088	7.0E-5	-1.7E-4	1.5E-3	-3.7E-3	3.7E-4	-3.6E-4
152	0.486	-0.195	0.018	-0.020	-0.040	-0.093	6.9E-5	-1.6E-4	1.7E-3	-4.0E-3	3.1E-4	-3.1E-4
153	0.493	-0.202	0.018	-0.019	-0.040	-0.094	6.6E-5	-1.6E-4	1.8E-3	-4.1E-3	2.4E-4	-2.5E-4
154	0.486	-0.195	0.019	-0.019	-0.039	-0.094	6.3E-5	-1.5E-4	1.7E-3	-4.0E-3	3.1E-4	-3.1E-4
155	0.435	-0.145	0.019	-0.019	-0.040	-0.089	5.9E-5	-1.5E-4	1.3E-3	-3.6E-3	4.1E-4	-3.9E-4
156	0.377	-0.087	0.018	-0.020	-0.045	-0.085	6.4E-5	-1.5E-4	7.7E-4	-3.0E-3	3.9E-4	-4.1E-4
157	0.320	-0.024	0.018	-0.020	-0.044	-0.081	7.0E-5	-1.5E-4	1.3E-4	-2.5E-3	4.5E-4	-3.9E-4
158	0.115	-0.017	0.015	-0.023	-0.039	-0.069	8.1E-5	-1.4E-4	6.4E-5	-8.3E-4	1.1E-3	1.6E-4
159	0.030	-0.031	0.177	-0.183	-0.038	-0.044	1.5E-3	-1.5E-3	1.6E-4	-2.5E-4	2.6E-4	-2.7E-4
160	0.031	-0.030	0.113	-0.120	-0.039	-0.044	9.6E-4	-9.8E-4	1.5E-4	-2.5E-4	4.9E-4	-4.9E-4
161	0.037	-0.025	0.084	-0.040	-0.038	-0.057	4.9E-4	-1.9E-4	1.2E-4	-2.3E-4	4.5E-4	-2.3E-4
162	0.025	-0.038	0.138	-0.094	-0.025	-0.070	1.2E-3	-8.4E-4	1.4E-4	-2.5E-4	5.3E-4	-7.4E-4
163	0.028	-0.040	0.091	-0.133	-0.023	-0.072	8.2E-4	-1.1E-3	1.6E-4	-2.7E-4	7.1E-4	-4.9E-4
164	0.039	-0.027	0.030	-0.075	-0.038	-0.058	1.4E-4	-4.5E-4	1.4E-4	-2.5E-4	2.2E-4	-4.4E-4
165	0.032	-0.033	0.184	-0.177	-0.037	-0.044	1.7E-3	-1.7E-3	1.8E-4	-2.6E-4	3.9E-4	-3.8E-4

166	0.034	-0.032	0.112	-0.105	-0.038	-0.044	9.4E-4	-9.2E-4	2.6E-4	-1.8E-4	4.1E-4	-4.1E-4
167	0.136	-0.136	2.099	-2.095	-0.013	-0.088	2.4E-4	-1.2E-4	1.8E-4	-1.5E-4	1.6E-3	-1.6E-3
168	0.145	-0.145	2.126	-2.118	-0.037	-0.058	3.1E-3	-3.3E-3	5.8E-5	-2.7E-5	9.1E-4	-9.3E-4
169	0.145	-0.145	2.120	-2.111	-0.036	-0.056	3.5E-3	-3.5E-3	3.9E-5	-7.7E-6	3.8E-4	-3.8E-4
170	0.145	-0.145	2.057	-2.050	-0.036	-0.054	3.4E-3	-3.4E-3	3.0E-5	-6.6E-6	7.1E-4	-6.8E-4
171	0.145	-0.144	1.972	-1.968	-0.037	-0.052	3.4E-3	-3.4E-3	2.4E-5	-8.6E-6	1.0E-3	-9.8E-4
172	0.145	-0.144	1.836	-1.837	-0.038	-0.051	3.2E-3	-3.2E-3	1.2E-5	-3.6E-6	1.3E-3	-1.2E-3
173	0.145	-0.144	1.629	-1.631	-0.038	-0.051	2.9E-3	-2.9E-3	6.0E-6	-3.5E-6	1.7E-3	-1.7E-3
174	0.145	-0.144	1.426	-1.429	-0.038	-0.051	2.5E-3	-2.5E-3	5.9E-6	-7.4E-6	2.0E-3	-2.0E-3
175	0.145	-0.144	1.228	-1.229	-0.039	-0.051	2.2E-3	-2.1E-3	3.2E-6	-9.7E-6	2.0E-3	-2.0E-3
176	0.145	-0.144	0.985	-0.983	-0.039	-0.052	1.8E-3	-1.8E-3	2.9E-6	-1.8E-5	2.1E-3	-2.2E-3
177	0.145	-0.144	0.785	-0.779	-0.039	-0.054	1.4E-3	-1.4E-3	4.8E-6	-3.0E-5	2.0E-3	-2.0E-3
178	0.145	-0.144	0.625	-0.617	-0.038	-0.056	1.0E-3	-1.1E-3	7.2E-6	-4.0E-5	1.6E-3	-1.6E-3
179	0.145	-0.144	0.443	-0.436	-0.039	-0.058	6.2E-4	-7.8E-4	2.7E-5	-6.0E-5	1.5E-3	-1.5E-3
180	0.136	-0.136	0.250	-0.246	-0.034	-0.067	1.1E-4	9.3E-6	3.6E-5	-7.1E-5	1.6E-3	-1.6E-3
181	0.397	-0.396	2.099	-2.096	-0.038	-0.080	1.7E-4	-7.2E-5	-1.7E-3	-2.5E-3	1.9E-3	-1.9E-3
182	0.394	-0.398	0.250	-0.246	-0.039	-0.080	9.6E-5	5.0E-6	2.5E-3	1.8E-3	1.9E-3	-1.9E-3
183	0.642	-0.642	2.099	-2.096	-0.046	-0.083	1.1E-4	-4.5E-5	-1.9E-3	-2.8E-3	1.9E-3	-1.9E-3
184	0.641	-0.644	0.250	-0.246	-0.042	-0.088	7.4E-5	-6.2E-6	2.8E-3	1.9E-3	2.0E-3	-1.9E-3
185	0.890	-0.889	2.100	-2.096	-0.048	-0.088	6.6E-5	-3.1E-5	-1.8E-3	-2.8E-3	1.9E-3	-1.9E-3
186	0.889	-0.891	0.250	-0.246	-0.044	-0.092	5.9E-5	-2.2E-5	2.8E-3	1.8E-3	1.9E-3	-1.9E-3
187	1.126	-1.124	2.100	-2.097	-0.048	-0.091	5.2E-5	-3.9E-5	-1.8E-3	-2.8E-3	1.9E-3	-1.9E-3
188	1.125	-1.126	0.250	-0.246	-0.046	-0.094	4.8E-5	-3.3E-5	2.8E-3	1.8E-3	1.9E-3	-1.9E-3
189	1.337	-1.334	2.100	-2.097	-0.046	-0.094	4.3E-5	-4.1E-5	-1.7E-3	-2.8E-3	1.9E-3	-1.9E-3
190	1.335	-1.334	0.250	-0.246	-0.046	-0.095	4.0E-5	-3.6E-5	2.8E-3	1.7E-3	1.9E-3	-1.9E-3
191	1.521	-1.517	2.100	-2.097	-0.043	-0.097	4.3E-5	-4.1E-5	-1.6E-3	-2.8E-3	1.6E-3	-1.6E-3
192	1.523	-1.522	0.250	-0.246	-0.043	-0.098	3.4E-5	-3.3E-5	2.8E-3	1.6E-3	1.8E-3	-1.8E-3
193	1.684	-1.683	0.250	-0.246	-0.041	-0.101	3.2E-5	-2.9E-5	2.9E-3	1.6E-3	1.6E-3	-1.6E-3
194	1.691	-1.687	2.100	-2.097	-0.041	-0.100	4.4E-5	-3.7E-5	-1.6E-3	-2.9E-3	1.3E-3	-1.3E-3
195	1.804	-1.804	0.250	-0.246	-0.039	-0.103	3.4E-5	-2.9E-5	2.9E-3	1.5E-3	1.2E-3	-1.2E-3
196	1.808	-1.805	2.100	-2.097	-0.041	-0.102	4.5E-5	-3.4E-5	-1.5E-3	-2.9E-3	1.1E-3	-1.1E-3
197	1.875	-1.876	0.250	-0.246	-0.039	-0.103	3.2E-5	-2.8E-5	2.9E-3	1.6E-3	8.8E-4	-8.9E-4
198	1.879	-1.877	2.100	-2.097	-0.041	-0.102	4.1E-5	-3.1E-5	-1.5E-3	-2.9E-3	8.6E-4	-8.7E-4
199	1.906	-1.909	0.250	-0.246	-0.040	-0.103	2.9E-5	-2.7E-5	2.9E-3	1.5E-3	5.3E-4	-5.4E-4
200	1.911	-1.910	2.100	-2.097	-0.043	-0.102	4.1E-5	-3.4E-5	-1.5E-3	-2.9E-3	5.1E-4	-5.2E-4
201	1.891	-1.895	0.249	-0.246	-0.040	-0.103	3.0E-5	-3.1E-5	2.9E-3	1.5E-3	3.4E-4	-3.5E-4
202	1.919	-1.920	2.100	-2.097	-0.043	-0.103	3.7E-5	-3.3E-5	-1.5E-3	-2.9E-3	3.4E-4	-3.5E-4
203	1.884	-1.889	0.249	-0.246	-0.041	-0.102	3.1E-5	-3.4E-5	3.0E-3	1.5E-3	6.4E-4	-6.5E-4
204	1.912	-1.915	2.100	-2.097	-0.042	-0.104	3.3E-5	-3.1E-5	-1.5E-3	-2.9E-3	6.1E-4	-6.2E-4
205	1.843	-1.849	0.249	-0.246	-0.041	-0.102	3.4E-5	-3.7E-5	3.0E-3	1.5E-3	8.9E-4	-8.9E-4
206	1.873	-1.877	2.100	-2.097	-0.042	-0.104	2.7E-5	-2.9E-5	-1.6E-3	-2.9E-3	8.4E-4	-8.5E-4
207	1.780	-1.788	0.249	-0.246	-0.042	-0.100	4.4E-5	-4.5E-5	2.9E-3	1.6E-3	9.1E-4	-9.1E-4
208	1.791	-1.795	2.100	-2.097	-0.042	-0.103	2.6E-5	-2.8E-5	-1.6E-3	-2.9E-3	1.3E-3	-1.3E-3
209	1.748	-1.752	2.100	-2.097	-0.043	-0.103	2.6E-5	-2.8E-5	-1.6E-3	-2.9E-3	1.5E-3	-1.5E-3
210	1.731	-1.738	0.249	-0.246	-0.043	-0.099	4.6E-5	-4.4E-5	2.9E-3	1.6E-3	1.1E-3	-1.1E-3
211	1.611	-1.615	2.099	-2.097	-0.044	-0.102	2.9E-5	-3.2E-5	-1.6E-3	-2.8E-3	1.6E-3	-1.6E-3
212	1.613	-1.620	0.249	-0.246	-0.046	-0.097	4.5E-5	-4.0E-5	2.9E-3	1.6E-3	1.6E-3	-1.6E-3
213	1.429	-1.432	2.099	-2.096	-0.045	-0.100	3.2E-5	-4.1E-5	-1.7E-3	-2.8E-3	1.9E-3	-1.9E-3
214	1.429	-1.434	0.249	-0.246	-0.047	-0.096	3.8E-5	-3.8E-5	2.8E-3	1.7E-3	1.9E-3	-1.9E-3
215	1.211	-1.213	2.099	-2.096	-0.047	-0.096	3.2E-5	-5.5E-5	-1.8E-3	-2.8E-3	2.0E-3	-2.0E-3
216	1.210	-1.214	0.249	-0.246	-0.049	-0.094	3.3E-5	-4.8E-5	2.8E-3	1.7E-3	2.0E-3	-2.0E-3
217	0.968	-0.969	2.099	-2.096	-0.046	-0.092	2.5E-5	-7.0E-5	-1.8E-3	-2.8E-3	2.1E-3	-2.1E-3
218	0.968	-0.972	0.249	-0.246	-0.048	-0.091	2.2E-5	-6.2E-5	2.8E-3	1.8E-3	2.0E-3	-2.0E-3
219	0.703	-0.703	2.098	-2.096	-0.042	-0.089	3.8E-5	-1.1E-4	-1.8E-3	-2.8E-3	2.1E-3	-2.1E-3
220	0.701	-0.705	0.249	-0.246	-0.046	-0.086	2.4E-6	-7.5E-5	2.8E-3	1.9E-3	2.1E-3	-2.1E-3
221	0.437	-0.436	2.098	-2.096	-0.035	-0.084	6.9E-5	-1.7E-4	-1.7E-3	-2.5E-3	2.0E-3	-2.0E-3
222	0.434	-0.437	0.249	-0.246	-0.041	-0.079	-1.2E-5	-9.6E-5	2.5E-3	1.7E-3	2.1E-3	-2.0E-3
223	0.145	-0.145	2.098	-2.095	-0.009	-0.091	1.2E-4	-2.4E-4	1.8E-4	-1.5E-4	1.8E-3	-1.8E-3
224	0.156	-0.156	2.117	-2.119	-0.034	-0.060	3.3E-3	-3.1E-3	7.0E-5	-3.8E-5	1.1E-3	-1.1E-3
225	0.156	-0.156	2.127	-2.130	-0.035	-0.055	3.6E-3	-3.5E-3	4.9E-5	-1.7E-5	5.3E-4	-5.3E-4
226	0.156	-0.155	2.066	-2.068	-0.035	-0.053	3.5E-3	-3.5E-3	3.3E-5	-9.1E-6	7.8E-4	-8.0E-4
227	0.156	-0.155	1.991	-1.989	-0.036	-0.052	3.4E-3	-3.4E-3	2.1E-5	-6.6E-6	1.1E-3	-1.1E-3
228	0.156	-0.155	1.863	-1.858	-0.037	-0.051	3.2E-3	-3.2E-3	1.2E-5	-6.2E-6	1.3E-3	-1.3E-3
229	0.156	-0.155	1.646	-1.640	-0.038	-0.051	2.9E-3	-2.9E-3	1.2E-5	-1.1E-5	1.9E-3	-1.9E-3
230	0.156	-0.155	1.433	-1.427	-0.039	-0.051	2.5E-3	-2.6E-3	1.0E-5	-1.2E-5	2.1E-3	-2.1E-3
231	0.156	-0.155	1.230	-1.225	-0.038	-0.051	2.1E-3	-2.2E-3	4.0E-6	-9.8E-6	2.0E-3	-2.0E-3
232	0.156	-0.155	0.970	-0.967	-0.039	-0.052	1.7E-3	-1.7E-3	3.2E-6	-1.7E-5	2.2E-3	-2.2E-3
233	0.156	-0.155	0.761	-0.761	-0.039	-0.053	1.3E-3	-1.3E-3	4.6E-6	-2.9E-5	2.1E-3	-2.1E-3
234	0.156	-0.155	0.604	-0.606	-0.038	-0.056	1.1E-3	-9.8E-4	9.8E-6	-4.2E-5	1.7E-3	-1.7E-3
235	0.156	-0.155	0.417	-0.418	-0.038	-0.058	7.8E-4	-6.0E-4	3.1E-5	-6.4E-5	1.5E-3	-1.6E-3
236	0.146	-0.145	0.249	-0.246	-0.033	-0.068	-1.8E-5	-1.1E-4	4.4E-5	-8.1E-5	1.8E-3	-1.8E-3
237	0.106	-0.106	1.141	-1.150	-0.037	-0.050	3.0E-3	-2.9E-3	1.4E-4	-2.3E-4	1.0E-3	-1.0E-3

238	0.106	-0.106	0.718	-0.726	-0.038	-0.050	1.9E-3	-1.9E-3	1.4E-4	-2.3E-4	1.6E-3	-1.6E-3
239	0.106	-0.100	0.298	-0.246	-0.036	-0.059	6.4E-4	-8.8E-4	2.6E-4	-1.2E-4	1.2E-3	-9.5E-4
240	0.102	-0.107	1.322	-1.270	-0.023	-0.071	5.1E-3	-5.3E-3	1.4E-4	-2.8E-4	1.0E-3	-1.3E-3
241	0.108	-0.113	1.244	-1.291	-0.020	-0.074	5.3E-3	-5.0E-3	1.5E-4	-2.9E-4	1.4E-3	-1.1E-3
242	0.113	-0.108	0.205	-0.255	-0.035	-0.060	8.1E-4	-5.4E-4	1.4E-4	-2.4E-4	9.8E-4	-1.3E-3
243	0.113	-0.113	1.265	-1.255	-0.036	-0.050	3.2E-3	-3.2E-3	2.4E-4	-1.5E-4	9.6E-4	-9.8E-4
244	0.114	-0.113	0.735	-0.724	-0.037	-0.050	1.8E-3	-1.9E-3	1.5E-4	-2.4E-4	1.5E-3	-1.5E-3
245	0.107	-0.105	0.163	-0.164	-0.033	-0.065	6.1E-4	-6.1E-4	2.8E-4	-2.6E-4	2.8E-3	-1.2E-4
246	0.578	-0.007	0.057	-0.057	-0.037	-0.075	4.1E-4	-4.0E-4	3.5E-4	-1.4E-3	2.3E-3	-5.2E-4
247	0.648	-0.073	0.162	-0.164	-0.039	-0.079	5.8E-4	-5.8E-4	1.3E-3	1.1E-5	3.2E-3	-1.4E-4
248	0.821	-0.092	0.057	-0.057	-0.039	-0.081	3.9E-4	-3.7E-4	9.1E-4	-1.7E-3	1.8E-3	-1.0E-3
249	0.970	-0.228	0.055	-0.055	-0.040	-0.085	3.8E-4	-3.7E-4	1.3E-3	-2.1E-3	1.4E-3	-1.5E-3
250	1.116	-0.383	0.055	-0.055	-0.042	-0.086	3.8E-4	-3.6E-4	1.7E-3	-2.5E-3	1.4E-3	-1.4E-3
251	1.246	-0.518	0.054	-0.056	-0.040	-0.088	3.7E-4	-3.7E-4	2.0E-3	-2.9E-3	1.4E-3	-1.4E-3
252	1.371	-0.642	0.054	-0.056	-0.038	-0.090	3.6E-4	-3.8E-4	2.4E-3	-3.2E-3	1.4E-3	-1.4E-3
253	1.472	-0.743	0.053	-0.056	-0.035	-0.094	3.6E-4	-3.8E-4	2.7E-3	-3.5E-3	1.2E-3	-1.2E-3
254	1.562	-0.832	0.053	-0.056	-0.035	-0.096	3.4E-4	-3.9E-4	2.9E-3	-3.8E-3	1.0E-3	-1.0E-3
255	1.609	-0.879	0.052	-0.058	-0.034	-0.097	3.4E-4	-3.9E-4	3.1E-3	-3.9E-3	7.4E-4	-7.4E-4
256	1.625	-0.895	0.052	-0.058	-0.035	-0.096	3.3E-4	-4.0E-4	3.1E-3	-3.9E-3	6.1E-4	-6.1E-4
257	1.620	-0.891	0.052	-0.058	-0.035	-0.097	3.1E-4	-3.9E-4	3.1E-3	-3.9E-3	4.5E-4	-4.5E-4
258	1.611	-0.883	0.052	-0.058	-0.035	-0.095	3.1E-4	-4.0E-4	3.1E-3	-3.9E-3	5.8E-4	-5.9E-4
259	1.597	-0.870	0.054	-0.059	-0.036	-0.095	3.1E-4	-3.9E-4	3.0E-3	-3.8E-3	6.9E-4	-6.9E-4
260	1.555	-0.827	0.054	-0.059	-0.036	-0.094	3.4E-4	-3.9E-4	2.9E-3	-3.7E-3	7.4E-4	-7.5E-4
261	1.501	-0.775	0.057	-0.059	-0.037	-0.092	3.4E-4	-3.8E-4	2.8E-3	-3.6E-3	1.0E-3	-1.0E-3
262	1.441	-0.715	0.057	-0.059	-0.040	-0.090	3.6E-4	-3.8E-4	2.6E-3	-3.4E-3	1.1E-3	-1.1E-3
263	1.321	-0.594	0.059	-0.059	-0.042	-0.089	3.7E-4	-3.7E-4	2.3E-3	-3.1E-3	1.4E-3	-1.4E-3
264	0.911	-0.243	0.156	-0.156	-0.041	-0.086	5.4E-4	-5.3E-4	1.8E-3	-7.0E-6	1.8E-3	-1.7E-3
265	1.137	-0.459	0.156	-0.156	-0.042	-0.091	5.5E-4	-5.4E-4	2.0E-3	-1.9E-4	1.7E-3	-1.7E-3
266	1.343	-0.670	0.155	-0.154	-0.044	-0.092	5.5E-4	-5.4E-4	2.3E-3	-4.6E-4	1.7E-3	-1.7E-3
267	1.525	-0.854	0.155	-0.154	-0.043	-0.094	5.5E-4	-5.4E-4	2.5E-3	-6.9E-4	1.7E-3	-1.7E-3
268	1.696	-1.024	0.151	-0.156	-0.040	-0.097	5.6E-4	-5.3E-4	2.7E-3	-9.1E-4	1.6E-3	-1.6E-3
269	1.837	-1.165	0.151	-0.156	-0.037	-0.100	5.4E-4	-5.4E-4	2.9E-3	-1.1E-3	1.6E-3	-1.6E-3
270	1.946	-1.274	0.144	-0.160	-0.037	-0.102	5.4E-4	-5.4E-4	3.1E-3	-1.3E-3	1.1E-3	-1.1E-3
271	2.008	-1.336	0.144	-0.160	-0.036	-0.104	5.4E-4	-5.4E-4	3.1E-3	-1.3E-3	9.4E-4	-9.5E-4
272	1.163	-0.433	0.059	-0.059	-0.043	-0.087	3.7E-4	-3.7E-4	1.8E-3	-2.7E-3	1.5E-3	-1.5E-3
273	1.025	-0.283	0.059	-0.060	-0.044	-0.084	3.6E-4	-3.7E-4	1.4E-3	-2.2E-3	1.4E-3	-1.4E-3
274	0.845	-0.116	0.059	-0.060	-0.042	-0.079	3.7E-4	-3.7E-4	9.6E-4	-1.8E-3	1.4E-3	-1.6E-3
275	0.588	-0.021	0.061	-0.064	-0.039	-0.074	3.9E-4	-4.1E-4	3.6E-4	-1.4E-3	-1.6E-4	-3.1E-3
276	0.087	-0.083	0.061	-0.064	-0.030	-0.066	3.9E-4	-4.0E-4	2.7E-4	-2.4E-4	6.5E-6	-2.6E-3
277	2.031	-1.351	0.138	-0.159	-0.037	-0.102	5.3E-4	-5.5E-4	3.2E-3	-1.5E-3	4.8E-4	-4.9E-4
278	2.022	-1.353	0.138	-0.159	-0.037	-0.103	5.3E-4	-5.4E-4	3.2E-3	-1.4E-3	4.5E-4	-4.5E-4
279	2.018	-1.349	0.138	-0.162	-0.038	-0.102	5.3E-4	-5.4E-4	3.1E-3	-1.3E-3	7.5E-4	-7.5E-4
280	1.984	-1.317	0.138	-0.162	-0.038	-0.101	5.2E-4	-5.5E-4	3.1E-3	-1.3E-3	8.2E-4	-8.3E-4
281	1.926	-1.259	0.146	-0.159	-0.038	-0.100	5.2E-4	-5.5E-4	3.0E-3	-1.2E-3	8.3E-4	-8.4E-4
282	1.876	-1.210	0.146	-0.159	-0.040	-0.098	5.5E-4	-5.4E-4	3.0E-3	-1.1E-3	9.5E-4	-9.5E-4
283	1.777	-1.110	0.155	-0.154	-0.042	-0.096	5.5E-4	-5.3E-4	2.9E-3	-1.1E-3	1.6E-3	-1.6E-3
284	1.609	-0.942	0.155	-0.154	-0.044	-0.095	5.4E-4	-5.4E-4	2.7E-3	-8.6E-4	1.7E-3	-1.7E-3
285	1.422	-0.752	0.155	-0.154	-0.046	-0.093	5.4E-4	-5.3E-4	2.3E-3	-5.3E-4	1.9E-3	-1.8E-3
286	1.208	-0.532	0.155	-0.154	-0.047	-0.089	5.5E-4	-5.3E-4	2.1E-3	-2.7E-4	1.9E-3	-1.8E-3
287	0.967	-0.299	0.158	-0.155	-0.044	-0.085	5.5E-4	-5.4E-4	1.8E-3	-2.2E-6	1.8E-3	-2.2E-3
288	0.686	-0.106	0.158	-0.155	-0.041	-0.078	5.4E-4	-5.1E-4	1.2E-3	2.6E-5	1.5E-3	-2.4E-3
289	0.113	-0.113	0.161	-0.157	-0.031	-0.067	7.7E-4	-7.1E-4	2.8E-4	-2.6E-4	7.5E-4	-2.2E-3
290	0.143	-0.610	1.697	-1.700	-0.041	-0.079	5.3E-3	-5.4E-3	-9.5E-4	-1.7E-3	1.4E-3	-1.8E-3
291	0.398	-0.394	2.250	-2.244	-0.323	-0.456	1.0E-3	-1.1E-3	-1.8E-3	-2.6E-3	1.4E-3	-1.4E-3
292	0.608	-0.147	0.198	-0.201	-0.040	-0.081	5.8E-4	-6.2E-4	1.7E-3	9.1E-4	2.4E-3	-1.0E-3
293	0.392	-0.399	0.447	-0.437	-0.319	-0.454	1.1E-4	-3.3E-4	2.6E-3	1.9E-3	1.5E-3	-1.4E-3
294	0.349	-0.873	1.705	-1.705	-0.046	-0.084	5.3E-3	-5.3E-3	-1.0E-3	-2.1E-3	1.6E-3	-1.7E-3
295	0.643	-0.640	2.257	-2.253	-0.356	-0.502	1.0E-3	-9.8E-4	-2.0E-3	-2.8E-3	1.5E-3	-1.5E-3
296	0.639	-0.645	0.452	-0.446	-0.340	-0.502	2.5E-4	-2.1E-4	2.8E-3	1.9E-3	1.5E-3	-1.5E-3
297	0.871	-0.350	0.193	-0.193	-0.042	-0.088	6.5E-4	-6.5E-4	2.1E-3	1.0E-3	1.8E-3	-1.7E-3
298	0.581	-1.110	1.706	-1.705	-0.047	-0.089	5.3E-3	-5.3E-3	-8.8E-4	-2.3E-3	1.6E-3	-1.6E-3
299	1.112	-0.583	0.194	-0.193	-0.043	-0.093	6.6E-4	-6.4E-4	2.3E-3	8.7E-4	1.7E-3	-1.7E-3
300	0.887	-0.891	0.445	-0.440	-0.336	-0.511	2.4E-4	-2.1E-4	2.8E-3	1.9E-3	1.5E-3	-1.4E-3
301	0.891	-0.887	2.257	-2.255	-0.346	-0.511	1.0E-3	-9.7E-4	-1.9E-3	-2.8E-3	1.4E-3	-1.4E-3
302	1.127	-1.122	2.248	-2.246	-0.339	-0.510	9.8E-4	-9.7E-4	-1.9E-3	-2.8E-3	1.4E-3	-1.4E-3
303	0.806	-1.330	1.707	-1.705	-0.046	-0.092	5.3E-3	-5.3E-3	-7.1E-4	-2.4E-3	1.7E-3	-1.7E-3
304	1.123	-1.126	0.426	-0.422	-0.339	-0.511	2.3E-4	-2.2E-4	2.8E-3	1.9E-3	1.4E-3	-1.4E-3
305	1.330	-0.804	0.193	-0.191	-0.045	-0.094	6.7E-4	-6.5E-4	2.4E-3	7.0E-4	1.7E-3	-1.7E-3
306	1.001	-1.523	1.708	-1.705	-0.044	-0.095	5.3E-3	-5.3E-3	-5.3E-4	-2.6E-3	1.7E-3	-1.7E-3
307	1.337	-1.331	2.237	-2.234	-0.336	-0.510	9.7E-4	-9.6E-4	-1.8E-3	-2.8E-3	1.4E-3	-1.4E-3
308	1.332	-1.335	0.404	-0.400	-0.336	-0.511	2.1E-4	-2.0E-4	2.8E-3	1.8E-3	1.4E-3	-1.4E-3
309	1.524	-0.999	0.193	-0.191	-0.044	-0.097	6.7E-4	-6.5E-4	2.6E-3	5.4E-4	1.7E-3	-1.7E-3

310	1.179	-1.700	1.708	-1.705	-0.041	-0.098	5.3E-3	-5.3E-3	-4.1E-4	-2.7E-3	1.5E-3	-1.5E-3
311	1.521	-1.515	2.209	-2.206	-0.314	-0.510	9.5E-4	-9.5E-4	-1.7E-3	-2.8E-3	1.2E-3	-1.2E-3
312	1.520	-1.522	0.387	-0.383	-0.322	-0.511	2.3E-4	-2.1E-4	2.8E-3	1.8E-3	1.4E-3	-1.4E-3
313	1.705	-1.180	0.190	-0.193	-0.041	-0.099	6.9E-4	-6.3E-4	2.7E-3	4.0E-4	1.6E-3	-1.6E-3
314	1.339	-1.860	1.718	-1.702	-0.038	-0.102	5.2E-3	-5.3E-3	-3.1E-4	-2.8E-3	1.2E-3	-1.2E-3
315	1.689	-1.682	2.186	-2.183	-0.310	-0.511	9.0E-4	-9.4E-4	-1.7E-3	-2.8E-3	1.0E-3	-1.0E-3
316	1.684	-1.686	0.359	-0.356	-0.313	-0.511	2.1E-4	-1.8E-4	2.8E-3	1.7E-3	1.4E-3	-1.4E-3
317	1.856	-1.330	0.189	-0.193	-0.038	-0.103	6.9E-4	-6.3E-4	2.8E-3	3.0E-4	1.5E-3	-1.5E-3
318	1.448	-1.970	1.721	-1.701	-0.038	-0.104	5.2E-3	-5.4E-3	-2.0E-4	-2.9E-3	1.1E-3	-1.1E-3
319	1.806	-1.800	2.188	-2.184	-0.308	-0.512	8.9E-4	-9.4E-4	-1.7E-3	-2.8E-3	1.0E-3	-1.0E-3
320	1.804	-1.807	0.312	-0.309	-0.310	-0.512	2.4E-4	-1.8E-4	2.8E-3	1.7E-3	1.1E-3	-1.1E-3
321	1.970	-1.445	0.183	-0.196	-0.037	-0.105	7.4E-4	-6.1E-4	2.9E-3	1.8E-4	1.1E-3	-1.1E-3
322	1.514	-2.038	1.724	-1.702	-0.039	-0.104	5.2E-3	-5.3E-3	-1.6E-4	-3.0E-3	8.1E-4	-8.1E-4
323	1.878	-1.873	2.181	-2.178	-0.305	-0.513	8.8E-4	-9.4E-4	-1.7E-3	-2.8E-3	9.5E-4	-9.6E-4
324	1.874	-1.878	0.298	-0.295	-0.314	-0.513	2.0E-4	-1.4E-4	2.8E-3	1.7E-3	1.0E-3	-1.0E-3
325	2.035	-1.510	0.182	-0.196	-0.037	-0.106	7.4E-4	-6.1E-4	3.0E-3	1.5E-4	8.9E-4	-8.8E-4
326	1.542	-2.067	1.726	-1.703	-0.041	-0.104	5.2E-3	-5.3E-3	-1.1E-4	-3.0E-3	4.9E-4	-4.9E-4
327	1.911	-1.908	2.172	-2.168	-0.317	-0.514	8.6E-4	-9.3E-4	-1.7E-3	-2.8E-3	9.6E-4	-9.6E-4
328	1.904	-1.910	0.285	-0.282	-0.305	-0.513	2.1E-4	-1.4E-4	2.8E-3	1.7E-3	1.0E-3	-1.0E-3
329	2.067	-1.543	0.181	-0.198	-0.038	-0.105	7.6E-4	-6.1E-4	3.0E-3	1.1E-4	4.9E-4	-4.9E-4
330	1.549	-2.076	1.728	-1.702	-0.040	-0.105	5.2E-3	-5.3E-3	-9.7E-5	-3.0E-3	4.0E-4	-3.9E-4
331	1.920	-1.918	2.163	-2.158	-0.312	-0.514	8.7E-4	-9.4E-4	-1.7E-3	-2.8E-3	1.0E-3	-1.0E-3
332	1.889	-1.896	0.273	-0.271	-0.311	-0.513	1.7E-4	-1.0E-4	2.8E-3	1.7E-3	1.0E-3	-1.0E-3
333	2.051	-1.529	0.178	-0.195	-0.038	-0.105	7.7E-4	-6.2E-4	3.0E-3	1.2E-4	2.9E-4	-2.9E-4
334	1.546	-2.074	1.729	-1.702	-0.039	-0.106	5.2E-3	-5.4E-3	-1.2E-4	-3.0E-3	6.5E-4	-6.5E-4
335	1.914	-1.914	2.149	-2.145	-0.314	-0.515	8.7E-4	-9.5E-4	-1.7E-3	-2.8E-3	9.8E-4	-9.8E-4
336	1.880	-1.888	0.259	-0.256	-0.305	-0.513	1.8E-4	-1.1E-4	2.8E-3	1.7E-3	9.9E-4	-9.9E-4
337	2.048	-1.527	0.178	-0.197	-0.038	-0.104	7.8E-4	-6.1E-4	3.0E-3	1.5E-4	6.2E-4	-6.2E-4
338	1.505	-2.035	1.729	-1.700	-0.039	-0.106	5.2E-3	-5.4E-3	-1.0E-4	-3.0E-3	8.9E-4	-8.8E-4
339	1.876	-1.876	2.146	-2.143	-0.320	-0.515	8.7E-4	-9.6E-4	-1.7E-3	-2.8E-3	9.6E-4	-9.6E-4
340	2.007	-1.486	0.177	-0.198	-0.039	-0.104	7.8E-4	-6.1E-4	3.0E-3	1.6E-4	8.0E-4	-8.0E-4
341	1.837	-1.847	0.254	-0.251	-0.305	-0.514	1.7E-4	-8.6E-5	2.8E-3	1.7E-3	9.8E-4	-9.8E-4
342	1.430	-1.961	1.730	-1.700	-0.040	-0.106	5.2E-3	-5.4E-3	-1.7E-4	-3.0E-3	1.2E-3	-1.2E-3
343	1.799	-1.801	2.194	-2.191	-0.321	-0.515	8.9E-4	-9.9E-4	-1.7E-3	-2.8E-3	1.3E-3	-1.3E-3
344	1.774	-1.784	0.294	-0.291	-0.315	-0.513	1.5E-4	-8.1E-5	2.8E-3	1.7E-3	1.2E-3	-1.2E-3
345	1.949	-1.429	0.184	-0.196	-0.039	-0.103	7.2E-4	-6.3E-4	2.9E-3	2.4E-4	8.3E-4	-8.3E-4
346	1.393	-1.924	1.710	-1.707	-0.040	-0.105	5.3E-3	-5.3E-3	-2.1E-4	-2.9E-3	1.3E-3	-1.3E-3
347	1.747	-1.748	2.200	-2.198	-0.322	-0.514	9.3E-4	-9.3E-4	-1.7E-3	-2.8E-3	1.3E-3	-1.3E-3
348	1.729	-1.739	0.306	-0.303	-0.315	-0.512	1.3E-4	-1.0E-4	2.8E-3	1.7E-3	1.3E-3	-1.3E-3
349	1.898	-1.379	0.186	-0.194	-0.041	-0.101	7.3E-4	-6.2E-4	2.9E-3	2.8E-4	1.0E-3	-9.9E-4
350	1.264	-1.793	1.708	-1.705	-0.042	-0.103	5.3E-3	-5.3E-3	-3.2E-4	-2.8E-3	1.4E-3	-1.4E-3
351	1.611	-1.612	2.191	-2.189	-0.324	-0.514	9.4E-4	-9.4E-4	-1.7E-3	-2.8E-3	1.3E-3	-1.2E-3
352	1.610	-1.620	0.284	-0.281	-0.317	-0.512	1.3E-4	-1.2E-4	2.8E-3	1.7E-3	1.2E-3	-1.2E-3
353	1.789	-1.270	0.193	-0.191	-0.043	-0.099	6.7E-4	-6.5E-4	2.8E-3	3.2E-4	1.5E-3	-1.5E-3
354	1.090	-1.618	1.709	-1.706	-0.043	-0.101	5.3E-3	-5.3E-3	-4.7E-4	-2.7E-3	1.7E-3	-1.7E-3
355	1.430	-1.429	2.210	-2.208	-0.327	-0.513	9.4E-4	-9.5E-4	-1.8E-3	-2.8E-3	1.4E-3	-1.4E-3
356	1.426	-1.435	0.291	-0.287	-0.334	-0.513	1.5E-4	-1.4E-4	2.8E-3	1.8E-3	1.4E-3	-1.4E-3
357	1.614	-1.094	0.193	-0.191	-0.045	-0.097	6.7E-4	-6.5E-4	2.7E-3	4.7E-4	1.7E-3	-1.7E-3
358	0.886	-1.414	1.708	-1.705	-0.045	-0.097	5.3E-3	-5.3E-3	-6.4E-4	-2.5E-3	1.7E-3	-1.7E-3
359	1.212	-1.211	2.227	-2.225	-0.339	-0.513	9.5E-4	-9.7E-4	-1.9E-3	-2.8E-3	1.4E-3	-1.4E-3
360	1.413	-0.891	0.193	-0.190	-0.047	-0.095	6.6E-4	-6.5E-4	2.5E-3	6.6E-4	1.8E-3	-1.8E-3
361	1.207	-1.215	0.304	-0.300	-0.337	-0.513	1.5E-4	-1.6E-4	2.8E-3	1.9E-3	1.5E-3	-1.4E-3
362	0.655	-1.186	1.708	-1.704	-0.045	-0.093	5.3E-3	-5.3E-3	-8.1E-4	-2.4E-3	1.7E-3	-1.7E-3
363	0.969	-0.967	2.237	-2.235	-0.339	-0.512	9.6E-4	-1.0E-3	-1.9E-3	-2.8E-3	1.6E-3	-1.6E-3
364	1.181	-0.655	0.193	-0.190	-0.047	-0.091	6.7E-4	-6.5E-4	2.4E-3	8.0E-4	1.9E-3	-1.8E-3
365	0.966	-0.972	0.328	-0.325	-0.350	-0.513	1.6E-4	-1.9E-4	2.8E-3	1.9E-3	1.5E-3	-1.5E-3
366	0.405	-0.930	1.708	-1.702	-0.041	-0.090	5.3E-3	-5.3E-3	-9.9E-4	-2.1E-3	1.9E-3	-1.8E-3
367	0.704	-0.702	2.236	-2.235	-0.335	-0.503	9.8E-4	-1.0E-3	-1.9E-3	-2.8E-3	1.6E-3	-1.6E-3
368	0.700	-0.706	0.340	-0.339	-0.348	-0.503	1.7E-4	-1.8E-4	2.8E-3	1.9E-3	1.6E-3	-1.6E-3
369	0.931	-0.410	0.195	-0.191	-0.045	-0.087	6.6E-4	-6.3E-4	2.1E-3	1.0E-3	1.8E-3	-2.0E-3
370	0.182	-0.650	1.703	-1.695	-0.036	-0.085	5.3E-3	-5.3E-3	-8.7E-4	-1.8E-3	2.0E-3	-1.6E-3
371	0.438	-0.434	2.227	-2.227	-0.318	-0.457	1.0E-3	-1.0E-3	-1.8E-3	-2.6E-3	1.5E-3	-1.5E-3
372	0.432	-0.439	0.361	-0.358	-0.316	-0.456	1.7E-4	-1.5E-4	2.6E-3	1.8E-3	1.5E-3	-1.5E-3
373	0.650	-0.186	0.196	-0.190	-0.041	-0.080	6.7E-4	-6.2E-4	1.7E-3	9.1E-4	1.7E-3	-2.1E-3
374	0.010	-0.010	0.012	-0.012	-0.035	-0.075	4.9E-5	-3.4E-5	3.3E-4	1.3E-5	4.8E-6	-5.2E-6
375	0.010	-0.010	0.012	-0.012	-0.034	-0.080	4.2E-5	-1.9E-5	3.8E-4	-1.0E-5	4.7E-6	-4.9E-6
376	0.010	-0.010	0.012	-0.012	-0.035	-0.082	3.7E-5	-2.4E-5	4.0E-4	-1.8E-5	4.7E-6	-4.8E-6
377	0.009	-0.010	0.012	-0.012	-0.036	-0.082	2.7E-5	-2.1E-5	4.0E-4	-2.2E-5	4.7E-6	-4.8E-6
378	0.009	-0.010	0.012	-0.012	-0.036	-0.082	2.3E-5	-2.0E-5	4.1E-4	-2.0E-5	4.5E-6	-4.6E-6
379	0.009	-0.010	0.012	-0.012	-0.036	-0.083	2.4E-5	-2.0E-5	4.1E-4	-2.1E-5	4.5E-6	-4.6E-6
380	0.009	-0.010	0.012	-0.012	-0.036	-0.084	3.0E-5	-2.1E-5	4.3E-4	-1.9E-5	4.7E-6	-4.7E-6
381	0.010	-0.010	0.012	-0.012	-0.036	-0.086	3.1E-5	-1.6E-5	4.4E-4	-1.3E-5	4.6E-6	-4.7E-6

382	0.010	-0.010	0.012	-0.012	-0.034	-0.051	1.5E-5	-1.4E-5	2.8E-4	2.7E-5	4.9E-6	-5.0E-6
383	0.010	-0.010	0.012	-0.012	-0.023	-0.040	1.1E-5	-8.6E-6	1.2E-4	2.5E-5	4.9E-6	-4.7E-6
384	0.010	-0.010	0.012	-0.012	-0.020	-0.034	7.2E-6	-6.8E-6	5.1E-5	-6.1E-6	4.8E-6	-4.7E-6
385	0.010	-0.010	0.012	-0.012	-0.022	-0.031	4.1E-6	-4.2E-6	2.5E-5	-3.1E-5	4.8E-6	-4.6E-6
386	0.010	-0.010	0.011	-0.011	-0.025	-0.031	2.3E-6	-2.6E-6	8.6E-6	-3.1E-5	4.7E-6	-4.6E-6
387	0.010	-0.010	0.011	-0.011	-0.027	-0.032	1.2E-6	-1.5E-6	1.6E-8	-2.2E-5	4.7E-6	-4.6E-6
388	0.010	-0.010	0.011	-0.011	-0.028	-0.033	5.3E-7	-9.8E-7	-2.3E-6	-1.3E-5	4.6E-6	-4.5E-6
389	0.010	-0.010	0.011	-0.011	-0.029	-0.034	1.6E-7	-7.2E-7	-1.6E-6	-6.3E-6	4.6E-6	-4.5E-6
390	0.010	-0.010	0.011	-0.011	-0.030	-0.034	-7.2E-8	-7.0E-7	1.9E-6	-4.5E-6	4.6E-6	-4.5E-6
391	0.010	-0.010	0.011	-0.011	-0.030	-0.034	1.4E-7	-4.7E-7	4.4E-6	-2.0E-6	4.5E-6	-4.5E-6
392	0.010	-0.010	0.011	-0.011	-0.029	-0.034	1.8E-7	-6.7E-7	5.9E-6	1.6E-6	4.5E-6	-4.5E-6
393	0.010	-0.010	0.011	-0.011	-0.029	-0.033	3.1E-7	-6.8E-7	1.2E-5	2.4E-6	4.5E-6	-4.6E-6
394	0.010	-0.010	0.011	-0.011	-0.027	-0.033	1.2E-6	-1.3E-6	2.0E-5	5.2E-7	4.5E-6	-4.6E-6
395	0.010	-0.010	0.011	-0.011	-0.025	-0.031	3.1E-6	-2.8E-6	2.8E-5	-7.3E-6	4.5E-6	-4.6E-6
396	0.010	-0.010	0.011	-0.011	-0.023	-0.031	6.3E-6	-5.5E-6	2.8E-5	-2.2E-5	4.5E-6	-4.6E-6
397	0.010	-0.010	0.011	-0.011	-0.021	-0.033	1.1E-5	-9.3E-6	4.8E-6	-4.5E-5	4.5E-6	-4.7E-6
398	0.010	-0.010	0.011	-0.011	-0.024	-0.039	1.5E-5	-1.3E-5	-2.3E-5	-1.1E-4	4.6E-6	-4.7E-6
399	0.010	-0.010	0.011	-0.011	-0.033	-0.048	1.8E-5	-1.6E-5	-2.8E-5	-2.4E-4	4.7E-6	-4.7E-6
400	0.010	-0.010	0.011	-0.011	-0.036	-0.079	2.5E-5	-3.9E-5	-4.2E-6	-3.8E-4	4.5E-6	-5.0E-6
401	0.010	-0.010	0.011	-0.011	-0.036	-0.082	1.9E-5	-4.0E-5	9.0E-6	-4.1E-4	4.6E-6	-4.8E-6
402	0.010	-0.009	0.011	-0.011	-0.036	-0.084	1.2E-5	-2.3E-5	1.8E-5	-4.2E-4	4.6E-6	-4.7E-6
403	0.010	-0.009	0.011	-0.011	-0.036	-0.085	1.9E-5	-2.3E-5	2.2E-5	-4.2E-4	4.4E-6	-4.5E-6
404	0.010	-0.009	0.011	-0.011	-0.036	-0.085	1.6E-5	-1.6E-5	2.4E-5	-4.3E-4	4.5E-6	-4.5E-6
405	0.010	-0.009	0.011	-0.011	-0.035	-0.086	2.1E-5	-1.8E-5	2.3E-5	-4.2E-4	4.7E-6	-4.7E-6
406	0.010	-0.010	0.011	-0.012	-0.035	-0.085	2.3E-5	-1.5E-5	1.6E-5	-4.2E-4	4.9E-6	-4.8E-6
407	0.010	-0.010	0.011	-0.012	-0.036	-0.083	3.4E-5	-1.5E-5	3.9E-6	-4.0E-4	4.9E-6	-4.7E-6
408	0.010	-0.010	0.011	-0.012	-0.036	-0.079	3.4E-5	-1.4E-5	-1.4E-5	-3.7E-4	5.3E-6	-4.8E-6
409	0.010	-0.010	0.011	-0.011	-0.033	-0.049	1.2E-5	-1.1E-5	-3.4E-5	-2.3E-4	4.8E-6	-4.5E-6
410	0.010	-0.010	0.011	-0.011	-0.024	-0.039	1.0E-5	-1.0E-5	-2.3E-5	-1.1E-4	4.7E-6	-4.5E-6
411	0.010	-0.010	0.011	-0.011	-0.021	-0.033	7.8E-6	-8.4E-6	5.4E-6	-4.6E-5	4.7E-6	-4.4E-6
412	0.010	-0.010	0.011	-0.011	-0.023	-0.031	5.1E-6	-5.3E-6	2.7E-5	-2.1E-5	4.6E-6	-4.4E-6
413	0.010	-0.010	0.011	-0.011	-0.025	-0.031	2.9E-6	-2.5E-6	2.7E-5	-5.9E-6	4.6E-6	-4.4E-6
414	0.010	-0.010	0.011	-0.011	-0.027	-0.033	1.7E-6	-9.4E-7	1.8E-5	1.6E-6	4.5E-6	-4.4E-6
415	0.010	-0.010	0.011	-0.011	-0.028	-0.033	1.2E-6	-2.1E-7	1.1E-5	2.5E-6	4.5E-6	-4.4E-6
416	0.010	-0.010	0.011	-0.011	-0.029	-0.034	1.0E-6	1.6E-8	5.9E-6	1.3E-6	4.5E-6	-4.4E-6
417	0.010	-0.010	0.011	-0.011	-0.030	-0.034	7.2E-7	6.0E-8	4.3E-6	-1.9E-6	4.5E-6	-4.5E-6
418	0.010	-0.010	0.011	-0.011	-0.030	-0.034	1.1E-6	6.0E-7	2.0E-6	-4.0E-6	4.5E-6	-4.5E-6
419	0.010	-0.010	0.011	-0.011	-0.029	-0.034	1.1E-6	2.8E-7	-1.4E-6	-5.6E-6	4.5E-6	-4.5E-6
420	0.010	-0.010	0.011	-0.011	-0.029	-0.033	1.2E-6	-3.2E-8	-2.6E-6	-1.0E-5	4.5E-6	-4.6E-6
421	0.010	-0.010	0.011	-0.011	-0.027	-0.033	1.7E-6	-7.5E-7	-1.6E-6	-1.7E-5	4.5E-6	-4.7E-6
422	0.010	-0.010	0.011	-0.011	-0.026	-0.032	3.0E-6	-2.3E-6	5.1E-6	-2.5E-5	4.6E-6	-4.7E-6
423	0.010	-0.010	0.012	-0.011	-0.024	-0.031	5.3E-6	-5.1E-6	1.9E-5	-2.4E-5	4.6E-6	-4.8E-6
424	0.010	-0.010	0.012	-0.012	-0.022	-0.033	8.3E-6	-9.2E-6	4.1E-5	-2.9E-6	4.7E-6	-4.9E-6
425	0.010	-0.010	0.012	-0.012	-0.025	-0.038	1.1E-5	-1.4E-5	1.0E-4	2.2E-5	4.8E-6	-4.9E-6
426	0.010	-0.010	0.012	-0.012	-0.033	-0.047	1.2E-5	-2.0E-5	2.1E-4	3.5E-5	5.0E-6	-5.2E-6
427	0.010	-0.010	0.012	-0.012	-0.037	-0.085	3.3E-5	-3.8E-5	4.3E-4	7.5E-6	4.7E-6	-4.8E-6
428	0.010	-0.010	0.012	-0.012	-0.039	-0.083	2.7E-5	-3.1E-5	4.0E-4	2.2E-5	4.9E-6	-4.8E-6
429	0.010	-0.011	0.012	-0.012	-0.041	-0.080	2.3E-5	-3.5E-5	3.7E-4	3.9E-5	4.8E-6	-4.7E-6
430	0.010	-0.011	0.013	-0.012	-0.042	-0.076	1.8E-5	-4.5E-5	3.3E-4	5.4E-5	4.8E-6	-4.5E-6
431	0.011	-0.011	0.013	-0.012	-0.041	-0.073	1.9E-5	-6.0E-5	2.9E-4	6.0E-5	5.2E-6	-4.6E-6
432	0.011	-0.011	0.013	-0.012	-0.038	-0.069	1.2E-5	-7.1E-5	2.4E-4	4.7E-5	6.0E-6	-4.4E-6
433	0.012	-0.012	0.013	-0.012	-0.028	-0.071	1.2E-4	-1.5E-4	1.9E-4	-4.0E-6	6.4E-6	-4.4E-6
434	0.012	-0.012	0.012	-0.012	-0.022	-0.064	1.2E-4	-1.1E-4	1.8E-4	-5.7E-5	6.6E-6	-4.7E-6
435	0.012	-0.012	0.012	-0.012	-0.026	-0.048	9.2E-5	-5.3E-5	7.0E-5	-2.8E-5	5.3E-6	-4.6E-6
436	0.012	-0.012	0.012	-0.012	-0.030	-0.042	8.2E-5	-3.2E-5	2.8E-5	-2.8E-5	5.0E-6	-4.7E-6
437	0.012	-0.012	0.011	-0.011	-0.033	-0.040	7.5E-5	-2.2E-5	8.8E-6	-1.9E-5	4.8E-6	-4.7E-6
438	0.012	-0.012	0.011	-0.011	-0.034	-0.040	7.0E-5	-1.8E-5	1.5E-5	-1.8E-5	4.7E-6	-4.6E-6
439	0.012	-0.012	0.011	-0.011	-0.034	-0.040	6.3E-5	-1.7E-5	8.5E-6	-5.2E-6	4.6E-6	-4.6E-6
440	0.012	-0.012	0.011	-0.011	-0.034	-0.040	5.4E-5	-9.8E-6	1.4E-5	-1.4E-5	4.6E-6	-4.6E-6
441	0.012	-0.012	0.011	-0.011	-0.034	-0.040	5.2E-5	-5.4E-6	5.6E-6	-8.8E-6	4.5E-6	-4.6E-6
442	0.012	-0.012	0.011	-0.011	-0.035	-0.040	4.9E-5	2.6E-6	1.8E-5	-1.5E-5	4.5E-6	-4.6E-6
443	0.012	-0.012	0.011	-0.011	-0.035	-0.040	4.7E-5	6.6E-6	1.7E-5	-7.5E-6	4.6E-6	-4.7E-6
444	0.012	-0.012	0.011	-0.011	-0.032	-0.039	4.4E-5	6.6E-6	2.3E-5	-2.4E-5	4.5E-6	-4.8E-6
445	0.012	-0.012	0.011	-0.011	-0.031	-0.044	4.3E-5	-3.7E-6	-8.1E-7	-4.1E-5	4.4E-6	-5.0E-6
446	0.012	-0.012	0.011	-0.011	-0.034	-0.052	3.5E-5	-2.3E-5	3.4E-6	-1.3E-4	4.0E-6	-5.7E-6
447	0.012	-0.011	0.012	-0.011	-0.036	-0.063	1.6E-5	-4.4E-5	-1.7E-5	-1.7E-4	3.8E-6	-5.8E-6
448	0.011	-0.011	0.012	-0.011	-0.040	-0.067	9.5E-7	-5.4E-5	-4.9E-5	-2.3E-4	4.2E-6	-5.6E-6
449	0.011	-0.011	0.012	-0.011	-0.042	-0.071	1.0E-5	-5.3E-5	-6.0E-5	-2.9E-4	4.7E-6	-5.3E-6
450	0.011	-0.010	0.012	-0.011	-0.043	-0.075	1.6E-5	-4.3E-5	-5.5E-5	-3.3E-4	4.8E-6	-5.1E-6
451	0.011	-0.010	0.012	-0.011	-0.042	-0.078	2.2E-5	-2.6E-5	-4.1E-5	-3.6E-4	5.0E-6	-5.0E-6
452	0.010	-0.010	0.011	-0.011	-0.040	-0.079	3.6E-5	-1.9E-5	-2.4E-5	-3.8E-4	5.0E-6	-4.9E-6
453	0.010	-0.010	0.011	-0.011	-0.037	-0.078	3.3E-5	-1.1E-5	-1.4E-5	-3.8E-4	4.8E-6	-4.3E-6

454	0.011	-0.011	0.012	-0.013	-0.030	-0.069	1.5E-4	-1.2E-4	1.9E-4	-1.1E-6	4.3E-6	-6.2E-6
455	0.011	-0.011	0.012	-0.013	-0.040	-0.066	7.0E-5	-1.5E-5	2.3E-4	5.3E-5	4.4E-6	-5.9E-6
456	0.010	-0.011	0.012	-0.013	-0.043	-0.070	5.8E-5	-2.3E-5	2.8E-4	6.7E-5	4.7E-6	-5.3E-6
457	0.010	-0.011	0.012	-0.012	-0.043	-0.073	3.7E-5	-2.5E-5	3.1E-4	6.3E-5	4.8E-6	-4.9E-6
458	0.010	-0.011	0.012	-0.012	-0.041	-0.074	2.0E-5	-3.4E-5	3.3E-4	5.2E-5	4.9E-6	-4.9E-6
459	0.010	-0.010	0.012	-0.012	-0.038	-0.074	1.1E-5	-4.3E-5	3.3E-4	3.6E-5	5.1E-6	-4.6E-6
460	0.010	-0.010	0.011	-0.012	-0.038	-0.077	1.8E-5	-3.3E-5	-3.2E-5	-3.5E-4	4.7E-6	-5.1E-6
461	0.011	-0.010	0.011	-0.012	-0.041	-0.076	2.1E-5	-2.9E-5	-4.9E-5	-3.4E-4	4.9E-6	-4.9E-6
462	0.011	-0.010	0.011	-0.012	-0.041	-0.075	3.6E-5	-2.1E-5	-6.2E-5	-3.2E-4	4.9E-6	-4.7E-6
463	0.011	-0.010	0.011	-0.012	-0.040	-0.073	4.5E-5	-9.2E-6	-6.9E-5	-2.8E-4	5.2E-6	-4.6E-6
464	0.011	-0.010	0.011	-0.012	-0.039	-0.068	5.6E-5	-9.1E-7	-6.0E-5	-2.2E-4	5.6E-6	-4.1E-6
465	0.011	-0.011	0.011	-0.012	-0.036	-0.063	4.6E-5	-1.6E-5	-2.5E-5	-1.7E-4	5.8E-6	-3.8E-6
466	0.011	-0.011	0.011	-0.011	-0.035	-0.052	2.3E-5	-3.3E-5	-3.2E-6	-1.2E-4	5.7E-6	-3.9E-6
467	0.011	-0.011	0.011	-0.011	-0.030	-0.044	3.8E-6	-4.3E-5	-9.9E-7	-4.1E-5	4.9E-6	-4.3E-6
468	0.011	-0.011	0.011	-0.011	-0.032	-0.040	-6.3E-6	-4.4E-5	2.3E-5	-2.4E-5	4.7E-6	-4.4E-6
469	0.011	-0.011	0.011	-0.011	-0.035	-0.040	-6.3E-6	-4.7E-5	1.8E-5	-8.3E-6	4.7E-6	-4.5E-6
470	0.011	-0.011	0.011	-0.011	-0.035	-0.040	-2.2E-6	-4.9E-5	1.6E-5	-1.2E-5	4.5E-6	-4.4E-6
471	0.011	-0.011	0.011	-0.011	-0.035	-0.040	4.5E-6	-5.1E-5	6.8E-6	-8.1E-6	4.5E-6	-4.4E-6
472	0.011	-0.011	0.011	-0.011	-0.035	-0.040	9.7E-6	-5.6E-5	7.9E-6	-6.0E-6	4.6E-6	-4.6E-6
473	0.011	-0.011	0.011	-0.011	-0.035	-0.040	1.2E-5	-6.0E-5	1.4E-5	-1.5E-5	4.5E-6	-4.6E-6
474	0.011	-0.011	0.011	-0.011	-0.033	-0.040	1.6E-5	-6.5E-5	3.7E-6	-1.1E-5	4.6E-6	-4.6E-6
475	0.011	-0.011	0.011	-0.011	-0.033	-0.040	2.3E-5	-7.3E-5	1.3E-5	-2.0E-5	4.7E-6	-4.8E-6
476	0.011	-0.011	0.012	-0.012	-0.030	-0.041	3.3E-5	-8.2E-5	2.3E-5	-2.1E-5	4.7E-6	-4.9E-6
477	0.011	-0.011	0.012	-0.012	-0.027	-0.047	5.4E-5	-9.2E-5	6.4E-5	-2.3E-5	4.6E-6	-5.2E-6
478	0.011	-0.011	0.012	-0.012	-0.024	-0.062	1.1E-4	-1.2E-4	1.7E-4	-5.2E-5	4.7E-6	-6.3E-6
479	0.010	-0.010	0.011	-0.011	-0.030	-0.035	1.0E-5	9.0E-6	1.9E-6	-4.4E-6	3.0E-7	-3.0E-7
480	0.010	-0.010	0.011	-0.011	-0.031	-0.036	1.0E-5	8.7E-6	2.2E-6	-4.5E-6	7.7E-7	-7.7E-7
481	0.010	-0.010	0.011	-0.011	-0.032	-0.037	7.3E-6	6.2E-6	2.3E-6	-4.6E-6	9.9E-7	-9.9E-7
482	0.010	-0.010	0.011	-0.011	-0.032	-0.037	4.1E-6	3.3E-6	2.3E-6	-4.7E-6	9.6E-8	-9.6E-8
483	0.010	-0.010	0.011	-0.011	-0.033	-0.038	1.7E-6	1.3E-6	2.4E-6	-4.7E-6	6.9E-7	-6.9E-7
484	0.010	-0.010	0.011	-0.011	-0.033	-0.038	2.1E-7	-2.3E-7	2.2E-6	-4.6E-6	6.5E-8	-6.5E-8
485	0.010	-0.010	0.011	-0.011	-0.033	-0.038	-1.2E-6	-1.7E-6	2.1E-6	-4.5E-6	5.0E-7	-5.0E-7
486	0.010	-0.010	0.011	-0.011	-0.032	-0.037	-3.3E-6	-4.1E-6	2.0E-6	-4.5E-6	6.8E-7	-6.8E-7
487	0.010	-0.010	0.011	-0.011	-0.032	-0.037	-6.1E-6	-7.4E-6	2.0E-6	-4.6E-6	1.0E-7	-1.0E-7
488	0.010	-0.010	0.011	-0.011	-0.031	-0.036	-8.7E-6	-1.0E-5	2.1E-6	-4.6E-6	8.4E-7	-8.4E-7
489	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-8.3E-6	-9.8E-6	2.1E-6	-4.5E-6	1.8E-7	-1.8E-7
490	0.009	-0.010	0.012	-0.012	-0.036	-0.053	1.6E-5	-1.4E-5	2.6E-4	1.3E-5	2.1E-7	-2.1E-7
491	0.009	-0.010	0.012	-0.012	-0.027	-0.044	9.3E-6	-9.6E-6	1.3E-4	1.8E-5	1.2E-6	-1.2E-6
492	0.009	-0.010	0.012	-0.012	-0.023	-0.038	6.3E-6	-7.5E-6	5.5E-5	5.0E-6	7.4E-7	-7.4E-7
493	0.009	-0.010	0.012	-0.012	-0.024	-0.035	3.8E-6	-5.0E-6	3.3E-5	-2.6E-5	8.6E-7	-8.6E-7
494	0.009	-0.010	0.011	-0.011	-0.026	-0.034	2.1E-6	-3.2E-6	1.6E-5	-3.4E-5	5.7E-7	-5.7E-7
495	0.009	-0.010	0.011	-0.011	-0.029	-0.035	1.1E-6	-1.8E-6	5.6E-6	-2.8E-5	6.5E-7	-6.5E-7
496	0.009	-0.010	0.011	-0.011	-0.030	-0.036	7.4E-7	-1.1E-6	-5.6E-7	-1.9E-5	1.1E-6	-1.1E-6
497	0.009	-0.010	0.011	-0.011	-0.032	-0.037	5.9E-7	-7.5E-7	-2.0E-6	-1.1E-5	1.3E-6	-1.3E-6
498	0.009	-0.010	0.011	-0.011	-0.032	-0.037	3.7E-7	-4.3E-7	-1.3E-6	-6.1E-6	7.3E-7	-7.3E-7
499	0.010	-0.010	0.011	-0.011	-0.026	-0.032	1.1E-5	4.4E-6	6.7E-6	-2.6E-5	8.0E-7	-8.0E-7
500	0.010	-0.010	0.011	-0.011	-0.026	-0.033	1.2E-5	5.4E-6	8.5E-6	-2.8E-5	8.2E-7	-8.2E-7
501	0.010	-0.010	0.011	-0.011	-0.026	-0.033	1.0E-5	4.0E-6	1.1E-5	-2.9E-5	9.3E-7	-9.3E-7
502	0.010	-0.010	0.011	-0.011	-0.027	-0.034	7.6E-6	1.7E-6	1.3E-5	-3.1E-5	4.0E-7	-4.0E-7
503	0.010	-0.010	0.011	-0.011	-0.027	-0.034	5.1E-6	-2.5E-7	1.4E-5	-3.2E-5	1.0E-6	-1.0E-6
504	0.009	-0.010	0.011	-0.011	-0.026	-0.034	3.4E-6	-1.9E-6	1.6E-5	-3.3E-5	4.5E-7	-4.5E-7
505	0.010	-0.010	0.012	-0.012	-0.034	-0.056	2.8E-5	-1.3E-5	2.7E-4	8.9E-6	7.3E-7	-7.3E-7
506	0.010	-0.010	0.012	-0.012	-0.028	-0.045	2.0E-5	-8.0E-6	1.6E-4	1.4E-5	9.9E-7	-9.9E-7
507	0.010	-0.010	0.012	-0.012	-0.023	-0.039	1.6E-5	-5.4E-6	7.7E-5	1.1E-5	7.1E-7	-7.1E-7
508	0.010	-0.010	0.012	-0.012	-0.023	-0.036	1.3E-5	-2.8E-6	4.3E-5	-1.3E-5	5.9E-7	-5.9E-7
509	0.010	-0.010	0.012	-0.012	-0.024	-0.033	9.7E-6	-3.3E-7	2.6E-5	-2.9E-5	3.9E-7	-3.9E-7
510	0.010	-0.010	0.012	-0.012	-0.022	-0.033	1.7E-5	-3.2E-6	4.1E-5	-7.1E-6	1.5E-7	-1.5E-7
511	0.010	-0.010	0.012	-0.012	-0.022	-0.034	1.8E-5	-8.8E-7	4.2E-5	-8.2E-6	8.9E-7	-8.9E-7
512	0.010	-0.010	0.012	-0.012	-0.023	-0.035	1.5E-5	-1.4E-6	4.3E-5	-1.1E-5	1.9E-7	-1.9E-7
513	0.010	-0.010	0.012	-0.012	-0.033	-0.055	2.8E-5	-7.8E-6	2.6E-4	1.5E-5	6.0E-7	-6.0E-7
514	0.010	-0.010	0.012	-0.012	-0.028	-0.043	2.5E-5	-7.3E-6	1.6E-4	1.7E-5	2.6E-7	-2.6E-7
515	0.010	-0.010	0.012	-0.012	-0.023	-0.038	2.1E-5	-4.3E-6	7.9E-5	1.2E-5	1.4E-6	-1.4E-6
516	0.010	-0.010	0.012	-0.012	-0.033	-0.049	2.6E-5	-1.8E-5	2.2E-4	2.8E-5	4.2E-7	-4.2E-7
517	0.010	-0.010	0.012	-0.012	-0.033	-0.052	2.9E-5	-1.3E-5	2.5E-4	1.8E-5	5.4E-7	-5.4E-7
518	0.010	-0.010	0.011	-0.011	-0.033	-0.049	1.3E-5	-2.6E-5	-2.2E-5	-2.5E-4	6.9E-7	-6.9E-7
519	0.010	-0.010	0.011	-0.011	-0.023	-0.040	9.0E-6	-2.2E-5	-2.2E-5	-1.1E-4	1.3E-6	-1.3E-6
520	0.010	-0.010	0.011	-0.011	-0.021	-0.034	4.7E-6	-1.7E-5	6.3E-6	-4.6E-5	1.2E-6	-1.2E-6
521	0.010	-0.010	0.011	-0.011	-0.023	-0.031	-6.6E-1	-1.3E-5	3.0E-5	-2.3E-5	9.1E-7	-9.1E-7
522	0.010	-0.010	0.011	-0.011	-0.025	-0.032	-3.7E-6	-1.0E-5	3.0E-5	-8.0E-6	6.5E-7	-6.5E-7
523	0.010	-0.010	0.011	-0.011	-0.027	-0.033	-6.1E-6	-8.8E-6	2.0E-5	2.7E-7	8.6E-7	-8.6E-7
524	0.010	-0.010	0.011	-0.011	-0.029	-0.034	-7.2E-6	-9.0E-6	1.2E-5	2.3E-6	7.3E-7	-7.3E-7
525	0.010	-0.010	0.011	-0.011	-0.030	-0.034	-7.7E-6	-9.4E-6	6.0E-6	1.5E-6	2.9E-7	-2.9E-7

526	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-8.2E-6	-9.7E-6	4.4E-6	-2.2E-6	3.8E-7	-3.8E-7
527	0.010	-0.010	0.011	-0.011	-0.034	-0.050	1.0E-5	-2.8E-5	-2.4E-5	-2.4E-4	2.9E-7	-2.9E-7
528	0.010	-0.010	0.011	-0.011	-0.024	-0.041	7.0E-6	-2.4E-5	-2.0E-5	-1.1E-4	6.6E-7	-6.6E-7
529	0.010	-0.010	0.011	-0.011	-0.021	-0.035	2.3E-6	-1.9E-5	8.9E-6	-4.9E-5	1.2E-6	-1.2E-6
530	0.010	-0.010	0.011	-0.011	-0.023	-0.032	-2.0E-6	-1.4E-5	3.1E-5	-2.5E-5	4.7E-7	-4.7E-7
531	0.010	-0.010	0.011	-0.011	-0.026	-0.033	-5.4E-6	-1.1E-5	3.1E-5	-9.1E-6	8.3E-7	-8.3E-7
532	0.010	-0.010	0.011	-0.011	-0.028	-0.034	-7.4E-6	-1.0E-5	2.2E-5	-3.6E-7	2.3E-7	-2.3E-7
533	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-8.2E-6	-1.0E-5	1.2E-5	2.2E-6	7.9E-7	-7.9E-7
534	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-8.6E-6	-1.0E-5	6.3E-6	1.5E-6	5.6E-7	-5.6E-7
535	0.010	-0.010	0.011	-0.011	-0.031	-0.036	-8.7E-6	-1.0E-5	4.6E-6	-2.2E-6	9.2E-7	-9.2E-7
536	0.010	-0.010	0.011	-0.011	-0.034	-0.051	8.6E-6	-2.6E-5	-1.6E-5	-2.6E-4	1.3E-6	-1.3E-6
537	0.010	-0.010	0.011	-0.011	-0.024	-0.042	5.7E-6	-2.1E-5	-2.0E-5	-1.1E-4	8.2E-7	-8.2E-7
538	0.010	-0.010	0.011	-0.011	-0.021	-0.036	2.1E-6	-1.7E-5	8.6E-6	-5.0E-5	6.7E-7	-6.7E-7
539	0.010	-0.010	0.011	-0.011	-0.023	-0.033	-1.9E-6	-1.3E-5	3.3E-5	-2.6E-5	3.1E-7	-3.1E-7
540	0.010	-0.010	0.011	-0.011	-0.026	-0.033	-4.6E-6	-9.6E-6	3.2E-5	-9.9E-6	1.1E-6	-1.1E-6
541	0.010	-0.010	0.011	-0.011	-0.029	-0.035	-5.9E-6	-8.2E-6	2.3E-5	-8.7E-7	9.1E-7	-9.1E-7
542	0.010	-0.010	0.011	-0.011	-0.030	-0.036	-6.3E-6	-8.1E-6	1.3E-5	2.1E-6	7.8E-7	-7.8E-7
543	0.010	-0.010	0.011	-0.011	-0.031	-0.036	-6.4E-6	-7.9E-6	6.6E-6	1.5E-6	7.6E-7	-7.6E-7
544	0.010	-0.010	0.011	-0.011	-0.032	-0.037	-6.3E-6	-7.7E-6	4.6E-6	-2.2E-6	9.4E-7	-9.4E-7
545	0.010	-0.010	0.011	-0.011	-0.034	-0.051	6.4E-6	-2.0E-5	-1.9E-5	-2.5E-4	8.7E-7	-8.7E-7
546	0.010	-0.010	0.011	-0.011	-0.024	-0.043	5.9E-6	-1.8E-5	-1.8E-5	-1.2E-4	5.5E-7	-5.5E-7
547	0.010	-0.010	0.011	-0.011	-0.021	-0.037	2.2E-6	-1.3E-5	1.1E-5	-5.2E-5	2.4E-7	-2.4E-7
548	0.010	-0.010	0.011	-0.011	-0.024	-0.033	-6.0E-7	-9.7E-6	3.4E-5	-2.7E-5	1.2E-7	-1.2E-7
549	0.010	-0.010	0.011	-0.011	-0.027	-0.034	-2.8E-6	-7.1E-6	3.3E-5	-1.1E-5	9.2E-7	-9.2E-7
550	0.010	-0.010	0.011	-0.011	-0.029	-0.035	-3.7E-6	-5.7E-6	2.3E-5	-1.2E-6	5.8E-7	-5.8E-7
551	0.010	-0.010	0.011	-0.011	-0.031	-0.036	-3.8E-6	-5.2E-6	1.3E-5	2.1E-6	1.1E-7	-1.1E-7
552	0.010	-0.010	0.011	-0.011	-0.032	-0.037	-3.7E-6	-4.9E-6	6.7E-6	1.6E-6	9.6E-7	-9.6E-7
553	0.010	-0.010	0.011	-0.011	-0.032	-0.037	-3.6E-6	-4.5E-6	4.6E-6	-2.1E-6	9.0E-7	-9.0E-7
554	0.010	-0.009	0.011	-0.011	-0.035	-0.052	9.8E-6	-1.8E-5	-1.1E-5	-2.7E-4	2.9E-7	-2.9E-7
555	0.010	-0.009	0.011	-0.011	-0.024	-0.043	6.2E-6	-1.4E-5	-1.9E-5	-1.1E-4	6.9E-7	-6.9E-7
556	0.010	-0.009	0.011	-0.011	-0.022	-0.037	3.8E-6	-1.1E-5	1.0E-5	-5.1E-5	6.4E-7	-6.4E-7
557	0.010	-0.009	0.011	-0.011	-0.024	-0.034	7.4E-7	-7.1E-6	3.5E-5	-2.8E-5	8.6E-7	-8.6E-7
558	0.010	-0.009	0.011	-0.011	-0.027	-0.034	-1.0E-6	-4.8E-6	3.4E-5	-1.1E-5	3.1E-7	-3.1E-7
559	0.010	-0.009	0.011	-0.011	-0.029	-0.036	-1.7E-6	-3.5E-6	2.4E-5	-1.3E-6	2.6E-7	-2.6E-7
560	0.010	-0.009	0.011	-0.011	-0.031	-0.037	-1.7E-6	-3.0E-6	1.3E-5	2.1E-6	9.1E-7	-9.1E-7
561	0.010	-0.010	0.011	-0.011	-0.032	-0.037	-1.6E-6	-2.5E-6	6.8E-6	1.6E-6	5.1E-7	-5.1E-7
562	0.010	-0.010	0.011	-0.011	-0.032	-0.037	-1.5E-6	-2.1E-6	4.7E-6	-2.1E-6	4.6E-7	-4.6E-7
563	0.010	-0.009	0.011	-0.011	-0.035	-0.052	1.1E-5	-1.7E-5	-1.6E-5	-2.5E-4	4.0E-7	-4.0E-7
564	0.010	-0.009	0.011	-0.011	-0.024	-0.044	8.0E-6	-1.2E-5	-1.7E-5	-1.2E-4	1.7E-7	-1.7E-7
565	0.010	-0.009	0.011	-0.011	-0.022	-0.038	4.3E-6	-8.0E-6	1.2E-5	-5.2E-5	3.5E-7	-3.5E-7
566	0.010	-0.009	0.011	-0.011	-0.024	-0.034	2.0E-6	-5.1E-6	3.5E-5	-2.8E-5	6.4E-7	-6.4E-7
567	0.010	-0.009	0.011	-0.011	-0.027	-0.034	3.0E-7	-3.0E-6	3.4E-5	-1.1E-5	3.3E-7	-3.3E-7
568	0.010	-0.009	0.011	-0.011	-0.030	-0.036	-3.0E-7	-1.8E-6	2.4E-5	-1.3E-6	5.5E-7	-5.5E-7
569	0.010	-0.009	0.011	-0.011	-0.031	-0.037	-1.9E-7	-1.4E-6	1.3E-5	2.1E-6	1.3E-7	-1.3E-7
570	0.010	-0.009	0.011	-0.011	-0.032	-0.037	-5.1E-8	-1.0E-6	6.8E-6	1.6E-6	1.8E-7	-1.8E-7
571	0.010	-0.009	0.011	-0.011	-0.033	-0.038	-3.4E-9	-5.1E-7	4.7E-6	-2.1E-6	2.9E-7	-2.9E-7
572	0.010	-0.009	0.011	-0.011	-0.035	-0.053	1.3E-5	-1.5E-5	-9.6E-6	-2.7E-4	4.4E-7	-4.4E-7
573	0.010	-0.009	0.011	-0.011	-0.024	-0.044	8.4E-6	-1.0E-5	-1.8E-5	-1.1E-4	3.8E-7	-3.8E-7
574	0.010	-0.009	0.011	-0.011	-0.022	-0.038	5.2E-6	-6.4E-6	1.1E-5	-5.2E-5	8.6E-7	-8.6E-7
575	0.010	-0.009	0.011	-0.011	-0.024	-0.034	2.6E-6	-3.4E-6	3.6E-5	-2.8E-5	7.7E-7	-7.7E-7
576	0.010	-0.009	0.011	-0.011	-0.027	-0.035	1.3E-6	-1.6E-6	3.4E-5	-1.1E-5	9.2E-7	-9.2E-7
577	0.010	-0.009	0.011	-0.011	-0.030	-0.036	9.3E-7	-7.1E-7	2.4E-5	-1.4E-6	7.8E-7	-7.8E-7
578	0.010	-0.009	0.011	-0.011	-0.031	-0.037	1.0E-6	-2.0E-7	1.3E-5	2.2E-6	1.4E-7	-1.4E-7
579	0.010	-0.010	0.011	-0.011	-0.032	-0.037	1.2E-6	3.1E-7	6.9E-6	1.5E-6	2.2E-7	-2.2E-7
580	0.010	-0.010	0.011	-0.011	-0.032	-0.038	1.3E-6	8.7E-7	4.8E-6	-2.2E-6	2.8E-7	-2.8E-7
581	0.010	-0.009	0.011	-0.011	-0.035	-0.053	1.2E-5	-1.4E-5	-1.4E-5	-2.5E-4	5.2E-7	-5.2E-7
582	0.010	-0.009	0.011	-0.011	-0.024	-0.044	8.9E-6	-8.7E-6	-1.6E-5	-1.2E-4	1.3E-6	-1.3E-6
583	0.010	-0.009	0.011	-0.011	-0.022	-0.038	5.7E-6	-5.3E-6	1.3E-5	-5.3E-5	1.8E-7	-1.8E-7
584	0.010	-0.009	0.011	-0.011	-0.024	-0.034	3.8E-6	-2.7E-6	3.6E-5	-2.8E-5	1.1E-6	-1.1E-6
585	0.010	-0.009	0.011	-0.011	-0.027	-0.035	2.8E-6	-1.1E-6	3.5E-5	-1.1E-5	1.0E-6	-1.0E-6
586	0.010	-0.009	0.011	-0.011	-0.030	-0.036	2.2E-6	2.9E-7	2.4E-5	-1.3E-6	6.5E-8	-6.5E-8
587	0.010	-0.010	0.011	-0.011	-0.031	-0.037	2.4E-6	1.1E-6	1.3E-5	2.2E-6	3.0E-7	-3.0E-7
588	0.010	-0.010	0.011	-0.011	-0.032	-0.037	2.7E-6	1.9E-6	6.9E-6	1.4E-6	4.6E-7	-4.6E-7
589	0.010	-0.010	0.011	-0.011	-0.032	-0.037	3.4E-6	2.7E-6	4.8E-6	-2.3E-6	3.7E-7	-3.7E-7
590	0.010	-0.010	0.011	-0.011	-0.033	-0.050	1.9E-5	-5.0E-6	-2.7E-5	-2.5E-4	2.6E-7	-2.6E-7
591	0.010	-0.010	0.011	-0.011	-0.033	-0.050	2.1E-5	-3.3E-6	-2.7E-5	-2.4E-4	6.5E-7	-6.5E-7
592	0.010	-0.010	0.011	-0.011	-0.033	-0.051	2.0E-5	-2.6E-6	-1.9E-5	-2.6E-4	1.3E-6	-1.3E-6
593	0.010	-0.010	0.011	-0.011	-0.034	-0.052	1.8E-5	-4.9E-6	-2.0E-5	-2.5E-4	1.1E-6	-1.1E-6
594	0.010	-0.010	0.011	-0.011	-0.034	-0.053	1.6E-5	-6.4E-6	-1.2E-5	-2.7E-4	7.9E-7	-7.9E-7
595	0.010	-0.010	0.011	-0.011	-0.034	-0.053	1.5E-5	-9.2E-6	-1.5E-5	-2.5E-4	1.2E-6	-1.2E-6
596	0.010	-0.009	0.011	-0.011	-0.034	-0.053	1.5E-5	-1.0E-5	-8.1E-6	-2.7E-4	7.1E-7	-7.1E-7
597	0.010	-0.009	0.011	-0.011	-0.035	-0.053	1.3E-5	-1.1E-5	-1.4E-5	-2.5E-4	2.2E-7	-2.2E-7

598	0.010	-0.009	0.011	-0.011	-0.035	-0.053	1.3E-5	-1.2E-5	-8.1E-6	-2.7E-4	9.3E-7	-9.3E-7
599	0.010	-0.009	0.011	-0.011	-0.024	-0.044	9.3E-6	-8.3E-6	-1.8E-5	-1.1E-4	2.0E-7	-2.0E-7
600	0.010	-0.009	0.011	-0.011	-0.022	-0.038	7.3E-6	-5.1E-6	1.2E-5	-5.2E-5	6.4E-7	-6.4E-7
601	0.010	-0.009	0.011	-0.011	-0.024	-0.034	5.6E-6	-2.5E-6	3.6E-5	-2.9E-5	4.4E-7	-4.4E-7
602	0.010	-0.010	0.011	-0.011	-0.027	-0.034	4.3E-6	-1.8E-7	3.4E-5	-1.1E-5	6.2E-7	-6.2E-7
603	0.010	-0.010	0.011	-0.011	-0.029	-0.036	3.8E-6	1.6E-6	2.3E-5	-1.1E-6	6.1E-7	-6.1E-7
604	0.010	-0.010	0.011	-0.011	-0.031	-0.036	4.1E-6	2.9E-6	1.3E-5	2.1E-6	5.0E-7	-5.0E-7
605	0.010	-0.010	0.011	-0.011	-0.032	-0.037	5.1E-6	4.0E-6	6.8E-6	1.3E-6	4.7E-7	-4.7E-7
606	0.010	-0.010	0.011	-0.011	-0.032	-0.037	6.2E-6	5.1E-6	4.8E-6	-2.3E-6	7.1E-7	-7.1E-7
607	0.010	-0.010	0.011	-0.011	-0.024	-0.039	1.8E-5	-6.1E-6	-2.2E-5	-1.1E-4	5.1E-7	-5.1E-7
608	0.010	-0.010	0.011	-0.011	-0.023	-0.040	2.1E-5	-4.3E-6	-1.9E-5	-1.2E-4	4.5E-7	-4.5E-7
609	0.010	-0.010	0.011	-0.011	-0.023	-0.041	2.0E-5	-4.2E-6	-1.9E-5	-1.1E-4	3.0E-7	-3.0E-7
610	0.010	-0.010	0.011	-0.011	-0.023	-0.042	1.8E-5	-4.3E-6	-1.7E-5	-1.2E-4	6.3E-7	-6.3E-7
611	0.010	-0.010	0.011	-0.011	-0.023	-0.043	1.6E-5	-5.9E-6	-1.7E-5	-1.2E-4	6.7E-7	-6.7E-7
612	0.010	-0.010	0.011	-0.011	-0.024	-0.044	1.4E-5	-6.6E-6	-1.6E-5	-1.2E-4	6.3E-7	-6.3E-7
613	0.010	-0.010	0.011	-0.011	-0.024	-0.044	1.3E-5	-8.5E-6	-1.7E-5	-1.2E-4	9.1E-7	-9.1E-7
614	0.010	-0.009	0.011	-0.011	-0.024	-0.044	1.1E-5	-7.8E-6	-1.6E-5	-1.2E-4	8.1E-7	-8.1E-7
615	0.010	-0.009	0.011	-0.011	-0.022	-0.038	9.3E-6	-5.3E-6	1.4E-5	-5.4E-5	7.6E-7	-7.6E-7
616	0.010	-0.010	0.011	-0.011	-0.024	-0.034	7.2E-6	-1.8E-6	3.6E-5	-2.8E-5	8.7E-7	-8.7E-7
617	0.010	-0.010	0.011	-0.011	-0.027	-0.034	6.1E-6	1.0E-6	3.4E-5	-1.1E-5	4.7E-7	-4.7E-7
618	0.010	-0.010	0.011	-0.011	-0.029	-0.035	5.8E-6	3.2E-6	2.3E-5	-7.2E-7	5.8E-7	-5.8E-7
619	0.010	-0.010	0.011	-0.011	-0.031	-0.036	6.6E-6	5.0E-6	1.3E-5	2.2E-6	2.9E-7	-2.9E-7
620	0.010	-0.010	0.011	-0.011	-0.031	-0.036	8.0E-6	6.5E-6	6.6E-6	1.2E-6	6.8E-7	-6.8E-7
621	0.010	-0.010	0.011	-0.011	-0.031	-0.036	9.3E-6	7.8E-6	4.7E-6	-2.3E-6	3.1E-7	-3.1E-7
622	0.010	-0.010	0.011	-0.011	-0.021	-0.033	1.4E-5	-3.7E-6	6.8E-6	-4.7E-5	1.0E-6	-1.0E-6
623	0.010	-0.010	0.011	-0.011	-0.021	-0.034	1.7E-5	-1.8E-6	9.4E-6	-5.0E-5	9.2E-7	-9.2E-7
624	0.010	-0.010	0.011	-0.011	-0.021	-0.035	1.7E-5	-1.1E-6	9.6E-6	-5.1E-5	8.5E-7	-8.5E-7
625	0.010	-0.010	0.011	-0.011	-0.021	-0.036	1.6E-5	-1.6E-6	1.2E-5	-5.3E-5	1.0E-6	-1.0E-6
626	0.010	-0.010	0.011	-0.011	-0.021	-0.036	1.4E-5	-2.3E-6	1.2E-5	-5.3E-5	3.5E-7	-3.5E-7
627	0.010	-0.010	0.011	-0.011	-0.021	-0.037	1.3E-5	-3.5E-6	1.4E-5	-5.4E-5	1.1E-6	-1.1E-6
628	0.010	-0.010	0.011	-0.011	-0.022	-0.037	1.1E-5	-4.2E-6	1.3E-5	-5.3E-5	4.0E-7	-4.0E-7
629	0.010	-0.010	0.011	-0.011	-0.024	-0.033	9.0E-6	-8.2E-7	3.6E-5	-2.8E-5	1.6E-7	-1.6E-7
630	0.010	-0.010	0.011	-0.011	-0.027	-0.034	8.0E-6	2.3E-6	3.3E-5	-1.0E-5	4.1E-7	-4.1E-7
631	0.010	-0.010	0.011	-0.011	-0.029	-0.035	7.8E-6	5.0E-6	2.2E-5	-2.7E-7	1.2E-7	-1.2E-7
632	0.010	-0.010	0.011	-0.011	-0.030	-0.035	8.9E-6	6.9E-6	1.2E-5	2.2E-6	4.5E-7	-4.5E-7
633	0.010	-0.010	0.011	-0.011	-0.030	-0.035	1.0E-5	8.3E-6	6.3E-6	1.1E-6	2.3E-7	-2.3E-7
634	0.010	-0.010	0.011	-0.011	-0.030	-0.035	1.0E-5	8.9E-6	4.6E-6	-2.2E-6	1.4E-7	-1.4E-7
635	0.010	-0.010	0.011	-0.011	-0.023	-0.031	1.1E-5	-8.5E-7	2.8E-5	-2.3E-5	1.1E-6	-1.1E-6
636	0.010	-0.010	0.011	-0.011	-0.023	-0.031	1.3E-5	1.4E-6	2.9E-5	-2.5E-5	1.2E-6	-1.2E-6
637	0.010	-0.010	0.011	-0.011	-0.023	-0.032	1.4E-5	2.1E-6	3.1E-5	-2.6E-5	7.7E-7	-7.7E-7
638	0.010	-0.010	0.011	-0.011	-0.023	-0.032	1.4E-5	2.0E-6	3.2E-5	-2.6E-5	1.4E-6	-1.4E-6
639	0.010	-0.010	0.011	-0.011	-0.024	-0.032	1.2E-5	1.2E-6	3.4E-5	-2.7E-5	1.0E-6	-1.0E-6
640	0.010	-0.010	0.011	-0.011	-0.024	-0.033	1.1E-5	3.1E-7	3.5E-5	-2.8E-5	7.0E-7	-7.0E-7
641	0.010	-0.010	0.011	-0.011	-0.027	-0.033	9.6E-6	3.6E-6	3.3E-5	-9.7E-6	1.2E-6	-1.2E-6
642	0.010	-0.010	0.011	-0.011	-0.028	-0.034	9.3E-6	6.3E-6	2.2E-5	-2.9E-8	1.1E-6	-1.1E-6
643	0.010	-0.010	0.011	-0.011	-0.029	-0.035	1.0E-5	7.9E-6	1.2E-5	2.2E-6	2.7E-7	-2.7E-7
644	0.010	-0.010	0.011	-0.011	-0.030	-0.035	1.0E-5	8.3E-6	6.7E-6	1.4E-6	7.5E-7	-7.5E-7
645	0.010	-0.010	0.011	-0.011	-0.030	-0.035	8.7E-6	7.3E-6	4.5E-6	-1.8E-6	5.6E-7	-5.6E-7
646	0.010	-0.010	0.011	-0.011	-0.029	-0.034	6.9E-6	5.7E-6	5.3E-6	5.8E-7	7.1E-7	-7.1E-7
647	0.010	-0.010	0.011	-0.011	-0.029	-0.034	6.2E-6	5.0E-6	9.0E-6	2.1E-6	1.0E-6	-1.0E-6
648	0.010	-0.010	0.011	-0.011	-0.028	-0.033	6.3E-6	4.4E-6	1.4E-5	2.5E-6	4.5E-7	-4.5E-7
649	0.010	-0.010	0.011	-0.011	-0.027	-0.032	6.8E-6	3.5E-6	2.2E-5	-2.7E-7	5.4E-7	-5.4E-7
650	0.010	-0.010	0.011	-0.011	-0.025	-0.031	8.0E-6	1.7E-6	2.9E-5	-8.1E-6	7.2E-7	-7.2E-7
651	0.010	-0.010	0.011	-0.011	-0.025	-0.032	1.1E-5	3.8E-6	3.0E-5	-1.0E-5	1.6E-6	-1.6E-6
652	0.010	-0.010	0.011	-0.011	-0.025	-0.032	1.2E-5	4.6E-6	3.1E-5	-1.1E-5	3.8E-7	-3.8E-7
653	0.010	-0.010	0.011	-0.011	-0.026	-0.033	1.2E-5	4.7E-6	3.2E-5	-1.1E-5	6.4E-7	-6.4E-7
654	0.010	-0.010	0.011	-0.011	-0.026	-0.033	1.1E-5	4.3E-6	3.2E-5	-1.0E-5	6.0E-7	-6.0E-7
655	0.010	-0.010	0.011	-0.011	-0.028	-0.034	1.0E-5	6.6E-6	2.3E-5	-1.1E-6	4.8E-7	-4.8E-7
656	0.010	-0.010	0.011	-0.011	-0.029	-0.034	1.0E-5	7.7E-6	1.5E-5	2.2E-6	1.3E-6	-1.3E-6
657	0.010	-0.010	0.011	-0.011	-0.029	-0.034	9.5E-6	7.7E-6	9.2E-6	2.0E-6	8.7E-7	-8.7E-7
658	0.010	-0.010	0.011	-0.011	-0.029	-0.034	8.8E-6	6.9E-6	1.3E-5	2.3E-6	6.3E-7	-6.3E-7
659	0.010	-0.010	0.011	-0.011	-0.028	-0.033	8.6E-6	6.1E-6	1.7E-5	1.7E-6	1.5E-6	-1.5E-6
660	0.010	-0.010	0.011	-0.011	-0.027	-0.033	9.2E-6	5.2E-6	2.4E-5	-1.8E-6	1.7E-6	-1.7E-6
661	0.010	-0.010	0.011	-0.011	-0.027	-0.033	1.0E-5	6.0E-6	2.6E-5	-3.2E-6	1.7E-7	-1.7E-7
662	0.010	-0.010	0.011	-0.011	-0.027	-0.033	1.0E-5	6.4E-6	2.5E-5	-2.5E-6	6.3E-7	-6.3E-7
663	0.010	-0.010	0.011	-0.011	-0.028	-0.034	9.7E-6	7.2E-6	1.8E-5	1.6E-6	1.5E-6	-1.5E-6
664	0.010	-0.010	0.011	-0.011	-0.028	-0.033	9.6E-6	6.6E-6	2.0E-5	6.2E-7	1.2E-6	-1.2E-6
665	0.009	-0.010	0.011	-0.011	-0.032	-0.037	-1.1E-6	-1.9E-6	-1.5E-6	-6.1E-6	6.1E-7	-6.1E-7
666	0.010	-0.010	0.011	-0.011	-0.032	-0.037	-3.2E-6	-4.1E-6	-1.5E-6	-6.2E-6	7.0E-8	-7.0E-8
667	0.010	-0.010	0.011	-0.011	-0.031	-0.036	-5.9E-6	-7.4E-6	-1.5E-6	-6.4E-6	3.6E-7	-3.6E-7
668	0.010	-0.010	0.011	-0.011	-0.031	-0.036	-8.4E-6	-1.0E-5	-1.6E-6	-6.4E-6	3.3E-7	-3.3E-7
669	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-8.1E-6	-9.8E-6	-1.6E-6	-6.4E-6	2.2E-7	-2.2E-7

670	0.009	-0.010	0.012	-0.012	-0.036	-0.053	1.4E-5	-1.4E-5	2.8E-4	7.2E-6	1.1E-6	-1.1E-6
671	0.009	-0.010	0.012	-0.012	-0.026	-0.044	8.2E-6	-9.7E-6	1.3E-4	2.0E-5	3.8E-7	-3.8E-7
672	0.009	-0.010	0.012	-0.012	-0.023	-0.039	5.1E-6	-8.0E-6	5.5E-5	6.1E-6	6.7E-7	-6.7E-7
673	0.009	-0.010	0.012	-0.012	-0.023	-0.035	2.4E-6	-5.8E-6	3.3E-5	-2.6E-5	3.5E-7	-3.5E-7
674	0.009	-0.010	0.011	-0.011	-0.026	-0.034	6.4E-7	-4.1E-6	1.7E-5	-3.4E-5	4.4E-7	-4.4E-7
675	0.009	-0.010	0.011	-0.011	-0.028	-0.035	-3.8E-7	-3.0E-6	5.7E-6	-2.9E-5	6.0E-7	-6.0E-7
676	0.009	-0.010	0.011	-0.011	-0.030	-0.036	-6.7E-7	-2.5E-6	-4.6E-7	-1.9E-5	4.4E-7	-4.4E-7
677	0.009	-0.010	0.011	-0.011	-0.031	-0.037	-8.8E-7	-2.2E-6	-2.1E-6	-1.2E-5	6.2E-7	-6.2E-7
678	0.010	-0.010	0.011	-0.011	-0.031	-0.037	-2.9E-6	-4.3E-6	-2.0E-6	-1.2E-5	1.0E-6	-1.0E-6
679	0.010	-0.010	0.011	-0.011	-0.031	-0.036	-5.6E-6	-7.3E-6	-2.0E-6	-1.2E-5	1.1E-6	-1.1E-6
680	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-8.1E-6	-1.0E-5	-2.1E-6	-1.3E-5	6.9E-7	-6.9E-7
681	0.010	-0.010	0.011	-0.011	-0.029	-0.034	-7.7E-6	-9.7E-6	-2.2E-6	-1.3E-5	7.5E-7	-7.5E-7
682	0.009	-0.010	0.012	-0.012	-0.036	-0.053	1.5E-5	-1.5E-5	2.6E-4	1.3E-5	2.2E-7	-2.2E-7
683	0.009	-0.010	0.012	-0.012	-0.026	-0.044	7.8E-6	-1.1E-5	1.4E-4	1.8E-5	1.2E-6	-1.2E-6
684	0.009	-0.010	0.012	-0.012	-0.022	-0.038	3.9E-6	-8.9E-6	5.7E-5	6.5E-6	1.2E-6	-1.2E-6
685	0.009	-0.010	0.012	-0.012	-0.023	-0.035	7.9E-7	-6.9E-6	3.4E-5	-2.6E-5	4.1E-7	-4.1E-7
686	0.009	-0.010	0.011	-0.011	-0.026	-0.034	-1.2E-6	-5.5E-6	1.7E-5	-3.4E-5	3.7E-7	-3.7E-7
687	0.009	-0.010	0.011	-0.011	-0.028	-0.035	-2.3E-6	-4.7E-6	6.3E-6	-3.0E-5	9.2E-7	-9.2E-7
688	0.009	-0.010	0.011	-0.011	-0.030	-0.036	-2.6E-6	-4.5E-6	-1.5E-7	-2.0E-5	1.0E-6	-1.0E-6
689	0.010	-0.010	0.011	-0.011	-0.029	-0.035	-5.3E-6	-7.2E-6	6.0E-8	-2.1E-5	3.7E-7	-3.7E-7
690	0.010	-0.010	0.011	-0.011	-0.028	-0.034	-7.6E-6	-1.0E-5	8.8E-8	-2.1E-5	8.8E-7	-8.8E-7
691	0.010	-0.010	0.011	-0.011	-0.028	-0.033	-6.9E-6	-9.9E-6	2.4E-9	-2.2E-5	5.0E-7	-5.0E-7
692	0.009	-0.010	0.012	-0.012	-0.036	-0.054	1.5E-5	-1.6E-5	2.9E-4	6.1E-6	7.7E-7	-7.7E-7
693	0.009	-0.010	0.012	-0.012	-0.026	-0.044	7.2E-6	-1.2E-5	1.4E-4	2.0E-5	2.6E-7	-2.6E-7
694	0.009	-0.010	0.012	-0.012	-0.022	-0.038	2.6E-6	-1.1E-5	5.9E-5	8.8E-6	1.3E-6	-1.3E-6
695	0.009	-0.010	0.012	-0.012	-0.023	-0.035	-9.9E-7	-9.2E-6	3.6E-5	-2.5E-5	4.7E-7	-4.7E-7
696	0.010	-0.010	0.011	-0.011	-0.025	-0.033	-3.3E-6	-8.0E-6	1.9E-5	-3.5E-5	9.9E-7	-9.9E-7
697	0.010	-0.010	0.011	-0.011	-0.027	-0.034	-4.7E-6	-7.5E-6	6.8E-6	-3.0E-5	1.8E-7	-1.8E-7
698	0.010	-0.010	0.011	-0.011	-0.027	-0.033	-6.9E-6	-1.0E-5	7.2E-6	-3.1E-5	3.1E-7	-3.1E-7
699	0.010	-0.010	0.011	-0.011	-0.025	-0.032	-6.0E-6	-1.1E-5	7.6E-6	-3.1E-5	6.6E-7	-6.6E-7
700	0.009	-0.010	0.012	-0.012	-0.035	-0.054	1.7E-5	-1.7E-5	2.8E-4	1.3E-5	1.3E-6	-1.3E-6
701	0.009	-0.010	0.012	-0.012	-0.026	-0.044	6.1E-6	-1.4E-5	1.5E-4	1.9E-5	1.0E-6	-1.0E-6
702	0.010	-0.010	0.012	-0.012	-0.022	-0.038	5.3E-7	-1.3E-5	6.3E-5	1.1E-5	5.1E-7	-5.1E-7
703	0.010	-0.010	0.012	-0.012	-0.022	-0.034	-3.0E-6	-1.2E-5	3.8E-5	-2.3E-5	2.1E-7	-2.1E-7
704	0.010	-0.010	0.011	-0.011	-0.024	-0.032	-5.7E-6	-1.1E-5	2.0E-5	-3.4E-5	1.2E-7	-1.2E-7
705	0.010	-0.010	0.011	-0.011	-0.023	-0.031	-5.0E-6	-1.2E-5	2.2E-5	-3.4E-5	4.9E-7	-4.9E-7
706	0.010	-0.010	0.012	-0.012	-0.035	-0.056	1.7E-5	-1.8E-5	3.1E-4	7.5E-6	1.1E-6	-1.1E-6
707	0.010	-0.010	0.012	-0.012	-0.027	-0.044	5.1E-6	-1.5E-5	1.7E-4	2.2E-5	1.1E-6	-1.1E-6
708	0.010	-0.010	0.012	-0.012	-0.021	-0.038	-1.0E-6	-1.4E-5	7.5E-5	1.6E-5	5.5E-7	-5.5E-7
709	0.010	-0.010	0.012	-0.012	-0.021	-0.034	-4.1E-6	-1.4E-5	4.3E-5	-1.6E-5	3.0E-7	-3.0E-7
710	0.010	-0.010	0.012	-0.012	-0.035	-0.058	1.7E-5	-1.6E-5	3.1E-4	1.4E-5	9.0E-8	-9.0E-8
711	0.010	-0.010	0.012	-0.012	-0.028	-0.045	3.2E-6	-1.3E-5	1.9E-4	2.4E-5	2.1E-7	-2.1E-7
712	0.010	-0.010	0.012	-0.012	-0.022	-0.039	2.5E-6	-1.4E-5	1.0E-4	2.1E-5	7.6E-7	-7.6E-7
713	0.010	-0.010	0.012	-0.012	-0.027	-0.044	4.5E-6	-1.3E-5	1.8E-4	2.7E-5	1.2E-6	-1.2E-6
714	0.010	-0.010	0.012	-0.012	-0.035	-0.056	8.8E-6	-1.2E-5	3.1E-4	2.4E-5	1.5E-6	-1.5E-6
715	0.010	-0.010	0.012	-0.012	-0.035	-0.060	1.4E-5	-1.3E-5	3.5E-4	8.7E-6	1.5E-6	-1.5E-6
716	0.010	-0.010	0.012	-0.012	-0.031	-0.048	4.5E-6	-1.2E-5	2.3E-4	2.5E-5	1.6E-6	-1.6E-6
717	0.010	-0.010	0.011	-0.011	-0.028	-0.033	9.2E-6	6.4E-6	-9.1E-7	-1.8E-5	8.1E-7	-8.1E-7
718	0.010	-0.010	0.011	-0.011	-0.029	-0.034	9.4E-6	7.6E-6	-2.3E-6	-1.1E-5	8.9E-7	-8.9E-7
719	0.010	-0.010	0.011	-0.011	-0.030	-0.034	9.8E-6	8.3E-6	-1.3E-6	-5.9E-6	1.0E-6	-1.0E-6
720	0.010	-0.010	0.011	-0.011	-0.028	-0.034	1.0E-5	7.3E-6	-4.1E-8	-2.0E-5	2.7E-7	-2.7E-7
721	0.010	-0.010	0.011	-0.011	-0.030	-0.035	1.0E-5	8.3E-6	-2.1E-6	-1.2E-5	3.5E-7	-3.5E-7
722	0.010	-0.010	0.011	-0.011	-0.030	-0.035	1.0E-5	8.7E-6	-1.3E-6	-6.4E-6	4.1E-7	-4.1E-7
723	0.009	-0.010	0.011	-0.011	-0.029	-0.035	2.4E-6	-5.6E-7	4.7E-6	-2.7E-5	1.2E-6	-1.2E-6
724	0.010	-0.010	0.011	-0.011	-0.029	-0.035	4.0E-6	1.1E-6	3.6E-6	-2.5E-5	6.1E-7	-6.1E-7
725	0.010	-0.010	0.011	-0.011	-0.029	-0.035	6.2E-6	3.2E-6	2.3E-6	-2.4E-5	9.5E-7	-9.5E-7
726	0.010	-0.010	0.011	-0.011	-0.029	-0.035	8.6E-6	5.6E-6	9.7E-7	-2.2E-5	5.3E-7	-5.3E-7
727	0.010	-0.010	0.011	-0.011	-0.030	-0.036	8.1E-6	6.3E-6	-2.0E-6	-1.3E-5	2.2E-7	-2.2E-7
728	0.010	-0.010	0.011	-0.011	-0.031	-0.036	7.8E-6	6.3E-6	-1.3E-6	-6.7E-6	7.6E-8	-7.6E-8
729	0.009	-0.010	0.011	-0.011	-0.031	-0.036	1.9E-6	1.4E-7	-1.0E-6	-1.7E-5	3.3E-7	-3.3E-7
730	0.010	-0.010	0.011	-0.011	-0.031	-0.036	3.3E-6	1.7E-6	-1.5E-6	-1.6E-5	8.1E-7	-8.1E-7
731	0.010	-0.010	0.011	-0.011	-0.031	-0.036	5.2E-6	3.8E-6	-1.8E-6	-1.4E-5	1.1E-6	-1.1E-6
732	0.010	-0.010	0.011	-0.011	-0.032	-0.037	4.9E-6	3.8E-6	-1.5E-6	-7.1E-6	5.6E-7	-5.6E-7
733	0.009	-0.010	0.011	-0.011	-0.032	-0.037	1.6E-6	3.5E-7	-1.9E-6	-1.0E-5	8.2E-7	-8.2E-7
734	0.010	-0.010	0.011	-0.011	-0.032	-0.037	2.7E-6	1.7E-6	-1.6E-6	-7.7E-6	7.1E-7	-7.1E-7
735	0.010	-0.010	0.011	-0.011	-0.032	-0.037	1.2E-6	4.2E-7	-1.1E-6	-6.0E-6	7.4E-7	-7.4E-7
736	0.010	-0.010	0.012	-0.012	-0.024	-0.034	7.0E-6	-2.1E-6	2.8E-5	-2.9E-5	1.2E-6	-1.2E-6
737	0.009	-0.010	0.012	-0.012	-0.024	-0.035	5.1E-6	-3.7E-6	3.1E-5	-2.8E-5	7.6E-7	-7.6E-7
738	0.010	-0.010	0.012	-0.012	-0.023	-0.037	9.5E-6	-4.4E-6	4.7E-5	-9.4E-6	8.5E-7	-8.5E-7
739	0.009	-0.010	0.012	-0.012	-0.023	-0.038	7.4E-6	-5.6E-6	5.1E-5	-2.8E-6	6.4E-7	-6.4E-7
740	0.010	-0.010	0.012	-0.012	-0.035	-0.058	2.6E-5	-1.6E-5	3.0E-4	2.4E-6	1.1E-6	-1.1E-6
741	0.010	-0.010	0.012	-0.012	-0.029	-0.046	1.8E-5	-1.0E-5	1.7E-4	1.5E-5	8.4E-7	-8.4E-7

742	0.010	-0.010	0.012	-0.012	-0.024	-0.041	1.2E-5	-6.3E-6	8.9E-5	1.3E-5	1.2E-6	-1.2E-6
743	0.009	-0.010	0.012	-0.012	-0.025	-0.042	1.0E-5	-7.6E-6	1.0E-4	1.6E-5	2.1E-7	-2.1E-7
744	0.009	-0.010	0.012	-0.012	-0.036	-0.059	2.4E-5	-1.7E-5	3.0E-4	4.7E-6	7.8E-7	-7.8E-7
745	0.009	-0.010	0.012	-0.012	-0.031	-0.048	1.6E-5	-1.2E-5	2.0E-4	1.3E-5	1.1E-6	-1.1E-6
746	0.009	-0.010	0.012	-0.012	-0.036	-0.064	2.1E-5	-1.7E-5	3.4E-4	-7.8E-6	1.5E-6	-1.5E-6
747	0.010	-0.010	0.012	-0.012	-0.024	-0.033	1.3E-5	1.7E-6	2.4E-5	-2.8E-5	9.8E-7	-9.8E-7
748	0.010	-0.010	0.012	-0.011	-0.024	-0.032	1.5E-5	2.4E-6	2.2E-5	-2.7E-5	8.3E-7	-8.3E-7
749	0.010	-0.010	0.012	-0.011	-0.024	-0.031	1.3E-5	1.2E-6	2.0E-5	-2.5E-5	9.5E-7	-9.5E-7
750	0.010	-0.010	0.012	-0.012	-0.034	-0.056	2.6E-5	-7.2E-6	2.8E-4	5.3E-6	1.5E-6	-1.5E-6
751	0.010	-0.010	0.012	-0.012	-0.028	-0.044	2.1E-5	-4.8E-6	1.6E-4	1.5E-5	1.0E-6	-1.0E-6
752	0.010	-0.010	0.012	-0.012	-0.023	-0.039	1.9E-5	-3.7E-6	7.9E-5	1.1E-5	1.1E-6	-1.1E-6
753	0.010	-0.010	0.012	-0.012	-0.027	-0.042	2.4E-5	-8.9E-6	1.4E-4	2.0E-5	1.1E-6	-1.1E-6
754	0.010	-0.010	0.012	-0.012	-0.025	-0.039	2.0E-5	-9.0E-6	1.1E-4	2.0E-5	9.8E-7	-9.8E-7
755	0.010	-0.010	0.012	-0.012	-0.023	-0.037	2.1E-5	-5.4E-6	7.8E-5	1.3E-5	6.4E-7	-6.4E-7
756	0.010	-0.010	0.011	-0.011	-0.030	-0.035	8.5E-6	6.9E-6	4.3E-6	-1.8E-6	7.8E-7	-7.8E-7
757	0.010	-0.010	0.011	-0.011	-0.031	-0.035	9.6E-6	7.6E-6	4.1E-6	-1.7E-6	1.3E-6	-1.3E-6
758	0.010	-0.010	0.011	-0.011	-0.031	-0.036	7.4E-6	5.1E-6	4.1E-6	-1.5E-6	7.7E-7	-7.7E-7
759	0.010	-0.010	0.011	-0.011	-0.032	-0.037	5.1E-6	1.5E-6	3.9E-6	-1.3E-6	9.8E-7	-9.8E-7
760	0.010	-0.010	0.011	-0.011	-0.032	-0.037	4.1E-6	-1.5E-6	3.8E-6	-1.2E-6	8.1E-7	-8.1E-7
761	0.011	-0.011	0.011	-0.011	-0.032	-0.037	4.5E-6	-2.5E-6	3.5E-6	-1.0E-6	1.4E-6	-1.4E-6
762	0.011	-0.011	0.011	-0.011	-0.031	-0.037	6.3E-6	-6.4E-7	3.0E-6	-8.0E-7	9.1E-7	-9.1E-7
763	0.011	-0.011	0.011	-0.011	-0.032	-0.037	8.8E-6	4.7E-6	3.0E-6	-1.2E-6	9.6E-7	-9.6E-7
764	0.011	-0.011	0.011	-0.011	-0.033	-0.038	1.9E-5	6.9E-6	3.4E-6	-2.5E-6	8.2E-7	-8.2E-7
765	0.012	-0.012	0.011	-0.011	-0.034	-0.039	3.5E-5	4.0E-6	6.4E-6	-6.9E-6	7.6E-7	-7.6E-7
766	0.012	-0.012	0.011	-0.011	-0.033	-0.038	5.3E-5	-4.4E-6	5.7E-6	-1.6E-5	5.3E-7	-5.3E-7
767	0.011	-0.011	0.011	-0.011	-0.030	-0.037	2.8E-5	7.2E-6	4.8E-6	-1.7E-5	8.7E-7	-8.7E-7
768	0.011	-0.011	0.011	-0.011	-0.029	-0.036	1.6E-5	5.7E-6	4.5E-6	-1.9E-5	8.7E-7	-8.7E-7
769	0.011	-0.011	0.011	-0.011	-0.029	-0.035	1.3E-5	-7.9E-7	4.2E-6	-2.1E-5	1.1E-6	-1.1E-6
770	0.011	-0.011	0.011	-0.011	-0.028	-0.035	1.1E-5	-3.7E-6	3.9E-6	-2.3E-5	1.2E-6	-1.2E-6
771	0.010	-0.011	0.011	-0.011	-0.028	-0.034	9.5E-6	-3.0E-6	4.0E-6	-2.5E-5	1.0E-7	-1.0E-7
772	0.010	-0.010	0.011	-0.011	-0.027	-0.034	9.1E-6	-1.6E-8	5.1E-6	-2.7E-5	4.0E-7	-4.0E-7
773	0.010	-0.010	0.011	-0.011	-0.027	-0.033	9.5E-6	3.8E-6	6.1E-6	-2.8E-5	3.7E-7	-3.7E-7
774	0.010	-0.010	0.011	-0.011	-0.026	-0.033	1.0E-5	6.2E-6	7.0E-6	-3.0E-5	2.5E-7	-2.5E-7
775	0.010	-0.010	0.011	-0.011	-0.025	-0.032	9.1E-6	5.1E-6	7.8E-6	-3.1E-5	8.5E-7	-8.5E-7
776	0.011	-0.011	0.012	-0.012	-0.036	-0.053	9.6E-6	-2.5E-5	2.1E-4	5.0E-5	5.4E-7	-5.4E-7
777	0.011	-0.011	0.012	-0.012	-0.029	-0.042	1.5E-5	-1.6E-5	1.2E-4	3.1E-5	7.2E-7	-7.2E-7
778	0.011	-0.011	0.012	-0.012	-0.025	-0.037	1.7E-5	-1.1E-5	5.6E-5	1.3E-5	1.6E-7	-1.6E-7
779	0.011	-0.011	0.012	-0.012	-0.025	-0.034	1.6E-5	-6.5E-6	3.0E-5	-1.4E-5	7.0E-7	-7.0E-7
780	0.011	-0.011	0.011	-0.012	-0.027	-0.034	1.3E-5	-3.8E-6	1.4E-5	-2.4E-5	1.0E-6	-1.0E-6
781	0.010	-0.010	0.012	-0.012	-0.035	-0.051	1.4E-5	-1.1E-5	2.4E-4	3.9E-5	8.0E-7	-8.0E-7
782	0.010	-0.010	0.012	-0.012	-0.025	-0.041	1.6E-5	-6.7E-6	1.1E-4	2.5E-5	1.1E-6	-1.1E-6
783	0.010	-0.010	0.012	-0.012	-0.023	-0.035	1.6E-5	-2.6E-6	4.7E-5	-6.6E-6	1.2E-6	-1.2E-6
784	0.010	-0.010	0.012	-0.012	-0.024	-0.033	1.2E-5	1.4E-6	2.2E-5	-2.9E-5	9.6E-7	-9.6E-7
785	0.010	-0.010	0.012	-0.012	-0.023	-0.041	1.7E-5	-3.0E-6	1.2E-4	2.6E-5	4.3E-7	-4.3E-7
786	0.010	-0.010	0.012	-0.012	-0.024	-0.041	1.7E-5	-3.5E-6	1.2E-4	2.6E-5	1.1E-6	-1.1E-6
787	0.010	-0.010	0.012	-0.012	-0.035	-0.051	1.5E-5	-9.3E-6	2.5E-4	3.4E-5	7.0E-7	-7.0E-7
788	0.010	-0.010	0.012	-0.012	-0.034	-0.051	2.0E-5	-1.2E-5	2.7E-4	3.0E-5	7.2E-7	-7.2E-7
789	0.010	-0.010	0.012	-0.012	-0.036	-0.066	2.5E-5	-2.7E-5	3.6E-4	2.3E-5	8.7E-8	-8.7E-8
790	0.012	-0.011	0.011	-0.011	-0.035	-0.052	2.8E-5	-2.3E-5	-1.2E-5	-1.4E-4	2.0E-7	-2.0E-7
791	0.012	-0.011	0.011	-0.011	-0.033	-0.044	3.9E-5	-7.7E-6	-6.5E-6	-9.3E-5	7.1E-7	-7.1E-7
792	0.012	-0.011	0.011	-0.011	-0.031	-0.041	4.0E-5	5.2E-7	-4.8E-6	-5.2E-5	1.0E-6	-1.0E-6
793	0.012	-0.011	0.011	-0.011	-0.030	-0.039	4.0E-5	8.3E-6	5.5E-6	-3.0E-5	4.2E-7	-4.2E-7
794	0.012	-0.011	0.011	-0.011	-0.031	-0.038	3.8E-5	1.1E-5	1.8E-5	-2.2E-5	3.3E-7	-3.3E-7
795	0.012	-0.011	0.011	-0.011	-0.032	-0.038	3.6E-5	1.4E-5	2.1E-5	-1.4E-5	5.0E-7	-5.0E-7
796	0.012	-0.011	0.011	-0.011	-0.033	-0.038	3.8E-5	1.1E-5	1.6E-5	-5.7E-6	1.0E-7	-1.0E-7
797	0.012	-0.011	0.011	-0.011	-0.034	-0.039	3.7E-5	1.1E-5	9.5E-6	-7.7E-7	9.1E-7	-9.1E-7
798	0.012	-0.011	0.011	-0.011	-0.034	-0.039	3.7E-5	8.7E-6	1.0E-5	-4.8E-6	3.1E-7	-3.1E-7
799	0.012	-0.011	0.011	-0.011	-0.034	-0.039	3.8E-5	5.9E-6	5.8E-6	-3.8E-6	2.0E-7	-2.0E-7
800	0.012	-0.012	0.011	-0.011	-0.034	-0.039	3.8E-5	2.1E-6	2.7E-6	-2.8E-6	3.0E-7	-3.0E-7
801	0.011	-0.011	0.011	-0.011	-0.035	-0.052	1.5E-5	-2.4E-5	-2.8E-5	-1.6E-4	1.1E-6	-1.1E-6
802	0.011	-0.011	0.011	-0.011	-0.033	-0.043	2.6E-5	-7.4E-6	-1.7E-5	-1.0E-4	2.7E-7	-2.7E-7
803	0.011	-0.011	0.011	-0.011	-0.030	-0.039	3.2E-5	1.2E-6	-8.7E-6	-5.9E-5	1.1E-6	-1.1E-6
804	0.011	-0.011	0.011	-0.011	-0.029	-0.037	3.2E-5	6.2E-6	1.8E-6	-3.1E-5	1.3E-6	-1.3E-6
805	0.011	-0.011	0.011	-0.011	-0.029	-0.037	3.0E-5	1.0E-5	1.5E-5	-2.1E-5	7.3E-7	-7.3E-7
806	0.011	-0.011	0.011	-0.011	-0.030	-0.037	2.7E-5	1.2E-5	1.8E-5	-1.2E-5	1.8E-7	-1.8E-7
807	0.011	-0.011	0.011	-0.011	-0.032	-0.037	2.5E-5	1.2E-5	1.5E-5	-4.2E-6	4.8E-7	-4.8E-7
808	0.011	-0.011	0.011	-0.011	-0.032	-0.037	2.3E-5	1.2E-5	1.0E-5	5.6E-7	6.5E-7	-6.5E-7
809	0.011	-0.011	0.011	-0.011	-0.032	-0.038	2.1E-5	1.1E-5	7.0E-6	9.1E-7	1.4E-6	-1.4E-6
810	0.011	-0.011	0.011	-0.011	-0.033	-0.038	2.1E-5	8.4E-6	4.7E-6	-1.8E-8	6.9E-7	-6.9E-7
811	0.011	-0.011	0.011	-0.011	-0.033	-0.038	2.0E-5	7.4E-6	2.6E-6	-3.2E-7	1.4E-6	-1.4E-6
812	0.011	-0.011	0.011	-0.011	-0.036	-0.052	7.5E-6	-2.5E-5	-4.1E-5	-1.8E-4	1.7E-6	-1.7E-6
813	0.011	-0.011	0.011	-0.011	-0.032	-0.043	1.7E-5	-9.3E-6	-2.5E-5	-1.1E-4	8.5E-7	-8.5E-7

814	0.011	-0.011	0.011	-0.011	-0.029	-0.039	2.3E-5	-2.6E-6	-1.3E-5	-6.4E-5	3.4E-7	-3.4E-7
815	0.011	-0.011	0.011	-0.011	-0.028	-0.036	2.5E-5	2.1E-6	1.5E-7	-3.3E-5	3.3E-7	-3.3E-7
816	0.011	-0.011	0.011	-0.011	-0.028	-0.035	2.2E-5	5.4E-6	1.4E-5	-2.0E-5	3.5E-7	-3.5E-7
817	0.011	-0.011	0.011	-0.011	-0.029	-0.036	1.9E-5	7.0E-6	1.8E-5	-1.0E-5	7.7E-7	-7.7E-7
818	0.011	-0.011	0.011	-0.011	-0.030	-0.036	1.7E-5	7.2E-6	1.6E-5	-3.4E-6	1.4E-6	-1.4E-6
819	0.011	-0.011	0.011	-0.011	-0.031	-0.036	1.4E-5	7.5E-6	1.2E-5	8.4E-7	5.5E-7	-5.5E-7
820	0.011	-0.011	0.011	-0.011	-0.031	-0.037	1.2E-5	7.2E-6	8.1E-6	2.0E-6	1.2E-6	-1.2E-6
821	0.011	-0.011	0.011	-0.011	-0.031	-0.037	1.1E-5	6.2E-6	5.3E-6	1.5E-6	8.0E-7	-8.0E-7
822	0.011	-0.011	0.011	-0.011	-0.032	-0.037	9.8E-6	5.2E-6	3.5E-6	4.3E-7	1.4E-6	-1.4E-6
823	0.011	-0.011	0.011	-0.011	-0.031	-0.037	6.6E-6	-1.2E-7	4.1E-6	1.0E-6	1.1E-6	-1.1E-6
824	0.011	-0.011	0.011	-0.011	-0.031	-0.037	4.5E-6	-2.1E-6	4.6E-6	1.3E-6	5.4E-7	-5.4E-7
825	0.011	-0.010	0.011	-0.011	-0.031	-0.037	4.0E-6	-1.2E-6	5.1E-6	1.5E-6	2.4E-7	-2.4E-7
826	0.010	-0.010	0.011	-0.011	-0.031	-0.036	5.0E-6	1.6E-6	5.5E-6	1.5E-6	2.1E-7	-2.1E-7
827	0.010	-0.010	0.011	-0.011	-0.031	-0.036	7.3E-6	5.1E-6	5.7E-6	1.5E-6	1.2E-6	-1.2E-6
828	0.010	-0.010	0.011	-0.011	-0.030	-0.035	9.7E-6	7.5E-6	5.8E-6	1.6E-6	1.1E-6	-1.1E-6
829	0.010	-0.010	0.011	-0.011	-0.030	-0.034	8.6E-6	6.8E-6	5.8E-6	1.6E-6	9.4E-7	-9.4E-7
830	0.011	-0.011	0.011	-0.011	-0.037	-0.052	7.4E-6	-2.9E-5	-4.8E-5	-1.9E-4	1.4E-6	-1.4E-6
831	0.011	-0.011	0.011	-0.011	-0.032	-0.043	1.4E-5	-1.5E-5	-3.2E-5	-1.3E-4	1.4E-6	-1.4E-6
832	0.011	-0.011	0.011	-0.011	-0.028	-0.038	1.8E-5	-7.1E-6	-1.7E-5	-6.9E-5	1.6E-6	-1.6E-6
833	0.011	-0.011	0.011	-0.011	-0.027	-0.035	1.8E-5	-2.6E-6	-1.0E-6	-3.6E-5	1.2E-6	-1.2E-6
834	0.011	-0.011	0.011	-0.011	-0.027	-0.035	1.7E-5	3.9E-7	1.4E-5	-2.1E-5	2.7E-7	-2.7E-7
835	0.011	-0.011	0.011	-0.011	-0.028	-0.035	1.4E-5	2.1E-6	1.9E-5	-1.0E-5	9.4E-7	-9.4E-7
836	0.011	-0.011	0.011	-0.011	-0.029	-0.035	1.1E-5	2.6E-6	1.8E-5	-3.1E-6	1.4E-6	-1.4E-6
837	0.011	-0.011	0.011	-0.011	-0.030	-0.036	9.0E-6	2.7E-6	1.4E-5	8.3E-7	9.5E-7	-9.5E-7
838	0.011	-0.011	0.011	-0.011	-0.031	-0.036	7.8E-6	1.8E-6	9.6E-6	2.5E-6	1.4E-6	-1.4E-6
839	0.011	-0.011	0.011	-0.011	-0.031	-0.037	7.1E-6	7.0E-7	6.2E-6	2.3E-6	8.5E-7	-8.5E-7
840	0.011	-0.011	0.011	-0.011	-0.031	-0.037	4.8E-6	-1.5E-6	7.3E-6	2.6E-6	1.2E-6	-1.2E-6
841	0.011	-0.010	0.011	-0.011	-0.031	-0.036	4.0E-6	-8.3E-7	8.4E-6	2.6E-6	4.5E-7	-4.5E-7
842	0.010	-0.010	0.011	-0.011	-0.031	-0.036	5.0E-6	1.8E-6	9.3E-6	2.6E-6	7.7E-7	-7.7E-7
843	0.010	-0.010	0.011	-0.011	-0.030	-0.036	7.4E-6	5.1E-6	1.0E-5	2.6E-6	1.2E-6	-1.2E-6
844	0.010	-0.010	0.011	-0.011	-0.030	-0.035	9.7E-6	7.4E-6	1.1E-5	2.5E-6	5.5E-7	-5.5E-7
845	0.010	-0.010	0.011	-0.011	-0.029	-0.034	8.6E-6	6.8E-6	1.1E-5	2.5E-6	4.0E-7	-4.0E-7
846	0.011	-0.011	0.011	-0.011	-0.037	-0.053	8.9E-6	-3.1E-5	-5.2E-5	-2.2E-4	1.7E-6	-1.7E-6
847	0.011	-0.011	0.011	-0.011	-0.032	-0.043	1.3E-5	-1.8E-5	-3.6E-5	-1.4E-4	3.2E-7	-3.2E-7
848	0.011	-0.011	0.011	-0.011	-0.028	-0.038	1.5E-5	-1.1E-5	-2.1E-5	-7.5E-5	1.5E-6	-1.5E-6
849	0.011	-0.011	0.011	-0.011	-0.026	-0.035	1.5E-5	-6.5E-6	-2.5E-6	-3.9E-5	1.1E-6	-1.1E-6
850	0.011	-0.011	0.011	-0.011	-0.026	-0.034	1.3E-5	-3.2E-6	1.5E-5	-2.2E-5	4.3E-7	-4.3E-7
851	0.011	-0.011	0.011	-0.011	-0.027	-0.034	1.0E-5	-1.1E-6	2.1E-5	-1.1E-5	1.6E-6	-1.6E-6
852	0.011	-0.011	0.011	-0.011	-0.029	-0.035	7.7E-6	-1.5E-7	2.0E-5	-3.4E-6	6.1E-7	-6.1E-7
853	0.011	-0.011	0.011	-0.011	-0.030	-0.036	5.9E-6	1.4E-8	1.6E-5	8.1E-7	5.0E-7	-5.0E-7
854	0.011	-0.011	0.011	-0.011	-0.031	-0.036	5.3E-6	-8.3E-7	1.1E-5	2.6E-6	5.6E-7	-5.6E-7
855	0.011	-0.010	0.011	-0.011	-0.030	-0.036	4.3E-6	-4.3E-7	1.3E-5	2.4E-6	6.6E-7	-6.6E-7
856	0.010	-0.010	0.011	-0.011	-0.030	-0.036	5.0E-6	1.9E-6	1.5E-5	2.1E-6	6.3E-7	-6.3E-7
857	0.010	-0.010	0.011	-0.011	-0.029	-0.035	7.4E-6	5.2E-6	1.6E-5	1.7E-6	4.2E-7	-4.2E-7
858	0.010	-0.010	0.011	-0.011	-0.029	-0.034	9.7E-6	7.6E-6	1.7E-5	1.4E-6	1.1E-6	-1.1E-6
859	0.010	-0.010	0.011	-0.011	-0.028	-0.033	8.7E-6	6.7E-6	1.8E-5	1.1E-6	1.1E-6	-1.1E-6
860	0.011	-0.010	0.011	-0.011	-0.038	-0.054	1.0E-5	-3.0E-5	-5.4E-5	-2.3E-4	1.6E-6	-1.6E-6
861	0.011	-0.010	0.011	-0.011	-0.032	-0.044	1.2E-5	-1.9E-5	-3.9E-5	-1.5E-4	1.0E-6	-1.0E-6
862	0.011	-0.010	0.011	-0.011	-0.027	-0.039	1.4E-5	-1.3E-5	-2.4E-5	-8.2E-5	5.7E-7	-5.7E-7
863	0.011	-0.010	0.011	-0.011	-0.025	-0.035	1.3E-5	-8.2E-6	-4.5E-6	-4.3E-5	5.3E-7	-5.3E-7
864	0.011	-0.010	0.011	-0.011	-0.026	-0.034	1.1E-5	-4.8E-6	1.5E-5	-2.5E-5	3.8E-7	-3.8E-7
865	0.011	-0.010	0.011	-0.011	-0.027	-0.034	8.5E-6	-2.3E-6	2.2E-5	-1.3E-5	1.3E-6	-1.3E-6
866	0.011	-0.010	0.011	-0.011	-0.028	-0.035	6.3E-6	-7.7E-7	2.2E-5	-4.6E-6	5.0E-7	-5.0E-7
867	0.011	-0.010	0.011	-0.011	-0.029	-0.035	4.7E-6	-1.0E-7	1.8E-5	3.4E-7	1.1E-6	-1.1E-6
868	0.010	-0.010	0.011	-0.011	-0.029	-0.035	5.5E-6	1.8E-6	2.0E-5	-7.0E-7	1.1E-6	-1.1E-6
869	0.010	-0.010	0.011	-0.011	-0.028	-0.034	7.5E-6	4.7E-6	2.3E-5	-2.2E-6	3.6E-7	-3.6E-7
870	0.010	-0.010	0.011	-0.011	-0.027	-0.033	9.8E-6	7.1E-6	2.5E-5	-3.6E-6	2.1E-7	-2.1E-7
871	0.010	-0.010	0.011	-0.011	-0.026	-0.032	9.2E-6	5.8E-6	2.6E-5	-5.1E-6	1.0E-6	-1.0E-6
872	0.011	-0.010	0.011	-0.011	-0.038	-0.056	1.2E-5	-2.6E-5	-5.2E-5	-2.5E-4	1.1E-6	-1.1E-6
873	0.011	-0.010	0.011	-0.011	-0.032	-0.045	1.3E-5	-1.7E-5	-4.1E-5	-1.6E-4	1.5E-6	-1.5E-6
874	0.011	-0.010	0.011	-0.011	-0.027	-0.040	1.4E-5	-1.2E-5	-2.7E-5	-9.1E-5	7.8E-7	-7.8E-7
875	0.011	-0.010	0.011	-0.011	-0.025	-0.036	1.3E-5	-7.9E-6	-8.2E-6	-4.8E-5	7.6E-7	-7.6E-7
876	0.011	-0.010	0.011	-0.011	-0.025	-0.034	1.1E-5	-4.3E-6	1.4E-5	-2.9E-5	2.3E-7	-2.3E-7
877	0.011	-0.010	0.011	-0.011	-0.026	-0.034	8.8E-6	-1.4E-6	2.3E-5	-1.6E-5	3.3E-8	-3.3E-8
878	0.010	-0.010	0.011	-0.011	-0.027	-0.034	6.8E-6	6.3E-7	2.4E-5	-6.7E-6	5.3E-7	-5.3E-7
879	0.010	-0.010	0.011	-0.011	-0.026	-0.033	8.7E-6	3.4E-6	2.6E-5	-9.6E-6	1.0E-6	-1.0E-6
880	0.010	-0.010	0.011	-0.011	-0.025	-0.032	1.1E-5	5.7E-6	2.7E-5	-1.3E-5	7.1E-7	-7.1E-7
881	0.010	-0.010	0.011	-0.011	-0.024	-0.031	1.2E-5	4.1E-6	2.8E-5	-1.7E-5	7.5E-7	-7.5E-7
882	0.011	-0.010	0.011	-0.011	-0.039	-0.057	1.4E-5	-2.0E-5	-5.1E-5	-2.6E-4	2.5E-7	-2.5E-7
883	0.011	-0.010	0.011	-0.011	-0.033	-0.046	1.5E-5	-1.3E-5	-4.2E-5	-1.8E-4	1.2E-6	-1.2E-6
884	0.011	-0.010	0.011	-0.011	-0.027	-0.041	1.5E-5	-9.4E-6	-3.0E-5	-1.0E-4	5.8E-7	-5.8E-7
885	0.010	-0.010	0.011	-0.011	-0.024	-0.037	1.4E-5	-5.4E-6	-1.4E-5	-5.4E-5	1.2E-6	-1.2E-6

886	0.010	-0.010	0.011	-0.011	-0.024	-0.034	1.2E-5	-1.9E-6	1.0E-5	-3.5E-5	3.9E-7	-3.9E-7
887	0.010	-0.010	0.011	-0.011	-0.025	-0.033	1.0E-5	1.1E-6	2.3E-5	-2.1E-5	9.7E-7	-9.7E-7
888	0.010	-0.010	0.011	-0.011	-0.024	-0.032	1.3E-5	3.5E-6	2.1E-5	-2.7E-5	1.1E-6	-1.1E-6
889	0.010	-0.010	0.011	-0.011	-0.022	-0.032	1.5E-5	1.7E-6	1.5E-5	-3.4E-5	5.0E-7	-5.0E-7
890	0.011	-0.010	0.011	-0.011	-0.039	-0.059	1.8E-5	-1.4E-5	-4.4E-5	-2.9E-4	6.8E-7	-6.8E-7
891	0.010	-0.010	0.011	-0.011	-0.034	-0.047	1.7E-5	-7.7E-6	-4.2E-5	-2.0E-4	1.0E-6	-1.0E-6
892	0.010	-0.010	0.011	-0.011	-0.027	-0.042	1.7E-5	-4.7E-6	-3.2E-5	-1.3E-4	4.0E-7	-4.0E-7
893	0.010	-0.010	0.011	-0.011	-0.024	-0.038	1.6E-5	-2.0E-6	-2.1E-5	-7.2E-5	1.2E-6	-1.2E-6
894	0.010	-0.010	0.011	-0.011	-0.023	-0.035	1.5E-5	5.7E-7	6.3E-7	-4.4E-5	1.8E-7	-1.8E-7
895	0.010	-0.010	0.011	-0.011	-0.022	-0.036	1.9E-5	-3.2E-7	-1.6E-5	-5.7E-5	2.0E-7	-2.0E-7
896	0.010	-0.010	0.011	-0.011	-0.039	-0.063	2.7E-5	-1.3E-5	-3.8E-5	-3.1E-4	1.6E-6	-1.6E-6
897	0.010	-0.010	0.011	-0.011	-0.036	-0.051	2.3E-5	-7.2E-6	-3.8E-5	-2.5E-4	1.1E-6	-1.1E-6
898	0.010	-0.010	0.011	-0.011	-0.031	-0.045	2.2E-5	-4.6E-6	-3.5E-5	-1.8E-4	6.9E-7	-6.9E-7
899	0.010	-0.010	0.011	-0.011	-0.026	-0.040	2.3E-5	-3.0E-6	-2.9E-5	-1.2E-4	3.8E-7	-3.8E-7
900	0.010	-0.010	0.011	-0.011	-0.039	-0.068	3.2E-5	-1.3E-5	-2.6E-5	-3.5E-4	1.7E-6	-1.7E-6
901	0.010	-0.010	0.011	-0.011	-0.037	-0.059	3.0E-5	-9.6E-6	-3.0E-5	-3.1E-4	8.5E-7	-8.5E-7
902	0.010	-0.010	0.011	-0.011	-0.035	-0.051	2.7E-5	-9.3E-6	-2.9E-5	-2.6E-4	1.2E-6	-1.2E-6
903	0.010	-0.010	0.011	-0.011	-0.037	-0.068	3.2E-5	-1.0E-5	-2.1E-5	-3.5E-4	1.6E-6	-1.6E-6
904	0.012	-0.012	0.011	-0.011	-0.035	-0.039	3.7E-5	4.2E-7	7.8E-6	-7.7E-6	1.2E-6	-1.2E-6
905	0.012	-0.012	0.011	-0.011	-0.034	-0.039	3.9E-5	3.5E-7	6.9E-6	-6.2E-6	4.9E-7	-4.9E-7
906	0.012	-0.012	0.011	-0.011	-0.034	-0.039	4.4E-5	-4.1E-6	2.5E-6	-2.4E-6	1.3E-6	-1.3E-6
907	0.012	-0.012	0.011	-0.011	-0.034	-0.039	4.5E-5	-1.7E-6	3.8E-6	-6.0E-6	8.1E-7	-8.1E-7
908	0.012	-0.012	0.011	-0.011	-0.034	-0.039	4.9E-5	-3.5E-6	4.8E-6	-1.0E-5	7.0E-7	-7.0E-7
909	0.012	-0.012	0.011	-0.011	-0.034	-0.039	4.8E-5	-2.0E-7	1.8E-6	-1.1E-5	9.1E-7	-9.1E-7
910	0.011	-0.011	0.011	-0.011	-0.033	-0.038	1.8E-5	7.6E-6	3.7E-6	-3.7E-6	1.1E-6	-1.1E-6
911	0.011	-0.011	0.011	-0.011	-0.032	-0.038	2.0E-5	5.7E-6	2.5E-6	-3.4E-6	2.0E-7	-2.0E-7
912	0.011	-0.011	0.011	-0.011	-0.032	-0.038	2.2E-5	6.1E-6	6.2E-7	-3.1E-6	1.5E-6	-1.5E-6
913	0.011	-0.011	0.011	-0.011	-0.032	-0.038	2.3E-5	5.8E-6	2.2E-7	-5.4E-6	1.2E-6	-1.2E-6
914	0.011	-0.011	0.011	-0.011	-0.032	-0.038	2.4E-5	7.5E-6	-2.2E-7	-8.3E-6	1.4E-6	-1.4E-6
915	0.011	-0.011	0.011	-0.011	-0.031	-0.037	2.6E-5	6.9E-6	2.3E-7	-1.2E-5	1.4E-6	-1.4E-6
916	0.011	-0.011	0.011	-0.011	-0.032	-0.037	8.1E-6	4.5E-6	2.4E-6	-2.4E-6	4.0E-7	-4.0E-7
917	0.011	-0.011	0.011	-0.011	-0.031	-0.037	9.1E-6	4.8E-6	1.4E-6	-3.3E-6	4.4E-7	-4.4E-7
918	0.011	-0.011	0.011	-0.011	-0.031	-0.037	9.9E-6	5.1E-6	1.6E-8	-4.4E-6	3.3E-7	-3.3E-7
919	0.011	-0.011	0.011	-0.011	-0.031	-0.037	1.1E-5	5.6E-6	-1.2E-6	-6.4E-6	5.6E-7	-5.6E-7
920	0.011	-0.011	0.011	-0.011	-0.030	-0.037	1.1E-5	6.5E-6	-1.8E-6	-9.2E-6	8.4E-7	-8.4E-7
921	0.011	-0.011	0.011	-0.011	-0.030	-0.036	1.4E-5	6.2E-6	-4.5E-8	-1.4E-5	1.2E-6	-1.2E-6
922	0.011	-0.011	0.011	-0.011	-0.031	-0.037	6.3E-6	-7.6E-7	2.1E-6	-2.3E-6	7.5E-8	-7.5E-8
923	0.011	-0.011	0.011	-0.011	-0.031	-0.037	6.6E-6	-9.1E-7	7.5E-7	-3.5E-6	8.2E-7	-8.2E-7
924	0.011	-0.011	0.011	-0.011	-0.031	-0.037	7.4E-6	-9.8E-7	-7.2E-7	-5.0E-6	8.0E-7	-8.0E-7
925	0.011	-0.011	0.011	-0.011	-0.031	-0.037	8.4E-6	-1.0E-6	-2.3E-6	-7.0E-6	1.4E-6	-1.4E-6
926	0.011	-0.011	0.011	-0.011	-0.030	-0.036	9.9E-6	-1.1E-6	-2.4E-6	-1.1E-5	3.8E-7	-3.8E-7
927	0.011	-0.011	0.011	-0.011	-0.029	-0.036	1.1E-5	-9.9E-7	-2.5E-7	-1.6E-5	1.0E-6	-1.0E-6
928	0.011	-0.011	0.011	-0.011	-0.032	-0.037	4.7E-6	-2.8E-6	2.4E-6	-2.7E-6	4.4E-7	-4.4E-7
929	0.011	-0.011	0.011	-0.011	-0.031	-0.037	5.1E-6	-3.0E-6	6.5E-7	-3.9E-6	8.3E-7	-8.3E-7
930	0.011	-0.011	0.011	-0.011	-0.031	-0.037	5.7E-6	-3.2E-6	-1.4E-6	-5.2E-6	9.2E-7	-9.2E-7
931	0.011	-0.011	0.011	-0.011	-0.031	-0.037	6.6E-6	-3.3E-6	-2.6E-6	-8.2E-6	3.2E-7	-3.2E-7
932	0.011	-0.011	0.011	-0.011	-0.030	-0.036	7.8E-6	-3.5E-6	-2.8E-6	-1.2E-5	4.2E-7	-4.2E-7
933	0.011	-0.011	0.011	-0.011	-0.029	-0.035	9.3E-6	-3.7E-6	-7.2E-7	-1.8E-5	2.8E-7	-2.8E-7
934	0.010	-0.011	0.011	-0.011	-0.029	-0.035	7.9E-6	-2.7E-6	-8.7E-7	-1.9E-5	1.2E-6	-1.2E-6
935	0.010	-0.010	0.011	-0.011	-0.029	-0.035	7.9E-6	4.6E-7	-9.0E-7	-2.0E-5	7.5E-7	-7.5E-7
936	0.010	-0.010	0.011	-0.011	-0.029	-0.034	8.7E-6	4.2E-6	-7.4E-7	-2.1E-5	1.2E-6	-1.2E-6
937	0.010	-0.010	0.011	-0.011	-0.028	-0.034	9.8E-6	7.1E-6	-4.4E-7	-2.2E-5	1.2E-6	-1.2E-6
938	0.010	-0.010	0.011	-0.011	-0.027	-0.033	8.5E-6	6.1E-6	-2.7E-7	-2.2E-5	1.1E-6	-1.1E-6
939	0.010	-0.010	0.011	-0.011	-0.032	-0.037	4.3E-6	-1.7E-6	2.5E-6	-2.9E-6	1.2E-6	-1.2E-6
940	0.010	-0.011	0.011	-0.011	-0.032	-0.037	4.6E-6	-1.9E-6	5.9E-7	-4.2E-6	3.1E-7	-3.1E-7
941	0.010	-0.011	0.011	-0.011	-0.031	-0.037	5.1E-6	-2.1E-6	-1.6E-6	-5.6E-6	1.5E-6	-1.5E-6
942	0.010	-0.011	0.011	-0.011	-0.031	-0.036	5.7E-6	-2.3E-6	-2.7E-6	-8.9E-6	1.5E-6	-1.5E-6
943	0.010	-0.011	0.011	-0.011	-0.030	-0.036	6.7E-6	-2.4E-6	-3.1E-6	-1.3E-5	3.8E-7	-3.8E-7
944	0.010	-0.010	0.011	-0.011	-0.030	-0.036	6.9E-6	6.7E-7	-3.1E-6	-1.4E-5	9.4E-7	-9.4E-7
945	0.010	-0.010	0.011	-0.011	-0.030	-0.035	8.1E-6	4.5E-6	-2.9E-6	-1.4E-5	8.6E-7	-8.6E-7
946	0.010	-0.010	0.011	-0.011	-0.029	-0.034	9.8E-6	7.4E-6	-2.7E-6	-1.4E-5	2.9E-7	-2.9E-7
947	0.010	-0.010	0.011	-0.011	-0.029	-0.034	8.6E-6	6.7E-6	-2.5E-6	-1.3E-5	1.0E-6	-1.0E-6
948	0.010	-0.010	0.011	-0.011	-0.032	-0.037	5.2E-6	1.3E-6	2.6E-6	-3.0E-6	7.3E-7	-7.3E-7
949	0.010	-0.010	0.011	-0.011	-0.032	-0.037	5.4E-6	1.2E-6	6.6E-7	-4.3E-6	1.3E-6	-1.3E-6
950	0.010	-0.010	0.011	-0.011	-0.031	-0.036	5.7E-6	9.8E-7	-1.6E-6	-5.7E-6	1.2E-6	-1.2E-6
951	0.010	-0.010	0.011	-0.011	-0.031	-0.036	6.2E-6	8.5E-7	-2.7E-6	-9.1E-6	7.1E-7	-7.1E-7
952	0.010	-0.010	0.011	-0.011	-0.030	-0.036	7.6E-6	4.6E-6	-2.5E-6	-9.0E-6	4.0E-8	-4.0E-8
953	0.010	-0.010	0.011	-0.011	-0.030	-0.035	9.8E-6	7.5E-6	-2.2E-6	-8.2E-6	7.2E-7	-7.2E-7
954	0.010	-0.010	0.011	-0.011	-0.029	-0.034	8.6E-6	6.8E-6	-1.9E-6	-7.3E-6	2.7E-7	-2.7E-7
955	0.010	-0.010	0.011	-0.011	-0.031	-0.036	7.4E-6	5.0E-6	2.8E-6	-3.1E-6	8.4E-7	-8.4E-7
956	0.010	-0.010	0.011	-0.011	-0.031	-0.036	7.4E-6	4.9E-6	1.1E-6	-4.3E-6	1.4E-6	-1.4E-6
957	0.010	-0.010	0.011	-0.011	-0.031	-0.036	7.4E-6	4.7E-6	-1.3E-6	-5.4E-6	1.2E-6	-1.2E-6

958	0.010	-0.010	0.011	-0.011	-0.030	-0.035	9.7E-6	7.5E-6	-6.3E-7	-5.1E-6	2.5E-7	-2.5E-7
959	0.010	-0.010	0.011	-0.011	-0.030	-0.035	8.7E-6	7.0E-6	6.9E-7	-4.8E-6	6.5E-7	-6.5E-7
960	0.010	-0.010	0.011	-0.011	-0.031	-0.036	9.4E-6	7.4E-6	3.2E-6	-3.1E-6	1.2E-6	-1.2E-6
961	0.010	-0.010	0.011	-0.011	-0.031	-0.035	9.6E-6	7.6E-6	1.8E-6	-4.1E-6	5.2E-7	-5.2E-7
962	0.010	-0.010	0.011	-0.011	-0.030	-0.035	8.6E-6	7.0E-6	2.9E-6	-3.6E-6	1.1E-6	-1.1E-6
963	0.010	-0.010	0.011	-0.011	-0.030	-0.035	9.1E-6	7.4E-6	3.3E-6	-3.1E-6	8.0E-7	-8.0E-7
964	0.012	-0.012	0.012	-0.012	-0.028	-0.057	1.0E-4	-9.4E-5	1.6E-4	-1.8E-5	5.1E-7	-5.1E-7
965	0.011	-0.012	0.012	-0.012	-0.032	-0.053	6.2E-5	-6.7E-5	1.6E-4	1.5E-5	8.2E-7	-8.2E-7
966	0.011	-0.011	0.012	-0.012	-0.033	-0.052	3.6E-5	-4.3E-5	1.8E-4	3.2E-5	9.0E-7	-9.0E-7
967	0.011	-0.011	0.012	-0.012	-0.034	-0.052	1.6E-5	-3.4E-5	1.9E-4	3.9E-5	2.2E-7	-2.2E-7
968	0.011	-0.011	0.012	-0.012	-0.035	-0.052	1.1E-5	-2.8E-5	2.1E-4	4.8E-5	1.3E-6	-1.3E-6
969	0.012	-0.012	0.012	-0.012	-0.029	-0.047	8.7E-5	-5.4E-5	1.1E-4	-2.0E-5	1.4E-6	-1.4E-6
970	0.011	-0.012	0.012	-0.012	-0.030	-0.044	6.0E-5	-3.6E-5	1.0E-4	1.7E-6	3.8E-7	-3.8E-7
971	0.011	-0.011	0.012	-0.012	-0.030	-0.043	3.6E-5	-2.2E-5	1.1E-4	1.3E-5	1.3E-6	-1.3E-6
972	0.011	-0.011	0.012	-0.012	-0.029	-0.043	1.9E-5	-1.4E-5	1.1E-4	2.2E-5	8.9E-7	-8.9E-7
973	0.011	-0.011	0.012	-0.012	-0.029	-0.042	1.6E-5	-1.5E-5	1.2E-4	2.7E-5	1.1E-6	-1.1E-6
974	0.011	-0.011	0.012	-0.012	-0.026	-0.037	1.8E-5	-7.8E-6	5.5E-5	9.6E-6	1.6E-7	-1.6E-7
975	0.011	-0.011	0.012	-0.012	-0.026	-0.034	1.8E-5	-3.4E-6	2.9E-5	-1.4E-5	1.3E-6	-1.3E-6
976	0.011	-0.011	0.011	-0.012	-0.027	-0.034	1.5E-5	-1.1E-6	1.4E-5	-2.3E-5	5.9E-7	-5.9E-7
977	0.012	-0.012	0.012	-0.012	-0.028	-0.043	7.8E-5	-3.5E-5	6.2E-5	-1.6E-5	1.6E-6	-1.6E-6
978	0.011	-0.012	0.012	-0.012	-0.028	-0.040	5.5E-5	-1.7E-5	5.6E-5	-4.8E-6	1.1E-6	-1.1E-6
979	0.011	-0.011	0.012	-0.012	-0.027	-0.038	3.4E-5	-6.5E-6	5.4E-5	2.0E-6	1.4E-7	-1.4E-7
980	0.011	-0.011	0.012	-0.012	-0.026	-0.038	2.2E-5	-4.6E-6	5.4E-5	5.5E-6	6.2E-7	-6.2E-7
981	0.011	-0.011	0.012	-0.012	-0.026	-0.035	2.1E-5	1.9E-6	2.9E-5	-1.5E-5	8.3E-7	-8.3E-7
982	0.011	-0.011	0.011	-0.012	-0.028	-0.035	1.9E-5	4.5E-6	1.4E-5	-2.2E-5	3.7E-7	-3.7E-7
983	0.012	-0.012	0.012	-0.012	-0.029	-0.040	7.0E-5	-2.0E-5	3.7E-5	-1.9E-5	7.1E-7	-7.1E-7
984	0.011	-0.012	0.012	-0.012	-0.029	-0.037	4.9E-5	-6.7E-6	3.3E-5	-1.7E-5	1.2E-6	-1.2E-6
985	0.011	-0.011	0.012	-0.012	-0.027	-0.036	3.0E-5	2.7E-6	3.0E-5	-1.6E-5	1.2E-6	-1.2E-6
986	0.011	-0.011	0.011	-0.012	-0.029	-0.036	2.7E-5	6.7E-6	1.5E-5	-2.1E-5	7.8E-7	-7.8E-7
987	0.012	-0.012	0.012	-0.012	-0.031	-0.038	6.7E-5	-1.7E-5	2.5E-5	-2.5E-5	7.7E-7	-7.7E-7
988	0.011	-0.012	0.011	-0.012	-0.031	-0.037	4.7E-5	-1.6E-6	1.8E-5	-2.3E-5	1.4E-6	-1.4E-6
989	0.012	-0.012	0.011	-0.012	-0.032	-0.039	6.6E-5	-1.4E-5	1.6E-5	-2.3E-5	1.9E-7	-1.9E-7
990	0.010	-0.011	0.012	-0.012	-0.037	-0.052	1.1E-5	-2.3E-5	2.3E-4	4.9E-5	1.5E-6	-1.5E-6
991	0.010	-0.011	0.012	-0.012	-0.036	-0.052	1.2E-5	-1.9E-5	2.3E-4	4.7E-5	5.6E-7	-5.6E-7
992	0.010	-0.011	0.012	-0.012	-0.036	-0.052	1.3E-5	-1.4E-5	2.4E-4	4.1E-5	1.1E-6	-1.1E-6
993	0.010	-0.011	0.012	-0.012	-0.028	-0.042	1.5E-5	-1.5E-5	1.2E-4	3.2E-5	8.6E-7	-8.6E-7
994	0.010	-0.011	0.012	-0.012	-0.027	-0.042	1.6E-5	-1.3E-5	1.2E-4	2.9E-5	2.2E-7	-2.2E-7
995	0.010	-0.011	0.012	-0.012	-0.026	-0.041	1.6E-5	-9.8E-6	1.1E-4	2.8E-5	6.1E-7	-6.1E-7
996	0.010	-0.011	0.012	-0.012	-0.025	-0.036	1.6E-5	-1.0E-5	5.2E-5	1.0E-5	4.6E-8	-4.6E-8
997	0.010	-0.011	0.012	-0.012	-0.024	-0.036	1.6E-5	-8.3E-6	5.0E-5	2.4E-6	9.9E-7	-9.9E-7
998	0.010	-0.011	0.012	-0.012	-0.023	-0.035	1.5E-5	-5.5E-6	4.7E-5	-2.7E-6	7.2E-7	-7.2E-7
999	0.010	-0.010	0.012	-0.012	-0.025	-0.033	1.2E-5	-1.5E-6	2.1E-5	-2.7E-5	1.1E-6	-1.1E-6
1000	0.010	-0.011	0.012	-0.012	-0.025	-0.034	1.4E-5	-6.4E-6	2.8E-5	-1.7E-5	2.5E-7	-2.5E-7
1001	0.010	-0.011	0.012	-0.012	-0.025	-0.033	1.3E-5	-4.0E-6	2.1E-5	-2.5E-5	3.2E-7	-3.2E-7
1002	0.010	-0.011	0.011	-0.012	-0.026	-0.034	1.2E-5	-4.0E-6	1.4E-5	-2.5E-5	5.4E-7	-5.4E-7
1003	0.010	-0.010	0.012	-0.012	-0.022	-0.031	1.1E-5	3.4E-6	2.4E-5	-3.1E-5	7.6E-7	-7.6E-7
1004	0.010	-0.010	0.012	-0.012	-0.023	-0.032	1.3E-5	4.2E-6	2.3E-5	-3.0E-5	8.8E-7	-8.8E-7
1005	0.010	-0.010	0.012	-0.012	-0.022	-0.035	1.6E-5	8.3E-7	4.9E-5	-6.5E-6	4.5E-7	-4.5E-7
1006	0.010	-0.010	0.012	-0.012	-0.021	-0.034	1.4E-5	6.2E-7	5.1E-5	-6.9E-6	1.6E-7	-1.6E-7
1007	0.010	-0.010	0.012	-0.012	-0.037	-0.065	1.9E-5	-1.5E-5	3.4E-4	3.0E-5	6.4E-7	-6.4E-7
1008	0.010	-0.010	0.012	-0.012	-0.037	-0.065	1.9E-5	-1.9E-5	3.4E-4	3.0E-5	8.2E-7	-8.2E-7
1009	0.010	-0.010	0.011	-0.011	-0.038	-0.071	3.4E-5	-1.1E-5	-1.9E-5	-3.8E-4	8.3E-7	-8.3E-7
1010	0.010	-0.010	0.011	-0.011	-0.036	-0.065	2.8E-5	-1.3E-5	-2.2E-5	-3.3E-4	5.9E-7	-5.9E-7
1011	0.011	-0.011	0.011	-0.011	-0.035	-0.039	-1.5E-6	-4.0E-5	4.1E-6	-4.1E-6	6.8E-7	-6.8E-7
1012	0.011	-0.011	0.011	-0.011	-0.033	-0.038	-7.3E-6	-2.2E-5	2.6E-6	-3.7E-6	4.2E-7	-4.2E-7
1013	0.011	-0.011	0.011	-0.011	-0.032	-0.038	-6.3E-6	-9.5E-6	1.9E-6	-3.7E-6	1.2E-7	-1.2E-7
1014	0.010	-0.011	0.011	-0.011	-0.031	-0.037	-1.5E-6	-8.5E-6	1.5E-6	-3.9E-6	7.0E-7	-7.0E-7
1015	0.010	-0.010	0.011	-0.011	-0.031	-0.037	3.4E-7	-7.7E-6	1.3E-6	-3.8E-6	6.8E-7	-6.8E-7
1016	0.010	-0.010	0.011	-0.011	-0.031	-0.036	-1.0E-6	-7.7E-6	1.3E-6	-3.8E-6	5.1E-7	-5.1E-7
1017	0.010	-0.010	0.011	-0.011	-0.031	-0.036	-3.9E-6	-8.6E-6	1.3E-6	-3.8E-6	1.2E-6	-1.2E-6
1018	0.010	-0.010	0.011	-0.011	-0.031	-0.035	-6.4E-6	-9.4E-6	1.5E-6	-3.9E-6	8.3E-7	-8.3E-7
1019	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-6.0E-6	-8.0E-6	1.7E-6	-4.0E-6	1.3E-7	-1.3E-7
1020	0.010	-0.011	0.012	-0.012	-0.037	-0.051	2.2E-5	-1.3E-5	2.0E-4	5.5E-5	8.2E-7	-8.2E-7
1021	0.010	-0.011	0.012	-0.012	-0.029	-0.041	1.2E-5	-1.6E-5	1.1E-4	3.2E-5	9.2E-7	-9.2E-7
1022	0.010	-0.011	0.012	-0.012	-0.026	-0.036	6.2E-6	-1.7E-5	4.7E-5	1.2E-5	2.2E-7	-2.2E-7
1023	0.010	-0.011	0.012	-0.012	-0.026	-0.034	2.3E-6	-1.5E-5	2.4E-5	-1.3E-5	1.4E-6	-1.4E-6
1024	0.010	-0.011	0.011	-0.011	-0.027	-0.034	1.1E-6	-1.4E-5	9.2E-6	-2.1E-5	1.4E-6	-1.4E-6
1025	0.010	-0.011	0.011	-0.011	-0.029	-0.035	1.3E-6	-1.2E-5	1.2E-6	-1.9E-5	5.2E-7	-5.2E-7
1026	0.010	-0.011	0.011	-0.011	-0.030	-0.036	1.2E-6	-1.1E-5	-2.0E-6	-1.3E-5	1.1E-6	-1.1E-6
1027	0.010	-0.010	0.011	-0.011	-0.030	-0.036	1.1E-6	-9.6E-6	-2.8E-6	-8.0E-6	2.3E-7	-2.3E-7
1028	0.010	-0.010	0.011	-0.011	-0.031	-0.037	7.5E-7	-8.5E-6	-1.2E-6	-5.1E-6	2.4E-7	-2.4E-7
1029	0.011	-0.011	0.011	-0.011	-0.032	-0.038	9.4E-6	-5.9E-5	1.4E-5	-1.9E-5	7.6E-7	-7.6E-7

1030	0.011	-0.011	0.011	-0.011	-0.031	-0.037	-1.3E-6	-3.9E-5	1.1E-5	-1.7E-5	1.5E-6	-1.5E-6
1031	0.011	-0.011	0.011	-0.011	-0.029	-0.036	-8.0E-6	-2.3E-5	8.9E-6	-1.7E-5	4.2E-7	-4.2E-7
1032	0.010	-0.011	0.011	-0.011	-0.028	-0.035	-5.7E-6	-1.6E-5	8.8E-6	-1.8E-5	7.4E-7	-7.4E-7
1033	0.010	-0.011	0.011	-0.011	-0.028	-0.035	-1.3E-6	-1.4E-5	9.0E-6	-1.9E-5	8.6E-7	-8.6E-7
1034	0.010	-0.011	0.012	-0.012	-0.030	-0.041	1.1E-5	-1.6E-5	1.0E-4	2.9E-5	3.0E-7	-3.0E-7
1035	0.010	-0.011	0.012	-0.012	-0.031	-0.040	1.6E-5	-2.6E-5	9.7E-5	2.3E-5	3.6E-7	-3.6E-7
1036	0.011	-0.011	0.012	-0.012	-0.032	-0.041	2.8E-5	-4.9E-5	9.2E-5	1.2E-5	1.3E-6	-1.3E-6
1037	0.011	-0.011	0.012	-0.012	-0.031	-0.045	4.8E-5	-8.1E-5	9.7E-5	-1.1E-5	3.7E-7	-3.7E-7
1038	0.011	-0.011	0.012	-0.012	-0.036	-0.054	7.3E-5	-5.3E-5	1.7E-4	3.2E-5	3.6E-7	-3.6E-7
1039	0.011	-0.011	0.012	-0.012	-0.035	-0.045	4.7E-5	-5.2E-5	1.3E-4	2.2E-5	6.7E-7	-6.7E-7
1040	0.011	-0.011	0.012	-0.012	-0.031	-0.059	1.1E-4	-1.0E-4	1.7E-4	-5.8E-6	1.3E-6	-1.3E-6
1041	0.011	-0.011	0.012	-0.012	-0.031	-0.050	7.3E-5	-8.9E-5	1.4E-4	-1.1E-5	7.0E-7	-7.0E-7
1042	0.011	-0.011	0.012	-0.012	-0.028	-0.060	1.1E-4	-1.2E-4	1.7E-4	-3.2E-5	9.9E-7	-9.9E-7
1043	0.011	-0.011	0.011	-0.011	-0.035	-0.051	2.0E-5	-2.9E-5	-1.4E-5	-1.3E-4	7.6E-7	-7.6E-7
1044	0.011	-0.011	0.011	-0.011	-0.034	-0.051	2.0E-5	-1.9E-5	-2.4E-5	-1.4E-4	3.9E-7	-3.9E-7
1045	0.011	-0.010	0.011	-0.011	-0.034	-0.051	2.1E-5	-1.1E-5	-3.9E-5	-1.6E-4	7.8E-7	-7.8E-7
1046	0.011	-0.010	0.011	-0.011	-0.034	-0.051	2.1E-5	-7.6E-6	-4.3E-5	-1.7E-4	1.2E-6	-1.2E-6
1047	0.011	-0.010	0.011	-0.011	-0.034	-0.052	2.0E-5	-7.5E-6	-5.0E-5	-2.0E-4	9.6E-7	-9.6E-7
1048	0.011	-0.010	0.011	-0.011	-0.035	-0.052	1.9E-5	-1.0E-5	-4.9E-5	-2.0E-4	5.9E-7	-5.9E-7
1049	0.011	-0.010	0.011	-0.011	-0.035	-0.051	1.7E-5	-1.3E-5	-5.1E-5	-2.2E-4	7.7E-7	-7.7E-7
1050	0.011	-0.010	0.011	-0.011	-0.035	-0.051	1.3E-5	-1.6E-5	-5.1E-5	-2.1E-4	2.0E-7	-2.0E-7
1051	0.011	-0.010	0.011	-0.011	-0.035	-0.050	7.9E-6	-1.8E-5	-4.7E-5	-2.3E-4	9.0E-7	-9.0E-7
1052	0.011	-0.010	0.011	-0.011	-0.035	-0.049	6.2E-6	-2.1E-5	-4.4E-5	-2.2E-4	1.0E-6	-1.0E-6
1053	0.010	-0.010	0.011	-0.011	-0.034	-0.049	6.8E-6	-1.9E-5	-3.7E-5	-2.4E-4	4.5E-7	-4.5E-7
1054	0.011	-0.011	0.011	-0.011	-0.031	-0.045	4.6E-6	-4.0E-5	-5.9E-6	-8.1E-5	5.5E-7	-5.5E-7
1055	0.011	-0.011	0.011	-0.011	-0.031	-0.043	3.0E-6	-2.9E-5	-1.2E-5	-8.9E-5	5.8E-7	-5.8E-7
1056	0.011	-0.010	0.011	-0.011	-0.030	-0.043	3.8E-6	-2.1E-5	-1.6E-5	-9.6E-5	6.4E-7	-6.4E-7
1057	0.011	-0.010	0.011	-0.011	-0.029	-0.042	6.4E-6	-1.6E-5	-2.1E-5	-1.0E-4	1.0E-6	-1.0E-6
1058	0.011	-0.010	0.011	-0.011	-0.028	-0.042	9.5E-6	-1.5E-5	-2.3E-5	-1.1E-4	1.3E-6	-1.3E-6
1059	0.011	-0.010	0.011	-0.011	-0.028	-0.042	1.0E-5	-1.5E-5	-2.6E-5	-1.1E-4	1.8E-7	-1.8E-7
1060	0.011	-0.010	0.011	-0.011	-0.027	-0.041	9.1E-6	-1.6E-5	-2.8E-5	-1.1E-4	3.6E-7	-3.6E-7
1061	0.011	-0.010	0.011	-0.011	-0.027	-0.041	6.3E-6	-1.7E-5	-2.9E-5	-1.1E-4	7.1E-7	-7.1E-7
1062	0.011	-0.010	0.011	-0.011	-0.026	-0.040	3.9E-6	-1.8E-5	-2.9E-5	-1.1E-4	3.7E-7	-3.7E-7
1063	0.010	-0.010	0.011	-0.011	-0.026	-0.039	2.7E-6	-1.9E-5	-2.7E-5	-1.1E-4	9.2E-7	-9.2E-7
1064	0.010	-0.010	0.011	-0.011	-0.025	-0.039	3.8E-6	-1.7E-5	-2.6E-5	-1.1E-4	1.1E-6	-1.1E-6
1065	0.011	-0.011	0.011	-0.011	-0.030	-0.042	-3.0E-6	-4.0E-5	-2.8E-6	-4.3E-5	9.1E-7	-9.1E-7
1066	0.011	-0.011	0.011	-0.011	-0.029	-0.039	-6.2E-6	-3.2E-5	-2.8E-6	-4.7E-5	1.1E-6	-1.1E-6
1067	0.011	-0.011	0.011	-0.011	-0.028	-0.038	-4.1E-6	-2.5E-5	-3.4E-6	-5.0E-5	1.4E-6	-1.4E-6
1068	0.011	-0.010	0.011	-0.011	-0.027	-0.037	-5.5E-8	-2.0E-5	-3.8E-6	-5.1E-5	1.5E-6	-1.5E-6
1069	0.011	-0.010	0.011	-0.011	-0.026	-0.036	3.0E-6	-1.7E-5	-4.6E-6	-5.2E-5	5.5E-7	-5.5E-7
1070	0.011	-0.010	0.011	-0.011	-0.025	-0.036	4.4E-6	-1.6E-5	-4.4E-6	-5.2E-5	7.6E-7	-7.6E-7
1071	0.011	-0.010	0.011	-0.011	-0.025	-0.035	3.8E-6	-1.6E-5	-4.7E-6	-5.1E-5	8.2E-7	-8.2E-7
1072	0.011	-0.010	0.011	-0.011	-0.024	-0.035	2.3E-6	-1.6E-5	-3.3E-6	-5.0E-5	7.6E-7	-7.6E-7
1073	0.010	-0.010	0.011	-0.011	-0.024	-0.034	8.3E-7	-1.7E-5	-2.7E-6	-4.8E-5	1.3E-6	-1.3E-6
1074	0.010	-0.010	0.011	-0.011	-0.023	-0.033	-4.1E-8	-1.7E-5	4.9E-7	-4.7E-5	4.0E-7	-4.0E-7
1075	0.010	-0.010	0.011	-0.011	-0.022	-0.033	1.4E-6	-1.5E-5	2.9E-6	-4.6E-5	9.6E-7	-9.6E-7
1076	0.010	-0.010	0.011	-0.011	-0.023	-0.031	-1.5E-6	-1.1E-5	2.6E-5	-2.1E-5	7.3E-7	-7.3E-7
1077	0.010	-0.010	0.011	-0.011	-0.026	-0.032	-3.8E-6	-8.6E-6	2.6E-5	-5.4E-6	9.1E-7	-9.1E-7
1078	0.010	-0.010	0.011	-0.011	-0.027	-0.033	-5.0E-6	-7.4E-6	1.8E-5	2.1E-6	7.9E-7	-7.9E-7
1079	0.010	-0.010	0.011	-0.011	-0.029	-0.034	-5.6E-6	-7.5E-6	1.1E-5	2.7E-6	1.2E-6	-1.2E-6
1080	0.010	-0.010	0.011	-0.011	-0.029	-0.034	-5.8E-6	-7.7E-6	5.8E-6	1.4E-6	1.2E-6	-1.2E-6
1081	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-5.9E-6	-7.8E-6	4.0E-6	-2.0E-6	4.7E-7	-4.7E-7
1082	0.011	-0.011	0.011	-0.011	-0.030	-0.039	-1.1E-5	-3.9E-5	1.4E-5	-3.2E-5	7.1E-7	-7.1E-7
1083	0.011	-0.011	0.011	-0.011	-0.029	-0.037	-1.2E-5	-3.1E-5	1.3E-5	-3.0E-5	1.1E-6	-1.1E-6
1084	0.011	-0.011	0.011	-0.011	-0.028	-0.036	-8.7E-6	-2.4E-5	1.4E-5	-2.9E-5	1.4E-7	-1.4E-7
1085	0.011	-0.010	0.011	-0.011	-0.027	-0.035	-4.4E-6	-2.0E-5	1.5E-5	-2.9E-5	3.5E-7	-3.5E-7
1086	0.011	-0.010	0.011	-0.011	-0.026	-0.034	-1.1E-6	-1.6E-5	1.6E-5	-2.8E-5	7.2E-7	-7.2E-7
1087	0.011	-0.010	0.011	-0.011	-0.026	-0.034	2.8E-7	-1.4E-5	1.8E-5	-2.7E-5	6.8E-7	-6.8E-7
1088	0.011	-0.010	0.011	-0.011	-0.025	-0.033	2.7E-7	-1.4E-5	1.9E-5	-2.5E-5	1.1E-6	-1.1E-6
1089	0.010	-0.010	0.011	-0.011	-0.025	-0.033	-8.2E-7	-1.4E-5	2.0E-5	-2.3E-5	6.6E-7	-6.6E-7
1090	0.010	-0.010	0.011	-0.011	-0.025	-0.032	-2.3E-6	-1.5E-5	2.2E-5	-2.2E-5	5.8E-7	-5.8E-7
1091	0.010	-0.010	0.011	-0.011	-0.024	-0.032	-3.1E-6	-1.4E-5	2.4E-5	-2.1E-5	6.6E-7	-6.6E-7
1092	0.010	-0.010	0.011	-0.011	-0.026	-0.032	-5.5E-6	-1.1E-5	2.6E-5	-5.4E-6	3.2E-7	-3.2E-7
1093	0.010	-0.010	0.011	-0.011	-0.028	-0.033	-6.6E-6	-9.6E-6	1.8E-5	2.1E-6	5.8E-7	-5.8E-7
1094	0.010	-0.010	0.011	-0.011	-0.029	-0.034	-6.8E-6	-9.5E-6	1.1E-5	3.0E-6	3.0E-7	-3.0E-7
1095	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-6.8E-6	-9.4E-6	5.8E-6	1.5E-6	6.8E-7	-6.8E-7
1096	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-6.7E-6	-9.5E-6	3.9E-6	-1.8E-6	4.9E-7	-4.9E-7
1097	0.011	-0.011	0.011	-0.011	-0.032	-0.038	-1.2E-5	-3.8E-5	2.1E-5	-2.1E-5	1.6E-6	-1.6E-6
1098	0.011	-0.011	0.011	-0.011	-0.030	-0.037	-1.5E-5	-2.9E-5	2.0E-5	-1.8E-5	6.5E-7	-6.5E-7
1099	0.011	-0.011	0.011	-0.011	-0.029	-0.036	-1.1E-5	-2.2E-5	2.0E-5	-1.6E-5	1.6E-6	-1.6E-6
1100	0.011	-0.010	0.011	-0.011	-0.029	-0.035	-6.3E-6	-1.8E-5	2.1E-5	-1.4E-5	5.2E-7	-5.2E-7
1101	0.011	-0.010	0.011	-0.011	-0.028	-0.035	-3.1E-6	-1.4E-5	2.2E-5	-1.2E-5	4.2E-7	-4.2E-7

1102	0.011	-0.010	0.011	-0.011	-0.028	-0.034	-1.8E-6	-1.2E-5	2.3E-5	-1.0E-5	1.0E-6	-1.0E-6
1103	0.011	-0.010	0.011	-0.011	-0.027	-0.034	-1.8E-6	-1.1E-5	2.4E-5	-8.7E-6	9.4E-7	-9.4E-7
1104	0.010	-0.010	0.011	-0.011	-0.027	-0.033	-3.1E-6	-1.1E-5	2.5E-5	-7.2E-6	1.9E-7	-1.9E-7
1105	0.010	-0.010	0.011	-0.011	-0.027	-0.033	-4.7E-6	-1.1E-5	2.5E-5	-5.9E-6	8.0E-7	-8.0E-7
1106	0.010	-0.010	0.011	-0.011	-0.028	-0.034	-5.7E-6	-9.1E-6	1.8E-5	1.8E-6	8.7E-7	-8.7E-7
1107	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-5.4E-6	-8.6E-6	1.1E-5	3.2E-6	5.8E-7	-5.8E-7
1108	0.010	-0.010	0.011	-0.011	-0.030	-0.036	-5.0E-6	-8.4E-6	5.7E-6	1.7E-6	8.6E-7	-8.6E-7
1109	0.010	-0.010	0.011	-0.011	-0.031	-0.036	-4.5E-6	-8.4E-6	3.8E-6	-1.7E-6	1.1E-6	-1.1E-6
1110	0.011	-0.011	0.011	-0.011	-0.033	-0.038	-1.3E-5	-3.8E-5	2.0E-5	-1.2E-5	1.1E-6	-1.1E-6
1111	0.011	-0.011	0.011	-0.011	-0.032	-0.037	-1.3E-5	-2.9E-5	1.8E-5	-8.4E-6	6.2E-7	-6.2E-7
1112	0.011	-0.011	0.011	-0.011	-0.031	-0.036	-1.0E-5	-2.2E-5	1.8E-5	-5.7E-6	7.0E-7	-7.0E-7
1113	0.011	-0.010	0.011	-0.011	-0.030	-0.036	-6.6E-6	-1.6E-5	1.8E-5	-3.7E-6	1.3E-6	-1.3E-6
1114	0.011	-0.010	0.011	-0.011	-0.030	-0.035	-3.8E-6	-1.2E-5	1.9E-5	-2.2E-6	1.4E-7	-1.4E-7
1115	0.011	-0.010	0.011	-0.011	-0.029	-0.035	-2.6E-6	-9.4E-6	1.9E-5	-8.6E-7	6.4E-7	-6.4E-7
1116	0.010	-0.010	0.011	-0.011	-0.029	-0.035	-2.8E-6	-8.5E-6	1.9E-5	3.4E-7	4.9E-7	-4.9E-7
1117	0.010	-0.010	0.011	-0.011	-0.029	-0.034	-4.0E-6	-8.6E-6	1.8E-5	1.3E-6	3.0E-7	-3.0E-7
1118	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-3.3E-6	-7.8E-6	1.1E-5	3.4E-6	5.2E-7	-5.2E-7
1119	0.010	-0.010	0.011	-0.011	-0.031	-0.036	-2.6E-6	-7.5E-6	5.7E-6	1.9E-6	1.2E-6	-1.2E-6
1120	0.010	-0.010	0.011	-0.011	-0.031	-0.036	-1.9E-6	-7.4E-6	3.7E-6	-1.5E-6	6.9E-7	-6.9E-7
1121	0.011	-0.011	0.011	-0.011	-0.034	-0.039	-9.8E-6	-4.0E-5	1.3E-5	-3.2E-6	5.1E-7	-5.1E-7
1122	0.011	-0.011	0.011	-0.011	-0.033	-0.038	-1.2E-5	-2.9E-5	1.1E-5	-5.1E-7	7.1E-7	-7.1E-7
1123	0.011	-0.011	0.011	-0.011	-0.032	-0.037	-1.1E-5	-2.0E-5	1.1E-5	8.3E-7	1.4E-6	-1.4E-6
1124	0.011	-0.011	0.011	-0.011	-0.031	-0.036	-7.3E-6	-1.3E-5	1.2E-5	1.7E-6	5.8E-7	-5.8E-7
1125	0.011	-0.010	0.011	-0.011	-0.031	-0.036	-4.2E-6	-9.7E-6	1.2E-5	2.5E-6	1.1E-6	-1.1E-6
1126	0.011	-0.010	0.011	-0.011	-0.030	-0.036	-2.0E-6	-8.2E-6	1.1E-5	3.2E-6	7.9E-7	-7.9E-7
1127	0.010	-0.010	0.011	-0.011	-0.030	-0.036	-1.9E-6	-7.6E-6	1.1E-5	3.5E-6	5.0E-7	-5.0E-7
1128	0.010	-0.010	0.011	-0.011	-0.031	-0.036	-1.0E-6	-7.1E-6	5.7E-6	2.1E-6	4.8E-7	-4.8E-7
1129	0.010	-0.010	0.011	-0.011	-0.031	-0.037	-3.6E-7	-7.1E-6	3.7E-6	-1.4E-6	9.5E-8	-9.5E-8
1130	0.011	-0.011	0.011	-0.011	-0.035	-0.039	-9.4E-6	-4.0E-5	1.2E-5	-4.4E-6	2.7E-7	-2.7E-7
1131	0.011	-0.011	0.011	-0.011	-0.033	-0.038	-1.1E-5	-2.8E-5	8.6E-6	-7.3E-7	8.7E-8	-8.7E-8
1132	0.011	-0.011	0.011	-0.011	-0.032	-0.038	-1.1E-5	-1.8E-5	6.9E-6	1.3E-6	1.1E-6	-1.1E-6
1133	0.011	-0.011	0.011	-0.011	-0.031	-0.037	-7.4E-6	-1.2E-5	6.1E-6	2.5E-6	6.8E-7	-6.8E-7
1134	0.011	-0.010	0.011	-0.011	-0.031	-0.037	-3.6E-6	-9.1E-6	5.8E-6	2.8E-6	9.9E-7	-9.9E-7
1135	0.011	-0.010	0.011	-0.011	-0.031	-0.037	-1.2E-6	-7.7E-6	5.7E-6	2.3E-6	5.9E-7	-5.9E-7
1136	0.010	-0.010	0.011	-0.011	-0.031	-0.037	-9.7E-7	-7.6E-6	3.6E-6	-1.2E-6	3.4E-7	-3.4E-7
1137	0.011	-0.011	0.011	-0.011	-0.035	-0.039	-4.4E-6	-4.3E-5	8.6E-6	-5.2E-6	1.3E-6	-1.3E-6
1138	0.011	-0.011	0.011	-0.011	-0.034	-0.039	-7.6E-6	-3.1E-5	3.8E-6	-5.9E-7	7.0E-7	-7.0E-7
1139	0.011	-0.011	0.011	-0.011	-0.033	-0.038	-8.6E-6	-2.0E-5	3.2E-6	3.8E-7	6.5E-8	-6.5E-8
1140	0.011	-0.011	0.011	-0.011	-0.032	-0.038	-7.1E-6	-1.1E-5	3.4E-6	-1.9E-7	9.2E-7	-9.2E-7
1141	0.011	-0.011	0.011	-0.011	-0.031	-0.037	-4.4E-6	-8.8E-6	3.2E-6	-9.1E-7	7.2E-7	-7.2E-7
1142	0.011	-0.011	0.011	-0.011	-0.035	-0.040	-1.6E-6	-4.4E-5	2.7E-6	-2.6E-6	6.4E-7	-6.4E-7
1143	0.011	-0.011	0.011	-0.011	-0.034	-0.039	-5.5E-6	-3.3E-5	3.4E-6	-1.9E-6	8.2E-7	-8.2E-7
1144	0.011	-0.011	0.011	-0.011	-0.033	-0.038	-7.9E-6	-2.3E-5	2.7E-6	-1.3E-6	1.4E-6	-1.4E-6
1145	0.011	-0.011	0.011	-0.011	-0.032	-0.038	-8.4E-6	-1.6E-5	2.1E-6	-1.2E-6	8.0E-7	-8.0E-7
1146	0.011	-0.011	0.011	-0.011	-0.034	-0.039	-6.2E-6	-2.7E-5	1.6E-6	-1.2E-6	8.1E-7	-8.1E-7
1147	0.011	-0.011	0.011	-0.011	-0.035	-0.039	1.5E-6	-4.3E-5	2.5E-6	-1.5E-6	6.8E-7	-6.8E-7
1148	0.011	-0.011	0.011	-0.011	-0.035	-0.040	-2.1E-7	-4.3E-5	6.2E-6	-5.4E-6	1.2E-6	-1.2E-6
1149	0.011	-0.011	0.011	-0.011	-0.035	-0.040	6.2E-7	-4.4E-5	5.8E-6	-5.5E-6	8.7E-7	-8.7E-7
1150	0.011	-0.011	0.011	-0.011	-0.034	-0.039	-5.0E-6	-3.1E-5	3.2E-6	-2.2E-6	8.9E-7	-8.9E-7
1151	0.011	-0.011	0.011	-0.011	-0.035	-0.039	-4.3E-6	-3.6E-5	4.3E-6	-3.4E-6	3.2E-7	-3.2E-7
1152	0.010	-0.010	0.011	-0.011	-0.031	-0.036	-6.6E-7	-8.4E-6	-1.7E-6	-5.0E-6	9.1E-7	-9.1E-7
1153	0.010	-0.010	0.011	-0.011	-0.031	-0.036	-3.6E-6	-9.1E-6	-1.8E-6	-5.2E-6	3.3E-7	-3.3E-7
1154	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-6.1E-6	-9.4E-6	-1.7E-6	-5.3E-6	5.8E-7	-5.8E-7
1155	0.010	-0.010	0.011	-0.011	-0.029	-0.034	-5.7E-6	-7.9E-6	-1.5E-6	-5.5E-6	9.5E-7	-9.5E-7
1156	0.010	-0.010	0.011	-0.011	-0.030	-0.036	-3.2E-7	-9.3E-6	-2.9E-6	-8.8E-6	3.0E-7	-3.0E-7
1157	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-3.3E-6	-9.7E-6	-3.0E-6	-9.3E-6	1.0E-6	-1.0E-6
1158	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-5.8E-6	-9.8E-6	-3.0E-6	-9.7E-6	1.4E-7	-1.4E-7
1159	0.010	-0.010	0.011	-0.011	-0.029	-0.034	-5.4E-6	-7.8E-6	-2.8E-6	-1.0E-5	3.1E-7	-3.1E-7
1160	0.010	-0.010	0.011	-0.011	-0.030	-0.035	-2.3E-8	-1.0E-5	-2.3E-6	-1.4E-5	1.3E-6	-1.3E-6
1161	0.010	-0.010	0.011	-0.011	-0.029	-0.035	-2.9E-6	-1.1E-5	-2.3E-6	-1.5E-5	6.0E-7	-6.0E-7
1162	0.010	-0.010	0.011	-0.011	-0.028	-0.034	-5.4E-6	-1.0E-5	-2.2E-6	-1.6E-5	1.4E-7	-1.4E-7
1163	0.010	-0.010	0.011	-0.011	-0.028	-0.033	-5.0E-6	-7.9E-6	-2.0E-6	-1.6E-5	1.2E-6	-1.2E-6
1164	0.010	-0.010	0.011	-0.011	-0.028	-0.034	3.1E-7	-1.2E-5	1.5E-6	-2.0E-5	1.3E-6	-1.3E-6
1165	0.010	-0.010	0.011	-0.011	-0.028	-0.034	-2.3E-6	-1.2E-5	2.1E-6	-2.1E-5	1.1E-6	-1.1E-6
1166	0.010	-0.010	0.011	-0.011	-0.027	-0.033	-4.8E-6	-1.1E-5	2.8E-6	-2.2E-5	8.2E-7	-8.2E-7
1167	0.010	-0.010	0.011	-0.011	-0.026	-0.032	-4.3E-6	-8.7E-6	3.8E-6	-2.3E-5	1.2E-6	-1.2E-6
1168	0.010	-0.011	0.012	-0.012	-0.037	-0.051	1.9E-5	-1.7E-5	2.2E-4	5.5E-5	5.0E-7	-5.0E-7
1169	0.010	-0.011	0.012	-0.012	-0.029	-0.041	1.1E-5	-1.7E-5	1.1E-4	3.5E-5	1.0E-6	-1.0E-6
1170	0.010	-0.011	0.012	-0.012	-0.026	-0.036	6.0E-6	-1.7E-5	5.1E-5	1.4E-5	3.1E-7	-3.1E-7
1171	0.010	-0.011	0.012	-0.012	-0.025	-0.034	2.1E-6	-1.4E-5	2.6E-5	-1.2E-5	9.4E-7	-9.4E-7
1172	0.010	-0.010	0.011	-0.011	-0.027	-0.034	9.5E-7	-1.3E-5	1.0E-5	-2.2E-5	1.3E-6	-1.3E-6
1173	0.010	-0.010	0.011	-0.011	-0.026	-0.033	-1.5E-6	-1.3E-5	1.2E-5	-2.2E-5	8.6E-7	-8.6E-7

1174	0.010	-0.010	0.012	-0.011	-0.025	-0.032	-3.9E-6	-1.3E-5	1.4E-5	-2.3E-5	6.6E-7	-6.6E-7
1175	0.010	-0.010	0.012	-0.011	-0.024	-0.031	-2.5E-6	-1.1E-5	1.6E-5	-2.3E-5	7.5E-7	-7.5E-7
1176	0.010	-0.011	0.012	-0.012	-0.037	-0.051	1.3E-5	-2.0E-5	2.2E-4	5.5E-5	1.4E-6	-1.4E-6
1177	0.010	-0.011	0.012	-0.012	-0.029	-0.041	7.5E-6	-1.8E-5	1.2E-4	3.6E-5	1.4E-6	-1.4E-6
1178	0.010	-0.010	0.012	-0.012	-0.025	-0.036	3.6E-6	-1.7E-5	5.5E-5	1.7E-5	5.0E-7	-5.0E-7
1179	0.010	-0.010	0.012	-0.012	-0.025	-0.033	1.2E-7	-1.4E-5	2.9E-5	-1.1E-5	7.2E-7	-7.2E-7
1180	0.010	-0.010	0.012	-0.012	-0.024	-0.032	-1.6E-6	-1.5E-5	3.2E-5	-9.7E-6	1.2E-6	-1.2E-6
1181	0.010	-0.010	0.012	-0.012	-0.023	-0.032	-3.0E-7	-1.4E-5	3.6E-5	-6.9E-6	1.2E-6	-1.2E-6
1182	0.010	-0.011	0.012	-0.012	-0.037	-0.052	7.7E-6	-2.4E-5	2.4E-4	5.0E-5	1.3E-6	-1.3E-6
1183	0.010	-0.010	0.012	-0.012	-0.029	-0.041	3.0E-6	-1.9E-5	1.3E-4	3.7E-5	6.3E-7	-6.3E-7
1184	0.010	-0.010	0.012	-0.012	-0.025	-0.036	1.0E-6	-1.8E-5	6.4E-5	1.9E-5	3.0E-7	-3.0E-7
1185	0.010	-0.010	0.012	-0.012	-0.024	-0.036	1.2E-6	-1.8E-5	7.6E-5	2.1E-5	1.2E-6	-1.2E-6
1186	0.010	-0.010	0.012	-0.012	-0.036	-0.053	6.3E-6	-2.8E-5	2.5E-4	4.7E-5	6.4E-7	-6.4E-7
1187	0.010	-0.010	0.012	-0.012	-0.030	-0.042	1.8E-6	-2.1E-5	1.6E-4	3.6E-5	9.0E-7	-9.0E-7
1188	0.010	-0.010	0.012	-0.012	-0.036	-0.057	6.9E-6	-3.1E-5	2.8E-4	3.8E-5	1.1E-6	-1.1E-6
1189	0.011	-0.011	0.011	-0.011	-0.035	-0.039	7.7E-7	-4.3E-5	6.6E-6	-8.9E-6	8.6E-7	-8.6E-7
1190	0.011	-0.011	0.011	-0.011	-0.033	-0.038	-8.0E-6	-2.2E-5	2.1E-6	-5.7E-6	9.5E-7	-9.5E-7
1191	0.011	-0.011	0.011	-0.011	-0.031	-0.037	-6.7E-6	-1.1E-5	4.6E-7	-5.1E-6	1.4E-6	-1.4E-6
1192	0.010	-0.011	0.011	-0.011	-0.031	-0.037	-1.2E-6	-9.4E-6	-4.4E-7	-5.1E-6	1.3E-6	-1.3E-6
1193	0.011	-0.011	0.011	-0.011	-0.033	-0.038	8.8E-6	-5.6E-5	8.6E-6	-1.7E-5	6.5E-7	-6.5E-7
1194	0.011	-0.011	0.011	-0.011	-0.034	-0.039	2.8E-6	-4.9E-5	5.0E-6	-1.4E-5	7.8E-7	-7.8E-7
1195	0.011	-0.011	0.011	-0.011	-0.034	-0.039	3.9E-6	-4.8E-5	4.2E-7	-8.3E-6	9.3E-7	-9.3E-7
1196	0.011	-0.011	0.011	-0.011	-0.034	-0.039	-7.2E-8	-4.4E-5	2.0E-6	-7.3E-6	7.7E-7	-7.7E-7
1197	0.011	-0.011	0.011	-0.011	-0.032	-0.038	-6.0E-6	-2.5E-5	-3.6E-7	-6.1E-6	1.0E-6	-1.0E-6
1198	0.011	-0.011	0.011	-0.011	-0.031	-0.037	-6.9E-6	-1.3E-5	-1.3E-6	-6.6E-6	6.9E-7	-6.9E-7
1199	0.010	-0.011	0.011	-0.011	-0.030	-0.037	-9.4E-7	-1.1E-5	-2.2E-6	-7.2E-6	4.9E-7	-4.9E-7
1200	0.011	-0.011	0.011	-0.011	-0.031	-0.037	-4.5E-6	-3.4E-5	6.1E-6	-1.7E-5	7.1E-7	-7.1E-7
1201	0.011	-0.011	0.011	-0.011	-0.032	-0.037	-4.9E-6	-3.0E-5	2.5E-6	-1.3E-5	9.3E-7	-9.3E-7
1202	0.011	-0.011	0.011	-0.011	-0.032	-0.038	-5.7E-6	-2.7E-5	-8.1E-7	-8.4E-6	1.0E-6	-1.0E-6
1203	0.011	-0.011	0.011	-0.011	-0.030	-0.037	-6.8E-6	-1.4E-5	-1.4E-6	-9.6E-6	6.5E-7	-6.5E-7
1204	0.010	-0.011	0.011	-0.011	-0.030	-0.036	-1.0E-6	-1.2E-5	-1.8E-6	-1.1E-5	1.2E-6	-1.2E-6
1205	0.011	-0.011	0.011	-0.011	-0.030	-0.036	-8.5E-6	-1.9E-5	4.2E-6	-1.7E-5	1.1E-6	-1.1E-6
1206	0.011	-0.011	0.011	-0.011	-0.030	-0.036	-7.4E-6	-1.6E-5	9.1E-7	-1.4E-5	1.4E-6	-1.4E-6
1207	0.010	-0.011	0.011	-0.011	-0.029	-0.036	-1.9E-6	-1.3E-5	4.6E-7	-1.5E-5	4.3E-7	-4.3E-7
1208	0.010	-0.011	0.011	-0.011	-0.029	-0.035	-4.5E-6	-1.5E-5	3.7E-6	-1.8E-5	3.4E-7	-3.4E-7
1209	0.010	-0.011	0.011	-0.011	-0.028	-0.035	-8.9E-7	-1.3E-5	4.4E-6	-1.9E-5	1.3E-6	-1.3E-6
1210	0.010	-0.011	0.012	-0.012	-0.027	-0.035	3.3E-8	-1.6E-5	2.2E-5	-1.2E-5	1.4E-6	-1.4E-6
1211	0.010	-0.011	0.012	-0.012	-0.027	-0.036	3.9E-6	-1.8E-5	4.5E-5	1.0E-5	8.6E-8	-8.6E-8
1212	0.010	-0.011	0.012	-0.012	-0.028	-0.035	-3.7E-6	-2.0E-5	2.1E-5	-1.2E-5	1.3E-6	-1.3E-6
1213	0.010	-0.011	0.012	-0.012	-0.028	-0.036	1.8E-6	-2.3E-5	4.2E-5	7.9E-6	6.1E-7	-6.1E-7
1214	0.011	-0.011	0.012	-0.012	-0.031	-0.038	1.8E-5	-6.7E-5	2.2E-5	-1.6E-5	8.3E-7	-8.3E-7
1215	0.011	-0.011	0.012	-0.012	-0.030	-0.037	3.2E-6	-4.6E-5	2.0E-5	-1.3E-5	8.5E-7	-8.5E-7
1216	0.011	-0.011	0.012	-0.012	-0.029	-0.036	-3.9E-6	-2.9E-5	2.1E-5	-1.2E-5	3.8E-7	-3.8E-7
1217	0.011	-0.011	0.012	-0.012	-0.029	-0.037	6.4E-6	-3.8E-5	4.1E-5	2.9E-6	1.1E-6	-1.1E-6
1218	0.011	-0.011	0.012	-0.012	-0.030	-0.040	2.5E-5	-7.3E-5	3.7E-5	-1.4E-5	5.0E-7	-5.0E-7
1219	0.011	-0.011	0.012	-0.012	-0.030	-0.038	1.6E-5	-5.7E-5	4.2E-5	-4.7E-6	1.1E-6	-1.1E-6
1220	0.011	-0.011	0.012	-0.012	-0.030	-0.043	4.3E-5	-8.4E-5	6.1E-5	-1.6E-5	2.3E-7	-2.3E-7
1221	0.010	-0.011	0.012	-0.012	-0.037	-0.054	4.8E-5	-2.4E-5	2.0E-4	4.7E-5	1.7E-6	-1.7E-6
1222	0.010	-0.011	0.012	-0.012	-0.035	-0.045	3.0E-5	-2.7E-5	1.4E-4	3.4E-5	4.9E-7	-4.9E-7
1223	0.010	-0.011	0.012	-0.012	-0.038	-0.055	4.3E-5	-1.8E-5	2.1E-4	5.5E-5	1.2E-6	-1.2E-6
1224	0.010	-0.011	0.012	-0.012	-0.035	-0.046	2.3E-5	-1.6E-5	1.6E-4	4.4E-5	5.3E-7	-5.3E-7
1225	0.010	-0.011	0.012	-0.012	-0.039	-0.058	3.8E-5	-1.7E-5	2.4E-4	6.1E-5	7.1E-7	-7.1E-7
1226	0.011	-0.011	0.012	-0.012	-0.028	-0.053	8.4E-5	-1.0E-4	1.4E-4	-3.2E-5	1.2E-6	-1.2E-6

1.2.2 Involuppi dei diagrammi delle sollecitazioni: Sforzo Normale.

I dati seguenti riportano i valori dello Sforzo Normale relativamente alle aste che definiscono la struttura ed in modo particolare:

Asta : numerazione interna dell'asta.
X : distanza dal nodo iniziale misurata lungo l'asse dell'asta.
Sforzo Normale (N) : valore dello Sforzo Normale nel punto considerato:
Max : valore massimo (rispetto al sistema di riferimento globale) dell'involuppo.
Min : valore minimo (rispetto al sistema di riferimento globale) dell'involuppo.
Comb : combinazione di appartenenza del valore considerato nell'involuppo.

Tabella 27.I

Sforzo Normale (N) [daN]

				SLU		SLE					
Asta	Imp.	Fili	X [cm]	Max	Min	Caratteristiche		Frequenti		Quasi Permanenti	
						Max	Min	Max	Min	Max	Min
1	Fondazio ne	1-2	0	387	-491	25	-180	-39	-80	-52	-52
			42	502	-573	13	-167	-42	-78	-52	-52
			83	666	-769	1	-155	-44	-75	-52	-52
2	Fondazio ne	1-2	0	689	-787	-15	-139	-45	-70	-49	-49
			42	745	-849	-27	-126	-48	-68	-49	-49
			83	809	-924	-39	-114	-49	-65	-49	-49
3	Fondazio ne	1-15	0	1263	-1027	183	74	129	103	103	103
			40	1169	-932	175	81	126	102	102	102
			80	1274	-1042	166	88	124	101	101	101
4	Fondazio ne	1-15	0	600	-339	164	114	134	114	114	114
			40	492	-234	162	113	133	113	113	113
			80	666	-396	161	112	132	112	112	112
5	Fondazio ne	2-3	0	1114	-1335	-55	-268	-115	-158	-124	-124
			35	1153	-1383	-65	-258	-117	-156	-124	-124
			69	1201	-1440	-76	-247	-119	-154	-124	-124
6	Fondazio ne	2-3	0	1072	-1233	-28	-193	-72	-105	-81	-81
			35	1123	-1266	-38	-182	-74	-103	-81	-81
			69	1143	-1295	-48	-172	-76	-101	-81	-81
7	Fondazio ne	3-4	0	1090	-1188	-5	-140	-40	-67	-49	-49
			35	1130	-1207	-15	-130	-42	-65	-49	-49
			69	1149	-1235	-25	-120	-44	-63	-49	-49
8	Fondazio ne	3-4	0	1115	-1131	10	-92	-14	-34	-23	-23
			35	1112	-1138	0	-82	-16	-32	-23	-23
			69	1131	-1167	-10	-72	-18	-31	-23	-23
9	Fondazio ne	4-5	0	1099	-1081	22	-54	7	-9	-2	-2
			35	1089	-1081	12	-44	4	-7	-2	-2
			69	1109	-1110	8	-34	4	-5	-2	-2
10	Fondazio ne	4-5	0	1079	-1043	29	-18	22	12	13	13
			35	1052	-1026	29	-8	21	13	13	13
			69	1077	-1052	28	1	21	12	12	12
11	Fondazio ne	5-6	0	1062	-1025	43	12	34	23	23	23
			35	1034	-981	42	6	33	22	22	22
			69	1074	-1016	42	-4	33	22	22	22
12	Fondazio ne	5-6	0	1125	-1054	50	-6	38	26	27	27
			35	1095	-1014	55	-16	38	24	26	26
			69	1133	-1044	64	-26	40	22	26	26
13	Fondazio ne	6-7	0	1043	-869	120	60	104	87	87	87
			35	1040	-848	118	70	104	87	87	87
			69	1064	-881	118	80	104	87	87	87
14	Fondazio ne	6-7	0	1068	-873	122	80	107	90	90	90
			35	1029	-829	122	70	107	90	90	90
			69	1079	-870	124	60	107	90	90	90
15	Fondazio ne	7-8	0	939	-861	76	-8	54	37	39	39
			35	942	-837	70	2	53	39	39	39
			69	957	-860	67	12	53	39	39	39
16	Fondazio ne	7-8	0	896	-811	69	25	56	42	42	42
			35	852	-772	69	35	56	42	42	42
			69	884	-786	69	27	56	42	42	42
17	Fondazio ne	8-9	0	927	-831	69	20	53	40	40	40
			35	877	-787	69	10	53	40	40	40
			69	900	-792	71	0	53	39	40	40
18	Fondazio ne	8-9	0	944	-877	71	-20	47	28	32	32

			35	879	-818	81	-30	49	27	33	33
			69	943	-821	91	-40	51	25	33	33
19	Fondazio ne	9-10	0	843	-679	110	66	94	79	79	79
			35	803	-638	110	74	95	79	79	79
			69	816	-638	110	65	95	79	79	79
20	Fondazio ne	9-10	0	893	-754	99	37	85	71	71	71
			35	809	-677	105	27	86	70	71	71
			69	859	-674	115	17	88	69	72	72
21	Fondazio ne	10-1 1	0	697	-702	10	-41	4	-7	-3	-3
			35	650	-655	10	-31	4	-4	-3	-3
			69	662	-667	10	-21	4	-2	-2	-2
22	Fondazio ne	10-1 1	0	665	-713	-6	-35	-9	-15	-14	-14
			35	607	-660	-6	-45	-9	-17	-14	-14
			69	622	-643	-5	-55	-9	-19	-13	-13
23	Fondazio ne	11-1 2	0	682	-763	-31	-76	-31	-40	-33	-33
			35	603	-690	-22	-86	-29	-42	-33	-33
			69	589	-682	-12	-96	-27	-44	-33	-33
24	Fondazio ne	11-1 2	0	699	-850	-45	-128	-57	-73	-59	-59
			35	601	-755	-34	-138	-55	-75	-59	-59
			69	568	-721	-24	-148	-53	-77	-59	-59
25	Fondazio ne	12-1 3	0	741	-957	-68	-185	-91	-114	-93	-93
			35	615	-855	-57	-195	-89	-116	-93	-93
			69	571	-721	-47	-205	-86	-118	-93	-93
26	Fondazio ne	12-1 3	0	793	-1129	-95	-264	-135	-169	-138	-138
			35	664	-1026	-85	-274	-133	-171	-138	-138
			69	617	-843	-75	-285	-131	-173	-138	-138
27	Fondazio ne	13-1 4	0	637	-740	-48	-115	-52	-68	-52	-52
			42	438	-593	-35	-128	-52	-71	-52	-52
			83	367	-450	-23	-141	-50	-74	-52	-52
28	Fondazio ne	13-1 4	0	676	-797	-9	-168	-54	-85	-60	-60
			42	476	-673	3	-180	-51	-88	-61	-61
			83	446	-505	15	-193	-49	-91	-61	-61
29	Fondazio ne	14-1 6	0	480	-284	200	96	145	117	117	117
			40	417	-185	191	103	142	116	116	116
			80	665	-386	182	110	139	115	115	115
30	Fondazio ne	14-1 6	0	450	-170	169	118	140	118	118	118
			40	421	-142	167	117	138	117	117	117
			80	599	-323	165	116	137	116	116	116
31	Fondazio ne	15-1 7	0	1320	-1097	166	90	118	90	90	90
			33	1311	-1090	161	90	116	90	90	90
			66	1397	-1178	156	89	115	89	89	89
32	Fondazio ne	15-1 7	0	580	-370	141	85	109	85	85	85
			33	543	-335	140	85	108	85	85	85
			66	674	-468	139	84	108	84	84	84
33	Fondazio ne	16-1 8	0	488	-297	169	96	123	96	96	96
			33	575	-338	164	95	121	95	95	95
			66	734	-487	159	94	120	94	94	94
34	Fondazio ne	16-1 8	0	423	-233	154	95	121	95	95	95
			33	451	-262	153	94	120	94	94	94
			66	600	-362	152	94	119	94	94	94
35	Fondazio ne	17-1 9	0	1515	-1072	300	172	230	190	190	190
			33	1520	-1078	295	178	228	190	190	190
			66	1604	-1164	291	184	227	189	189	189
36	Fondazio ne	17-1 9	0	721	-339	243	164	197	164	164	164
			33	672	-291	238	164	197	164	164	164

			66	795	-413	234	164	196	164	164	164
37	Fondazio ne	18-2 0	0	528	-150	292	181	227	189	189	189
			33	629	-181	287	187	226	188	188	188
			66	785	-339	283	187	225	187	187	187
38	Fondazio ne	18-2 0	0	451	-106	252	173	207	173	173	173
			33	462	-108	247	172	206	172	172	172
			66	634	-229	246	172	206	172	172	172
39	Fondazio ne	19-2 1	0	1344	-1146	168	22	109	80	81	81
			33	1336	-1139	161	28	108	81	81	81
			66	1420	-1223	155	34	106	81	81	81
40	Fondazio ne	19-2 1	0	607	-456	109	26	79	61	61	61
			33	539	-389	105	32	79	61	61	61
			66	663	-513	101	38	79	61	61	61
41	Fondazio ne	20-2 2	0	412	-262	159	36	109	83	83	83
			33	446	-259	153	42	108	83	83	83
			66	603	-394	146	48	106	82	82	82
42	Fondazio ne	20-2 2	0	405	-276	109	37	83	64	64	64
			33	414	-287	106	43	82	64	64	64
			66	517	-353	105	49	82	63	63	63
43	Fondazio ne	21-2 3	0	1452	-1141	229	71	166	134	134	134
			33	1423	-1112	222	77	164	134	134	134
			66	1512	-1201	216	83	163	134	134	134
44	Fondazio ne	21-2 3	0	689	-424	171	79	137	114	114	114
			33	602	-337	167	86	137	114	114	114
			66	713	-448	164	92	137	114	114	114
45	Fondazio ne	22-2 4	0	512	-236	220	90	168	138	138	138
			33	529	-253	215	96	166	138	138	138
			66	635	-308	211	102	165	138	138	138
46	Fondazio ne	22-2 4	0	539	-303	173	93	142	118	118	118
			33	535	-299	173	99	141	118	118	118
			66	588	-347	172	105	141	118	118	118
47	Fondazio ne	23-2 5	0	1361	-1400	44	-125	-3	-36	-16	-16
			33	1304	-1343	38	-119	-4	-35	-16	-16
			66	1395	-1434	32	-112	-5	-34	-16	-16
48	Fondazio ne	23-2 5	0	602	-742	-22	-138	-48	-71	-52	-52
			33	485	-625	-22	-131	-48	-70	-52	-52
			66	575	-715	-22	-125	-48	-69	-52	-52
49	Fondazio ne	24-2 6	0	413	-427	42	-90	8	-18	-3	-3
			33	433	-440	36	-84	7	-17	-3	-3
			66	478	-485	30	-78	5	-16	-3	-3
50	Fondazio ne	24-2 6	0	376	-486	3	-102	-27	-48	-35	-35
			33	363	-433	3	-96	-28	-47	-35	-35
			66	432	-485	2	-90	-28	-46	-35	-35
51	Fondazio ne	25-2 6	0	931	-594	344	36	222	160	169	169
			49	841	-509	327	48	216	160	166	166
			97	916	-589	309	60	210	160	164	164
52	Fondazio ne	25-2 6	0	798	-486	308	44	204	151	156	156
			49	701	-394	291	56	199	152	154	154
			97	801	-497	274	68	193	152	152	152
53	Fondazio ne	25-2 6	0	762	-431	308	68	213	165	166	166
			49	650	-323	291	80	208	164	164	164
			97	760	-436	275	93	203	162	162	162
54	Fondazio ne	25-2 6	0	733	-381	309	92	222	176	176	176
			49	606	-258	293	105	218	174	174	174
			97	722	-376	281	117	213	173	173	173

55	Fondazio ne	25-2 6	0	693	-325	306	116	229	184	184	184
			49	550	-186	295	128	224	182	182	182
			97	677	-315	284	141	223	181	181	181
56	Fondazio ne	25-2 6	0	650	-272	303	137	232	189	189	189
			49	513	-114	293	150	231	188	188	188
			97	630	-256	284	163	229	187	187	187
57	Fondazio ne	25-2 6	0	603	-220	297	157	235	192	192	192
			49	478	-46	291	170	234	191	191	191
			97	579	-199	290	183	233	190	190	190
58	Fondazio ne	25-2 6	0	553	-167	295	176	237	193	193	193
			49	437	24	294	189	236	193	193	193
			97	529	-145	294	192	236	192	192	192
59	Fondazio ne	25-2 6	0	502	-114	297	194	238	194	194	194
			49	394	96	296	194	237	194	194	194
			97	499	-112	296	193	237	193	193	193
60	Fondazio ne	25-2 6	0	463	-73	299	195	239	195	195	195
			49	399	115	299	195	239	195	195	195
			97	533	-143	299	195	239	195	195	195
61	Fondazio ne	25-2 6	0	471	-80	299	195	239	195	195	195
			49	408	53	300	195	240	195	195	195
			97	581	-189	301	193	240	196	196	196
62	Fondazio ne	25-2 6	0	512	-121	300	196	240	196	196	196
			49	428	-17	301	191	240	196	196	196
			97	632	-239	302	178	241	197	197	197
63	Fondazio ne	25-2 6	0	565	-175	299	187	239	195	195	195
			49	481	-89	300	174	241	196	196	196
			97	687	-292	308	161	242	197	197	197
64	Fondazio ne	25-2 6	0	623	-237	296	168	237	193	193	193
			49	553	-164	306	156	239	195	195	195
			97	741	-350	316	143	241	196	196	196
65	Fondazio ne	25-2 6	0	676	-298	300	148	233	189	189	189
			49	618	-237	310	136	235	191	191	191
			97	795	-410	323	124	240	192	192	192
66	Fondazio ne	25-2 6	0	724	-360	299	126	225	182	182	182
			49	670	-302	313	114	230	184	184	184
			97	839	-467	329	102	235	186	186	186
67	Fondazio ne	25-2 6	0	762	-417	297	103	217	173	173	173
			49	708	-359	314	91	223	175	175	175
			97	873	-519	331	79	228	177	177	177
68	Fondazio ne	25-2 6	0	781	-458	291	82	205	161	161	161
			49	724	-397	308	70	211	163	164	164
			97	889	-556	326	58	217	163	166	166
69	Fondazio ne	25-2 6	0	873	-524	327	75	223	173	174	174
			49	837	-483	345	64	229	173	177	177
			97	1011	-651	363	52	236	173	180	180
70	Fondazio ne	25-2 8	0	1782	-1672	131	-62	73	34	53	53
			43	1735	-1625	123	-54	71	36	53	53
			85	1845	-1735	115	-46	70	37	53	53
71	Fondazio ne	25-2 8	0	976	-829	102	-4	78	57	66	66
			43	867	-720	102	4	78	58	66	66
			85	999	-852	102	12	78	60	66	66
72	Fondazio ne	26-2 7	0	487	-373	109	-14	73	49	57	57
			33	498	-384	108	-8	73	50	57	57
			66	560	-447	108	-1	73	51	57	57
73	Fondazio	26-2	0	611	-469	109	35	85	70	71	71

	ne	7									
			33	591	-450	109	42	85	71	71	71
			66	647	-506	108	48	85	71	71	71
74	Fondazio ne	27-2 9	0	564	-590	9	-97	-8	-29	-13	-13
			33	575	-602	3	-91	-10	-28	-13	-13
			66	626	-652	-1	-84	-11	-27	-13	-13
75	Fondazio ne	27-2 9	0	651	-671	-6	-61	-9	-20	-10	-10
			33	618	-639	-6	-55	-9	-19	-10	-10
			66	659	-680	-6	-49	-9	-18	-11	-11
76	Fondazio ne	28-3 0	0	2287	-2359	47	-185	-17	-63	-30	-30
			37	2259	-2331	40	-178	-18	-62	-30	-30
			73	2347	-2419	34	-172	-19	-60	-30	-30
77	Fondazio ne	28-3 0	0	1715	-1750	35	-135	-5	-39	-15	-15
			37	1667	-1702	29	-129	-7	-38	-15	-15
			73	1764	-1799	22	-122	-8	-37	-15	-15
78	Fondazio ne	29-3 1	0	735	-575	117	19	94	74	80	80
			33	731	-572	113	25	93	75	80	80
			66	782	-623	109	32	93	76	80	80
79	Fondazio ne	29-3 1	0	807	-643	114	54	95	82	82	82
			33	771	-608	114	60	95	81	81	81
			66	818	-655	114	67	95	81	81	81
80	Fondazio ne	30-3 2	0	1466	-1467	36	-103	7	-21	-1	-1
			34	1407	-1408	30	-97	5	-20	-1	-1
			69	1500	-1501	24	-90	4	-19	-1	-1
81	Fondazio ne	30-3 2	0	1123	-1121	18	-83	4	-16	0	0
			34	1058	-1057	12	-77	3	-15	0	0
			69	1158	-1156	6	-70	2	-13	0	0
82	Fondazio ne	31-3 3	0	701	-731	-7	-91	-13	-30	-15	-15
			33	673	-703	-12	-85	-14	-29	-15	-15
			66	721	-750	-12	-79	-14	-28	-15	-15
83	Fondazio ne	31-3 3	0	808	-827	-2	-52	-8	-18	-10	-10
			33	744	-763	-2	-46	-8	-17	-10	-10
			66	771	-790	-2	-45	-8	-16	-10	-10
84	Fondazio ne	32-3 4	0	1001	-987	15	-67	8	-8	5	5
			35	939	-928	11	-60	7	-7	5	5
			69	1003	-990	11	-54	7	-6	5	5
85	Fondazio ne	32-3 4	0	861	-855	6	-53	4	-8	3	3
			35	826	-821	6	-47	4	-6	3	3
			69	874	-869	6	-41	4	-5	3	3
86	Fondazio ne	33-3 5	0	833	-691	96	16	82	66	71	71
			33	808	-667	95	22	82	67	71	71
			66	854	-713	95	29	82	68	71	71
87	Fondazio ne	33-3 5	0	917	-760	110	59	91	79	79	79
			33	843	-686	110	62	91	79	79	79
			66	896	-739	110	56	91	79	79	79
88	Fondazio ne	34-3 6	0	863	-849	14	-40	9	-1	7	7
			35	813	-799	14	-34	9	0	7	7
			69	854	-840	13	-27	9	1	7	7
89	Fondazio ne	34-3 6	0	784	-773	11	-26	8	1	6	6
			35	735	-723	11	-31	8	0	6	6
			69	811	-800	11	-37	8	-2	6	6
90	Fondazio ne	35-3 7	0	778	-822	-19	-92	-22	-37	-22	-22
			33	723	-767	-19	-86	-22	-36	-22	-22
			66	746	-790	-19	-80	-22	-34	-22	-22
91	Fondazio ne	35-3 7	0	833	-859	-9	-48	-12	-20	-13	-13

			33	754	-780	-9	-52	-12	-21	-13	-13
			66	796	-822	-9	-59	-12	-22	-13	-13
92	Fondazio ne	36-3 8	0	831	-809	19	-26	14	5	11	11
			35	789	-767	19	-32	14	4	11	11
			69	850	-828	19	-39	14	2	11	11
93	Fondazio ne	36-3 8	0	862	-850	15	-47	9	-3	6	6
			35	826	-814	15	-54	9	-5	6	6
			69	881	-869	15	-60	9	-6	6	6
94	Fondazio ne	37-3 9	0	842	-705	94	21	80	65	69	69
			33	795	-657	94	27	80	66	69	69
			66	837	-699	94	33	80	67	69	69
95	Fondazio ne	37-3 9	0	865	-713	103	61	89	76	76	76
			33	811	-659	103	55	89	76	76	76
			66	856	-704	103	49	89	76	76	76
96	Fondazio ne	38-4 0	0	946	-909	31	-40	23	9	18	18
			34	910	-874	31	-46	23	8	18	18
			69	948	-912	36	-52	24	6	18	18
97	Fondazio ne	38-4 0	0	1202	-1188	26	-70	12	-7	7	7
			34	1110	-1095	33	-77	14	-8	7	7
			69	1190	-1176	39	-83	15	-9	7	7
98	Fondazio ne	39-4 1	0	736	-783	-17	-89	-23	-38	-24	-24
			33	686	-733	-17	-83	-23	-36	-24	-24
			66	705	-753	-16	-77	-23	-35	-24	-24
99	Fondazio ne	39-4 1	0	715	-754	-12	-58	-19	-28	-20	-20
			33	667	-706	-11	-56	-19	-27	-20	-20
			66	677	-716	-11	-62	-18	-29	-20	-20
100	Fondazio ne	40-4 2	0	1447	-1402	59	-60	33	9	23	23
			35	1357	-1312	65	-67	34	8	23	23
			69	1409	-1364	72	-73	36	7	23	23
101	Fondazio ne	40-4 2	0	1894	-1852	81	-83	37	4	21	21
			35	1807	-1764	87	-90	38	3	21	21
			69	1837	-1795	94	-96	39	1	21	21
102	Fondazio ne	41-4 4	0	640	-711	-18	-89	-34	-48	-36	-36
			33	584	-655	-18	-95	-34	-49	-36	-36
			66	576	-647	-18	-101	-34	-50	-36	-36
103	Fondazio ne	41-4 4	0	556	-670	-30	-141	-54	-77	-56	-56
			33	485	-598	-30	-147	-54	-78	-56	-56
			66	480	-593	-30	-153	-54	-79	-56	-56
104	Fondazio ne	42-4 3	0	2189	-2126	114	-84	54	14	32	32
			23	2133	-2069	119	-88	55	13	32	32
			46	2113	-2049	123	-93	56	13	32	32
105	Fondazio ne	43-4 4	0	1448	-939	485	129	328	255	255	255
			49	1321	-818	466	141	321	252	252	252
			97	1341	-844	448	152	314	249	249	249
106	Fondazio ne	43-4 4	0	1245	-790	427	118	292	227	227	227
			49	1129	-679	409	129	286	225	225	225
			97	1163	-719	391	141	280	222	222	222
107	Fondazio ne	43-4 4	0	1115	-684	391	120	274	215	215	215
			49	997	-572	374	131	269	213	213	213
			97	1043	-622	357	143	263	210	210	210
108	Fondazio ne	43-4 4	0	1049	-618	375	136	271	216	216	216
			49	919	-492	358	148	266	213	213	213
			97	965	-542	345	160	261	211	211	211
109	Fondazio ne	43-4 4	0	960	-527	359	152	269	217	217	217
			49	820	-391	348	164	264	215	215	215

			97	879	-452	337	176	262	213	213	213
110	Fondazio ne	43-4 4	0	869	-434	349	169	267	218	218	218
			49	720	-288	339	182	265	216	216	216
			97	794	-364	328	194	263	215	215	215
111	Fondazio ne	43-4 4	0	775	-340	338	186	267	218	218	218
			49	619	-186	328	199	265	216	216	216
			97	710	-279	324	211	264	215	215	215
112	Fondazio ne	43-4 4	0	681	-248	327	202	265	217	217	217
			49	545	-83	326	215	264	216	216	216
			97	626	-196	325	215	263	215	215	215
113	Fondazio ne	43-4 4	0	602	-172	325	215	263	215	215	215
			49	497	17	325	214	263	214	214	214
			97	550	-122	324	214	262	214	214	214
114	Fondazio ne	43-4 4	0	528	-102	323	213	261	213	213	213
			49	455	100	323	213	261	213	213	213
			97	508	-83	323	213	261	213	213	213
115	Fondazio ne	43-4 4	0	487	-58	321	211	258	211	211	211
			49	411	81	321	211	259	211	211	211
			97	558	-135	322	212	259	212	212	212
116	Fondazio ne	43-4 4	0	535	-117	317	209	256	209	209	209
			49	446	-3	318	209	256	209	209	209
			97	622	-202	319	197	257	210	210	210
117	Fondazio ne	43-4 4	0	599	-188	312	202	252	205	205	205
			49	504	-92	313	189	253	206	206	206
			97	692	-277	320	177	254	207	207	207
118	Fondazio ne	43-4 4	0	664	-263	304	180	246	200	200	200
			49	586	-182	314	167	247	202	202	202
			97	760	-354	324	155	249	203	203	203
119	Fondazio ne	43-4 4	0	727	-340	304	156	238	194	194	194
			49	663	-273	314	144	240	195	195	195
			97	822	-429	325	131	244	197	197	197
120	Fondazio ne	43-4 4	0	781	-412	300	132	227	185	185	185
			49	729	-356	311	119	232	186	186	186
			97	872	-495	328	107	237	188	188	188
121	Fondazio ne	43-4 4	0	826	-476	295	108	219	175	175	175
			49	781	-427	312	96	224	177	177	177
			97	908	-549	329	84	230	179	179	179
122	Fondazio ne	43-4 4	0	861	-528	294	89	211	167	167	167
			49	812	-474	311	77	216	169	169	169
			97	924	-581	329	65	222	169	172	172
123	Fondazio ne	43-4 4	0	949	-600	322	79	223	174	175	175
			49	914	-560	340	67	229	174	177	177
			97	1010	-650	358	55	235	174	180	180
124	Fondazio ne	43-4 5	0	1314	-1116	157	36	120	96	99	99
			33	1231	-1033	163	30	122	95	99	99
			66	1294	-1095	169	24	123	94	99	99
125	Fondazio ne	43-4 5	0	2002	-1796	192	9	130	93	103	103
			33	1920	-1715	198	3	131	92	103	103
			66	1933	-1726	205	-3	133	91	103	103
126	Fondazio ne	44-4 6	0	573	-478	94	15	61	45	47	47
			33	511	-416	94	9	61	44	47	47
			66	560	-465	95	2	61	43	47	47
127	Fondazio ne	44-4 6	0	655	-501	117	21	92	72	77	77
			33	610	-456	119	15	92	71	77	77
			66	629	-475	125	8	93	70	77	77

128	Fondazio ne	45-4 7	0	889	-849	49	-43	29	11	20	20
			33	792	-752	55	-49	31	10	20	20
			66	878	-838	61	-55	32	9	20	20
129	Fondazio ne	45-4 7	0	1661	-1593	103	-59	53	21	34	34
			33	1578	-1509	109	-65	54	19	34	34
			66	1621	-1552	116	-71	56	18	35	35
130	Fondazio ne	46-4 8	0	531	-543	13	-36	-1	-11	-6	-6
			33	480	-492	14	-42	-1	-12	-6	-6
			66	516	-528	14	-48	0	-13	-6	-6
131	Fondazio ne	46-4 8	0	623	-580	46	-34	30	14	21	21
			33	582	-540	52	-40	31	13	21	21
			66	564	-521	58	-47	33	12	21	21
132	Fondazio ne	47-4 9	0	916	-650	195	106	159	133	133	133
			33	811	-544	199	99	159	133	133	133
			66	882	-615	203	93	159	134	134	134
133	Fondazio ne	47-4 9	0	1662	-1359	245	98	185	152	152	152
			33	1574	-1269	252	92	186	152	152	152
			66	1603	-1298	259	86	188	153	153	153
134	Fondazio ne	48-5 0	0	622	-356	175	121	144	121	121	121
			33	549	-306	175	122	144	122	122	122
			66	577	-334	176	121	144	122	122	122
135	Fondazio ne	48-5 0	0	659	-355	208	138	176	148	148	148
			33	589	-293	212	132	176	148	148	148
			66	591	-295	216	126	176	148	148	148
136	Fondazio ne	49-5 1	0	760	-633	108	36	82	64	64	64
			33	646	-517	113	30	83	64	64	64
			66	706	-577	118	24	84	65	65	65
137	Fondazio ne	49-5 1	0	1502	-1328	168	37	114	87	87	87
			33	1414	-1239	174	31	116	87	87	87
			66	1425	-1249	181	25	118	87	88	88
138	Fondazio ne	50-5 2	0	517	-360	92	44	70	54	54	54
			33	389	-269	93	50	70	55	55	55
			66	469	-312	93	55	70	55	55	55
139	Fondazio ne	50-5 2	0	558	-333	130	84	105	84	84	84
			33	389	-221	131	84	106	84	84	84
			66	412	-243	131	81	106	85	85	85
140	Fondazio ne	51-5 3	0	837	-474	246	171	205	171	171	171
			33	710	-354	251	172	206	172	172	172
			66	752	-404	255	172	207	172	172	172
141	Fondazio ne	51-5 3	0	1583	-1197	296	187	231	193	193	193
			33	1493	-1107	301	181	233	193	193	193
			66	1487	-1099	306	175	235	194	194	194
142	Fondazio ne	52-5 4	0	599	-346	148	95	118	95	95	95
			33	407	-217	149	95	118	95	95	95
			66	403	-212	150	90	119	95	95	95
143	Fondazio ne	52-5 4	0	699	-408	176	112	139	112	112	112
			33	503	-266	180	112	140	112	112	112
			66	452	-227	184	106	140	113	113	113
144	Fondazio ne	53-5 5	0	713	-503	148	91	116	91	91	91
			33	576	-375	150	92	117	92	92	92
			66	612	-419	151	93	118	93	93	93
145	Fondazio ne	53-5 5	0	1371	-1182	164	94	121	94	94	94
			33	1280	-1089	169	95	123	95	95	95
			66	1292	-1099	176	93	125	96	96	96
146	Fondazio	54-5	0	789	-495	181	111	139	111	111	111

	ne	6									
			33	598	-317	185	111	139	111	111	111
			66	487	-264	190	106	141	112	112	112
147	Fondazio ne	54-5 6	0	904	-633	185	104	134	104	104	104
			33	720	-457	192	98	136	105	105	105
			66	567	-344	198	92	138	106	106	106
148	Fondazio ne	55-5 7	0	712	-440	164	114	135	114	114	114
			40	537	-275	165	115	136	115	115	115
			80	629	-377	167	117	138	117	117	117
149	Fondazio ne	55-5 7	0	1318	-1088	185	106	140	115	115	115
			40	1206	-973	195	100	143	116	116	116
			80	1295	-1059	204	93	147	118	118	118
150	Fondazio ne	56-7 0	0	681	-377	171	120	141	120	120	120
			40	476	-171	172	121	143	121	121	121
			80	429	-167	177	122	144	122	122	122
151	Fondazio ne	56-7 0	0	755	-496	188	100	140	114	114	114
			40	494	-241	196	94	143	115	115	115
			80	510	-243	205	87	145	116	116	116
152	Fondazio ne	57-5 8	0	392	-628	17	-193	-48	-90	-60	-60
			42	487	-653	5	-180	-50	-87	-60	-60
			83	674	-793	-7	-167	-52	-84	-60	-60
153	Fondazio ne	57-5 8	0	682	-822	-23	-142	-51	-75	-53	-53
			42	683	-829	-36	-129	-52	-72	-52	-52
			83	756	-903	-48	-116	-52	-69	-52	-52
154	Fondazio ne	58-5 9	0	1169	-1496	-76	-287	-133	-175	-139	-139
			35	1170	-1506	-86	-276	-135	-173	-139	-139
			69	1183	-1528	-96	-266	-137	-171	-139	-139
155	Fondazio ne	58-5 9	0	1156	-1371	-49	-208	-89	-120	-95	-95
			35	1154	-1379	-60	-198	-91	-118	-95	-95
			69	1165	-1400	-70	-188	-93	-117	-95	-95
156	Fondazio ne	59-6 0	0	1153	-1286	-26	-151	-54	-79	-61	-61
			35	1140	-1282	-36	-141	-57	-77	-61	-61
			69	1151	-1303	-46	-130	-59	-76	-61	-61
157	Fondazio ne	59-6 0	0	1143	-1207	-11	-98	-27	-45	-33	-33
			35	1119	-1193	-21	-88	-29	-43	-33	-33
			69	1131	-1212	-31	-78	-32	-41	-33	-33
158	Fondazio ne	60-6 1	0	1131	-1149	-1	-53	-6	-16	-11	-11
			35	1096	-1124	-3	-43	-6	-14	-11	-11
			69	1105	-1134	-3	-33	-7	-13	-11	-11
159	Fondazio ne	60-6 1	0	1131	-1142	12	-16	6	-1	-1	-1
			35	1091	-1115	11	-26	6	-2	-1	-1
			69	1101	-1126	11	-37	6	-4	-1	-1
160	Fondazio ne	61-6 2	0	1156	-1041	115	15	88	67	71	71
			35	1156	-973	105	25	85	69	71	71
			69	1159	-986	98	35	84	70	70	70
161	Fondazio ne	61-6 2	0	1139	-980	108	60	95	80	80	80
			35	1093	-919	107	70	95	79	79	79
			69	1085	-920	107	72	95	79	79	79
162	Fondazio ne	62-6 3	0	1063	-1033	96	-42	54	26	35	35
			35	1070	-941	86	-32	51	28	34	34
			69	1075	-955	76	-22	49	30	34	34
163	Fondazio ne	62-6 3	0	1020	-953	79	-4	57	40	42	42
			35	989	-867	73	6	57	42	42	42
			69	992	-879	70	16	56	42	42	42
164	Fondazio ne	63-6 4	0	987	-898	75	20	61	46	46	46

			35	922	-808	75	30	61	46	46	46
			69	913	-809	75	41	61	46	46	46
165	Fondazio ne	63-6 4	0	961	-846	76	42	62	47	47	47
			35	893	-771	76	32	62	47	47	47
			69	881	-771	76	22	62	47	47	47
166	Fondazio ne	64-6 5	0	942	-851	73	19	59	45	45	45
			35	883	-794	77	9	60	45	45	45
			69	875	-769	83	-1	60	43	45	45
167	Fondazio ne	64-6 5	0	971	-894	82	-16	54	35	39	39
			35	921	-843	92	-26	56	33	39	39
			69	897	-801	103	-36	59	31	39	39
168	Fondazio ne	65-6 6	0	896	-711	114	79	101	84	84	84
			35	828	-630	114	77	101	84	84	84
			69	796	-602	115	67	101	85	85	85
169	Fondazio ne	65-6 6	0	891	-737	108	44	92	77	77	77
			35	831	-676	115	34	93	77	77	77
			69	802	-626	125	24	96	75	78	78
170	Fondazio ne	66-6 7	0	740	-752	20	-28	13	3	5	5
			35	671	-672	20	-17	14	5	5	5
			69	644	-633	21	-7	14	6	6	6
171	Fondazio ne	66-6 7	0	698	-717	4	-26	0	-6	-6	-6
			35	640	-651	5	-36	0	-8	-6	-6
			69	594	-604	7	-46	1	-10	-5	-5
172	Fondazio ne	67-6 8	0	713	-763	-20	-66	-22	-31	-25	-25
			35	642	-691	-9	-76	-19	-33	-24	-24
			69	587	-636	1	-86	-17	-34	-24	-24
173	Fondazio ne	67-6 8	0	749	-850	-32	-116	-47	-63	-50	-50
			35	641	-741	-21	-126	-44	-65	-50	-50
			69	585	-685	-11	-137	-42	-67	-50	-50
174	Fondazio ne	68-6 9	0	776	-944	-55	-173	-81	-104	-84	-84
			35	623	-791	-45	-183	-78	-106	-84	-84
			69	566	-734	-35	-194	-76	-108	-84	-84
175	Fondazio ne	68-6 9	0	811	-1066	-81	-250	-123	-157	-128	-128
			35	660	-915	-71	-260	-121	-159	-127	-127
			69	566	-821	-60	-270	-119	-161	-127	-127
176	Fondazio ne	69-7 0	0	669	-766	-41	-110	-48	-64	-48	-48
			42	447	-543	-29	-123	-48	-67	-48	-48
			83	350	-446	-17	-136	-45	-69	-48	-48
177	Fondazio ne	69-7 0	0	688	-807	-7	-166	-52	-84	-59	-59
			42	481	-600	5	-179	-50	-87	-60	-60
			83	377	-499	18	-192	-47	-89	-60	-60
178	Primo Impalcat o	1-2	0	1821	-676	773	464	625	538	538	538
			83	1821	-676	773	464	625	538	538	538
			166	1821	-676	773	464	625	538	538	538
179	Primo Impalcat o	1-15	0	3104	-3095	419	-204	223	99	167	167
			80	3104	-3095	419	-204	223	99	167	167
			159	3104	-3095	419	-204	223	99	167	167
180	Primo Impalcat o	2-3	0	2106	-1103	635	409	521	447	447	447
			69	2106	-1103	635	409	521	447	447	447
			138	2106	-1103	635	409	521	447	447	447
181	Primo Impalcat o	3-4	0	1793	-789	634	410	520	447	447	447
			69	1793	-789	634	410	520	447	447	447

			138	1793	-789	634	410	520	447	447	447
182	Primo Impalcato	4-5	0	1499	-494	632	411	519	446	446	446
			69	1499	-494	632	411	519	446	446	446
			138	1499	-494	632	411	519	446	446	446
183	Primo Impalcato	5-6	0	1489	-368	632	412	519	445	445	445
			69	1489	-368	632	412	519	445	445	445
			138	1489	-368	632	412	519	445	445	445
184	Primo Impalcato	6-7	0	1444	-145	746	545	630	545	545	545
			69	1444	-145	746	545	630	545	545	545
			138	1444	-145	746	545	630	545	545	545
185	Primo Impalcato	7-8	0	1185	-141	608	428	499	428	428	428
			69	1185	-141	608	428	499	428	428	428
			138	1185	-141	608	428	499	428	428	428
186	Primo Impalcato	8-9	0	1406	-404	608	428	499	428	428	428
			69	1406	-404	608	428	499	428	428	428
			138	1406	-404	608	428	499	428	428	428
187	Primo Impalcato	9-10	0	1425	-163	762	559	645	559	559	559
			69	1425	-163	762	559	645	559	559	559
			138	1425	-163	762	559	645	559	559	559
188	Primo Impalcato	10-11	0	1195	-173	650	426	537	461	461	461
			69	1195	-173	650	426	537	461	461	461
			138	1195	-173	650	426	537	461	461	461
189	Primo Impalcato	11-12	0	1495	-484	652	425	538	461	461	461
			69	1495	-484	652	425	538	461	461	461
			138	1495	-484	652	425	538	461	461	461
190	Primo Impalcato	12-13	0	1927	-807	654	424	538	462	462	462
			69	1927	-807	654	424	538	462	462	462
			138	1927	-807	654	424	538	462	462	462
191	Primo Impalcato	13-14	0	1832	-535	794	478	641	552	552	552
			83	1832	-535	794	478	641	552	552	552
			166	1832	-535	794	478	641	552	552	552
192	Primo Impalcato	14-16	0	933	-662	340	-133	202	108	162	162
			80	933	-662	340	-133	202	108	162	162
			159	933	-662	340	-133	202	108	162	162
193	Primo Impalcato	15-17	0	2002	-2392	180	-335	46	-57	24	24
			66	2002	-2392	180	-335	46	-57	24	24
			132	2002	-2392	180	-335	46	-57	24	24
194	Primo Impalcato	16-18	0	811	-787	103	-276	19	-56	12	12
			66	811	-787	103	-276	19	-56	12	12
			132	811	-787	103	-276	19	-56	12	12
195	Primo Impalcato	17-19	0	1463	-1557	256	-151	153	72	133	133
			66	1463	-1557	256	-151	153	72	133	133
			132	1463	-1557	256	-151	153	72	133	133
196	Primo Impalcato	18-20	0	887	-675	218	-157	129	54	114	114

			66	887	-675	218	-157	129	54	114	114
			132	887	-675	218	-157	129	54	114	114
197	Primo Impalcato	19-21	0	752	-1077	18	-274	-19	-85	-19	-19
			66	752	-1077	18	-274	-19	-85	-19	-19
			132	752	-1077	18	-274	-19	-85	-19	-19
198	Primo Impalcato	20-22	0	796	-1083	-9	-309	-45	-114	-45	-45
			66	796	-1083	-9	-309	-45	-114	-45	-45
			132	796	-1083	-9	-309	-45	-114	-45	-45
199	Primo Impalcato	21-23	0	1366	-1063	167	-21	139	102	136	136
			66	1366	-1063	167	-21	139	102	136	136
			132	1366	-1063	167	-21	139	102	136	136
200	Primo Impalcato	22-24	0	906	-929	127	-110	92	44	91	91
			66	906	-929	127	-110	92	44	91	91
			132	906	-929	127	-110	92	44	91	91
201	Primo Impalcato	23-25	0	2001	-2006	10	-116	9	-27	9	9
			66	2001	-2006	10	-116	9	-27	9	9
			132	2001	-2006	10	-116	9	-27	9	9
202	Primo Impalcato	24-26	0	784	-1011	-43	-235	-43	-97	-43	-43
			66	784	-1011	-43	-235	-43	-97	-43	-43
			132	784	-1011	-43	-235	-43	-97	-43	-43
203	Primo Impalcato	25-28	0	3977	-3591	240	71	205	172	193	193
			85	3977	-3591	240	71	205	172	193	193
			170	3977	-3591	240	71	205	172	193	193
204	Primo Impalcato	26-27	0	949	-794	87	-43	87	55	87	87
			66	949	-794	87	-43	87	55	87	87
			132	949	-794	87	-43	87	55	87	87
205	Primo Impalcato	27-29	0	818	-1031	-52	-174	-52	-91	-52	-52
			66	818	-1031	-52	-174	-52	-91	-52	-52
			132	818	-1031	-52	-174	-52	-91	-52	-52
206	Primo Impalcato	28-30	0	5585	-5599	83	-261	5	-64	-2	-2
			73	5585	-5599	83	-261	5	-64	-2	-2
			146	5585	-5599	83	-261	5	-64	-2	-2
207	Primo Impalcato	29-31	0	1009	-987	75	-14	75	52	75	75
			66	1009	-987	75	-14	75	52	75	75
			132	1009	-987	75	-14	75	52	75	75
208	Primo Impalcato	30-32	0	4257	-4309	24	-240	-16	-73	-16	-16
			69	4257	-4309	24	-240	-16	-73	-16	-16
			137	4257	-4309	24	-240	-16	-73	-16	-16
209	Primo Impalcato	31-33	0	926	-1221	-48	-190	-48	-91	-48	-48
			66	926	-1221	-48	-190	-48	-91	-48	-48
			132	926	-1221	-48	-190	-48	-91	-48	-48
210	Primo Impalcato	32-34	0	2943	-3036	-32	-221	-32	-82	-32	-32
			69	2943	-3036	-32	-221	-32	-82	-32	-32
			138	2943	-3036	-32	-221	-32	-82	-32	-32
211	Primo Impalcato	33-35	0	1132	-1145	113	-44	100	68	100	100

	o										
			66	1132	-1145	113	-44	100	68	100	100
			132	1132	-1145	113	-44	100	68	100	100
212	Primo Impalcato	34-36	0	1624	-1763	-48	-203	-48	-94	-48	-48
			69	1624	-1763	-48	-203	-48	-94	-48	-48
			138	1624	-1763	-48	-203	-48	-94	-48	-48
213	Primo Impalcato	35-37	0	1057	-1372	4	-212	-15	-65	-15	-15
			66	1057	-1372	4	-212	-15	-65	-15	-15
			132	1057	-1372	4	-212	-15	-65	-15	-15
214	Primo Impalcato	36-38	0	641	-775	-67	-188	-67	-108	-67	-67
			69	641	-775	-67	-188	-67	-108	-67	-67
			138	641	-775	-67	-188	-67	-108	-67	-67
215	Primo Impalcato	37-39	0	1314	-1319	238	-55	165	107	146	146
			66	1314	-1319	238	-55	165	107	146	146
			132	1314	-1319	238	-55	165	107	146	146
216	Primo Impalcato	38-40	0	1446	-1732	-87	-227	-87	-134	-87	-87
			69	1446	-1732	-87	-227	-87	-134	-87	-87
			137	1446	-1732	-87	-227	-87	-134	-87	-87
217	Primo Impalcato	39-41	0	1240	-1596	116	-249	29	-44	17	17
			66	1240	-1596	116	-249	29	-44	17	17
			132	1240	-1596	116	-249	29	-44	17	17
218	Primo Impalcato	40-42	0	2772	-3050	-109	-296	-109	-168	-109	-109
			69	2772	-3050	-109	-296	-109	-168	-109	-109
			138	2772	-3050	-109	-296	-109	-168	-109	-109
219	Primo Impalcato	41-44	0	895	-1101	95	-166	47	-6	41	41
			66	895	-1101	95	-166	47	-6	41	41
			132	895	-1101	95	-166	47	-6	41	41
220	Primo Impalcato	42-43	0	4066	-4341	-133	-368	-133	-203	-133	-133
			23	4066	-4341	-133	-368	-133	-203	-133	-133
			46	4066	-4341	-133	-368	-133	-203	-133	-133
221	Primo Impalcato	43-45	0	3226	-3251	19	-123	19	-22	19	19
			66	3226	-3251	19	-123	19	-22	19	19
			132	3226	-3251	19	-123	19	-22	19	19
222	Primo Impalcato	44-46	0	1116	-1034	285	-46	197	131	171	171
			66	1116	-1034	285	-46	197	131	171	171
			132	1116	-1034	285	-46	197	131	171	171
223	Primo Impalcato	45-47	0	2196	-2610	-114	-255	-114	-164	-114	-114
			66	2196	-2610	-114	-255	-114	-164	-114	-114
			132	2196	-2610	-114	-255	-114	-164	-114	-114
224	Primo Impalcato	46-48	0	1046	-1341	155	-255	52	-30	34	34
			66	1046	-1341	155	-255	52	-30	34	34
			132	1046	-1341	155	-255	52	-30	34	34
225	Primo Impalcato	47-49	0	1486	-1637	44	-123	44	-1	44	44
			66	1486	-1637	44	-123	44	-1	44	44
			132	1486	-1637	44	-123	44	-1	44	44
226	Primo	48-5	0	1260	-1228	361	-116	217	122	178	178

	Impalcat o	0									
			66	1260	-1228	361	-116	217	122	178	178
			132	1260	-1228	361	-116	217	122	178	178
227	Primo Impalcat o	49-5 1	0	698	-864	-75	-343	-83	-155	-83	-83
			66	698	-864	-75	-343	-83	-155	-83	-83
			132	698	-864	-75	-343	-83	-155	-83	-83
228	Primo Impalcat o	50-5 2	0	1100	-1003	230	-339	68	-46	37	37
			66	1100	-1003	230	-339	68	-46	37	37
			132	1100	-1003	230	-339	68	-46	37	37
229	Primo Impalcat o	51-5 3	0	1038	-858	191	-197	100	23	88	88
			66	1038	-858	191	-197	100	23	88	88
			132	1038	-858	191	-197	100	23	88	88
230	Primo Impalcat o	52-5 4	0	712	-672	176	-280	58	-33	39	39
			66	712	-672	176	-280	58	-33	39	39
			132	712	-672	176	-280	58	-33	39	39
231	Primo Impalcat o	53-5 5	0	1811	-1674	134	-367	8	-92	-7	-7
			66	1811	-1674	134	-367	8	-92	-7	-7
			132	1811	-1674	134	-367	8	-92	-7	-7
232	Primo Impalcat o	54-5 6	0	653	-599	115	-257	35	-39	27	27
			66	653	-599	115	-257	35	-39	27	27
			132	653	-599	115	-257	35	-39	27	27
233	Primo Impalcat o	55-5 7	0	2857	-2508	395	-221	204	81	151	151
			80	2857	-2508	395	-221	204	81	151	151
			159	2857	-2508	395	-221	204	81	151	151
234	Primo Impalcat o	56-7 0	0	826	-459	322	-53	216	141	183	183
			80	826	-459	322	-53	216	141	183	183
			159	826	-459	322	-53	216	141	183	183
235	Primo Impalcat o	57-5 8	0	1838	-644	777	466	628	541	541	541
			83	1840	-644	777	466	628	541	541	541
			166	1842	-644	777	466	628	541	541	541
236	Primo Impalcat o	58-5 9	0	2086	-993	645	417	529	454	454	454
			69	2086	-993	645	417	529	454	454	454
			138	2086	-993	645	417	529	454	454	454
237	Primo Impalcat o	59-6 0	0	1835	-746	644	419	529	454	454	454
			69	1835	-746	644	419	529	454	454	454
			138	1835	-746	644	419	529	454	454	454
238	Primo Impalcat o	60-6 1	0	1590	-505	642	420	528	453	453	453
			69	1590	-505	642	420	528	453	453	453
			138	1590	-505	642	420	528	453	453	453
239	Primo Impalcat o	61-6 2	0	1619	-345	758	554	640	554	554	554
			69	1619	-345	758	554	640	554	554	554
			138	1619	-345	758	554	640	554	554	554
240	Primo Impalcat o	62-6 3	0	1393	-398	604	424	496	424	424	424
			69	1393	-398	604	424	496	424	424	424
			138	1393	-398	604	424	496	424	424	424

241	Primo Impalcato	63-64	0	1183	-190	604	424	496	424	424	424
			69	1183	-190	604	424	496	424	424	424
			138	1183	-190	604	424	496	424	424	424
242	Primo Impalcato	64-65	0	1299	-326	604	425	496	425	425	425
			69	1299	-326	604	425	496	425	425	425
			138	1299	-326	604	425	496	425	425	425
243	Primo Impalcato	65-66	0	1399	-97	761	558	644	558	558	558
			69	1399	-97	761	558	644	558	558	558
			138	1399	-97	761	558	644	558	558	558
244	Primo Impalcato	66-67	0	1246	-149	649	426	536	460	460	460
			69	1246	-149	649	426	536	460	460	460
			138	1246	-149	649	426	536	460	460	460
245	Primo Impalcato	67-68	0	1507	-529	651	425	537	460	460	460
			69	1507	-529	651	425	537	460	460	460
			138	1507	-529	651	425	537	460	460	460
246	Primo Impalcato	68-69	0	1843	-920	653	424	538	461	461	461
			69	1843	-920	653	424	538	461	461	461
			138	1843	-920	653	424	538	461	461	461
247	Primo Impalcato	69-70	0	1740	-635	794	479	642	553	553	553
			83	1740	-635	794	479	642	553	553	553
			166	1740	-635	794	479	642	553	553	553
248	Primo Impalcato	1-1	0	7793	-10148	-933	-1690	-1130	-1344	-1130	-1130
			188	7706	-10235	-1019	-1777	-1217	-1431	-1217	-1217
			376	7619	-10322	-1106	-1864	-1304	-1518	-1304	-1304
249	Primo Impalcato	2-2	0	-290	-2867	-1428	-1765	-1428	-1550	-1428	-1428
			188	-328	-2905	-1466	-1803	-1466	-1588	-1466	-1466
			376	-366	-2943	-1503	-1841	-1503	-1626	-1503	-1503
250	Primo Impalcato	3-3	0	-685	-2073	-1287	-1499	-1287	-1393	-1287	-1287
			188	-723	-2111	-1325	-1537	-1325	-1431	-1325	-1325
			376	-761	-2150	-1363	-1575	-1363	-1469	-1363	-1363
251	Primo Impalcato	4-4	0	-712	-1861	-1164	-1334	-1164	-1257	-1164	-1164
			188	-750	-1910	-1202	-1372	-1202	-1295	-1202	-1202
			376	-788	-1960	-1240	-1410	-1240	-1333	-1240	-1240
252	Primo Impalcato	5-5	0	-759	-1668	-1040	-1202	-1040	-1122	-1040	-1040
			188	-797	-1717	-1078	-1240	-1078	-1160	-1078	-1078
			376	-835	-1766	-1116	-1278	-1116	-1198	-1116	-1116
253	Primo Impalcato	6-6	0	-150	-1653	-832	-1164	-902	-1002	-902	-902
			188	-188	-1691	-870	-1202	-939	-1040	-939	-939
			376	-226	-1729	-908	-1240	-977	-1078	-977	-977
254	Primo Impalcato	7-7	0	-101	-1702	-793	-1152	-879	-982	-879	-879
			188	-139	-1740	-831	-1190	-917	-1019	-917	-917
			376	-177	-1778	-869	-1228	-955	-1057	-955	-955
255	Primo Impalcato	8-8	0	-850	-1490	-925	-1066	-925	-998	-925	-925
			188	-888	-1539	-963	-1104	-963	-1036	-963	-963

			376	-926	-1589	-1001	-1142	-1001	-1074	-1001	-1001
256	Primo Impalcato	9-9	0	-26	-1766	-790	-1194	-896	-1004	-896	-896
			188	-64	-1803	-828	-1232	-934	-1042	-934	-934
			376	-102	-1841	-866	-1270	-972	-1079	-972	-972
257	Primo Impalcato	10-10	0	-211	-1706	-900	-1214	-954	-1054	-954	-954
			188	-249	-1743	-938	-1252	-991	-1092	-991	-991
			376	-287	-1781	-976	-1290	-1029	-1130	-1029	-1029
258	Primo Impalcato	11-11	0	-713	-1811	-1134	-1327	-1134	-1224	-1134	-1134
			188	-750	-1860	-1172	-1365	-1172	-1262	-1172	-1172
			376	-788	-1909	-1210	-1403	-1210	-1300	-1210	-1210
259	Primo Impalcato	12-12	0	-699	-2048	-1286	-1498	-1286	-1391	-1286	-1286
			188	-737	-2097	-1324	-1536	-1324	-1429	-1324	-1324
			376	-775	-2147	-1361	-1574	-1361	-1467	-1361	-1361
260	Primo Impalcato	13-13	0	-233	-2607	-1420	-1746	-1420	-1542	-1420	-1420
			188	-271	-2645	-1458	-1783	-1458	-1580	-1458	-1458
			376	-309	-2683	-1496	-1821	-1496	-1617	-1496	-1496
261	Primo Impalcato	14-14	0	820	-3203	-1036	-1640	-1150	-1352	-1150	-1150
			188	733	-3290	-1123	-1727	-1237	-1439	-1237	-1237
			376	647	-3377	-1210	-1814	-1324	-1526	-1324	-1324
262	Primo Impalcato	15-15	0	183	-4982	-2169	-2722	-2169	-2417	-2169	-2169
			188	120	-5046	-2232	-2785	-2232	-2480	-2232	-2232
			376	57	-5109	-2295	-2848	-2295	-2543	-2295	-2295
263	Primo Impalcato	16-16	0	152	-4514	-2181	-2739	-2181	-2429	-2181	-2181
			188	88	-4577	-2244	-2802	-2244	-2492	-2244	-2244
			376	25	-4641	-2308	-2865	-2308	-2556	-2308	-2308
264	Primo Impalcato	17-17	0	935	-6555	-2389	-3130	-2389	-2702	-2389	-2389
			188	872	-6619	-2453	-3193	-2453	-2765	-2453	-2453
			376	809	-6682	-2516	-3256	-2516	-2828	-2516	-2516
265	Primo Impalcato	18-18	0	102	-4940	-2419	-3154	-2419	-2734	-2419	-2419
			188	38	-5003	-2482	-3217	-2482	-2798	-2482	-2482
			376	-25	-5066	-2545	-3280	-2545	-2861	-2545	-2545
266	Primo Impalcato	19-19	0	289	-5942	-2484	-3240	-2484	-2827	-2484	-2484
			188	226	-6005	-2548	-3303	-2548	-2891	-2548	-2548
			376	163	-6068	-2611	-3366	-2611	-2954	-2611	-2611
267	Primo Impalcato	20-20	0	222	-5279	-2503	-3249	-2503	-2848	-2503	-2503
			188	159	-5342	-2567	-3312	-2567	-2911	-2567	-2567
			376	96	-5405	-2630	-3375	-2630	-2974	-2630	-2630
268	Primo Impalcato	21-21	0	-460	-5643	-2576	-3365	-2576	-2947	-2576	-2576
			188	-523	-5706	-2639	-3428	-2639	-3010	-2639	-2639
			376	-586	-5769	-2702	-3491	-2702	-3073	-2702	-2702
269	Primo Impalcato	22-22	0	-338	-5359	-2613	-3418	-2613	-2991	-2613	-2613
			188	-401	-5422	-2676	-3481	-2676	-3054	-2676	-2676
			376	-464	-5485	-2739	-3544	-2739	-3117	-2739	-2739
270	Primo Impalcato	23-23	0	1017	-7298	-2734	-3634	-2734	-3140	-2734	-2734

			188	954	-7362	-2797	-3697	-2797	-3203	-2797	-2797
			376	891	-7425	-2861	-3760	-2861	-3266	-2861	-2861
271	Primo Impalcato	24-24	0	-198	-5958	-2733	-3609	-2733	-3138	-2733	-2733
			188	-261	-6022	-2796	-3672	-2796	-3201	-2796	-2796
			376	-325	-6085	-2859	-3735	-2859	-3264	-2859	-2859
272	Primo Impalcato	25-25	0	175	-6682	-3015	-3939	-3015	-3451	-3015	-3015
			188	112	-6746	-3078	-4002	-3078	-3514	-3078	-3078
			376	49	-6809	-3141	-4065	-3141	-3577	-3141	-3141
273	Primo Impalcato	26-26	0	-48	-5996	-2855	-3749	-2855	-3277	-2855	-2855
			188	-111	-6059	-2918	-3812	-2918	-3340	-2918	-2918
			376	-174	-6122	-2981	-3875	-2981	-3403	-2981	-2981
274	Primo Impalcato	27-27	0	398	-6036	-2713	-3573	-2713	-3114	-2713	-2713
			188	335	-6099	-2776	-3636	-2776	-3177	-2776	-2776
			376	272	-6163	-2839	-3699	-2839	-3240	-2839	-2839
275	Primo Impalcato	28-28	0	1107	-7914	-2972	-3916	-2972	-3399	-2972	-2972
			188	1044	-7977	-3035	-3979	-3035	-3462	-3035	-3035
			376	980	-8040	-3098	-4042	-3098	-3526	-3098	-3098
276	Primo Impalcato	29-29	0	426	-5703	-2638	-3464	-2638	-3026	-2638	-2638
			188	363	-5766	-2702	-3527	-2702	-3089	-2702	-2702
			376	299	-5829	-2765	-3590	-2765	-3152	-2765	-2765
277	Primo Impalcato	30-30	0	339	-6362	-3012	-3944	-3012	-3448	-3012	-3012
			188	275	-6425	-3075	-4007	-3075	-3511	-3075	-3075
			376	212	-6488	-3138	-4070	-3138	-3574	-3138	-3138
278	Primo Impalcato	31-31	0	563	-5781	-2609	-3430	-2609	-2991	-2609	-2609
			188	500	-5844	-2672	-3493	-2672	-3054	-2672	-2672
			376	437	-5907	-2735	-3556	-2735	-3117	-2735	-2735
279	Primo Impalcato	32-32	0	217	-6248	-3016	-3950	-3016	-3452	-3016	-3016
			188	154	-6311	-3079	-4013	-3079	-3515	-3079	-3079
			376	90	-6374	-3142	-4076	-3142	-3578	-3142	-3142
280	Primo Impalcato	33-33	0	275	-5498	-2611	-3427	-2611	-2992	-2611	-2611
			188	212	-5561	-2675	-3490	-2675	-3055	-2675	-2675
			376	149	-5624	-2738	-3553	-2738	-3119	-2738	-2738
281	Primo Impalcato	34-34	0	-37	-6049	-3043	-3988	-3043	-3484	-3043	-3043
			188	-100	-6112	-3106	-4052	-3106	-3547	-3106	-3106
			376	-163	-6175	-3169	-4115	-3169	-3610	-3169	-3169
282	Primo Impalcato	35-35	0	428	-5668	-2620	-3441	-2620	-3002	-2620	-2620
			188	365	-5731	-2683	-3505	-2683	-3065	-2683	-2683
			376	302	-5794	-2746	-3568	-2746	-3128	-2746	-2746
283	Primo Impalcato	36-36	0	49	-6186	-3069	-4031	-3069	-3516	-3069	-3069
			188	-15	-6249	-3132	-4094	-3132	-3579	-3132	-3132
			376	-78	-6312	-3195	-4158	-3195	-3643	-3195	-3195
284	Primo Impalcato	37-37	0	308	-5522	-2607	-3427	-2607	-2988	-2607	-2607
			188	245	-5586	-2671	-3490	-2671	-3051	-2671	-2671
			376	181	-5649	-2734	-3553	-2734	-3114	-2734	-2734
285	Primo Impalcato	38-38	0	182	-6308	-3063	-4032	-3063	-3514	-3063	-3063

	o										
			188	119	-6372	-3126	-4095	-3126	-3577	-3126	-3126
			376	56	-6435	-3189	-4159	-3189	-3640	-3189	-3189
286	Primo Impalcato	39-39	0	370	-5772	-2701	-3551	-2701	-3096	-2701	-2701
			188	307	-5835	-2764	-3614	-2764	-3159	-2764	-2764
			376	244	-5898	-2827	-3677	-2827	-3222	-2827	-2827
287	Primo Impalcato	40-40	0	102	-6128	-3013	-3967	-3013	-3461	-3013	-3013
			188	39	-6191	-3076	-4030	-3076	-3524	-3076	-3076
			376	-24	-6255	-3140	-4093	-3140	-3587	-3140	-3140
288	Primo Impalcato	41-41	0	162	-6095	-2966	-3892	-2966	-3402	-2966	-2966
			188	99	-6158	-3030	-3956	-3030	-3465	-3030	-3030
			376	36	-6221	-3093	-4019	-3093	-3529	-3093	-3093
289	Primo Impalcato	42-42	0	717	-7192	-2702	-3613	-2702	-3119	-2702	-2702
			188	654	-7255	-2765	-3676	-2765	-3182	-2765	-2765
			376	591	-7318	-2828	-3739	-2828	-3245	-2828	-2828
290	Primo Impalcato	43-43	0	-96	-5385	-2617	-3469	-2617	-3023	-2617	-2617
			188	-159	-5449	-2681	-3532	-2681	-3086	-2681	-2681
			376	-222	-5512	-2744	-3595	-2744	-3150	-2744	-2744
291	Primo Impalcato	44-44	0	33	-6362	-2919	-3845	-2919	-3350	-2919	-2919
			188	-31	-6426	-2982	-3908	-2982	-3413	-2982	-2982
			376	-94	-6489	-3045	-3971	-3045	-3477	-3045	-3045
292	Primo Impalcato	45-45	0	157	-5990	-2687	-3548	-2687	-3094	-2687	-2687
			188	94	-6053	-2750	-3611	-2750	-3157	-2750	-2750
			376	31	-6116	-2813	-3674	-2813	-3221	-2813	-2813
293	Primo Impalcato	46-46	0	-53	-5740	-2729	-3592	-2729	-3134	-2729	-2729
			188	-116	-5803	-2792	-3655	-2792	-3197	-2792	-2792
			376	-180	-5866	-2855	-3719	-2855	-3260	-2855	-2855
294	Primo Impalcato	47-47	0	916	-7284	-2665	-3558	-2665	-3066	-2665	-2665
			188	853	-7348	-2729	-3622	-2729	-3129	-2729	-2729
			376	790	-7411	-2792	-3685	-2792	-3193	-2792	-2792
295	Primo Impalcato	48-48	0	-190	-5942	-2658	-3525	-2658	-3053	-2658	-2658
			188	-254	-6006	-2721	-3588	-2721	-3116	-2721	-2721
			376	-317	-6069	-2785	-3651	-2785	-3179	-2785	-2785
296	Primo Impalcato	49-49	0	-206	-5909	-2648	-3477	-2648	-3036	-2648	-2648
			188	-269	-5972	-2711	-3540	-2711	-3099	-2711	-2711
			376	-333	-6035	-2774	-3603	-2774	-3162	-2774	-2774
297	Primo Impalcato	50-50	0	-471	-5500	-2678	-3509	-2678	-3065	-2678	-2678
			188	-534	-5563	-2741	-3572	-2741	-3128	-2741	-2741
			376	-597	-5626	-2804	-3635	-2804	-3191	-2804	-2804
298	Primo Impalcato	51-51	0	551	-6562	-2537	-3314	-2537	-2891	-2537	-2537
			188	488	-6626	-2600	-3377	-2600	-2954	-2600	-2600
			376	425	-6689	-2664	-3440	-2664	-3017	-2664	-2664
299	Primo Impalcato	52-52	0	-590	-5474	-2834	-3675	-2834	-3225	-2834	-2834
			188	-654	-5537	-2897	-3738	-2897	-3289	-2897	-2897
			376	-717	-5600	-2960	-3801	-2960	-3352	-2960	-2960
300	Primo	53-5	0	1455	-7100	-2442	-3201	-2442	-2764	-2442	-2442

	Impalcat o	3									
			188	1392	-7164	-2506	-3265	-2506	-2827	-2506	-2506
			376	1329	-7227	-2569	-3328	-2569	-2891	-2569	-2569
301	Primo Impalcat o	54-5 4	0	-376	-5054	-2702	-3480	-2702	-3054	-2702	-2702
			188	-440	-5118	-2766	-3543	-2766	-3117	-2766	-2766
			376	-503	-5181	-2829	-3606	-2829	-3180	-2829	-2829
302	Primo Impalcat o	55-5 5	0	723	-5566	-2176	-2733	-2176	-2424	-2176	-2176
			188	660	-5629	-2240	-2796	-2240	-2488	-2240	-2240
			376	596	-5692	-2303	-2859	-2303	-2551	-2303	-2303
303	Primo Impalcat o	56-5 6	0	-228	-4286	-2257	-2838	-2257	-2517	-2257	-2257
			188	-291	-4350	-2320	-2901	-2320	-2580	-2320	-2320
			376	-354	-4413	-2384	-2964	-2384	-2643	-2384	-2384
304	Primo Impalcat o	57-5 7	0	7861	-10836	-918	-1681	-1121	-1334	-1121	-1121
			188	7774	-10923	-1005	-1767	-1208	-1421	-1208	-1208
			376	7687	-11010	-1092	-1854	-1295	-1508	-1295	-1295
305	Primo Impalcat o	58-5 8	0	-176	-2657	-1417	-1750	-1417	-1538	-1417	-1417
			188	-214	-2695	-1454	-1788	-1454	-1575	-1454	-1454
			376	-252	-2733	-1492	-1826	-1492	-1613	-1492	-1492
306	Primo Impalcat o	59-5 9	0	-615	-2053	-1278	-1485	-1278	-1382	-1278	-1278
			188	-653	-2091	-1316	-1523	-1316	-1420	-1316	-1316
			376	-691	-2134	-1354	-1561	-1354	-1458	-1354	-1354
307	Primo Impalcat o	60-6 0	0	-598	-1806	-1131	-1318	-1131	-1221	-1131	-1131
			188	-635	-1855	-1169	-1356	-1169	-1258	-1169	-1169
			376	-673	-1905	-1207	-1394	-1207	-1296	-1207	-1207
308	Primo Impalcat o	61-6 1	0	-138	-1771	-907	-1209	-954	-1054	-954	-954
			188	-176	-1809	-945	-1247	-992	-1092	-992	-992
			376	-214	-1846	-983	-1284	-1030	-1130	-1030	-1030
309	Primo Impalcat o	62-6 2	0	4	-1812	-809	-1195	-904	-1011	-904	-904
			188	-34	-1850	-847	-1233	-942	-1049	-942	-942
			376	-72	-1888	-885	-1271	-980	-1087	-980	-980
310	Primo Impalcat o	63-6 3	0	-657	-1535	-953	-1119	-953	-1033	-953	-953
			188	-695	-1584	-991	-1157	-991	-1071	-991	-991
			376	-732	-1633	-1028	-1195	-1028	-1109	-1028	-1028
311	Primo Impalcat o	64-6 4	0	-663	-1536	-953	-1120	-953	-1034	-953	-953
			188	-701	-1585	-991	-1157	-991	-1072	-991	-991
			376	-738	-1634	-1029	-1195	-1029	-1110	-1029	-1029
312	Primo Impalcat o	65-6 5	0	25	-1835	-810	-1196	-905	-1012	-905	-905
			188	-12	-1873	-848	-1234	-943	-1050	-943	-943
			376	-50	-1911	-886	-1272	-981	-1088	-981	-981
313	Primo Impalcat o	66-6 6	0	-201	-1711	-909	-1211	-956	-1056	-956	-956
			188	-239	-1749	-947	-1249	-994	-1094	-994	-994
			376	-277	-1787	-984	-1287	-1032	-1132	-1032	-1032
314	Primo Impalcat o	67-6 7	0	-723	-1809	-1132	-1320	-1132	-1222	-1132	-1132
			188	-761	-1858	-1170	-1358	-1170	-1260	-1170	-1170
			376	-799	-1907	-1208	-1396	-1208	-1298	-1208	-1208

315	Primo Impalcato	68-68	0	-678	-2042	-1282	-1490	-1282	-1387	-1282	-1282
			188	-716	-2091	-1320	-1528	-1320	-1424	-1320	-1320
			376	-754	-2140	-1358	-1566	-1358	-1462	-1358	-1358
316	Primo Impalcato	69-69	0	-272	-2566	-1419	-1749	-1419	-1539	-1419	-1419
			188	-310	-2604	-1457	-1787	-1457	-1577	-1457	-1457
			376	-348	-2641	-1494	-1824	-1494	-1615	-1494	-1494
317	Primo Impalcato	70-70	0	1247	-3541	-1040	-1624	-1147	-1346	-1147	-1147
			188	1160	-3627	-1127	-1711	-1234	-1432	-1234	-1234
			376	1073	-3714	-1214	-1798	-1321	-1519	-1321	-1321
318	Primo Impalcato	1-71	0	5412	-6353	-257	-739	-387	-498	-387	-387
			102	5417	-6347	-251	-733	-382	-493	-382	-382
			204	5423	-6342	-246	-727	-376	-487	-376	-376
319	Primo Impalcato	1-92	0	1546	-1652	223	-334	-7	-119	-53	-53
			103	1551	-1646	229	-328	-2	-113	-47	-47
			206	1557	-1640	235	-323	4	-107	-42	-42
320	Primo Impalcato	92-2	0	1474	-2366	-223	-791	-416	-530	-446	-446
			103	1468	-2372	-229	-797	-422	-535	-452	-452
			206	1462	-2377	-235	-802	-428	-541	-457	-457
321	Primo Impalcato	6-89	0	1568	-2090	59	-631	-210	-348	-261	-261
			100	1573	-2084	65	-625	-204	-342	-256	-256
			200	1579	-2079	71	-619	-198	-336	-250	-250
322	Primo Impalcato	89-7	0	1617	-2078	95	-604	-178	-317	-231	-231
			100	1611	-2084	89	-610	-183	-323	-236	-236
			200	1606	-2089	83	-616	-189	-329	-242	-242
323	Primo Impalcato	9-90	0	1639	-2115	94	-617	-183	-325	-238	-238
			100	1644	-2109	100	-611	-177	-319	-233	-233
			200	1650	-2104	105	-606	-172	-314	-227	-227
324	Primo Impalcato	90-10	0	1558	-2101	43	-642	-222	-359	-271	-271
			100	1552	-2106	37	-648	-228	-365	-277	-277
			200	1546	-2112	32	-654	-234	-371	-283	-283
325	Primo Impalcato	13-91	0	1352	-2272	-238	-806	-431	-544	-460	-460
			103	1358	-2266	-233	-800	-425	-538	-454	-454
			206	1364	-2261	-227	-795	-419	-533	-448	-448
326	Primo Impalcato	88-14	0	858	-1670	-313	-739	-406	-517	-406	-406
			102	852	-1676	-318	-745	-412	-522	-412	-412
			204	846	-1682	-324	-751	-418	-528	-418	-418
327	Primo Impalcato	91-14	0	1612	-1690	239	-321	7	-105	-39	-39
			103	1606	-1695	233	-326	1	-111	-45	-45
			206	1600	-1701	227	-332	-5	-116	-50	-50
328	Primo Impalcato	71-15	0	5188	-5371	146	-267	-36	-119	-97	-97
			102	5182	-5376	140	-273	-42	-124	-103	-103
			204	5176	-5382	134	-279	-47	-130	-108	-108
329	Primo Impalcato	16-88	0	1181	-1346	140	-214	-23	-94	-83	-83
			102	1186	-1340	145	-209	-17	-88	-77	-77

			204	1192	-1335	151	-203	-11	-82	-71	-71
330	Primo Impalcato	17-72	0	5867	-7009	-276	-861	-469	-586	-479	-479
			100	5872	-7003	-270	-855	-464	-581	-473	-473
			199	5878	-6997	-265	-850	-458	-575	-467	-467
331	Primo Impalcato	87-18	0	835	-1800	-350	-858	-503	-608	-503	-503
			100	829	-1805	-356	-864	-508	-614	-508	-508
			199	824	-1811	-361	-870	-514	-620	-514	-514
332	Primo Impalcato	72-19	0	5955	-6620	-115	-679	-306	-419	-332	-332
			100	5950	-6626	-121	-685	-312	-425	-338	-338
			199	5944	-6632	-126	-691	-317	-430	-344	-344
333	Primo Impalcato	20-87	0	1111	-1822	-128	-615	-293	-390	-317	-317
			100	1117	-1816	-122	-609	-287	-385	-311	-311
			199	1122	-1810	-116	-603	-281	-379	-305	-305
334	Primo Impalcato	21-73	0	6123	-7089	-194	-770	-390	-505	-408	-408
			100	6129	-7083	-189	-764	-384	-499	-402	-402
			199	6134	-7077	-183	-758	-378	-493	-397	-397
335	Primo Impalcato	86-22	0	966	-1833	-282	-784	-440	-541	-444	-444
			100	960	-1838	-288	-789	-446	-547	-450	-450
			199	954	-1844	-293	-795	-452	-552	-455	-455
336	Primo Impalcato	73-23	0	6338	-7312	-283	-888	-469	-590	-473	-473
			100	6333	-7317	-288	-893	-475	-596	-479	-479
			199	6327	-7323	-294	-899	-481	-602	-484	-484
337	Primo Impalcato	24-86	0	1112	-2133	-283	-802	-442	-546	-444	-444
			100	1118	-2127	-277	-796	-436	-540	-438	-438
			199	1123	-2122	-271	-791	-430	-534	-432	-432
338	Primo Impalcato	25-74	0	7357	-8454	-214	-891	-446	-581	-468	-468
			103	7363	-8448	-208	-885	-440	-576	-462	-462
			206	7368	-8443	-202	-879	-435	-570	-457	-457
339	Primo Impalcato	85-26	0	1224	-1950	-346	-849	-497	-601	-497	-497
			100	1218	-1956	-352	-855	-502	-607	-502	-502
			199	1213	-1962	-358	-861	-508	-612	-508	-508
340	Primo Impalcato	27-85	0	1169	-2184	-265	-779	-424	-526	-427	-427
			100	1174	-2178	-259	-773	-418	-521	-421	-421
			199	1180	-2173	-253	-768	-412	-515	-415	-415
341	Primo Impalcato	74-28	0	7497	-8408	-213	-909	-438	-577	-453	-453
			103	7491	-8414	-218	-915	-443	-583	-459	-459
			206	7485	-8420	-224	-921	-449	-588	-464	-464
342	Primo Impalcato	84-29	0	1268	-1914	-303	-808	-459	-560	-459	-459
			100	1263	-1920	-308	-814	-465	-566	-465	-465
			199	1257	-1925	-314	-819	-471	-572	-471	-471
343	Primo Impalcato	31-84	0	1222	-2190	-247	-754	-406	-508	-413	-413
			100	1228	-2185	-241	-749	-401	-502	-407	-407
			199	1233	-2179	-235	-743	-395	-497	-401	-401
344	Primo Impalcato	83-33	0	1078	-1955	-280	-787	-437	-538	-439	-439

			100	1072	-1961	-286	-793	-443	-544	-444	-444
			199	1066	-1967	-291	-799	-448	-550	-450	-450
345	Primo Impalcato	35-83	0	1232	-2197	-264	-771	-425	-526	-431	-431
			100	1238	-2191	-258	-765	-419	-521	-425	-425
			199	1244	-2186	-253	-760	-414	-515	-419	-419
346	Primo Impalcato	82-37	0	1202	-2053	-266	-778	-423	-525	-425	-425
			100	1197	-2059	-271	-783	-428	-531	-431	-431
			199	1191	-2064	-277	-789	-434	-537	-437	-437
347	Primo Impalcato	39-82	0	1153	-2173	-290	-798	-451	-553	-455	-455
			100	1158	-2167	-284	-792	-446	-547	-450	-450
			199	1164	-2162	-278	-786	-440	-542	-444	-444
348	Primo Impalcato	78-43	0	6427	-7384	-203	-801	-396	-516	-408	-408
			100	6422	-7390	-209	-807	-402	-522	-414	-414
			199	6416	-7396	-214	-813	-408	-527	-420	-420
349	Primo Impalcato	81-44	0	1166	-2160	-349	-878	-497	-609	-497	-497
			100	1160	-2166	-355	-884	-503	-615	-503	-503
			199	1155	-2172	-361	-889	-509	-621	-509	-509
350	Primo Impalcato	45-78	0	6554	-7513	-273	-875	-467	-588	-474	-474
			100	6559	-7507	-268	-870	-462	-582	-468	-468
			199	6565	-7502	-262	-864	-456	-576	-463	-463
351	Primo Impalcato	46-81	0	1178	-2160	-261	-778	-430	-533	-437	-437
			100	1183	-2154	-256	-772	-424	-528	-432	-432
			199	1189	-2148	-250	-767	-419	-522	-426	-426
352	Primo Impalcato	77-47	0	6545	-7458	-175	-791	-375	-498	-391	-391
			100	6539	-7463	-181	-797	-381	-504	-397	-397
			199	6533	-7469	-187	-802	-387	-510	-403	-403
353	Primo Impalcato	80-48	0	1202	-2059	-260	-803	-425	-534	-428	-428
			100	1197	-2065	-265	-809	-431	-540	-434	-434
			199	1191	-2071	-271	-814	-437	-545	-440	-440
354	Primo Impalcato	49-77	0	6265	-7271	-296	-884	-485	-603	-492	-492
			100	6271	-7265	-290	-879	-479	-597	-486	-486
			199	6276	-7260	-284	-873	-474	-591	-481	-481
355	Primo Impalcato	50-80	0	1142	-2170	-279	-801	-449	-553	-456	-456
			100	1148	-2164	-273	-795	-443	-548	-450	-450
			199	1154	-2158	-268	-790	-437	-542	-445	-445
356	Primo Impalcato	76-51	0	6181	-6844	-61	-638	-262	-377	-295	-295
			100	6175	-6849	-67	-643	-267	-383	-301	-301
			199	6169	-6855	-72	-649	-273	-388	-306	-306
357	Primo Impalcato	53-76	0	6078	-7187	-340	-938	-532	-651	-534	-534
			100	6084	-7181	-335	-933	-526	-646	-528	-528
			199	6090	-7175	-329	-927	-520	-640	-522	-522
358	Primo Impalcato	75-55	0	5373	-5495	199	-228	7	-79	-61	-61
			102	5367	-5501	193	-234	1	-84	-67	-67
			204	5362	-5507	187	-240	-5	-90	-73	-73
359	Primo Impalcato	56-79	0	1482	-1578	140	-255	-35	-114	-96	-96

	o										
			102	1487	-1573	145	-249	-30	-108	-90	-90
			204	1493	-1567	151	-243	-24	-103	-85	-85
360	Primo Impalcato	57-75	0	5607	-6455	-296	-792	-424	-542	-424	-424
			102	5613	-6449	-291	-786	-418	-536	-418	-418
			204	5619	-6444	-285	-781	-412	-530	-412	-412
361	Primo Impalcato	57-93	0	1662	-1755	233	-328	0	-112	-47	-47
			103	1667	-1750	239	-322	6	-107	-41	-41
			206	1673	-1744	244	-317	11	-101	-35	-35
362	Primo Impalcato	93-58	0	1623	-2561	-226	-796	-419	-533	-448	-448
			103	1617	-2566	-232	-802	-424	-539	-454	-454
			206	1612	-2572	-237	-807	-430	-544	-460	-460
363	Primo Impalcato	61-95	0	1730	-2288	37	-649	-229	-366	-279	-279
			100	1736	-2282	43	-643	-223	-360	-273	-273
			200	1742	-2277	48	-637	-218	-355	-267	-267
364	Primo Impalcato	95-62	0	1816	-2283	97	-613	-179	-321	-233	-233
			100	1811	-2289	91	-619	-185	-327	-239	-239
			200	1805	-2294	86	-624	-190	-332	-245	-245
365	Primo Impalcato	96-65	0	1807	-2262	104	-606	-173	-315	-228	-228
			100	1801	-2268	98	-612	-178	-320	-233	-233
			200	1796	-2274	92	-617	-184	-326	-239	-239
366	Primo Impalcato	66-96	0	1712	-2283	29	-657	-236	-373	-285	-285
			100	1718	-2277	35	-651	-230	-368	-280	-280
			200	1724	-2271	41	-645	-225	-362	-274	-274
367	Primo Impalcato	69-94	0	1432	-2348	-234	-803	-428	-542	-458	-458
			103	1438	-2342	-229	-797	-422	-536	-452	-452
			206	1443	-2336	-223	-791	-416	-530	-447	-447
368	Primo Impalcato	79-70	0	1108	-2086	-286	-751	-403	-516	-403	-403
			102	1103	-2092	-292	-757	-409	-522	-409	-409
			204	1097	-2097	-297	-762	-415	-527	-415	-415
369	Primo Impalcato	94-70	0	1682	-1763	237	-323	6	-107	-40	-40
			103	1677	-1769	232	-329	0	-112	-46	-46
			206	1671	-1774	226	-334	-6	-118	-52	-52
370	Primo Impalcato	1-71	0	5203	-5359	159	-254	-23	-105	-84	-84
			102	5197	-5364	153	-259	-28	-111	-89	-89
			204	5191	-5370	148	-265	-34	-117	-95	-95
371	Primo Impalcato	1-92	0	1482	-2347	-210	-777	-403	-516	-432	-432
			103	1476	-2352	-215	-783	-408	-522	-438	-438
			206	1471	-2358	-221	-789	-414	-528	-444	-444
372	Primo Impalcato	92-2	0	1555	-1634	237	-320	6	-105	-39	-39
			103	1561	-1628	243	-315	12	-100	-34	-34
			206	1566	-1622	248	-309	18	-94	-28	-28
373	Primo Impalcato	6-89	0	1626	-2061	108	-592	-165	-305	-218	-218
			100	1620	-2067	102	-597	-170	-310	-223	-223
			200	1614	-2072	96	-603	-176	-316	-229	-229
374	Primo	89-7	0	1576	-2073	72	-618	-197	-335	-248	-248

	Impalcat o										
			100	1582	-2067	78	-612	-191	-329	-243	-243
			200	1588	-2061	84	-607	-185	-323	-237	-237
375	Primo Impalcat o	9-90	0	1567	-2084	56	-629	-209	-346	-259	-259
			100	1561	-2089	50	-635	-215	-352	-264	-264
			200	1555	-2095	45	-641	-221	-358	-270	-270
376	Primo Impalcat o	90-1 0	0	1647	-2098	107	-604	-170	-312	-225	-225
			100	1653	-2092	113	-598	-164	-307	-220	-220
			200	1659	-2087	118	-593	-159	-301	-214	-214
377	Primo Impalcat o	13-9 1	0	1622	-1673	252	-307	20	-91	-25	-25
			103	1617	-1679	247	-313	15	-97	-31	-31
			206	1611	-1685	241	-319	9	-103	-37	-37
378	Primo Impalcat o	88-1 4	0	1197	-1335	153	-201	-9	-80	-69	-69
			102	1203	-1330	159	-195	-4	-75	-63	-63
			204	1208	-1324	165	-190	2	-69	-58	-58
379	Primo Impalcat o	91-1 4	0	1361	-2253	-225	-792	-417	-530	-446	-446
			103	1366	-2248	-219	-787	-411	-525	-441	-441
			206	1372	-2242	-214	-781	-406	-519	-435	-435
380	Primo Impalcat o	71-1 5	0	5426	-6340	-244	-725	-374	-485	-374	-374
			102	5431	-6335	-238	-720	-368	-479	-368	-368
			204	5437	-6329	-232	-714	-363	-474	-363	-363
381	Primo Impalcat o	16-8 8	0	871	-1657	-299	-726	-393	-503	-393	-393
			102	866	-1663	-305	-732	-398	-509	-398	-398
			204	860	-1668	-311	-737	-404	-515	-404	-404
382	Primo Impalcat o	17-7 2	0	5968	-6608	-102	-667	-293	-406	-320	-320
			100	5963	-6613	-108	-672	-299	-412	-325	-325
			199	5957	-6619	-114	-678	-305	-418	-331	-331
383	Primo Impalcat o	87-1 8	0	1123	-1812	-115	-602	-280	-377	-304	-304
			100	1128	-1806	-109	-596	-274	-372	-298	-298
			199	1134	-1800	-104	-590	-269	-366	-292	-292
384	Primo Impalcat o	72-1 9	0	5881	-6997	-263	-848	-457	-574	-466	-466
			100	5886	-6992	-258	-843	-451	-568	-460	-460
			199	5892	-6986	-252	-837	-445	-562	-454	-454
385	Primo Impalcat o	20-8 7	0	853	-1790	-337	-846	-490	-596	-490	-490
			100	847	-1796	-343	-851	-495	-601	-495	-495
			199	842	-1801	-348	-857	-501	-607	-501	-501
386	Primo Impalcat o	21-7 3	0	6351	-7299	-270	-875	-457	-578	-460	-460
			100	6346	-7305	-275	-881	-462	-583	-466	-466
			199	6340	-7310	-281	-886	-468	-589	-471	-471
387	Primo Impalcat o	86-2 2	0	1123	-2122	-270	-789	-429	-533	-431	-431
			100	1129	-2116	-264	-784	-423	-527	-425	-425
			199	1135	-2111	-258	-778	-418	-522	-420	-420
388	Primo Impalcat o	73-2 3	0	6136	-7076	-182	-757	-377	-492	-395	-395
			100	6142	-7070	-176	-751	-371	-486	-390	-390
			199	6148	-7065	-170	-746	-366	-481	-384	-384

389	Primo Impalcato	24-86	0	983	-1823	-269	-771	-428	-528	-431	-431
			100	977	-1829	-275	-777	-433	-534	-437	-437
			199	971	-1834	-281	-782	-439	-539	-442	-442
390	Primo Impalcato	25-74	0	7510	-8395	-199	-896	-424	-563	-439	-439
			103	7505	-8400	-205	-901	-430	-569	-445	-445
			206	7499	-8406	-210	-907	-435	-575	-451	-451
391	Primo Impalcato	85-26	0	1176	-2168	-252	-766	-411	-514	-414	-414
			100	1182	-2162	-246	-761	-405	-508	-408	-408
			199	1187	-2156	-241	-755	-399	-502	-403	-403
392	Primo Impalcato	27-85	0	1238	-1939	-333	-836	-484	-588	-484	-484
			100	1232	-1945	-339	-842	-489	-594	-489	-489
			199	1227	-1951	-345	-848	-495	-600	-495	-495
393	Primo Impalcato	74-28	0	7370	-8440	-200	-877	-432	-568	-454	-454
			103	7376	-8435	-194	-871	-427	-562	-449	-449
			206	7382	-8429	-189	-866	-421	-556	-443	-443
394	Primo Impalcato	84-29	0	1230	-2174	-234	-742	-394	-495	-400	-400
			100	1236	-2169	-228	-736	-388	-490	-394	-394
			199	1241	-2163	-223	-730	-382	-484	-389	-389
395	Primo Impalcato	31-84	0	1282	-1902	-290	-795	-447	-548	-447	-447
			100	1276	-1908	-296	-801	-452	-553	-452	-452
			199	1270	-1913	-301	-806	-458	-559	-458	-458
396	Primo Impalcato	83-33	0	1241	-2180	-251	-758	-412	-514	-418	-418
			100	1246	-2174	-246	-753	-406	-508	-412	-412
			199	1252	-2169	-240	-747	-401	-502	-406	-406
397	Primo Impalcato	35-83	0	1090	-1942	-267	-774	-424	-526	-426	-426
			100	1084	-1947	-273	-780	-430	-531	-432	-432
			199	1079	-1953	-279	-786	-435	-537	-437	-437
398	Primo Impalcato	82-37	0	1165	-2160	-277	-785	-439	-540	-442	-442
			100	1171	-2154	-271	-779	-433	-535	-437	-437
			199	1176	-2148	-266	-773	-427	-529	-431	-431
399	Primo Impalcato	39-82	0	1210	-2036	-253	-765	-410	-512	-413	-413
			100	1205	-2041	-258	-771	-416	-518	-418	-418
			199	1199	-2047	-264	-776	-421	-524	-424	-424
400	Primo Impalcato	78-43	0	6567	-7501	-261	-863	-455	-575	-461	-461
			100	6573	-7495	-255	-857	-449	-569	-456	-456
			199	6578	-7489	-249	-851	-443	-564	-450	-450
401	Primo Impalcato	81-44	0	1191	-2148	-249	-765	-417	-521	-425	-425
			100	1197	-2142	-243	-760	-412	-515	-419	-419
			199	1203	-2136	-237	-754	-406	-509	-413	-413
402	Primo Impalcato	45-78	0	6440	-7371	-190	-789	-384	-503	-396	-396
			100	6434	-7377	-196	-794	-389	-509	-401	-401
			199	6428	-7382	-202	-800	-395	-515	-407	-407
403	Primo Impalcato	46-81	0	1172	-2141	-336	-865	-484	-597	-484	-484
			100	1166	-2147	-342	-871	-490	-602	-490	-490

			199	1161	-2152	-348	-877	-496	-608	-496	-496
404	Primo Impalcato	77-47	0	6278	-7259	-283	-871	-472	-590	-479	-479
			100	6284	-7253	-277	-866	-467	-584	-473	-473
			199	6290	-7247	-272	-860	-461	-579	-468	-468
405	Primo Impalcato	80-48	0	1155	-2158	-266	-788	-436	-540	-443	-443
			100	1161	-2152	-261	-783	-430	-535	-437	-437
			199	1167	-2146	-255	-777	-425	-529	-432	-432
406	Primo Impalcato	49-77	0	6557	-7445	-162	-778	-363	-486	-378	-378
			100	6552	-7451	-168	-784	-368	-491	-384	-384
			199	6546	-7456	-174	-789	-374	-497	-390	-390
407	Primo Impalcato	50-80	0	1214	-2045	-247	-790	-412	-521	-416	-416
			100	1208	-2051	-252	-796	-418	-527	-421	-421
			199	1202	-2056	-258	-802	-424	-533	-427	-427
408	Primo Impalcato	76-51	0	6091	-7174	-328	-925	-519	-638	-521	-521
			100	6096	-7168	-322	-920	-513	-633	-515	-515
			199	6102	-7162	-316	-914	-508	-627	-510	-510
409	Primo Impalcato	53-76	0	6193	-6831	-48	-625	-249	-364	-282	-282
			100	6188	-6836	-54	-631	-255	-370	-288	-288
			199	6182	-6842	-59	-636	-260	-376	-294	-294
410	Primo Impalcato	75-55	0	5620	-6441	-283	-778	-410	-528	-410	-410
			102	5626	-6436	-277	-773	-405	-523	-405	-405
			204	5632	-6430	-272	-767	-399	-517	-399	-399
411	Primo Impalcato	56-79	0	1122	-2073	-273	-738	-390	-502	-390	-390
			102	1116	-2078	-278	-743	-395	-508	-395	-395
			204	1110	-2084	-284	-749	-401	-514	-401	-401
412	Primo Impalcato	57-75	0	5387	-5483	212	-215	20	-65	-48	-48
			102	5381	-5488	206	-221	14	-71	-53	-53
			204	5376	-5494	201	-226	9	-77	-59	-59
413	Primo Impalcato	57-93	0	1630	-2543	-212	-783	-405	-519	-435	-435
			103	1625	-2549	-218	-788	-411	-525	-440	-440
			206	1619	-2554	-224	-794	-417	-531	-446	-446
414	Primo Impalcato	93-58	0	1672	-1739	247	-315	13	-99	-33	-33
			103	1678	-1733	252	-309	19	-93	-28	-28
			206	1684	-1728	258	-303	25	-87	-22	-22
415	Primo Impalcato	61-95	0	1824	-2265	110	-600	-166	-308	-221	-221
			100	1818	-2270	104	-606	-172	-314	-226	-226
			200	1812	-2276	98	-612	-177	-319	-232	-232
416	Primo Impalcato	95-62	0	1738	-2270	50	-636	-216	-353	-266	-266
			100	1744	-2265	55	-630	-210	-348	-260	-260
			200	1750	-2259	61	-625	-205	-342	-255	-255
417	Primo Impalcato	96-65	0	1721	-2266	42	-644	-223	-360	-272	-272
			100	1727	-2260	48	-638	-217	-355	-267	-267
			200	1732	-2254	54	-632	-212	-349	-261	-261
418	Primo Impalcato	66-96	0	1816	-2245	117	-593	-160	-302	-215	-215

			100	1810	-2251	111	-599	-165	-307	-220	-220
			200	1804	-2257	105	-604	-171	-313	-226	-226
419	Primo Impalcato	69-94	0	1692	-1746	251	-309	19	-93	-27	-27
			103	1687	-1751	245	-315	13	-99	-32	-32
			206	1681	-1757	240	-321	8	-104	-38	-38
420	Primo Impalcato	79-70	0	1496	-1566	153	-241	-22	-101	-83	-83
			102	1501	-1560	159	-236	-16	-95	-77	-77
			204	1507	-1555	164	-230	-11	-89	-71	-71
421	Primo Impalcato	94-70	0	1439	-2327	-221	-789	-414	-528	-444	-444
			103	1444	-2322	-215	-784	-409	-522	-439	-439
			206	1450	-2316	-209	-778	-403	-517	-433	-433
422	Copertura	1-2	0	2057	-3967	864	-1631	209	-290	48	48
			83	2057	-3968	865	-1632	209	-291	48	48
			166	2057	-3969	865	-1633	209	-291	48	48
423	Copertura	15-1	0	3328	-3454	232	-820	4	-206	-45	-45
			80	3328	-3454	232	-820	4	-206	-45	-45
			159	3328	-3454	232	-820	4	-206	-45	-45
424	Copertura	2-3	0	1985	-3839	887	-1641	221	-285	62	62
			69	1985	-3839	887	-1641	221	-285	62	62
			138	1985	-3839	887	-1641	221	-285	62	62
425	Copertura	3-4	0	1809	-3744	888	-1639	221	-284	63	63
			69	1809	-3744	888	-1639	221	-284	63	63
			138	1809	-3744	888	-1639	221	-284	63	63
426	Copertura	4-5	0	1651	-3651	888	-1639	222	-283	63	63
			69	1651	-3651	888	-1639	222	-283	63	63
			138	1651	-3651	888	-1639	222	-283	63	63
427	Copertura	5-6	0	1542	-3576	889	-1638	223	-283	64	64
			69	1542	-3576	889	-1638	223	-283	64	64
			138	1542	-3576	889	-1638	223	-283	64	64
428	Copertura	6-7	0	1515	-3513	927	-1596	258	-247	94	94
			69	1515	-3513	927	-1596	258	-247	94	94
			138	1515	-3513	927	-1596	258	-247	94	94
429	Copertura	7-8	0	1418	-3566	904	-1623	234	-271	74	74
			69	1418	-3566	904	-1623	234	-271	74	74
			138	1418	-3566	904	-1623	234	-271	74	74
430	Copertura	8-9	0	1509	-3534	904	-1623	234	-271	74	74
			69	1509	-3534	904	-1623	234	-271	74	74
			138	1509	-3534	904	-1623	234	-271	74	74
431	Copertura	9-10	0	1551	-3633	933	-1604	259	-249	93	93
			69	1551	-3633	933	-1604	259	-249	93	93
			138	1551	-3633	933	-1604	259	-249	93	93
432	Copertura	10-11	0	1562	-3710	893	-1660	218	-293	57	57
			69	1562	-3710	893	-1660	218	-293	57	57
			138	1562	-3710	893	-1660	218	-293	57	57
433	Copertura	11-12	0	1729	-3879	893	-1661	217	-293	57	57
			69	1729	-3879	893	-1661	217	-293	57	57
			138	1729	-3879	893	-1661	217	-293	57	57
434	Copertura	12-13	0	1910	-4061	892	-1663	216	-294	56	56
			69	1910	-4061	892	-1663	216	-294	56	56
			138	1910	-4061	892	-1663	216	-294	56	56
435	Copertura	13-14	0	1907	-4012	869	-1656	204	-301	41	41
			83	1907	-4010	869	-1655	204	-301	41	41
			166	1907	-4009	868	-1654	204	-301	41	41

436	Copertura	16-14	0	1175	-1278	264	-861	4	-220	-51	-51
			80	1175	-1278	264	-861	4	-220	-51	-51
			159	1175	-1278	264	-861	4	-220	-51	-51
437	Copertura	15-17	0	2989	-3108	176	-777	-12	-202	-50	-50
			66	2989	-3108	176	-777	-12	-202	-50	-50
			132	2989	-3108	176	-777	-12	-202	-50	-50
438	Copertura	16-18	0	1199	-1321	218	-852	-14	-228	-61	-61
			66	1199	-1321	218	-852	-14	-228	-61	-61
			132	1199	-1321	218	-852	-14	-228	-61	-61
439	Copertura	17-19	0	2782	-2889	122	-733	-26	-197	-53	-53
			66	2782	-2889	122	-733	-26	-197	-53	-53
			132	2782	-2889	122	-733	-26	-197	-53	-53
440	Copertura	18-20	0	1202	-1338	153	-805	-33	-225	-68	-68
			66	1202	-1338	153	-805	-33	-225	-68	-68
			132	1202	-1338	153	-805	-33	-225	-68	-68
441	Copertura	19-21	0	2548	-2658	70	-686	-38	-189	-55	-55
			66	2548	-2658	70	-686	-38	-189	-55	-55
			132	2548	-2658	70	-686	-38	-189	-55	-55
442	Copertura	20-22	0	1183	-1324	93	-756	-48	-218	-70	-70
			66	1183	-1324	93	-756	-48	-218	-70	-70
			132	1183	-1324	93	-756	-48	-218	-70	-70
443	Copertura	21-23	0	2260	-2372	19	-637	-49	-180	-56	-56
			66	2260	-2372	19	-637	-49	-180	-56	-56
			132	2260	-2372	19	-637	-49	-180	-56	-56
444	Copertura	22-24	0	1194	-1333	36	-697	-59	-205	-70	-70
			66	1194	-1333	36	-697	-59	-205	-70	-70
			132	1194	-1333	36	-697	-59	-205	-70	-70
445	Copertura	23-25	0	2171	-2282	-2	-587	-53	-169	-55	-55
			66	2171	-2282	-2	-587	-53	-169	-55	-55
			132	2171	-2282	-2	-587	-53	-169	-55	-55
446	Copertura	24-26	0	1399	-1535	-8	-638	-66	-192	-68	-68
			66	1399	-1535	-8	-638	-66	-192	-68	-68
			132	1399	-1535	-8	-638	-66	-192	-68	-68
447	Copertura	25-28	0	2144	-2256	-1	-537	-53	-160	-56	-56
			85	2144	-2256	-1	-537	-53	-160	-56	-56
			170	2144	-2256	-1	-537	-53	-160	-56	-56
448	Copertura	26-27	0	1505	-1618	12	-564	-51	-167	-56	-56
			66	1505	-1618	12	-564	-51	-167	-56	-56
			132	1505	-1618	12	-564	-51	-167	-56	-56
449	Copertura	27-29	0	1542	-1677	-4	-521	-64	-168	-67	-67
			66	1542	-1677	-4	-521	-64	-168	-67	-67
			132	1542	-1677	-4	-521	-64	-168	-67	-67
450	Copertura	28-30	0	2003	-2116	0	-488	-53	-151	-57	-57
			73	2003	-2116	0	-488	-53	-151	-57	-57
			146	2003	-2116	0	-488	-53	-151	-57	-57
451	Copertura	29-31	0	1552	-1688	-6	-464	-66	-158	-68	-68
			66	1552	-1688	-6	-464	-66	-158	-68	-68
			132	1552	-1688	-6	-464	-66	-158	-68	-68
452	Copertura	30-32	0	1913	-2028	0	-439	-54	-142	-58	-58
			69	1913	-2028	0	-439	-54	-142	-58	-58
			137	1913	-2028	0	-439	-54	-142	-58	-58
453	Copertura	31-33	0	1688	-1835	-16	-413	-72	-152	-73	-73
			66	1688	-1835	-16	-413	-72	-152	-73	-73
			132	1688	-1835	-16	-413	-72	-152	-73	-73
454	Copertura	32-3	0	1889	-2006	-1	-389	-55	-133	-59	-59

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			69	1889	-2006	-1	-389	-55	-133	-59	-59
			138	1889	-2006	-1	-389	-55	-133	-59	-59
455	Copertura	33-35	0	1753	-1903	-20	-360	-75	-143	-75	-75
			66	1753	-1903	-20	-360	-75	-143	-75	-75
			132	1753	-1903	-20	-360	-75	-143	-75	-75
456	Copertura	34-36	0	1787	-1905	0	-340	-56	-124	-59	-59
			69	1787	-1905	0	-340	-56	-124	-59	-59
			138	1787	-1905	0	-340	-56	-124	-59	-59
457	Copertura	35-37	0	1736	-1894	-29	-383	-79	-151	-79	-79
			66	1736	-1894	-29	-383	-79	-151	-79	-79
			132	1736	-1894	-29	-383	-79	-151	-79	-79
458	Copertura	36-38	0	1778	-1898	0	-339	-56	-124	-60	-60
			69	1778	-1898	0	-339	-56	-124	-60	-60
			138	1778	-1898	0	-339	-56	-124	-60	-60
459	Copertura	37-39	0	1743	-1909	-37	-445	-83	-167	-83	-83
			66	1743	-1909	-37	-445	-83	-167	-83	-83
			132	1743	-1909	-37	-445	-83	-167	-83	-83
460	Copertura	38-40	0	1830	-1950	0	-390	-56	-134	-60	-60
			69	1830	-1950	0	-390	-56	-134	-60	-60
			137	1830	-1950	0	-390	-56	-134	-60	-60
461	Copertura	39-41	0	1827	-2002	-45	-511	-87	-184	-87	-87
			66	1827	-2002	-45	-511	-87	-184	-87	-87
			132	1827	-2002	-45	-511	-87	-184	-87	-87
462	Copertura	40-42	0	1937	-2291	2	-440	-57	-145	-60	-60
			69	1937	-2291	2	-440	-57	-145	-60	-60
			138	1937	-2291	2	-440	-57	-145	-60	-60
463	Copertura	41-44	0	2098	-2329	-96	-602	-116	-228	-116	-116
			66	2098	-2329	-96	-602	-116	-228	-116	-116
			132	2098	-2329	-96	-602	-116	-228	-116	-116
464	Copertura	42-43	0	2057	-2365	-1	-494	-57	-155	-60	-60
			23	2057	-2365	-1	-494	-57	-155	-60	-60
			46	2057	-2365	-1	-494	-57	-155	-60	-60
465	Copertura	43-45	0	2085	-2531	-1	-544	-57	-165	-60	-60
			66	2085	-2531	-1	-544	-57	-165	-60	-60
			132	2085	-2531	-1	-544	-57	-165	-60	-60
466	Copertura	44-46	0	1983	-2164	-57	-627	-90	-210	-90	-90
			66	1983	-2164	-57	-627	-90	-210	-90	-90
			132	1983	-2164	-57	-627	-90	-210	-90	-90
467	Copertura	45-47	0	2144	-2720	-3	-593	-57	-175	-60	-60
			66	2144	-2720	-3	-593	-57	-175	-60	-60
			132	2144	-2720	-3	-593	-57	-175	-60	-60
468	Copertura	46-48	0	1774	-1954	-32	-682	-90	-221	-90	-90
			66	1774	-1954	-32	-682	-90	-221	-90	-90
			132	1774	-1954	-32	-682	-90	-221	-90	-90
469	Copertura	47-49	0	2537	-3162	15	-643	-53	-184	-59	-59
			66	2537	-3162	15	-643	-53	-184	-59	-59
			132	2537	-3162	15	-643	-53	-184	-59	-59
470	Copertura	48-50	0	1624	-1798	29	-734	-75	-228	-87	-87
			66	1624	-1798	29	-734	-75	-228	-87	-87
			132	1624	-1798	29	-734	-75	-228	-87	-87
471	Copertura	49-51	0	3040	-3731	67	-691	-41	-193	-58	-58
			66	3040	-3731	67	-691	-41	-193	-58	-58
			132	3040	-3731	67	-691	-41	-193	-58	-58
472	Copertura	50-52	0	1591	-1757	91	-785	-60	-235	-83	-83

			66	1591	-1757	91	-785	-60	-235	-83	-83
			132	1591	-1757	91	-785	-60	-235	-83	-83
473	Copertura	51-53	0	3348	-4119	120	-737	-28	-199	-55	-55
			66	3348	-4119	120	-737	-28	-199	-55	-55
			132	3348	-4119	120	-737	-28	-199	-55	-55
474	Copertura	52-54	0	1515	-1727	156	-833	-41	-238	-77	-77
			66	1515	-1727	156	-833	-41	-238	-77	-77
			132	1515	-1727	156	-833	-41	-238	-77	-77
475	Copertura	53-55	0	3485	-4346	175	-780	-13	-204	-51	-51
			66	3485	-4346	175	-780	-13	-204	-51	-51
			132	3485	-4346	175	-780	-13	-204	-51	-51
476	Copertura	54-56	0	1279	-1616	222	-864	-17	-235	-66	-66
			66	1279	-1616	222	-864	-17	-235	-66	-66
			132	1279	-1616	222	-864	-17	-235	-66	-66
477	Copertura	55-57	0	3886	-4848	231	-822	2	-208	-47	-47
			80	3886	-4848	231	-822	2	-208	-47	-47
			159	3886	-4848	231	-822	2	-208	-47	-47
478	Copertura	56-70	0	1122	-1751	296	-898	11	-228	-51	-51
			80	1122	-1751	296	-898	11	-228	-51	-51
			159	1122	-1751	296	-898	11	-228	-51	-51
479	Copertura	57-58	0	3063	-1812	853	-1644	199	-301	39	39
			83	3064	-1812	853	-1645	199	-301	39	39
			166	3065	-1812	854	-1646	199	-301	39	39
480	Copertura	58-59	0	2890	-1702	876	-1653	211	-295	54	54
			69	2890	-1702	876	-1653	211	-295	54	54
			138	2890	-1702	876	-1653	211	-295	54	54
481	Copertura	59-60	0	2763	-1574	877	-1652	212	-294	54	54
			69	2763	-1574	877	-1652	212	-294	54	54
			138	2763	-1574	877	-1652	212	-294	54	54
482	Copertura	60-61	0	2658	-1470	877	-1651	212	-293	55	55
			69	2658	-1470	877	-1651	212	-293	55	55
			138	2658	-1470	877	-1651	212	-293	55	55
483	Copertura	61-62	0	2601	-1406	922	-1599	254	-250	91	91
			69	2601	-1406	922	-1599	254	-250	91	91
			138	2601	-1406	922	-1599	254	-250	91	91
484	Copertura	62-63	0	2378	-1394	897	-1623	230	-274	71	71
			69	2378	-1394	897	-1623	230	-274	71	71
			138	2378	-1394	897	-1623	230	-274	71	71
485	Copertura	63-64	0	2360	-1310	897	-1623	230	-274	71	71
			69	2360	-1310	897	-1623	230	-274	71	71
			138	2360	-1310	897	-1623	230	-274	71	71
486	Copertura	64-65	0	2451	-1363	897	-1624	230	-274	71	71
			69	2451	-1363	897	-1624	230	-274	71	71
			138	2451	-1363	897	-1624	230	-274	71	71
487	Copertura	65-66	0	2253	-1362	925	-1605	254	-252	90	90
			69	2253	-1362	925	-1605	254	-252	90	90
			138	2253	-1362	925	-1605	254	-252	90	90
488	Copertura	66-67	0	2126	-1430	884	-1663	212	-298	53	53
			69	2126	-1430	884	-1663	212	-298	53	53
			138	2126	-1430	884	-1663	212	-298	53	53
489	Copertura	67-68	0	2142	-1553	883	-1664	211	-298	52	52
			69	2142	-1553	883	-1664	211	-298	52	52
			138	2142	-1553	883	-1664	211	-298	52	52
490	Copertura	68-69	0	2161	-1685	882	-1666	210	-300	51	51
			69	2161	-1685	882	-1666	210	-300	51	51

			138	2161	-1685	882	-1666	210	-300	51	51
491	Copertura	69-70	0	2038	-1719	858	-1660	196	-307	35	35
			83	2037	-1719	858	-1659	196	-307	35	35
			166	2037	-1719	857	-1658	196	-307	35	35
492	Copertura	1-1	0	1201	-2743	-764	-1237	-771	-954	-771	-771
			220	1099	-2845	-866	-1338	-873	-1056	-873	-873
			440	998	-2947	-968	-1440	-974	-1157	-974	-974
493	Copertura	2-2	0	1057	-1857	-204	-790	-379	-513	-379	-379
			220	1012	-1901	-248	-834	-423	-557	-423	-423
			440	968	-1946	-293	-879	-467	-601	-467	-467
494	Copertura	3-3	0	27	-1266	-573	-818	-573	-678	-573	-573
			220	-18	-1311	-617	-863	-617	-722	-617	-617
			440	-62	-1355	-661	-907	-661	-766	-661	-661
495	Copertura	4-4	0	-20	-1123	-477	-652	-477	-571	-477	-477
			220	-65	-1168	-521	-696	-521	-615	-521	-521
			440	-109	-1212	-565	-740	-565	-660	-565	-565
496	Copertura	5-5	0	27	-758	-357	-546	-357	-444	-357	-357
			220	-17	-803	-401	-590	-401	-488	-401	-401
			440	-62	-847	-445	-634	-445	-532	-445	-445
497	Copertura	6-6	0	477	-1108	-225	-600	-316	-421	-316	-316
			220	432	-1152	-270	-645	-360	-465	-360	-360
			440	388	-1197	-314	-689	-404	-510	-404	-404
498	Copertura	7-7	0	533	-1091	-182	-559	-279	-382	-279	-279
			220	489	-1135	-226	-604	-323	-426	-323	-323
			440	444	-1179	-270	-648	-368	-471	-368	-368
499	Copertura	8-8	0	-167	-497	-246	-379	-246	-319	-246	-246
			220	-212	-555	-291	-424	-291	-363	-291	-291
			440	-256	-613	-335	-468	-335	-407	-335	-335
500	Copertura	9-9	0	425	-1061	-224	-558	-297	-397	-297	-297
			220	381	-1105	-268	-603	-342	-441	-342	-342
			440	337	-1150	-312	-647	-386	-485	-386	-386
501	Copertura	10-10	0	502	-1239	-275	-669	-368	-477	-368	-368
			220	458	-1283	-320	-714	-413	-521	-413	-413
			440	414	-1327	-364	-758	-457	-566	-457	-457
502	Copertura	11-11	0	10	-935	-463	-661	-463	-554	-463	-463
			220	-34	-980	-507	-705	-507	-599	-507	-507
			440	-78	-1024	-551	-749	-551	-643	-551	-551
503	Copertura	12-12	0	4	-1171	-564	-815	-564	-668	-564	-564
			220	-40	-1215	-608	-859	-608	-712	-608	-608
			440	-85	-1260	-652	-904	-652	-757	-652	-652
504	Copertura	13-13	0	965	-1861	-196	-808	-382	-520	-382	-382
			220	920	-1906	-240	-852	-427	-564	-427	-427
			440	876	-1950	-284	-896	-471	-608	-471	-471
505	Copertura	57-57	0	1626	-3093	-719	-1179	-733	-908	-733	-733
			220	1524	-3194	-820	-1281	-835	-1010	-835	-835
			440	1423	-3296	-922	-1383	-937	-1111	-937	-937
506	Copertura	58-58	0	1167	-1900	-182	-783	-367	-501	-367	-367
			220	1122	-1945	-226	-828	-411	-546	-411	-411
			440	1078	-1989	-270	-872	-456	-590	-456	-456
507	Copertura	59-59	0	99	-1320	-558	-803	-558	-661	-558	-558
			220	55	-1365	-602	-848	-602	-705	-602	-602
			440	10	-1409	-646	-892	-646	-750	-646	-646
508	Copertura	60-60	0	113	-1172	-460	-663	-460	-551	-460	-460
			220	69	-1216	-505	-707	-505	-596	-505	-505
			440	25	-1261	-549	-751	-549	-640	-549	-549

509	Copertura	61-61	0	613	-1355	-271	-680	-371	-482	-371	-371
			220	568	-1400	-315	-725	-416	-526	-416	-416
			440	524	-1444	-360	-769	-460	-570	-460	-460
510	Copertura	62-62	0	469	-1082	-238	-566	-307	-407	-307	-307
			220	424	-1127	-282	-610	-351	-451	-351	-351
			440	380	-1171	-327	-655	-395	-495	-395	-395
511	Copertura	63-63	0	17	-536	-259	-425	-259	-340	-259	-259
			220	-27	-580	-304	-469	-304	-384	-304	-304
			440	-71	-637	-348	-514	-348	-428	-348	-348
512	Copertura	64-64	0	37	-588	-260	-426	-260	-341	-260	-260
			220	-8	-633	-304	-470	-304	-385	-304	-304
			440	-52	-677	-349	-515	-349	-429	-349	-349
513	Copertura	65-65	0	465	-1082	-240	-569	-309	-409	-309	-309
			220	420	-1126	-284	-613	-353	-453	-353	-353
			440	376	-1171	-329	-657	-397	-497	-397	-397
514	Copertura	66-66	0	628	-1371	-272	-680	-372	-482	-372	-372
			220	584	-1416	-317	-725	-416	-527	-416	-416
			440	539	-1460	-361	-769	-461	-571	-461	-461
515	Copertura	67-67	0	38	-961	-461	-664	-461	-553	-461	-461
			220	-6	-1005	-506	-708	-506	-597	-506	-506
			440	-51	-1049	-550	-752	-550	-641	-550	-550
516	Copertura	68-68	0	27	-1147	-560	-805	-560	-664	-560	-560
			220	-17	-1192	-604	-850	-604	-708	-604	-604
			440	-62	-1236	-649	-894	-649	-752	-649	-649
517	Copertura	69-69	0	1049	-1803	-194	-796	-377	-513	-377	-377
			220	1004	-1847	-238	-840	-421	-557	-421	-421
			440	960	-1891	-282	-885	-466	-601	-466	-466
518	Copertura	1-74	0	1852	-1771	226	-218	49	-40	18	18
			118	1858	-1764	232	-211	55	-33	24	24
			235	1865	-1757	239	-204	62	-27	31	31
519	Copertura	74-2	0	1480	-2133	-98	-450	-217	-288	-231	-231
			118	1473	-2140	-104	-457	-224	-294	-238	-238
			235	1467	-2147	-111	-463	-231	-301	-245	-245
520	Copertura	6-71	0	1717	-1889	150	-367	-50	-154	-86	-86
			115	1724	-1882	156	-360	-44	-147	-79	-79
			231	1731	-1876	163	-354	-37	-141	-73	-73
521	Copertura	71-7	0	1691	-1904	125	-393	-74	-177	-106	-106
			115	1685	-1910	118	-400	-80	-184	-113	-113
			231	1678	-1917	112	-406	-87	-191	-119	-119
522	Copertura	9-72	0	1675	-1954	91	-432	-108	-212	-139	-139
			115	1681	-1947	97	-426	-101	-206	-133	-133
			231	1688	-1940	104	-419	-94	-199	-126	-126
523	Copertura	72-10	0	1704	-1848	159	-346	-37	-138	-72	-72
			115	1697	-1854	153	-352	-43	-144	-78	-78
			231	1691	-1861	146	-359	-50	-151	-85	-85
524	Copertura	73-13	0	1356	-1819	-98	-453	-218	-289	-232	-232
			118	1349	-1826	-105	-459	-225	-296	-238	-238
			235	1342	-1833	-112	-466	-231	-302	-245	-245
525	Copertura	14-73	0	1779	-1739	235	-218	53	-37	20	20
			118	1785	-1732	242	-211	60	-31	27	27
			235	1792	-1725	249	-204	67	-24	33	33
526	Copertura	57-75	0	1888	-1850	232	-218	52	-38	19	19
			118	1895	-1843	239	-211	58	-32	26	26
			235	1902	-1836	245	-205	65	-25	33	33
527	Copertura	75-5	0	1455	-1907	-90	-444	-211	-282	-226	-226

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			118	1449	-1914	-97	-451	-218	-288	-233	-233
			235	1442	-1920	-104	-457	-224	-295	-239	-239
528	Copertura	77-61	0	1792	-1941	155	-350	-40	-141	-74	-74
			115	1785	-1947	149	-356	-47	-148	-81	-81
			231	1778	-1954	142	-363	-53	-155	-88	-88
529	Copertura	62-77	0	1769	-2050	94	-436	-108	-213	-140	-140
			115	1776	-2043	100	-429	-101	-207	-134	-134
			231	1782	-2036	107	-422	-94	-200	-127	-127
530	Copertura	65-78	0	1805	-2094	88	-441	-112	-218	-144	-144
			115	1812	-2087	95	-434	-106	-212	-138	-138
			231	1818	-2081	101	-427	-99	-205	-131	-131
531	Copertura	78-66	0	1816	-1958	160	-345	-36	-137	-71	-71
			115	1809	-1964	153	-352	-43	-144	-78	-78
			231	1802	-1971	146	-359	-49	-150	-84	-84
532	Copertura	69-76	0	1438	-1934	-114	-469	-234	-305	-248	-248
			118	1445	-1928	-108	-462	-228	-299	-242	-242
			235	1451	-1921	-101	-456	-221	-292	-235	-235
533	Copertura	76-70	0	1875	-1802	251	-201	70	-21	37	37
			118	1868	-1808	244	-208	63	-27	30	30
			235	1862	-1815	237	-214	56	-34	23	23
534	Copertura	1-74	0	1494	-2117	-82	-435	-202	-273	-216	-216
			118	1488	-2124	-89	-442	-209	-279	-223	-223
			235	1481	-2130	-96	-448	-215	-286	-230	-230
535	Copertura	74-2	0	1867	-1757	241	-202	64	-25	33	33
			118	1874	-1751	248	-196	71	-18	39	39
			235	1881	-1744	254	-189	77	-11	46	46
536	Copertura	6-71	0	1707	-1890	140	-378	-59	-163	-92	-92
			115	1700	-1897	133	-385	-66	-169	-98	-98
			231	1693	-1903	126	-392	-72	-176	-105	-105
537	Copertura	71-7	0	1733	-1876	164	-352	-36	-139	-71	-71
			115	1740	-1869	171	-346	-29	-133	-65	-65
			231	1746	-1862	178	-339	-23	-126	-58	-58
538	Copertura	9-72	0	1719	-1834	174	-331	-22	-123	-57	-57
			115	1713	-1840	167	-338	-29	-130	-64	-64
			231	1706	-1847	160	-344	-36	-136	-70	-70
539	Copertura	72-10	0	1690	-1940	105	-418	-93	-198	-125	-125
			115	1697	-1933	112	-411	-86	-191	-118	-118
			231	1703	-1926	119	-405	-80	-184	-112	-112
540	Copertura	73-13	0	1794	-1724	250	-202	68	-22	35	35
			118	1801	-1717	257	-196	75	-16	42	42
			235	1808	-1710	264	-189	82	-9	49	49
541	Copertura	14-73	0	1370	-1803	-83	-437	-203	-274	-217	-217
			118	1363	-1810	-90	-444	-209	-280	-223	-223
			235	1357	-1817	-96	-451	-216	-287	-230	-230
542	Copertura	15-125	0	6721	6	4270	1627	2545	1892	1892	1892
			75	6721	6	4270	1627	2545	1892	1892	1892
			150	6721	6	4270	1627	2545	1892	1892	1892
543	Copertura	127-16	0	6128	-18	4347	1682	2606	1943	1943	1943
			75	6128	-18	4347	1682	2606	1943	1943	1943
			150	6128	-18	4347	1682	2606	1943	1943	1943
544	Copertura	17-129	0	4045	-655	2525	1695	2060	1695	1695	1695
			75	4045	-655	2525	1695	2060	1695	1695	1695
			150	4045	-655	2525	1695	2060	1695	1695	1695
545	Copertura	130-18	0	4713	-1323	2528	1695	2060	1695	1695	1695

			75	4713	-1323	2528	1695	2060	1695	1695	1695
			150	4713	-1323	2528	1695	2060	1695	1695	1695
546	Copertura	19-135	0	4768	-1299	2655	1734	2106	1734	1734	1734
			75	4768	-1299	2655	1734	2106	1734	1734	1734
			150	4768	-1299	2655	1734	2106	1734	1734	1734
547	Copertura	134-20	0	5097	-1636	2654	1730	2102	1730	1730	1730
			75	5097	-1636	2654	1730	2102	1730	1730	1730
			150	5097	-1636	2654	1730	2102	1730	1730	1730
548	Copertura	21-136	0	5194	-1715	2718	1740	2114	1740	1740	1740
			75	5194	-1715	2718	1740	2114	1740	1740	1740
			150	5194	-1715	2718	1740	2114	1740	1740	1740
549	Copertura	138-22	0	5547	-2070	2722	1739	2113	1739	1739	1739
			75	5547	-2070	2722	1739	2113	1739	1739	1739
			150	5547	-2070	2722	1739	2113	1739	1739	1739
550	Copertura	23-141	0	6151	-2667	2760	1742	2116	1742	1742	1742
			75	6151	-2667	2760	1742	2116	1742	1742	1742
			150	6151	-2667	2760	1742	2116	1742	1742	1742
551	Copertura	142-24	0	5648	-2166	2758	1741	2116	1741	1741	1741
			75	5648	-2166	2758	1741	2116	1741	1741	1741
			150	5648	-2166	2758	1741	2116	1741	1741	1741
552	Copertura	25-145	0	5835	-2341	2763	1747	2123	1747	1747	1747
			75	5835	-2341	2763	1747	2123	1747	1747	1747
			150	5835	-2341	2763	1747	2123	1747	1747	1747
553	Copertura	146-26	0	7831	-4347	2792	1742	2124	1742	1742	1742
			75	7831	-4347	2792	1742	2124	1742	1742	1742
			150	7831	-4347	2792	1742	2124	1742	1742	1742
554	Copertura	150-27	0	6254	-2776	2753	1739	2113	1739	1739	1739
			75	6254	-2776	2753	1739	2113	1739	1739	1739
			150	6254	-2776	2753	1739	2113	1739	1739	1739
555	Copertura	28-149	0	8205	-4720	2805	1742	2128	1742	1742	1742
			75	8205	-4720	2805	1742	2128	1742	1742	1742
			150	8205	-4720	2805	1742	2128	1742	1742	1742
556	Copertura	154-29	0	7621	-4152	2791	1735	2118	1735	1735	1735
			75	7621	-4152	2791	1735	2118	1735	1735	1735
			150	7621	-4152	2791	1735	2118	1735	1735	1735
557	Copertura	30-153	0	7637	-4170	2769	1734	2111	1734	1734	1734
			75	7637	-4170	2769	1734	2111	1734	1734	1734
			150	7637	-4170	2769	1734	2111	1734	1734	1734
558	Copertura	158-31	0	7479	-4012	2783	1733	2115	1733	1733	1733
			75	7479	-4012	2783	1733	2115	1733	1733	1733
			150	7479	-4012	2783	1733	2115	1733	1733	1733
559	Copertura	32-157	0	7575	-4112	2772	1732	2110	1732	1732	1732
			75	7575	-4112	2772	1732	2110	1732	1732	1732
			150	7575	-4112	2772	1732	2110	1732	1732	1732
560	Copertura	162-33	0	7732	-4269	2772	1731	2110	1731	1731	1731
			75	7732	-4269	2772	1731	2110	1731	1731	1731
			150	7732	-4269	2772	1731	2110	1731	1731	1731
561	Copertura	34-161	0	7847	-4382	2771	1732	2110	1732	1732	1732
			75	7847	-4382	2771	1732	2110	1732	1732	1732
			150	7847	-4382	2771	1732	2110	1732	1732	1732
562	Copertura	166-35	0	7559	-4099	2761	1730	2105	1730	1730	1730
			75	7559	-4099	2761	1730	2105	1730	1730	1730
			150	7559	-4099	2761	1730	2105	1730	1730	1730
563	Copertura	36-165	0	7660	-4195	2767	1733	2109	1733	1733	1733
			75	7660	-4195	2767	1733	2109	1733	1733	1733

			150	7660	-4195	2767	1733	2109	1733	1733	1733
564	Copertura	170-37	0	7661	-4201	2750	1730	2102	1730	1730	1730
			75	7661	-4201	2750	1730	2102	1730	1730	1730
			150	7661	-4201	2750	1730	2102	1730	1730	1730
565	Copertura	38-169	0	7814	-4352	2761	1731	2106	1731	1731	1731
			75	7814	-4352	2761	1731	2106	1731	1731	1731
			150	7814	-4352	2761	1731	2106	1731	1731	1731
566	Copertura	175-39	0	7368	-3907	2739	1731	2103	1731	1731	1731
			75	7368	-3907	2739	1731	2103	1731	1731	1731
			150	7368	-3907	2739	1731	2103	1731	1731	1731
567	Copertura	40-173	0	8134	-4679	2765	1727	2105	1727	1727	1727
			75	8134	-4679	2765	1727	2105	1727	1727	1727
			150	8134	-4679	2765	1727	2105	1727	1727	1727
568	Copertura	178-41	0	11873	-8404	2832	1735	2131	1735	1735	1735
			75	11873	-8404	2832	1735	2131	1735	1735	1735
			150	11873	-8404	2832	1735	2131	1735	1735	1735
569	Copertura	42-177	0	9233	-4986	2708	1726	2097	1726	1726	1726
			75	9233	-4986	2708	1726	2097	1726	1726	1726
			150	9233	-4986	2708	1726	2097	1726	1726	1726
570	Copertura	43-181	0	11337	-7866	2809	1733	2125	1735	1735	1735
			75	11337	-7866	2809	1733	2125	1735	1735	1735
			150	11337	-7866	2809	1733	2125	1735	1735	1735
571	Copertura	182-44	0	8178	-3822	2731	1742	2117	1742	1742	1742
			75	8178	-3822	2731	1742	2117	1742	1742	1742
			150	8178	-3822	2731	1742	2117	1742	1742	1742
572	Copertura	45-185	0	6597	-3121	2749	1738	2113	1738	1738	1738
			75	6597	-3121	2749	1738	2113	1738	1738	1738
			150	6597	-3121	2749	1738	2113	1738	1738	1738
573	Copertura	186-46	0	7815	-4331	2767	1742	2117	1742	1742	1742
			75	7815	-4331	2767	1742	2117	1742	1742	1742
			150	7815	-4331	2767	1742	2117	1742	1742	1742
574	Copertura	47-189	0	6249	-2768	2737	1740	2115	1740	1740	1740
			75	6249	-2768	2737	1740	2115	1740	1740	1740
			150	6249	-2768	2737	1740	2115	1740	1740	1740
575	Copertura	190-48	0	6413	-2940	2726	1736	2110	1736	1736	1736
			75	6413	-2940	2726	1736	2110	1736	1736	1736
			150	6413	-2940	2726	1736	2110	1736	1736	1736
576	Copertura	49-193	0	5791	-2307	2710	1742	2117	1742	1742	1742
			75	5791	-2307	2710	1742	2117	1742	1742	1742
			150	5791	-2307	2710	1742	2117	1742	1742	1742
577	Copertura	195-50	0	5361	-1890	2694	1736	2109	1736	1736	1736
			75	5361	-1890	2694	1736	2109	1736	1736	1736
			150	5361	-1890	2694	1736	2109	1736	1736	1736
578	Copertura	51-197	0	5136	-1647	2653	1738	2111	1738	1738	1738
			75	5136	-1647	2653	1738	2111	1738	1738	1738
			150	5136	-1647	2653	1738	2111	1738	1738	1738
579	Copertura	199-52	0	5054	-1601	2633	1726	2097	1726	1726	1726
			75	5054	-1601	2633	1726	2097	1726	1726	1726
			150	5054	-1601	2633	1726	2097	1726	1726	1726
580	Copertura	53-201	0	4894	-1507	2521	1694	2059	1694	1694	1694
			75	4894	-1507	2521	1694	2059	1694	1694	1694
			150	4894	-1507	2521	1694	2059	1694	1694	1694
581	Copertura	202-54	0	4196	-813	2516	1691	2056	1691	1691	1691
			75	4196	-813	2516	1691	2056	1691	1691	1691
			150	4196	-813	2516	1691	2056	1691	1691	1691

582	Copertura	55-205	0	4711	-530	4291	1645	2562	1906	1906	1906
			75	4711	-530	4291	1645	2562	1906	1906	1906
			150	4711	-530	4291	1645	2562	1906	1906	1906
583	Copertura	206-56	0	6423	-28	4336	1666	2594	1933	1933	1933
			75	6423	-28	4336	1666	2594	1933	1933	1933
			150	6423	-28	4336	1666	2594	1933	1933	1933
584	Copertura	57-75	0	1471	-1892	-75	-429	-196	-266	-211	-211
			118	1464	-1899	-82	-435	-202	-273	-217	-217
			235	1458	-1906	-88	-442	-209	-280	-224	-224
585	Copertura	75-58	0	1902	-1833	247	-203	67	-23	35	35
			118	1909	-1826	254	-196	74	-16	41	41
			235	1916	-1820	260	-189	80	-10	48	48
586	Copertura	77-61	0	1786	-2038	108	-421	-93	-199	-126	-126
			115	1793	-2031	115	-414	-86	-192	-119	-119
			231	1800	-2024	122	-408	-80	-186	-112	-112
587	Copertura	62-77	0	1809	-1928	170	-335	-26	-127	-60	-60
			115	1802	-1935	163	-342	-32	-133	-66	-66
			231	1795	-1942	157	-349	-39	-140	-73	-73
588	Copertura	65-78	0	1832	-1945	174	-331	-22	-123	-56	-56
			115	1826	-1952	168	-337	-28	-129	-63	-63
			231	1819	-1958	161	-344	-35	-136	-70	-70
589	Copertura	78-66	0	1819	-2079	103	-426	-98	-204	-130	-130
			115	1826	-2072	109	-419	-91	-197	-123	-123
			231	1832	-2066	116	-413	-85	-190	-117	-117
590	Copertura	69-76	0	1890	-1786	266	-186	85	-5	52	52
			118	1884	-1793	259	-192	78	-12	45	45
			235	1877	-1800	253	-199	71	-19	39	39
591	Copertura	76-70	0	1451	-1917	-99	-454	-219	-290	-233	-233
			118	1458	-1911	-92	-447	-213	-283	-226	-226
			235	1465	-1904	-86	-440	-206	-277	-220	-220
592	Copertura	79-81	0	169	-234	45	-56	10	-11	0	0
			80	169	-234	45	-56	10	-11	0	0
			159	169	-234	45	-56	10	-11	0	0
593	Copertura	80-82	0	133	-180	33	-43	7	-8	1	1
			66	133	-180	33	-43	7	-8	1	1
			132	132	-180	32	-44	7	-8	1	1
594	Copertura	83-84	0	17	-26	-3	-13	-5	-7	-5	-5
			66	17	-26	-3	-13	-5	-7	-5	-5
			132	17	-26	-3	-13	-5	-7	-5	-5
595	Copertura	85-86	0	38	-65	-13	-21	-13	-16	-13	-13
			66	38	-65	-13	-21	-13	-16	-13	-13
			132	38	-65	-13	-21	-13	-16	-13	-13
596	Copertura	87-88	0	67	-115	-24	-37	-24	-29	-24	-24
			66	67	-115	-24	-37	-24	-29	-24	-24
			132	67	-115	-24	-37	-24	-29	-24	-24
597	Copertura	89-90	0	59	-82	-11	-20	-11	-14	-11	-11
			66	59	-82	-11	-20	-11	-14	-11	-11
			132	59	-82	-11	-20	-11	-14	-11	-11
598	Copertura	91-92	0	55	-70	-6	-18	-8	-11	-8	-8
			66	55	-70	-6	-18	-8	-11	-8	-8
			132	55	-70	-6	-18	-8	-11	-8	-8
599	Copertura	93-94	0	94	-58	30	18	22	18	18	18
			66	94	-58	30	18	22	18	18	18
			132	94	-58	30	18	22	18	18	18
600	Copertura	95-9	0	120	-59	47	31	37	31	31	31

	a	6									
			66	120	-59	47	31	37	31	31	31
			132	120	-59	47	31	37	31	31	31
601	Copertura	97-106	0	28	-35	5	-6	2	-1	1	1
			66	28	-35	5	-6	2	-1	1	1
			132	28	-35	5	-6	2	-1	1	1
602	Copertura	98-99	0	18	-25	4	-8	1	-2	0	0
			66	18	-25	4	-8	1	-2	0	0
			132	18	-25	4	-8	1	-2	0	0
603	Copertura	100-101	0	10	-14	-2	-5	-2	-3	-2	-2
			66	10	-14	-2	-5	-2	-3	-2	-2
			132	10	-14	-2	-5	-2	-3	-2	-2
604	Copertura	102-103	0	51	-92	-20	-33	-20	-25	-20	-20
			66	51	-92	-20	-33	-20	-25	-20	-20
			132	51	-92	-20	-33	-20	-25	-20	-20
605	Copertura	104-105	0	34	-46	-6	-10	-6	-7	-6	-6
			66	34	-46	-6	-10	-6	-7	-6	-6
			132	34	-46	-6	-10	-6	-7	-6	-6
606	Copertura	107-108	0	22	-34	0	-20	-6	-10	-6	-6
			66	22	-34	0	-20	-6	-10	-6	-6
			132	22	-34	0	-20	-6	-10	-6	-6
607	Copertura	109-110	0	139	-125	30	-78	-4	-25	-13	-13
			80	139	-125	30	-78	-4	-25	-13	-13
			159	139	-125	30	-78	-4	-25	-13	-13
608	Copertura	111-112	0	65	-74	4	-18	-4	-8	-5	-5
			66	66	-73	4	-18	-3	-8	-5	-5
			132	66	-73	5	-18	-3	-8	-4	-4
609	Copertura	113-114	0	23	-27	0	-2	0	-1	0	0
			66	23	-27	0	-2	0	-1	0	0
			132	23	-27	0	-2	0	-1	0	0
610	Copertura	115-116	0	197	-102	74	47	57	47	47	47
			66	197	-102	74	47	57	47	47	47
			132	197	-102	74	47	57	47	47	47
611	Copertura	117-118	0	17	-8	6	3	5	4	4	4
			66	17	-8	6	3	5	4	4	4
			132	17	-8	6	3	5	4	4	4
612	Copertura	119-120	0	5	-9	0	-4	-1	-1	-1	-1
			66	5	-9	0	-4	-1	-1	-1	-1
			132	5	-9	0	-4	-1	-1	-1	-1
613	Copertura	121-122	0	38	-34	9	-16	1	-4	-1	-1
			66	38	-34	9	-16	1	-4	-1	-1
			132	38	-34	9	-16	1	-4	-1	-1
614	Copertura	124-125	0	-538	-7118	-3472	-5059	-3472	-4182	-3472	-3472
			99	-530	-7110	-3464	-5051	-3464	-4174	-3464	-3464
			198	-522	-7102	-3456	-5043	-3456	-4166	-3456	-3456
615	Copertura	125-127	0	2474	-1668	1053	-1756	-364	-926	-648	-648
			775	2474	-1668	1053	-1756	-364	-926	-648	-648
			1550	2474	-1668	1053	-1756	-364	-926	-648	-648
616	Copertura	126-127	0	44	-7216	-3540	-5159	-3540	-4264	-3540	-3540
			99	52	-7208	-3532	-5151	-3532	-4256	-3532	-3532
			198	60	-7200	-3524	-5143	-3524	-4248	-3524	-3524
617	Copertura	128-129	0	1124	-7236	-3056	-4571	-3056	-3715	-3056	-3056
			99	1132	-7228	-3048	-4563	-3048	-3707	-3048	-3048
			198	1140	-7220	-3040	-4555	-3040	-3700	-3040	-3040
618	Copertura	129-130	0	365	-1427	-531	-807	-531	-648	-531	-531

			775	365	-1427	-531	-807	-531	-648	-531	-531
			1550	365	-1427	-531	-807	-531	-648	-531	-531
619	Copertura	131-130	0	2235	-8348	-3056	-4574	-3056	-3716	-3056	-3056
			99	2243	-8340	-3048	-4566	-3048	-3708	-3048	-3048
			198	2251	-8332	-3040	-4558	-3040	-3700	-3040	-3040
620	Copertura	132-135	0	1865	-7994	-3064	-4682	-3064	-3725	-3064	-3064
			99	1873	-7986	-3056	-4674	-3056	-3717	-3056	-3056
			198	1881	-7978	-3049	-4667	-3049	-3709	-3049	-3049
621	Copertura	133-134	0	2720	-8839	-3059	-4681	-3059	-3719	-3059	-3059
			99	2728	-8831	-3051	-4673	-3051	-3711	-3051	-3051
			198	2736	-8823	-3044	-4665	-3044	-3703	-3044	-3044
622	Copertura	135-134	0	153	-1229	-497	-769	-497	-607	-497	-497
			775	153	-1229	-497	-769	-497	-607	-497	-497
			1550	153	-1229	-497	-769	-497	-607	-497	-497
623	Copertura	137-136	0	3069	-9261	-3096	-4801	-3096	-3764	-3096	-3096
			99	3077	-9253	-3088	-4793	-3088	-3756	-3088	-3088
			198	3085	-9245	-3080	-4785	-3080	-3748	-3080	-3080
624	Copertura	136-138	0	-37	-1034	-515	-783	-515	-628	-515	-515
			775	-37	-1034	-515	-783	-515	-628	-515	-515
			1550	-37	-1034	-515	-783	-515	-628	-515	-515
625	Copertura	139-138	0	3228	-9417	-3095	-4806	-3095	-3762	-3095	-3095
			99	3236	-9409	-3087	-4798	-3087	-3754	-3087	-3087
			198	3243	-9401	-3079	-4791	-3079	-3746	-3079	-3079
626	Copertura	140-141	0	4529	-10749	-3110	-4867	-3110	-3780	-3110	-3110
			99	4537	-10741	-3102	-4859	-3102	-3772	-3102	-3102
			198	4545	-10733	-3094	-4851	-3094	-3764	-3094	-3094
627	Copertura	141-142	0	408	-1461	-523	-801	-523	-638	-523	-523
			775	408	-1461	-523	-801	-523	-638	-523	-523
			1550	408	-1461	-523	-801	-523	-638	-523	-523
628	Copertura	143-142	0	4262	-10480	-3109	-4879	-3109	-3779	-3109	-3109
			99	4270	-10472	-3101	-4871	-3101	-3771	-3101	-3101
			198	4278	-10464	-3093	-4863	-3093	-3763	-3093	-3093
629	Copertura	144-145	0	6064	-12299	-3118	-4896	-3118	-3790	-3118	-3118
			99	6072	-12291	-3110	-4888	-3110	-3782	-3110	-3110
			198	6079	-12283	-3102	-4880	-3102	-3774	-3102	-3102
630	Copertura	145-146	0	1387	-2435	-524	-808	-524	-639	-524	-524
			775	1387	-2435	-524	-808	-524	-639	-524	-524
			1550	1387	-2435	-524	-808	-524	-639	-524	-524
631	Copertura	147-146	0	5309	-11532	-3111	-4909	-3111	-3782	-3111	-3111
			99	5317	-11524	-3103	-4901	-3103	-3774	-3103	-3103
			198	5325	-11516	-3096	-4893	-3096	-3766	-3096	-3096
632	Copertura	148-149	0	6564	-12786	-3111	-4895	-3111	-3782	-3111	-3111
			99	6572	-12778	-3103	-4887	-3103	-3774	-3103	-3103
			198	6580	-12770	-3095	-4879	-3095	-3766	-3095	-3095
633	Copertura	149-150	0	1161	-2208	-524	-835	-524	-638	-524	-524
			775	1161	-2208	-524	-835	-524	-638	-524	-524
			1550	1161	-2208	-524	-835	-524	-638	-524	-524
634	Copertura	151-150	0	6284	-12497	-3107	-4918	-3107	-3776	-3107	-3107
			99	6292	-12490	-3099	-4910	-3099	-3768	-3099	-3099
			198	6300	-12482	-3091	-4903	-3091	-3761	-3091	-3091
635	Copertura	152-153	0	7212	-13405	-3096	-4888	-3096	-3764	-3096	-3096
			99	7220	-13397	-3088	-4880	-3088	-3756	-3088	-3088
			198	7228	-13389	-3081	-4872	-3081	-3748	-3081	-3081
636	Copertura	153-154	0	207	-1282	-521	-796	-521	-636	-521	-521
			775	207	-1282	-521	-796	-521	-636	-521	-521

			1551	207	-1282	-521	-796	-521	-636	-521	-521
637	Copertura	155-154	0	7122	-13317	-3097	-4910	-3097	-3765	-3097	-3097
			99	7130	-13309	-3090	-4902	-3090	-3757	-3090	-3090
			198	7137	-13301	-3082	-4894	-3082	-3750	-3082	-3082
638	Copertura	156-157	0	7387	-13574	-3094	-4887	-3094	-3761	-3094	-3094
			99	7395	-13567	-3086	-4879	-3086	-3753	-3086	-3086
			198	7403	-13559	-3078	-4871	-3078	-3745	-3078	-3078
639	Copertura	157-158	0	234	-1336	-521	-794	-521	-636	-521	-521
			775	234	-1336	-521	-794	-521	-636	-521	-521
			1551	234	-1336	-521	-794	-521	-636	-521	-521
640	Copertura	159-158	0	7599	-13790	-3095	-4903	-3095	-3763	-3095	-3095
			99	7607	-13782	-3088	-4896	-3088	-3755	-3088	-3088
			198	7615	-13774	-3080	-4888	-3080	-3747	-3080	-3080
641	Copertura	160-161	0	7468	-13657	-3094	-4883	-3094	-3762	-3094	-3094
			99	7476	-13649	-3087	-4875	-3087	-3754	-3087	-3087
			198	7484	-13641	-3079	-4867	-3079	-3746	-3079	-3079
642	Copertura	161-162	0	24	-1222	-521	-796	-521	-636	-521	-521
			776	24	-1222	-521	-796	-521	-636	-521	-521
			1551	24	-1222	-521	-796	-521	-636	-521	-521
643	Copertura	163-162	0	7652	-13838	-3093	-4891	-3093	-3760	-3093	-3093
			99	7660	-13830	-3085	-4883	-3085	-3752	-3085	-3085
			198	7668	-13823	-3077	-4876	-3077	-3744	-3077	-3077
644	Copertura	164-165	0	7503	-13694	-3095	-4877	-3095	-3762	-3095	-3095
			99	7511	-13686	-3087	-4869	-3087	-3755	-3087	-3087
			198	7519	-13678	-3079	-4861	-3079	-3747	-3079	-3079
645	Copertura	165-166	0	25	-1119	-521	-796	-521	-636	-521	-521
			776	25	-1119	-521	-796	-521	-636	-521	-521
			1551	25	-1119	-521	-796	-521	-636	-521	-521
646	Copertura	167-166	0	7611	-13794	-3092	-4877	-3092	-3758	-3092	-3092
			99	7619	-13786	-3084	-4870	-3084	-3750	-3084	-3084
			198	7627	-13778	-3076	-4862	-3076	-3742	-3076	-3076
647	Copertura	168-169	0	7616	-13802	-3093	-4867	-3093	-3759	-3093	-3093
			99	7624	-13794	-3085	-4859	-3085	-3752	-3085	-3085
			198	7632	-13786	-3077	-4851	-3077	-3744	-3077	-3077
648	Copertura	169-170	0	247	-1349	-521	-798	-521	-635	-521	-521
			776	247	-1349	-521	-798	-521	-635	-521	-521
			1552	247	-1349	-521	-798	-521	-635	-521	-521
649	Copertura	171-170	0	7658	-13840	-3091	-4864	-3091	-3757	-3091	-3091
			99	7666	-13832	-3083	-4856	-3083	-3749	-3083	-3083
			198	7673	-13824	-3075	-4848	-3075	-3742	-3075	-3075
650	Copertura	172-173	0	7381	-13553	-3086	-4858	-3086	-3751	-3086	-3086
			99	7389	-13545	-3078	-4850	-3078	-3743	-3078	-3078
			198	7397	-13537	-3070	-4842	-3070	-3736	-3070	-3070
651	Copertura	173-175	0	1187	-2484	-520	-800	-520	-634	-520	-520
			776	1187	-2484	-520	-800	-520	-634	-520	-520
			1552	1187	-2484	-520	-800	-520	-634	-520	-520
652	Copertura	174-175	0	7530	-13711	-3090	-4852	-3090	-3756	-3090	-3090
			99	7538	-13703	-3082	-4844	-3082	-3749	-3082	-3082
			198	7546	-13695	-3075	-4836	-3075	-3741	-3075	-3075
653	Copertura	176-177	0	6847	-13018	-3086	-4876	-3086	-3750	-3086	-3086
			99	6855	-13010	-3078	-4868	-3078	-3742	-3078	-3078
			198	6863	-13003	-3070	-4861	-3070	-3735	-3070	-3070
654	Copertura	177-178	0	5563	-6810	-521	-848	-521	-640	-521	-521
			776	5563	-6810	-521	-848	-521	-640	-521	-521
			1552	5563	-6810	-521	-848	-521	-640	-521	-521

655	Copertura	179-178	0	7355	-13550	-3097	-4860	-3097	-3765	-3097	-3097
			99	7363	-13542	-3089	-4852	-3089	-3757	-3089	-3089
			198	7371	-13534	-3082	-4845	-3082	-3749	-3082	-3082
656	Copertura	180-181	0	6337	-12533	-3098	-4893	-3098	-3766	-3098	-3098
			99	6345	-12525	-3090	-4885	-3090	-3758	-3090	-3090
			198	6353	-12517	-3082	-4877	-3082	-3750	-3082	-3082
657	Copertura	181-182	0	5013	-6394	-521	-826	-521	-635	-521	-521
			775	5013	-6394	-521	-826	-521	-635	-521	-521
			1550	5013	-6394	-521	-826	-521	-635	-521	-521
658	Copertura	183-182	0	6818	-13032	-3107	-4876	-3107	-3777	-3107	-3107
			99	6826	-13024	-3099	-4869	-3099	-3769	-3099	-3099
			198	6834	-13017	-3091	-4861	-3091	-3761	-3091	-3091
659	Copertura	184-185	0	6073	-12274	-3101	-4866	-3101	-3770	-3101	-3101
			99	6081	-12267	-3093	-4858	-3093	-3762	-3093	-3093
			198	6089	-12259	-3085	-4850	-3085	-3754	-3085	-3085
660	Copertura	185-186	0	920	-2160	-520	-801	-520	-634	-520	-520
			775	920	-2160	-520	-801	-520	-634	-520	-520
			1550	920	-2160	-520	-801	-520	-634	-520	-520
661	Copertura	187-186	0	6434	-12645	-3105	-4853	-3105	-3775	-3105	-3105
			99	6442	-12637	-3098	-4845	-3098	-3767	-3098	-3098
			198	6450	-12629	-3090	-4837	-3090	-3759	-3090	-3090
662	Copertura	188-189	0	5153	-11363	-3105	-4841	-3105	-3775	-3105	-3105
			99	5161	-11355	-3097	-4833	-3097	-3767	-3097	-3097
			198	5169	-11347	-3089	-4825	-3089	-3759	-3089	-3089
663	Copertura	189-190	0	361	-1404	-521	-794	-521	-636	-521	-521
			775	361	-1404	-521	-794	-521	-636	-521	-521
			1550	361	-1404	-521	-794	-521	-636	-521	-521
664	Copertura	191-190	0	5404	-11604	-3100	-4822	-3100	-3769	-3100	-3100
			99	5412	-11596	-3092	-4814	-3092	-3761	-3092	-3092
			198	5420	-11588	-3084	-4806	-3084	-3753	-3084	-3084
665	Copertura	192-193	0	3784	-9980	-3098	-4788	-3098	-3766	-3098	-3098
			99	3792	-9972	-3090	-4781	-3090	-3758	-3090	-3090
			198	3800	-9964	-3082	-4773	-3082	-3750	-3082	-3082
666	Copertura	193-195	0	-10	-1027	-514	-783	-514	-627	-514	-514
			775	-10	-1027	-514	-783	-514	-627	-514	-514
			1550	-10	-1027	-514	-783	-514	-627	-514	-514
667	Copertura	194-195	0	3650	-9830	-3090	-4769	-3090	-3756	-3090	-3090
			99	3658	-9822	-3082	-4761	-3082	-3748	-3082	-3082
			198	3666	-9814	-3074	-4753	-3074	-3740	-3074	-3074
668	Copertura	196-197	0	3014	-9152	-3069	-4679	-3069	-3730	-3069	-3069
			99	3022	-9144	-3061	-4671	-3061	-3722	-3061	-3061
			198	3030	-9136	-3053	-4663	-3053	-3714	-3053	-3053
669	Copertura	197-199	0	113	-1118	-497	-768	-497	-607	-497	-497
			775	113	-1118	-497	-768	-497	-607	-497	-497
			1550	113	-1118	-497	-768	-497	-607	-497	-497
670	Copertura	198-199	0	2402	-8508	-3053	-4651	-3053	-3712	-3053	-3053
			99	2410	-8501	-3045	-4644	-3045	-3704	-3045	-3045
			198	2418	-8493	-3038	-4636	-3038	-3696	-3038	-3038
671	Copertura	200-201	0	2842	-8958	-3058	-4570	-3058	-3717	-3058	-3058
			99	2849	-8950	-3050	-4562	-3050	-3710	-3050	-3050
			198	2857	-8942	-3042	-4554	-3042	-3702	-3042	-3042
672	Copertura	201-202	0	554	-1621	-534	-811	-534	-651	-534	-534
			775	554	-1621	-534	-811	-534	-651	-534	-534
			1550	554	-1621	-534	-811	-534	-651	-534	-534
673	Copertura	203-	0	1877	-7986	-3055	-4563	-3055	-3714	-3055	-3055

	a	202									
			99	1885	-7978	-3047	-4556	-3047	-3706	-3047	-3047
			198	1893	-7970	-3039	-4548	-3039	-3698	-3039	-3039
674	Copertur a	204- 205	0	762	-7722	-3480	-5068	-3480	-4192	-3480	-3480
			99	770	-7714	-3472	-5060	-3472	-4184	-3472	-3472
			198	778	-7706	-3464	-5053	-3464	-4176	-3464	-3464
675	Copertur a	205- 206	0	1793	-2318	1065	-1744	-353	-915	-639	-639
			775	1793	-2318	1065	-1744	-353	-915	-639	-639
			1550	1793	-2318	1065	-1744	-353	-915	-639	-639
676	Copertur a	207- 206	0	-80	-7253	-3515	-5117	-3515	-4233	-3515	-3515
			99	-72	-7245	-3507	-5109	-3507	-4226	-3507	-3507
			198	-64	-7238	-3499	-5101	-3499	-4218	-3499	-3499
677	Copertur a	79-1 4	0	1234	-2931	-838	-1304	-848	-1027	-848	-848
			125	1176	-2988	-896	-1362	-906	-1085	-906	-906
			250	1119	-3046	-954	-1420	-964	-1143	-964	-964
678	Copertur a	124- 15	0	4475	-8791	-1736	-2578	-1736	-2065	-1736	-1736
			155	4423	-8843	-1789	-2630	-1789	-2117	-1789	-1789
			310	4371	-8895	-1841	-2682	-1841	-2169	-1841	-1841
679	Copertur a	80-1 6	0	297	-4085	-1846	-2673	-1846	-2179	-1846	-1846
			45	282	-4100	-1861	-2688	-1861	-2194	-1861	-1861
			90	267	-4115	-1876	-2703	-1876	-2209	-1876	-1876
680	Copertur a	128- 17	0	126	-4850	-2027	-2795	-2027	-2381	-2027	-2027
			155	73	-4902	-2079	-2847	-2079	-2433	-2079	-2079
			310	21	-4954	-2131	-2899	-2131	-2486	-2131	-2131
681	Copertur a	82-1 8	0	706	-4940	-2117	-2886	-2117	-2470	-2117	-2117
			43	692	-4954	-2131	-2900	-2131	-2485	-2131	-2131
			85	678	-4969	-2145	-2915	-2145	-2499	-2145	-2145
682	Copertur a	132- 19	0	139	-5642	-2225	-3112	-2225	-2631	-2225	-2225
			155	87	-5694	-2277	-3164	-2277	-2683	-2277	-2277
			310	35	-5746	-2330	-3216	-2330	-2735	-2330	-2330
683	Copertur a	83-2 0	0	207	-5159	-2340	-3247	-2340	-2750	-2340	-2340
			43	192	-5174	-2354	-3262	-2354	-2765	-2354	-2354
			85	178	-5188	-2368	-3276	-2368	-2779	-2368	-2368
684	Copertur a	137- 21	0	1343	-6877	-2326	-3301	-2326	-2764	-2326	-2326
			155	1291	-6929	-2378	-3353	-2378	-2816	-2378	-2378
			310	1239	-6981	-2430	-3405	-2430	-2868	-2430	-2430
685	Copertur a	84-2 2	0	226	-5694	-2418	-3386	-2418	-2858	-2418	-2418
			43	212	-5708	-2432	-3400	-2432	-2872	-2432	-2432
			85	197	-5722	-2446	-3414	-2446	-2886	-2446	-2446
686	Copertur a	140- 23	0	65	-5744	-2452	-3426	-2452	-2914	-2452	-2452
			155	13	-5796	-2504	-3478	-2504	-2966	-2504	-2504
			310	-40	-5848	-2556	-3530	-2556	-3018	-2556	-2556
687	Copertur a	85-2 4	0	-104	-5660	-2528	-3511	-2528	-2992	-2528	-2528
			43	-119	-5675	-2542	-3525	-2542	-3007	-2542	-2542
			85	-133	-5689	-2557	-3540	-2557	-3021	-2557	-2557
688	Copertur a	144- 25	0	1945	-8127	-2604	-3698	-2604	-3098	-2604	-2604
			155	1893	-8179	-2656	-3750	-2656	-3150	-2656	-2656
			310	1841	-8231	-2708	-3803	-2708	-3202	-2708	-2708
689	Copertur a	86-2 6	0	382	-6211	-2601	-3632	-2601	-3077	-2601	-2601
			43	368	-6225	-2615	-3646	-2615	-3091	-2615	-2615
			85	354	-6240	-2629	-3661	-2629	-3105	-2629	-2629
690	Copertur a	87-2 7	0	572	-5850	-2547	-3540	-2547	-3014	-2547	-2547
			43	558	-5865	-2562	-3555	-2562	-3029	-2562	-2562
			85	543	-5879	-2576	-3569	-2576	-3043	-2576	-2576
691	Copertur a	148- 28	0	1313	-7647	-2538	-3583	-2538	-3019	-2538	-2538

			155	1261	-7699	-2590	-3635	-2590	-3071	-2590	-2590
			310	1209	-7751	-2642	-3687	-2642	-3123	-2642	-2642
692	Copertura	88-29	0	886	-5803	-2409	-3370	-2409	-2853	-2409	-2409
			43	872	-5817	-2423	-3385	-2423	-2867	-2423	-2423
			85	857	-5831	-2438	-3399	-2438	-2881	-2438	-2438
693	Copertura	152-30	0	576	-5266	-2332	-3276	-2332	-2773	-2332	-2332
			155	524	-5318	-2384	-3328	-2384	-2826	-2384	-2384
			310	472	-5370	-2436	-3380	-2436	-2878	-2436	-2436
694	Copertura	89-31	0	714	-5531	-2408	-3361	-2408	-2851	-2408	-2408
			43	699	-5545	-2423	-3376	-2423	-2865	-2423	-2423
			85	685	-5559	-2437	-3390	-2437	-2880	-2437	-2437
695	Copertura	156-32	0	586	-5185	-2300	-3232	-2300	-2735	-2300	-2300
			155	534	-5237	-2352	-3284	-2352	-2788	-2352	-2352
			310	482	-5290	-2404	-3337	-2404	-2840	-2404	-2404
696	Copertura	90-33	0	782	-5545	-2382	-3326	-2382	-2818	-2382	-2382
			43	768	-5560	-2396	-3340	-2396	-2832	-2396	-2396
			85	753	-5574	-2410	-3355	-2410	-2846	-2410	-2410
697	Copertura	160-34	0	307	-4969	-2331	-3278	-2331	-2772	-2331	-2331
			155	255	-5021	-2383	-3330	-2383	-2824	-2383	-2383
			310	203	-5073	-2435	-3382	-2435	-2876	-2435	-2435
698	Copertura	91-35	0	582	-5406	-2412	-3365	-2412	-2854	-2412	-2412
			43	568	-5420	-2426	-3379	-2426	-2869	-2426	-2426
			85	553	-5435	-2441	-3394	-2441	-2883	-2441	-2441
699	Copertura	164-36	0	384	-5098	-2357	-3321	-2357	-2805	-2357	-2357
			155	332	-5150	-2409	-3373	-2409	-2857	-2409	-2409
			310	280	-5202	-2461	-3425	-2461	-2909	-2461	-2461
700	Copertura	92-37	0	778	-5598	-2410	-3361	-2410	-2850	-2410	-2410
			43	764	-5613	-2424	-3376	-2424	-2865	-2424	-2424
			85	749	-5627	-2439	-3390	-2439	-2879	-2439	-2439
701	Copertura	168-38	0	545	-5243	-2349	-3318	-2349	-2800	-2349	-2349
			155	493	-5295	-2401	-3370	-2401	-2852	-2401	-2401
			310	441	-5347	-2453	-3422	-2453	-2904	-2453	-2453
702	Copertura	93-39	0	710	-5608	-2449	-3439	-2449	-2899	-2449	-2449
			43	696	-5622	-2463	-3453	-2463	-2913	-2463	-2463
			85	681	-5637	-2478	-3467	-2478	-2928	-2478	-2478
703	Copertura	172-40	0	288	-4849	-2280	-3226	-2280	-2724	-2280	-2280
			155	236	-4901	-2332	-3278	-2332	-2776	-2332	-2332
			310	184	-4953	-2385	-3330	-2385	-2828	-2385	-2385
704	Copertura	94-41	0	446	-5410	-2422	-3369	-2422	-2867	-2422	-2422
			43	431	-5424	-2436	-3384	-2436	-2882	-2436	-2436
			85	417	-5438	-2450	-3398	-2450	-2896	-2450	-2450
705	Copertura	176-42	0	664	-6222	-2333	-3280	-2333	-2772	-2333	-2333
			155	612	-6274	-2385	-3332	-2385	-2824	-2385	-2385
			310	560	-6326	-2437	-3384	-2437	-2876	-2437	-2437
706	Copertura	180-43	0	17	-4932	-2396	-3341	-2396	-2845	-2396	-2396
			155	-35	-4984	-2448	-3393	-2448	-2897	-2448	-2448
			310	-87	-5037	-2501	-3445	-2501	-2949	-2501	-2501
707	Copertura	95-44	0	413	-5794	-2636	-3665	-2636	-3116	-2636	-2636
			43	399	-5808	-2650	-3680	-2650	-3130	-2650	-2650
			85	384	-5822	-2665	-3694	-2665	-3144	-2665	-2665
708	Copertura	184-45	0	1459	-7439	-2391	-3420	-2391	-2856	-2391	-2391
			155	1407	-7491	-2443	-3472	-2443	-2908	-2443	-2443
			310	1355	-7543	-2495	-3524	-2495	-2961	-2495	-2495
709	Copertura	96-46	0	221	-6171	-2580	-3595	-2580	-3055	-2580	-2580
			43	207	-6186	-2595	-3609	-2595	-3070	-2595	-2595

			85	193	-6200	-2609	-3624	-2609	-3084	-2609	-2609
710	Copertura	188-47	0	368	-5794	-2400	-3386	-2400	-2864	-2400	-2400
			155	316	-5846	-2452	-3438	-2452	-2917	-2452	-2452
			310	264	-5898	-2504	-3490	-2504	-2969	-2504	-2504
711	Copertura	97-48	0	75	-5569	-2485	-3454	-2485	-2943	-2485	-2485
			43	60	-5583	-2499	-3468	-2499	-2958	-2499	-2499
			85	46	-5597	-2513	-3482	-2513	-2972	-2513	-2513
712	Copertura	192-49	0	1332	-7196	-2349	-3343	-2349	-2796	-2349	-2349
			155	1280	-7248	-2401	-3395	-2401	-2848	-2401	-2401
			310	1228	-7300	-2453	-3447	-2453	-2900	-2453	-2453
713	Copertura	106-50	0	-140	-5631	-2429	-3411	-2429	-2871	-2429	-2429
			43	-155	-5645	-2444	-3426	-2444	-2885	-2444	-2444
			85	-169	-5660	-2458	-3440	-2458	-2900	-2458	-2458
714	Copertura	196-51	0	462	-6097	-2303	-3221	-2303	-2724	-2303	-2303
			155	410	-6149	-2355	-3273	-2355	-2776	-2355	-2355
			310	357	-6201	-2407	-3325	-2407	-2828	-2407	-2407
715	Copertura	107-52	0	-234	-4808	-2256	-3107	-2256	-2653	-2256	-2256
			43	-249	-4822	-2271	-3121	-2271	-2667	-2271	-2271
			85	-263	-4837	-2285	-3135	-2285	-2681	-2285	-2285
716	Copertura	200-53	0	941	-5767	-2064	-2845	-2064	-2424	-2064	-2064
			155	889	-5819	-2116	-2897	-2116	-2476	-2116	-2116
			310	837	-5871	-2168	-2949	-2168	-2528	-2168	-2168
717	Copertura	108-54	0	-19	-4446	-2113	-2922	-2113	-2471	-2113	-2113
			43	-33	-4460	-2128	-2937	-2128	-2485	-2128	-2128
			85	-47	-4475	-2142	-2951	-2142	-2499	-2142	-2142
718	Copertura	204-55	0	5013	-9152	-1769	-2621	-1769	-2102	-1769	-1769
			155	4960	-9204	-1821	-2673	-1821	-2154	-1821	-1821
			310	4908	-9257	-1873	-2725	-1873	-2206	-1873	-1873
719	Copertura	109-56	0	224	-4298	-1908	-2754	-1908	-2248	-1908	-1908
			43	209	-4312	-1923	-2768	-1923	-2262	-1923	-1923
			85	195	-4326	-1937	-2782	-1937	-2277	-1937	-1937
720	Copertura	110-70	0	1379	-3261	-941	-1399	-941	-1122	-941	-941
			43	1360	-3281	-961	-1418	-961	-1142	-961	-961
			85	1340	-3300	-980	-1438	-980	-1161	-980	-980
721	Copertura	14-79	0	1036	-2493	-712	-1172	-728	-902	-728	-728
			95	992	-2536	-756	-1216	-772	-946	-772	-772
			190	948	-2580	-800	-1260	-816	-990	-816	-816
722	Copertura	15-124	0	6409	-5043	1170	678	835	678	678	678
			65	6387	-5065	1148	656	813	656	656	656
			130	6366	-5087	1126	634	791	634	634	634
723	Copertura	16-126	0	2699	-1086	1161	690	847	690	690	690
			65	2678	-1108	1139	668	825	668	668	668
			130	2656	-1130	1117	646	803	646	646	646
724	Copertura	17-128	0	2553	-2325	397	114	222	114	114	114
			65	2531	-2346	375	93	200	93	93	93
			130	2510	-2368	353	71	178	71	71	71
725	Copertura	18-131	0	1910	-1687	392	112	219	112	112	112
			65	1888	-1709	371	90	197	90	90	90
			130	1866	-1730	349	68	175	68	68	68
726	Copertura	19-132	0	3115	-3270	243	-185	14	-78	-78	-78
			65	3093	-3292	222	-207	-8	-99	-99	-99
			130	3071	-3314	200	-229	-30	-121	-121	-121
727	Copertura	20-133	0	2979	-3203	198	-224	-27	-112	-112	-112
			65	2957	-3225	176	-246	-48	-134	-134	-134
			130	2936	-3247	155	-268	-70	-156	-156	-156

728	Copertura	21-1 37	0	3796	-4120	213	-394	-72	-193	-156	-156
			65	3774	-4142	191	-416	-94	-215	-178	-178
			130	3752	-4164	169	-438	-116	-237	-200	-200
729	Copertura	22-1 39	0	3246	-3576	206	-391	-81	-201	-165	-165
			65	3225	-3598	184	-413	-103	-223	-187	-187
			130	3203	-3620	162	-435	-125	-245	-209	-209
730	Copertura	23-1 40	0	3884	-4432	109	-579	-199	-336	-274	-274
			65	3862	-4454	87	-601	-220	-358	-296	-296
			130	3840	-4475	65	-623	-242	-380	-318	-318
731	Copertura	24-1 43	0	4297	-4811	134	-560	-181	-320	-257	-257
			65	4275	-4833	112	-581	-203	-342	-279	-279
			130	4254	-4855	90	-603	-225	-364	-301	-301
732	Copertura	25-1 44	0	4768	-5609	-76	-768	-369	-507	-420	-420
			65	4746	-5631	-98	-790	-391	-529	-442	-442
			130	4724	-5652	-120	-812	-413	-551	-464	-464
733	Copertura	26-1 47	0	4508	-5176	63	-672	-264	-412	-334	-334
			65	4486	-5198	42	-694	-286	-433	-356	-356
			130	4465	-5220	20	-716	-308	-455	-378	-378
734	Copertura	27-1 51	0	5467	-6004	162	-610	-186	-340	-268	-268
			65	5445	-6026	140	-632	-208	-362	-290	-290
			130	5424	-6048	119	-654	-230	-384	-312	-312
735	Copertura	28-1 48	0	5632	-6349	8	-689	-296	-436	-358	-358
			65	5611	-6371	-14	-711	-318	-457	-380	-380
			130	5589	-6393	-36	-733	-340	-479	-402	-402
736	Copertura	29-1 55	0	5425	-5741	304	-480	-59	-216	-158	-158
			65	5403	-5763	283	-502	-81	-238	-180	-180
			130	5381	-5784	261	-524	-103	-260	-202	-202
737	Copertura	30-1 52	0	5687	-6012	279	-474	-66	-216	-162	-162
			65	5665	-6034	258	-495	-88	-238	-184	-184
			130	5643	-6055	236	-517	-109	-260	-206	-206
738	Copertura	31-1 59	0	6064	-6333	331	-449	-32	-188	-135	-135
			65	6042	-6355	310	-471	-54	-210	-156	-156
			130	6020	-6377	288	-493	-75	-232	-178	-178
739	Copertura	32-1 56	0	5752	-6016	320	-441	-30	-183	-132	-132
			65	5730	-6038	299	-463	-52	-204	-154	-154
			130	5708	-6060	277	-485	-74	-226	-176	-176
740	Copertura	33-1 63	0	5813	-6093	310	-442	-40	-191	-140	-140
			65	5791	-6115	289	-464	-62	-213	-162	-162
			130	5769	-6137	267	-486	-84	-234	-184	-184
741	Copertura	34-1 60	0	5922	-6247	273	-467	-67	-215	-163	-163
			65	5900	-6269	251	-489	-89	-236	-184	-184
			130	5878	-6291	229	-510	-110	-258	-206	-206
742	Copertura	35-1 67	0	6076	-6354	302	-440	-41	-189	-139	-139
			65	6054	-6376	280	-462	-63	-211	-161	-161
			130	6032	-6397	259	-483	-84	-233	-183	-183
743	Copertura	36-1 64	0	5847	-6224	225	-483	-100	-242	-188	-188
			65	5826	-6246	203	-505	-122	-263	-210	-210
			130	5804	-6268	182	-527	-144	-285	-232	-232
744	Copertura	37-1 71	0	5836	-6181	242	-467	-82	-224	-172	-172
			65	5815	-6203	220	-488	-104	-246	-194	-194
			130	5793	-6225	198	-510	-126	-268	-216	-216
745	Copertura	38-1 68	0	5881	-6244	220	-467	-97	-235	-182	-182
			65	5859	-6266	198	-489	-119	-256	-203	-203
			130	5837	-6287	176	-511	-141	-278	-225	-225
746	Copertura	39-1	0	5646	-6008	223	-483	-95	-236	-181	-181

	a	74									
			65	5624	-6030	201	-505	-117	-258	-203	-203
			130	5602	-6052	180	-527	-139	-280	-225	-225
747	Copertura	40-172	0	5798	-6034	304	-405	-27	-169	-118	-118
			65	5776	-6056	282	-426	-49	-191	-140	-140
			130	5755	-6078	260	-448	-71	-213	-161	-161
748	Copertura	41-179	0	5225	-5583	218	-469	-96	-233	-179	-179
			65	5203	-5604	196	-491	-118	-255	-200	-200
			130	5182	-5626	174	-513	-140	-277	-222	-222
749	Copertura	42-176	0	5896	-6237	290	-502	-72	-230	-171	-171
			65	5874	-6259	268	-524	-93	-252	-192	-192
			130	5852	-6280	247	-546	-115	-274	-214	-214
750	Copertura	43-180	0	5419	-5871	224	-567	-133	-291	-226	-226
			65	5398	-5893	202	-589	-155	-313	-248	-248
			130	5376	-5915	181	-611	-177	-335	-270	-270
751	Copertura	44-183	0	5040	-5764	-4	-692	-301	-438	-362	-362
			65	5019	-5786	-26	-713	-323	-460	-384	-384
			130	4997	-5808	-48	-735	-345	-482	-406	-406
752	Copertura	45-184	0	5537	-5974	174	-528	-145	-285	-219	-219
			65	5515	-5996	152	-550	-166	-307	-241	-241
			130	5493	-6018	130	-572	-188	-329	-263	-263
753	Copertura	46-187	0	4682	-5334	22	-649	-266	-400	-326	-326
			65	4661	-5356	1	-671	-288	-422	-348	-348
			130	4639	-5378	-21	-693	-310	-444	-369	-369
754	Copertura	47-188	0	4420	-4869	126	-493	-156	-280	-224	-224
			65	4398	-4890	104	-514	-178	-302	-246	-246
			130	4376	-4912	83	-536	-200	-323	-268	-268
755	Copertura	48-191	0	4223	-4669	131	-501	-151	-278	-223	-223
			65	4202	-4691	109	-522	-173	-300	-245	-245
			130	4180	-4713	88	-544	-195	-322	-267	-267
756	Copertura	49-192	0	4184	-4541	157	-387	-104	-213	-179	-179
			65	4162	-4563	135	-408	-126	-235	-200	-200
			130	4140	-4585	113	-430	-148	-256	-222	-222
757	Copertura	50-194	0	3741	-4105	153	-403	-107	-218	-182	-182
			65	3720	-4127	131	-424	-128	-240	-204	-204
			130	3698	-4149	109	-446	-150	-261	-226	-226
758	Copertura	51-196	0	3105	-3410	129	-255	-76	-153	-152	-152
			65	3083	-3432	107	-277	-98	-175	-174	-174
			130	3061	-3453	85	-299	-120	-197	-196	-196
759	Copertura	52-198	0	3063	-3122	289	-114	64	-29	-29	-29
			65	3042	-3144	267	-136	43	-51	-51	-51
			130	3020	-3166	245	-158	21	-73	-73	-73
760	Copertura	53-200	0	2662	-2504	344	79	180	79	79	79
			65	2640	-2526	322	57	159	57	57	57
			130	2618	-2547	301	35	137	35	35	35
761	Copertura	54-203	0	2677	-2472	379	103	206	103	103	103
			65	2655	-2494	357	81	184	81	81	81
			130	2634	-2515	335	59	162	59	59	59
762	Copertura	55-204	0	6695	-5121	1137	651	805	651	651	651
			65	6673	-5143	1115	629	784	629	629	629
			130	6652	-5165	1093	607	762	607	607	607
763	Copertura	56-207	0	2403	-1008	1078	635	786	635	635	635
			65	2381	-1030	1056	613	764	613	613	613
			130	2359	-1052	1034	591	742	591	591	591
764	Copertura	70-123	0	1475	-2980	-748	-1205	-752	-930	-752	-752

			95	1431	-3024	-792	-1249	-796	-974	-796	-796
			190	1387	-3067	-835	-1292	-840	-1018	-840	-840
765	Copertura	81-80	0	142	-3689	-1774	-2544	-1774	-2103	-1774	-1774
			80	115	-3716	-1801	-2571	-1801	-2130	-1801	-1801
			160	88	-3743	-1828	-2598	-1828	-2157	-1828	-1828
766	Copertura	126-81	0	334	-3988	-1769	-2597	-1769	-2104	-1769	-1769
			30	324	-3998	-1779	-2607	-1779	-2114	-1779	-1779
			60	314	-4008	-1789	-2617	-1789	-2124	-1789	-1789
767	Copertura	98-82	0	581	-4712	-2066	-2851	-2066	-2423	-2066	-2066
			82	553	-4740	-2093	-2879	-2093	-2451	-2093	-2093
			165	526	-4768	-2121	-2907	-2121	-2479	-2121	-2121
768	Copertura	99-83	0	381	-4990	-2275	-3159	-2275	-2684	-2275	-2275
			82	353	-5017	-2302	-3187	-2302	-2712	-2302	-2302
			165	325	-5045	-2330	-3215	-2330	-2740	-2330	-2330
769	Copertura	100-84	0	54	-5442	-2358	-3291	-2358	-2799	-2358	-2358
			82	26	-5470	-2386	-3319	-2386	-2827	-2386	-2386
			165	-1	-5497	-2413	-3346	-2413	-2854	-2413	-2413
770	Copertura	101-85	0	40	-5568	-2464	-3446	-2464	-2928	-2464	-2464
			82	12	-5596	-2492	-3474	-2492	-2956	-2492	-2492
			165	-15	-5623	-2520	-3502	-2520	-2983	-2520	-2520
771	Copertura	102-86	0	220	-5954	-2540	-3546	-2540	-3016	-2540	-2540
			82	192	-5981	-2567	-3573	-2567	-3044	-2567	-2567
			165	164	-6009	-2595	-3601	-2595	-3072	-2595	-2595
772	Copertura	103-87	0	643	-5636	-2473	-3459	-2473	-2938	-2473	-2473
			82	615	-5663	-2501	-3487	-2501	-2965	-2501	-2501
			165	587	-5691	-2528	-3514	-2528	-2993	-2528	-2528
773	Copertura	104-88	0	758	-5611	-2359	-3309	-2359	-2805	-2359	-2359
			82	731	-5638	-2386	-3337	-2386	-2833	-2386	-2386
			165	703	-5666	-2414	-3364	-2414	-2860	-2414	-2414
774	Copertura	105-89	0	752	-5406	-2327	-3265	-2327	-2766	-2327	-2327
			82	724	-5433	-2355	-3292	-2355	-2793	-2355	-2355
			165	696	-5461	-2382	-3320	-2382	-2821	-2382	-2382
775	Copertura	111-90	0	679	-5359	-2340	-3284	-2340	-2780	-2340	-2340
			80	652	-5386	-2367	-3310	-2367	-2807	-2367	-2367
			160	626	-5413	-2394	-3337	-2394	-2834	-2394	-2394
776	Copertura	112-91	0	593	-5249	-2328	-3265	-2328	-2766	-2328	-2328
			82	565	-5277	-2356	-3293	-2356	-2793	-2356	-2356
			165	537	-5305	-2384	-3321	-2384	-2821	-2384	-2384
777	Copertura	113-92	0	698	-5437	-2369	-3324	-2369	-2814	-2369	-2369
			82	670	-5464	-2397	-3351	-2397	-2842	-2397	-2397
			165	643	-5492	-2425	-3379	-2425	-2870	-2425	-2425
778	Copertura	114-93	0	677	-5417	-2370	-3322	-2370	-2816	-2370	-2370
			82	649	-5444	-2398	-3350	-2398	-2844	-2398	-2398
			165	621	-5472	-2425	-3377	-2425	-2871	-2425	-2425
779	Copertura	115-94	0	555	-5595	-2376	-3339	-2376	-2826	-2376	-2376
			82	527	-5623	-2404	-3367	-2404	-2853	-2404	-2404
			165	500	-5651	-2432	-3394	-2432	-2881	-2432	-2432
780	Copertura	116-95	0	723	-6041	-2565	-3636	-2565	-3043	-2565	-2565
			82	695	-6069	-2593	-3663	-2593	-3071	-2593	-2593
			165	667	-6097	-2621	-3691	-2621	-3099	-2621	-2621
781	Copertura	117-96	0	329	-6326	-2526	-3588	-2526	-3003	-2526	-2526
			82	301	-6354	-2554	-3616	-2554	-3030	-2554	-2554
			165	274	-6381	-2582	-3644	-2582	-3058	-2582	-2582
782	Copertura	118-97	0	380	-5710	-2424	-3434	-2424	-2883	-2424	-2424
			82	352	-5738	-2451	-3462	-2451	-2911	-2451	-2451

			165	324	-5766	-2479	-3489	-2479	-2938	-2479	-2479
783	Copertura	131-98	0	828	-4887	-2030	-2801	-2030	-2384	-2030	-2030
			30	818	-4897	-2040	-2811	-2040	-2394	-2040	-2040
			60	807	-4907	-2050	-2821	-2050	-2404	-2050	-2050
784	Copertura	133-99	0	262	-5145	-2256	-3186	-2256	-2669	-2256	-2256
			30	252	-5156	-2267	-3196	-2267	-2679	-2267	-2267
			60	242	-5166	-2277	-3206	-2277	-2689	-2277	-2277
785	Copertura	139-100	0	369	-5687	-2333	-3323	-2333	-2774	-2333	-2333
			30	358	-5697	-2343	-3333	-2343	-2784	-2343	-2343
			60	348	-5707	-2353	-3343	-2353	-2794	-2353	-2353
786	Copertura	143-101	0	-27	-5611	-2435	-3436	-2435	-2899	-2435	-2435
			30	-37	-5621	-2445	-3446	-2445	-2909	-2445	-2445
			60	-47	-5632	-2455	-3456	-2455	-2919	-2455	-2455
787	Copertura	147-102	0	523	-6198	-2514	-3567	-2514	-2990	-2514	-2514
			30	513	-6208	-2524	-3577	-2524	-3001	-2524	-2524
			60	503	-6218	-2534	-3587	-2534	-3011	-2534	-2534
788	Copertura	151-103	0	628	-5777	-2445	-3453	-2445	-2909	-2445	-2445
			30	618	-5787	-2455	-3463	-2455	-2919	-2455	-2455
			60	608	-5797	-2465	-3473	-2465	-2929	-2465	-2465
789	Copertura	155-104	0	1038	-5811	-2328	-3313	-2328	-2774	-2328	-2328
			30	1027	-5821	-2338	-3323	-2338	-2784	-2338	-2338
			60	1017	-5831	-2348	-3333	-2348	-2794	-2348	-2348
790	Copertura	159-105	0	757	-5363	-2303	-3269	-2303	-2743	-2303	-2303
			30	746	-5373	-2313	-3279	-2313	-2753	-2313	-2313
			60	736	-5383	-2324	-3289	-2324	-2763	-2324	-2324
791	Copertura	119-106	0	8	-5652	-2365	-3390	-2365	-2806	-2365	-2365
			82	-20	-5680	-2393	-3417	-2393	-2834	-2393	-2393
			165	-47	-5707	-2421	-3445	-2421	-2862	-2421	-2421
792	Copertura	120-107	0	-168	-4896	-2205	-3065	-2205	-2605	-2205	-2205
			82	-196	-4923	-2233	-3092	-2233	-2632	-2233	-2233
			165	-224	-4951	-2261	-3120	-2261	-2660	-2261	-2261
793	Copertura	121-108	0	-16	-4174	-2040	-2809	-2040	-2394	-2040	-2040
			82	-43	-4201	-2067	-2837	-2067	-2422	-2067	-2067
			165	-71	-4229	-2095	-2864	-2095	-2449	-2095	-2095
794	Copertura	122-109	0	452	-4480	-1861	-2747	-1861	-2205	-1861	-1861
			82	424	-4507	-1888	-2775	-1888	-2233	-1888	-1888
			165	397	-4535	-1916	-2803	-1916	-2260	-1916	-1916
795	Copertura	123-110	0	1416	-3097	-835	-1292	-840	-1018	-840	-840
			82	1378	-3135	-873	-1330	-878	-1056	-878	-878
			165	1340	-3173	-912	-1369	-916	-1094	-916	-916
796	Copertura	163-111	0	967	-5581	-2307	-3278	-2307	-2746	-2307	-2307
			33	956	-5592	-2318	-3289	-2318	-2757	-2318	-2318
			65	945	-5603	-2329	-3300	-2329	-2768	-2329	-2329
797	Copertura	167-112	0	631	-5241	-2305	-3272	-2305	-2744	-2305	-2305
			30	621	-5251	-2315	-3282	-2315	-2754	-2315	-2315
			60	611	-5261	-2325	-3292	-2325	-2764	-2325	-2325
798	Copertura	171-113	0	983	-5659	-2338	-3318	-2338	-2782	-2338	-2338
			30	973	-5669	-2348	-3328	-2348	-2792	-2348	-2348
			60	963	-5679	-2358	-3338	-2358	-2802	-2358	-2358
799	Copertura	174-114	0	759	-5453	-2347	-3351	-2347	-2794	-2347	-2347
			30	749	-5463	-2357	-3361	-2357	-2804	-2357	-2357
			60	739	-5473	-2367	-3371	-2367	-2814	-2367	-2367
800	Copertura	179-115	0	623	-5403	-2349	-3306	-2349	-2798	-2349	-2349
			30	613	-5413	-2359	-3316	-2359	-2808	-2359	-2359
			60	603	-5423	-2369	-3326	-2369	-2818	-2369	-2369

801	Copertura	183-116	0	313	-5561	-2539	-3554	-2539	-3017	-2539	-2539
			30	303	-5571	-2549	-3564	-2549	-3027	-2549	-2549
			60	293	-5581	-2559	-3574	-2559	-3037	-2559	-2559
802	Copertura	187-117	0	273	-5967	-2501	-3507	-2501	-2978	-2501	-2501
			30	263	-5977	-2511	-3517	-2511	-2989	-2511	-2511
			60	253	-5987	-2521	-3527	-2521	-2999	-2521	-2521
803	Copertura	191-118	0	104	-5423	-2395	-3362	-2395	-2853	-2395	-2395
			30	94	-5433	-2405	-3373	-2405	-2863	-2405	-2405
			60	84	-5443	-2415	-3383	-2415	-2873	-2415	-2415
804	Copertura	194-119	0	-117	-5461	-2347	-3311	-2347	-2790	-2347	-2347
			30	-127	-5471	-2357	-3321	-2357	-2800	-2357	-2357
			60	-137	-5481	-2367	-3331	-2367	-2810	-2367	-2367
805	Copertura	198-120	0	-166	-4747	-2170	-3032	-2170	-2567	-2170	-2170
			30	-176	-4757	-2180	-3042	-2180	-2577	-2180	-2180
			60	-187	-4767	-2190	-3052	-2190	-2587	-2190	-2190
806	Copertura	203-121	0	61	-4396	-2038	-2870	-2038	-2398	-2038	-2038
			30	50	-4406	-2048	-2880	-2048	-2408	-2048	-2048
			60	40	-4416	-2058	-2890	-2058	-2419	-2058	-2058
807	Copertura	207-122	0	91	-3948	-1809	-2621	-1809	-2146	-1809	-1809
			30	81	-3958	-1819	-2631	-1819	-2156	-1819	-1819
			60	71	-3969	-1829	-2641	-1829	-2166	-1829	-1829

1.2.3 Involuppi dei diagrammi delle sollecitazioni: Momento Torcente.

I dati seguenti riportano i valori del Momento Torcente relativamente alle aste che definiscono la struttura ed in modo particolare:

Asta : numerazione interna dell'asta.
X : distanza dal nodo iniziale misurata lungo l'asse dell'asta.
Momento Torcente (M_T) : valore del Momento Torcente nel punto considerato:
Max : valore massimo (rispetto al sistema di riferimento globale) dell'involuppo.
Min : valore minimo (rispetto al sistema di riferimento globale) dell'involuppo.
Comb : combinazione di appartenenza del valore considerato nell'involuppo.

Tabella 28.I

Momento Torcente (Mt) [daNm]											
				SLU		SLE					
						Caratteristiche		Frequenti		Quasi Permanenti	
Asta	Imp.	Fili	X [cm]	Max	Min	Max	Min	Max	Min	Max	Min
1	Fondazione	1-2	0	1185	-1386	-38	-104	-58	-76	-76	-76
			42	1184	-1386	-38	-104	-58	-76	-76	-76
			83	1184	-1386	-38	-104	-58	-76	-76	-76
2	Fondazione	1-2	0	768	-968	-10	-172	-94	-127	-127	-127
			42	768	-968	-10	-172	-94	-127	-127	-127
			83	767	-968	-10	-172	-94	-127	-127	-127
3	Fondazione	1-15	0	1633	-1162	258	139	183	159	168	168
			40	1633	-1162	258	139	183	159	168	168
			80	1633	-1162	258	139	183	159	168	168
4	Fondazione	1-15	0	1883	-785	665	413	519	453	453	453
			40	1883	-785	665	413	519	453	453	453
			80	1883	-784	665	413	519	453	453	453
5	Fondazione	2-3	0	721	-914	-80	-118	-88	-97	-97	-97
			35	721	-914	-80	-118	-88	-97	-97	-97
			69	721	-914	-80	-118	-88	-97	-97	-97
6	Fondazione	2-3	0	380	-234	194	-171	1	-72	-55	-55
			35	380	-234	194	-171	1	-72	-55	-55

			69	380	-234	194	-171	1	-72	-55	-55
7	Fondazio ne	3-4	0	596	-704	9	-116	-27	-52	-42	-42
			35	596	-704	9	-116	-27	-52	-42	-42
			69	596	-704	9	-116	-27	-52	-42	-42
8	Fondazio ne	3-4	0	645	-276	253	-147	40	-40	-17	-17
			35	645	-276	253	-147	40	-40	-17	-17
			69	645	-276	253	-147	40	-40	-17	-17
9	Fondazio ne	4-5	0	582	-678	76	-125	17	-24	-1	-1
			35	582	-678	76	-125	17	-24	-1	-1
			69	582	-678	76	-125	17	-24	-1	-1
10	Fondazio ne	4-5	0	690	-334	270	-131	55	-25	0	0
			35	690	-334	270	-131	55	-25	0	0
			69	690	-334	270	-131	55	-25	0	0
11	Fondazio ne	5-6	0	545	-705	99	-160	25	-27	5	5
			35	545	-705	99	-160	25	-27	5	5
			69	545	-705	99	-160	25	-27	5	5
12	Fondazio ne	5-6	0	607	-268	266	-131	54	-26	0	0
			35	607	-268	266	-131	54	-26	0	0
			69	607	-268	267	-131	54	-26	0	0
13	Fondazio ne	6-7	0	467	-746	118	-195	31	-31	8	8
			35	467	-746	118	-195	31	-31	8	8
			69	467	-746	118	-195	31	-31	8	8
14	Fondazio ne	6-7	0	524	-253	260	-122	56	-20	5	5
			35	524	-253	260	-122	56	-20	5	5
			69	524	-253	260	-122	56	-20	5	5
15	Fondazio ne	7-8	0	463	-736	130	-218	35	-34	11	11
			35	463	-736	130	-218	35	-34	11	11
			69	463	-736	130	-218	35	-34	11	11
16	Fondazio ne	7-8	0	593	-309	233	-120	46	-25	0	0
			35	593	-310	233	-120	46	-25	0	0
			69	593	-310	233	-120	46	-25	0	0
17	Fondazio ne	8-9	0	391	-689	119	-255	19	-56	-6	-6
			35	391	-689	119	-255	19	-56	-6	-6
			69	391	-689	119	-255	19	-56	-6	-6
18	Fondazio ne	8-9	0	391	-179	178	-124	20	-41	-19	-19
			35	391	-179	178	-124	20	-41	-19	-19
			69	391	-179	178	-124	20	-41	-19	-19
19	Fondazio ne	9-10	0	376	-746	115	-277	11	-67	-14	-14
			35	376	-746	115	-277	11	-67	-14	-14
			69	376	-746	115	-277	11	-67	-14	-14
20	Fondazio ne	9-10	0	302	-251	140	-100	16	-32	-13	-13
			35	302	-251	140	-100	16	-32	-13	-13
			69	302	-251	140	-100	16	-32	-13	-13
21	Fondazio ne	10-1 1	0	355	-680	135	-270	28	-53	3	3
			35	355	-680	135	-270	28	-53	3	3
			69	355	-680	135	-270	28	-53	3	3
22	Fondazio ne	10-1 1	0	274	-297	122	-59	29	-7	9	9
			35	274	-297	122	-59	29	-7	9	9
			69	274	-297	122	-59	29	-7	9	9
23	Fondazio ne	11-1 2	0	267	-520	149	-247	44	-35	21	21
			35	267	-520	149	-247	44	-35	21	21
			69	267	-520	149	-247	44	-35	21	21
24	Fondazio ne	11-1 2	0	252	-229	104	-2	49	28	40	40
			35	252	-229	104	-2	49	28	40	40
			69	252	-229	104	-2	49	28	40	40

25	Fondazio ne	12-1 3	0	258	-474	165	-195	69	-3	52	52
			35	258	-474	165	-195	69	-3	52	52
			69	258	-474	165	-195	69	-3	52	52
26	Fondazio ne	12-1 3	0	336	-122	128	92	107	98	107	107
			35	336	-122	128	92	107	98	107	107
			69	336	-122	128	92	107	98	107	107
27	Fondazio ne	13-1 4	0	311	-256	166	-7	118	83	118	118
			42	311	-256	166	-7	118	83	118	118
			83	312	-256	166	-7	118	83	118	118
28	Fondazio ne	13-1 4	0	325	-156	94	42	73	56	73	73
			42	325	-156	94	42	73	56	73	73
			83	325	-156	94	42	73	56	73	73
29	Fondazio ne	14-1 6	0	208	-560	-159	-257	-170	-189	-176	-176
			40	208	-560	-159	-257	-170	-189	-176	-176
			80	208	-560	-159	-258	-170	-190	-176	-176
30	Fondazio ne	14-1 6	0	254	-1124	-396	-636	-435	-497	-435	-435
			40	254	-1124	-396	-636	-435	-497	-435	-435
			80	254	-1124	-396	-637	-435	-497	-435	-435
31	Fondazio ne	15-1 7	0	653	-351	214	123	159	141	149	149
			33	653	-351	214	123	159	141	149	149
			66	653	-351	214	123	159	141	149	149
32	Fondazio ne	15-1 7	0	1504	-488	800	438	606	508	508	508
			33	1504	-488	800	438	606	508	508	508
			66	1504	-488	800	438	606	508	508	508
33	Fondazio ne	16-1 8	0	300	-620	-140	-223	-153	-170	-160	-160
			33	300	-620	-140	-223	-153	-170	-160	-160
			66	300	-620	-140	-223	-153	-170	-160	-160
34	Fondazio ne	16-1 8	0	484	-1483	-435	-783	-500	-594	-500	-500
			33	484	-1483	-435	-783	-500	-594	-500	-500
			66	484	-1483	-435	-783	-500	-595	-500	-500
35	Fondazio ne	17-1 9	0	597	-710	-20	-193	-80	-119	-80	-80
			33	597	-710	-20	-193	-80	-119	-80	-80
			66	597	-710	-20	-193	-80	-119	-80	-80
36	Fondazio ne	17-1 9	0	1519	-794	628	261	448	363	363	363
			33	1519	-794	628	262	448	363	363	363
			66	1519	-794	628	262	448	363	363	363
37	Fondazio ne	18-2 0	0	545	-430	157	1	92	58	58	58
			33	545	-430	157	1	92	57	57	57
			66	545	-430	156	1	92	57	57	57
38	Fondazio ne	18-2 0	0	767	-1495	-261	-641	-364	-453	-364	-364
			33	767	-1495	-261	-641	-364	-453	-364	-364
			66	767	-1495	-261	-641	-364	-453	-364	-364
39	Fondazio ne	19-2 1	0	228	-559	-96	-318	-165	-216	-165	-165
			33	228	-559	-96	-318	-165	-216	-165	-165
			66	228	-559	-96	-318	-165	-216	-165	-165
40	Fondazio ne	19-2 1	0	1544	-997	534	148	355	273	273	273
			33	1544	-998	534	148	356	273	273	273
			66	1544	-998	534	148	356	273	273	273
41	Fondazio ne	20-2 2	0	633	-318	304	86	205	156	156	156
			33	632	-318	304	86	204	156	156	156
			66	632	-318	304	86	204	156	156	156
42	Fondazio ne	20-2 2	0	977	-1542	-163	-549	-282	-366	-282	-282
			33	977	-1542	-163	-549	-282	-366	-282	-282
			66	977	-1542	-163	-549	-282	-366	-282	-282
43	Fondazio	21-2	0	481	-886	-131	-423	-225	-286	-225	-225

	ne	3									
			33	481	-886	-131	-423	-225	-286	-225	-225
			66	481	-886	-131	-423	-225	-286	-225	-225
44	Fondazio ne	21-2 3	0	1636	-1232	440	68	276	202	202	202
			33	1637	-1233	440	68	276	202	202	202
			66	1637	-1233	440	68	276	202	202	202
45	Fondazio ne	22-2 4	0	812	-401	395	111	264	206	206	206
			33	812	-401	395	111	264	205	205	205
			66	812	-401	395	111	263	205	205	205
46	Fondazio ne	22-2 4	0	1118	-1567	-105	-467	-224	-300	-224	-224
			33	1118	-1567	-105	-467	-224	-300	-224	-224
			66	1118	-1567	-105	-467	-224	-300	-224	-224
47	Fondazio ne	23-2 5	0	779	-1411	-186	-591	-316	-401	-316	-316
			33	779	-1411	-186	-591	-316	-401	-316	-316
			66	779	-1411	-186	-591	-316	-401	-316	-316
48	Fondazio ne	23-2 5	0	899	-731	187	13	114	79	84	84
			33	899	-732	187	13	114	79	84	84
			66	899	-732	187	13	114	79	84	84
49	Fondazio ne	24-2 6	0	1208	-699	496	130	327	253	254	254
			33	1208	-699	496	130	327	253	254	254
			66	1208	-699	496	130	326	253	254	254
50	Fondazio ne	24-2 6	0	856	-1120	-60	-278	-132	-178	-132	-132
			33	856	-1121	-60	-278	-132	-178	-132	-132
			66	856	-1121	-60	-278	-132	-178	-132	-132
51	Fondazio ne	25-2 6	0	270	-174	68	48	56	48	48	48
			49	270	-174	68	48	56	48	48	48
			97	270	-174	68	48	56	48	48	48
52	Fondazio ne	25-2 6	0	216	-168	33	24	28	24	24	24
			49	216	-168	33	24	28	24	24	24
			97	216	-168	33	24	28	24	24	24
53	Fondazio ne	25-2 6	0	142	-123	14	7	11	9	9	9
			49	142	-123	14	7	11	9	9	9
			97	142	-123	14	7	11	9	9	9
54	Fondazio ne	25-2 6	0	98	-87	8	4	6	5	6	6
			49	98	-87	8	4	6	5	6	6
			97	98	-87	8	4	6	5	6	6
55	Fondazio ne	25-2 6	0	69	-63	4	2	3	2	3	3
			49	69	-63	4	2	3	2	3	3
			97	69	-63	4	2	3	2	3	3
56	Fondazio ne	25-2 6	0	41	-38	2	1	2	1	1	1
			49	41	-38	2	1	2	1	1	1
			97	41	-38	2	1	2	1	1	1
57	Fondazio ne	25-2 6	0	22	-20	2	1	1	1	1	1
			49	22	-20	2	1	1	1	1	1
			97	22	-20	2	1	1	1	1	1
58	Fondazio ne	25-2 6	0	10	-8	1	1	1	1	1	1
			49	10	-8	1	1	1	1	1	1
			97	10	-8	1	1	1	1	1	1
59	Fondazio ne	25-2 6	0	7	-4	2	1	2	1	1	1
			49	7	-4	2	1	2	1	1	1
			97	7	-4	2	1	2	1	1	1
60	Fondazio ne	25-2 6	0	3	-11	-4	-6	-4	-5	-4	-4
			49	3	-11	-4	-6	-4	-5	-4	-4
			97	3	-11	-4	-6	-4	-5	-4	-4
61	Fondazio ne	25-2 6	0	7	-5	1	1	1	1	1	1

			49	7	-5	1	1	1	1	1	1
			97	7	-5	1	1	1	1	1	1
62	Fondazio ne	25-2 6	0	9	-10	0	0	0	0	0	0
			49	9	-10	0	0	0	0	0	0
			97	9	-10	0	0	0	0	0	0
63	Fondazio ne	25-2 6	0	20	-22	-1	-2	-1	-1	-1	-1
			49	20	-22	-1	-2	-1	-1	-1	-1
			97	20	-22	-1	-2	-1	-1	-1	-1
64	Fondazio ne	25-2 6	0	38	-43	-1	-4	-2	-3	-2	-2
			49	38	-43	-1	-4	-2	-3	-2	-2
			97	38	-43	-1	-4	-2	-3	-2	-2
65	Fondazio ne	25-2 6	0	60	-66	-2	-5	-3	-4	-3	-3
			49	60	-66	-2	-5	-3	-4	-3	-3
			97	60	-66	-2	-5	-3	-4	-3	-3
66	Fondazio ne	25-2 6	0	75	-79	0	-4	-2	-2	-2	-2
			49	75	-79	0	-4	-2	-2	-2	-2
			97	75	-79	0	-4	-2	-2	-2	-2
67	Fondazio ne	25-2 6	0	87	-84	3	1	2	1	1	1
			49	87	-84	3	1	2	1	1	1
			97	87	-84	3	1	2	1	1	1
68	Fondazio ne	25-2 6	0	200	-192	11	0	6	4	4	4
			49	200	-192	11	0	6	4	4	4
			97	200	-192	11	0	6	4	4	4
69	Fondazio ne	25-2 6	0	303	-293	18	-4	8	4	5	5
			49	303	-293	18	-4	8	4	5	5
			97	303	-293	18	-4	8	4	5	5
70	Fondazio ne	25-2 8	0	472	-829	-133	-319	-184	-230	-184	-184
			43	472	-829	-133	-319	-184	-230	-184	-184
			85	472	-829	-133	-319	-184	-230	-184	-184
71	Fondazio ne	25-2 8	0	2072	-1526	553	107	354	264	273	273
			43	2072	-1526	553	107	354	265	273	273
			85	2073	-1526	553	107	354	265	273	273
72	Fondazio ne	26-2 7	0	443	-204	226	77	156	120	120	120
			33	443	-204	226	77	156	120	120	120
			66	443	-204	226	77	156	120	120	120
73	Fondazio ne	26-2 7	0	1575	-2120	-109	-566	-265	-357	-272	-272
			33	1576	-2120	-109	-566	-266	-357	-272	-272
			66	1576	-2120	-109	-567	-266	-357	-272	-272
74	Fondazio ne	27-2 9	0	1188	-797	403	95	261	195	195	195
			33	1187	-797	402	95	261	195	195	195
			66	1187	-797	402	95	261	195	195	195
75	Fondazio ne	27-2 9	0	1555	-2036	-95	-501	-235	-316	-241	-241
			33	1555	-2036	-95	-501	-235	-316	-241	-241
			66	1555	-2037	-95	-501	-235	-316	-241	-241
76	Fondazio ne	28-3 0	0	827	-1185	-58	-386	-178	-244	-179	-179
			37	827	-1185	-57	-386	-178	-244	-179	-179
			73	827	-1185	-57	-386	-178	-244	-179	-179
77	Fondazio ne	28-3 0	0	2125	-1587	543	117	350	264	269	269
			37	2125	-1587	543	117	350	264	269	269
			73	2125	-1587	543	117	350	264	269	269
78	Fondazio ne	29-3 1	0	1422	-987	449	103	290	218	218	218
			33	1422	-987	449	103	290	218	218	218
			66	1422	-987	448	103	290	218	218	218
79	Fondazio ne	29-3 1	0	1514	-1963	-90	-467	-220	-296	-225	-225
			33	1514	-1963	-90	-467	-220	-296	-225	-225

			66	1514	-1964	-90	-467	-220	-296	-225	-225
80	Fondazio ne	30-3 2	0	1075	-1476	-71	-421	-198	-268	-201	-201
			34	1075	-1476	-71	-421	-198	-268	-201	-201
			69	1075	-1476	-71	-421	-198	-268	-200	-200
81	Fondazio ne	30-3 2	0	2075	-1571	519	109	332	250	252	252
			34	2075	-1571	519	109	332	250	252	252
			69	2075	-1571	519	109	332	250	252	252
82	Fondazio ne	31-3 3	0	1628	-1183	461	100	295	223	223	223
			33	1628	-1183	461	100	295	222	222	222
			66	1628	-1183	461	100	295	222	222	222
83	Fondazio ne	31-3 3	0	1421	-1863	-96	-453	-219	-291	-221	-221
			33	1421	-1863	-96	-453	-219	-291	-221	-221
			66	1421	-1863	-96	-453	-219	-291	-221	-221
84	Fondazio ne	32-3 4	0	1171	-1625	-89	-468	-224	-300	-227	-227
			35	1171	-1625	-89	-468	-224	-300	-227	-227
			69	1171	-1625	-89	-468	-224	-300	-227	-227
85	Fondazio ne	32-3 4	0	1894	-1397	488	128	321	249	249	249
			35	1894	-1397	488	128	321	249	249	249
			69	1895	-1397	489	128	322	249	249	249
86	Fondazio ne	33-3 5	0	1723	-1280	462	96	294	221	222	222
			33	1723	-1280	462	96	294	221	222	222
			66	1723	-1280	462	96	294	221	222	222
87	Fondazio ne	33-3 5	0	1364	-1802	-101	-442	-219	-287	-219	-219
			33	1364	-1802	-101	-442	-219	-288	-219	-219
			66	1364	-1802	-101	-443	-219	-288	-219	-219
88	Fondazio ne	34-3 6	0	1323	-1747	-74	-446	-207	-282	-212	-212
			35	1323	-1747	-74	-446	-207	-282	-212	-212
			69	1323	-1747	-74	-446	-207	-282	-212	-212
89	Fondazio ne	34-3 6	0	1876	-1391	485	125	318	243	243	243
			35	1876	-1391	485	125	318	243	243	243
			69	1877	-1391	485	125	318	243	243	243
90	Fondazio ne	35-3 7	0	1802	-1359	462	92	293	219	222	222
			33	1802	-1359	462	92	293	219	222	222
			66	1802	-1359	462	92	293	219	221	221
91	Fondazio ne	35-3 7	0	1234	-1673	-106	-439	-219	-288	-219	-219
			33	1234	-1673	-106	-439	-219	-288	-219	-219
			66	1234	-1673	-106	-439	-219	-288	-219	-219
92	Fondazio ne	36-3 8	0	1355	-1759	-60	-431	-194	-269	-202	-202
			35	1355	-1759	-60	-431	-194	-269	-202	-202
			69	1355	-1759	-60	-431	-194	-268	-202	-202
93	Fondazio ne	36-3 8	0	1843	-1323	507	152	339	260	260	260
			35	1843	-1323	507	152	339	260	260	260
			69	1843	-1323	507	152	339	260	260	260
94	Fondazio ne	37-3 9	0	1844	-1394	467	93	296	222	225	225
			33	1844	-1394	467	93	296	222	225	225
			66	1844	-1393	466	93	296	222	225	225
95	Fondazio ne	37-3 9	0	1204	-1631	-105	-428	-214	-282	-214	-214
			33	1204	-1631	-105	-428	-214	-282	-214	-214
			66	1204	-1631	-105	-428	-214	-282	-214	-214
96	Fondazio ne	38-4 0	0	1364	-1721	-36	-393	-167	-239	-179	-179
			34	1364	-1721	-36	-393	-167	-238	-179	-179
			69	1363	-1721	-36	-393	-167	-238	-179	-179
97	Fondazio ne	38-4 0	0	1841	-1278	538	187	366	282	282	282
			34	1841	-1278	538	187	366	282	282	282
			69	1842	-1278	538	187	366	282	282	282

98	Fondazio ne	39-4 1	0	1958	-1471	494	105	316	239	243	243
			33	1957	-1471	493	104	316	239	243	243
			66	1957	-1471	493	104	316	239	243	243
99	Fondazio ne	39-4 1	0	989	-1379	-98	-392	-195	-259	-195	-195
			33	989	-1379	-98	-392	-195	-259	-195	-195
			66	989	-1379	-98	-392	-195	-259	-195	-195
100	Fondazio ne	40-4 2	0	1440	-1733	-5	-343	-131	-199	-146	-146
			35	1440	-1732	-5	-343	-131	-199	-146	-146
			69	1440	-1732	-5	-343	-131	-199	-146	-146
101	Fondazio ne	40-4 2	0	1921	-1209	640	272	451	356	356	356
			35	1921	-1209	641	273	451	356	356	356
			69	1921	-1209	641	273	451	356	356	356
102	Fondazio ne	41-4 4	0	2161	-1649	527	102	335	250	256	256
			33	2161	-1649	527	102	335	250	256	256
			66	2161	-1649	527	102	335	250	256	256
103	Fondazio ne	41-4 4	0	424	-690	-86	-245	-133	-171	-133	-133
			33	424	-690	-87	-245	-133	-171	-133	-133
			66	425	-690	-87	-245	-133	-171	-133	-133
104	Fondazio ne	42-4 3	0	1258	-1498	-16	-293	-113	-168	-120	-120
			23	1258	-1498	-16	-292	-113	-168	-120	-120
			46	1258	-1498	-16	-292	-113	-168	-120	-120
105	Fondazio ne	43-4 4	0	443	-336	79	44	60	49	49	49
			49	443	-336	79	44	60	49	49	49
			97	443	-336	79	44	60	49	49	49
106	Fondazio ne	43-4 4	0	212	-209	9	-3	4	2	3	3
			49	212	-209	9	-3	4	2	3	3
			97	212	-209	9	-3	4	2	3	3
107	Fondazio ne	43-4 4	0	95	-110	-7	-11	-7	-9	-7	-7
			49	95	-110	-7	-11	-7	-9	-7	-7
			97	95	-110	-7	-11	-7	-9	-7	-7
108	Fondazio ne	43-4 4	0	68	-75	-2	-5	-3	-3	-3	-3
			49	68	-75	-2	-5	-3	-3	-3	-3
			97	68	-75	-2	-5	-3	-3	-3	-3
109	Fondazio ne	43-4 4	0	50	-51	0	-2	0	-1	-1	-1
			49	50	-51	0	-2	0	-1	-1	-1
			97	50	-51	0	-2	0	-1	-1	-1
110	Fondazio ne	43-4 4	0	31	-31	0	-1	0	0	0	0
			49	31	-31	0	-1	0	0	0	0
			97	31	-31	0	-1	0	0	0	0
111	Fondazio ne	43-4 4	0	16	-17	0	-1	0	-1	0	0
			49	16	-17	0	-1	0	-1	0	0
			97	16	-17	0	-1	0	-1	0	0
112	Fondazio ne	43-4 4	0	9	-10	-1	-1	-1	-1	-1	-1
			49	9	-10	-1	-1	-1	-1	-1	-1
			97	9	-10	-1	-1	-1	-1	-1	-1
113	Fondazio ne	43-4 4	0	5	-7	-1	-1	-1	-1	-1	-1
			49	5	-7	-1	-1	-1	-1	-1	-1
			97	5	-7	-1	-1	-1	-1	-1	-1
114	Fondazio ne	43-4 4	0	8	-5	3	2	2	2	2	2
			49	8	-5	3	2	2	2	2	2
			97	8	-5	3	2	2	2	2	2
115	Fondazio ne	43-4 4	0	4	-5	-1	-1	-1	-1	-1	-1
			49	4	-5	-1	-1	-1	-1	-1	-1
			97	4	-5	-1	-1	-1	-1	-1	-1
116	Fondazio	43-4	0	9	-7	1	1	1	1	1	1

	ne	4									
			49	9	-7	1	1	1	1	1	1
			97	9	-7	1	1	1	1	1	1
117	Fondazio ne	43-4 4	0	24	-22	2	1	1	1	1	1
			49	24	-22	2	1	1	1	1	1
			97	24	-22	2	1	1	1	1	1
118	Fondazio ne	43-4 4	0	48	-44	4	1	2	2	2	2
			49	48	-44	4	1	2	2	2	2
			97	48	-44	4	1	2	2	2	2
119	Fondazio ne	43-4 4	0	78	-74	4	1	3	2	2	2
			49	78	-74	4	1	3	2	2	2
			97	78	-74	4	1	3	2	2	2
120	Fondazio ne	43-4 4	0	108	-102	5	2	4	3	3	3
			49	108	-102	5	2	4	3	3	3
			97	108	-102	5	2	4	3	3	3
121	Fondazio ne	43-4 4	0	125	-122	3	1	2	1	1	1
			49	125	-122	3	1	2	1	1	1
			97	125	-122	3	1	2	1	1	1
122	Fondazio ne	43-4 4	0	214	-206	13	-2	6	3	4	4
			49	214	-206	13	-2	6	3	4	4
			97	214	-206	13	-2	6	3	4	4
123	Fondazio ne	43-4 4	0	212	-193	15	8	11	9	10	10
			49	212	-193	15	8	11	9	10	10
			97	212	-193	15	8	11	9	10	10
124	Fondazio ne	43-4 5	0	1192	-1677	-181	-439	-243	-308	-243	-243
			33	1192	-1677	-181	-439	-243	-308	-243	-243
			66	1192	-1677	-181	-439	-243	-308	-243	-243
125	Fondazio ne	43-4 5	0	1306	-933	393	64	246	180	186	186
			33	1306	-933	393	64	246	180	186	186
			66	1306	-933	393	64	246	180	187	187
126	Fondazio ne	44-4 6	0	951	-696	245	72	165	128	128	128
			33	951	-696	245	72	165	128	128	128
			66	951	-696	245	72	165	128	128	128
127	Fondazio ne	44-4 6	0	1189	-1795	-159	-581	-302	-387	-303	-303
			33	1189	-1795	-159	-581	-302	-387	-303	-303
			66	1189	-1795	-159	-581	-302	-387	-303	-303
128	Fondazio ne	45-4 7	0	1458	-2051	-188	-571	-296	-385	-296	-296
			33	1458	-2050	-188	-571	-296	-385	-296	-296
			66	1458	-2050	-188	-571	-296	-385	-296	-296
129	Fondazio ne	45-4 7	0	917	-545	363	84	237	181	186	186
			33	917	-545	363	84	237	182	186	186
			66	917	-545	363	84	237	182	186	186
130	Fondazio ne	46-4 8	0	1826	-1385	458	97	296	221	221	221
			33	1826	-1385	458	97	296	221	221	221
			66	1826	-1385	458	97	296	221	221	221
131	Fondazio ne	46-4 8	0	658	-1137	-134	-449	-239	-303	-239	-239
			33	658	-1137	-134	-449	-239	-303	-239	-239
			66	658	-1137	-134	-449	-240	-303	-240	-240
132	Fondazio ne	47-4 9	0	1354	-1900	-162	-532	-273	-355	-273	-273
			33	1354	-1900	-162	-532	-273	-355	-273	-273
			66	1354	-1900	-162	-532	-273	-355	-273	-273
133	Fondazio ne	47-4 9	0	856	-487	344	81	226	173	173	173
			33	856	-487	344	81	226	173	173	173
			66	856	-487	344	81	226	173	173	173
134	Fondazio ne	48-5 0	0	1872	-1380	503	117	327	246	246	246

			33	1872	-1380	503	117	327	246	246	246
			66	1872	-1380	503	117	327	246	246	246
135	Fondazio ne	48-5 0	0	383	-773	-105	-375	-195	-252	-195	-195
			33	383	-773	-106	-375	-195	-252	-195	-195
			66	383	-774	-106	-376	-195	-252	-195	-195
136	Fondazio ne	49-5 1	0	1111	-1719	-192	-574	-304	-390	-304	-304
			33	1111	-1719	-192	-574	-304	-390	-304	-304
			66	1111	-1719	-192	-574	-304	-390	-304	-304
137	Fondazio ne	49-5 1	0	614	-324	288	74	192	145	145	145
			33	614	-325	288	74	192	145	145	145
			66	614	-325	288	74	192	145	145	145
138	Fondazio ne	50-5 2	0	1747	-1132	578	186	394	308	308	308
			33	1747	-1132	578	186	394	308	308	308
			66	1747	-1132	578	186	393	308	308	308
139	Fondazio ne	50-5 2	0	326	-617	-74	-292	-145	-194	-145	-145
			33	326	-617	-74	-292	-145	-194	-145	-145
			66	326	-617	-74	-292	-145	-194	-145	-145
140	Fondazio ne	51-5 3	0	950	-1700	-277	-654	-375	-466	-375	-375
			33	950	-1700	-277	-654	-375	-465	-375	-375
			66	949	-1700	-277	-654	-375	-465	-375	-375
141	Fondazio ne	51-5 3	0	816	-645	153	-3	89	55	55	55
			33	816	-645	153	-3	89	55	55	55
			66	816	-645	153	-3	89	55	55	55
142	Fondazio ne	52-5 4	0	1625	-856	663	284	476	385	385	385
			33	1625	-856	663	284	475	385	385	385
			66	1625	-856	663	284	475	385	385	385
143	Fondazio ne	52-5 4	0	328	-442	2	-159	-57	-92	-57	-57
			33	328	-442	2	-159	-57	-92	-57	-57
			66	328	-442	2	-159	-57	-92	-57	-57
144	Fondazio ne	53-5 5	0	601	-1623	-451	-798	-511	-607	-511	-511
			33	601	-1623	-451	-798	-511	-607	-511	-511
			66	601	-1623	-451	-798	-511	-606	-511	-511
145	Fondazio ne	53-5 5	0	396	-727	-145	-232	-159	-176	-166	-166
			33	396	-727	-145	-232	-159	-176	-166	-166
			66	396	-727	-145	-232	-159	-176	-165	-165
146	Fondazio ne	54-5 6	0	1553	-548	786	438	597	502	502	502
			33	1553	-548	785	438	596	502	502	502
			66	1553	-548	785	438	596	502	502	502
147	Fondazio ne	54-5 6	0	516	-218	214	122	158	140	149	149
			33	516	-218	214	121	158	140	149	149
			66	516	-218	214	121	158	140	149	149
148	Fondazio ne	55-5 7	0	955	-1955	-407	-646	-442	-505	-442	-442
			40	955	-1955	-407	-646	-442	-505	-442	-442
			80	955	-1955	-407	-646	-442	-505	-442	-442
149	Fondazio ne	55-5 7	0	1099	-1468	-154	-271	-172	-195	-179	-179
			40	1099	-1468	-153	-271	-172	-195	-179	-179
			80	1099	-1469	-153	-271	-172	-195	-179	-179
150	Fondazio ne	56-7 0	0	1066	-193	638	400	499	436	436	436
			40	1066	-193	637	400	499	436	436	436
			80	1066	-193	637	400	499	436	436	436
151	Fondazio ne	56-7 0	0	530	-153	258	152	188	167	174	174
			40	530	-153	258	152	188	167	174	174
			80	530	-153	258	152	188	167	173	173
152	Fondazio ne	57-5 8	0	1294	-1141	103	40	76	59	76	76
			42	1294	-1141	103	40	76	59	76	76

			83	1293	-1141	103	40	76	59	76	76
153	Fondazio ne	57-5 8	0	1078	-883	164	4	121	88	121	121
			42	1078	-883	164	4	121	88	121	121
			83	1078	-883	164	4	121	88	121	121
154	Fondazio ne	58-5 9	0	919	-689	134	89	108	98	108	108
			35	919	-689	134	89	108	98	108	108
			69	919	-689	134	89	108	98	108	108
155	Fondazio ne	58-5 9	0	266	-293	170	-198	71	-3	53	53
			35	266	-293	170	-198	71	-3	53	53
			69	266	-293	170	-198	71	-3	53	53
156	Fondazio ne	59-6 0	0	666	-589	105	-7	48	26	38	38
			35	666	-589	105	-7	48	26	38	38
			69	666	-588	105	-7	48	26	38	38
157	Fondazio ne	59-6 0	0	457	-262	153	-252	45	-36	20	20
			35	457	-262	153	-252	45	-36	20	20
			69	457	-262	153	-252	45	-36	20	20
158	Fondazio ne	60-6 1	0	568	-545	138	-67	34	-7	11	11
			35	568	-545	138	-67	34	-7	11	11
			69	568	-545	138	-67	34	-7	11	11
159	Fondazio ne	60-6 1	0	394	-303	131	-261	27	-51	3	3
			35	394	-303	131	-261	27	-51	3	3
			69	394	-303	131	-261	27	-51	3	3
160	Fondazio ne	61-6 2	0	526	-693	154	-108	19	-33	-13	-13
			35	526	-693	154	-108	19	-33	-13	-13
			69	526	-693	153	-108	19	-33	-13	-13
161	Fondazio ne	61-6 2	0	320	-323	115	-275	12	-66	-13	-13
			35	320	-323	115	-275	12	-66	-13	-13
			69	320	-323	115	-275	12	-66	-13	-13
162	Fondazio ne	62-6 3	0	408	-543	184	-133	19	-44	-20	-20
			35	408	-543	184	-133	19	-44	-20	-20
			69	408	-543	184	-133	19	-44	-20	-20
163	Fondazio ne	62-6 3	0	407	-248	109	-256	12	-61	-12	-12
			35	407	-248	109	-257	12	-61	-12	-12
			69	407	-248	109	-257	12	-61	-12	-12
164	Fondazio ne	63-6 4	0	462	-481	221	-126	38	-31	-7	-7
			35	462	-481	221	-126	38	-31	-7	-7
			69	461	-481	221	-126	38	-31	-7	-7
165	Fondazio ne	63-6 4	0	472	-285	123	-217	31	-37	7	7
			35	472	-285	123	-217	31	-37	7	7
			69	472	-285	123	-217	31	-37	7	7
166	Fondazio ne	64-6 5	0	398	-421	259	-112	62	-13	12	12
			35	398	-421	259	-112	62	-13	12	12
			69	398	-421	259	-112	62	-13	12	12
167	Fondazio ne	64-6 5	0	325	-147	129	-180	43	-18	20	20
			35	325	-147	129	-180	43	-18	20	20
			69	325	-147	129	-180	43	-18	20	20
168	Fondazio ne	65-6 6	0	419	-586	276	-115	66	-12	13	13
			35	419	-586	276	-115	66	-12	13	13
			69	419	-586	276	-115	66	-12	13	13
169	Fondazio ne	65-6 6	0	201	-156	105	-150	33	-18	13	13
			35	201	-156	105	-150	33	-18	13	13
			69	201	-156	105	-150	33	-18	13	13
170	Fondazio ne	66-6 7	0	317	-510	266	-134	52	-28	-3	-3
			35	317	-510	266	-134	52	-28	-3	-3
			69	317	-510	266	-134	52	-28	-3	-3

171	Fondazio ne	66-6 7	0	264	-182	59	-122	7	-29	-8	-8
			35	264	-182	59	-122	7	-29	-8	-8
			69	264	-182	59	-122	7	-29	-8	-8
172	Fondazio ne	67-6 8	0	218	-382	243	-146	35	-43	-20	-20
			35	218	-382	243	-146	35	-43	-20	-20
			69	218	-382	243	-146	35	-43	-20	-20
173	Fondazio ne	67-6 8	0	146	-276	2	-102	-27	-48	-40	-40
			35	146	-276	2	-102	-27	-48	-40	-40
			69	146	-276	2	-102	-27	-48	-40	-40
174	Fondazio ne	68-6 9	0	158	-379	190	-160	3	-67	-51	-51
			35	158	-379	190	-160	3	-67	-51	-51
			69	158	-378	190	-160	3	-67	-51	-51
175	Fondazio ne	68-6 9	0	96	-293	-89	-129	-97	-106	-106	-106
			35	96	-293	-89	-129	-97	-106	-106	-106
			69	96	-293	-89	-129	-97	-106	-106	-106
176	Fondazio ne	69-7 0	0	113	-414	4	-157	-81	-115	-115	-115
			42	113	-414	4	-157	-81	-115	-115	-115
			83	113	-414	4	-157	-81	-115	-115	-115
177	Fondazio ne	69-7 0	0	183	-329	-42	-97	-57	-74	-74	-74
			42	183	-329	-42	-97	-57	-74	-74	-74
			83	183	-329	-42	-97	-57	-74	-74	-74
178	Primo Impalcat o	1-2	0	126	-113	17	-10	3	-2	0	0
			83	126	-113	17	-10	3	-2	0	0
			166	126	-113	17	-10	3	-2	0	0
179	Primo Impalcat o	1-15	0	46	-12	28	17	21	17	17	17
			80	46	-12	28	17	21	17	17	17
			159	46	-12	28	17	21	17	17	17
180	Primo Impalcat o	2-3	0	21	-17	17	-9	3	-2	0	0
			69	21	-17	17	-9	3	-2	0	0
			138	21	-17	17	-9	3	-2	0	0
181	Primo Impalcat o	3-4	0	20	-18	15	-8	3	-2	-1	-1
			69	20	-18	15	-8	3	-2	-1	-1
			138	20	-18	15	-8	3	-2	-1	-1
182	Primo Impalcat o	4-5	0	25	-24	13	-7	2	-2	0	0
			69	25	-24	13	-7	2	-2	0	0
			138	25	-24	13	-7	2	-2	0	0
183	Primo Impalcat o	5-6	0	25	-25	9	-4	2	-1	0	0
			69	25	-25	9	-4	2	-1	0	0
			138	25	-25	9	-4	2	-1	0	0
184	Primo Impalcat o	6-7	0	21	-22	5	-2	1	0	0	0
			69	21	-22	5	-2	1	0	0	0
			138	21	-22	5	-2	1	0	0	0
185	Primo Impalcat o	7-8	0	26	-26	1	-1	0	0	0	0
			69	26	-26	1	-1	0	0	0	0
			138	26	-26	1	-1	0	0	0	0
186	Primo Impalcat o	8-9	0	25	-29	3	-5	1	-1	0	0
			69	25	-29	3	-5	1	-1	0	0
			138	25	-29	3	-5	1	-1	0	0
187	Primo	9-10	0	27	-38	5	-10	1	-2	0	0

	Impalcat o										
			69	27	-38	5	-10	1	-2	0	0
			138	27	-38	5	-10	1	-2	0	0
188	Primo Impalcat o	10-1 1	0	28	-45	7	-14	2	-3	0	0
			69	28	-45	7	-14	2	-3	0	0
			138	28	-45	7	-14	2	-3	0	0
189	Primo Impalcat o	11-1 2	0	23	-42	9	-16	2	-3	1	1
			69	23	-42	9	-16	2	-3	1	1
			138	23	-42	9	-16	2	-3	1	1
190	Primo Impalcat o	12-1 3	0	24	-44	9	-17	2	-3	0	0
			69	24	-44	9	-17	2	-3	0	0
			138	24	-44	9	-17	2	-3	0	0
191	Primo Impalcat o	13-1 4	0	28	-42	9	-15	2	-3	0	0
			83	28	-42	9	-15	2	-3	0	0
			166	28	-42	9	-15	2	-3	0	0
192	Primo Impalcat o	14-1 6	0	12	-46	-16	-27	-17	-20	-17	-17
			80	12	-46	-16	-27	-17	-20	-17	-17
			159	12	-46	-16	-27	-17	-20	-17	-17
193	Primo Impalcat o	15-1 7	0	34	-30	7	-2	3	1	2	2
			66	34	-30	7	-2	3	1	2	2
			132	34	-30	7	-2	3	1	2	2
194	Primo Impalcat o	16-1 8	0	30	-34	2	-8	-2	-4	-2	-2
			66	30	-34	2	-8	-2	-4	-2	-2
			132	30	-34	2	-8	-2	-4	-2	-2
195	Primo Impalcat o	17-1 9	0	31	-31	4	-4	1	-1	0	0
			66	31	-31	4	-4	1	-1	0	0
			132	31	-31	4	-4	1	-1	0	0
196	Primo Impalcat o	18-2 0	0	30	-30	4	-4	1	-1	0	0
			66	30	-30	4	-4	1	-1	0	0
			132	30	-30	4	-4	1	-1	0	0
197	Primo Impalcat o	19-2 1	0	31	-32	3	-3	0	-1	0	0
			66	31	-32	3	-3	0	-1	0	0
			132	31	-32	3	-3	0	-1	0	0
198	Primo Impalcat o	20-2 2	0	32	-32	3	-3	1	0	0	0
			66	32	-32	3	-3	1	0	0	0
			132	32	-32	3	-3	1	0	0	0
199	Primo Impalcat o	21-2 3	0	30	-30	2	-2	0	0	0	0
			66	30	-30	2	-2	0	0	0	0
			132	30	-30	2	-2	0	0	0	0
200	Primo Impalcat o	22-2 4	0	31	-30	2	-2	0	0	0	0
			66	31	-30	2	-2	0	0	0	0
			132	31	-30	2	-2	0	0	0	0
201	Primo Impalcat o	23-2 5	0	30	-29	1	-1	0	0	0	0
			66	30	-29	1	-1	0	0	0	0
			132	30	-29	1	-1	0	0	0	0

202	Primo Impalcato	24-26	0	30	-30	1	-1	0	0	0	0
			66	30	-30	1	-1	0	0	0	0
			132	30	-30	1	-1	0	0	0	0
203	Primo Impalcato	25-28	0	22	-22	0	-1	0	0	0	0
			85	22	-22	0	-1	0	0	0	0
			170	22	-22	0	-1	0	0	0	0
204	Primo Impalcato	26-27	0	29	-29	1	-1	0	0	0	0
			66	29	-29	1	-1	0	0	0	0
			132	29	-29	1	-1	0	0	0	0
205	Primo Impalcato	27-29	0	23	-23	0	0	0	0	0	0
			66	23	-23	0	0	0	0	0	0
			132	23	-23	0	0	0	0	0	0
206	Primo Impalcato	28-30	0	20	-20	0	0	0	0	0	0
			73	20	-20	0	0	0	0	0	0
			146	20	-20	0	0	0	0	0	0
207	Primo Impalcato	29-31	0	17	-17	0	0	0	0	0	0
			66	17	-17	0	0	0	0	0	0
			132	17	-17	0	0	0	0	0	0
208	Primo Impalcato	30-32	0	16	-16	0	0	0	0	0	0
			69	16	-16	0	0	0	0	0	0
			137	16	-16	0	0	0	0	0	0
209	Primo Impalcato	31-33	0	12	-12	0	0	0	0	0	0
			66	12	-12	0	0	0	0	0	0
			132	12	-12	0	0	0	0	0	0
210	Primo Impalcato	32-34	0	10	-10	0	0	0	0	0	0
			69	10	-10	0	0	0	0	0	0
			138	10	-10	0	0	0	0	0	0
211	Primo Impalcato	33-35	0	9	-9	0	0	0	0	0	0
			66	9	-9	0	0	0	0	0	0
			132	9	-9	0	0	0	0	0	0
212	Primo Impalcato	34-36	0	7	-7	0	0	0	0	0	0
			69	7	-7	0	0	0	0	0	0
			138	7	-7	0	0	0	0	0	0
213	Primo Impalcato	35-37	0	9	-9	1	0	0	0	0	0
			66	9	-9	1	0	0	0	0	0
			132	9	-9	1	0	0	0	0	0
214	Primo Impalcato	36-38	0	7	-7	1	0	0	0	0	0
			69	7	-7	1	0	0	0	0	0
			138	7	-7	1	0	0	0	0	0
215	Primo Impalcato	37-39	0	14	-14	0	0	0	0	0	0
			66	14	-14	0	0	0	0	0	0
			132	14	-14	0	0	0	0	0	0
216	Primo Impalcato	38-40	0	13	-13	1	0	0	0	0	0
			69	13	-13	1	0	0	0	0	0

			137	13	-13	1	0	0	0	0	0
217	Primo Impalcato	39-41	0	16	-16	0	0	0	0	0	0
			66	16	-16	0	0	0	0	0	0
			132	16	-16	0	0	0	0	0	0
218	Primo Impalcato	40-42	0	17	-17	1	-1	0	0	0	0
			69	17	-17	1	-1	0	0	0	0
			138	17	-17	1	-1	0	0	0	0
219	Primo Impalcato	41-44	0	15	-15	0	0	0	0	0	0
			66	15	-15	0	0	0	0	0	0
			132	15	-15	0	0	0	0	0	0
220	Primo Impalcato	42-43	0	36	-35	1	0	0	0	0	0
			23	36	-35	1	0	0	0	0	0
			46	36	-35	1	0	0	0	0	0
221	Primo Impalcato	43-45	0	24	-24	0	0	0	0	0	0
			66	24	-24	0	0	0	0	0	0
			132	24	-24	0	0	0	0	0	0
222	Primo Impalcato	44-46	0	23	-23	1	0	0	0	0	0
			66	23	-23	1	0	0	0	0	0
			132	23	-23	1	0	0	0	0	0
223	Primo Impalcato	45-47	0	29	-29	1	-1	0	0	0	0
			66	29	-29	1	-1	0	0	0	0
			132	29	-29	1	-1	0	0	0	0
224	Primo Impalcato	46-48	0	30	-30	1	-1	0	0	0	0
			66	30	-30	1	-1	0	0	0	0
			132	30	-30	1	-1	0	0	0	0
225	Primo Impalcato	47-49	0	31	-31	2	-2	0	0	0	0
			66	31	-31	2	-2	0	0	0	0
			132	31	-31	2	-2	0	0	0	0
226	Primo Impalcato	48-50	0	31	-31	1	-2	0	0	0	0
			66	31	-31	1	-2	0	0	0	0
			132	31	-31	1	-2	0	0	0	0
227	Primo Impalcato	49-51	0	35	-34	3	-2	1	0	0	0
			66	35	-34	3	-2	1	0	0	0
			132	35	-34	3	-2	1	0	0	0
228	Primo Impalcato	50-52	0	34	-34	2	-3	0	-1	0	0
			66	34	-34	2	-3	0	-1	0	0
			132	34	-34	2	-3	0	-1	0	0
229	Primo Impalcato	51-53	0	33	-33	3	-4	1	-1	0	0
			66	33	-33	3	-4	1	-1	0	0
			132	33	-33	3	-4	1	-1	0	0
230	Primo Impalcato	52-54	0	34	-34	4	-3	1	-1	0	0
			66	34	-34	4	-3	1	-1	0	0
			132	34	-34	4	-3	1	-1	0	0
231	Primo Impalcato	53-55	0	33	-37	2	-7	-1	-3	-2	-2

			66	33	-37	2	-7	-1	-3	-2	-2
			132	33	-37	2	-7	-1	-3	-2	-2
232	Primo Impalcato	54-56	0	37	-33	7	-2	3	2	2	2
			66	37	-33	7	-2	3	2	2	2
			132	37	-33	7	-2	3	2	2	2
233	Primo Impalcato	55-57	0	15	-49	-17	-28	-17	-21	-17	-17
			80	15	-49	-17	-28	-17	-21	-17	-17
			159	15	-49	-17	-28	-17	-21	-17	-17
234	Primo Impalcato	56-70	0	50	-16	27	16	20	17	17	17
			80	50	-16	27	16	20	17	17	17
			159	50	-16	27	16	20	17	17	17
235	Primo Impalcato	57-58	0	112	-112	10	-17	2	-3	0	0
			83	112	-112	10	-17	2	-3	0	0
			166	112	-112	10	-17	2	-3	0	0
236	Primo Impalcato	58-59	0	16	-33	9	-17	2	-3	0	0
			69	16	-33	9	-17	2	-3	0	0
			138	16	-33	9	-17	2	-3	0	0
237	Primo Impalcato	59-60	0	15	-31	8	-15	2	-3	0	0
			69	15	-31	8	-15	2	-3	0	0
			138	15	-31	8	-15	2	-3	0	0
238	Primo Impalcato	60-61	0	17	-31	7	-13	1	-2	0	0
			69	17	-31	7	-13	1	-2	0	0
			138	17	-31	7	-13	1	-2	0	0
239	Primo Impalcato	61-62	0	16	-26	4	-9	1	-2	0	0
			69	16	-26	4	-9	1	-2	0	0
			138	16	-26	4	-9	1	-2	0	0
240	Primo Impalcato	62-63	0	20	-23	2	-5	0	-1	0	0
			69	20	-23	2	-5	0	-1	0	0
			138	20	-23	2	-5	0	-1	0	0
241	Primo Impalcato	63-64	0	24	-25	1	-1	0	0	0	0
			69	24	-25	1	-1	0	0	0	0
			138	24	-25	1	-1	0	0	0	0
242	Primo Impalcato	64-65	0	26	-26	6	-3	1	-1	0	0
			69	26	-26	6	-3	1	-1	0	0
			138	26	-26	6	-3	1	-1	0	0
243	Primo Impalcato	65-66	0	26	-26	10	-5	2	-1	0	0
			69	26	-26	10	-5	2	-1	0	0
			138	26	-26	10	-5	2	-1	0	0
244	Primo Impalcato	66-67	0	29	-32	14	-7	3	-2	0	0
			69	29	-32	14	-7	3	-2	0	0
			138	29	-32	14	-7	3	-2	0	0
245	Primo Impalcato	67-68	0	23	-33	16	-9	3	-2	-1	-1
			69	23	-33	16	-9	3	-2	-1	-1
			138	23	-33	16	-9	3	-2	-1	-1
246	Primo Impalcato	68-69	0	23	-35	17	-9	3	-2	0	0

	o										
			69	23	-35	17	-9	3	-2	0	0
			138	23	-35	17	-9	3	-2	0	0
247	Primo Impalcato	69-70	0	26	-39	16	-9	3	-2	0	0
			83	26	-39	16	-9	3	-2	0	0
			166	26	-39	16	-9	3	-2	0	0
248	Primo Impalcato	1-1	0	76	-142	-17	-47	-21	-28	-21	-21
			188	76	-142	-17	-47	-21	-28	-21	-21
			376	76	-142	-17	-47	-21	-28	-21	-21
249	Primo Impalcato	2-2	0	17	-22	3	-5	1	-1	1	1
			188	17	-22	3	-5	1	-1	1	1
			376	17	-22	3	-5	1	-1	1	1
250	Primo Impalcato	3-3	0	8	-10	3	-3	1	0	1	1
			188	8	-10	3	-3	1	0	1	1
			376	8	-10	3	-3	1	0	1	1
251	Primo Impalcato	4-4	0	8	-12	2	-3	1	0	0	0
			188	8	-12	2	-3	1	0	0	0
			376	8	-12	2	-3	1	0	0	0
252	Primo Impalcato	5-5	0	5	-5	1	-2	0	0	0	0
			188	5	-5	1	-2	0	0	0	0
			376	5	-5	1	-2	0	0	0	0
253	Primo Impalcato	6-6	0	10	-10	1	-1	0	0	0	0
			188	10	-10	1	-1	0	0	0	0
			376	10	-10	1	-1	0	0	0	0
254	Primo Impalcato	7-7	0	7	-7	0	0	0	0	0	0
			188	7	-7	0	0	0	0	0	0
			376	7	-7	0	0	0	0	0	0
255	Primo Impalcato	8-8	0	8	-8	1	0	0	0	0	0
			188	8	-8	1	0	0	0	0	0
			376	8	-8	1	0	0	0	0	0
256	Primo Impalcato	9-9	0	12	-10	2	-1	0	0	0	0
			188	12	-10	2	-1	0	0	0	0
			376	12	-10	2	-1	0	0	0	0
257	Primo Impalcato	10-10	0	8	-5	2	-1	0	0	0	0
			188	8	-5	2	-1	0	0	0	0
			376	8	-5	2	-1	0	0	0	0
258	Primo Impalcato	11-11	0	11	-10	3	-2	0	-1	0	0
			188	11	-10	3	-2	0	-1	0	0
			376	11	-10	3	-2	0	-1	0	0
259	Primo Impalcato	12-12	0	13	-9	3	-3	0	-1	-1	-1
			188	13	-9	3	-3	0	-1	-1	-1
			376	13	-9	3	-3	0	-1	-1	-1
260	Primo Impalcato	13-13	0	12	-7	5	-3	0	-1	-1	-1
			188	12	-7	5	-3	0	-1	-1	-1
			376	12	-7	5	-3	0	-1	-1	-1
261	Primo	14-1	0	94	-34	47	19	29	22	22	22

	Impalcat o	4									
			188	94	-34	47	19	29	22	22	22
			376	94	-34	47	19	29	22	22	22
262	Primo Impalcat o	15-1 5	0	13	-36	-10	-18	-11	-14	-11	-11
			188	13	-36	-10	-18	-11	-14	-11	-11
			376	13	-36	-10	-18	-11	-14	-11	-11
263	Primo Impalcat o	16-1 6	0	37	-15	18	10	14	11	11	11
			188	37	-15	18	10	14	11	11	11
			376	37	-15	18	10	14	11	11	11
264	Primo Impalcat o	17-1 7	0	23	-27	0	-5	-2	-3	-2	-2
			188	23	-27	0	-5	-2	-3	-2	-2
			376	23	-27	0	-5	-2	-3	-2	-2
265	Primo Impalcat o	18-1 8	0	27	-23	6	0	3	2	2	2
			188	27	-23	6	0	3	2	2	2
			376	27	-23	6	0	3	2	2	2
266	Primo Impalcat o	19-1 9	0	26	-26	3	-2	1	0	0	0
			188	26	-26	3	-2	1	0	0	0
			376	26	-26	3	-2	1	0	0	0
267	Primo Impalcat o	20-2 0	0	27	-27	2	-3	0	-1	0	0
			188	27	-27	2	-3	0	-1	0	0
			376	27	-27	2	-3	0	-1	0	0
268	Primo Impalcat o	21-2 1	0	28	-27	2	-1	1	0	0	0
			188	28	-27	2	-1	1	0	0	0
			376	28	-27	2	-1	1	0	0	0
269	Primo Impalcat o	22-2 2	0	25	-25	1	-2	0	-1	0	0
			188	25	-25	1	-2	0	-1	0	0
			376	25	-25	1	-2	0	-1	0	0
270	Primo Impalcat o	23-2 3	0	26	-26	1	-1	0	0	0	0
			188	26	-26	1	-1	0	0	0	0
			376	26	-26	1	-1	0	0	0	0
271	Primo Impalcat o	24-2 4	0	25	-25	1	-1	0	0	0	0
			188	25	-25	1	-1	0	0	0	0
			376	25	-25	1	-1	0	0	0	0
272	Primo Impalcat o	25-2 5	0	22	-22	1	-1	0	0	0	0
			188	22	-22	1	-1	0	0	0	0
			376	22	-22	1	-1	0	0	0	0
273	Primo Impalcat o	26-2 6	0	23	-23	1	-1	0	0	0	0
			188	23	-23	1	-1	0	0	0	0
			376	23	-23	1	-1	0	0	0	0
274	Primo Impalcat o	27-2 7	0	23	-23	0	0	0	0	0	0
			188	23	-23	0	0	0	0	0	0
			376	23	-23	0	0	0	0	0	0
275	Primo Impalcat o	28-2 8	0	19	-20	0	0	0	0	0	0
			188	19	-20	0	0	0	0	0	0
			376	19	-20	0	0	0	0	0	0

276	Primo Impalcato	29-29	0	18	-18	0	0	0	0	0	0
			188	18	-18	0	0	0	0	0	0
			376	18	-18	0	0	0	0	0	0
277	Primo Impalcato	30-30	0	16	-16	0	0	0	0	0	0
			188	16	-16	0	0	0	0	0	0
			376	16	-16	0	0	0	0	0	0
278	Primo Impalcato	31-31	0	16	-16	0	0	0	0	0	0
			188	16	-16	0	0	0	0	0	0
			376	16	-16	0	0	0	0	0	0
279	Primo Impalcato	32-32	0	16	-16	0	0	0	0	0	0
			188	16	-16	0	0	0	0	0	0
			376	16	-16	0	0	0	0	0	0
280	Primo Impalcato	33-33	0	12	-12	0	0	0	0	0	0
			188	12	-12	0	0	0	0	0	0
			376	12	-12	0	0	0	0	0	0
281	Primo Impalcato	34-34	0	11	-11	0	0	0	0	0	0
			188	11	-11	0	0	0	0	0	0
			376	11	-11	0	0	0	0	0	0
282	Primo Impalcato	35-35	0	10	-10	0	0	0	0	0	0
			188	10	-10	0	0	0	0	0	0
			376	10	-10	0	0	0	0	0	0
283	Primo Impalcato	36-36	0	11	-11	0	0	0	0	0	0
			188	11	-11	0	0	0	0	0	0
			376	11	-11	0	0	0	0	0	0
284	Primo Impalcato	37-37	0	14	-14	0	0	0	0	0	0
			188	14	-14	0	0	0	0	0	0
			376	14	-14	0	0	0	0	0	0
285	Primo Impalcato	38-38	0	13	-13	0	-1	0	0	0	0
			188	13	-13	0	-1	0	0	0	0
			376	13	-13	0	-1	0	0	0	0
286	Primo Impalcato	39-39	0	13	-13	0	0	0	0	0	0
			188	13	-13	0	0	0	0	0	0
			376	13	-13	0	0	0	0	0	0
287	Primo Impalcato	40-40	0	13	-14	0	-1	0	0	0	0
			188	13	-14	0	-1	0	0	0	0
			376	13	-14	0	-1	0	0	0	0
288	Primo Impalcato	41-41	0	15	-15	0	0	0	0	0	0
			188	15	-15	0	0	0	0	0	0
			376	15	-15	0	0	0	0	0	0
289	Primo Impalcato	42-42	0	19	-19	0	-1	0	0	0	0
			188	19	-19	0	-1	0	0	0	0
			376	19	-19	0	-1	0	0	0	0
290	Primo Impalcato	43-43	0	19	-19	0	0	0	0	0	0
			188	19	-19	0	0	0	0	0	0

			376	19	-19	0	0	0	0	0	0
291	Primo Impalcato	44-44	0	20	-20	0	0	0	0	0	0
			188	20	-20	0	0	0	0	0	0
			376	20	-20	0	0	0	0	0	0
292	Primo Impalcato	45-45	0	20	-20	0	0	0	0	0	0
			188	20	-20	0	0	0	0	0	0
			376	20	-20	0	0	0	0	0	0
293	Primo Impalcato	46-46	0	20	-20	0	0	0	0	0	0
			188	20	-20	0	0	0	0	0	0
			376	20	-20	0	0	0	0	0	0
294	Primo Impalcato	47-47	0	25	-25	1	-1	0	0	0	0
			188	25	-25	1	-1	0	0	0	0
			376	25	-25	1	-1	0	0	0	0
295	Primo Impalcato	48-48	0	26	-26	1	-1	0	0	0	0
			188	26	-26	1	-1	0	0	0	0
			376	26	-26	1	-1	0	0	0	0
296	Primo Impalcato	49-49	0	27	-28	1	-2	0	-1	0	0
			188	27	-28	1	-2	0	-1	0	0
			376	27	-28	1	-2	0	-1	0	0
297	Primo Impalcato	50-50	0	30	-29	2	-1	1	0	0	0
			188	30	-29	2	-1	1	0	0	0
			376	30	-29	2	-1	1	0	0	0
298	Primo Impalcato	51-51	0	29	-29	2	-2	0	-1	0	0
			188	29	-29	2	-2	0	-1	0	0
			376	29	-29	2	-2	0	-1	0	0
299	Primo Impalcato	52-52	0	28	-27	3	-2	1	0	0	0
			188	28	-27	3	-2	1	0	0	0
			376	28	-27	3	-2	1	0	0	0
300	Primo Impalcato	53-53	0	31	-27	5	0	3	2	2	2
			188	31	-27	5	0	3	2	2	2
			376	31	-27	5	0	3	2	2	2
301	Primo Impalcato	54-54	0	26	-30	0	-5	-2	-3	-2	-2
			188	26	-30	0	-5	-2	-3	-2	-2
			376	26	-30	0	-5	-2	-3	-2	-2
302	Primo Impalcato	55-55	0	40	-18	18	10	14	11	11	11
			188	40	-18	18	10	14	11	11	11
			376	40	-18	18	10	14	11	11	11
303	Primo Impalcato	56-56	0	14	-36	-10	-19	-11	-14	-11	-11
			188	14	-36	-10	-19	-11	-14	-11	-11
			376	14	-36	-10	-19	-11	-14	-11	-11
304	Primo Impalcato	57-57	0	123	-76	47	17	28	21	21	21
			188	123	-76	47	17	28	21	21	21
			376	123	-76	47	17	28	21	21	21
305	Primo Impalcato	58-58	0	15	-17	5	-3	1	-1	-1	-1

			188	15	-17	5	-3	1	-1	-1	-1
			376	15	-17	5	-3	1	-1	-1	-1
306	Primo Impalcato	59-59	0	5	-9	3	-3	0	-1	-1	-1
			188	5	-9	3	-3	0	-1	-1	-1
			376	5	-9	3	-3	0	-1	-1	-1
307	Primo Impalcato	60-60	0	6	-7	3	-2	0	-1	0	0
			188	6	-7	3	-2	0	-1	0	0
			376	6	-7	3	-2	0	-1	0	0
308	Primo Impalcato	61-61	0	6	-4	2	-1	0	0	0	0
			188	6	-4	2	-1	0	0	0	0
			376	6	-4	2	-1	0	0	0	0
309	Primo Impalcato	62-62	0	8	-8	1	-1	0	0	0	0
			188	8	-8	1	-1	0	0	0	0
			376	8	-8	1	-1	0	0	0	0
310	Primo Impalcato	63-63	0	7	-7	0	0	0	0	0	0
			188	7	-7	0	0	0	0	0	0
			376	7	-7	0	0	0	0	0	0
311	Primo Impalcato	64-64	0	7	-7	0	-1	0	0	0	0
			188	7	-7	0	-1	0	0	0	0
			376	7	-7	0	-1	0	0	0	0
312	Primo Impalcato	65-65	0	9	-9	1	-2	0	0	0	0
			188	9	-9	1	-2	0	0	0	0
			376	9	-9	1	-2	0	0	0	0
313	Primo Impalcato	66-66	0	5	-5	1	-2	0	0	0	0
			188	5	-5	1	-2	0	0	0	0
			376	5	-5	1	-2	0	0	0	0
314	Primo Impalcato	67-67	0	10	-8	2	-3	1	0	0	0
			188	10	-8	2	-3	1	0	0	0
			376	10	-8	2	-3	1	0	0	0
315	Primo Impalcato	68-68	0	8	-6	3	-3	1	0	1	1
			188	8	-6	3	-3	1	0	1	1
			376	8	-6	3	-3	1	0	1	1
316	Primo Impalcato	69-69	0	10	-5	3	-4	1	0	1	1
			188	10	-5	3	-4	1	0	1	1
			376	10	-5	3	-4	1	0	1	1
317	Primo Impalcato	70-70	0	34	-78	-19	-47	-22	-29	-22	-22
			188	34	-78	-19	-47	-22	-29	-22	-22
			376	34	-78	-19	-47	-22	-29	-22	-22
318	Primo Impalcato	1-71	0	0	-1	0	-1	0	0	0	0
			102	0	-1	0	-1	0	0	0	0
			204	0	-1	0	-1	0	0	0	0
319	Primo Impalcato	1-92	0	1	-1	0	0	0	0	0	0
			103	1	-1	0	0	0	0	0	0
			206	1	-1	0	0	0	0	0	0
320	Primo Impalcato	92-2	0	2	-3	0	-1	0	0	0	0

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			103	2	-3	0	-1	0	0	0	0
			206	2	-3	0	-1	0	0	0	0
321	Primo Impalcato	6-89	0	3	-2	1	0	0	0	0	0
			100	3	-2	1	0	0	0	0	0
			200	3	-2	1	0	0	0	0	0
322	Primo Impalcato	89-7	0	1	-2	0	-1	0	0	0	0
			100	1	-2	0	-1	0	0	0	0
			200	1	-2	0	-1	0	0	0	0
323	Primo Impalcato	9-90	0	3	-2	1	0	0	0	0	0
			100	3	-2	1	0	0	0	0	0
			200	3	-2	1	0	0	0	0	0
324	Primo Impalcato	90-10	0	1	-2	0	-1	0	0	0	0
			100	1	-2	0	-1	0	0	0	0
			200	1	-2	0	-1	0	0	0	0
325	Primo Impalcato	13-91	0	2	-1	1	0	0	0	0	0
			103	2	-1	1	0	0	0	0	0
			206	2	-1	1	0	0	0	0	0
326	Primo Impalcato	88-14	0	1	0	1	0	0	0	0	0
			102	1	0	1	0	0	0	0	0
			204	1	0	1	0	0	0	0	0
327	Primo Impalcato	91-14	0	1	0	0	0	0	0	0	0
			103	1	0	0	0	0	0	0	0
			206	1	0	0	0	0	0	0	0
328	Primo Impalcato	71-15	0	1	-2	0	-1	-1	-1	-1	-1
			102	1	-2	0	-1	-1	-1	-1	-1
			204	1	-2	0	-1	-1	-1	-1	-1
329	Primo Impalcato	16-88	0	2	-1	1	0	1	1	1	1
			102	2	-1	1	0	1	1	1	1
			204	2	-1	1	0	1	1	1	1
330	Primo Impalcato	17-72	0	1	0	0	0	0	0	0	0
			100	1	0	0	0	0	0	0	0
			199	1	0	0	0	0	0	0	0
331	Primo Impalcato	87-18	0	0	-1	0	0	0	0	0	0
			100	0	-1	0	0	0	0	0	0
			199	0	-1	0	0	0	0	0	0
332	Primo Impalcato	72-19	0	1	-2	0	-1	0	0	0	0
			100	1	-2	0	-1	0	0	0	0
			199	1	-2	0	-1	0	0	0	0
333	Primo Impalcato	20-87	0	2	-1	1	0	0	0	0	0
			100	2	-1	1	0	0	0	0	0
			199	2	-1	1	0	0	0	0	0
334	Primo Impalcato	21-73	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
335	Primo	86-2	0	1	-1	0	0	0	0	0	0

	Impalcat o	2									
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
336	Primo Impalcat o	73-2 3	0	2	-2	0	-1	0	0	0	0
			100	2	-2	0	-1	0	0	0	0
			199	2	-2	0	-1	0	0	0	0
337	Primo Impalcat o	24-8 6	0	2	-2	1	0	0	0	0	0
			100	2	-2	1	0	0	0	0	0
			199	2	-2	1	0	0	0	0	0
338	Primo Impalcat o	25-7 4	0	2	-2	1	0	0	0	0	0
			103	2	-2	1	0	0	0	0	0
			206	2	-2	1	0	0	0	0	0
339	Primo Impalcat o	85-2 6	0	1	-2	0	-1	0	0	0	0
			100	1	-2	0	-1	0	0	0	0
			199	1	-2	0	-1	0	0	0	0
340	Primo Impalcat o	27-8 5	0	2	-2	1	0	0	0	0	0
			100	2	-2	1	0	0	0	0	0
			199	2	-2	1	0	0	0	0	0
341	Primo Impalcat o	74-2 8	0	2	-3	0	-1	0	0	0	0
			103	2	-3	0	-1	0	0	0	0
			206	2	-3	0	-1	0	0	0	0
342	Primo Impalcat o	84-2 9	0	2	-2	0	-1	0	0	0	0
			100	2	-2	0	-1	0	0	0	0
			199	2	-2	0	-1	0	0	0	0
343	Primo Impalcat o	31-8 4	0	3	-2	1	0	0	0	0	0
			100	3	-2	1	0	0	0	0	0
			199	3	-2	1	0	0	0	0	0
344	Primo Impalcat o	83-3 3	0	2	-2	0	-1	0	0	0	0
			100	2	-2	0	-1	0	0	0	0
			199	2	-2	0	-1	0	0	0	0
345	Primo Impalcat o	35-8 3	0	2	-2	1	0	0	0	0	0
			100	2	-2	1	0	0	0	0	0
			199	2	-2	1	0	0	0	0	0
346	Primo Impalcat o	82-3 7	0	2	-3	0	-1	0	0	0	0
			100	2	-3	0	-1	0	0	0	0
			199	2	-3	0	-1	0	0	0	0
347	Primo Impalcat o	39-8 2	0	2	-2	1	0	0	0	0	0
			100	2	-2	1	0	0	0	0	0
			199	2	-2	1	0	0	0	0	0
348	Primo Impalcat o	78-4 3	0	2	-2	1	0	0	0	0	0
			100	2	-2	1	0	0	0	0	0
			199	2	-2	1	0	0	0	0	0
349	Primo Impalcat o	81-4 4	0	2	-2	0	-1	0	0	0	0
			100	2	-2	0	-1	0	0	0	0
			199	2	-2	0	-1	0	0	0	0

350	Primo Impalcato	45-78	0	1	-2	0	-1	0	0	0	0
			100	1	-2	0	-1	0	0	0	0
			199	1	-2	0	-1	0	0	0	0
351	Primo Impalcato	46-81	0	2	-1	1	0	0	0	0	0
			100	2	-1	1	0	0	0	0	0
			199	2	-1	1	0	0	0	0	0
352	Primo Impalcato	77-47	0	2	-2	1	0	0	0	0	0
			100	2	-2	1	0	0	0	0	0
			199	2	-2	1	0	0	0	0	0
353	Primo Impalcato	80-48	0	2	-2	0	-1	0	0	0	0
			100	2	-2	0	-1	0	0	0	0
			199	2	-2	0	-1	0	0	0	0
354	Primo Impalcato	49-77	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
355	Primo Impalcato	50-80	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
356	Primo Impalcato	76-51	0	2	-1	1	0	0	0	0	0
			100	2	-1	1	0	0	0	0	0
			199	2	-1	1	0	0	0	0	0
357	Primo Impalcato	53-76	0	0	-1	0	0	0	0	0	0
			100	0	-1	0	0	0	0	0	0
			199	0	-1	0	0	0	0	0	0
358	Primo Impalcato	75-55	0	2	-1	1	0	1	1	1	1
			102	2	-1	1	0	1	1	1	1
			204	2	-1	1	0	1	1	1	1
359	Primo Impalcato	56-79	0	1	-2	0	-1	-1	-1	-1	-1
			102	1	-2	0	-1	-1	-1	-1	-1
			204	1	-2	0	-1	-1	-1	-1	-1
360	Primo Impalcato	57-75	0	1	0	1	0	0	0	0	0
			102	1	0	1	0	0	0	0	0
			204	1	0	1	0	0	0	0	0
361	Primo Impalcato	57-93	0	1	0	0	0	0	0	0	0
			103	1	0	0	0	0	0	0	0
			206	1	0	0	0	0	0	0	0
362	Primo Impalcato	93-58	0	2	-2	1	0	0	0	0	0
			103	2	-2	1	0	0	0	0	0
			206	2	-2	1	0	0	0	0	0
363	Primo Impalcato	61-95	0	2	-2	0	-1	0	0	0	0
			100	2	-2	0	-1	0	0	0	0
			200	2	-2	0	-1	0	0	0	0
364	Primo Impalcato	95-62	0	1	-2	1	0	0	0	0	0
			100	1	-2	1	0	0	0	0	0

			200	1	-2	1	0	0	0	0	0
365	Primo Impalcato	96-65	0	2	-1	0	-1	0	0	0	0
			100	2	-1	0	-1	0	0	0	0
			200	2	-1	0	-1	0	0	0	0
366	Primo Impalcato	66-96	0	1	-1	1	0	0	0	0	0
			100	1	-1	1	0	0	0	0	0
			200	1	-1	1	0	0	0	0	0
367	Primo Impalcato	69-94	0	1	-1	0	-1	0	0	0	0
			103	1	-1	0	-1	0	0	0	0
			206	1	-1	0	-1	0	0	0	0
368	Primo Impalcato	79-70	0	0	-1	0	-1	0	0	0	0
			102	0	-1	0	-1	0	0	0	0
			204	0	-1	0	-1	0	0	0	0
369	Primo Impalcato	94-70	0	1	0	0	0	0	0	0	0
			103	1	0	0	0	0	0	0	0
			206	1	0	0	0	0	0	0	0
370	Primo Impalcato	1-71	0	3	-4	0	-1	0	0	0	0
			102	3	-4	0	-1	0	0	0	0
			204	3	-4	0	-1	0	0	0	0
371	Primo Impalcato	1-92	0	1	-3	-1	-1	-1	-1	-1	-1
			103	1	-3	-1	-1	-1	-1	-1	-1
			206	1	-3	-1	-1	-1	-1	-1	-1
372	Primo Impalcato	92-2	0	2	-2	1	-1	0	0	0	0
			103	2	-2	1	-1	0	0	0	0
			206	2	-2	1	-1	0	0	0	0
373	Primo Impalcato	6-89	0	2	-2	0	0	0	0	0	0
			100	2	-2	0	0	0	0	0	0
			200	2	-2	0	0	0	0	0	0
374	Primo Impalcato	89-7	0	2	-2	0	0	0	0	0	0
			100	2	-2	0	0	0	0	0	0
			200	2	-2	0	0	0	0	0	0
375	Primo Impalcato	9-90	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			200	1	-1	0	0	0	0	0	0
376	Primo Impalcato	90-10	0	2	-2	1	0	0	0	0	0
			100	2	-2	1	0	0	0	0	0
			200	2	-2	1	0	0	0	0	0
377	Primo Impalcato	13-91	0	2	-2	1	-1	0	0	0	0
			103	2	-2	1	-1	0	0	0	0
			206	2	-2	1	-1	0	0	0	0
378	Primo Impalcato	88-14	0	2	-1	1	0	0	0	0	0
			102	2	-1	1	0	0	0	0	0
			204	2	-1	1	0	0	0	0	0
379	Primo Impalcato	91-14	0	2	-1	1	1	1	1	1	1

			103	2	-1	1	1	1	1	1	1
			206	2	-1	1	1	1	1	1	1
380	Primo Impalcato	71-15	0	1	-2	0	-1	0	0	0	0
			102	1	-2	0	-1	0	0	0	0
			204	1	-2	0	-1	0	0	0	0
381	Primo Impalcato	16-88	0	2	-1	1	0	0	0	0	0
			102	2	-1	1	0	0	0	0	0
			204	2	-1	1	0	0	0	0	0
382	Primo Impalcato	17-72	0	2	-2	0	0	0	0	0	0
			100	2	-2	0	0	0	0	0	0
			199	2	-2	0	0	0	0	0	0
383	Primo Impalcato	87-18	0	2	-2	0	0	0	0	0	0
			100	2	-2	0	0	0	0	0	0
			199	2	-2	0	0	0	0	0	0
384	Primo Impalcato	72-19	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
385	Primo Impalcato	20-87	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
386	Primo Impalcato	21-73	0	2	-2	0	0	0	0	0	0
			100	2	-2	0	0	0	0	0	0
			199	2	-2	0	0	0	0	0	0
387	Primo Impalcato	86-22	0	2	-2	0	0	0	0	0	0
			100	2	-2	0	0	0	0	0	0
			199	2	-2	0	0	0	0	0	0
388	Primo Impalcato	73-23	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
389	Primo Impalcato	24-86	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
390	Primo Impalcato	25-74	0	2	-2	0	0	0	0	0	0
			103	2	-2	0	0	0	0	0	0
			206	2	-2	0	0	0	0	0	0
391	Primo Impalcato	85-26	0	2	-2	0	0	0	0	0	0
			100	2	-2	0	0	0	0	0	0
			199	2	-2	0	0	0	0	0	0
392	Primo Impalcato	27-85	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
393	Primo Impalcato	74-28	0	1	-1	0	0	0	0	0	0
			103	1	-1	0	0	0	0	0	0
			206	1	-1	0	0	0	0	0	0
394	Primo Impalcato	84-29	0	2	-2	0	0	0	0	0	0

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			100	2	-2	0	0	0	0	0	0
			199	2	-2	0	0	0	0	0	0
395	Primo Impalcato	31-84	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
396	Primo Impalcato	83-33	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
397	Primo Impalcato	35-83	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
398	Primo Impalcato	82-37	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
399	Primo Impalcato	39-82	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
400	Primo Impalcato	78-43	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
401	Primo Impalcato	81-44	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
402	Primo Impalcato	45-78	0	2	-2	0	0	0	0	0	0
			100	2	-2	0	0	0	0	0	0
			199	2	-2	0	0	0	0	0	0
403	Primo Impalcato	46-81	0	2	-2	0	0	0	0	0	0
			100	2	-2	0	0	0	0	0	0
			199	2	-2	0	0	0	0	0	0
404	Primo Impalcato	77-47	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
405	Primo Impalcato	80-48	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
406	Primo Impalcato	49-77	0	2	-2	0	0	0	0	0	0
			100	2	-2	0	0	0	0	0	0
			199	2	-2	0	0	0	0	0	0
407	Primo Impalcato	50-80	0	2	-2	0	0	0	0	0	0
			100	2	-2	0	0	0	0	0	0
			199	2	-2	0	0	0	0	0	0
408	Primo Impalcato	76-51	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			199	1	-1	0	0	0	0	0	0
409	Primo	53-7	0	2	-2	0	0	0	0	0	0

	Impalcat o	6									
			100	2	-2	0	0	0	0	0	0
			199	2	-2	0	0	0	0	0	0
410	Primo Impalcat o	75-5 5	0	2	-1	1	0	0	0	0	0
			102	2	-1	1	0	0	0	0	0
			204	2	-1	1	0	0	0	0	0
411	Primo Impalcat o	56-7 9	0	1	-2	0	-1	0	0	0	0
			102	1	-2	0	-1	0	0	0	0
			204	1	-2	0	-1	0	0	0	0
412	Primo Impalcat o	57-7 5	0	3	-3	1	0	0	0	0	0
			102	3	-3	1	0	0	0	0	0
			204	3	-3	1	0	0	0	0	0
413	Primo Impalcat o	57-9 3	0	3	-2	1	1	1	1	1	1
			103	3	-2	1	1	1	1	1	1
			206	3	-2	1	1	1	1	1	1
414	Primo Impalcat o	93-5 8	0	1	-2	1	-1	0	0	0	0
			103	1	-2	1	-1	0	0	0	0
			206	1	-2	1	-1	0	0	0	0
415	Primo Impalcat o	61-9 5	0	1	-1	1	0	0	0	0	0
			100	1	-1	1	0	0	0	0	0
			200	1	-1	1	0	0	0	0	0
416	Primo Impalcat o	95-6 2	0	2	-2	0	0	0	0	0	0
			100	2	-2	0	0	0	0	0	0
			200	2	-2	0	0	0	0	0	0
417	Primo Impalcat o	96-6 5	0	1	-1	0	0	0	0	0	0
			100	1	-1	0	0	0	0	0	0
			200	1	-1	0	0	0	0	0	0
418	Primo Impalcat o	66-9 6	0	2	-2	0	-1	0	0	0	0
			100	2	-2	0	-1	0	0	0	0
			200	2	-2	0	-1	0	0	0	0
419	Primo Impalcat o	69-9 4	0	2	-1	1	-1	0	0	0	0
			103	2	-1	1	-1	0	0	0	0
			206	2	-1	1	-1	0	0	0	0
420	Primo Impalcat o	79-7 0	0	1	-1	0	-1	0	0	0	0
			102	1	-1	0	-1	0	0	0	0
			204	1	-1	0	-1	0	0	0	0
421	Primo Impalcat o	94-7 0	0	1	-2	-1	-1	-1	-1	-1	-1
			103	1	-2	-1	-1	-1	-1	-1	-1
			206	1	-2	-1	-1	-1	-1	-1	-1
422	Copertur a	1-2	0	1720	-1790	26	-100	-22	-47	-30	-30
			83	1720	-1790	26	-100	-22	-47	-30	-30
			166	1720	-1790	26	-100	-22	-47	-30	-30
423	Copertur a	15-1	0	-314	-840	-460	-664	-460	-554	-460	-460
			80	-314	-840	-460	-664	-460	-554	-460	-460
			159	-314	-840	-460	-664	-460	-554	-460	-460
424	Copertur a	2-3	0	422	-310	111	-39	30	0	9	9

			69	422	-310	111	-39	30	0	9	9
			138	422	-310	111	-39	30	0	9	9
425	Copertura	3-4	0	233	-159	166	-57	44	-1	12	12
			69	233	-159	166	-57	44	-1	12	12
			138	233	-159	166	-57	44	-1	12	12
426	Copertura	4-5	0	325	-287	163	-68	37	-9	5	5
			69	325	-287	163	-68	37	-9	5	5
			138	325	-287	163	-68	37	-9	5	5
427	Copertura	5-6	0	323	-313	124	-57	26	-11	1	1
			69	323	-313	124	-57	26	-11	1	1
			138	323	-313	124	-57	26	-11	1	1
428	Copertura	6-7	0	266	-279	62	-29	12	-6	0	0
			69	266	-279	62	-29	12	-6	0	0
			138	266	-279	62	-29	12	-6	0	0
429	Copertura	7-8	0	368	-368	15	-16	3	-3	0	0
			69	368	-368	15	-16	3	-3	0	0
			138	368	-368	15	-16	3	-3	0	0
430	Copertura	8-9	0	336	-384	36	-69	7	-14	0	0
			69	336	-384	36	-69	7	-14	0	0
			138	336	-384	36	-69	7	-14	0	0
431	Copertura	9-10	0	379	-518	62	-128	12	-26	-1	-1
			69	379	-518	62	-128	12	-26	-1	-1
			138	379	-518	62	-128	12	-26	-1	-1
432	Copertura	10-11	0	396	-610	75	-171	10	-39	-5	-5
			69	396	-610	75	-171	10	-39	-5	-5
			138	396	-610	75	-171	10	-39	-5	-5
433	Copertura	11-12	0	293	-495	63	-173	2	-45	-12	-12
			69	293	-495	63	-173	2	-45	-12	-12
			138	293	-495	63	-173	2	-45	-12	-12
434	Copertura	12-13	0	371	-459	42	-114	1	-30	-8	-8
			69	371	-459	42	-114	1	-30	-8	-8
			138	371	-459	42	-114	1	-30	-8	-8
435	Copertura	13-14	0	403	-342	74	0	42	27	30	30
			83	403	-342	74	0	42	27	30	30
			166	403	-342	74	0	42	27	30	30
436	Copertura	16-14	0	825	326	660	458	551	458	458	458
			80	825	326	660	458	551	458	458	458
			159	825	326	660	458	551	458	458	458
437	Copertura	15-17	0	149	-281	-55	-85	-55	-71	-55	-55
			66	149	-281	-55	-85	-55	-71	-55	-55
			132	149	-281	-55	-85	-55	-71	-55	-55
438	Copertura	16-18	0	285	-135	89	58	74	58	58	58
			66	285	-135	89	58	74	58	58	58
			132	285	-135	89	58	74	58	58	58
439	Copertura	17-19	0	141	-153	-2	-15	-6	-9	-6	-6
			66	141	-153	-2	-15	-6	-9	-6	-6
			132	141	-153	-2	-15	-6	-9	-6	-6
440	Copertura	18-20	0	129	-116	15	2	9	6	6	6
			66	129	-116	15	2	9	6	6	6
			132	129	-116	15	2	9	6	6	6
441	Copertura	19-21	0	174	-172	9	-1	5	3	3	3
			66	174	-172	9	-1	5	3	3	3
			132	174	-172	9	-1	5	3	3	3
442	Copertura	20-22	0	170	-185	0	-9	-3	-5	-3	-3
			66	170	-185	0	-9	-3	-5	-3	-3

			132	170	-185	0	-9	-3	-5	-3	-3
443	Copertura	21-23	0	118	-115	5	-1	2	1	2	2
			66	118	-115	5	-1	2	1	2	2
			132	118	-115	5	-1	2	1	2	2
444	Copertura	22-24	0	152	-156	1	-6	-1	-3	-2	-2
			66	152	-156	1	-6	-1	-3	-2	-2
			132	152	-156	1	-6	-1	-3	-2	-2
445	Copertura	23-25	0	156	-156	2	0	1	0	0	0
			66	156	-156	2	0	1	0	0	0
			132	156	-156	2	0	1	0	0	0
446	Copertura	24-26	0	177	-177	2	-4	0	-1	0	0
			66	177	-177	2	-4	0	-1	0	0
			132	177	-177	2	-4	0	-1	0	0
447	Copertura	25-28	0	80	-81	0	-1	0	-1	-1	-1
			85	80	-81	0	-1	0	-1	-1	-1
			170	80	-81	0	-1	0	-1	-1	-1
448	Copertura	26-27	0	201	-200	2	-1	1	0	1	1
			66	201	-200	2	-1	1	0	1	1
			132	201	-200	2	-1	1	0	1	1
449	Copertura	27-29	0	169	-167	2	1	1	1	1	1
			66	169	-167	2	1	1	1	1	1
			132	169	-167	2	1	1	1	1	1
450	Copertura	28-30	0	135	-137	0	-4	-1	-2	-1	-1
			73	135	-137	0	-4	-1	-2	-1	-1
			146	135	-137	0	-4	-1	-2	-1	-1
451	Copertura	29-31	0	161	-160	2	0	1	0	0	0
			66	161	-160	2	0	1	0	0	0
			132	161	-160	2	0	1	0	0	0
452	Copertura	30-32	0	118	-119	0	-2	0	-1	0	0
			69	118	-119	0	-2	0	-1	0	0
			137	118	-119	0	-2	0	-1	0	0
453	Copertura	31-33	0	135	-134	1	0	0	0	0	0
			66	135	-134	1	0	0	0	0	0
			132	135	-134	1	0	0	0	0	0
454	Copertura	32-34	0	126	-126	0	0	0	0	0	0
			69	126	-126	0	0	0	0	0	0
			138	126	-126	0	0	0	0	0	0
455	Copertura	33-35	0	164	-163	1	0	1	0	0	0
			66	164	-163	1	0	1	0	0	0
			132	164	-163	1	0	1	0	0	0
456	Copertura	34-36	0	134	-134	1	-1	0	0	0	0
			69	134	-134	1	-1	0	0	0	0
			138	134	-134	1	-1	0	0	0	0
457	Copertura	35-37	0	145	-144	2	0	1	0	0	0
			66	145	-144	2	0	1	0	0	0
			132	145	-144	2	0	1	0	0	0
458	Copertura	36-38	0	102	-103	0	-1	0	0	0	0
			69	102	-103	0	-1	0	0	0	0
			138	102	-103	0	-1	0	0	0	0
459	Copertura	37-39	0	158	-156	3	-1	1	0	0	0
			66	158	-156	3	-1	1	0	0	0
			132	158	-156	3	-1	1	0	0	0
460	Copertura	38-40	0	142	-143	0	-3	0	-1	0	0
			69	142	-143	0	-3	0	-1	0	0
			137	142	-143	0	-3	0	-1	0	0

461	Copertura	39-41	0	180	-180	3	-2	1	0	0	0
			66	180	-180	3	-2	1	0	0	0
			132	180	-180	3	-2	1	0	0	0
462	Copertura	40-42	0	121	-121	3	-6	1	-1	0	0
			69	121	-121	3	-6	1	-1	0	0
			138	121	-121	3	-6	1	-1	0	0
463	Copertura	41-44	0	101	-104	-2	-3	-2	-2	-2	-2
			66	101	-104	-2	-3	-2	-2	-2	-2
			132	101	-104	-2	-3	-2	-2	-2	-2
464	Copertura	42-43	0	638	-629	6	4	5	4	4	4
			23	638	-629	6	4	5	4	4	4
			46	638	-629	6	4	5	4	4	4
465	Copertura	43-45	0	141	-140	8	-3	2	0	1	1
			66	141	-140	8	-3	2	0	1	1
			132	141	-140	8	-3	2	0	1	1
466	Copertura	44-46	0	142	-143	0	-2	0	-1	0	0
			66	142	-143	0	-2	0	-1	0	0
			132	142	-143	0	-2	0	-1	0	0
467	Copertura	45-47	0	150	-147	4	-3	1	0	0	0
			66	150	-147	4	-3	1	0	0	0
			132	150	-147	4	-3	1	0	0	0
468	Copertura	46-48	0	164	-164	0	-1	0	0	0	0
			66	164	-164	0	-1	0	0	0	0
			132	164	-164	0	-1	0	0	0	0
469	Copertura	47-49	0	144	-147	1	-5	-1	-2	-1	-1
			66	144	-147	1	-5	-1	-2	-1	-1
			132	144	-147	1	-5	-1	-2	-1	-1
470	Copertura	48-50	0	105	-102	4	-1	2	1	1	1
			66	105	-102	4	-1	2	1	1	1
			132	105	-102	4	-1	2	1	1	1
471	Copertura	49-51	0	174	-180	0	-8	-3	-4	-3	-3
			66	174	-180	0	-8	-3	-4	-3	-3
			132	174	-180	0	-8	-3	-4	-3	-3
472	Copertura	50-52	0	165	-158	8	-1	4	2	3	3
			66	165	-158	8	-1	4	2	3	3
			132	165	-158	8	-1	4	2	3	3
473	Copertura	51-53	0	142	-131	14	2	9	6	6	6
			66	142	-131	14	2	9	6	6	6
			132	142	-131	14	2	9	6	6	6
474	Copertura	52-54	0	146	-158	-3	-14	-6	-9	-6	-6
			66	146	-158	-3	-14	-6	-9	-6	-6
			132	146	-158	-3	-14	-6	-9	-6	-6
475	Copertura	53-55	0	295	-155	84	55	70	55	55	55
			66	295	-155	84	55	70	55	55	55
			132	295	-155	84	55	70	55	55	55
476	Copertura	54-56	0	121	-252	-56	-86	-56	-71	-56	-56
			66	121	-252	-56	-86	-56	-71	-56	-56
			132	121	-252	-56	-86	-56	-71	-56	-56
477	Copertura	55-57	0	845	296	665	461	555	461	461	461
			80	845	296	665	461	555	461	461	461
			159	845	296	665	461	555	461	461	461
478	Copertura	56-70	0	-302	-829	-460	-664	-460	-554	-460	-460
			80	-302	-829	-460	-664	-460	-554	-460	-460
			159	-302	-829	-460	-664	-460	-554	-460	-460
479	Copertura	57-5	0	1785	-1721	101	-25	48	23	31	31

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			83	1785	-1721	101	-25	48	23	31	31
			166	1785	-1721	101	-25	48	23	31	31
480	Copertura	58-59	0	292	-303	40	-111	1	-29	-8	-8
			69	292	-303	40	-111	1	-29	-8	-8
			138	292	-303	40	-111	1	-29	-8	-8
481	Copertura	59-60	0	136	-317	57	-167	1	-44	-11	-11
			69	136	-317	57	-167	1	-44	-11	-11
			138	136	-317	57	-167	1	-44	-11	-11
482	Copertura	60-61	0	211	-397	69	-165	9	-37	-5	-5
			69	211	-397	69	-165	9	-37	-5	-5
			138	211	-397	69	-165	9	-37	-5	-5
483	Copertura	61-62	0	219	-337	55	-121	10	-25	-1	-1
			69	219	-337	55	-121	10	-25	-1	-1
			138	219	-337	55	-121	10	-25	-1	-1
484	Copertura	62-63	0	244	-270	28	-61	6	-12	0	0
			69	244	-270	28	-61	6	-12	0	0
			138	244	-270	28	-61	6	-12	0	0
485	Copertura	63-64	0	397	-402	15	-15	3	-3	0	0
			69	397	-402	15	-15	3	-3	0	0
			138	397	-402	15	-15	3	-3	0	0
486	Copertura	64-65	0	324	-327	68	-35	13	-7	0	0
			69	324	-327	68	-35	13	-7	0	0
			138	324	-327	68	-35	13	-7	0	0
487	Copertura	65-66	0	384	-382	127	-62	26	-12	1	1
			69	384	-382	127	-62	26	-12	1	1
			138	384	-382	127	-62	26	-12	1	1
488	Copertura	66-67	0	374	-372	171	-75	39	-10	5	5
			69	374	-372	171	-75	39	-10	5	5
			138	374	-372	171	-75	39	-10	5	5
489	Copertura	67-68	0	339	-402	174	-63	46	-2	12	12
			69	339	-402	174	-63	46	-2	12	12
			138	339	-402	174	-63	46	-2	12	12
490	Copertura	68-69	0	359	-418	114	-42	30	-1	9	9
			69	359	-418	114	-42	30	-1	9	9
			138	359	-418	114	-42	30	-1	9	9
491	Copertura	69-70	0	336	-464	-3	-77	-30	-45	-32	-32
			83	336	-464	-3	-77	-30	-45	-32	-32
			166	336	-464	-3	-77	-30	-45	-32	-32
492	Copertura	1-1	0	127	-80	27	18	22	18	18	18
			220	127	-80	27	18	22	18	18	18
			440	127	-80	27	18	22	18	18	18
493	Copertura	2-2	0	16	-16	0	-3	0	-1	0	0
			220	16	-16	0	-3	0	-1	0	0
			440	16	-16	0	-3	0	-1	0	0
494	Copertura	3-3	0	9	-11	2	-6	0	-2	0	0
			220	9	-11	2	-6	0	-2	0	0
			440	9	-11	2	-6	0	-2	0	0
495	Copertura	4-4	0	11	-13	3	-6	0	-1	0	0
			220	11	-13	3	-6	0	-1	0	0
			440	11	-13	3	-6	0	-1	0	0
496	Copertura	5-5	0	8	-8	2	-5	0	-1	0	0
			220	8	-8	2	-5	0	-1	0	0
			440	8	-8	2	-5	0	-1	0	0
497	Copertura	6-6	0	12	-12	1	-3	0	-1	0	0

			220	12	-12	1	-3	0	-1	0	0
			440	12	-12	1	-3	0	-1	0	0
498	Copertura	7-7	0	11	-10	1	-1	0	0	0	0
			220	11	-10	1	-1	0	0	0	0
			440	11	-10	1	-1	0	0	0	0
499	Copertura	8-8	0	11	-11	1	-1	0	0	0	0
			220	11	-11	1	-1	0	0	0	0
			440	11	-11	1	-1	0	0	0	0
500	Copertura	9-9	0	17	-14	3	-2	1	0	0	0
			220	17	-14	3	-2	1	0	0	0
			440	17	-14	3	-2	1	0	0	0
501	Copertura	10-10	0	17	-11	5	-2	1	0	0	0
			220	17	-11	5	-2	1	0	0	0
			440	17	-11	5	-2	1	0	0	0
502	Copertura	11-11	0	21	-13	6	-3	1	0	0	0
			220	21	-13	6	-3	1	0	0	0
			440	21	-13	6	-3	1	0	0	0
503	Copertura	12-12	0	17	-11	6	-2	2	0	0	0
			220	17	-11	6	-2	2	0	0	0
			440	17	-11	6	-2	2	0	0	0
504	Copertura	13-13	0	11	-8	4	-1	1	0	0	0
			220	11	-8	4	-1	1	0	0	0
			440	11	-8	4	-1	1	0	0	0
505	Copertura	57-57	0	84	-128	-18	-27	-18	-22	-18	-18
			220	84	-128	-18	-27	-18	-22	-18	-18
			440	84	-128	-18	-27	-18	-22	-18	-18
506	Copertura	58-58	0	20	-15	3	0	1	0	0	0
			220	20	-15	3	0	1	0	0	0
			440	20	-15	3	0	1	0	0	0
507	Copertura	59-59	0	16	-9	6	-2	2	0	0	0
			220	16	-9	6	-2	2	0	0	0
			440	16	-9	6	-2	2	0	0	0
508	Copertura	60-60	0	12	-5	6	-3	1	0	0	0
			220	12	-5	6	-3	1	0	0	0
			440	12	-5	6	-3	1	0	0	0
509	Copertura	61-61	0	11	-5	5	-2	1	0	0	0
			220	11	-5	5	-2	1	0	0	0
			440	11	-5	5	-2	1	0	0	0
510	Copertura	62-62	0	10	-9	3	-1	1	0	0	0
			220	10	-9	3	-1	1	0	0	0
			440	10	-9	3	-1	1	0	0	0
511	Copertura	63-63	0	12	-12	1	-1	0	0	0	0
			220	12	-12	1	-1	0	0	0	0
			440	12	-12	1	-1	0	0	0	0
512	Copertura	64-64	0	13	-13	1	-1	0	0	0	0
			220	13	-13	1	-1	0	0	0	0
			440	13	-13	1	-1	0	0	0	0
513	Copertura	65-65	0	13	-13	2	-3	0	-1	0	0
			220	13	-13	2	-3	0	-1	0	0
			440	13	-13	2	-3	0	-1	0	0
514	Copertura	66-66	0	12	-11	2	-5	0	-1	0	0
			220	12	-11	2	-5	0	-1	0	0
			440	12	-11	2	-5	0	-1	0	0
515	Copertura	67-67	0	15	-12	3	-6	0	-1	0	0
			220	15	-12	3	-6	0	-1	0	0

			440	15	-12	3	-6	0	-1	0	0
516	Copertura	68-68	0	13	-11	2	-6	0	-2	0	0
			220	13	-11	2	-6	0	-2	0	0
			440	13	-11	2	-6	0	-2	0	0
517	Copertura	69-69	0	10	-9	1	-4	0	-1	0	0
			220	10	-9	1	-4	0	-1	0	0
			440	10	-9	1	-4	0	-1	0	0
518	Copertura	1-74	0	6	-4	1	0	1	1	1	1
			118	6	-4	1	0	1	1	1	1
			235	6	-4	1	0	1	1	1	1
519	Copertura	74-2	0	2	-2	0	0	0	0	0	0
			118	2	-2	0	0	0	0	0	0
			235	2	-2	0	0	0	0	0	0
520	Copertura	6-71	0	2	-2	0	0	0	0	0	0
			115	2	-2	0	0	0	0	0	0
			231	2	-2	0	0	0	0	0	0
521	Copertura	71-7	0	2	-2	0	0	0	0	0	0
			115	2	-2	0	0	0	0	0	0
			231	2	-2	0	0	0	0	0	0
522	Copertura	9-72	0	3	-2	1	0	0	0	0	0
			115	3	-2	1	0	0	0	0	0
			231	3	-2	1	0	0	0	0	0
523	Copertura	72-10	0	2	-2	1	0	0	0	0	0
			115	2	-2	1	0	0	0	0	0
			231	2	-2	1	0	0	0	0	0
524	Copertura	73-13	0	2	-1	0	0	0	0	0	0
			118	2	-1	0	0	0	0	0	0
			235	2	-1	0	0	0	0	0	0
525	Copertura	14-73	0	1	-2	0	-1	-1	-1	-1	-1
			118	1	-2	0	-1	-1	-1	-1	-1
			235	1	-2	0	-1	-1	-1	-1	-1
526	Copertura	57-75	0	5	-6	0	-1	-1	-1	-1	-1
			118	5	-6	0	-1	-1	-1	-1	-1
			235	5	-6	0	-1	-1	-1	-1	-1
527	Copertura	75-58	0	2	-1	0	0	0	0	0	0
			118	2	-1	0	0	0	0	0	0
			235	2	-1	0	0	0	0	0	0
528	Copertura	77-61	0	2	-1	0	0	0	0	0	0
			115	2	-1	0	0	0	0	0	0
			231	2	-1	0	0	0	0	0	0
529	Copertura	62-77	0	1	-1	0	0	0	0	0	0
			115	1	-1	0	0	0	0	0	0
			231	1	-1	0	0	0	0	0	0
530	Copertura	65-78	0	2	-2	0	-1	0	0	0	0
			115	2	-2	0	-1	0	0	0	0
			231	2	-2	0	-1	0	0	0	0
531	Copertura	78-66	0	2	-1	0	-1	0	0	0	0
			115	2	-1	0	-1	0	0	0	0
			231	2	-1	0	-1	0	0	0	0
532	Copertura	69-76	0	1	-2	0	0	0	0	0	0
			118	1	-2	0	0	0	0	0	0
			235	1	-2	0	0	0	0	0	0
533	Copertura	76-70	0	2	-1	1	0	1	1	1	1
			118	2	-1	1	0	1	1	1	1
			235	2	-1	1	0	1	1	1	1

534	Copertura	1-74	0	6	-6	1	0	0	0	0	0
			118	6	-6	1	0	0	0	0	0
			235	6	-6	1	0	0	0	0	0
535	Copertura	74-2	0	1	-1	0	0	0	0	0	0
			118	1	-1	0	0	0	0	0	0
			235	1	-1	0	0	0	0	0	0
536	Copertura	6-71	0	1	-1	0	-1	0	0	0	0
			115	1	-1	0	-1	0	0	0	0
			231	1	-1	0	-1	0	0	0	0
537	Copertura	71-7	0	2	-2	0	0	0	0	0	0
			115	2	-2	0	0	0	0	0	0
			231	2	-2	0	0	0	0	0	0
538	Copertura	9-72	0	2	-2	0	0	0	0	0	0
			115	2	-2	0	0	0	0	0	0
			231	2	-2	0	0	0	0	0	0
539	Copertura	72-10	0	3	-2	1	0	0	0	0	0
			115	3	-2	1	0	0	0	0	0
			231	3	-2	1	0	0	0	0	0
540	Copertura	73-13	0	2	-2	1	0	0	0	0	0
			118	2	-2	1	0	0	0	0	0
			235	2	-2	1	0	0	0	0	0
541	Copertura	14-73	0	1	-2	0	-1	0	0	0	0
			118	1	-2	0	-1	0	0	0	0
			235	1	-2	0	-1	0	0	0	0
542	Copertura	15-125	0	128	-134	0	-8	-3	-4	-3	-3
			75	128	-134	0	-8	-3	-4	-3	-3
			150	128	-134	0	-8	-3	-4	-3	-3
543	Copertura	127-16	0	31	-14	13	9	10	9	9	9
			75	31	-14	13	9	10	9	9	9
			150	31	-14	13	9	10	9	9	9
544	Copertura	17-129	0	133	-134	4	-6	0	-2	-1	-1
			75	133	-134	4	-6	0	-2	-1	-1
			150	133	-134	4	-6	0	-2	-1	-1
545	Copertura	130-18	0	26	-25	4	-2	1	0	1	1
			75	26	-25	4	-2	1	0	1	1
			150	26	-25	4	-2	1	0	1	1
546	Copertura	19-135	0	134	-134	4	-5	1	-1	0	0
			75	134	-134	4	-5	1	-1	0	0
			150	134	-134	4	-5	1	-1	0	0
547	Copertura	134-20	0	24	-24	3	-3	1	0	0	0
			75	24	-24	3	-3	1	0	0	0
			150	24	-24	3	-3	1	0	0	0
548	Copertura	21-136	0	135	-135	5	-5	1	-1	0	0
			75	135	-135	5	-5	1	-1	0	0
			150	135	-135	5	-5	1	-1	0	0
549	Copertura	138-22	0	24	-25	3	-3	0	-1	0	0
			75	24	-25	3	-3	0	-1	0	0
			150	24	-25	3	-3	0	-1	0	0
550	Copertura	23-141	0	134	-134	5	-5	1	-1	0	0
			75	134	-134	5	-5	1	-1	0	0
			150	134	-134	5	-5	1	-1	0	0
551	Copertura	142-24	0	22	-22	3	-3	0	-1	0	0
			75	22	-22	3	-3	0	-1	0	0
			150	22	-22	3	-3	0	-1	0	0
552	Copertura	25-1	0	132	-132	5	-5	1	-1	0	0

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			75	132	-132	5	-5	1	-1	0	0
			150	132	-132	5	-5	1	-1	0	0
553	Copertura	146-26	0	23	-24	2	-3	0	-1	0	0
			75	23	-24	2	-3	0	-1	0	0
			150	23	-24	2	-3	0	-1	0	0
554	Copertura	150-27	0	20	-21	2	-4	0	-2	-1	-1
			75	20	-21	2	-4	0	-2	-1	-1
			150	20	-21	2	-4	0	-2	-1	-1
555	Copertura	28-149	0	129	-132	3	-6	-1	-2	-1	-1
			75	129	-132	3	-6	-1	-2	-1	-1
			150	129	-132	3	-6	-1	-2	-1	-1
556	Copertura	154-29	0	21	-24	1	-5	-1	-2	-2	-2
			75	21	-24	1	-5	-1	-2	-2	-2
			150	21	-24	1	-5	-1	-2	-2	-2
557	Copertura	30-153	0	129	-134	2	-7	-1	-3	-2	-2
			75	129	-134	2	-7	-1	-3	-2	-2
			150	129	-134	2	-7	-1	-3	-2	-2
558	Copertura	158-31	0	16	-19	1	-5	-1	-2	-2	-2
			75	16	-19	1	-5	-1	-2	-2	-2
			150	16	-19	1	-5	-1	-2	-2	-2
559	Copertura	32-157	0	129	-134	2	-7	-1	-3	-2	-2
			75	129	-134	2	-7	-1	-3	-2	-2
			150	129	-134	2	-7	-1	-3	-2	-2
560	Copertura	162-33	0	17	-21	0	-5	-2	-3	-2	-2
			75	17	-21	0	-5	-2	-3	-2	-2
			150	17	-21	0	-5	-2	-3	-2	-2
561	Copertura	34-161	0	127	-132	2	-7	-1	-3	-2	-2
			75	127	-132	2	-7	-1	-3	-2	-2
			150	127	-132	2	-7	-1	-3	-2	-2
562	Copertura	166-35	0	15	-19	0	-5	-2	-3	-2	-2
			75	15	-19	0	-5	-2	-3	-2	-2
			150	15	-19	0	-5	-2	-3	-2	-2
563	Copertura	36-165	0	127	-132	2	-7	-2	-3	-2	-2
			75	127	-132	2	-7	-2	-3	-2	-2
			150	127	-132	2	-7	-2	-3	-2	-2
564	Copertura	170-37	0	14	-19	0	-6	-2	-3	-2	-2
			75	14	-19	0	-6	-2	-3	-2	-2
			150	14	-19	0	-6	-2	-3	-2	-2
565	Copertura	38-169	0	128	-133	2	-8	-2	-4	-2	-2
			75	128	-133	2	-8	-2	-4	-2	-2
			150	128	-133	2	-8	-2	-4	-2	-2
566	Copertura	175-39	0	13	-18	0	-6	-2	-3	-2	-2
			75	13	-18	0	-6	-2	-3	-2	-2
			150	13	-18	0	-6	-2	-3	-2	-2
567	Copertura	40-173	0	128	-134	1	-8	-2	-4	-2	-2
			75	128	-134	1	-8	-2	-4	-2	-2
			150	128	-134	1	-8	-2	-4	-2	-2
568	Copertura	178-41	0	12	-17	0	-5	-1	-3	-2	-2
			75	12	-17	0	-5	-1	-3	-2	-2
			150	12	-17	0	-5	-1	-3	-2	-2
569	Copertura	42-177	0	129	-135	1	-8	-2	-4	-3	-3
			75	129	-135	1	-8	-2	-4	-3	-3
			150	129	-135	1	-8	-2	-4	-3	-3
570	Copertura	43-181	0	131	-131	5	-5	1	-1	0	0

			75	131	-131	5	-5	1	-1	0	0
			150	131	-131	5	-5	1	-1	0	0
571	Copertura	182-44	0	13	-19	2	-4	0	-1	-1	-1
			75	13	-19	2	-4	0	-1	-1	-1
			150	13	-19	2	-4	0	-1	-1	-1
572	Copertura	45-185	0	132	-131	5	-5	1	-1	0	0
			75	132	-131	5	-5	1	-1	0	0
			150	132	-131	5	-5	1	-1	0	0
573	Copertura	186-46	0	15	-19	3	-3	0	-1	0	0
			75	15	-19	3	-3	0	-1	0	0
			150	15	-19	3	-3	0	-1	0	0
574	Copertura	47-189	0	133	-133	5	-5	1	-1	0	0
			75	133	-133	5	-5	1	-1	0	0
			150	133	-133	5	-5	1	-1	0	0
575	Copertura	190-48	0	16	-20	3	-3	0	-1	0	0
			75	16	-20	3	-3	0	-1	0	0
			150	16	-20	3	-3	0	-1	0	0
576	Copertura	49-193	0	134	-134	5	-4	1	-1	0	0
			75	134	-134	5	-4	1	-1	0	0
			150	134	-134	5	-4	1	-1	0	0
577	Copertura	195-50	0	15	-19	3	-3	0	-1	0	0
			75	15	-19	3	-3	0	-1	0	0
			150	15	-19	3	-3	0	-1	0	0
578	Copertura	51-197	0	133	-133	5	-4	1	-1	0	0
			75	133	-133	5	-4	1	-1	0	0
			150	133	-133	5	-4	1	-1	0	0
579	Copertura	199-52	0	17	-21	2	-3	0	-1	0	0
			75	17	-21	2	-3	0	-1	0	0
			150	17	-21	2	-3	0	-1	0	0
580	Copertura	53-201	0	134	-132	6	-4	2	0	1	1
			75	134	-132	6	-4	2	0	1	1
			150	134	-132	6	-4	2	0	1	1
581	Copertura	202-54	0	17	-25	1	-5	-1	-3	-2	-2
			75	17	-25	1	-5	-1	-3	-2	-2
			150	17	-25	1	-5	-1	-3	-2	-2
582	Copertura	55-205	0	133	-127	8	-1	4	2	3	3
			75	133	-127	8	-1	4	2	3	3
			150	133	-127	8	-1	4	2	3	3
583	Copertura	206-56	0	16	-28	-2	-7	-3	-5	-3	-3
			75	16	-28	-2	-7	-3	-5	-3	-3
			150	16	-28	-2	-7	-3	-5	-3	-3
584	Copertura	57-75	0	6	-6	0	-1	0	0	0	0
			118	6	-6	0	-1	0	0	0	0
			235	6	-6	0	-1	0	0	0	0
585	Copertura	75-58	0	1	-1	0	0	0	0	0	0
			118	1	-1	0	0	0	0	0	0
			235	1	-1	0	0	0	0	0	0
586	Copertura	77-61	0	2	-1	1	0	0	0	0	0
			115	2	-1	1	0	0	0	0	0
			231	2	-1	1	0	0	0	0	0
587	Copertura	62-77	0	1	-1	0	0	0	0	0	0
			115	1	-1	0	0	0	0	0	0
			231	1	-1	0	0	0	0	0	0
588	Copertura	65-78	0	2	-2	0	0	0	0	0	0
			115	2	-2	0	0	0	0	0	0

			231	2	-2	0	0	0	0	0	0
589	Copertura	78-66	0	2	-2	0	-1	0	0	0	0
			115	2	-2	0	-1	0	0	0	0
			231	2	-2	0	-1	0	0	0	0
590	Copertura	69-76	0	2	-2	0	-1	0	0	0	0
			118	2	-2	0	-1	0	0	0	0
			235	2	-2	0	-1	0	0	0	0
591	Copertura	76-70	0	2	-2	1	0	0	0	0	0
			118	2	-2	1	0	0	0	0	0
			235	2	-2	1	0	0	0	0	0
592	Copertura	79-81	0	6	-2	3	2	3	2	2	2
			80	6	-2	3	2	3	2	2	2
			159	6	-2	3	2	3	2	2	2
593	Copertura	80-82	0	5	-4	1	0	1	0	0	0
			66	5	-4	1	0	1	0	0	0
			132	5	-4	1	0	1	0	0	0
594	Copertura	83-84	0	5	-5	0	0	0	0	0	0
			66	5	-5	0	0	0	0	0	0
			132	5	-5	0	0	0	0	0	0
595	Copertura	85-86	0	5	-5	0	0	0	0	0	0
			66	5	-5	0	0	0	0	0	0
			132	5	-5	0	0	0	0	0	0
596	Copertura	87-88	0	4	-4	0	0	0	0	0	0
			66	4	-4	0	0	0	0	0	0
			132	4	-4	0	0	0	0	0	0
597	Copertura	89-90	0	2	-2	0	0	0	0	0	0
			66	2	-2	0	0	0	0	0	0
			132	2	-2	0	0	0	0	0	0
598	Copertura	91-92	0	2	-2	0	0	0	0	0	0
			66	2	-2	0	0	0	0	0	0
			132	2	-2	0	0	0	0	0	0
599	Copertura	93-94	0	3	-3	0	0	0	0	0	0
			66	3	-3	0	0	0	0	0	0
			132	3	-3	0	0	0	0	0	0
600	Copertura	95-96	0	4	-4	0	0	0	0	0	0
			66	4	-4	0	0	0	0	0	0
			132	4	-4	0	0	0	0	0	0
601	Copertura	97-106	0	5	-5	0	0	0	0	0	0
			66	5	-5	0	0	0	0	0	0
			132	5	-5	0	0	0	0	0	0
602	Copertura	98-99	0	4	-4	0	0	0	0	0	0
			66	4	-4	0	0	0	0	0	0
			132	4	-4	0	0	0	0	0	0
603	Copertura	100-101	0	3	-3	0	0	0	0	0	0
			66	3	-3	0	0	0	0	0	0
			132	3	-3	0	0	0	0	0	0
604	Copertura	102-103	0	3	-3	0	0	0	0	0	0
			66	3	-3	0	0	0	0	0	0
			132	3	-3	0	0	0	0	0	0
605	Copertura	104-105	0	2	-2	0	0	0	0	0	0
			66	2	-2	0	0	0	0	0	0
			132	2	-2	0	0	0	0	0	0
606	Copertura	107-108	0	6	-6	0	-1	0	0	0	0
			66	6	-6	0	-1	0	0	0	0
			132	6	-6	0	-1	0	0	0	0

607	Copertura	109-110	0	8	-4	3	2	2	2	2	2
			80	8	-4	3	2	2	2	2	2
			159	8	-4	3	2	2	2	2	2
608	Copertura	111-112	0	2	-2	0	0	0	0	0	0
			66	2	-2	0	0	0	0	0	0
			132	2	-2	0	0	0	0	0	0
609	Copertura	113-114	0	3	-3	0	0	0	0	0	0
			66	3	-3	0	0	0	0	0	0
			132	3	-3	0	0	0	0	0	0
610	Copertura	115-116	0	3	-3	0	0	0	0	0	0
			66	3	-3	0	0	0	0	0	0
			132	3	-3	0	0	0	0	0	0
611	Copertura	117-118	0	4	-4	0	0	0	0	0	0
			66	4	-4	0	0	0	0	0	0
			132	4	-4	0	0	0	0	0	0
612	Copertura	119-120	0	5	-4	0	0	0	0	0	0
			66	5	-4	0	0	0	0	0	0
			132	5	-4	0	0	0	0	0	0
613	Copertura	121-122	0	3	-5	-1	-2	-1	-1	-1	-1
			66	3	-5	-1	-2	-1	-1	-1	-1
			132	3	-5	-1	-2	-1	-1	-1	-1
614	Copertura	124-125	0	33	-33	2	-1	1	0	0	0
			99	33	-33	2	-1	1	0	0	0
			198	33	-33	2	-1	1	0	0	0
615	Copertura	125-127	0	14	-15	0	-1	-1	-1	-1	-1
			775	14	-15	0	-1	-1	-1	-1	-1
			1550	14	-15	0	-1	-1	-1	-1	-1
616	Copertura	126-127	0	5	-8	-1	-2	-1	-1	-1	-1
			99	5	-8	-1	-2	-1	-1	-1	-1
			198	5	-8	-1	-2	-1	-1	-1	-1
617	Copertura	128-129	0	33	-33	1	-1	0	0	0	0
			99	33	-33	1	-1	0	0	0	0
			198	33	-33	1	-1	0	0	0	0
618	Copertura	129-130	0	13	-13	0	0	0	0	0	0
			775	13	-13	0	0	0	0	0	0
			1550	13	-13	0	0	0	0	0	0
619	Copertura	131-130	0	8	-7	0	-1	0	0	0	0
			99	8	-7	0	-1	0	0	0	0
			198	8	-7	0	-1	0	0	0	0
620	Copertura	132-135	0	33	-33	1	-1	0	0	0	0
			99	33	-33	1	-1	0	0	0	0
			198	33	-33	1	-1	0	0	0	0
621	Copertura	133-134	0	8	-7	0	-1	0	0	0	0
			99	8	-7	0	-1	0	0	0	0
			198	8	-7	0	-1	0	0	0	0
622	Copertura	135-134	0	13	-13	0	0	0	0	0	0
			775	13	-13	0	0	0	0	0	0
			1550	13	-13	0	0	0	0	0	0
623	Copertura	137-136	0	33	-33	1	-1	0	0	0	0
			99	33	-33	1	-1	0	0	0	0
			198	33	-33	1	-1	0	0	0	0
624	Copertura	136-138	0	13	-13	0	0	0	0	0	0
			775	13	-13	0	0	0	0	0	0
			1550	13	-13	0	0	0	0	0	0
625	Copertura	139-	0	8	-7	1	-1	0	0	0	0

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			99	8	-7	1	-1	0	0	0	0
			198	8	-7	1	-1	0	0	0	0
626	Copertura	140-141	0	33	-33	1	-1	0	0	0	0
			99	33	-33	1	-1	0	0	0	0
			198	33	-33	1	-1	0	0	0	0
627	Copertura	141-142	0	13	-13	0	0	0	0	0	0
			775	13	-13	0	0	0	0	0	0
			1550	13	-13	0	0	0	0	0	0
628	Copertura	143-142	0	8	-7	1	-1	0	0	0	0
			99	8	-7	1	-1	0	0	0	0
			198	8	-7	1	-1	0	0	0	0
629	Copertura	144-145	0	33	-33	1	-1	0	0	0	0
			99	33	-33	1	-1	0	0	0	0
			198	33	-33	1	-1	0	0	0	0
630	Copertura	145-146	0	13	-13	0	0	0	0	0	0
			775	13	-13	0	0	0	0	0	0
			1550	13	-13	0	0	0	0	0	0
631	Copertura	147-146	0	8	-7	1	0	0	0	0	0
			99	8	-7	1	0	0	0	0	0
			198	8	-7	1	0	0	0	0	0
632	Copertura	148-149	0	33	-33	1	-1	0	0	0	0
			99	33	-33	1	-1	0	0	0	0
			198	33	-33	1	-1	0	0	0	0
633	Copertura	149-150	0	12	-13	0	-1	0	0	0	0
			775	12	-13	0	-1	0	0	0	0
			1550	12	-13	0	-1	0	0	0	0
634	Copertura	151-150	0	9	-8	1	0	0	0	0	0
			99	9	-8	1	0	0	0	0	0
			198	9	-8	1	0	0	0	0	0
635	Copertura	152-153	0	33	-32	1	-1	0	0	0	0
			99	33	-32	1	-1	0	0	0	0
			198	33	-32	1	-1	0	0	0	0
636	Copertura	153-154	0	12	-13	0	-1	0	0	0	0
			775	12	-13	0	-1	0	0	0	0
			1551	12	-13	0	-1	0	0	0	0
637	Copertura	155-154	0	8	-7	1	0	0	0	0	0
			99	8	-7	1	0	0	0	0	0
			198	8	-7	1	0	0	0	0	0
638	Copertura	156-157	0	33	-33	1	-1	0	0	0	0
			99	33	-33	1	-1	0	0	0	0
			198	33	-33	1	-1	0	0	0	0
639	Copertura	157-158	0	12	-13	0	-1	0	0	0	0
			775	12	-13	0	-1	0	0	0	0
			1551	12	-13	0	-1	0	0	0	0
640	Copertura	159-158	0	8	-7	1	0	0	0	0	0
			99	8	-7	1	0	0	0	0	0
			198	8	-7	1	0	0	0	0	0
641	Copertura	160-161	0	33	-32	1	-1	0	0	0	0
			99	33	-32	1	-1	0	0	0	0
			198	33	-32	1	-1	0	0	0	0
642	Copertura	161-162	0	12	-13	0	-1	0	-1	0	0
			776	12	-13	0	-1	0	-1	0	0
			1551	12	-13	0	-1	0	-1	0	0
643	Copertura	163-162	0	8	-7	1	0	0	0	0	0

			99	8	-7	1	0	0	0	0	0
			198	8	-7	1	0	0	0	0	0
644	Copertura	164-165	0	33	-33	1	-1	0	0	0	0
			99	33	-33	1	-1	0	0	0	0
			198	33	-33	1	-1	0	0	0	0
645	Copertura	165-166	0	11	-12	0	-1	0	-1	0	0
			776	11	-12	0	-1	0	-1	0	0
			1551	11	-12	0	-1	0	-1	0	0
646	Copertura	167-166	0	8	-8	1	0	0	0	0	0
			99	8	-8	1	0	0	0	0	0
			198	8	-8	1	0	0	0	0	0
647	Copertura	168-169	0	33	-32	1	-1	0	0	0	0
			99	33	-32	1	-1	0	0	0	0
			198	33	-32	1	-1	0	0	0	0
648	Copertura	169-170	0	12	-13	-1	-1	-1	-1	-1	-1
			776	12	-13	-1	-1	-1	-1	-1	-1
			1552	12	-13	-1	-1	-1	-1	-1	-1
649	Copertura	171-170	0	8	-7	1	0	0	0	0	0
			99	8	-7	1	0	0	0	0	0
			198	8	-7	1	0	0	0	0	0
650	Copertura	172-173	0	33	-32	1	-1	0	0	0	0
			99	33	-32	1	-1	0	0	0	0
			198	33	-32	1	-1	0	0	0	0
651	Copertura	173-175	0	11	-13	-1	-1	-1	-1	-1	-1
			776	11	-13	-1	-1	-1	-1	-1	-1
			1552	11	-13	-1	-1	-1	-1	-1	-1
652	Copertura	174-175	0	8	-7	1	0	0	0	0	0
			99	8	-7	1	0	0	0	0	0
			198	8	-7	1	0	0	0	0	0
653	Copertura	176-177	0	33	-33	1	-1	0	0	0	0
			99	33	-33	1	-1	0	0	0	0
			198	33	-33	1	-1	0	0	0	0
654	Copertura	177-178	0	11	-13	-1	-1	-1	-1	-1	-1
			776	11	-13	-1	-1	-1	-1	-1	-1
			1552	11	-13	-1	-1	-1	-1	-1	-1
655	Copertura	179-178	0	7	-7	1	0	0	0	0	0
			99	7	-7	1	0	0	0	0	0
			198	7	-7	1	0	0	0	0	0
656	Copertura	180-181	0	33	-33	1	-1	0	0	0	0
			99	33	-33	1	-1	0	0	0	0
			198	33	-33	1	-1	0	0	0	0
657	Copertura	181-182	0	12	-12	0	0	0	0	0	0
			775	12	-12	0	0	0	0	0	0
			1550	12	-12	0	0	0	0	0	0
658	Copertura	183-182	0	8	-7	1	0	0	0	0	0
			99	8	-7	1	0	0	0	0	0
			198	8	-7	1	0	0	0	0	0
659	Copertura	184-185	0	33	-33	1	-1	0	0	0	0
			99	33	-33	1	-1	0	0	0	0
			198	33	-33	1	-1	0	0	0	0
660	Copertura	185-186	0	13	-13	0	0	0	0	0	0
			775	13	-13	0	0	0	0	0	0
			1550	13	-13	0	0	0	0	0	0
661	Copertura	187-186	0	8	-8	1	-1	0	0	0	0
			99	8	-8	1	-1	0	0	0	0

			198	8	-8	1	-1	0	0	0	0
662	Copertura	188-189	0	33	-33	1	-1	0	0	0	0
			99	33	-33	1	-1	0	0	0	0
			198	33	-33	1	-1	0	0	0	0
663	Copertura	189-190	0	13	-13	0	0	0	0	0	0
			775	13	-13	0	0	0	0	0	0
			1550	13	-13	0	0	0	0	0	0
664	Copertura	191-190	0	8	-8	1	-1	0	0	0	0
			99	8	-8	1	-1	0	0	0	0
			198	8	-8	1	-1	0	0	0	0
665	Copertura	192-193	0	33	-33	1	-1	0	0	0	0
			99	33	-33	1	-1	0	0	0	0
			198	33	-33	1	-1	0	0	0	0
666	Copertura	193-195	0	13	-13	0	0	0	0	0	0
			775	13	-13	0	0	0	0	0	0
			1550	13	-13	0	0	0	0	0	0
667	Copertura	194-195	0	8	-8	1	-1	0	0	0	0
			99	8	-8	1	-1	0	0	0	0
			198	8	-8	1	-1	0	0	0	0
668	Copertura	196-197	0	33	-33	1	-1	0	0	0	0
			99	33	-33	1	-1	0	0	0	0
			198	33	-33	1	-1	0	0	0	0
669	Copertura	197-199	0	13	-13	0	0	0	0	0	0
			775	13	-13	0	0	0	0	0	0
			1550	13	-13	0	0	0	0	0	0
670	Copertura	198-199	0	8	-8	1	0	0	0	0	0
			99	8	-8	1	0	0	0	0	0
			198	8	-8	1	0	0	0	0	0
671	Copertura	200-201	0	33	-33	1	-1	0	0	0	0
			99	33	-33	1	-1	0	0	0	0
			198	33	-33	1	-1	0	0	0	0
672	Copertura	201-202	0	14	-13	0	0	0	0	0	0
			775	14	-13	0	0	0	0	0	0
			1550	14	-13	0	0	0	0	0	0
673	Copertura	203-202	0	9	-8	1	0	0	0	0	0
			99	9	-8	1	0	0	0	0	0
			198	9	-8	1	0	0	0	0	0
674	Copertura	204-205	0	33	-34	1	-2	0	-1	0	0
			99	33	-34	1	-2	0	-1	0	0
			198	33	-34	1	-2	0	-1	0	0
675	Copertura	205-206	0	14	-13	0	0	0	0	0	0
			775	14	-13	0	0	0	0	0	0
			1550	14	-13	0	0	0	0	0	0
676	Copertura	207-206	0	9	-7	1	0	1	0	0	0
			99	9	-7	1	0	1	0	0	0
			198	9	-7	1	0	1	0	0	0
677	Copertura	79-14	0	80	-56	24	8	16	12	12	12
			125	80	-56	24	8	16	12	12	12
			250	80	-56	24	8	16	12	12	12
678	Copertura	124-15	0	33	-10	17	11	14	11	11	11
			155	33	-10	17	11	14	11	11	11
			310	33	-10	17	11	14	11	11	11
679	Copertura	80-16	0	36	-57	-11	-16	-11	-13	-11	-11
			45	36	-57	-11	-16	-11	-13	-11	-11
			90	36	-57	-11	-16	-11	-13	-11	-11

680	Copertura	128-17	0	25	-21	5	0	3	2	2	2
			155	25	-21	5	0	3	2	2	2
			310	25	-21	5	0	3	2	2	2
681	Copertura	82-18	0	44	-32	14	3	8	6	6	6
			43	44	-32	14	3	8	6	6	6
			85	44	-32	14	3	8	6	6	6
682	Copertura	132-19	0	26	-26	2	-3	0	-1	0	0
			155	26	-26	2	-3	0	-1	0	0
			310	26	-26	2	-3	0	-1	0	0
683	Copertura	83-20	0	38	-37	3	-2	1	0	0	0
			43	38	-37	3	-2	1	0	0	0
			85	38	-37	3	-2	1	0	0	0
684	Copertura	137-21	0	28	-29	1	-2	0	-1	0	0
			155	28	-29	1	-2	0	-1	0	0
			310	28	-29	1	-2	0	-1	0	0
685	Copertura	84-22	0	37	-37	3	-3	0	-1	0	0
			43	37	-37	3	-3	0	-1	0	0
			85	37	-37	3	-3	0	-1	0	0
686	Copertura	140-23	0	27	-27	1	-1	0	0	0	0
			155	27	-27	1	-1	0	0	0	0
			310	27	-27	1	-1	0	0	0	0
687	Copertura	85-24	0	33	-33	1	-1	0	0	0	0
			43	33	-33	1	-1	0	0	0	0
			85	33	-33	1	-1	0	0	0	0
688	Copertura	144-25	0	23	-23	1	-1	0	0	0	0
			155	23	-23	1	-1	0	0	0	0
			310	23	-23	1	-1	0	0	0	0
689	Copertura	86-26	0	38	-38	1	-1	0	0	0	0
			43	38	-38	1	-1	0	0	0	0
			85	38	-38	1	-1	0	0	0	0
690	Copertura	87-27	0	26	-26	0	0	0	0	0	0
			43	26	-26	0	0	0	0	0	0
			85	26	-26	0	0	0	0	0	0
691	Copertura	148-28	0	21	-20	1	0	0	0	0	0
			155	21	-20	1	0	0	0	0	0
			310	21	-20	1	0	0	0	0	0
692	Copertura	88-29	0	34	-34	0	0	0	0	0	0
			43	34	-34	0	0	0	0	0	0
			85	34	-34	0	0	0	0	0	0
693	Copertura	152-30	0	18	-18	1	0	0	0	0	0
			155	18	-18	1	0	0	0	0	0
			310	18	-18	1	0	0	0	0	0
694	Copertura	89-31	0	19	-19	0	-1	0	0	0	0
			43	19	-19	0	-1	0	0	0	0
			85	19	-19	0	-1	0	0	0	0
695	Copertura	156-32	0	19	-19	1	0	0	0	0	0
			155	19	-19	1	0	0	0	0	0
			310	19	-19	1	0	0	0	0	0
696	Copertura	90-33	0	25	-25	0	0	0	0	0	0
			43	25	-25	0	0	0	0	0	0
			85	25	-25	0	0	0	0	0	0
697	Copertura	160-34	0	12	-12	1	0	0	0	0	0
			155	12	-12	1	0	0	0	0	0
			310	12	-12	1	0	0	0	0	0
698	Copertura	91-3	0	23	-23	0	-1	0	0	0	0

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			43	23	-23	0	-1	0	0	0	0
			85	23	-23	0	-1	0	0	0	0
699	Copertura	164-36	0	14	-14	1	0	0	0	0	0
			155	14	-14	1	0	0	0	0	0
			310	14	-14	1	0	0	0	0	0
700	Copertura	92-37	0	25	-26	0	0	0	0	0	0
			43	25	-26	0	0	0	0	0	0
			85	25	-26	0	0	0	0	0	0
701	Copertura	168-38	0	17	-16	1	0	0	0	0	0
			155	17	-16	1	0	0	0	0	0
			310	17	-16	1	0	0	0	0	0
702	Copertura	93-39	0	31	-32	0	0	0	0	0	0
			43	31	-32	0	0	0	0	0	0
			85	31	-32	0	0	0	0	0	0
703	Copertura	172-40	0	16	-15	1	0	0	0	0	0
			155	16	-15	1	0	0	0	0	0
			310	16	-15	1	0	0	0	0	0
704	Copertura	94-41	0	24	-23	0	0	0	0	0	0
			43	24	-23	0	0	0	0	0	0
			85	24	-23	0	0	0	0	0	0
705	Copertura	176-42	0	21	-20	1	0	0	0	0	0
			155	21	-20	1	0	0	0	0	0
			310	21	-20	1	0	0	0	0	0
706	Copertura	180-43	0	21	-21	0	-1	0	0	0	0
			155	21	-21	0	-1	0	0	0	0
			310	21	-21	0	-1	0	0	0	0
707	Copertura	95-44	0	31	-30	1	0	0	0	0	0
			43	31	-30	1	0	0	0	0	0
			85	31	-30	1	0	0	0	0	0
708	Copertura	184-45	0	21	-21	1	-1	0	0	0	0
			155	21	-21	1	-1	0	0	0	0
			310	21	-21	1	-1	0	0	0	0
709	Copertura	96-46	0	33	-34	0	-1	0	0	0	0
			43	33	-34	0	-1	0	0	0	0
			85	33	-34	0	-1	0	0	0	0
710	Copertura	188-47	0	25	-25	1	-1	0	0	0	0
			155	25	-25	1	-1	0	0	0	0
			310	25	-25	1	-1	0	0	0	0
711	Copertura	97-48	0	41	-40	2	-1	1	0	0	0
			43	41	-40	2	-1	1	0	0	0
			85	41	-40	2	-1	1	0	0	0
712	Copertura	192-49	0	29	-28	2	-1	1	0	0	0
			155	29	-28	2	-1	1	0	0	0
			310	29	-28	2	-1	1	0	0	0
713	Copertura	106-50	0	41	-42	1	-2	0	-1	0	0
			43	41	-42	1	-2	0	-1	0	0
			85	41	-42	1	-2	0	-1	0	0
714	Copertura	196-51	0	29	-28	2	-1	1	0	0	0
			155	29	-28	2	-1	1	0	0	0
			310	29	-28	2	-1	1	0	0	0
715	Copertura	107-52	0	47	-50	2	-6	-1	-3	-2	-2
			43	47	-50	2	-6	-1	-3	-2	-2
			85	47	-50	2	-6	-1	-3	-2	-2
716	Copertura	200-53	0	25	-29	0	-5	-2	-3	-2	-2

			155	25	-29	0	-5	-2	-3	-2	-2
			310	25	-29	0	-5	-2	-3	-2	-2
717	Copertura	108-54	0	45	-37	8	3	5	4	4	4
			43	45	-37	8	3	5	4	4	4
			85	45	-37	8	3	5	4	4	4
718	Copertura	204-55	0	13	-37	-12	-17	-12	-14	-12	-12
			155	13	-37	-12	-17	-12	-14	-12	-12
			310	13	-37	-12	-17	-12	-14	-12	-12
719	Copertura	109-56	0	22	-64	-18	-29	-18	-22	-18	-18
			43	22	-64	-18	-29	-18	-22	-18	-18
			85	22	-64	-18	-29	-18	-22	-18	-18
720	Copertura	110-70	0	68	-130	-21	-51	-31	-38	-31	-31
			43	68	-130	-21	-51	-31	-38	-31	-31
			85	68	-130	-21	-51	-31	-38	-31	-31
721	Copertura	14-79	0	-4	-145	-59	-90	-59	-71	-59	-59
			95	-4	-145	-59	-90	-59	-71	-59	-59
			190	-4	-145	-59	-90	-59	-71	-59	-59
722	Copertura	15-124	0	27	-17	9	4	6	5	5	5
			65	27	-17	9	4	6	5	5	5
			130	27	-17	9	4	6	5	5	5
723	Copertura	16-126	0	-3	-43	-20	-29	-20	-24	-20	-20
			65	-3	-43	-20	-29	-20	-24	-20	-20
			130	-3	-43	-20	-29	-20	-24	-20	-20
724	Copertura	17-128	0	30	-28	4	-1	2	1	1	1
			65	30	-28	4	-1	2	1	1	1
			130	30	-28	4	-1	2	1	1	1
725	Copertura	18-131	0	17	-19	1	-4	-1	-2	-1	-1
			65	17	-19	1	-4	-1	-2	-1	-1
			130	17	-19	1	-4	-1	-2	-1	-1
726	Copertura	19-132	0	25	-25	2	-2	0	-1	0	0
			65	25	-25	2	-2	0	-1	0	0
			130	25	-25	2	-2	0	-1	0	0
727	Copertura	20-133	0	16	-16	1	-1	0	0	0	0
			65	16	-16	1	-1	0	0	0	0
			130	16	-16	1	-1	0	0	0	0
728	Copertura	21-137	0	24	-24	1	-2	0	0	0	0
			65	24	-24	1	-2	0	0	0	0
			130	24	-24	1	-2	0	0	0	0
729	Copertura	22-139	0	17	-17	2	-1	0	0	0	0
			65	17	-17	2	-1	0	0	0	0
			130	17	-17	2	-1	0	0	0	0
730	Copertura	23-140	0	23	-23	1	-1	0	0	0	0
			65	23	-23	1	-1	0	0	0	0
			130	23	-23	1	-1	0	0	0	0
731	Copertura	24-143	0	14	-14	1	0	0	0	0	0
			65	14	-14	1	0	0	0	0	0
			130	14	-14	1	0	0	0	0	0
732	Copertura	25-144	0	24	-24	1	-1	0	0	0	0
			65	24	-24	1	-1	0	0	0	0
			130	24	-24	1	-1	0	0	0	0
733	Copertura	26-147	0	20	-20	1	-1	0	0	0	0
			65	20	-20	1	-1	0	0	0	0
			130	20	-20	1	-1	0	0	0	0
734	Copertura	27-151	0	17	-17	0	0	0	0	0	0
			65	17	-17	0	0	0	0	0	0

			130	17	-17	0	0	0	0	0	0
735	Copertura	28-148	0	23	-24	1	-1	0	0	0	0
			65	23	-24	1	-1	0	0	0	0
			130	23	-24	1	-1	0	0	0	0
736	Copertura	29-155	0	15	-15	0	0	0	0	0	0
			65	15	-15	0	0	0	0	0	0
			130	15	-15	0	0	0	0	0	0
737	Copertura	30-152	0	19	-20	1	-2	0	0	0	0
			65	19	-20	1	-2	0	0	0	0
			130	19	-20	1	-2	0	0	0	0
738	Copertura	31-159	0	13	-13	0	0	0	0	0	0
			65	13	-13	0	0	0	0	0	0
			130	13	-13	0	0	0	0	0	0
739	Copertura	32-156	0	20	-21	1	-2	0	0	0	0
			65	20	-21	1	-2	0	0	0	0
			130	20	-21	1	-2	0	0	0	0
740	Copertura	33-163	0	14	-14	0	0	0	0	0	0
			65	14	-14	0	0	0	0	0	0
			130	14	-14	0	0	0	0	0	0
741	Copertura	34-160	0	21	-22	1	-2	0	0	0	0
			65	21	-22	1	-2	0	0	0	0
			130	21	-22	1	-2	0	0	0	0
742	Copertura	35-167	0	19	-19	0	-1	0	0	0	0
			65	19	-19	0	-1	0	0	0	0
			130	19	-19	0	-1	0	0	0	0
743	Copertura	36-164	0	24	-24	1	-2	0	-1	0	0
			65	24	-24	1	-2	0	-1	0	0
			130	24	-24	1	-2	0	-1	0	0
744	Copertura	37-171	0	15	-16	0	-1	0	0	0	0
			65	15	-16	0	-1	0	0	0	0
			130	15	-16	0	-1	0	0	0	0
745	Copertura	38-168	0	21	-21	1	-2	0	-1	0	0
			65	21	-21	1	-2	0	-1	0	0
			130	21	-21	1	-2	0	-1	0	0
746	Copertura	39-174	0	14	-15	0	-1	0	0	0	0
			65	14	-15	0	-1	0	0	0	0
			130	14	-15	0	-1	0	0	0	0
747	Copertura	40-172	0	18	-19	1	-2	0	-1	0	0
			65	18	-19	1	-2	0	-1	0	0
			130	18	-19	1	-2	0	-1	0	0
748	Copertura	41-179	0	10	-10	0	0	0	0	0	0
			65	10	-10	0	0	0	0	0	0
			130	10	-10	0	0	0	0	0	0
749	Copertura	42-176	0	22	-23	1	-2	0	-1	0	0
			65	22	-23	1	-2	0	-1	0	0
			130	22	-23	1	-2	0	-1	0	0
750	Copertura	43-180	0	26	-26	1	-1	0	0	0	0
			65	26	-26	1	-1	0	0	0	0
			130	26	-26	1	-1	0	0	0	0
751	Copertura	44-183	0	17	-17	0	0	0	0	0	0
			65	17	-17	0	0	0	0	0	0
			130	17	-17	0	0	0	0	0	0
752	Copertura	45-184	0	27	-28	1	-1	0	0	0	0
			65	27	-28	1	-1	0	0	0	0
			130	27	-28	1	-1	0	0	0	0

753	Copertura	46-187	0	21	-20	0	0	0	0	0	0
			65	21	-20	0	0	0	0	0	0
			130	21	-20	0	0	0	0	0	0
754	Copertura	47-188	0	22	-23	1	-1	0	0	0	0
			65	22	-23	1	-1	0	0	0	0
			130	22	-23	1	-1	0	0	0	0
755	Copertura	48-191	0	19	-19	1	-1	0	0	0	0
			65	19	-19	1	-1	0	0	0	0
			130	19	-19	1	-1	0	0	0	0
756	Copertura	49-192	0	25	-26	1	-1	0	0	0	0
			65	25	-26	1	-1	0	0	0	0
			130	25	-26	1	-1	0	0	0	0
757	Copertura	50-194	0	18	-19	0	-1	0	0	0	0
			65	18	-19	0	-1	0	0	0	0
			130	18	-19	0	-1	0	0	0	0
758	Copertura	51-196	0	25	-27	2	-2	1	0	0	0
			65	25	-27	2	-2	1	0	0	0
			130	25	-27	2	-2	1	0	0	0
759	Copertura	52-198	0	19	-19	2	-2	0	-1	0	0
			65	19	-19	2	-2	0	-1	0	0
			130	19	-19	2	-2	0	-1	0	0
760	Copertura	53-200	0	30	-35	1	-4	-1	-2	-1	-1
			65	30	-35	1	-4	-1	-2	-1	-1
			130	30	-35	1	-4	-1	-2	-1	-1
761	Copertura	54-203	0	27	-22	5	2	4	3	3	3
			65	27	-22	5	2	4	3	3	3
			130	27	-22	5	2	4	3	3	3
762	Copertura	55-204	0	18	-30	-4	-9	-5	-6	-5	-5
			65	18	-30	-4	-9	-5	-6	-5	-5
			130	18	-30	-4	-9	-5	-6	-5	-5
763	Copertura	56-207	0	22	-9	10	6	8	6	6	6
			65	22	-9	10	6	8	6	6	6
			130	22	-9	10	6	8	6	6	6
764	Copertura	70-123	0	102	-24	47	31	37	31	31	31
			95	102	-24	47	31	37	31	31	31
			190	102	-24	47	31	37	31	31	31
765	Copertura	81-80	0	53	-20	22	14	16	14	14	14
			80	53	-20	22	14	16	14	14	14
			160	53	-20	22	14	16	14	14	14
766	Copertura	126-81	0	-27	-90	-48	-71	-48	-57	-48	-48
			30	-27	-90	-48	-71	-48	-57	-48	-48
			60	-27	-90	-48	-71	-48	-57	-48	-48
767	Copertura	98-82	0	26	-39	-7	-10	-7	-8	-7	-7
			82	26	-39	-7	-10	-7	-8	-7	-7
			165	26	-39	-7	-10	-7	-8	-7	-7
768	Copertura	99-83	0	35	-33	5	-3	2	0	1	1
			82	35	-33	5	-3	2	0	1	1
			165	35	-33	5	-3	2	0	1	1
769	Copertura	100-84	0	36	-34	2	0	1	1	1	1
			82	36	-34	2	0	1	1	1	1
			165	36	-34	2	0	1	1	1	1
770	Copertura	101-85	0	36	-36	2	-2	0	0	0	0
			82	36	-36	2	-2	0	0	0	0
			165	36	-36	2	-2	0	0	0	0
771	Copertura	102-	0	31	-31	0	0	0	0	0	0

	a	86									
			82	31	-31	0	0	0	0	0	0
			165	31	-31	0	0	0	0	0	0
772	Copertura	103-87	0	35	-35	1	-1	0	0	0	0
			82	35	-35	1	-1	0	0	0	0
			165	35	-35	1	-1	0	0	0	0
773	Copertura	104-88	0	23	-23	0	0	0	0	0	0
			82	23	-23	0	0	0	0	0	0
			165	23	-23	0	0	0	0	0	0
774	Copertura	105-89	0	28	-28	0	0	0	0	0	0
			82	28	-28	0	0	0	0	0	0
			165	28	-28	0	0	0	0	0	0
775	Copertura	111-90	0	20	-20	0	0	0	0	0	0
			80	20	-20	0	0	0	0	0	0
			160	20	-20	0	0	0	0	0	0
776	Copertura	112-91	0	19	-19	0	0	0	0	0	0
			82	19	-19	0	0	0	0	0	0
			165	19	-19	0	0	0	0	0	0
777	Copertura	113-92	0	22	-22	0	0	0	0	0	0
			82	22	-22	0	0	0	0	0	0
			165	22	-22	0	0	0	0	0	0
778	Copertura	114-93	0	18	-18	0	-1	0	0	0	0
			82	18	-18	0	-1	0	0	0	0
			165	18	-18	0	-1	0	0	0	0
779	Copertura	115-94	0	21	-21	0	0	0	0	0	0
			82	21	-21	0	0	0	0	0	0
			165	21	-21	0	0	0	0	0	0
780	Copertura	116-95	0	22	-22	0	0	0	0	0	0
			82	22	-22	0	0	0	0	0	0
			165	22	-22	0	0	0	0	0	0
781	Copertura	117-96	0	41	-41	1	-1	0	0	0	0
			82	41	-41	1	-1	0	0	0	0
			165	41	-41	1	-1	0	0	0	0
782	Copertura	118-97	0	27	-27	0	0	0	0	0	0
			82	27	-27	0	0	0	0	0	0
			165	27	-27	0	0	0	0	0	0
783	Copertura	131-98	0	23	-27	-1	-5	-2	-3	-2	-2
			30	23	-27	-1	-5	-2	-3	-2	-2
			60	23	-27	-1	-5	-2	-3	-2	-2
784	Copertura	133-99	0	24	-24	0	-1	0	0	0	0
			30	24	-24	0	-1	0	0	0	0
			60	24	-24	0	-1	0	0	0	0
785	Copertura	139-100	0	25	-23	2	-1	1	0	0	0
			30	25	-23	2	-1	1	0	0	0
			60	25	-23	2	-1	1	0	0	0
786	Copertura	143-101	0	25	-24	1	0	0	0	0	0
			30	25	-24	1	0	0	0	0	0
			60	25	-24	1	0	0	0	0	0
787	Copertura	147-102	0	28	-27	1	-1	0	0	0	0
			30	28	-27	1	-1	0	0	0	0
			60	28	-27	1	-1	0	0	0	0
788	Copertura	151-103	0	30	-30	0	-1	0	0	0	0
			30	30	-30	0	-1	0	0	0	0
			60	30	-30	0	-1	0	0	0	0
789	Copertura	155-104	0	29	-29	0	0	0	0	0	0

			30	29	-29	0	0	0	0	0	0
			60	29	-29	0	0	0	0	0	0
790	Copertura	159-105	0	29	-29	0	0	0	0	0	0
			30	29	-29	0	0	0	0	0	0
			60	29	-29	0	0	0	0	0	0
791	Copertura	119-106	0	39	-39	3	-3	1	-1	0	0
			82	39	-39	3	-3	1	-1	0	0
			165	39	-39	3	-3	1	-1	0	0
792	Copertura	120-107	0	32	-32	2	-1	1	0	0	0
			82	32	-32	2	-1	1	0	0	0
			165	32	-32	2	-1	1	0	0	0
793	Copertura	121-108	0	27	-32	2	-7	-2	-3	-2	-2
			82	27	-32	2	-7	-2	-3	-2	-2
			165	27	-32	2	-7	-2	-3	-2	-2
794	Copertura	122-109	0	67	-15	37	25	30	25	25	25
			82	67	-15	37	25	30	25	25	25
			165	67	-15	37	25	30	25	25	25
795	Copertura	123-110	0	102	-24	47	31	37	31	31	31
			82	102	-24	47	31	37	31	31	31
			165	102	-24	47	31	37	31	31	31
796	Copertura	163-111	0	33	-32	0	0	0	0	0	0
			33	33	-32	0	0	0	0	0	0
			65	33	-32	0	0	0	0	0	0
797	Copertura	167-112	0	33	-33	0	0	0	0	0	0
			30	33	-33	0	0	0	0	0	0
			60	33	-33	0	0	0	0	0	0
798	Copertura	171-113	0	32	-32	0	0	0	0	0	0
			30	32	-32	0	0	0	0	0	0
			60	32	-32	0	0	0	0	0	0
799	Copertura	174-114	0	31	-30	0	0	0	0	0	0
			30	31	-30	0	0	0	0	0	0
			60	31	-30	0	0	0	0	0	0
800	Copertura	179-115	0	21	-20	1	0	0	0	0	0
			30	21	-20	1	0	0	0	0	0
			60	21	-20	1	0	0	0	0	0
801	Copertura	183-116	0	21	-21	1	0	0	0	0	0
			30	21	-21	1	0	0	0	0	0
			60	21	-21	1	0	0	0	0	0
802	Copertura	187-117	0	28	-28	1	-1	0	0	0	0
			30	28	-28	1	-1	0	0	0	0
			60	28	-28	1	-1	0	0	0	0
803	Copertura	191-118	0	30	-31	1	-1	0	0	0	0
			30	30	-31	1	-1	0	0	0	0
			60	30	-31	1	-1	0	0	0	0
804	Copertura	194-119	0	34	-34	0	-1	0	-1	-1	-1
			30	34	-34	0	-1	0	-1	-1	-1
			60	34	-34	0	-1	0	-1	-1	-1
805	Copertura	198-120	0	33	-34	1	-2	0	-1	-1	-1
			30	33	-34	1	-2	0	-1	-1	-1
			60	33	-34	1	-2	0	-1	-1	-1
806	Copertura	203-121	0	38	-24	10	6	8	6	6	6
			30	38	-24	10	6	8	6	6	6
			60	38	-24	10	6	8	6	6	6
807	Copertura	207-122	0	55	-17	22	15	18	15	15	15
			30	55	-17	22	15	18	15	15	15

			60	55	-17	22	15	18	15	15	15
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1.2.4 Involuppi dei diagrammi delle sollecitazioni: Momento Flettente X-Z.

I dati seguenti riportano i valori del Momento Flettente X-Z relativamente alle aste che definiscono la struttura ed in modo particolare:

Asta : numerazione interna dell'asta.
X : distanza dal nodo iniziale misurata lungo l'asse dell'asta.
Momento Flettente (M_{xz}) : valore del Momento Flettente X-Z nel punto considerato:
Max : valore massimo (rispetto al sistema di riferimento globale) dell'involuppo.
Min : valore minimo (rispetto al sistema di riferimento globale) dell'involuppo.
Comb : combinazione di appartenenza del valore considerato nell'involuppo.

Tabella 29.I

Momento Flettente (M_{xz}) [daNm]											
				SLU		SLE					
						Caratteristiche		Frequenti		Quasi Permanenti	
Asta	Imp.	Fili	X [cm]	Max	Min	Max	Min	Max	Min	Max	Min
1	Fondazio ne	1-2	0	1315	-1345	74	-70	13	-16	-15	-15
			42	504	-919	-150	-403	-238	-289	-245	-245
			83	1453	-1975	-187	-512	-300	-365	-310	-310
2	Fondazio ne	1-2	0	437	-1197	-313	-603	-404	-462	-417	-417
			42	1132	-1639	-176	-521	-294	-363	-305	-305
			83	1694	-1670	121	-281	-34	-114	-71	-71
3	Fondazio ne	1-15	0	989	-1196	-58	-126	-74	-89	-89	-89
			40	498	-976	-157	-309	-213	-244	-220	-220
			80	1946	-2135	-21	-303	-146	-202	-176	-176
4	Fondazio ne	1-15	0	785	-1589	-283	-495	-355	-397	-370	-370
			40	1970	-2188	-1	-282	-122	-179	-154	-154
			80	3117	-2449	500	173	321	243	243	243
5	Fondazio ne	2-3	0	1155	-1282	48	-354	-102	-182	-145	-145
			35	1041	-1392	-104	-400	-207	-266	-224	-224
			69	932	-1344	-159	-360	-224	-265	-235	-235
6	Fondazio ne	2-3	0	631	-1152	-212	-409	-273	-312	-289	-289
			35	631	-956	-134	-266	-174	-200	-179	-179
			69	651	-634	34	-50	5	-12	-9	-9
7	Fondazio ne	3-4	0	507	-535	20	-87	-18	-39	-37	-37
			35	433	-639	-91	-153	-107	-120	-109	-109
			69	388	-647	-117	-148	-122	-128	-124	-124
8	Fondazio ne	3-4	0	360	-566	-83	-173	-121	-139	-134	-134
			35	237	-378	-65	-81	-65	-70	-65	-65
			69	230	-99	101	4	75	56	59	59
9	Fondazio ne	4-5	0	183	-52	85	47	71	56	56	56
			35	127	-193	-31	-40	-31	-34	-31	-31
			69	168	-292	-46	-79	-57	-64	-62	-62
10	Fondazio ne	4-5	0	110	-189	-21	-73	-47	-58	-58	-58
			35	117	-149	1	-40	-14	-22	-16	-16
			69	260	-112	132	28	101	80	84	84
11	Fondazio ne	5-6	0	244	-79	124	64	102	87	87	87
			35	142	-149	23	-36	0	-12	-4	-4
			69	196	-264	11	-76	-23	-41	-34	-34
12	Fondazio ne	5-6	0	156	-217	12	-67	-20	-36	-30	-30
			35	332	-311	75	-58	22	-5	10	10
			69	597	-373	225	31	144	105	112	112
13	Fondazio ne	6-7	0	611	-390	234	31	148	108	116	116

			35	228	-205	53	-34	18	1	11	11
			69	103	-147	-17	-41	-26	-31	-31	-31
14	Fondazio ne	6-7	0	15	-68	0	-35	-19	-26	-26	-26
			35	253	-243	52	-48	12	-8	5	5
			69	597	-402	217	6	129	87	98	98
15	Fondazio ne	7-8	0	605	-401	223	13	135	93	102	102
			35	318	-326	59	-74	6	-20	-4	-4
			69	119	-196	-20	-77	-42	-54	-48	-48
16	Fondazio ne	7-8	0	154	-256	-11	-91	-42	-58	-51	-51
			35	55	-100	-15	-43	-23	-30	-23	-23
			69	169	-74	103	24	80	64	67	67
17	Fondazio ne	8-9	0	196	-120	110	6	80	59	65	65
			35	54	-101	-10	-36	-18	-25	-18	-18
			69	154	-232	0	-76	-30	-45	-39	-39
18	Fondazio ne	8-9	0	73	-182	-24	-76	-44	-54	-50	-50
			35	295	-297	58	-66	9	-16	-1	-1
			69	601	-382	226	27	142	102	110	110
19	Fondazio ne	9-10	0	605	-411	221	12	134	92	102	102
			35	245	-218	58	-33	21	3	14	14
			69	110	-120	19	-21	-4	-13	-13	-13
20	Fondazio ne	9-10	0	54	-105	-18	-30	-22	-26	-26	-26
			35	261	-228	64	-32	25	6	17	17
			69	607	-368	241	36	154	113	120	120
21	Fondazio ne	10-1 1	0	607	-363	239	40	155	115	122	122
			35	368	-354	78	-66	21	-8	7	7
			69	198	-295	0	-91	-35	-53	-48	-48
22	Fondazio ne	10-1 1	0	213	-314	-5	-95	-39	-57	-50	-50
			35	166	-226	-3	-66	-26	-38	-30	-30
			69	182	-80	79	39	64	48	48	48
23	Fondazio ne	11-1 2	0	230	-116	101	-1	74	53	57	57
			35	85	-227	-70	-90	-71	-76	-71	-71
			69	36	-322	-96	-180	-130	-147	-143	-143
24	Fondazio ne	11-1 2	0	10	-270	-130	-152	-130	-134	-130	-130
			35	82	-324	-108	-163	-121	-132	-121	-121
			69	217	-328	2	-108	-36	-57	-55	-55
25	Fondazio ne	12-1 3	0	167	-222	14	-72	-15	-32	-28	-28
			35	138	-513	-140	-282	-183	-211	-188	-188
			69	165	-739	-205	-417	-271	-313	-287	-287
26	Fondazio ne	12-1 3	0	145	-628	-163	-371	-231	-272	-241	-241
			35	342	-806	-112	-412	-216	-276	-232	-232
			69	701	-1009	36	-367	-113	-193	-154	-154
27	Fondazio ne	13-1 4	0	687	-844	112	-293	-43	-124	-78	-78
			42	336	-946	-175	-527	-295	-365	-305	-305
			83	163	-979	-301	-600	-395	-455	-408	-408
28	Fondazio ne	13-1 4	0	257	-806	-160	-463	-265	-326	-275	-275
			42	279	-743	-139	-385	-225	-275	-232	-232
			83	514	-583	70	-82	6	-24	-23	-23
29	Fondazio ne	14-1 6	0	189	-353	-48	-115	-66	-82	-82	-82
			40	-42	-439	-166	-311	-219	-248	-224	-224
			80	179	-535	-63	-304	-168	-216	-191	-191
30	Fondazio ne	14-1 6	0	9	-619	-266	-464	-334	-374	-350	-350
			40	304	-507	-30	-276	-136	-185	-162	-162
			80	857	-284	425	154	274	206	206	206
31	Fondazio ne	15-1 7	0	2637	-2538	241	-68	98	36	37	37
			33	1842	-1896	70	-164	-36	-83	-71	-71

			66	1146	-1080	68	-87	-12	-47	-47	-47
32	Fondazio ne	15-1 7	0	834	-1315	-170	-317	-221	-251	-239	-239
			33	197	-112	84	22	47	22	22	22
			66	1621	-613	607	421	506	421	421	421
33	Fondazio ne	16-1 8	0	791	-488	204	-55	82	29	29	29
			33	367	-381	50	-152	-42	-82	-73	-73
			66	200	-243	64	-73	-8	-43	-43	-43
34	Fondazio ne	16-1 8	0	68	-464	-154	-280	-199	-224	-216	-216
			33	127	-86	74	14	39	14	14	14
			66	850	-11	552	385	464	385	385	385
35	Fondazio ne	17-1 9	0	1280	-614	397	267	329	267	267	267
			33	252	-152	77	35	55	35	35	35
			66	590	-627	-1	-62	-31	-51	-51	-51
36	Fondazio ne	17-1 9	0	203	-453	-94	-165	-116	-131	-126	-126
			33	919	-805	109	34	68	47	47	47
			66	2078	-1253	547	372	442	372	372	372
37	Fondazio ne	18-2 0	0	569	-27	381	257	318	257	257	257
			33	175	-94	82	41	61	41	41	41
			66	167	-202	20	-35	-9	-28	-28	-28
38	Fondazio ne	18-2 0	0	140	-378	-88	-155	-109	-122	-119	-119
			33	322	-177	90	24	55	36	36	36
			66	1040	-288	500	344	407	344	344	344
39	Fondazio ne	19-2 1	0	2048	-1352	446	299	357	299	299	299
			33	915	-808	97	29	63	47	47	47
			66	116	-215	-40	-55	-44	-49	-49	-49
40	Fondazio ne	19-2 1	0	212	-380	-66	-115	-80	-90	-84	-84
			33	678	-543	102	43	72	59	59	59
			66	1890	-1056	514	359	421	359	359	359
41	Fondazio ne	20-2 2	0	961	-228	417	283	337	283	283	283
			33	314	-179	81	22	52	38	38	38
			66	70	-169	-42	-54	-45	-50	-50	-50
42	Fondazio ne	20-2 2	0	152	-335	-76	-127	-89	-99	-92	-92
			33	180	-79	88	38	62	51	51	51
			66	836	-131	501	352	413	352	352	352
43	Fondazio ne	21-2 3	0	1641	-838	486	341	399	341	341	341
			33	607	-472	97	46	71	60	60	60
			66	100	-244	-61	-82	-64	-68	-64	-64
44	Fondazio ne	21-2 3	0	203	-339	-62	-90	-68	-74	-68	-68
			33	665	-530	100	55	74	64	64	64
			66	1858	-1088	503	351	410	351	351	351
45	Fondazio ne	22-2 4	0	703	38	465	329	384	329	329	329
			33	157	-64	76	34	55	46	46	46
			66	10	-163	-77	-96	-77	-82	-77	-77
46	Fondazio ne	22-2 4	0	145	-313	-83	-115	-84	-94	-84	-84
			33	226	-133	54	11	33	25	28	28
			66	924	-298	430	299	350	299	299	299
47	Fondazio ne	23-2 5	0	2086	-1270	556	386	450	386	386	386
			33	649	-627	39	-14	15	5	11	11
			66	101	-571	-213	-286	-213	-241	-213	-213
48	Fondazio ne	23-2 5	0	72	-386	-143	-185	-143	-163	-143	-143
			33	896	-1170	-104	-192	-121	-146	-121	-121
			66	2000	-1881	147	-10	76	45	48	48
49	Fondazio ne	24-2 6	0	930	-208	441	305	355	305	305	305
			33	164	-194	-13	-65	-31	-43	-31	-31
			66	-55	-383	-211	-279	-211	-238	-211	-211

50	Fondazio ne	24-2 6	0	80	-473	-196	-261	-196	-224	-196	-196
			33	60	-406	-139	-194	-139	-162	-139	-139
			66	591	-446	153	50	99	72	72	72
51	Fondazio ne	25-2 6	0	2212	-3096	-135	-939	-423	-583	-442	-442
			49	1481	-2787	-428	-1118	-653	-791	-653	-653
			97	1101	-2236	-390	-928	-559	-666	-568	-568
52	Fondazio ne	25-2 6	0	906	-2117	-447	-947	-597	-697	-605	-605
			49	633	-1898	-529	-931	-633	-719	-633	-633
			97	541	-1542	-404	-729	-492	-557	-500	-500
53	Fondazio ne	25-2 6	0	421	-1327	-380	-638	-444	-495	-453	-453
			49	272	-1131	-398	-585	-430	-471	-430	-430
			97	253	-888	-280	-429	-309	-338	-317	-317
54	Fondazio ne	25-2 6	0	190	-709	-236	-341	-251	-272	-260	-260
			49	88	-548	-230	-292	-230	-248	-230	-230
			97	105	-378	-127	-166	-128	-137	-137	-137
55	Fondazio ne	25-2 6	0	78	-265	-73	-99	-79	-88	-88	-88
			49	95	-265	-82	-107	-85	-90	-85	-85
			97	151	-186	5	-22	-4	-17	-17	-17
56	Fondazio ne	25-2 6	0	188	-169	38	3	25	9	9	9
			49	164	-189	6	-35	-10	-18	-13	-13
			97	198	-119	72	35	55	40	40	40
57	Fondazio ne	25-2 6	0	200	-99	84	47	66	51	51	51
			49	143	-118	29	-5	14	7	12	12
			97	172	-56	89	58	73	58	58	58
58	Fondazio ne	25-2 6	0	159	-38	89	60	74	60	60	60
			49	92	-64	24	2	14	9	14	14
			97	125	-8	84	58	71	58	58	58
59	Fondazio ne	25-2 6	0	109	6	81	57	69	57	57	57
			49	47	-29	12	1	9	4	9	9
			97	102	27	77	56	67	56	56	56
60	Fondazio ne	25-2 6	0	100	41	74	55	65	55	55	55
			49	12	1	6	0	6	2	6	6
			97	99	42	74	54	65	54	54	54
61	Fondazio ne	25-2 6	0	97	29	73	53	64	53	53	53
			49	44	-27	11	0	8	3	8	8
			97	111	5	82	58	70	58	58	58
62	Fondazio ne	25-2 6	0	129	-9	86	60	72	60	60	60
			49	99	-66	27	4	16	11	16	16
			97	171	-45	94	63	78	63	63	63
63	Fondazio ne	25-2 6	0	186	-64	93	61	76	61	61	61
			49	160	-129	35	-2	18	11	16	16
			97	225	-117	90	50	71	54	54	54
64	Fondazio ne	25-2 6	0	224	-139	78	38	59	43	43	43
			49	191	-213	10	-34	-7	-16	-11	-11
			97	218	-201	40	1	25	8	8	8
65	Fondazio ne	25-2 6	0	177	-218	3	-27	-7	-20	-20	-20
			49	117	-299	-88	-114	-91	-97	-91	-91
			97	90	-287	-85	-112	-90	-99	-99	-99
66	Fondazio ne	25-2 6	0	112	-407	-140	-180	-140	-149	-147	-147
			49	98	-587	-245	-311	-245	-265	-245	-245
			97	209	-769	-261	-368	-274	-296	-280	-280
67	Fondazio ne	25-2 6	0	289	-979	-312	-469	-340	-370	-345	-345
			49	343	-1279	-437	-645	-468	-517	-468	-468
			97	534	-1540	-425	-720	-497	-556	-503	-503
68	Fondazio	25-2	0	666	-1760	-445	-812	-542	-615	-547	-547

	ne	6									
			49	729	-2061	-568	-986	-666	-760	-666	-666
			97	923	-2165	-477	-971	-617	-716	-621	-621
69	Fondazio ne	25-2 6	0	1126	-2302	-417	-975	-586	-697	-588	-588
			49	1581	-2968	-473	-1197	-693	-845	-693	-693
			97	2340	-3316	-180	-1030	-473	-643	-488	-488
70	Fondazio ne	25-2 8	0	1686	-1421	193	63	126	92	92	92
			43	649	-1114	-214	-301	-214	-251	-214	-214
			85	-35	-532	-283	-381	-283	-323	-283	-283
71	Fondazio ne	25-2 8	0	273	-865	-296	-409	-296	-336	-296	-296
			43	539	-784	-107	-164	-107	-130	-107	-107
			85	2231	-1527	477	324	382	324	324	324
72	Fondazio ne	26-2 7	0	350	-195	134	49	88	65	65	65
			33	113	-406	-147	-200	-147	-170	-147	-147
			66	-75	-343	-204	-265	-204	-232	-204	-204
73	Fondazio ne	26-2 7	0	157	-612	-227	-309	-227	-258	-227	-227
			33	134	-220	-45	-86	-52	-65	-52	-52
			66	1017	-454	404	282	328	282	282	282
74	Fondazio ne	27-2 9	0	948	-320	385	263	310	263	263	263
			33	210	-211	23	-29	2	-8	-1	-1
			66	40	-246	-103	-135	-103	-116	-103	-103
75	Fondazio ne	27-2 9	0	138	-375	-119	-163	-119	-132	-119	-119
			33	188	-209	34	-18	13	3	9	9
			66	1007	-403	431	302	351	302	302	302
76	Fondazio ne	28-3 0	0	2412	-1748	478	309	376	317	317	317
			37	1113	-1117	47	-51	9	-11	2	2
			73	291	-610	-129	-177	-129	-145	-129	-129
77	Fondazio ne	28-3 0	0	461	-808	-147	-216	-152	-171	-152	-152
			37	163	-198	-12	-24	-12	-17	-12	-12
			73	1097	-460	454	319	372	319	319	319
78	Fondazio ne	29-3 1	0	823	-226	421	299	349	299	299	299
			33	167	-176	32	-10	16	7	12	12
			66	14	-231	-109	-146	-109	-122	-109	-109
79	Fondazio ne	29-3 1	0	130	-361	-116	-160	-116	-129	-116	-116
			33	177	-191	7	-32	-6	-14	-7	-7
			66	986	-447	382	269	314	269	269	269
80	Fondazio ne	30-3 2	0	939	-338	423	301	352	301	301	301
			34	168	-154	7	3	7	5	7	7
			69	125	-384	-116	-160	-116	-130	-116	-116
81	Fondazio ne	30-3 2	0	159	-436	-138	-193	-138	-155	-138	-138
			34	277	-267	11	-7	5	1	5	5
			69	1173	-531	452	321	373	321	321	321
82	Fondazio ne	31-3 3	0	990	-425	398	275	323	275	275	275
			33	210	-227	11	-38	-7	-17	-9	-9
			66	29	-276	-124	-167	-124	-139	-124	-124
83	Fondazio ne	31-3 3	0	108	-371	-132	-179	-132	-147	-132	-132
			33	160	-248	-1	-54	-20	-30	-20	-20
			66	908	-387	378	260	306	260	260	260
84	Fondazio ne	32-3 4	0	963	-346	432	309	360	309	309	309
			35	152	-173	-11	-20	-11	-15	-11	-11
			69	90	-430	-153	-207	-153	-171	-153	-153
85	Fondazio ne	32-3 4	0	149	-438	-144	-201	-144	-163	-144	-144
			35	203	-237	-13	-28	-14	-19	-14	-14
			69	1028	-439	420	295	346	295	295	295
86	Fondazio ne	33-3 5	0	869	-330	385	269	315	269	269	269

			33	136	-200	2	-41	-13	-22	-14	-14
			66	11	-266	-127	-172	-127	-143	-127	-127
87	Fondazio ne	33-3 5	0	77	-347	-135	-184	-135	-152	-135	-135
			33	122	-170	-14	-51	-24	-33	-24	-24
			66	904	-390	365	257	300	257	257	257
88	Fondazio ne	34-3 6	0	896	-341	391	278	323	278	278	278
			35	70	-125	-26	-41	-26	-33	-26	-26
			69	82	-385	-151	-209	-151	-170	-151	-151
89	Fondazio ne	34-3 6	0	76	-389	-157	-216	-157	-177	-157	-157
			35	78	-152	-30	-46	-30	-37	-30	-30
			69	919	-368	390	276	323	276	276	276
90	Fondazio ne	35-3 7	0	1022	-485	387	268	314	268	268	268
			33	181	-203	7	-41	-10	-20	-11	-11
			66	97	-340	-122	-166	-122	-136	-122	-122
91	Fondazio ne	35-3 7	0	70	-328	-129	-177	-129	-146	-129	-129
			33	207	-282	8	-47	-12	-23	-14	-14
			66	916	-376	392	270	318	270	270	270
92	Fondazio ne	36-3 8	0	879	-358	367	260	304	260	260	260
			35	134	-237	-39	-59	-39	-47	-39	-39
			69	133	-448	-157	-220	-157	-177	-157	-157
93	Fondazio ne	36-3 8	0	109	-449	-170	-237	-170	-193	-170	-170
			35	84	-164	-40	-61	-40	-49	-40	-40
			69	852	-309	383	272	319	272	272	272
94	Fondazio ne	37-3 9	0	983	-422	401	281	327	281	281	281
			33	198	-208	22	-20	6	-2	3	3
			66	117	-330	-106	-148	-106	-118	-106	-106
95	Fondazio ne	37-3 9	0	92	-314	-111	-152	-111	-125	-111	-111
			33	250	-219	33	-18	14	4	10	10
			66	983	-391	421	296	346	296	296	296
96	Fondazio ne	38-4 0	0	844	-372	331	236	275	236	236	236
			34	168	-284	-48	-74	-48	-59	-48	-48
			69	131	-436	-152	-214	-152	-172	-152	-152
97	Fondazio ne	38-4 0	0	113	-485	-183	-256	-183	-210	-183	-183
			34	75	-168	-47	-71	-47	-57	-47	-47
			69	823	-281	383	271	318	271	271	271
98	Fondazio ne	39-4 1	0	1207	-585	446	311	363	311	311	311
			33	287	-267	46	-30	16	1	10	10
			66	118	-373	-128	-176	-128	-143	-128	-128
99	Fondazio ne	39-4 1	0	66	-324	-119	-167	-119	-134	-119	-119
			33	84	-139	-28	-43	-28	-34	-28	-28
			66	659	-213	317	223	262	223	223	223
100	Fondazio ne	40-4 2	0	741	-302	308	219	256	219	219	219
			35	49	-160	-55	-79	-55	-67	-55	-55
			69	209	-523	-145	-191	-145	-161	-145	-145
101	Fondazio ne	40-4 2	0	51	-494	-200	-270	-200	-229	-200	-200
			35	608	-635	11	-40	-12	-22	-14	-14
			69	1843	-999	534	360	429	360	360	360
102	Fondazio ne	41-4 4	0	845	-362	350	241	282	241	241	241
			33	48	-207	-77	-106	-77	-91	-77	-77
			66	233	-712	-239	-324	-239	-271	-239	-239
103	Fondazio ne	41-4 4	0	3	-486	-229	-302	-229	-260	-229	-229
			33	208	-529	-143	-222	-152	-178	-152	-152
			66	769	-478	176	50	110	80	80	80
104	Fondazio ne	42-4 3	0	1382	-660	441	305	358	305	305	305
			23	1342	-893	296	192	229	192	192	192

			46	1530	-1140	278	164	206	164	164	164
105	Fondazio ne	43-4 4	0	3209	-4275	-232	-1122	-527	-705	-533	-533
			49	2411	-4055	-603	-1408	-822	-1003	-822	-822
			97	1973	-3517	-592	-1267	-772	-918	-772	-772
106	Fondazio ne	43-4 4	0	1575	-3099	-611	-1196	-762	-886	-762	-762
			49	1138	-2701	-689	-1158	-781	-897	-781	-781
			97	924	-2178	-542	-921	-627	-708	-627	-627
107	Fondazio ne	43-4 4	0	700	-1794	-485	-782	-547	-608	-547	-547
			49	458	-1476	-489	-703	-509	-565	-509	-509
			97	385	-1148	-354	-523	-381	-414	-381	-381
108	Fondazio ne	43-4 4	0	258	-853	-285	-395	-295	-318	-298	-298
			49	118	-644	-263	-337	-263	-287	-263	-263
			97	125	-460	-165	-209	-163	-173	-168	-168
109	Fondazio ne	43-4 4	0	86	-299	-96	-125	-99	-106	-106	-106
			49	134	-329	-96	-124	-97	-104	-97	-97
			97	194	-249	-6	-36	-14	-27	-27	-27
110	Fondazio ne	43-4 4	0	243	-228	39	-1	24	8	8	8
			49	223	-246	11	-35	-7	-17	-11	-11
			97	252	-169	78	36	58	42	42	42
111	Fondazio ne	43-4 4	0	252	-140	93	52	73	56	56	56
			49	189	-154	38	0	21	13	18	18
			97	212	-87	96	63	78	63	63	63
112	Fondazio ne	43-4 4	0	193	-62	98	66	81	66	66	66
			49	120	-83	31	6	18	14	18	18
			97	147	-23	89	62	75	62	62	62
113	Fondazio ne	43-4 4	0	126	-4	86	61	73	61	61	61
			49	56	-34	15	3	11	6	11	11
			97	102	23	77	56	66	56	56	56
114	Fondazio ne	43-4 4	0	103	40	76	56	67	56	56	56
			49	15	3	8	2	8	5	8	8
			97	104	43	77	57	68	57	57	57
115	Fondazio ne	43-4 4	0	102	26	76	56	67	56	56	56
			49	51	-32	13	2	10	5	10	10
			97	119	-1	83	59	71	59	59	59
116	Fondazio ne	43-4 4	0	138	-17	86	60	73	60	60	60
			49	109	-77	27	4	16	11	16	16
			97	180	-54	93	63	77	63	63	63
117	Fondazio ne	43-4 4	0	197	-76	92	61	75	61	61	61
			49	171	-141	33	-3	17	10	15	15
			97	231	-125	88	49	69	53	53	53
118	Fondazio ne	43-4 4	0	229	-148	75	36	57	41	41	41
			49	196	-221	7	-35	-9	-17	-12	-12
			97	216	-200	38	1	24	8	8	8
119	Fondazio ne	43-4 4	0	169	-212	0	-28	-8	-22	-22	-22
			49	109	-290	-89	-114	-91	-96	-91	-91
			97	76	-268	-84	-109	-89	-96	-96	-96
120	Fondazio ne	43-4 4	0	108	-405	-142	-182	-142	-151	-148	-148
			49	95	-579	-242	-308	-242	-262	-242	-242
			97	220	-766	-255	-359	-267	-288	-273	-273
121	Fondazio ne	43-4 4	0	329	-1016	-310	-467	-339	-369	-344	-344
			49	387	-1316	-435	-638	-465	-512	-465	-465
			97	601	-1594	-424	-706	-492	-548	-497	-497
122	Fondazio ne	43-4 4	0	777	-1876	-452	-808	-546	-617	-550	-550
			49	875	-2224	-577	-991	-675	-768	-675	-675
			97	1141	-2411	-488	-984	-631	-730	-635	-635

123	Fondazio ne	43-4 4	0	1380	-2622	-452	-1005	-619	-730	-621	-621
			49	1877	-3279	-485	-1190	-701	-849	-701	-701
			97	2682	-3623	-169	-985	-456	-619	-470	-470
124	Fondazio ne	43-4 5	0	1779	-1032	491	311	378	311	311	311
			33	329	-457	-53	-86	-61	-71	-61	-61
			66	421	-938	-249	-376	-259	-302	-259	-259
125	Fondazio ne	43-4 5	0	15	-326	-147	-195	-147	-166	-147	-147
			33	702	-764	-6	-65	-26	-39	-26	-26
			66	1897	-1282	393	267	313	267	267	267
126	Fondazio ne	44-4 6	0	603	-427	156	43	97	68	68	68
			33	98	-422	-147	-205	-147	-171	-147	-147
			66	93	-506	-207	-276	-207	-237	-207	-207
127	Fondazio ne	44-4 6	0	55	-583	-264	-362	-264	-302	-264	-264
			33	155	-232	-32	-68	-39	-51	-39	-39
			66	995	-305	496	345	402	345	345	345
128	Fondazio ne	45-4 7	0	2198	-1545	443	298	353	298	298	298
			33	876	-966	-8	-87	-35	-51	-35	-35
			66	193	-589	-198	-276	-198	-227	-198	-198
129	Fondazio ne	45-4 7	0	135	-439	-123	-168	-123	-139	-123	-123
			33	664	-677	17	-39	-4	-15	-7	-7
			66	2023	-1326	417	280	332	280	280	280
130	Fondazio ne	46-4 8	0	1156	-532	451	312	366	312	312	312
			33	251	-206	50	-2	28	17	22	22
			66	202	-412	-105	-146	-105	-119	-105	-105
131	Fondazio ne	46-4 8	0	30	-224	-93	-126	-93	-103	-93	-93
			33	247	-176	69	12	43	31	36	36
			66	896	-161	470	329	383	329	329	329
132	Fondazio ne	47-4 9	0	1780	-1106	430	296	349	296	296	296
			33	582	-579	22	-23	5	-4	2	2
			66	177	-425	-124	-173	-124	-139	-124	-124
133	Fondazio ne	47-4 9	0	51	-273	-99	-128	-99	-108	-99	-99
			33	556	-522	44	-9	22	11	16	16
			66	1624	-934	429	298	348	298	298	298
134	Fondazio ne	48-5 0	0	986	-234	502	353	412	353	353	353
			33	295	-143	85	39	62	53	53	53
			66	261	-422	-69	-119	-81	-92	-81	-81
135	Fondazio ne	48-5 0	0	25	-177	-73	-101	-76	-82	-76	-76
			33	260	-142	82	28	57	46	47	47
			66	847	-134	483	336	393	336	336	336
136	Fondazio ne	49-5 1	0	1905	-1137	495	341	401	341	341	341
			33	665	-603	64	3	37	25	27	27
			66	189	-435	-114	-168	-123	-135	-123	-123
137	Fondazio ne	49-5 1	0	49	-205	-75	-92	-76	-80	-78	-78
			33	876	-847	53	-14	23	9	12	12
			66	2091	-1450	399	261	315	261	261	261
138	Fondazio ne	50-5 2	0	1129	-360	551	385	450	385	385	385
			33	316	-197	105	22	66	50	51	51
			66	204	-441	-105	-160	-118	-129	-119	-119
139	Fondazio ne	50-5 2	0	109	-245	-52	-91	-63	-71	-68	-68
			33	151	-106	43	22	30	22	22	22
			66	646	10	382	271	325	271	271	271
140	Fondazio ne	51-5 3	0	2068	-1292	497	336	398	336	336	336
			33	903	-846	76	0	38	21	21	21
			66	199	-479	-113	-182	-132	-146	-140	-140
141	Fondazio	51-5	0	521	-637	2	-57	-27	-45	-45	-45

	ne	3									
			33	260	-175	69	30	49	30	30	30
			66	1239	-641	380	253	314	253	253	253
142	Fondazio ne	52-5 4	0	856	-119	510	356	423	356	356	356
			33	149	-98	49	21	34	21	21	21
			66	177	-497	-134	-206	-153	-167	-160	-160
143	Fondazio ne	52-5 4	0	67	-186	-25	-64	-46	-60	-60	-60
			33	202	-177	57	-6	21	1	1	1
			66	602	-106	335	209	263	209	209	209
144	Fondazio ne	53-5 5	0	1571	-655	566	391	471	391	391	391
			33	175	-127	71	11	36	11	11	11
			66	785	-1323	-159	-302	-210	-239	-228	-228
145	Fondazio ne	53-5 5	0	1003	-1114	66	-88	-13	-48	-48	-48
			33	1790	-1995	61	-176	-45	-92	-79	-79
			66	2680	-2619	225	-89	81	18	23	23
146	Fondazio ne	54-5 6	0	826	34	522	354	428	354	354	354
			33	233	-235	78	-41	15	-14	-14	-14
			66	190	-700	-163	-334	-224	-258	-243	-243
147	Fondazio ne	54-5 6	0	254	-374	60	-123	-30	-66	-66	-66
			33	387	-555	64	-171	-42	-89	-76	-76
			66	721	-631	238	-47	103	45	45	45
148	Fondazio ne	55-5 7	0	2923	-2443	453	128	280	206	206	206
			40	1871	-2304	-14	-296	-135	-191	-164	-164
			80	848	-1688	-264	-477	-338	-380	-354	-354
149	Fondazio ne	55-5 7	0	1665	-2226	-49	-316	-164	-218	-190	-190
			40	506	-1044	-165	-315	-220	-250	-225	-225
			80	949	-1121	-52	-122	-70	-86	-86	-86
150	Fondazio ne	56-7 0	0	822	-467	472	170	305	231	231	231
			40	275	-626	-10	-270	-123	-176	-152	-152
			80	0	-769	-271	-472	-340	-380	-355	-355
151	Fondazio ne	56-7 0	0	204	-624	-51	-296	-158	-207	-182	-182
			40	10	-486	-164	-307	-216	-245	-221	-221
			80	143	-334	-50	-121	-69	-85	-85	-85
152	Fondazio ne	57-5 8	0	1449	-1431	62	-89	-1	-31	-29	-29
			42	399	-935	-142	-389	-228	-278	-235	-235
			83	1318	-2021	-160	-464	-266	-327	-275	-275
153	Fondazio ne	57-5 8	0	505	-1475	-304	-600	-396	-456	-409	-409
			42	1104	-1870	-175	-525	-294	-364	-305	-305
			83	1531	-1782	112	-291	-42	-123	-77	-77
154	Fondazio ne	58-5 9	0	977	-1365	35	-366	-113	-193	-154	-154
			35	957	-1544	-111	-410	-214	-274	-231	-231
			69	933	-1507	-161	-368	-228	-269	-239	-239
155	Fondazio ne	58-5 9	0	637	-1337	-205	-414	-270	-312	-286	-286
			35	642	-1094	-139	-280	-182	-210	-186	-186
			69	626	-697	14	-70	-14	-31	-27	-27
156	Fondazio ne	59-6 0	0	460	-597	0	-110	-37	-59	-56	-56
			35	427	-714	-108	-163	-120	-132	-120	-120
			69	410	-675	-128	-153	-128	-133	-128	-128
157	Fondazio ne	59-6 0	0	286	-590	-94	-190	-134	-153	-147	-147
			35	254	-407	-72	-92	-73	-78	-73	-73
			69	278	-232	104	-7	75	52	57	57
158	Fondazio ne	60-6 1	0	193	-86	84	43	68	53	53	53
			35	219	-273	3	-65	-22	-35	-27	-27
			69	283	-383	1	-97	-37	-56	-50	-50
159	Fondazio ne	60-6 1	0	236	-325	5	-89	-31	-50	-45	-45

			35	402	-386	81	-66	22	-7	8	8
			69	671	-431	239	37	154	113	120	120
160	Fondazio ne	61-6 2	0	710	-460	253	37	161	118	125	125
			35	303	-262	72	-30	31	10	21	21
			69	104	-150	-14	-25	-19	-23	-23	-23
161	Fondazio ne	61-6 2	0	93	-121	16	-24	-5	-14	-14	-14
			35	257	-226	59	-30	23	5	15	15
			69	648	-436	228	16	139	97	106	106
162	Fondazio ne	62-6 3	0	648	-414	237	33	150	109	117	117
			35	359	-347	71	-63	17	-10	6	6
			69	153	-247	-7	-79	-35	-50	-44	-44
163	Fondazio ne	62-6 3	0	196	-262	12	-74	-23	-40	-33	-33
			35	127	-159	6	-49	-15	-26	-16	-16
			69	158	-35	100	13	75	58	61	61
164	Fondazio ne	63-6 4	0	270	-126	113	24	83	65	68	68
			35	48	-96	-17	-43	-24	-31	-24	-24
			69	22	-137	-40	-65	-52	-57	-55	-55
165	Fondazio ne	63-6 4	0	-2	-108	-41	-65	-52	-57	-55	-55
			35	49	-97	-18	-43	-24	-32	-24	-24
			69	276	-126	112	25	82	65	67	67
166	Fondazio ne	64-6 5	0	246	-71	100	12	75	57	61	61
			35	130	-163	6	-50	-16	-27	-17	-17
			69	193	-261	11	-75	-24	-41	-34	-34
167	Fondazio ne	64-6 5	0	144	-234	-9	-81	-37	-51	-45	-45
			35	355	-345	70	-65	16	-11	5	5
			69	656	-425	235	31	148	108	115	115
168	Fondazio ne	65-6 6	0	664	-456	226	14	137	95	104	104
			35	248	-220	58	-32	21	4	14	14
			69	88	-131	15	-25	-6	-15	-15	-15
169	Fondazio ne	65-6 6	0	45	-94	-16	-28	-20	-25	-25	-25
			35	306	-265	71	-31	30	10	20	20
			69	676	-425	253	37	162	119	126	126
170	Fondazio ne	66-6 7	0	646	-405	239	38	154	114	121	121
			35	416	-402	79	-67	21	-8	7	7
			69	240	-335	2	-91	-34	-53	-47	-47
171	Fondazio ne	66-6 7	0	249	-343	2	-93	-34	-53	-47	-47
			35	193	-248	1	-64	-23	-36	-27	-27
			69	185	-87	80	39	65	49	49	49
172	Fondazio ne	67-6 8	0	251	-143	95	1	70	51	54	54
			35	75	-217	-69	-90	-71	-76	-71	-71
			69	36	-315	-98	-173	-129	-144	-140	-140
173	Fondazio ne	67-6 8	0	39	-292	-127	-146	-127	-131	-127	-127
			35	106	-344	-106	-160	-119	-130	-119	-119
			69	239	-347	2	-106	-35	-57	-54	-54
174	Fondazio ne	68-6 9	0	231	-295	11	-74	-18	-35	-32	-32
			35	185	-559	-139	-281	-182	-210	-187	-187
			69	225	-790	-201	-410	-267	-308	-283	-283
175	Fondazio ne	68-6 9	0	244	-720	-158	-366	-226	-268	-238	-238
			35	452	-912	-110	-408	-213	-273	-230	-230
			69	822	-1128	36	-363	-112	-192	-153	-153
176	Fondazio ne	69-7 0	0	847	-1012	107	-295	-47	-128	-83	-83
			42	464	-1081	-177	-528	-297	-367	-308	-308
			83	248	-1068	-303	-601	-397	-456	-410	-410
177	Fondazio ne	69-7 0	0	401	-972	-166	-478	-275	-338	-285	-285
			42	324	-800	-144	-393	-231	-281	-238	-238

			83	508	-535	65	-83	4	-26	-25	-25
178	Primo Impalcato	1-2	0	1159	-1100	153	-65	56	12	29	29
			83	654	-429	198	37	130	98	112	112
			166	201	-378	-62	-165	-101	-122	-109	-109
179	Primo Impalcato	1-15	0	7057	-7212	180	-345	-25	-130	-67	-67
			80	2716	-2565	185	-28	98	56	78	78
			159	1830	-1931	10	-89	-38	-58	-56	-56
180	Primo Impalcato	2-3	0	246	-414	-43	-169	-92	-117	-102	-102
			69	160	-140	20	-21	6	-2	3	3
			138	21	-225	-83	-127	-98	-107	-102	-102
181	Primo Impalcato	3-4	0	-11	-191	-95	-110	-98	-101	-99	-99
			69	79	-44	22	10	19	16	18	18
			138	-43	-112	-72	-80	-75	-76	-76	-76
182	Primo Impalcato	4-5	0	-14	-131	-65	-86	-73	-77	-75	-75
			69	104	-35	49	20	38	32	35	35
			138	18	-150	-48	-84	-62	-69	-66	-66
183	Primo Impalcato	5-6	0	83	-214	-32	-99	-59	-72	-66	-66
			69	175	-107	66	1	41	28	34	34
			138	348	-501	22	-176	-57	-96	-77	-77
184	Primo Impalcato	6-7	0	295	-447	10	-163	-59	-94	-76	-76
			69	44	21	30	27	30	29	30	30
			138	293	-443	11	-161	-58	-92	-75	-75
185	Primo Impalcato	7-8	0	346	-496	24	-174	-55	-95	-75	-75
			69	230	-156	81	-9	45	27	37	37
			138	-20	-103	-54	-71	-61	-64	-62	-62
186	Primo Impalcato	8-9	0	-19	-104	-54	-71	-61	-64	-62	-62
			69	229	-155	81	-9	45	27	37	37
			138	345	-496	24	-174	-55	-95	-75	-75
187	Primo Impalcato	9-10	0	292	-442	11	-161	-58	-92	-75	-75
			69	44	17	30	28	30	29	30	30
			138	287	-440	9	-162	-59	-93	-76	-76
188	Primo Impalcato	10-11	0	341	-493	21	-175	-57	-96	-76	-76
			69	169	-105	63	0	39	26	32	32
			138	83	-222	-35	-105	-62	-76	-70	-70
189	Primo Impalcato	11-12	0	22	-162	-51	-90	-66	-74	-70	-70
			69	67	-27	24	11	21	18	20	20
			138	-39	-162	-98	-111	-100	-102	-100	-100
190	Primo Impalcato	12-13	0	18	-223	-86	-128	-99	-108	-103	-103
			69	90	-82	21	-20	6	-2	4	4
			138	165	-365	-41	-165	-89	-114	-100	-100
191	Primo Impalcato	13-14	0	107	-320	-61	-160	-99	-118	-107	-107
			83	485	-274	191	28	123	90	106	106
			166	571	-544	139	-89	39	-7	13	13
192	Primo Impalcato	14-16	0	855	-950	47	-226	-54	-109	-71	-71

			80	441	-245	137	12	86	61	75	75
			159	213	-330	-27	-63	-47	-58	-58	-58
193	Primo Impalcato	15-17	0	1623	-1757	9	-137	-55	-84	-72	-72
			66	472	-380	63	41	49	42	42	42
			132	2480	-2535	70	-119	-11	-48	-37	-37
194	Primo Impalcato	16-18	0	231	-325	-13	-127	-63	-86	-76	-76
			66	124	-41	57	41	47	41	41	41
			132	330	-430	47	-88	-12	-39	-34	-34
195	Primo Impalcato	17-19	0	913	-1013	-15	-68	-39	-50	-50	-50
			66	202	-100	63	48	54	48	48	48
			132	683	-767	-27	-51	-40	-47	-47	-47
196	Primo Impalcato	18-20	0	117	-203	-22	-52	-39	-48	-48	-48
			66	121	-5	65	46	54	47	47	47
			132	90	-191	-40	-51	-47	-51	-51	-51
197	Primo Impalcato	19-21	0	2776	-2881	65	-159	-28	-72	-53	-53
			66	107	-11	52	45	48	45	45	45
			132	2699	-2789	61	-154	-26	-69	-50	-50
198	Primo Impalcato	20-22	0	398	-471	17	-132	-44	-74	-60	-60
			66	73	17	48	43	46	43	43	43
			132	343	-484	32	-115	-29	-58	-46	-46
199	Primo Impalcato	21-23	0	755	-856	-31	-64	-45	-52	-50	-50
			66	96	0	51	45	48	45	45	45
			132	713	-813	-32	-62	-47	-53	-52	-52
200	Primo Impalcato	22-24	0	75	-159	-37	-46	-42	-46	-46	-46
			66	76	11	50	43	46	43	43	43
			132	66	-185	-54	-59	-58	-59	-59	-59
201	Primo Impalcato	23-25	0	2763	-2858	68	-151	-22	-66	-47	-47
			66	54	-15	20	19	19	19	19	19
			132	2746	-2958	-2	-223	-87	-131	-106	-106
202	Primo Impalcato	24-26	0	398	-466	13	-134	-46	-76	-62	-62
			66	51	3	27	26	27	27	27	27
			132	336	-528	-6	-152	-63	-92	-76	-76
203	Primo Impalcato	25-28	0	609	-826	-96	-124	-105	-111	-106	-106
			85	176	-83	50	40	49	46	49	49
			170	803	-1034	-96	-143	-113	-122	-115	-115
204	Primo Impalcato	26-27	0	59	-213	-77	-81	-77	-79	-77	-77
			66	61	-8	27	25	26	26	26	26
			132	74	-198	-59	-62	-61	-62	-62	-62
205	Primo Impalcato	27-29	0	364	-478	-9	-155	-66	-95	-79	-79
			66	53	9	31	30	31	31	31	31
			132	352	-508	24	-123	-35	-65	-51	-51
206	Primo Impalcato	28-30	0	2477	-2687	-6	-204	-85	-125	-105	-105
			73	328	-259	47	22	37	32	34	34
			146	1964	-2088	12	-136	-47	-77	-62	-62
207	Primo Impalcato	29-31	0	59	-179	-59	-61	-60	-60	-60	-60

	o										
			66	90	-12	42	39	40	39	39	39
			132	96	-199	-49	-54	-52	-54	-54	-54
208	Primo Impalcato	30-32	0	1526	-1622	11	-95	-34	-55	-48	-48
			69	172	-85	48	39	44	42	42	42
			137	1686	-1838	-16	-141	-64	-90	-76	-76
209	Primo Impalcato	31-33	0	390	-484	-3	-150	-60	-90	-73	-73
			66	63	2	32	32	32	32	32	32
			132	349	-508	21	-127	-39	-68	-55	-55
210	Primo Impalcato	32-34	0	1730	-1844	10	-117	-42	-68	-57	-57
			69	81	-7	38	37	37	37	37	37
			138	1689	-1847	-19	-145	-68	-93	-79	-79
211	Primo Impalcato	33-35	0	59	-198	-70	-74	-70	-71	-70	-70
			66	85	-13	37	36	37	36	36	36
			132	98	-191	-44	-50	-48	-50	-50	-50
212	Primo Impalcato	34-36	0	1724	-1838	9	-116	-43	-68	-57	-57
			69	69	3	36	36	36	36	36	36
			138	1691	-1854	-22	-148	-71	-96	-81	-81
213	Primo Impalcato	35-37	0	391	-482	0	-147	-57	-87	-71	-71
			66	71	-3	34	33	34	34	34	34
			132	351	-506	21	-123	-38	-67	-54	-54
214	Primo Impalcato	36-38	0	1724	-1838	10	-116	-42	-68	-57	-57
			69	66	3	35	34	35	34	35	35
			138	1702	-1870	-25	-152	-74	-99	-84	-84
215	Primo Impalcato	37-39	0	59	-206	-70	-75	-71	-72	-71	-71
			66	81	-25	31	23	28	27	28	28
			132	67	-207	-60	-71	-64	-66	-66	-66
216	Primo Impalcato	38-40	0	1712	-1828	8	-117	-44	-69	-58	-58
			69	127	-59	37	30	34	33	34	34
			137	1522	-1684	-29	-142	-72	-95	-81	-81
217	Primo Impalcato	39-41	0	329	-460	-18	-147	-67	-93	-78	-78
			66	139	-57	55	27	43	38	40	40
			132	204	-276	9	-64	-24	-38	-35	-35
218	Primo Impalcato	40-42	0	1920	-2027	20	-120	-37	-66	-53	-53
			69	196	-83	62	54	57	55	55	55
			138	2163	-2252	35	-123	-30	-61	-47	-47
219	Primo Impalcato	41-44	0	206	-297	-4	-84	-38	-54	-47	-47
			66	134	-83	41	11	29	23	27	27
			132	304	-520	-27	-165	-81	-109	-92	-92
220	Primo Impalcato	42-43	0	1328	-1352	48	-46	4	-15	-12	-12
			23	413	-470	-7	-45	-25	-33	-31	-31
			46	2090	-2239	8	-161	-59	-93	-75	-75
221	Primo Impalcato	43-45	0	1277	-1423	-35	-112	-65	-81	-72	-72
			66	260	-198	39	22	32	29	31	31
			132	868	-982	-36	-80	-53	-62	-58	-58
222	Primo	44-4	0	40	-224	-92	-101	-92	-96	-92	-92

	Impalcat o	6									
			66	70	-27	24	15	21	19	21	21
			132	62	-171	-50	-63	-56	-58	-57	-57
223	Primo Impalcat o	45-4 7	0	2598	-2710	48	-159	-35	-76	-56	-56
			66	118	-47	39	33	36	35	35	35
			132	2730	-2862	44	-174	-44	-87	-66	-66
224	Primo Impalcat o	46-4 8	0	406	-530	1	-156	-60	-91	-74	-74
			66	73	-2	38	36	36	36	36	36
			132	422	-541	40	-122	-28	-61	-48	-48
225	Primo Impalcat o	47-4 9	0	706	-832	-45	-76	-59	-65	-63	-63
			66	72	12	45	41	43	41	41	41
			132	737	-821	-28	-59	-42	-48	-47	-47
226	Primo Impalcat o	48-5 0	0	75	-164	-37	-50	-45	-49	-49	-49
			66	87	-1	46	39	42	40	40	40
			132	40	-167	-62	-64	-63	-64	-64	-64
227	Primo Impalcat o	49-5 1	0	2737	-2818	74	-144	-15	-59	-40	-40
			66	104	-14	48	42	45	42	42	42
			132	2794	-2929	47	-178	-44	-89	-67	-67
228	Primo Impalcat o	50-5 2	0	357	-458	9	-128	-46	-73	-60	-60
			66	107	-7	60	45	52	47	47	47
			132	269	-349	25	-82	-22	-44	-38	-38
229	Primo Impalcat o	51-5 3	0	634	-745	-40	-62	-52	-56	-56	-56
			66	211	-114	59	44	50	44	44	44
			132	912	-993	-13	-64	-37	-48	-48	-48
230	Primo Impalcat o	52-5 4	0	171	-220	4	-45	-20	-31	-31	-31
			66	111	14	68	55	61	55	55	55
			132	145	-251	-14	-77	-42	-55	-53	-53
231	Primo Impalcat o	53-5 5	0	2507	-2570	79	-112	-3	-41	-31	-31
			66	467	-384	62	41	49	41	41	41
			132	1641	-1799	1	-147	-62	-92	-79	-79
232	Primo Impalcat o	54-5 6	0	243	-280	23	-55	-14	-31	-31	-31
			66	122	-34	67	34	47	39	39	39
			132	226	-409	-4	-147	-67	-96	-83	-83
233	Primo Impalcat o	55-5 7	0	1782	-1900	5	-92	-42	-62	-59	-59
			80	2724	-2576	180	-34	93	51	74	74
			159	7042	-7186	173	-352	-31	-136	-72	-72
234	Primo Impalcat o	56-7 0	0	179	-297	-35	-73	-57	-67	-67	-67
			80	323	-211	111	23	77	59	70	70
			159	635	-865	15	-198	-61	-104	-72	-72
235	Primo Impalcat o	57-5 8	0	1214	-1118	158	-65	58	13	30	30
			83	699	-441	199	38	130	98	113	113
			166	170	-389	-64	-164	-102	-122	-109	-109
236	Primo Impalcat o	58-5 9	0	231	-436	-45	-169	-93	-117	-103	-103
			69	148	-150	19	-22	5	-3	2	2
			138	34	-240	-86	-128	-100	-108	-103	-103

237	Primo Impalcato	59-60	0	-7	-201	-98	-111	-100	-103	-100	-100
			69	89	-53	25	11	21	18	20	20
			138	37	-177	-51	-89	-66	-73	-70	-70
238	Primo Impalcato	60-61	0	102	-240	-34	-104	-62	-76	-69	-69
			69	178	-114	63	1	39	26	32	32
			138	369	-522	20	-174	-57	-96	-77	-77
239	Primo Impalcato	61-62	0	312	-464	8	-161	-59	-93	-76	-76
			69	47	13	31	28	30	30	30	30
			138	319	-466	12	-159	-57	-91	-74	-74
240	Primo Impalcato	62-63	0	377	-524	24	-171	-54	-93	-74	-74
			69	187	-118	67	2	41	28	35	35
			138	80	-214	-36	-100	-61	-74	-67	-67
241	Primo Impalcato	63-64	0	10	-145	-52	-84	-64	-71	-67	-67
			69	56	27	39	34	38	37	38	38
			138	12	-147	-52	-84	-64	-71	-67	-67
242	Primo Impalcato	64-65	0	85	-220	-36	-100	-61	-74	-67	-67
			69	186	-117	67	1	41	28	34	34
			138	377	-526	24	-172	-55	-94	-74	-74
243	Primo Impalcato	65-66	0	319	-467	11	-159	-57	-91	-74	-74
			69	45	18	31	28	30	30	30	30
			138	321	-473	8	-161	-59	-93	-76	-76
244	Primo Impalcato	66-67	0	380	-532	21	-174	-57	-96	-76	-76
			69	184	-120	63	1	39	26	32	32
			138	95	-233	-35	-105	-62	-76	-69	-69
245	Primo Impalcato	67-68	0	27	-167	-51	-90	-66	-74	-70	-70
			69	70	-30	25	11	21	18	20	20
			138	-43	-158	-98	-111	-100	-102	-100	-100
246	Primo Impalcato	68-69	0	20	-226	-86	-128	-99	-108	-103	-103
			69	104	-97	20	-20	6	-2	3	3
			138	209	-409	-42	-165	-90	-115	-100	-100
247	Primo Impalcato	69-70	0	143	-357	-62	-160	-99	-119	-107	-107
			83	502	-289	192	29	123	91	107	107
			166	561	-530	141	-87	41	-4	16	16
248	Primo Impalcato	1-1	0	359	-243	80	11	40	26	27	27
			188	262	-243	10	-2	9	6	8	8
			376	326	-313	36	-50	-4	-21	-10	-10
249	Primo Impalcato	2-2	0	1923	-2164	-93	-179	-93	-119	-93	-93
			188	1491	-1419	144	-73	39	-4	14	14
			376	2195	-1217	698	-137	244	77	120	120
250	Primo Impalcato	3-3	0	1028	-1095	24	-194	-23	-66	-29	-29
			188	1691	-1431	272	-136	64	-18	13	13
			376	3532	-2283	965	-410	239	-35	55	55
251	Primo Impalcato	4-4	0	786	-764	54	-125	11	-25	2	2
			188	1832	-1397	388	-197	85	-32	10	10

			376	3761	-2286	1127	-561	239	-99	18	18
252	Primo Impalcato	5-5	0	1014	-985	29	-50	12	-3	9	9
			188	1933	-1345	485	-246	102	-44	8	8
			376	4005	-2332	1246	-635	254	-123	7	7
253	Primo Impalcato	6-6	0	766	-752	15	-1	8	5	7	7
			188	1950	-1242	555	-280	116	-51	7	7
			376	3686	-1859	1330	-673	271	-130	7	7
254	Primo Impalcato	7-7	0	849	-835	27	-14	9	1	5	5
			188	1901	-1116	590	-297	123	-55	7	7
			376	3746	-1806	1379	-693	281	-133	8	8
255	Primo Impalcato	8-8	0	830	-818	26	-12	9	2	6	6
			188	1763	-983	588	-295	122	-55	6	6
			376	3645	-1681	1377	-691	280	-133	7	7
256	Primo Impalcato	9-9	0	605	-586	17	-2	9	5	7	7
			188	1552	-835	547	-273	114	-50	7	7
			376	3104	-1303	1323	-665	269	-129	7	7
257	Primo Impalcato	10-10	0	731	-722	31	-49	13	-3	8	8
			188	1305	-686	475	-236	101	-42	8	8
			376	2836	-1269	1224	-616	250	-118	8	8
258	Primo Impalcato	11-11	0	445	-427	58	-129	12	-26	2	2
			188	1001	-536	373	-183	82	-30	10	10
			376	2354	-924	1101	-537	234	-94	18	18
259	Primo Impalcato	12-12	0	455	-532	34	-206	-21	-69	-30	-30
			188	688	-407	254	-118	60	-14	13	13
			376	1995	-824	939	-383	235	-29	56	56
260	Primo Impalcato	13-13	0	374	-576	-91	-213	-94	-127	-94	-94
			188	379	-281	122	-51	35	0	14	14
			376	1359	-534	690	-128	243	79	121	121
261	Primo Impalcato	14-14	0	133	-50	71	27	41	30	30	30
			188	38	-27	14	-6	9	5	8	8
			376	184	-134	35	-59	-7	-26	-13	-13
262	Primo Impalcato	15-15	0	406	-387	28	-6	13	6	7	7
			188	9	-7	1	1	1	1	1	1
			376	373	-390	7	-25	-5	-11	-6	-6
263	Primo Impalcato	16-16	0	89	-76	27	-1	14	8	9	9
			188	3	-1	1	1	1	1	1	1
			376	76	-86	3	-25	-7	-13	-8	-8
264	Primo Impalcato	17-17	0	356	-340	24	-9	10	4	6	6
			188	14	-14	1	0	0	0	0	0
			376	368	-382	11	-24	-3	-10	-5	-5
265	Primo Impalcato	18-18	0	82	-85	24	-4	12	6	8	8
			188	3	-2	1	0	0	0	0	0
			376	81	-85	6	-24	-6	-12	-7	-7
266	Primo Impalcato	19-19	0	375	-368	20	-15	6	-1	2	2

			188	12	-12	1	0	0	0	0	0
			376	390	-396	16	-20	1	-6	-2	-2
267	Primo Impalcat o	20-2 0	0	86	-99	21	-10	8	2	5	5
			188	2	-2	0	0	0	0	0	0
			376	102	-88	11	-21	-2	-8	-4	-4
268	Primo Impalcat o	21-2 1	0	379	-379	16	-19	3	-4	0	0
			188	11	-11	1	0	0	0	0	0
			376	401	-399	20	-16	5	-2	1	1
269	Primo Impalcat o	22-2 2	0	86	-105	18	-13	5	-1	2	2
			188	2	-2	1	0	0	0	0	0
			376	108	-87	14	-17	1	-5	-2	-2
270	Primo Impalcat o	23-2 3	0	382	-389	12	-22	-1	-8	-4	-4
			188	11	-10	1	0	0	0	0	0
			376	409	-401	24	-12	9	2	4	4
271	Primo Impalcat o	24-2 4	0	86	-111	14	-17	2	-4	-1	-1
			188	2	-1	0	0	0	0	0	0
			376	113	-87	17	-14	4	-2	1	1
272	Primo Impalcat o	25-2 5	0	381	-384	14	-20	1	-5	-1	-1
			188	11	-10	1	0	1	1	1	1
			376	403	-398	22	-14	7	0	3	3
273	Primo Impalcat o	26-2 6	0	87	-108	16	-15	4	-2	1	1
			188	2	-2	0	0	0	0	0	0
			376	111	-89	15	-17	2	-4	-1	-1
274	Primo Impalcat o	27-2 7	0	89	-106	18	-12	6	0	3	3
			188	1	-2	0	-1	0	0	0	0
			376	108	-91	12	-19	0	-7	-3	-3
275	Primo Impalcat o	28-2 8	0	366	-363	17	-15	5	-2	1	1
			188	14	-15	0	-1	0	0	0	0
			376	390	-394	16	-19	2	-5	-2	-2
276	Primo Impalcat o	29-2 9	0	91	-108	18	-13	6	0	2	2
			188	1	-2	0	0	0	0	0	0
			376	110	-92	13	-19	0	-6	-3	-3
277	Primo Impalcat o	30-3 0	0	428	-424	21	-17	5	-2	2	2
			188	9	-8	0	0	0	0	0	0
			376	439	-443	18	-21	2	-5	-1	-1
278	Primo Impalcat o	31-3 1	0	91	-97	16	-14	4	-2	1	1
			188	2	-2	0	0	0	0	0	0
			376	99	-93	14	-17	2	-4	-1	-1
279	Primo Impalcat o	32-3 2	0	413	-413	18	-19	4	-4	0	0
			188	12	-12	1	0	0	0	0	0
			376	435	-435	20	-19	4	-4	0	0
280	Primo Impalcat o	33-3 3	0	93	-100	16	-14	4	-2	1	1
			188	2	-2	0	0	0	0	0	0
			376	102	-94	15	-17	2	-4	-1	-1
281	Primo Impalcat o	34-3 4	0	414	-415	18	-19	3	-4	-1	-1

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			188	11	-11	1	0	0	0	0	0
			376	436	-435	20	-18	5	-3	1	1
282	Primo Impalcato	35-35	0	93	-103	15	-15	3	-3	0	0
			188	2	-2	0	0	0	0	0	0
			376	104	-94	15	-16	3	-3	0	0
283	Primo Impalcato	36-36	0	416	-417	18	-19	3	-4	-1	-1
			188	11	-11	1	0	0	0	0	0
			376	438	-436	20	-18	5	-3	1	1
284	Primo Impalcato	37-37	0	94	-105	15	-16	3	-4	0	0
			188	2	-2	0	0	0	0	0	0
			376	106	-94	16	-16	3	-3	0	0
285	Primo Impalcato	38-38	0	417	-418	18	-19	3	-4	0	0
			188	11	-11	0	0	0	0	0	0
			376	440	-439	20	-19	4	-3	0	0
286	Primo Impalcato	39-39	0	91	-101	15	-15	3	-3	-1	-1
			188	3	-2	1	0	0	0	0	0
			376	105	-93	17	-15	4	-2	1	1
287	Primo Impalcato	40-40	0	429	-429	20	-18	4	-4	0	0
			188	9	-9	0	0	0	0	0	0
			376	445	-446	19	-20	4	-4	0	0
288	Primo Impalcato	41-41	0	105	-116	16	-19	2	-5	-2	-2
			188	2	-1	0	0	0	0	0	0
			376	116	-103	20	-15	6	-1	2	2
289	Primo Impalcato	42-42	0	400	-406	16	-21	1	-6	-3	-3
			188	10	-12	-1	-1	-1	-1	-1	-1
			376	425	-423	19	-18	5	-3	1	1
290	Primo Impalcato	43-43	0	374	-378	15	-19	1	-5	-2	-2
			188	14	-14	1	0	0	0	0	0
			376	405	-401	20	-15	6	-1	2	2
291	Primo Impalcato	44-44	0	92	-98	16	-15	3	-3	0	0
			188	2	-2	0	-1	0	0	0	0
			376	102	-96	15	-17	2	-4	-1	-1
292	Primo Impalcato	45-45	0	404	-407	16	-20	2	-5	-2	-2
			188	8	-7	0	0	0	0	0	0
			376	422	-418	20	-17	5	-2	2	2
293	Primo Impalcato	46-46	0	99	-99	20	-13	6	0	2	2
			188	1	-2	0	-1	0	0	0	0
			376	101	-100	12	-21	0	-7	-3	-3
294	Primo Impalcato	47-47	0	392	-396	16	-20	1	-6	-2	-2
			188	11	-11	0	0	0	0	0	0
			376	417	-413	20	-16	6	-2	2	2
295	Primo Impalcato	48-48	0	98	-100	18	-14	5	-2	1	1
			188	1	-1	0	0	0	0	0	0
			376	102	-99	15	-19	2	-5	-1	-1
296	Primo	49-4	0	387	-395	13	-22	-1	-8	-4	-4

	Impalcat o	9									
			188	11	-11	0	-1	0	0	0	0
			376	416	-408	23	-15	8	0	4	4
297	Primo Impalcat o	50-5 0	0	93	-100	15	-17	2	-5	-1	-1
			188	2	-2	1	0	0	0	0	0
			376	104	-96	18	-15	5	-2	2	2
298	Primo Impalcat o	51-5 1	0	377	-389	11	-25	-3	-10	-6	-6
			188	12	-12	0	-1	0	0	0	0
			376	410	-399	25	-12	10	2	6	6
299	Primo Impalcat o	52-5 2	0	101	-114	13	-23	-1	-9	-5	-5
			188	2	-1	0	0	0	0	0	0
			376	117	-102	23	-13	9	2	5	5
300	Primo Impalcat o	53-5 3	0	350	-366	6	-27	-7	-13	-8	-8
			188	14	-15	0	-1	0	0	0	0
			376	393	-378	28	-8	13	6	8	8
301	Primo Impalcat o	54-5 4	0	93	-117	7	-28	-6	-13	-8	-8
			188	1	-2	0	-1	0	-1	0	0
			376	118	-96	27	-9	12	5	7	7
302	Primo Impalcat o	55-5 5	0	396	-415	4	-31	-8	-15	-9	-9
			188	7	-9	-1	-1	-1	-1	-1	-1
			376	398	-382	29	-5	14	7	8	8
303	Primo Impalcat o	56-5 6	0	82	-109	1	-27	-9	-14	-9	-9
			188	1	-3	-1	-1	-1	-1	-1	-1
			376	107	-84	25	-4	12	6	7	7
304	Primo Impalcat o	57-5 7	0	221	-289	-17	-84	-30	-44	-30	-30
			188	259	-262	2	-10	-6	-9	-8	-8
			376	358	-303	57	-31	26	8	14	14
305	Primo Impalcat o	58-5 8	0	2127	-1907	179	93	119	93	93	93
			188	1405	-1432	74	-142	5	-38	-13	-13
			376	1209	-1452	140	-695	-74	-241	-118	-118
306	Primo Impalcat o	59-5 9	0	1039	-861	194	-23	66	23	30	30
			188	1439	-1464	137	-271	19	-63	-12	-12
			376	2465	-2337	411	-962	37	-238	-54	-54
307	Primo Impalcat o	60-6 0	0	876	-702	123	-52	24	-10	-1	-1
			188	1469	-1421	198	-387	33	-84	-9	-9
			376	2712	-2306	560	-1122	99	-237	-17	-17
308	Primo Impalcat o	61-6 1	0	951	-902	44	-25	3	-11	-8	-8
			188	1507	-1370	247	-485	44	-102	-7	-7
			376	2749	-2261	632	-1239	122	-252	-7	-7
309	Primo Impalcat o	62-6 2	0	861	-875	3	-16	-4	-8	-7	-7
			188	1496	-1264	280	-553	52	-115	-6	-6
			376	2643	-1928	675	-1332	131	-270	-6	-6
310	Primo Impalcat o	63-6 3	0	837	-847	13	-24	-1	-8	-5	-5
			188	1440	-1127	298	-590	56	-122	-6	-6
			376	2700	-1805	697	-1382	135	-281	-6	-6

311	Primo Impalcato	64-64	0	803	-811	12	-23	-1	-8	-5	-5
			188	1350	-987	296	-588	55	-122	-6	-6
			376	2575	-1641	694	-1380	135	-280	-6	-6
312	Primo Impalcato	65-65	0	637	-643	3	-15	-4	-8	-7	-7
			188	1207	-843	275	-547	51	-114	-6	-6
			376	2257	-1320	667	-1324	130	-268	-6	-6
313	Primo Impalcato	66-66	0	592	-599	49	-30	4	-12	-8	-8
			188	1035	-692	237	-474	42	-100	-7	-7
			376	2092	-1174	617	-1223	119	-249	-7	-7
314	Primo Impalcato	67-67	0	569	-427	129	-57	26	-11	-1	-1
			188	810	-540	184	-372	30	-81	-9	-9
			376	1692	-894	538	-1100	95	-233	-17	-17
315	Primo Impalcato	68-68	0	533	-355	207	-32	70	23	32	32
			188	592	-420	119	-253	15	-60	-12	-12
			376	1378	-828	383	-939	29	-235	-56	-56
316	Primo Impalcato	69-69	0	692	-379	218	96	131	98	98	98
			188	352	-281	52	-121	0	-34	-13	-13
			376	872	-736	124	-693	-82	-246	-124	-124
317	Primo Impalcato	70-70	0	89	-160	-28	-61	-28	-38	-28	-28
			188	28	-35	8	-15	-5	-10	-8	-8
			376	214	-145	61	-43	25	4	11	11
318	Primo Impalcato	1-71	0	0	0	0	0	0	0	0	0
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
319	Primo Impalcato	1-92	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
320	Primo Impalcato	92-2	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
321	Primo Impalcato	6-89	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
322	Primo Impalcato	89-7	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
323	Primo Impalcato	9-90	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
324	Primo Impalcato	90-10	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
325	Primo Impalcato	13-91	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1

			206	0	0	0	0	0	0	0	0
326	Primo Impalcato	88-14	0	0	0	0	0	0	0	0	0
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
327	Primo Impalcato	91-14	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
328	Primo Impalcato	71-15	0	0	0	0	0	0	0	0	0
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
329	Primo Impalcato	16-88	0	0	0	0	0	0	0	0	0
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
330	Primo Impalcato	17-72	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
331	Primo Impalcato	87-18	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
332	Primo Impalcato	72-19	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
333	Primo Impalcato	20-87	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
334	Primo Impalcato	21-73	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
335	Primo Impalcato	86-22	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
336	Primo Impalcato	73-23	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
337	Primo Impalcato	24-86	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
338	Primo Impalcato	25-74	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
339	Primo Impalcato	85-26	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
340	Primo Impalcato	27-85	0	0	0	0	0	0	0	0	0

			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
341	Primo Impalcato	74-28	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
342	Primo Impalcato	84-29	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
343	Primo Impalcato	31-84	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
344	Primo Impalcato	83-33	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
345	Primo Impalcato	35-83	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
346	Primo Impalcato	82-37	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
347	Primo Impalcato	39-82	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
348	Primo Impalcato	78-43	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
349	Primo Impalcato	81-44	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
350	Primo Impalcato	45-78	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
351	Primo Impalcato	46-81	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
352	Primo Impalcato	77-47	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
353	Primo Impalcato	80-48	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
354	Primo Impalcato	49-77	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
355	Primo Impalcato	50-80	0	0	0	0	0	0	0	0	0

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			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
356	Primo Impalcato	76-51	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
357	Primo Impalcato	53-76	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
358	Primo Impalcato	75-55	0	0	0	0	0	0	0	0	0
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
359	Primo Impalcato	56-79	0	0	0	0	0	0	0	0	0
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
360	Primo Impalcato	57-75	0	0	0	0	0	0	0	0	0
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
361	Primo Impalcato	57-93	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
362	Primo Impalcato	93-58	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
363	Primo Impalcato	61-95	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
364	Primo Impalcato	95-62	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
365	Primo Impalcato	96-65	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
366	Primo Impalcato	66-96	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
367	Primo Impalcato	69-94	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
368	Primo Impalcato	79-70	0	0	0	0	0	0	0	0	0
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
369	Primo Impalcato	94-70	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
370	Primo	1-71	0	0	0	0	0	0	0	0	0

	Impalcat o										
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
371	Primo Impalcat o	1-92	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
372	Primo Impalcat o	92-2	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
373	Primo Impalcat o	6-89	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
374	Primo Impalcat o	89-7	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
375	Primo Impalcat o	9-90	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
376	Primo Impalcat o	90-1 0	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
377	Primo Impalcat o	13-9 1	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
378	Primo Impalcat o	88-1 4	0	0	0	0	0	0	0	0	0
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
379	Primo Impalcat o	91-1 4	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
380	Primo Impalcat o	71-1 5	0	0	0	0	0	0	0	0	0
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
381	Primo Impalcat o	16-8 8	0	0	0	0	0	0	0	0	0
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
382	Primo Impalcat o	17-7 2	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
383	Primo Impalcat o	87-1 8	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
384	Primo Impalcat o	72-1 9	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0

385	Primo Impalcato	20-87	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
386	Primo Impalcato	21-73	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
387	Primo Impalcato	86-22	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
388	Primo Impalcato	73-23	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
389	Primo Impalcato	24-86	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
390	Primo Impalcato	25-74	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
391	Primo Impalcato	85-26	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
392	Primo Impalcato	27-85	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
393	Primo Impalcato	74-28	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
394	Primo Impalcato	84-29	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
395	Primo Impalcato	31-84	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
396	Primo Impalcato	83-33	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
397	Primo Impalcato	35-83	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
398	Primo Impalcato	82-37	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
399	Primo Impalcato	39-82	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1

			199	0	0	0	0	0	0	0	0
400	Primo Impalcato	78-43	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
401	Primo Impalcato	81-44	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
402	Primo Impalcato	45-78	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
403	Primo Impalcato	46-81	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
404	Primo Impalcato	77-47	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
405	Primo Impalcato	80-48	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
406	Primo Impalcato	49-77	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
407	Primo Impalcato	50-80	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
408	Primo Impalcato	76-51	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
409	Primo Impalcato	53-76	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			199	0	0	0	0	0	0	0	0
410	Primo Impalcato	75-55	0	0	0	0	0	0	0	0	0
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
411	Primo Impalcato	56-79	0	0	0	0	0	0	0	0	0
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
412	Primo Impalcato	57-75	0	0	0	0	0	0	0	0	0
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
413	Primo Impalcato	57-93	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
414	Primo Impalcato	93-58	0	0	0	0	0	0	0	0	0

			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
415	Primo Impalcato	61-95	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
416	Primo Impalcato	95-62	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
417	Primo Impalcato	96-65	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
418	Primo Impalcato	66-96	0	0	0	0	0	0	0	0	0
			100	1	1	1	1	1	1	1	1
			200	0	0	0	0	0	0	0	0
419	Primo Impalcato	69-94	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
420	Primo Impalcato	79-70	0	0	0	0	0	0	0	0	0
			102	2	1	1	1	1	1	1	1
			204	0	0	0	0	0	0	0	0
421	Primo Impalcato	94-70	0	0	0	0	0	0	0	0	0
			103	2	1	1	1	1	1	1	1
			206	0	0	0	0	0	0	0	0
422	Copertura	1-2	0	2909	-1685	754	510	611	510	510	510
			83	3070	-2240	898	157	559	411	415	415
			166	3960	-3685	866	-509	309	34	138	138
423	Copertura	15-1	0	12413	-9500	2157	1202	1552	1255	1255	1255
			80	10673	-9401	1198	436	794	627	627	627
			159	9314	-9560	139	-429	-63	-176	-101	-101
424	Copertura	2-3	0	3956	-3678	871	-512	310	34	139	139
			69	3158	-3156	639	-579	157	-87	1	1
			138	2322	-2847	243	-811	-148	-359	-263	-263
425	Copertura	3-4	0	2349	-2870	251	-815	-145	-358	-260	-260
			69	1819	-2327	120	-656	-161	-316	-254	-254
			138	1249	-1997	-175	-662	-329	-426	-374	-374
426	Copertura	4-5	0	1271	-2016	-167	-666	-326	-426	-373	-373
			69	806	-1384	-213	-417	-263	-304	-289	-289
			138	709	-1447	-331	-459	-331	-359	-331	-331
427	Copertura	5-6	0	690	-1431	-330	-457	-330	-358	-330	-330
			69	1087	-1589	-146	-420	-229	-284	-251	-251
			138	1396	-1993	-119	-587	-277	-370	-298	-298
428	Copertura	6-7	0	1365	-1960	-124	-581	-277	-368	-298	-298
			69	470	-883	-185	-341	-193	-228	-193	-193
			138	1013	-1439	-83	-437	-202	-273	-213	-213
429	Copertura	7-8	0	1045	-1470	-77	-443	-201	-274	-213	-213
			69	660	-918	-67	-266	-120	-160	-129	-129
			138	310	-665	-170	-316	-170	-210	-170	-170
430	Copertura	8-9	0	318	-659	-170	-316	-170	-210	-170	-170
			69	782	-1117	-82	-306	-153	-198	-167	-167
			138	1191	-1771	-127	-563	-271	-358	-290	-290
431	Copertura	9-10	0	1163	-1744	-133	-558	-273	-358	-290	-290

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			69	587	-1179	-296	-417	-296	-323	-296	-296
			138	1231	-2087	-359	-635	-425	-481	-428	-428
432	Copertura	10-11	0	1260	-2118	-354	-642	-425	-483	-429	-429
			69	840	-1557	-359	-461	-359	-380	-359	-359
			138	819	-1647	-346	-590	-398	-447	-414	-414
433	Copertura	11-12	0	797	-1628	-354	-588	-401	-447	-415	-415
			69	1544	-2099	-7	-585	-206	-322	-277	-277
			138	2234	-2764	175	-749	-164	-349	-265	-265
434	Copertura	12-13	0	2206	-2740	166	-746	-167	-350	-267	-267
			69	2898	-2881	600	-519	156	-67	9	9
			138	3678	-3361	870	-457	328	63	159	159
435	Copertura	13-14	0	3659	-3344	865	-454	326	63	158	158
			83	2691	-1789	928	220	597	451	451	451
			166	1580	-456	818	562	673	562	562	562
436	Copertura	16-14	0	4137	-1633	2002	1216	1485	1216	1216	1216
			80	2547	-1149	1055	524	747	606	606	606
			159	1207	-1413	8	-299	-91	-152	-103	-103
437	Copertura	15-17	0	15463	-12576	2248	1079	1560	1244	1244	1244
			66	12140	-9021	2282	1341	1666	1341	1341	1341
			132	9142	-5709	2269	1369	1703	1369	1369	1369
438	Copertura	16-18	0	4411	-1847	2034	1180	1482	1206	1206	1206
			66	4704	-1736	2119	1303	1597	1303	1303	1303
			132	4769	-2106	2167	1332	1648	1332	1332	1332
439	Copertura	17-19	0	11990	-8770	2344	1361	1715	1361	1361	1361
			66	9521	-6447	2090	1250	1564	1250	1250	1250
			132	7092	-4300	1789	1070	1347	1070	1070	1070
440	Copertura	18-20	0	5332	-2158	2198	1323	1647	1323	1323	1323
			66	4758	-2162	2001	1213	1509	1213	1213	1213
			132	4659	-2309	1735	1035	1303	1035	1035	1035
441	Copertura	19-21	0	9908	-7321	1859	1065	1362	1065	1065	1065
			66	6113	-3855	1462	876	1103	876	876	876
			132	3065	-1829	1008	618	795	618	618	618
442	Copertura	20-22	0	4906	-2378	1781	1031	1312	1031	1031	1031
			66	3691	-1681	1433	865	1083	865	865	865
			132	2774	-1514	1025	630	803	630	630	630
443	Copertura	21-23	0	5283	-3587	1072	617	794	617	617	617
			66	2976	-1941	716	416	539	416	416	416
			132	2314	-2022	294	146	216	146	146	146
444	Copertura	22-24	0	2847	-1525	1072	630	803	630	630	630
			66	2212	-1298	777	457	583	457	457	457
			132	1859	-1427	413	216	294	216	216	216
445	Copertura	23-25	0	3603	-3134	365	147	224	147	147	147
			66	2267	-2231	90	18	46	18	18	18
			132	3146	-3526	-124	-272	-178	-207	-180	-180
446	Copertura	24-26	0	1977	-1541	475	206	307	218	218	218
			66	1830	-1619	222	106	150	106	106	106
			132	2077	-2227	8	-123	-56	-82	-75	-75
447	Copertura	25-28	0	2781	-3141	-162	-235	-180	-200	-180	-180
			85	2779	-3052	-136	-212	-137	-167	-137	-137
			170	2862	-3276	-207	-306	-207	-247	-207	-207
448	Copertura	26-27	0	2039	-2164	-22	-63	-50	-63	-63	-63
			66	1820	-1945	-45	-78	-62	-68	-62	-62
			132	1917	-2177	-128	-167	-130	-147	-130	-130
449	Copertura	27-29	0	2129	-2355	-64	-189	-111	-135	-113	-113

			66	2035	-2127	-33	-83	-46	-59	-46	-46
			132	2336	-2430	33	-157	-36	-74	-47	-47
450	Copertura	28-30	0	4995	-5571	-152	-452	-236	-303	-236	-236
			73	3214	-3402	-59	-216	-94	-134	-94	-94
			146	3325	-3397	-36	-79	-36	-51	-36	-36
451	Copertura	29-31	0	2393	-2414	25	-44	-5	-18	-10	-10
			66	2388	-2295	79	16	53	41	47	47
			132	2758	-2688	65	8	43	31	35	35
452	Copertura	30-32	0	4248	-4447	8	-227	-70	-117	-76	-76
			69	3702	-3629	63	-21	38	21	36	36
			137	4042	-3891	111	45	86	73	75	75
453	Copertura	31-33	0	3060	-2916	140	26	91	68	72	72
			66	2760	-2556	141	82	115	102	102	102
			132	2991	-2863	151	-17	86	52	64	64
454	Copertura	32-34	0	4275	-4211	98	-56	44	13	32	32
			69	3148	-2930	127	89	115	108	109	109
			138	3100	-2877	172	69	130	110	111	111
455	Copertura	33-35	0	3122	-2905	160	98	128	109	109	109
			66	2697	-2468	150	101	128	115	115	115
			132	2789	-2685	71	35	59	52	52	52
456	Copertura	34-36	0	3054	-2926	117	-1	76	53	64	64
			69	2317	-2066	145	112	133	125	125	125
			138	3033	-2798	182	61	132	108	112	112
457	Copertura	35-37	0	3178	-2982	194	33	126	93	98	98
			66	3225	-3069	99	61	86	78	78	78
			132	3582	-3603	29	-74	-4	-25	-10	-10
458	Copertura	36-38	0	2789	-2668	104	4	70	50	61	61
			69	2455	-2206	150	114	133	124	124	124
			138	3639	-3357	210	50	139	107	113	113
459	Copertura	37-39	0	3793	-3710	73	19	51	41	42	42
			66	3500	-3465	41	-26	20	7	18	18
			132	3390	-3540	-60	-139	-75	-95	-75	-75
460	Copertura	38-40	0	2745	-2630	88	26	64	52	57	57
			69	2737	-2503	183	89	136	117	117	117
			137	4378	-4059	266	16	146	96	103	103
461	Copertura	39-41	0	3870	-3913	90	-148	-1	-49	-21	-21
			66	2876	-2964	-28	-97	-44	-62	-44	-44
			132	2512	-2783	-114	-215	-135	-163	-135	-135
462	Copertura	40-42	0	2212	-2123	95	38	58	44	44	44
			69	3425	-3203	188	-5	89	51	54	54
			138	5573	-5527	224	-133	49	-22	-11	-11
463	Copertura	41-44	0	2681	-2882	-89	-146	-100	-118	-100	-100
			66	2597	-2839	-116	-173	-121	-143	-121	-121
			132	2639	-3059	-156	-326	-210	-247	-210	-210
464	Copertura	42-43	0	2430	-2576	31	-105	-46	-73	-73	-73
			23	2807	-2819	51	-104	-35	-66	-66	-66
			46	3262	-3270	62	-110	-33	-68	-68	-68
465	Copertura	43-45	0	2482	-2617	27	-67	-40	-67	-67	-67
			66	2448	-2339	163	55	92	55	55	55
			132	2890	-2675	230	108	156	108	108	108
466	Copertura	44-46	0	2706	-3076	-185	-225	-185	-204	-185	-185
			66	2800	-2954	-42	-110	-73	-86	-77	-77
			132	3072	-3146	50	-73	-14	-38	-37	-37
467	Copertura	45-47	0	4139	-3922	275	90	163	108	108	108
			66	2588	-2064	418	262	334	262	262	262

			132	3804	-2914	609	347	447	347	347	347
468	Copertura	46-48	0	3158	-3230	12	-36	-20	-36	-36	-36
			66	2985	-2632	311	177	232	177	177	177
			132	3050	-2408	560	321	414	321	321	321
469	Copertura	47-49	0	2795	-2098	546	348	445	348	348	348
			66	2909	-1578	860	539	674	539	539	539
			132	5280	-3586	1106	661	835	661	661	661
470	Copertura	48-50	0	3202	-2553	519	324	419	324	324	324
			66	3154	-2011	892	571	714	571	571	571
			132	3282	-1782	1197	750	940	750	750	750
471	Copertura	49-51	0	2626	-1297	1045	664	838	664	664	664
			66	6378	-4208	1416	859	1075	859	859	859
			132	10597	-8096	1748	985	1264	985	985	985
472	Copertura	50-52	0	3355	-1847	1159	754	946	754	754	754
			66	3772	-1342	1569	1004	1243	1004	1004	1004
			132	4741	-1532	1911	1185	1471	1185	1185	1185
473	Copertura	51-53	0	7644	-5128	1663	991	1250	991	991	991
			66	10335	-7420	1962	1159	1456	1159	1159	1159
			132	13047	-9869	2207	1258	1593	1258	1258	1258
474	Copertura	52-54	0	4466	-1402	1879	1194	1483	1194	1194	1194
			66	5006	-1370	2142	1330	1635	1330	1330	1330
			132	5353	-1828	2349	1397	1742	1397	1397	1397
475	Copertura	53-55	0	10048	-6847	2120	1267	1583	1267	1267	1267
			66	12865	-9739	2164	1220	1560	1250	1250	1250
			132	15534	-12801	2147	973	1469	1165	1165	1165
476	Copertura	54-56	0	5141	-1633	2317	1411	1746	1411	1411	1411
			66	4664	-1655	2219	1345	1654	1345	1345	1345
			132	4342	-1920	2069	1172	1494	1211	1211	1211
477	Copertura	55-57	0	12511	-9730	2057	1097	1462	1177	1177	1177
			80	10864	-9506	1146	382	748	586	586	586
			159	9232	-9438	135	-432	-66	-179	-103	-103
478	Copertura	56-70	0	4108	-1630	2025	1230	1503	1230	1230	1230
			80	2351	-1198	1049	541	748	610	610	610
			159	1057	-1403	-26	-289	-105	-157	-110	-110
479	Copertura	57-58	0	2742	-1621	753	510	610	510	510	510
			83	3124	-2264	892	174	561	417	419	419
			166	4152	-3862	849	-472	311	47	145	145
480	Copertura	58-59	0	4150	-3858	853	-475	313	47	146	146
			69	3238	-3234	593	-530	149	-76	2	2
			138	2453	-2988	168	-749	-168	-351	-267	-267
481	Copertura	59-60	0	2481	-3011	176	-753	-164	-350	-265	-265
			69	1878	-2429	3	-591	-203	-322	-276	-276
			138	1187	-2011	-335	-593	-394	-446	-412	-412
482	Copertura	60-61	0	1215	-2036	-327	-597	-391	-445	-410	-410
			69	967	-1676	-354	-464	-354	-374	-354	-354
			138	1173	-2023	-382	-599	-424	-470	-424	-424
483	Copertura	61-62	0	1148	-2001	-387	-595	-423	-468	-423	-423
			69	1082	-1659	-237	-419	-281	-317	-289	-289
			138	1875	-2434	-46	-616	-245	-359	-279	-279
484	Copertura	62-63	0	1904	-2463	-40	-621	-244	-360	-279	-279
			69	1502	-1792	38	-371	-109	-191	-145	-145
			138	979	-1252	-47	-285	-125	-173	-137	-137
485	Copertura	63-64	0	1011	-1285	-41	-292	-124	-174	-137	-137
			69	441	-608	-48	-192	-67	-96	-75	-75
			138	866	-1143	-41	-295	-126	-177	-139	-139

486	Copertura	64-65	0	830	-1107	-48	-289	-127	-175	-139	-139
			69	1295	-1592	36	-376	-112	-194	-149	-149
			138	1663	-2231	-44	-627	-249	-365	-284	-284
487	Copertura	65-66	0	1628	-2197	-50	-622	-250	-365	-285	-285
			69	748	-1340	-244	-428	-288	-325	-296	-296
			138	917	-1783	-399	-607	-433	-478	-433	-433
488	Copertura	66-67	0	945	-1813	-394	-611	-434	-480	-434	-434
			69	775	-1503	-364	-474	-364	-385	-364	-364
			138	967	-1806	-337	-606	-401	-455	-419	-419
489	Copertura	67-68	0	941	-1782	-345	-601	-404	-455	-421	-421
			69	1728	-2295	-7	-596	-211	-329	-283	-283
			138	2436	-2979	167	-756	-171	-356	-272	-272
490	Copertura	68-69	0	2401	-2949	159	-753	-174	-357	-274	-274
			69	3213	-3216	586	-530	145	-78	-1	-1
			138	3961	-3670	849	-471	312	48	146	146
491	Copertura	69-70	0	3939	-3650	844	-468	311	48	145	145
			83	2793	-1938	896	190	570	427	427	427
			166	1546	-491	769	528	632	528	528	528
492	Copertura	1-1	0	7401	-7300	279	-149	91	6	39	39
			220	214	-242	22	-32	5	-6	0	0
			440	6879	-6974	232	-309	12	-96	-38	-38
493	Copertura	2-2	0	1789	-1698	100	34	61	45	45	45
			220	257	-356	41	-171	-11	-53	-21	-21
			440	2074	-2296	-87	-156	-87	-109	-87	-87
494	Copertura	3-3	0	388	-397	55	-17	14	-1	3	3
			220	426	-484	73	-208	2	-54	-13	-13
			440	1025	-1091	23	-193	-23	-66	-29	-29
495	Copertura	4-4	0	141	-154	2	-19	-5	-10	-7	-7
			220	437	-461	90	-202	15	-43	-3	-3
			440	785	-763	52	-123	11	-24	2	2
496	Copertura	5-5	0	301	-334	11	-39	-2	-12	-4	-4
			220	456	-463	89	-182	19	-35	2	2
			440	1007	-978	27	-46	12	-3	8	8
497	Copertura	6-6	0	135	-201	25	-55	4	-12	-1	-1
			220	443	-445	81	-164	18	-31	3	3
			440	774	-760	16	-2	8	5	7	7
498	Copertura	7-7	0	202	-229	31	-64	7	-12	0	0
			220	445	-449	77	-154	17	-29	3	3
			440	846	-833	34	-17	11	0	5	5
499	Copertura	8-8	0	278	-294	32	-64	7	-13	0	0
			220	398	-406	78	-156	18	-29	3	3
			440	823	-812	31	-15	10	1	6	6
500	Copertura	9-9	0	126	-161	26	-57	4	-12	-1	-1
			220	344	-358	83	-165	19	-31	3	3
			440	602	-585	16	-2	8	5	7	7
501	Copertura	10-10	0	235	-288	9	-35	-2	-11	-4	-4
			220	375	-397	90	-183	19	-35	2	2
			440	717	-710	32	-51	13	-4	8	8
502	Copertura	11-11	0	153	-166	2	-19	-5	-10	-7	-7
			220	291	-328	92	-204	16	-44	-3	-3
			440	441	-422	57	-127	11	-25	1	1
503	Copertura	12-12	0	278	-234	60	-21	15	-1	3	3
			220	280	-342	76	-212	3	-55	-13	-13
			440	446	-522	33	-204	-21	-69	-30	-30
504	Copertura	13-1	0	375	-285	132	35	68	45	45	45

	a	3									
			220	215	-273	44	-173	-10	-54	-21	-21
			440	411	-590	-88	-192	-88	-118	-88	-88
505	Copertura	57-57	0	7282	-7363	146	-281	-8	-93	-41	-41
			220	212	-227	32	-22	5	-5	-1	-1
			440	6936	-6858	309	-229	97	-11	39	39
506	Copertura	58-58	0	1667	-1757	-35	-101	-45	-61	-45	-45
			220	468	-266	170	-42	52	10	21	21
			440	2250	-2047	156	87	109	87	87	87
507	Copertura	59-59	0	317	-330	17	-56	0	-14	-3	-3
			220	607	-351	208	-73	54	-2	13	13
			440	1037	-862	192	-23	66	23	30	30
508	Copertura	60-60	0	147	-134	18	-2	9	5	7	7
			220	601	-359	201	-89	43	-15	3	3
			440	876	-707	120	-50	24	-10	-1	-1
509	Copertura	61-61	0	219	-211	36	-10	11	2	4	4
			220	622	-404	181	-88	35	-19	-2	-2
			440	964	-912	46	-26	3	-11	-8	-8
510	Copertura	62-62	0	225	-205	58	-26	13	-4	1	1
			220	556	-357	164	-81	31	-18	-3	-3
			440	822	-844	4	-15	-4	-8	-7	-7
511	Copertura	63-63	0	218	-219	64	-32	13	-7	0	0
			220	562	-374	157	-78	30	-18	-3	-3
			440	835	-848	16	-29	0	-9	-5	-5
512	Copertura	64-64	0	221	-223	64	-32	13	-7	0	0
			220	516	-333	158	-79	30	-18	-3	-3
			440	800	-808	14	-28	-1	-9	-5	-5
513	Copertura	65-65	0	164	-162	58	-26	13	-4	1	1
			220	479	-293	165	-83	31	-18	-3	-3
			440	627	-633	2	-15	-5	-8	-7	-7
514	Copertura	66-66	0	207	-199	36	-9	11	2	4	4
			220	461	-259	183	-90	36	-19	-2	-2
			440	579	-585	51	-31	4	-12	-8	-8
515	Copertura	67-67	0	138	-124	19	-2	10	6	7	7
			220	466	-237	204	-92	44	-15	3	3
			440	561	-421	127	-56	26	-11	-1	-1
516	Copertura	68-68	0	203	-210	21	-60	1	-15	-3	-3
			220	420	-167	212	-75	55	-2	14	14
			440	523	-348	205	-31	70	23	31	31
517	Copertura	69-69	0	240	-373	-39	-135	-47	-70	-47	-47
			220	346	-125	174	-43	55	11	22	22
			440	667	-405	197	92	122	92	92	92
518	Copertura	1-74	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1
			235	0	0	0	0	0	0	0	0
519	Copertura	74-2	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1
			235	0	0	0	0	0	0	0	0
520	Copertura	6-71	0	0	0	0	0	0	0	0	0
			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
521	Copertura	71-7	0	0	0	0	0	0	0	0	0
			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
522	Copertura	9-72	0	0	0	0	0	0	0	0	0

			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
523	Copertura	72-10	0	0	0	0	0	0	0	0	0
			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
524	Copertura	73-13	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1
			235	0	0	0	0	0	0	0	0
525	Copertura	14-73	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1
			235	0	0	0	0	0	0	0	0
526	Copertura	57-75	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1
			235	0	0	0	0	0	0	0	0
527	Copertura	75-58	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1
			235	0	0	0	0	0	0	0	0
528	Copertura	77-61	0	0	0	0	0	0	0	0	0
			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
529	Copertura	62-77	0	0	0	0	0	0	0	0	0
			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
530	Copertura	65-78	0	0	0	0	0	0	0	0	0
			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
531	Copertura	78-66	0	0	0	0	0	0	0	0	0
			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
532	Copertura	69-76	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1
			235	0	0	0	0	0	0	0	0
533	Copertura	76-70	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1
			235	0	0	0	0	0	0	0	0
534	Copertura	1-74	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1
			235	0	0	0	0	0	0	0	0
535	Copertura	74-2	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1
			235	0	0	0	0	0	0	0	0
536	Copertura	6-71	0	0	0	0	0	0	0	0	0
			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
537	Copertura	71-7	0	0	0	0	0	0	0	0	0
			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
538	Copertura	9-72	0	0	0	0	0	0	0	0	0
			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
539	Copertura	72-10	0	0	0	0	0	0	0	0	0
			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
540	Copertura	73-13	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1

			235	0	0	0	0	0	0	0	0
541	Copertura	14-73	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1
			235	0	0	0	0	0	0	0	0
542	Copertura	15-125	0	174	-809	-238	-372	-238	-283	-238	-238
			75	1020	-1860	-416	-626	-416	-500	-416	-416
			150	2498	-4007	-728	-1108	-728	-878	-728	-728
543	Copertura	127-16	0	2271	-3855	-792	-1202	-792	-955	-792	-792
			75	927	-1833	-453	-677	-453	-544	-453	-453
			150	64	-735	-248	-384	-248	-295	-248	-248
544	Copertura	17-129	0	435	-223	179	72	127	106	106	106
			75	1435	-1358	57	-44	39	19	38	38
			150	2863	-3173	-155	-432	-155	-235	-155	-155
545	Copertura	130-18	0	3161	-3475	-157	-439	-157	-239	-157	-157
			75	1530	-1459	51	-49	36	16	36	36
			150	463	-256	176	69	124	103	103	103
546	Copertura	19-135	0	577	-266	243	117	180	147	147	147
			75	2328	-2178	150	-56	94	53	75	75
			150	4794	-5040	17	-521	-113	-221	-123	-123
547	Copertura	134-20	0	4970	-5206	17	-523	-109	-217	-118	-118
			75	2403	-2247	151	-56	96	55	78	78
			150	614	-293	245	119	181	148	148	148
548	Copertura	21-136	0	586	-271	263	125	194	157	157	157
			75	2587	-2449	192	-109	98	37	69	69
			150	5294	-5582	94	-647	-117	-265	-144	-144
549	Copertura	138-22	0	5262	-5547	83	-656	-118	-266	-143	-143
			75	2556	-2415	188	-113	98	38	70	70
			150	608	-292	264	127	194	158	158	158
550	Copertura	23-141	0	605	-285	271	123	198	160	160	160
			75	2733	-2602	215	-144	99	27	65	65
			150	5616	-5927	142	-724	-117	-290	-156	-156
551	Copertura	142-24	0	5770	-6079	136	-743	-118	-294	-155	-155
			75	2782	-2651	214	-154	99	25	65	65
			150	662	-343	270	127	197	160	160	160
552	Copertura	25-145	0	793	-465	280	124	203	164	164	164
			75	3471	-3341	217	-152	99	25	65	65
			150	7248	-7567	144	-751	-120	-299	-159	-159
553	Copertura	146-26	0	7037	-7349	172	-782	-112	-302	-156	-156
			75	3375	-3244	232	-170	103	22	66	66
			150	754	-431	276	126	200	162	162	162
554	Copertura	150-27	0	7742	-8052	194	-803	-107	-306	-155	-155
			75	3687	-3560	239	-182	102	18	64	64
			150	844	-530	273	118	196	157	157	157
555	Copertura	28-149	0	871	-554	272	118	196	158	158	158
			75	3784	-3658	217	-162	97	21	63	63
			150	7816	-8131	151	-761	-118	-300	-158	-158
556	Copertura	154-29	0	8347	-8652	203	-807	-103	-305	-153	-153
			75	3994	-3872	240	-191	100	14	61	61
			150	812	-513	259	111	186	149	149	149
557	Copertura	30-153	0	1122	-795	259	105	185	149	149	149
			75	4098	-3976	231	-174	98	17	61	61
			150	8497	-8802	191	-773	-105	-298	-152	-152
558	Copertura	158-31	0	8486	-8789	203	-800	-102	-302	-151	-151
			75	4088	-3965	239	-189	100	14	61	61
			150	795	-498	257	110	185	148	148	148

559	Copertura	32-157	0	1161	-841	256	105	183	147	147	147
			75	4212	-4090	236	-178	99	16	61	61
			150	8727	-9029	201	-777	-102	-297	-151	-151
560	Copertura	162-33	0	8716	-9018	198	-788	-102	-299	-151	-151
			75	4169	-4048	236	-184	99	14	61	61
			150	850	-558	254	108	182	146	146	146
561	Copertura	34-161	0	1267	-951	254	106	182	147	147	147
			75	4134	-4014	230	-176	97	16	60	60
			150	8508	-8812	189	-773	-105	-297	-152	-152
562	Copertura	166-35	0	8562	-8863	191	-772	-103	-296	-150	-150
			75	4109	-3988	232	-177	98	16	60	60
			150	837	-546	251	107	181	145	145	145
563	Copertura	36-165	0	1320	-1008	252	107	181	146	146	146
			75	4233	-4115	221	-174	94	15	59	59
			150	8641	-8947	170	-765	-110	-297	-153	-153
564	Copertura	170-37	0	8773	-9075	182	-755	-105	-293	-151	-151
			75	4179	-4060	226	-170	96	16	60	60
			150	857	-569	249	106	179	144	144	144
565	Copertura	38-169	0	1378	-1073	248	108	179	144	144	144
			75	4227	-4110	215	-171	93	15	59	59
			150	8607	-8912	156	-756	-112	-294	-152	-152
566	Copertura	175-39	0	8546	-8848	172	-738	-107	-289	-151	-151
			75	4032	-3914	221	-163	94	17	59	59
			150	904	-619	247	105	177	143	143	143
567	Copertura	40-173	0	1417	-1119	240	108	173	140	140	140
			75	4073	-3957	222	-176	94	14	58	58
			150	8227	-8526	170	-757	-106	-292	-149	-149
568	Copertura	178-41	0	7617	-7927	164	-740	-112	-293	-155	-155
			75	3673	-3557	221	-165	93	16	58	58
			150	785	-495	244	112	179	145	145	145
569	Copertura	42-177	0	1812	-1531	234	104	169	136	136	136
			75	3740	-3631	251	-195	96	7	55	55
			150	7884	-8189	231	-791	-97	-301	-153	-153
570	Copertura	43-181	0	992	-670	267	137	198	161	161	161
			75	3664	-3521	272	-172	116	27	72	72
			150	7732	-8019	242	-777	-87	-290	-143	-143
571	Copertura	182-44	0	7675	-7975	169	-731	-107	-287	-150	-150
			75	3643	-3504	231	-146	106	30	70	70
			150	913	-587	274	128	201	163	163	163
572	Copertura	45-185	0	741	-425	266	130	195	158	158	158
			75	3496	-3361	224	-152	103	27	68	68
			150	7259	-7556	153	-735	-109	-287	-149	-149
573	Copertura	186-46	0	7322	-7623	145	-706	-112	-283	-151	-151
			75	3500	-3364	219	-135	102	31	68	68
			150	805	-484	270	127	198	161	161	161
574	Copertura	47-189	0	741	-424	267	130	196	159	159	159
			75	3081	-2948	195	-131	96	31	66	66
			150	6449	-6753	95	-694	-124	-281	-152	-152
575	Copertura	190-48	0	6072	-6367	114	-671	-116	-273	-148	-148
			75	2933	-2796	203	-120	99	34	68	68
			150	659	-342	266	126	195	158	158	158
576	Copertura	49-193	0	632	-315	263	130	195	158	158	158
			75	2728	-2588	172	-99	94	40	70	70
			150	5606	-5896	48	-627	-127	-262	-145	-145
577	Copertura	195-	0	5738	-6013	71	-608	-116	-251	-138	-138

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			75	2778	-2632	183	-90	99	45	73	73
			150	626	-309	263	129	194	158	158	158
578	Copertura	51-197	0	618	-318	247	122	183	149	149	149
			75	2455	-2304	137	-49	92	55	76	76
			150	5099	-5347	-13	-510	-121	-220	-124	-124
579	Copertura	199-52	0	4847	-5076	6	-489	-109	-208	-115	-115
			75	2355	-2198	144	-42	95	58	78	78
			150	601	-283	240	116	177	145	145	145
580	Copertura	53-201	0	498	-283	181	75	129	107	107	107
			75	1660	-1581	57	-40	40	21	39	39
			150	3449	-3758	-155	-427	-155	-234	-155	-155
581	Copertura	202-54	0	3210	-3516	-153	-423	-153	-233	-153	-153
			75	1571	-1493	55	-40	39	20	39	39
			150	482	-270	178	73	127	106	106	106
582	Copertura	55-205	0	196	-785	-239	-373	-239	-284	-239	-239
			75	1313	-2151	-419	-632	-419	-504	-419	-419
			150	3162	-4630	-734	-1114	-734	-885	-734	-734
583	Copertura	206-56	0	3028	-4555	-764	-1155	-764	-920	-764	-764
			75	1258	-2127	-434	-652	-434	-521	-434	-434
			150	173	-671	-239	-372	-239	-284	-239	-239
584	Copertura	57-75	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1
			235	0	0	0	0	0	0	0	0
585	Copertura	75-58	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1
			235	0	0	0	0	0	0	0	0
586	Copertura	77-61	0	0	0	0	0	0	0	0	0
			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
587	Copertura	62-77	0	0	0	0	0	0	0	0	0
			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
588	Copertura	65-78	0	0	0	0	0	0	0	0	0
			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
589	Copertura	78-66	0	0	0	0	0	0	0	0	0
			115	2	1	1	1	1	1	1	1
			231	0	0	0	0	0	0	0	0
590	Copertura	69-76	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1
			235	0	0	0	0	0	0	0	0
591	Copertura	76-70	0	0	0	0	0	0	0	0	0
			118	2	1	1	1	1	1	1	1
			235	0	0	0	0	0	0	0	0
592	Copertura	79-81	0	413	-441	29	-89	-13	-37	-21	-21
			80	5	-3	1	1	1	1	1	1
			159	429	-413	84	-35	32	8	16	16
593	Copertura	80-82	0	368	-357	43	-68	0	-22	-9	-9
			66	4	-3	1	0	1	0	1	1
			132	348	-363	62	-44	18	-3	6	6
594	Copertura	83-84	0	350	-327	46	-55	6	-14	-3	-3
			66	2	0	1	0	1	1	1	1
			132	323	-353	52	-50	11	-10	0	0
595	Copertura	85-86	0	349	-321	49	-53	8	-12	-2	-2

			66	3	0	2	1	2	1	1	1
			132	318	-351	52	-50	11	-10	0	0
596	Copertura	87-88	0	342	-320	40	-62	1	-20	-8	-8
			66	5	-2	2	2	2	2	2	2
			132	318	-344	61	-41	19	-1	7	7
597	Copertura	89-90	0	339	-321	34	-69	-5	-26	-14	-14
			66	4	-1	1	1	1	1	1	1
			132	320	-343	67	-36	24	3	12	12
598	Copertura	91-92	0	326	-313	30	-70	-8	-28	-15	-15
			66	3	-1	1	1	1	1	1	1
			132	312	-330	68	-32	25	5	13	13
599	Copertura	93-94	0	329	-319	33	-68	-6	-26	-14	-14
			66	5	-5	0	-1	0	0	0	0
			132	317	-334	62	-39	20	0	9	9
600	Copertura	95-96	0	328	-318	39	-58	1	-18	-8	-8
			66	5	-5	0	-1	0	0	0	0
			132	316	-332	53	-44	14	-6	3	3
601	Copertura	97-106	0	336	-318	49	-48	10	-10	0	0
			66	2	-1	1	1	1	1	1	1
			132	315	-338	45	-51	7	-12	-3	-3
602	Copertura	98-99	0	486	-466	58	-81	4	-23	-8	-8
			66	3	-3	1	0	1	0	1	1
			132	465	-495	78	-64	20	-9	4	4
603	Copertura	100-101	0	504	-461	72	-73	14	-15	0	0
			66	2	-1	1	0	1	1	1	1
			132	458	-508	70	-76	11	-18	-3	-3
604	Copertura	102-103	0	502	-456	74	-73	15	-14	0	0
			66	3	0	2	2	2	2	2	2
			132	453	-503	72	-75	13	-16	-1	-1
605	Copertura	104-105	0	495	-454	69	-78	10	-19	-4	-4
			66	3	-1	1	1	1	1	1	1
			132	450	-497	74	-72	16	-14	1	1
606	Copertura	107-108	0	355	-321	58	-41	17	-3	6	6
			66	1	-1	1	0	1	0	1	1
			132	318	-360	37	-62	-1	-21	-9	-9
607	Copertura	109-110	0	316	-270	58	-29	22	4	10	10
			80	2	0	2	1	1	1	1	1
			159	264	-321	25	-64	-9	-27	-15	-15
608	Copertura	111-112	0	492	-456	68	-78	10	-19	-4	-4
			66	3	-2	1	0	1	1	1	1
			132	453	-495	75	-71	16	-13	1	1
609	Copertura	113-114	0	486	-456	69	-77	11	-19	-4	-4
			66	3	-1	1	1	1	1	1	1
			132	453	-487	75	-70	17	-13	2	2
610	Copertura	115-116	0	486	-463	70	-77	12	-18	-3	-3
			66	6	-6	0	-1	0	-1	0	0
			132	459	-489	70	-76	12	-17	-2	-2
611	Copertura	117-118	0	491	-469	74	-71	15	-14	0	0
			66	3	-1	1	1	1	1	1	1
			132	467	-494	69	-76	12	-17	-2	-2
612	Copertura	119-120	0	503	-467	78	-66	19	-9	4	4
			66	2	-1	1	0	1	0	1	1
			132	463	-508	61	-82	6	-23	-7	-7
613	Copertura	121-122	0	516	-453	90	-47	32	4	14	14
			66	4	-3	1	-1	0	0	0	0

			132	444	-513	39	-92	-9	-35	-18	-18
614	Copertura	124-125	0	-33	-348	-180	-263	-180	-216	-180	-180
			99	-11	-111	-57	-85	-57	-70	-57	-57
			198	130	-4	83	56	68	56	56	56
615	Copertura	125-127	0	2581	-3941	-672	-1025	-672	-810	-672	-672
			775	11630	6123	9302	6445	7766	6445	6445	6445
			1550	2346	-3820	-737	-1119	-737	-887	-737	-737
616	Copertura	126-127	0	-8	-362	-180	-263	-180	-217	-180	-180
			99	-1	-121	-58	-86	-58	-70	-58	-58
			198	119	-9	82	55	67	55	55	55
617	Copertura	128-129	0	25	-370	-173	-257	-173	-209	-173	-173
			99	21	-122	-51	-78	-51	-62	-51	-51
			198	132	3	93	62	76	62	62	62
618	Copertura	129-130	0	2930	-3115	-87	-345	-93	-162	-93	-93
			775	12090	6061	9544	6620	8030	6620	6620	6620
			1550	3251	-3441	-94	-352	-95	-165	-95	-95
619	Copertura	131-130	0	80	-425	-172	-257	-172	-209	-172	-172
			99	35	-136	-51	-78	-51	-62	-51	-51
			198	148	-24	93	62	76	62	62	62
620	Copertura	132-135	0	69	-417	-174	-264	-174	-211	-174	-174
			99	35	-136	-51	-79	-51	-62	-51	-51
			198	157	-13	96	64	78	64	64	64
621	Copertura	133-134	0	110	-457	-174	-264	-174	-211	-174	-174
			99	47	-148	-51	-79	-51	-62	-51	-51
			198	158	-30	96	64	78	64	64	64
622	Copertura	135-134	0	4858	-4977	94	-430	-40	-145	-59	-59
			775	12167	6320	9583	6657	8078	6657	6657	6657
			1550	5050	-5158	93	-432	-36	-141	-54	-54
623	Copertura	137-136	0	121	-471	-175	-269	-175	-212	-175	-175
			99	57	-159	-51	-81	-51	-62	-51	-51
			198	149	-21	98	64	78	64	64	64
624	Copertura	136-138	0	5344	-5505	169	-555	-44	-189	-81	-81
			775	12126	6385	9551	6634	8051	6634	6634	6634
			1550	5313	-5471	159	-563	-45	-189	-79	-79
625	Copertura	139-138	0	126	-475	-175	-269	-175	-212	-175	-175
			99	59	-161	-51	-81	-51	-62	-51	-51
			198	151	-23	98	64	78	64	64	64
626	Copertura	140-141	0	183	-534	-175	-272	-175	-212	-175	-175
			99	83	-185	-51	-82	-51	-62	-51	-51
			198	156	-28	98	64	78	64	64	64
627	Copertura	141-142	0	5632	-5815	217	-630	-44	-214	-91	-91
			775	12106	6305	9534	6623	8037	6623	6623	6623
			1550	5803	-5984	212	-650	-45	-217	-91	-91
628	Copertura	143-142	0	174	-524	-175	-272	-175	-212	-175	-175
			99	79	-181	-51	-82	-51	-62	-51	-51
			198	155	-27	98	64	78	64	64	64
629	Copertura	144-145	0	257	-608	-175	-273	-175	-213	-175	-175
			99	109	-211	-51	-82	-51	-62	-51	-51
			198	185	-56	99	65	79	65	65	65
630	Copertura	145-146	0	7295	-7484	219	-656	-47	-222	-95	-95
			775	12102	6081	9531	6621	8035	6621	6621	6621
			1550	7072	-7255	247	-688	-38	-225	-91	-91
631	Copertura	147-146	0	230	-580	-175	-273	-175	-212	-175	-175
			99	98	-200	-51	-83	-51	-63	-51	-51
			198	179	-47	99	64	79	64	64	64

632	Copertura	148-149	0	295	-646	-175	-274	-175	-213	-175	-175
			99	120	-222	-51	-83	-51	-63	-51	-51
			198	196	-67	99	64	79	64	64	64
633	Copertura	149-150	0	7845	-8031	226	-667	-44	-223	-93	-93
			775	12109	6132	9538	6625	8040	6625	6625	6625
			1550	7778	-7960	269	-709	-34	-229	-91	-91
634	Copertura	151-150	0	272	-623	-175	-274	-175	-212	-175	-175
			99	114	-216	-51	-83	-51	-63	-51	-51
			198	184	-55	99	64	78	64	64	64
635	Copertura	152-153	0	316	-666	-175	-273	-175	-212	-175	-175
			99	132	-234	-51	-83	-51	-63	-51	-51
			198	198	-70	99	64	78	64	64	64
636	Copertura	153-154	0	8527	-8704	265	-680	-32	-221	-88	-88
			775	12120	6224	9546	6632	8047	6632	6632	6632
			1551	8369	-8547	278	-713	-30	-228	-89	-89
637	Copertura	155-154	0	308	-659	-175	-274	-175	-212	-175	-175
			99	129	-232	-51	-83	-51	-63	-51	-51
			198	193	-66	99	64	78	64	64	64
638	Copertura	156-157	0	334	-685	-175	-273	-175	-212	-175	-175
			99	135	-237	-51	-83	-51	-63	-51	-51
			198	206	-78	98	64	78	64	64	64
639	Copertura	157-158	0	8759	-8934	275	-683	-29	-221	-87	-87
			775	12125	6240	9550	6634	8050	6634	6634	6634
			1551	8500	-8675	277	-707	-29	-226	-87	-87
640	Copertura	159-158	0	327	-677	-175	-274	-175	-212	-175	-175
			99	139	-241	-51	-83	-51	-63	-51	-51
			198	191	-64	99	64	78	64	64	64
641	Copertura	160-161	0	324	-674	-175	-273	-175	-212	-175	-175
			99	139	-241	-51	-83	-51	-63	-51	-51
			198	191	-63	99	64	78	64	64	64
642	Copertura	161-162	0	8517	-8693	263	-679	-32	-221	-88	-88
			776	12127	6305	9551	6636	8052	6636	6636	6636
			1551	8742	-8916	272	-694	-30	-223	-87	-87
643	Copertura	163-162	0	338	-689	-175	-274	-175	-212	-175	-175
			99	139	-242	-51	-83	-51	-63	-51	-51
			198	203	-76	98	64	78	64	64	64
644	Copertura	164-165	0	334	-685	-175	-273	-175	-212	-175	-175
			99	138	-241	-51	-83	-51	-63	-51	-51
			198	202	-73	99	64	78	64	64	64
645	Copertura	165-166	0	8664	-8842	245	-671	-37	-220	-89	-89
			776	12130	6344	9554	6637	8054	6637	6637	6637
			1551	8579	-8752	265	-678	-30	-219	-86	-86
646	Copertura	167-166	0	328	-678	-175	-273	-175	-212	-175	-175
			99	140	-242	-51	-83	-51	-63	-51	-51
			198	194	-67	98	64	78	64	64	64
647	Copertura	168-169	0	338	-689	-175	-273	-175	-212	-175	-175
			99	140	-242	-51	-83	-51	-63	-51	-51
			198	200	-72	99	64	78	64	64	64
648	Copertura	169-170	0	8618	-8794	231	-663	-39	-218	-88	-88
			776	12134	6217	9557	6640	8057	6640	6640	6640
			1552	8802	-8976	256	-661	-32	-216	-87	-87
649	Copertura	171-170	0	339	-689	-175	-273	-175	-212	-175	-175
			99	140	-242	-51	-83	-51	-63	-51	-51
			198	204	-76	98	64	78	64	64	64
650	Copertura	172-	0	316	-667	-175	-273	-175	-212	-175	-175

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			99	137	-239	-51	-83	-51	-63	-51	-51
			198	189	-61	98	64	78	64	64	64
651	Copertura	173-175	0	8236	-8407	245	-663	-33	-215	-86	-86
			776	12139	6202	9561	6643	8060	6643	6643	6643
			1552	8578	-8752	247	-644	-34	-212	-87	-87
652	Copertura	174-175	0	332	-683	-175	-272	-175	-212	-175	-175
			99	137	-239	-51	-82	-51	-63	-51	-51
			198	202	-74	98	64	78	64	64	64
653	Copertura	176-177	0	291	-642	-175	-273	-175	-212	-175	-175
			99	125	-227	-51	-83	-51	-63	-51	-51
			198	182	-54	98	64	78	64	64	64
654	Copertura	177-178	0	7894	-8071	307	-698	-24	-224	-89	-89
			776	12137	5948	9560	6642	8059	6642	6642	6642
			1552	7633	-7814	239	-646	-39	-216	-91	-91
655	Copertura	179-178	0	328	-679	-175	-273	-175	-212	-175	-175
			99	136	-238	-51	-83	-51	-63	-51	-51
			198	196	-68	99	64	78	64	64	64
656	Copertura	180-181	0	284	-634	-175	-273	-175	-212	-175	-175
			99	121	-223	-51	-83	-51	-62	-51	-51
			198	180	-52	98	64	78	64	64	64
657	Copertura	181-182	0	7732	-7890	317	-684	-13	-214	-79	-79
			775	12122	6122	9547	6632	8048	6632	6632	6632
			1550	7706	-7876	244	-637	-33	-209	-85	-85
658	Copertura	183-182	0	282	-633	-175	-272	-175	-212	-175	-175
			99	122	-224	-51	-82	-51	-62	-51	-51
			198	183	-54	99	64	79	64	64	64
659	Copertura	184-185	0	256	-606	-175	-272	-175	-212	-175	-175
			99	110	-212	-51	-82	-51	-62	-51	-51
			198	178	-50	98	64	78	64	64	64
660	Copertura	185-186	0	7275	-7444	229	-641	-36	-210	-85	-85
			775	12116	6089	9542	6628	8044	6628	6628	6628
			1550	7340	-7513	221	-612	-39	-206	-86	-86
661	Copertura	187-186	0	279	-629	-175	-271	-175	-212	-175	-175
			99	116	-218	-51	-82	-51	-62	-51	-51
			198	185	-57	98	64	79	64	64	64
662	Copertura	188-189	0	216	-566	-175	-270	-175	-212	-175	-175
			99	93	-195	-51	-82	-51	-62	-51	-51
			198	171	-43	98	64	78	64	64	64
663	Copertura	189-190	0	6491	-6666	171	-601	-50	-205	-88	-88
			775	12115	6121	9541	6628	8044	6628	6628	6628
			1550	6096	-6263	190	-579	-43	-197	-84	-84
664	Copertura	191-190	0	221	-571	-175	-270	-175	-212	-175	-175
			99	98	-200	-51	-81	-51	-62	-51	-51
			198	165	-37	98	64	78	64	64	64
665	Copertura	192-193	0	150	-500	-175	-268	-175	-212	-175	-175
			99	70	-172	-51	-81	-51	-62	-51	-51
			198	155	-27	98	64	78	64	64	64
666	Copertura	193-195	0	5647	-5809	125	-535	-53	-185	-81	-81
			775	12130	6350	9555	6636	8054	6636	6636	6636
			1550	5788	-5936	147	-516	-43	-175	-74	-74
667	Copertura	194-195	0	146	-495	-175	-267	-175	-212	-175	-175
			99	67	-169	-51	-81	-51	-62	-51	-51
			198	155	-27	97	64	78	64	64	64
668	Copertura	196-197	0	121	-469	-174	-264	-174	-211	-174	-174

			99	52	-153	-51	-79	-51	-62	-51	-51
			198	173	-29	97	64	78	64	64	64
669	Copertura	197-199	0	5163	-5284	65	-419	-47	-144	-60	-60
			775	12168	6295	9585	6658	8079	6658	6658	6658
			1550	4897	-5000	82	-399	-36	-132	-51	-51
670	Copertura	198-199	0	85	-432	-173	-263	-173	-210	-173	-173
			99	45	-146	-51	-79	-51	-62	-51	-51
			198	159	-12	96	63	77	63	63	63
671	Copertura	200-201	0	112	-457	-173	-257	-173	-209	-173	-173
			99	45	-146	-51	-78	-51	-62	-51	-51
			198	158	-33	93	62	76	62	62	62
672	Copertura	201-202	0	3544	-3729	-92	-340	-92	-161	-92	-92
			775	12093	5894	9548	6622	8033	6622	6622	6622
			1550	3283	-3465	-91	-336	-91	-159	-91	-91
673	Copertura	203-202	0	63	-408	-172	-257	-172	-209	-172	-172
			99	32	-133	-51	-77	-51	-62	-51	-51
			198	144	-11	93	62	76	62	62	62
674	Copertura	204-205	0	19	-380	-180	-263	-180	-217	-180	-180
			99	8	-125	-58	-85	-58	-70	-58	-58
			198	131	-19	84	56	68	56	56	56
675	Copertura	205-206	0	3247	-4602	-678	-1030	-678	-817	-678	-678
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			1550	3114	-4529	-707	-1071	-707	-852	-707	-707
676	Copertura	207-206	0	-9	-356	-181	-264	-181	-218	-181	-181
			99	-3	-121	-58	-86	-58	-70	-58	-58
			198	127	-15	84	56	68	56	56	56
677	Copertura	79-14	0	303	-286	64	-23	28	10	17	17
			125	240	-263	6	-44	-9	-19	-12	-12
			250	833	-828	96	-182	-16	-72	-40	-40
678	Copertura	124-15	0	1334	-1322	51	-38	14	-3	5	5
			155	897	-904	27	-35	3	-9	-2	-2
			310	3115	-3141	91	-120	9	-33	-9	-9
679	Copertura	80-16	0	81	-66	15	-14	3	-3	0	0
			45	229	-223	27	-42	0	-13	-5	-5
			90	377	-380	38	-69	-2	-23	-9	-9
680	Copertura	128-17	0	1344	-1335	50	-40	13	-5	3	3
			155	873	-878	28	-33	4	-8	-2	-2
			310	3080	-3099	95	-115	13	-30	-7	-7
681	Copertura	82-18	0	9	-11	3	-7	1	-2	0	0
			43	220	-209	28	-36	3	-10	-3	-3
			85	450	-413	62	-75	7	-21	-6	-6
682	Copertura	132-19	0	1351	-1345	48	-43	11	-7	2	2
			155	881	-883	29	-32	5	-7	-1	-1
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683	Copertura	83-20	0	51	-43	9	-5	3	0	1	1
			43	218	-205	28	-34	4	-9	-2	-2
			85	385	-368	47	-63	5	-17	-5	-5
684	Copertura	137-21	0	1352	-1350	47	-45	10	-8	1	1
			155	883	-884	30	-31	6	-6	0	0
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685	Copertura	84-22	0	37	-39	3	-6	0	-2	-1	-1
			43	219	-200	32	-31	7	-6	0	0
			85	401	-363	61	-55	14	-10	2	2
686	Copertura	140-23	0	1352	-1351	46	-46	9	-9	0	0
			155	885	-884	31	-30	7	-6	0	0

			310	3121	-3120	108	-106	22	-20	1	1
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			43	219	-198	32	-30	7	-5	1	1
			85	389	-359	51	-61	7	-15	-3	-3
688	Copertura	144-25	0	1351	-1351	46	-46	9	-9	0	0
			155	883	-883	30	-31	6	-6	0	0
			310	3116	-3118	107	-108	21	-22	-1	-1
689	Copertura	86-26	0	37	-44	-1	-12	-4	-6	-4	-4
			43	216	-199	28	-34	3	-9	-2	-2
			85	392	-357	57	-57	11	-12	0	0
690	Copertura	87-27	0	60	-44	17	4	10	8	8	8
			43	215	-199	27	-35	3	-10	-3	-3
			85	381	-363	38	-75	-5	-27	-14	-14
691	Copertura	148-28	0	1343	-1381	21	-71	-13	-31	-19	-19
			155	868	-878	26	-35	2	-10	-4	-4
			310	3113	-3089	122	-91	35	-7	12	12
692	Copertura	88-29	0	41	-51	-5	-17	-8	-10	-8	-8
			43	211	-199	22	-40	-2	-14	-7	-7
			85	384	-355	49	-64	4	-19	-6	-6
693	Copertura	152-30	0	1350	-1401	12	-80	-21	-39	-26	-26
			155	881	-895	25	-37	0	-12	-5	-5
			310	3157	-3125	129	-87	40	-3	16	16
694	Copertura	89-31	0	45	-36	11	1	6	4	4	4
			43	212	-199	22	-41	-2	-14	-7	-7
			85	382	-368	33	-82	-10	-33	-18	-18
695	Copertura	156-32	0	1350	-1407	9	-84	-24	-42	-28	-28
			155	873	-887	24	-37	0	-12	-5	-5
			310	3149	-3112	132	-83	43	0	19	19
696	Copertura	90-33	0	42	-47	2	-12	-3	-6	-4	-4
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			85	382	-359	39	-75	-5	-28	-14	-14
697	Copertura	160-34	0	1356	-1419	5	-88	-28	-46	-32	-32
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698	Copertura	91-35	0	45	-37	9	0	5	3	3	3
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			85	367	-357	29	-84	-12	-35	-20	-20
699	Copertura	164-36	0	1357	-1427	0	-92	-31	-50	-35	-35
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701	Copertura	168-38	0	1358	-1435	-4	-97	-35	-54	-38	-38
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702	Copertura	93-39	0	46	-49	-1	-13	-5	-7	-5	-5
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			85	362	-352	37	-72	-4	-26	-13	-13
703	Copertura	172-40	0	1358	-1440	-7	-100	-38	-57	-41	-41
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704	Copertura	94-41	0	60	-48	14	0	8	5	6	6
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			85	385	-365	40	-77	-5	-28	-14	-14

705	Copertura	176-42	0	1355	-1443	-11	-104	-42	-61	-44	-44
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707	Copertura	95-44	0	44	-53	-4	-15	-7	-10	-7	-7
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713	Copertura	106-50	0	49	-46	8	-8	2	-2	0	0
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714	Copertura	196-51	0	1340	-1346	42	-49	6	-12	-3	-3
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			85	402	-371	63	-57	15	-9	2	2
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717	Copertura	108-54	0	54	-50	8	-10	2	-2	0	0
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			85	407	-353	73	-34	27	6	13	13
718	Copertura	204-55	0	1318	-1328	37	-51	3	-15	-5	-5
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			43	252	-221	44	-26	14	0	6	6
			85	464	-403	85	-67	25	-6	7	7
720	Copertura	110-70	0	363	-308	68	-34	26	6	14	14
			43	530	-435	106	-40	46	17	28	28
			85	704	-563	148	-54	67	27	43	43
721	Copertura	14-79	0	956	-883	177	-54	71	24	38	38
			95	407	-389	80	-33	32	9	17	17
			190	148	-157	6	-25	-3	-9	-5	-5
722	Copertura	15-124	0	2971	-2948	115	-91	31	-10	8	8
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			130	1285	-1261	55	-28	20	3	10	10
723	Copertura	16-1	0	378	-385	54	-42	12	-7	1	1

	a	26									
			65	230	-213	45	-14	19	7	10	10
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725	Copertura	18-1 31	0	463	-489	85	-60	25	-4	8	8
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729	Copertura	22-1 39	0	459	-508	76	-76	15	-15	0	0
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730	Copertura	23-1 40	0	2994	-2993	105	-106	21	-21	0	0
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732	Copertura	25-1 44	0	2996	-2994	106	-105	21	-21	0	0
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734	Copertura	27-1 51	0	449	-518	50	-101	-8	-38	-20	-20
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			130	48	-23	19	12	15	12	12	12
735	Copertura	28-1 48	0	3031	-2944	146	-64	57	15	31	31
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740	Copertura	33-1 63	0	437	-561	10	-137	-41	-71	-48	-48
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742	Copertura	35-167	0	469	-597	13	-144	-42	-73	-50	-50
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745	Copertura	38-168	0	3078	-2939	182	-27	90	48	59	59
			65	2146	-2107	93	-55	31	2	14	14
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			130	1294	-1360	0	-87	-30	-47	-33	-33
748	Copertura	41-179	0	459	-562	21	-128	-32	-62	-40	-40
			65	237	-255	29	-47	0	-16	-7	-7
			130	124	-72	42	26	32	26	26	26
749	Copertura	42-176	0	3069	-2914	191	-17	98	56	66	66
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			130	1292	-1364	-4	-91	-33	-50	-36	-36
750	Copertura	43-180	0	2980	-2981	104	-105	20	-22	0	0
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			130	1279	-1279	43	-43	8	-9	0	0
751	Copertura	44-183	0	465	-527	44	-107	-13	-43	-24	-24
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			130	42	-26	12	8	10	8	8	8
752	Copertura	45-184	0	2997	-2998	104	-106	20	-22	0	0
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753	Copertura	46-187	0	468	-493	72	-76	13	-16	-1	-1
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			130	22	-26	0	-2	-1	-1	-1	-1
754	Copertura	47-188	0	2995	-2998	103	-107	19	-23	-1	-1
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755	Copertura	48-191	0	467	-497	70	-79	11	-19	-4	-4
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756	Copertura	49-192	0	2993	-2999	100	-109	17	-25	-3	-3
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			130	1280	-1282	41	-44	7	-10	-1	-1
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759	Copertura	52-198	0	466	-511	61	-86	4	-25	-9	-9
			65	240	-265	31	-44	2	-13	-5	-5

			130	24	-26	0	-2	0	-1	0	0
760	Copertura	53-200	0	2950	-2966	91	-115	10	-31	-8	-8
			65	2104	-2117	63	-82	7	-22	-6	-6
			130	1267	-1276	36	-49	3	-14	-5	-5
761	Copertura	54-203	0	446	-497	47	-85	-2	-29	-13	-13
			65	233	-265	24	-46	-2	-16	-8	-8
			130	24	-36	1	-7	-2	-4	-3	-3
762	Copertura	55-204	0	2948	-2966	89	-116	9	-32	-9	-9
			65	2098	-2117	58	-86	3	-26	-10	-10
			130	1254	-1274	27	-55	-4	-20	-10	-10
763	Copertura	56-207	0	442	-505	46	-92	-5	-33	-16	-16
			65	227	-267	18	-50	-7	-21	-12	-12
			130	16	-34	-7	-12	-7	-9	-7	-7
764	Copertura	70-123	0	813	-937	21	-167	-37	-75	-45	-45
			95	452	-537	33	-103	-17	-44	-25	-25
			190	92	-125	28	-31	1	-11	-5	-5
765	Copertura	81-80	0	320	-344	64	-47	20	-2	7	7
			80	52	-52	5	-9	0	-3	-1	-1
			160	449	-424	58	-81	3	-25	-9	-9
766	Copertura	126-81	0	61	-79	8	-18	-1	-6	-3	-3
			30	25	-43	-6	-15	-6	-9	-6	-6
			60	92	-110	-9	-20	-9	-12	-9	-9
767	Copertura	98-82	0	263	-267	44	-29	13	-2	4	4
			82	44	-45	4	-8	0	-2	-1	-1
			165	355	-352	37	-59	1	-18	-6	-6
768	Copertura	99-83	0	274	-292	45	-38	12	-5	3	3
			82	55	-49	9	-8	2	-1	0	0
			165	402	-370	56	-61	9	-14	-2	-2
769	Copertura	100-84	0	262	-282	41	-38	9	-7	1	1
			82	54	-50	8	-8	1	-2	0	0
			165	390	-361	53	-58	9	-13	-1	-1
770	Copertura	101-85	0	261	-287	38	-43	6	-11	-2	-2
			82	56	-49	10	-7	3	-1	1	1
			165	398	-359	63	-52	16	-7	4	4
771	Copertura	102-86	0	264	-276	53	-27	19	3	10	10
			82	57	-49	11	-5	5	1	3	3
			165	390	-360	50	-63	6	-17	-5	-5
772	Copertura	103-87	0	260	-282	42	-39	10	-6	2	2
			82	55	-50	9	-7	2	-1	1	1
			165	390	-356	57	-57	11	-12	-1	-1
773	Copertura	104-88	0	268	-280	68	-13	32	16	21	21
			82	56	-49	12	-5	5	1	3	3
			165	382	-362	36	-78	-7	-29	-15	-15
774	Copertura	105-89	0	260	-269	60	-20	26	10	16	16
			82	58	-49	12	-4	5	2	3	3
			165	378	-352	45	-68	1	-22	-9	-9
775	Copertura	111-90	0	275	-267	72	-11	35	18	23	23
			80	58	-49	13	-3	6	3	4	4
			160	387	-366	38	-79	-6	-29	-15	-15
776	Copertura	112-91	0	247	-244	63	-11	31	16	20	20
			82	63	-53	14	-3	6	3	4	4
			165	366	-344	39	-69	-3	-25	-12	-12
777	Copertura	113-92	0	273	-274	74	-7	38	21	25	25
			82	62	-50	15	-2	7	4	5	5
			165	377	-363	37	-79	-7	-30	-16	-16

778	Copertura	114-93	0	268	-269	73	-6	37	22	25	25
			82	60	-51	13	-4	5	2	3	3
			165	371	-359	32	-80	-11	-33	-19	-19
779	Copertura	115-94	0	263	-273	49	-33	15	-1	6	6
			82	54	-49	10	-6	3	0	1	1
			165	381	-360	53	-62	8	-15	-3	-3
780	Copertura	116-95	0	270	-264	67	-12	32	16	21	21
			82	58	-50	11	-3	5	2	3	3
			165	371	-365	35	-73	-6	-28	-15	-15
781	Copertura	117-96	0	264	-278	39	-43	7	-10	-1	-1
			82	52	-47	10	-5	4	1	2	2
			165	382	-358	63	-49	18	-5	6	6
782	Copertura	118-97	0	264	-276	40	-39	8	-7	1	1
			82	51	-49	7	-7	2	-1	0	0
			165	379	-361	54	-53	11	-11	-1	-1
783	Copertura	131-98	0	26	-25	3	0	1	1	1	1
			30	108	-98	15	-17	2	-5	-1	-1
			60	220	-204	29	-37	3	-10	-3	-3
784	Copertura	133-99	0	29	-29	3	-4	1	-1	0	0
			30	95	-90	11	-15	1	-4	-1	-1
			60	204	-193	26	-33	4	-8	-1	-1
785	Copertura	139-100	0	24	-23	3	-1	1	0	0	0
			30	108	-95	17	-15	4	-2	1	1
			60	223	-200	35	-32	8	-6	1	1
786	Copertura	143-101	0	22	-23	2	-3	0	-1	0	0
			30	106	-94	15	-15	3	-3	0	0
			60	221	-199	33	-32	7	-6	1	1
787	Copertura	147-102	0	28	-24	6	2	4	3	3	3
			30	114	-98	24	-7	11	4	6	6
			60	228	-199	47	-20	18	5	10	10
788	Copertura	151-103	0	60	-28	25	16	19	16	16	16
			30	119	-96	27	-3	14	8	9	9
			60	223	-195	36	-30	10	-3	3	3
789	Copertura	155-104	0	117	-64	42	26	32	26	26	26
			30	158	-115	44	14	28	22	22	22
			60	244	-201	55	-10	26	13	17	17
790	Copertura	159-105	0	118	-64	43	27	33	27	27	27
			30	154	-108	43	12	28	21	21	21
			60	237	-199	52	-14	24	11	15	15
791	Copertura	119-106	0	264	-283	38	-43	6	-10	-2	-2
			82	52	-49	8	-8	2	-1	0	0
			165	387	-360	59	-53	14	-8	3	3
792	Copertura	120-107	0	262	-286	32	-45	2	-13	-4	-4
			82	55	-49	10	-5	3	0	1	1
			165	396	-358	64	-42	20	-2	7	7
793	Copertura	121-108	0	270	-307	32	-53	-1	-18	-8	-8
			82	53	-50	8	-7	2	-1	1	1
			165	414	-368	70	-47	22	-1	9	9
794	Copertura	122-109	0	247	-282	18	-48	-6	-19	-10	-10
			82	39	-34	6	2	4	3	3	3
			165	356	-311	61	-14	26	11	15	15
795	Copertura	123-110	0	92	-125	28	-31	1	-11	-5	-5
			82	270	-241	44	-2	20	10	12	12
			165	684	-572	132	-59	53	15	29	29
796	Copertura	163-	0	151	-88	50	31	38	31	31	31

	a	111									
			33	174	-124	47	20	32	25	25	25
			65	243	-194	57	-7	28	16	19	19
797	Copertura	167-112	0	151	-84	53	33	41	33	33	33
			30	185	-133	52	17	34	26	26	26
			60	266	-217	61	-11	29	15	19	19
798	Copertura	171-113	0	172	-99	58	37	45	37	37	37
			30	197	-138	53	24	37	29	29	29
			60	255	-199	61	-3	32	19	22	22
799	Copertura	174-114	0	176	-96	62	40	48	40	40	40
			30	199	-136	57	26	40	32	32	32
			60	259	-198	64	-3	34	21	24	24
800	Copertura	179-115	0	157	-87	55	35	42	35	35	35
			30	149	-112	40	11	25	19	19	19
			60	215	-204	37	-28	10	-3	3	3
801	Copertura	183-116	0	40	-22	12	8	10	8	8	8
			30	138	-100	36	5	21	15	16	16
			60	262	-202	64	-3	34	20	23	23
802	Copertura	187-117	0	23	-22	1	-3	-1	-2	-1	-1
			30	103	-101	14	-15	2	-4	-1	-1
			60	214	-206	31	-32	6	-7	-1	-1
803	Copertura	191-118	0	22	-19	3	-1	1	1	1	1
			30	107	-100	18	-13	5	-1	2	2
			60	219	-204	37	-29	10	-3	3	3
804	Copertura	194-119	0	24	-20	3	-2	1	0	0	0
			30	105	-101	17	-13	4	-2	1	1
			60	220	-206	35	-28	9	-4	2	2
805	Copertura	198-120	0	22	-26	0	-3	-1	-1	-1	-1
			30	106	-100	17	-14	4	-2	1	1
			60	222	-203	37	-29	10	-3	3	3
806	Copertura	203-121	0	33	-26	5	-4	1	-1	0	0
			30	97	-88	16	-5	6	2	3	3
			60	209	-185	36	-15	14	3	7	7
807	Copertura	207-122	0	21	-23	0	-2	0	-1	0	0
			30	114	-100	21	-12	8	1	4	4
			60	232	-200	44	-22	16	3	8	8

1.2.5 Involuppi dei diagrammi delle sollecitazioni: Taglio X-Z.

I dati seguenti riportano i valori del Taglio X-Z relativamente alle aste che definiscono la struttura ed in modo particolare:

- Asta : numerazione interna dell'asta.
X : distanza dal nodo iniziale misurata lungo l'asse dell'asta.
Taglio (T_{xz}) : valore del Taglio X-Z nel punto considerato:
Max : valore massimo (rispetto al sistema di riferimento globale) dell'involuppo.
Min : valore minimo (rispetto al sistema di riferimento globale) dell'involuppo.
Comb : combinazione di appartenenza del valore considerato nell'involuppo.

Tabella 30.I

Taglio (T_{xz}) [daN]											
				SLU		SLE					
						Caratteristiche		Frequenti		Quasi Permanenti	
Asta	Imp.	Fili	X [cm]	Max	Min	Max	Min	Max	Min	Max	Min
1	Fondazione	1-2	0	3822	-5478	-725	-1133	-773	-924	-773	-773
			42	2814	-3481	-293	-529	-345	-412	-345	-345
			83	2161	-2024	127	-32	61	22	22	22
2	Fondazione	1-2	0	2015	-1792	137	-20	106	41	106	106

	ne										
			42	1589	-630	535	392	452	422	422	422
			83	1349	50	914	700	795	700	700	700
3	Fondazio ne	1-15	0	4855	-5813	-354	-904	-549	-682	-549	-549
			40	3895	-3845	104	-292	-80	-159	-110	-110
			80	3329	-2321	594	310	422	329	329	329
4	Fondazio ne	1-15	0	3163	-2385	454	232	327	282	322	322
			40	2967	-1287	1020	769	859	769	769	769
			80	3270	-499	1674	1230	1419	1230	1230	1230
5	Fondazio ne	2-3	0	921	-1592	-270	-581	-336	-436	-336	-336
			35	815	-1072	-10	-292	-118	-174	-129	-129
			69	767	-644	228	-41	121	61	61	61
6	Fondazio ne	2-3	0	904	-448	294	50	228	160	228	228
			35	969	-322	549	243	442	380	407	407
			69	1377	-370	814	426	671	577	577	577
7	Fondazio ne	3-4	0	303	-896	-291	-444	-291	-371	-291	-291
			35	269	-519	-92	-191	-125	-149	-125	-125
			69	322	-262	125	12	82	37	37	37
8	Fondazio ne	3-4	0	478	-448	140	-40	118	54	118	118
			35	790	-445	396	126	310	256	279	279
			69	1153	-455	656	290	531	441	441	441
9	Fondazio ne	4-5	0	162	-887	-323	-488	-335	-415	-335	-335
			35	176	-536	-161	-221	-172	-193	-172	-172
			69	246	-261	70	-8	35	-8	-8	-8
10	Fondazio ne	4-5	0	299	-384	38	-91	38	-21	38	38
			35	587	-388	296	70	230	185	204	204
			69	948	-406	568	232	460	374	374	374
11	Fondazio ne	5-6	0	112	-885	-297	-510	-347	-429	-347	-347
			35	195	-546	-135	-231	-176	-196	-176	-176
			69	348	-353	86	-2	46	-2	-2	-2
12	Fondazio ne	5-6	0	495	-433	53	-83	31	-23	31	31
			35	732	-320	303	87	235	192	206	206
			69	975	-224	576	250	473	384	384	384
13	Fondazio ne	6-7	0	542	-1246	-302	-655	-391	-495	-391	-391
			35	643	-940	-66	-403	-194	-261	-212	-212
			69	762	-715	174	-154	38	-33	-33	-33
14	Fondazio ne	6-7	0	696	-697	119	-218	0	-76	0	0
			35	848	-489	362	28	224	157	179	179
			69	1045	-310	609	239	458	359	359	359
15	Fondazio ne	7-8	0	292	-1085	-295	-595	-397	-490	-397	-397
			35	427	-861	-134	-347	-213	-256	-217	-217
			69	569	-645	105	-101	18	-38	-38	-38
16	Fondazio ne	7-8	0	453	-467	12	-128	-7	-65	-7	-7
			35	639	-296	254	80	195	160	171	171
			69	838	-187	525	239	432	350	350	350
17	Fondazio ne	8-9	0	167	-826	-198	-514	-329	-414	-329	-329
			35	327	-629	-38	-228	-135	-173	-151	-151
			69	500	-445	148	11	85	28	28	28
18	Fondazio ne	8-9	0	631	-526	108	-84	52	-3	52	52
			35	854	-393	357	155	268	228	231	231
			69	1084	-263	608	351	502	410	410	410
19	Fondazio ne	9-10	0	542	-1144	-217	-603	-346	-445	-346	-346
			35	687	-915	-6	-354	-141	-211	-166	-166
			69	847	-703	235	-108	90	12	12	12
20	Fondazio ne	9-10	0	718	-628	155	-169	33	-35	33	33

			35	895	-430	398	73	261	195	211	211
			69	1089	-248	644	311	491	387	387	387
21	Fondazio ne	10-1 1	0	93	-973	-272	-625	-420	-510	-420	-420
			35	245	-737	-105	-348	-226	-275	-246	-246
			69	414	-553	62	-99	-16	-75	-75	-75
22	Fondazio ne	10-1 1	0	301	-351	-25	-112	-25	-72	-25	-25
			35	479	-193	195	128	164	143	143	143
			69	792	-64	458	297	387	309	309	309
23	Fondazio ne	11-1 2	0	-28	-908	-304	-667	-454	-543	-454	-454
			35	114	-692	-138	-406	-266	-319	-289	-289
			69	305	-558	30	-150	-62	-127	-127	-127
24	Fondazio ne	11-1 2	0	321	-431	-34	-158	-55	-104	-55	-55
			35	559	-343	190	59	136	108	108	108
			69	845	-296	434	274	357	274	274	274
25	Fondazio ne	12-1 3	0	-19	-1079	-403	-780	-549	-642	-549	-549
			35	181	-936	-218	-516	-353	-413	-378	-378
			69	467	-864	-23	-271	-132	-199	-199	-199
26	Fondazio ne	12-1 3	0	640	-775	15	-232	-68	-127	-68	-68
			35	977	-730	281	9	167	113	124	124
			69	1363	-699	571	272	431	332	332	332
27	Fondazio ne	13-1 4	0	74	-1440	-683	-892	-683	-777	-683	-683
			42	0	-807	-374	-509	-403	-431	-403	-403
			83	354	-521	45	-108	-17	-84	-84	-84
28	Fondazio ne	13-1 4	0	396	-552	-49	-170	-78	-116	-78	-78
			42	910	-324	449	260	353	293	293	293
			83	1745	-276	1048	706	868	725	725	725
29	Fondazio ne	14-1 6	0	521	-1680	-453	-897	-580	-709	-580	-580
			40	547	-765	16	-288	-122	-183	-137	-137
			80	887	-213	515	305	384	305	305	305
30	Fondazio ne	14-1 6	0	736	-240	334	168	248	206	248	248
			40	1370	95	912	697	776	697	697	697
			80	2319	-1	1573	1159	1339	1159	1159	1159
31	Fondazio ne	15-1 7	0	1723	-2960	-523	-763	-523	-636	-523	-523
			33	2324	-2612	-35	-262	-122	-168	-129	-129
			66	3097	-2431	499	257	364	275	275	275
32	Fondazio ne	15-1 7	0	3556	-2277	805	505	625	566	581	581
			33	4430	-2119	1383	997	1135	997	997	997
			66	5340	-1962	1990	1427	1664	1427	1427	1427
33	Fondazio ne	16-1 8	0	492	-1613	-506	-722	-506	-609	-506	-506
			33	606	-973	-34	-212	-104	-140	-111	-111
			66	1058	-421	501	295	383	295	295	295
34	Fondazio ne	16-1 8	0	1214	-283	666	426	519	472	490	490
			33	1842	5	1246	908	1032	908	908	908
			66	2650	28	1864	1339	1562	1339	1339	1339
35	Fondazio ne	17-1 9	0	1332	-3547	-923	-1296	-923	-1100	-923	-923
			33	1594	-2749	-482	-682	-482	-559	-482	-482
			66	2112	-2150	90	-89	16	-34	-34	-34
36	Fondazio ne	17-1 9	0	2363	-1768	395	230	302	269	298	298
			33	3177	-1542	1045	754	860	754	754	754
			66	4121	-1374	1725	1219	1433	1219	1219	1219
37	Fondazio ne	18-2 0	0	-174	-1742	-876	-1234	-876	-1049	-876	-876
			33	-22	-949	-434	-616	-434	-505	-434	-434
			66	661	-629	131	-18	65	16	16	16
38	Fondazio ne	18-2 0	0	860	-376	308	172	242	207	242	242
			33	1869	-469	960	700	794	700	700	700

			66	2943	-609	1643	1167	1370	1167	1167	1167
39	Fondazio ne	19-2 1	0	1588	-3799	-998	-1409	-998	-1188	-998	-998
			33	1849	-3064	-528	-749	-528	-609	-528	-528
			66	2334	-2421	67	-114	-3	-54	-54	-54
40	Fondazio ne	19-2 1	0	2568	-2180	279	103	194	158	194	194
			33	3334	-1783	936	670	770	670	670	670
			66	4192	-1449	1639	1149	1361	1149	1149	1149
41	Fondazio ne	20-2 2	0	281	-2446	-977	-1369	-977	-1163	-977	-977
			33	298	-1431	-504	-707	-504	-580	-504	-504
			66	664	-797	87	-67	24	-28	-28	-28
42	Fondazio ne	20-2 2	0	916	-602	265	115	191	159	191	191
			33	1728	-385	942	671	773	671	671	671
			66	2682	-372	1653	1155	1369	1155	1155	1155
43	Fondazio ne	21-2 3	0	1055	-3693	-1093	-1548	-1093	-1298	-1093	-1093
			33	1293	-2813	-614	-859	-614	-707	-614	-614
			66	1812	-2077	-30	-213	-95	-138	-138	-138
44	Fondazio ne	21-2 3	0	2307	-1961	263	60	166	125	163	163
			33	3198	-1799	900	635	733	635	635	635
			66	4219	-1728	1578	1104	1312	1104	1104	1104
45	Fondazio ne	22-2 4	0	-87	-2302	-1099	-1550	-1099	-1304	-1099	-1099
			33	-219	-1238	-614	-852	-614	-706	-614	-614
			66	357	-620	-30	-193	-89	-132	-132	-132
46	Fondazio ne	22-2 4	0	692	-493	170	1	99	59	99	99
			33	1725	-564	820	580	672	580	580	580
			66	2901	-781	1525	1060	1264	1060	1060	1060
47	Fondazio ne	23-2 5	0	1907	-4974	-1368	-1941	-1368	-1616	-1368	-1368
			33	2066	-4016	-905	-1261	-905	-1045	-905	-905
			66	2295	-3199	-403	-624	-446	-490	-452	-452
48	Fondazio ne	23-2 5	0	2504	-2903	-121	-330	-154	-224	-154	-154
			33	3128	-2467	466	262	354	291	291	291
			66	3949	-2230	1073	731	888	731	731	731
49	Fondazio ne	24-2 6	0	412	-2951	-1257	-1776	-1257	-1485	-1257	-1257
			33	224	-2026	-781	-1073	-781	-897	-781	-781
			66	380	-1164	-249	-417	-289	-323	-310	-310
50	Fondazio ne	24-2 6	0	701	-978	-28	-183	-60	-112	-60	-60
			33	1545	-731	595	407	480	407	407	407
			66	2638	-891	1283	874	1056	874	874	874
51	Fondazio ne	25-2 6	0	438	-2039	-801	-1002	-801	-871	-801	-801
			49	1117	-1319	45	-232	-55	-111	-101	-101
			97	1628	-782	685	373	534	423	423	423
52	Fondazio ne	25-2 6	0	657	-1175	-213	-411	-259	-316	-259	-259
			49	722	-473	239	66	160	124	124	124
			97	883	-76	572	404	485	404	404	404
53	Fondazio ne	25-2 6	0	630	-753	-9	-189	-62	-118	-62	-62
			49	552	-260	221	116	167	146	146	146
			97	575	71	427	308	373	308	308	308
54	Fondazio ne	25-2 6	0	472	-494	16	-112	-11	-67	-11	-11
			49	410	-156	176	115	140	127	127	127
			97	492	115	357	256	315	256	256	256
55	Fondazio ne	25-2 6	0	227	-346	-60	-147	-60	-115	-60	-60
			49	229	-88	89	70	75	70	70	70
			97	416	64	307	207	265	207	207	207
56	Fondazio ne	25-2 6	0	49	-285	-118	-207	-118	-172	-118	-118
			49	156	-98	38	26	30	28	29	29
			97	386	41	285	187	244	187	187	187

57	Fondazio ne	25-2 6	0	-26	-354	-162	-257	-162	-219	-162	-162
			49	146	-134	15	-4	7	3	6	6
			97	381	45	280	183	240	183	183	183
58	Fondazio ne	25-2 6	0	-40	-392	-187	-288	-187	-246	-187	-187
			49	136	-142	6	-14	-2	-6	-3	-3
			97	389	55	285	187	244	187	187	187
59	Fondazio ne	25-2 6	0	-55	-404	-196	-297	-196	-255	-196	-196
			49	131	-136	7	-12	0	-4	-2	-2
			97	401	64	293	194	252	194	194	194
60	Fondazio ne	25-2 6	0	-65	-407	-198	-298	-198	-256	-198	-198
			49	132	-133	9	-9	2	-2	0	0
			97	406	60	298	198	256	198	198	198
61	Fondazio ne	25-2 6	0	-62	-394	-191	-288	-191	-248	-191	-191
			49	143	-132	16	-3	8	4	5	5
			97	410	50	302	199	258	199	199	199
62	Fondazio ne	25-2 6	0	-52	-384	-185	-281	-185	-241	-185	-185
			49	150	-140	17	-4	8	4	5	5
			97	395	32	290	189	248	189	189	189
63	Fondazio ne	25-2 6	0	-38	-378	-181	-278	-181	-238	-181	-181
			49	143	-153	6	-15	-2	-6	-5	-5
			97	353	15	257	161	219	161	161	161
64	Fondazio ne	25-2 6	0	-35	-387	-188	-286	-188	-245	-188	-188
			49	100	-166	-30	-42	-31	-34	-33	-33
			97	284	-61	200	111	166	111	111	111
65	Fondazio ne	25-2 6	0	-59	-422	-211	-311	-211	-268	-211	-211
			49	93	-250	-78	-100	-78	-84	-78	-78
			97	350	-256	132	47	101	47	47	47
66	Fondazio ne	25-2 6	0	-107	-501	-261	-364	-261	-321	-261	-261
			49	162	-436	-127	-190	-137	-151	-137	-137
			97	508	-515	97	-38	51	-3	-3	-3
67	Fondazio ne	25-2 6	0	-16	-642	-329	-463	-329	-398	-329	-329
			49	333	-672	-131	-268	-170	-198	-170	-170
			97	873	-795	178	-40	96	39	39	39
68	Fondazio ne	25-2 6	0	8	-768	-380	-526	-380	-454	-380	-380
			49	358	-546	-55	-180	-94	-121	-94	-94
			97	1109	-500	440	289	362	304	304	304
69	Fondazio ne	25-2 6	0	778	-1729	-424	-765	-475	-593	-475	-475
			49	1263	-1118	211	-93	84	24	73	73
			97	2079	-462	1020	809	883	809	809	809
70	Fondazio ne	25-2 8	0	1030	-3469	-1002	-1466	-1002	-1213	-1002	-1002
			43	1299	-2344	-441	-639	-441	-519	-441	-441
			85	2152	-1850	270	102	186	115	115	115
71	Fondazio ne	25-2 8	0	2276	-1947	238	56	164	116	164	164
			43	3495	-1905	1027	727	837	727	727	727
			85	5034	-2079	1883	1303	1550	1303	1303	1303
72	Fondazio ne	26-2 7	0	71	-1983	-876	-1260	-876	-1056	-876	-876
			33	-22	-940	-409	-590	-409	-479	-409	-409
			66	864	-744	182	37	113	60	60	60
73	Fondazio ne	26-2 7	0	1116	-523	395	242	307	276	296	296
			33	2365	-825	1079	770	886	770	770	770
			66	3701	-1201	1792	1250	1478	1250	1250	1250
74	Fondazio ne	27-2 9	0	681	-2798	-1041	-1487	-1041	-1242	-1041	-1041
			33	416	-1681	-555	-786	-555	-643	-555	-555
			66	650	-895	46	-127	-20	-65	-65	-65
75	Fondazio	27-2	0	911	-632	210	41	141	99	141	141

	ne	9									
			33	2027	-756	887	636	731	636	636	636
			66	3317	-1045	1627	1136	1346	1136	1136	1136
76	Fondazio ne	28-3 0	0	1829	-4339	-1115	-1592	-1115	-1328	-1115	-1115
			37	1668	-2972	-611	-855	-611	-706	-611	-611
			73	1794	-1985	-7	-153	-59	-102	-102	-102
77	Fondazio ne	28-3 0	0	1552	-1337	159	62	127	90	127	127
			37	2295	-1010	916	643	742	643	643	643
			73	3566	-1232	1692	1167	1388	1167	1167	1167
78	Fondazio ne	29-3 1	0	551	-2795	-1122	-1599	-1122	-1333	-1122	-1122
			33	144	-1380	-618	-856	-618	-714	-618	-618
			66	309	-529	-21	-170	-74	-113	-113	-113
79	Fondazio ne	29-3 1	0	576	-425	122	-25	75	29	75	75
			33	1847	-681	812	583	670	583	583	583
			66	3323	-1136	1565	1093	1297	1093	1093	1093
80	Fondazio ne	30-3 2	0	901	-3112	-1106	-1586	-1106	-1316	-1106	-1106
			34	455	-1788	-609	-851	-609	-704	-609	-609
			69	572	-789	-66	-116	-80	-109	-109	-109
81	Fondazio ne	30-3 2	0	1017	-699	197	122	166	136	166	166
			34	2134	-796	940	669	770	669	669	669
			69	3467	-1112	1691	1177	1395	1177	1177	1177
82	Fondazio ne	31-3 3	0	1018	-3250	-1116	-1593	-1116	-1325	-1116	-1116
			33	558	-1772	-604	-845	-604	-697	-604	-604
			66	603	-905	13	-157	-49	-93	-93	-93
83	Fondazio ne	31-3 3	0	791	-643	138	-27	82	34	82	82
			33	1802	-615	828	594	683	594	594	594
			66	3224	-1010	1579	1107	1313	1107	1107	1107
84	Fondazio ne	32-3 4	0	866	-3232	-1183	-1685	-1183	-1402	-1183	-1183
			35	432	-1770	-669	-926	-669	-770	-669	-669
			69	240	-550	-116	-167	-127	-155	-155	-155
85	Fondazio ne	32-3 4	0	703	-463	137	79	120	92	120	120
			35	1930	-658	899	636	737	636	636	636
			69	3347	-1038	1665	1155	1374	1155	1155	1155
86	Fondazio ne	33-3 5	0	814	-3045	-1115	-1594	-1115	-1323	-1115	-1115
			33	374	-1576	-601	-837	-601	-693	-601	-601
			66	402	-453	9	-140	-45	-88	-88	-88
87	Fondazio ne	33-3 5	0	475	-312	129	-17	82	37	82	82
			33	1721	-533	823	594	685	594	594	594
			66	3179	-963	1577	1108	1315	1108	1108	1108
88	Fondazio ne	34-3 6	0	924	-3205	-1141	-1636	-1141	-1353	-1141	-1141
			35	519	-1762	-621	-869	-621	-715	-621	-621
			69	318	-524	-49	-103	-68	-103	-103	-103
89	Fondazio ne	34-3 6	0	557	-349	110	64	107	78	107	107
			35	1806	-553	877	627	724	627	627	627
			69	3250	-953	1648	1148	1366	1148	1148	1148
90	Fondazio ne	35-3 7	0	1212	-3419	-1103	-1580	-1103	-1309	-1103	-1103
			33	787	-1967	-590	-824	-590	-679	-590	-590
			66	811	-827	31	-134	-31	-79	-79	-79
91	Fondazio ne	35-3 7	0	803	-624	157	-6	95	53	95	95
			33	1707	-496	845	606	699	606	606	606
			66	3136	-903	1589	1116	1326	1116	1116	1116
92	Fondazio ne	36-3 8	0	952	-3208	-1128	-1623	-1128	-1340	-1128	-1128
			35	563	-1774	-605	-851	-605	-697	-605	-605
			69	347	-514	-23	-84	-46	-84	-84	-84
93	Fondazio ne	36-3 8	0	560	-333	124	77	117	90	117	117

			35	1777	-498	898	640	741	640	640	640
			69	3240	-909	1676	1166	1388	1166	1166	1166
94	Fondazio ne	37-3 9	0	966	-3156	-1095	-1572	-1095	-1300	-1095	-1095
			33	554	-1726	-586	-822	-586	-675	-586	-586
			66	523	-543	29	-141	-33	-80	-80	-80
95	Fondazio ne	37-3 9	0	567	-335	179	11	113	72	113	113
			33	1635	-402	860	616	712	616	616	616
			66	3023	-787	1589	1118	1328	1118	1118	1118
96	Fondazio ne	38-4 0	0	953	-3134	-1090	-1570	-1090	-1296	-1090	-1090
			34	599	-1733	-567	-795	-567	-652	-567	-567
			69	561	-639	28	-43	-1	-43	-43	-43
97	Fondazio ne	38-4 0	0	739	-463	154	103	136	113	136	136
			34	1855	-471	932	662	770	662	662	662
			69	3297	-911	1718	1193	1423	1193	1193	1193
98	Fondazio ne	39-4 1	0	1221	-3542	-1160	-1656	-1160	-1373	-1160	-1160
			33	839	-2165	-663	-922	-663	-761	-663	-663
			66	626	-890	-97	-228	-137	-172	-172	-172
99	Fondazio ne	39-4 1	0	619	-538	48	-45	32	-8	32	32
			33	1417	-261	721	519	601	519	519	519
			66	2618	-617	1436	1001	1196	1001	1001	1001
100	Fondazio ne	40-4 2	0	946	-3077	-1065	-1522	-1065	-1265	-1065	-1065
			35	664	-1720	-528	-725	-528	-604	-528	-528
			69	1058	-974	114	11	65	11	11	11
101	Fondazio ne	40-4 2	0	1623	-1040	362	257	283	262	266	266
			35	2934	-1034	1164	809	952	809	809	809
			69	4358	-1315	1979	1358	1627	1358	1358	1358
102	Fondazio ne	41-4 4	0	1124	-3533	-1204	-1727	-1204	-1425	-1204	-1204
			33	836	-2291	-727	-1020	-727	-837	-727	-727
			66	612	-1125	-205	-320	-234	-257	-257	-257
103	Fondazio ne	41-4 4	0	814	-812	32	-94	1	-42	1	1
			33	1471	-303	669	469	549	469	469	469
			66	2529	-420	1347	936	1127	936	936	936
104	Fondazio ne	42-4 3	0	912	-2261	-674	-944	-674	-787	-674	-674
			23	886	-1512	-305	-402	-306	-335	-306	-306
			46	1399	-1184	191	62	125	62	62	62
105	Fondazio ne	43-4 4	0	393	-2585	-1020	-1272	-1020	-1127	-1020	-1020
			49	1107	-1529	-105	-332	-181	-227	-211	-211
			97	1644	-880	625	357	487	382	382	382
106	Fondazio ne	43-4 4	0	1009	-1539	-196	-433	-265	-325	-265	-265
			49	1055	-739	302	95	203	158	158	158
			97	1196	-284	651	456	547	456	456	456
107	Fondazio ne	43-4 4	0	918	-989	45	-167	-35	-89	-35	-35
			49	753	-397	275	149	208	178	178	178
			97	675	1	471	338	409	338	338	338
108	Fondazio ne	43-4 4	0	619	-613	41	-95	3	-50	3	3
			49	465	-196	188	127	149	134	134	134
			97	491	112	359	255	315	255	255	255
109	Fondazio ne	43-4 4	0	316	-401	-43	-125	-43	-96	-43	-43
			49	260	-102	102	79	86	79	79	79
			97	418	56	308	209	266	209	209	209
110	Fondazio ne	43-4 4	0	75	-294	-109	-196	-109	-163	-109	-109
			49	159	-95	42	30	34	31	32	32
			97	383	27	283	186	243	186	186	186
111	Fondazio ne	43-4 4	0	-24	-350	-161	-254	-161	-217	-161	-161
			49	151	-141	15	-6	6	2	5	5

			97	376	33	277	181	237	181	181	181
112	Fondazio ne	43-4 4	0	-36	-395	-190	-290	-190	-248	-190	-190
			49	139	-150	4	-18	-4	-9	-5	-5
			97	384	48	281	185	242	185	185	185
113	Fondazio ne	43-4 4	0	-54	-413	-201	-303	-201	-260	-201	-201
			49	132	-144	2	-17	-5	-9	-6	-6
			97	395	59	289	192	248	192	192	192
114	Fondazio ne	43-4 4	0	-62	-407	-199	-298	-199	-256	-199	-199
			49	136	-134	10	-8	3	-1	1	1
			97	410	63	300	200	258	200	200	200
115	Fondazio ne	43-4 4	0	-63	-399	-194	-292	-194	-251	-194	-194
			49	140	-132	14	-4	7	3	4	4
			97	409	54	301	199	258	199	199	199
116	Fondazio ne	43-4 4	0	-53	-387	-187	-284	-187	-244	-187	-187
			49	147	-139	15	-5	7	3	4	4
			97	394	38	289	189	247	189	189	189
117	Fondazio ne	43-4 4	0	-40	-380	-183	-279	-183	-239	-183	-183
			49	138	-149	4	-16	-3	-7	-6	-6
			97	352	27	255	162	218	162	162	162
118	Fondazio ne	43-4 4	0	-34	-386	-188	-285	-188	-244	-188	-188
			49	94	-156	-29	-40	-30	-33	-31	-31
			97	286	-59	201	114	167	114	114	114
119	Fondazio ne	43-4 4	0	-57	-418	-209	-308	-209	-266	-209	-209
			49	93	-242	-75	-95	-75	-81	-75	-75
			97	371	-267	136	52	106	52	52	52
120	Fondazio ne	43-4 4	0	-114	-489	-254	-356	-254	-313	-254	-254
			49	173	-430	-120	-178	-129	-142	-129	-129
			97	551	-538	104	-22	60	7	7	7
121	Fondazio ne	43-4 4	0	-20	-631	-325	-454	-325	-393	-325	-325
			49	358	-687	-131	-254	-165	-191	-165	-165
			97	926	-837	177	-24	100	45	45	45
122	Fondazio ne	43-4 4	0	70	-852	-391	-543	-391	-467	-391	-391
			49	463	-673	-60	-198	-105	-134	-105	-105
			97	1205	-619	434	272	351	293	293	293
123	Fondazio ne	43-4 4	0	836	-1684	-377	-689	-424	-536	-424	-424
			49	1383	-1134	258	-16	136	81	124	124
			97	2119	-395	1079	862	941	862	862	862
124	Fondazio ne	43-4 5	0	2374	-5214	-1388	-2092	-1388	-1671	-1388	-1388
			33	1972	-3890	-851	-1311	-862	-1029	-862	-862
			66	2099	-2766	-245	-553	-330	-391	-340	-340
125	Fondazio ne	43-4 5	0	2612	-2415	191	-33	107	55	107	107
			33	3301	-1831	882	628	722	628	628	628
			66	4223	-1504	1638	1149	1362	1149	1149	1149
126	Fondazio ne	44-4 6	0	857	-2627	-885	-1295	-885	-1073	-885	-885
			33	564	-1398	-417	-620	-417	-498	-417	-417
			66	636	-366	178	6	103	54	54	54
127	Fondazio ne	44-4 6	0	1271	-246	604	399	480	440	445	445
			33	2151	-308	1298	921	1065	921	921	921
			66	3388	-577	2015	1405	1661	1405	1405	1405
128	Fondazio ne	45-4 7	0	1713	-4671	-1271	-1830	-1271	-1512	-1271	-1271
			33	2031	-3697	-752	-1062	-752	-873	-752	-752
			66	2470	-2939	-149	-350	-207	-247	-235	-235
129	Fondazio ne	45-4 7	0	2814	-2618	183	-31	94	47	94	94
			33	3707	-2188	875	610	708	610	610	610
			66	4632	-2023	1606	1126	1341	1126	1126	1126

130	Fondazio ne	46-4 8	0	1130	-3376	-1123	-1622	-1123	-1339	-1123	-1123
			33	1011	-2277	-633	-899	-633	-735	-633	-633
			66	1013	-1292	-38	-226	-103	-141	-139	-139
131	Fondazio ne	46-4 8	0	911	-631	212	48	140	101	140	140
			33	1635	-171	891	638	735	638	638	638
			66	2731	-174	1614	1140	1353	1140	1140	1140
132	Fondazio ne	47-4 9	0	1742	-4440	-1149	-1647	-1149	-1369	-1149	-1149
			33	1794	-3247	-635	-906	-635	-736	-635	-635
			66	1986	-2236	-17	-218	-84	-125	-125	-125
133	Fondazio ne	47-4 9	0	2105	-1931	161	-31	94	43	94	94
			33	2842	-1432	843	602	692	602	602	602
			66	3813	-1180	1559	1107	1313	1107	1107	1107
134	Fondazio ne	48-5 0	0	672	-2995	-1162	-1661	-1162	-1381	-1162	-1162
			33	491	-1806	-658	-929	-658	-761	-658	-658
			66	483	-792	-55	-254	-118	-158	-155	-155
135	Fondazio ne	48-5 0	0	703	-318	203	4	123	77	123	123
			33	1427	23	882	625	721	625	625	625
			66	2566	-82	1592	1126	1337	1126	1126	1126
136	Fondazio ne	49-5 1	0	1489	-4290	-1203	-1721	-1203	-1426	-1203	-1203
			33	1830	-3412	-702	-987	-702	-810	-702	-702
			66	2225	-2641	-121	-303	-175	-211	-208	-208
137	Fondazio ne	49-5 1	0	2485	-2430	82	-105	27	-28	27	27
			33	3192	-1950	731	514	594	514	514	514
			66	4192	-1724	1406	996	1186	996	996	996
138	Fondazio ne	50-5 2	0	598	-3115	-1258	-1787	-1258	-1486	-1258	-1258
			33	588	-2110	-761	-1061	-761	-874	-761	-761
			66	663	-1204	-219	-344	-247	-271	-271	-271
139	Fondazio ne	50-5 2	0	720	-657	32	-37	31	-7	31	31
			33	1304	-92	701	515	597	515	515	515
			66	2240	107	1398	992	1186	992	992	992
140	Fondazio ne	51-5 3	0	1461	-4223	-1192	-1681	-1192	-1400	-1192	-1192
			33	1585	-3210	-719	-988	-719	-816	-719	-719
			66	1784	-2294	-175	-339	-218	-255	-255	-255
141	Fondazio ne	51-5 3	0	2088	-2119	51	-127	-1	-50	-1	-1
			33	2616	-1574	650	453	531	453	453	453
			66	3547	-1429	1272	898	1076	898	898	898
142	Fondazio ne	52-5 4	0	395	-2891	-1248	-1762	-1248	-1466	-1248	-1248
			33	328	-1887	-779	-1077	-779	-888	-779	-779
			66	429	-1071	-269	-408	-296	-323	-321	-321
143	Fondazio ne	52-5 4	0	620	-699	-39	-123	-39	-82	-39	-39
			33	1042	-109	557	409	475	409	409	409
			66	1784	112	1190	847	1015	847	847	847
144	Fondazio ne	53-5 5	0	2063	-5239	-1368	-1905	-1368	-1597	-1368	-1368
			33	2145	-4245	-934	-1299	-934	-1063	-934	-934
			66	2250	-3304	-430	-716	-495	-552	-515	-515
145	Fondazio ne	53-5 5	0	2488	-3083	-282	-531	-297	-390	-297	-297
			33	2643	-2415	240	5	144	97	109	109
			66	2934	-1807	739	504	614	504	504	504
146	Fondazio ne	54-5 6	0	51	-2737	-1331	-1853	-1331	-1552	-1331	-1331
			33	59	-1872	-903	-1232	-903	-1026	-903	-903
			66	259	-1250	-464	-642	-478	-517	-489	-489
147	Fondazio ne	54-5 6	0	546	-1049	-234	-408	-234	-309	-234	-234
			33	896	-558	270	121	203	169	169	169
			66	1489	-344	791	562	671	562	562	562
148	Fondazio	55-5	0	634	-3295	-1163	-1579	-1163	-1344	-1163	-1163

	ne	7									
			40	1297	-2884	-702	-930	-702	-783	-702	-702
			80	2376	-2931	-151	-371	-209	-255	-255	-255
149	Fondazio ne	55-5 7	0	2204	-2952	-294	-544	-309	-393	-309	-309
			40	3966	-3451	309	-54	182	109	131	131
			80	6142	-4541	922	404	706	570	570	570
150	Fondazio ne	56-7 0	0	-83	-2306	-1195	-1623	-1195	-1380	-1195	-1195
			40	-163	-1380	-734	-969	-734	-820	-734	-734
			80	211	-759	-206	-395	-247	-287	-287	-287
151	Fondazio ne	56-7 0	0	109	-909	-320	-541	-320	-401	-320	-320
			40	812	-516	273	-39	167	105	122	122
			80	1786	-641	878	433	692	563	563	563
152	Fondazio ne	57-5 8	0	4053	-5925	-661	-1064	-715	-862	-715	-715
			42	2888	-3689	-228	-458	-286	-348	-286	-286
			83	2123	-2002	175	53	120	82	82	82
153	Fondazio ne	57-5 8	0	1864	-1779	116	-39	89	23	89	89
			42	1418	-504	513	376	434	405	405	405
			83	1451	-86	892	683	777	683	683	683
154	Fondazio ne	58-5 9	0	1146	-1866	-265	-562	-326	-424	-326	-326
			35	896	-1135	-5	-275	-109	-163	-119	-119
			69	786	-646	234	-12	130	70	70	70
155	Fondazio ne	58-5 9	0	922	-525	269	27	199	133	199	199
			35	1075	-240	513	218	411	352	376	376
			69	1353	-192	777	400	638	546	546	546
156	Fondazio ne	59-6 0	0	457	-993	-267	-430	-268	-352	-268	-268
			35	407	-613	-53	-188	-103	-132	-103	-103
			69	455	-338	161	39	107	59	59	59
157	Fondazio ne	59-6 0	0	662	-360	169	-40	134	68	134	134
			35	924	-299	426	126	330	270	295	295
			69	1352	-291	686	290	552	458	458	458
158	Fondazio ne	60-6 1	0	196	-826	-303	-460	-315	-391	-315	-315
			35	251	-551	-127	-204	-150	-169	-150	-150
			69	354	-319	110	17	67	17	17	17
159	Fondazio ne	60-6 1	0	582	-447	94	-52	67	13	67	67
			35	921	-313	333	112	266	222	237	237
			69	1167	-271	609	278	501	411	411	411
160	Fondazio ne	61-6 2	0	496	-1470	-307	-652	-390	-495	-390	-390
			35	609	-1055	-68	-409	-197	-265	-215	-215
			69	774	-851	174	-169	33	-39	-39	-39
161	Fondazio ne	61-6 2	0	808	-815	123	-230	-4	-81	-4	-4
			35	994	-646	370	8	221	148	174	174
			69	1228	-525	621	229	454	351	351	351
162	Fondazio ne	62-6 3	0	305	-1126	-337	-600	-410	-501	-410	-410
			35	400	-865	-168	-348	-232	-268	-233	-233
			69	498	-610	64	-97	-4	-56	-56	-56
163	Fondazio ne	62-6 3	0	339	-416	-39	-140	-39	-92	-39	-39
			35	486	-212	204	35	157	123	137	137
			69	706	-29	487	193	394	312	312	312
164	Fondazio ne	63-6 4	0	139	-936	-248	-530	-352	-437	-352	-352
			35	241	-602	-92	-250	-169	-201	-177	-177
			69	380	-387	98	-10	48	-3	-3	-3
165	Fondazio ne	63-6 4	0	378	-372	9	-98	3	-49	3	3
			35	606	-216	249	95	200	169	177	177
			69	991	-80	525	252	435	351	351	351
166	Fondazio ne	64-6 5	0	59	-776	-190	-491	-313	-395	-313	-313

			35	235	-511	-32	-209	-123	-159	-138	-138
			69	424	-349	139	38	90	38	38	38
167	Fondazio ne	64-6 5	0	607	-496	96	-65	55	3	55	55
			35	850	-386	347	167	267	231	232	232
			69	1136	-278	599	340	500	409	409	409
168	Fondazio ne	65-6 6	0	569	-1393	-230	-620	-351	-453	-351	-351
			35	685	-1031	-8	-369	-148	-220	-173	-173
			69	820	-812	229	-122	82	4	4	4
169	Fondazio ne	65-6 6	0	834	-750	173	-171	42	-30	42	42
			35	989	-553	413	72	269	201	218	218
			69	1164	-377	655	311	498	393	393	393
170	Fondazio ne	66-6 7	0	110	-974	-282	-615	-416	-506	-416	-416
			35	255	-740	-115	-340	-227	-272	-243	-243
			69	406	-550	51	-99	-17	-72	-72	-72
171	Fondazio ne	66-6 7	0	295	-352	-28	-118	-28	-76	-28	-28
			35	463	-184	193	120	160	139	139	139
			69	741	-79	450	298	381	305	305	305
172	Fondazio ne	67-6 8	0	-54	-873	-311	-648	-444	-532	-444	-444
			35	123	-684	-144	-388	-260	-309	-281	-281
			69	325	-562	24	-139	-57	-118	-118	-118
173	Fondazio ne	67-6 8	0	328	-445	-36	-162	-59	-108	-59	-59
			35	575	-367	184	54	131	104	104	104
			69	915	-375	428	270	352	270	270	270
174	Fondazio ne	68-6 9	0	-46	-1026	-408	-755	-536	-627	-536	-536
			35	213	-943	-222	-492	-344	-398	-365	-365
			69	545	-919	-27	-255	-123	-187	-187	-187
175	Fondazio ne	68-6 9	0	667	-809	14	-234	-71	-131	-71	-71
			35	1063	-823	273	7	162	109	120	120
			69	1532	-877	561	270	425	328	328	328
176	Fondazio ne	69-7 0	0	25	-1384	-679	-886	-679	-773	-679	-679
			42	32	-832	-372	-505	-400	-428	-400	-400
			83	463	-626	45	-107	-16	-82	-82	-82
177	Fondazio ne	69-7 0	0	491	-632	-31	-165	-66	-106	-66	-66
			42	1176	-470	466	264	364	303	303	303
			83	2151	-599	1060	712	878	735	735	735
178	Primo Impalcat o	1-2	0	997	-430	307	232	286	271	283	283
			83	630	-797	-60	-134	-80	-95	-83	-83
			166	264	-1163	-426	-501	-447	-462	-450	-450
179	Primo Impalcat o	1-15	0	6024	-5289	575	182	408	330	358	358
			80	5673	-5640	224	-169	57	-21	7	7
			159	5322	-5991	-127	-520	-294	-372	-344	-344
180	Primo Impalcat o	2-3	0	595	16	367	243	319	294	305	305
			69	290	-289	63	-61	14	-11	1	1
			138	-14	-594	-242	-366	-291	-316	-304	-304
181	Primo Impalcat o	3-4	0	478	281	327	322	323	322	322	322
			69	61	-24	22	17	18	17	17	17
			138	-244	-428	-282	-288	-286	-288	-288	-288
182	Primo Impalcat o	4-5	0	462	286	317	306	312	310	311	311
			69	32	-19	12	1	7	5	7	7
			138	-273	-443	-293	-303	-297	-299	-298	-298
183	Primo Impalcat o	5-6	0	710	-116	393	200	316	277	297	297

			69	405	-421	88	-104	11	-27	-8	-8
			138	100	-726	-217	-409	-294	-332	-313	-313
184	Primo Impalcato	6-7	0	839	-228	431	181	331	281	306	306
			69	534	-533	126	-124	26	-24	1	1
			138	230	-837	-178	-429	-279	-329	-304	-304
185	Primo Impalcato	7-8	0	646	-17	391	236	329	298	314	314
			69	341	-322	87	-69	25	-6	10	10
			138	37	-627	-218	-374	-280	-311	-295	-295
186	Primo Impalcato	8-9	0	627	-37	373	218	311	280	295	295
			69	323	-342	69	-87	6	-25	-10	-10
			138	18	-647	-236	-391	-299	-330	-314	-314
187	Primo Impalcato	9-10	0	833	-225	428	179	329	279	304	304
			69	528	-529	123	-125	24	-26	-1	-1
			138	223	-834	-182	-430	-281	-330	-305	-305
188	Primo Impalcato	10-11	0	718	-99	406	213	329	290	310	310
			69	414	-404	101	-91	24	-14	5	5
			138	109	-708	-203	-396	-280	-319	-300	-300
189	Primo Impalcato	11-12	0	421	198	299	262	286	279	283	283
			69	64	-107	-6	-42	-19	-26	-22	-22
			138	-241	-485	-311	-347	-324	-331	-326	-326
190	Primo Impalcato	12-13	0	579	35	367	247	318	294	307	307
			69	274	-270	63	-58	13	-11	2	2
			138	-31	-574	-242	-362	-291	-315	-303	-303
191	Primo Impalcato	13-14	0	667	207	497	409	451	434	439	439
			83	301	-159	131	43	85	67	72	72
			166	-66	-526	-236	-324	-282	-299	-294	-294
192	Primo Impalcato	14-16	0	1070	-352	474	289	389	352	359	359
			80	719	-703	123	-62	38	1	8	8
			159	368	-1054	-228	-413	-313	-350	-343	-343
193	Primo Impalcato	15-17	0	3496	-2843	449	195	347	296	318	318
			66	3205	-3134	158	-97	56	5	26	26
			132	2913	-3426	-134	-388	-236	-287	-265	-265
194	Primo Impalcato	16-18	0	782	-214	423	234	347	309	323	323
			66	490	-505	132	-57	56	18	32	32
			132	199	-797	-160	-348	-236	-274	-260	-260
195	Primo Impalcato	17-19	0	1563	-975	323	264	299	287	294	294
			66	1272	-1267	31	-27	7	-4	2	2
			132	980	-1558	-260	-319	-284	-296	-289	-289
196	Primo Impalcato	18-20	0	503	71	294	278	289	285	289	289
			66	211	-221	3	-14	-2	-6	-2	-2
			132	-80	-512	-289	-305	-294	-298	-294	-294
197	Primo Impalcato	19-21	0	4513	-3921	458	125	326	260	294	294
			66	4221	-4212	166	-166	35	-32	2	2
			132	3930	-4503	-125	-458	-257	-323	-289	-289
198	Primo Impalcato	20-22	0	906	-379	415	192	326	281	303	303

	o										
			66	615	-670	124	-100	34	-10	11	11
			132	323	-962	-168	-391	-257	-302	-280	-280
199	Primo Impalcato	21-23	0	1470	-890	316	267	295	286	290	290
			66	1179	-1181	24	-24	4	-6	-1	-1
			132	887	-1473	-267	-316	-288	-297	-293	-293
200	Primo Impalcato	22-24	0	460	98	282	277	281	280	281	281
			66	169	-193	-10	-15	-10	-12	-10	-10
			132	-123	-484	-301	-306	-302	-303	-302	-302
201	Primo Impalcato	23-25	0	4534	-4040	404	71	276	209	247	247
			66	4242	-4332	113	-220	-16	-83	-45	-45
			132	3951	-4623	-178	-512	-307	-374	-336	-336
202	Primo Impalcato	24-26	0	898	-411	389	166	301	257	281	281
			66	607	-703	97	-126	10	-35	-10	-10
			132	315	-994	-194	-417	-281	-326	-302	-302
203	Primo Impalcato	25-28	0	1324	-585	392	347	374	365	370	370
			85	949	-961	17	-28	-1	-10	-6	-6
			170	574	-1336	-359	-403	-377	-386	-381	-381
204	Primo Impalcato	26-27	0	498	107	308	303	305	303	303	303
			66	207	-185	16	11	13	11	11	11
			132	-84	-476	-275	-280	-278	-280	-280	-280
205	Primo Impalcato	27-29	0	918	-371	427	205	337	292	312	312
			66	627	-663	135	-87	45	1	21	21
			132	335	-954	-156	-378	-246	-291	-271	-271
206	Primo Impalcato	28-30	0	3502	-2797	470	234	376	328	351	351
			73	3179	-3120	148	-89	53	6	29	29
			146	2857	-3442	-174	-411	-269	-316	-293	-293
207	Primo Impalcato	29-31	0	475	117	300	296	297	296	296	296
			66	183	-174	8	4	6	4	4	4
			132	-108	-466	-283	-287	-286	-287	-287	-287
208	Primo Impalcato	30-32	0	2700	-2136	360	192	296	262	282	282
			69	2398	-2438	58	-111	-7	-40	-20	-20
			137	2095	-2741	-245	-413	-309	-343	-323	-323
209	Primo Impalcato	31-33	0	915	-382	421	198	330	285	305	305
			66	624	-674	130	-94	38	-6	14	14
			132	332	-965	-162	-385	-253	-298	-278	-278
210	Primo Impalcato	32-34	0	2859	-2281	376	192	305	268	289	289
			69	2554	-2586	71	-112	0	-37	-16	-16
			138	2250	-2891	-234	-417	-305	-341	-321	-321
211	Primo Impalcato	33-35	0	511	112	314	306	309	306	306	306
			66	219	-180	23	15	18	15	15	15
			132	-72	-471	-269	-277	-274	-277	-277	-277
212	Primo Impalcato	34-36	0	2859	-2284	373	191	302	266	287	287
			69	2554	-2589	68	-114	-2	-39	-18	-18
			138	2249	-2894	-237	-419	-307	-343	-322	-322
213	Primo	35-3	0	918	-392	419	198	328	284	304	304

	Impalcat o	7									
			66	627	-683	127	-93	37	-8	12	12
			132	335	-975	-164	-385	-255	-299	-279	-279
214	Primo Impalcat o	36-3 8	0	2867	-2297	371	188	300	264	285	285
			69	2562	-2602	66	-117	-5	-41	-20	-20
			138	2257	-2906	-239	-422	-309	-346	-324	-324
215	Primo Impalcat o	37-3 9	0	482	108	300	295	297	295	295	295
			66	190	-184	8	3	5	4	4	4
			132	-101	-475	-283	-288	-286	-288	-288	-288
216	Primo Impalcat o	38-4 0	0	2744	-2172	367	193	300	265	286	286
			69	2441	-2475	64	-110	-3	-37	-17	-17
			137	2139	-2777	-238	-412	-305	-340	-319	-319
217	Primo Impalcat o	39-4 1	0	787	-171	410	257	344	313	324	324
			66	495	-463	118	-35	52	22	33	33
			132	204	-754	-173	-326	-239	-270	-259	-259
218	Primo Impalcat o	40-4 2	0	3334	-2715	417	201	331	287	309	309
			69	3029	-3019	112	-104	26	-17	5	5
			138	2724	-3324	-192	-408	-279	-322	-300	-300
219	Primo Impalcat o	41-4 4	0	735	-248	335	169	271	238	257	257
			66	443	-540	44	-122	-21	-54	-34	-34
			132	152	-831	-248	-413	-312	-345	-326	-326
220	Primo Impalcat o	42-4 3	0	7569	-7640	219	-353	5	-110	-35	-35
			23	7468	-7741	117	-455	-97	-211	-137	-137
			46	7366	-7843	16	-556	-198	-313	-238	-238
221	Primo Impalcat o	43-4 5	0	2022	-1414	349	257	312	294	302	302
			66	1730	-1705	57	-34	21	2	11	11
			132	1439	-1997	-234	-325	-271	-289	-281	-281
222	Primo Impalcat o	44-4 6	0	506	141	327	318	321	318	318	318
			66	214	-150	35	26	30	26	26	26
			132	-77	-442	-256	-265	-261	-265	-265	-265
223	Primo Impalcat o	45-4 7	0	4410	-3843	445	124	316	252	284	284
			66	4119	-4134	154	-168	25	-40	-8	-8
			132	3827	-4426	-138	-459	-267	-331	-299	-299
224	Primo Impalcat o	46-4 8	0	1007	-431	439	198	339	291	311	311
			66	716	-722	148	-93	48	-1	20	20
			132	424	-1014	-144	-385	-244	-292	-272	-272
225	Primo Impalcat o	47-4 9	0	1469	-859	328	281	309	299	303	303
			66	1177	-1151	37	-11	17	8	12	12
			132	886	-1442	-255	-302	-274	-284	-280	-280
226	Primo Impalcat o	48-5 0	0	436	121	281	271	280	277	280	280
			66	144	-170	-11	-20	-11	-14	-11	-11
			132	-147	-462	-302	-312	-303	-306	-303	-303
227	Primo Impalcat o	49-5 1	0	4539	-3997	436	100	302	235	271	271
			66	4248	-4289	144	-191	11	-56	-20	-20
			132	3956	-4580	-147	-482	-281	-348	-312	-312

228	Primo Impalcato	50-52	0	835	-243	407	223	330	293	309	309
			66	544	-535	116	-69	39	2	17	17
			132	252	-826	-176	-360	-253	-290	-274	-274
229	Primo Impalcato	51-53	0	1530	-929	329	273	306	295	298	298
			66	1238	-1221	37	-18	15	3	7	7
			132	947	-1512	-254	-310	-277	-288	-285	-285
230	Primo Impalcato	52-54	0	557	-17	314	230	282	265	275	275
			66	265	-309	23	-62	-9	-26	-17	-17
			132	-26	-600	-268	-353	-301	-318	-308	-308
231	Primo Impalcato	53-55	0	3476	-2965	377	120	276	224	255	255
			66	3185	-3257	85	-171	-16	-67	-36	-36
			132	2893	-3548	-206	-463	-307	-359	-327	-327
232	Primo Impalcato	54-56	0	664	-204	330	162	263	230	252	252
			66	372	-495	38	-129	-28	-62	-39	-39
			132	81	-787	-253	-421	-320	-353	-331	-331
233	Primo Impalcato	55-57	0	5962	-5277	518	126	371	292	343	343
			80	5611	-5628	167	-225	20	-59	-8	-8
			159	5260	-5979	-184	-576	-331	-410	-359	-359
234	Primo Impalcato	56-70	0	932	-302	406	248	353	322	348	348
			80	581	-653	55	-103	2	-29	-3	-3
			159	230	-1004	-296	-454	-349	-380	-354	-354
235	Primo Impalcato	57-58	0	1005	-508	307	231	285	270	282	282
			83	639	-875	-60	-135	-81	-96	-84	-84
			166	272	-1241	-426	-502	-448	-463	-451	-451
236	Primo Impalcato	58-59	0	620	-11	365	244	318	293	305	305
			69	315	-315	60	-60	13	-11	0	0
			138	10	-620	-245	-365	-292	-316	-305	-305
237	Primo Impalcato	59-60	0	486	236	347	311	331	324	327	327
			69	113	-69	43	6	26	19	22	22
			138	-191	-421	-262	-298	-278	-285	-283	-283
238	Primo Impalcato	60-61	0	739	-141	395	204	319	280	299	299
			69	435	-445	90	-101	14	-25	-5	-5
			138	130	-750	-214	-406	-291	-329	-310	-310
239	Primo Impalcato	61-62	0	870	-257	430	184	331	282	306	306
			69	565	-562	125	-121	26	-23	2	2
			138	260	-866	-179	-426	-278	-328	-303	-303
240	Primo Impalcato	62-63	0	742	-123	403	215	328	290	309	309
			69	437	-427	98	-90	23	-14	5	5
			138	132	-732	-207	-395	-282	-319	-300	-300
241	Primo Impalcato	63-64	0	452	196	328	282	309	300	305	305
			69	108	-108	23	-23	5	-5	0	0
			138	-196	-452	-282	-328	-300	-309	-305	-305
242	Primo Impalcato	64-65	0	735	-136	394	206	319	281	300	300
			69	430	-440	90	-99	14	-24	-5	-5

			138	125	-745	-215	-403	-291	-328	-310	-310
243	Primo Impalcato	65-66	0	873	-266	426	180	328	279	303	303
			69	568	-571	121	-125	23	-26	-1	-1
			138	264	-876	-183	-429	-281	-331	-306	-306
244	Primo Impalcato	66-67	0	751	-131	405	214	329	291	310	310
			69	446	-436	101	-91	24	-14	5	5
			138	141	-741	-204	-395	-281	-319	-300	-300
245	Primo Impalcato	67-68	0	421	192	299	262	286	278	283	283
			69	68	-112	-6	-42	-19	-26	-22	-22
			138	-236	-486	-311	-347	-324	-331	-327	-327
246	Primo Impalcato	68-69	0	616	-3	367	247	318	294	307	307
			69	312	-308	62	-58	13	-11	2	2
			138	7	-613	-243	-362	-292	-316	-303	-303
247	Primo Impalcato	69-70	0	657	243	500	411	453	435	440	440
			83	271	-124	133	44	87	69	74	74
			166	-95	-490	-234	-322	-280	-298	-293	-293
248	Primo Impalcato	1-1	0	23	-126	11	-66	-7	-23	-10	-10
			188	23	-50	-10	-16	-10	-13	-10	-10
			376	84	-100	60	-52	3	-20	-10	-10
249	Primo Impalcato	2-2	0	469	-338	126	50	75	57	57	57
			188	498	-338	225	1	95	50	57	57
			376	632	-436	373	-73	124	35	57	57
250	Primo Impalcato	3-3	0	751	-472	204	-63	60	7	22	22
			188	895	-472	300	-111	80	-3	22	22
			376	1111	-472	445	-183	109	-17	22	22
251	Primo Impalcato	4-4	0	785	-479	229	-111	49	-19	4	4
			188	929	-479	325	-159	68	-28	4	4
			376	1146	-479	469	-232	97	-43	4	4
252	Primo Impalcato	5-5	0	880	-550	240	-124	47	-25	0	0
			188	1024	-550	337	-173	67	-35	0	0
			376	1241	-550	481	-245	96	-50	0	0
253	Primo Impalcato	6-6	0	694	-345	248	-127	49	-26	0	0
			188	838	-345	344	-175	69	-35	0	0
			376	1054	-345	489	-247	98	-50	0	0
254	Primo Impalcato	7-7	0	750	-383	255	-128	51	-25	1	1
			188	894	-383	351	-177	71	-35	1	1
			376	1111	-383	496	-249	100	-49	1	1
255	Primo Impalcato	8-8	0	760	-391	255	-128	51	-25	0	0
			188	905	-391	351	-177	70	-35	0	0
			376	1121	-391	496	-249	99	-50	0	0
256	Primo Impalcato	9-9	0	580	-264	248	-126	49	-25	0	0
			188	724	-264	344	-174	69	-35	0	0
			376	941	-264	489	-246	98	-50	0	0
257	Primo Impalcato	10-10	0	585	-341	234	-120	46	-24	0	0

			188	730	-341	330	-168	66	-34	0	0
			376	946	-341	475	-240	95	-48	0	0
258	Primo Impalcato	11-11	0	479	-219	223	-106	48	-18	4	4
			188	624	-219	319	-154	67	-27	4	4
			376	840	-219	464	-226	96	-42	4	4
259	Primo Impalcato	12-12	0	462	-249	200	-59	60	8	23	23
			188	607	-249	297	-107	79	-1	23	23
			376	823	-249	441	-179	108	-16	23	23
260	Primo Impalcato	13-13	0	355	-186	133	44	77	57	57	57
			188	444	-260	232	-6	97	49	57	57
			376	577	-371	380	-80	126	34	57	57
261	Primo Impalcato	14-14	0	41	-119	5	-64	-10	-24	-11	-11
			188	41	-69	-11	-21	-11	-15	-11	-11
			376	89	-125	62	-59	1	-23	-11	-11
262	Primo Impalcato	15-15	0	202	-212	4	-14	-3	-6	-3	-3
			188	202	-212	4	-14	-3	-6	-3	-3
			376	202	-212	4	-14	-3	-6	-3	-3
263	Primo Impalcato	16-16	0	41	-47	1	-14	-4	-7	-4	-4
			188	41	-47	1	-14	-4	-7	-4	-4
			376	41	-47	1	-14	-4	-7	-4	-4
264	Primo Impalcato	17-17	0	188	-196	5	-13	-2	-5	-3	-3
			188	188	-196	5	-13	-2	-5	-3	-3
			376	188	-196	5	-13	-2	-5	-3	-3
265	Primo Impalcato	18-18	0	41	-45	3	-13	-3	-6	-4	-4
			188	41	-45	3	-13	-3	-6	-4	-4
			376	41	-45	3	-13	-3	-6	-4	-4
266	Primo Impalcato	19-19	0	202	-205	8	-11	1	-3	-1	-1
			188	202	-205	8	-11	1	-3	-1	-1
			376	202	-205	8	-11	1	-3	-1	-1
267	Primo Impalcato	20-20	0	54	-46	6	-11	-1	-4	-2	-2
			188	54	-46	6	-11	-1	-4	-2	-2
			376	54	-46	6	-11	-1	-4	-2	-2
268	Primo Impalcato	21-21	0	207	-207	10	-9	2	-1	0	0
			188	207	-207	10	-9	2	-1	0	0
			376	207	-207	10	-9	2	-1	0	0
269	Primo Impalcato	22-22	0	57	-46	7	-9	1	-3	-1	-1
			188	57	-46	7	-9	1	-3	-1	-1
			376	57	-46	7	-9	1	-3	-1	-1
270	Primo Impalcato	23-23	0	212	-208	12	-6	4	1	2	2
			188	212	-208	12	-6	4	1	2	2
			376	212	-208	12	-6	4	1	2	2
271	Primo Impalcato	24-24	0	60	-46	9	-8	2	-1	0	0
			188	60	-46	9	-8	2	-1	0	0
			376	60	-46	9	-8	2	-1	0	0
272	Primo Impalcato	25-25	0	209	-207	11	-7	3	0	1	1

	o										
			188	209	-207	11	-7	3	0	1	1
			376	209	-207	11	-7	3	0	1	1
273	Primo Impalcato	26-26	0	58	-47	8	-9	1	-2	-1	-1
			188	58	-47	8	-9	1	-2	-1	-1
			376	58	-47	8	-9	1	-2	-1	-1
274	Primo Impalcato	27-27	0	57	-48	7	-10	0	-3	-2	-2
			188	57	-48	7	-10	0	-3	-2	-2
			376	57	-48	7	-10	0	-3	-2	-2
275	Primo Impalcato	28-28	0	200	-202	8	-10	1	-3	-1	-1
			188	200	-202	8	-10	1	-3	-1	-1
			376	200	-202	8	-10	1	-3	-1	-1
276	Primo Impalcato	29-29	0	58	-49	7	-10	0	-3	-1	-1
			188	58	-49	7	-10	0	-3	-1	-1
			376	58	-49	7	-10	0	-3	-1	-1
277	Primo Impalcato	30-30	0	230	-231	9	-11	1	-3	-1	-1
			188	230	-231	9	-11	1	-3	-1	-1
			376	230	-231	9	-11	1	-3	-1	-1
278	Primo Impalcato	31-31	0	52	-49	8	-9	1	-2	-1	-1
			188	52	-49	8	-9	1	-2	-1	-1
			376	52	-49	8	-9	1	-2	-1	-1
279	Primo Impalcato	32-32	0	226	-225	10	-10	2	-2	0	0
			188	226	-225	10	-10	2	-2	0	0
			376	226	-225	10	-10	2	-2	0	0
280	Primo Impalcato	33-33	0	54	-50	8	-9	1	-2	0	0
			188	54	-50	8	-9	1	-2	0	0
			376	54	-50	8	-9	1	-2	0	0
281	Primo Impalcato	34-34	0	226	-226	10	-10	2	-2	0	0
			188	226	-226	10	-10	2	-2	0	0
			376	226	-226	10	-10	2	-2	0	0
282	Primo Impalcato	35-35	0	55	-50	8	-8	2	-2	0	0
			188	55	-50	8	-8	2	-2	0	0
			376	55	-50	8	-8	2	-2	0	0
283	Primo Impalcato	36-36	0	228	-227	10	-10	2	-2	0	0
			188	228	-227	10	-10	2	-2	0	0
			376	228	-227	10	-10	2	-2	0	0
284	Primo Impalcato	37-37	0	56	-50	8	-8	2	-1	0	0
			188	56	-50	8	-8	2	-1	0	0
			376	56	-50	8	-8	2	-1	0	0
285	Primo Impalcato	38-38	0	228	-228	10	-10	2	-2	0	0
			188	228	-228	10	-10	2	-2	0	0
			376	228	-228	10	-10	2	-2	0	0
286	Primo Impalcato	39-39	0	55	-49	9	-8	2	-1	0	0
			188	55	-49	9	-8	2	-1	0	0
			376	55	-49	9	-8	2	-1	0	0
287	Primo	40-4	0	232	-233	10	-11	2	-2	0	0

	Impalcat o	0									
			188	232	-233	10	-11	2	-2	0	0
			376	232	-233	10	-11	2	-2	0	0
288	Primo Impalcat o	41-4 1	0	62	-55	10	-8	3	-1	1	1
			188	62	-55	10	-8	3	-1	1	1
			376	62	-55	10	-8	3	-1	1	1
289	Primo Impalcat o	42-4 2	0	221	-219	11	-9	3	-1	1	1
			188	221	-219	11	-9	3	-1	1	1
			376	221	-219	11	-9	3	-1	1	1
290	Primo Impalcat o	43-4 3	0	208	-206	10	-8	3	-1	1	1
			188	208	-206	10	-8	3	-1	1	1
			376	208	-206	10	-8	3	-1	1	1
291	Primo Impalcat o	44-4 4	0	53	-50	8	-9	1	-2	0	0
			188	53	-50	8	-9	1	-2	0	0
			376	53	-50	8	-9	1	-2	0	0
292	Primo Impalcat o	45-4 5	0	220	-219	11	-9	3	-1	1	1
			188	220	-219	11	-9	3	-1	1	1
			376	220	-219	11	-9	3	-1	1	1
293	Primo Impalcat o	46-4 6	0	53	-53	7	-11	0	-3	-1	-1
			188	53	-53	7	-11	0	-3	-1	-1
			376	53	-53	7	-11	0	-3	-1	-1
294	Primo Impalcat o	47-4 7	0	216	-214	11	-9	3	-1	1	1
			188	216	-214	11	-9	3	-1	1	1
			376	216	-214	11	-9	3	-1	1	1
295	Primo Impalcat o	48-4 8	0	54	-52	8	-10	1	-2	-1	-1
			188	54	-52	8	-10	1	-2	-1	-1
			376	54	-52	8	-10	1	-2	-1	-1
296	Primo Impalcat o	49-4 9	0	216	-212	12	-7	4	0	2	2
			188	216	-212	12	-7	4	0	2	2
			376	216	-212	12	-7	4	0	2	2
297	Primo Impalcat o	50-5 0	0	54	-50	9	-8	3	-1	1	1
			188	54	-50	9	-8	3	-1	1	1
			376	54	-50	9	-8	3	-1	1	1
298	Primo Impalcat o	51-5 1	0	213	-206	13	-6	5	1	3	3
			188	213	-206	13	-6	5	1	3	3
			376	213	-206	13	-6	5	1	3	3
299	Primo Impalcat o	52-5 2	0	61	-54	12	-7	5	1	2	2
			188	61	-54	12	-7	5	1	2	2
			376	61	-54	12	-7	5	1	2	2
300	Primo Impalcat o	53-5 3	0	202	-193	15	-4	7	3	4	4
			188	202	-193	15	-4	7	3	4	4
			376	202	-193	15	-4	7	3	4	4
301	Primo Impalcat o	54-5 4	0	62	-50	15	-4	7	3	4	4
			188	62	-50	15	-4	7	3	4	4
			376	62	-50	15	-4	7	3	4	4

302	Primo Impalcato	55-55	0	216	-207	16	-2	8	4	5	5
			188	216	-207	16	-2	8	4	5	5
			376	216	-207	16	-2	8	4	5	5
303	Primo Impalcato	56-56	0	57	-44	14	-1	7	4	4	4
			188	57	-44	14	-1	7	4	4	4
			376	57	-44	14	-1	7	4	4	4
304	Primo Impalcato	57-57	0	66	-55	69	-8	25	10	12	12
			188	56	-30	19	12	15	12	12	12
			376	89	-124	55	-58	22	0	12	12
305	Primo Impalcato	58-58	0	308	-518	-49	-125	-56	-74	-56	-56
			188	344	-666	0	-224	-49	-94	-56	-56
			376	411	-888	74	-372	-34	-124	-56	-56
306	Primo Impalcato	59-59	0	438	-481	63	-203	-7	-60	-22	-22
			188	511	-481	111	-300	3	-79	-22	-22
			376	619	-481	184	-444	17	-108	-22	-22
307	Primo Impalcato	60-60	0	539	-477	111	-227	19	-49	-4	-4
			188	611	-477	159	-323	28	-68	-4	-4
			376	719	-477	231	-467	43	-97	-4	-4
308	Primo Impalcato	61-61	0	546	-491	123	-237	25	-47	0	0
			188	618	-491	171	-333	35	-66	0	0
			376	726	-491	243	-477	49	-95	0	0
309	Primo Impalcato	62-62	0	506	-383	128	-250	26	-50	0	0
			188	578	-383	176	-346	35	-69	0	0
			376	686	-399	248	-490	50	-98	0	0
310	Primo Impalcato	63-63	0	554	-378	130	-257	26	-52	0	0
			188	626	-378	178	-353	35	-71	0	0
			376	734	-378	250	-498	50	-100	0	0
311	Primo Impalcato	64-64	0	551	-371	129	-257	26	-51	0	0
			188	623	-371	178	-353	35	-71	0	0
			376	731	-375	250	-497	50	-100	0	0
312	Primo Impalcato	65-65	0	464	-283	127	-249	26	-49	0	0
			188	536	-283	175	-345	35	-69	0	0
			376	645	-451	247	-489	50	-98	0	0
313	Primo Impalcato	66-66	0	462	-282	120	-234	25	-46	0	0
			188	534	-282	168	-330	34	-66	0	0
			376	642	-433	240	-474	49	-94	0	0
314	Primo Impalcato	67-67	0	355	-198	106	-223	18	-48	-4	-4
			188	427	-295	154	-319	27	-67	-4	-4
			376	535	-511	226	-463	42	-96	-4	-4
315	Primo Impalcato	68-68	0	318	-240	58	-200	-9	-60	-23	-23
			188	390	-240	106	-297	1	-80	-23	-23
			376	498	-448	178	-441	15	-108	-23	-23
316	Primo Impalcato	69-69	0	166	-313	-46	-135	-59	-79	-59	-59
			188	166	-426	4	-234	-51	-99	-59	-59

			376	168	-647	78	-382	-36	-128	-59	-59
317	Primo Impalcato	70-70	0	90	-65	60	-3	22	10	10	10
			188	90	-66	23	9	15	10	10	10
			376	116	-180	61	-67	22	-3	10	10
318	Primo Impalcato	1-71	0	3	2	2	2	2	2	2	2
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
319	Primo Impalcato	1-92	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
320	Primo Impalcato	92-2	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
321	Primo Impalcato	6-89	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2
322	Primo Impalcato	89-7	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2
323	Primo Impalcato	9-90	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2
324	Primo Impalcato	90-10	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2
325	Primo Impalcato	13-91	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
326	Primo Impalcato	88-14	0	3	2	2	2	2	2	2	2
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
327	Primo Impalcato	91-14	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
328	Primo Impalcato	71-15	0	3	2	2	2	2	2	2	2
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
329	Primo Impalcato	16-88	0	3	2	2	2	2	2	2	2
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
330	Primo Impalcato	17-72	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
331	Primo Impalcato	87-18	0	3	2	2	2	2	2	2	2

			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
332	Primo Impalcato	72-19	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
333	Primo Impalcato	20-87	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
334	Primo Impalcato	21-73	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
335	Primo Impalcato	86-22	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
336	Primo Impalcato	73-23	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
337	Primo Impalcato	24-86	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
338	Primo Impalcato	25-74	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
339	Primo Impalcato	85-26	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
340	Primo Impalcato	27-85	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
341	Primo Impalcato	74-28	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
342	Primo Impalcato	84-29	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
343	Primo Impalcato	31-84	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
344	Primo Impalcato	83-33	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
345	Primo Impalcato	35-83	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
346	Primo Impalcato	82-37	0	3	2	2	2	2	2	2	2

	o										
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
347	Primo Impalcat o	39-8 2	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
348	Primo Impalcat o	78-4 3	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
349	Primo Impalcat o	81-4 4	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
350	Primo Impalcat o	45-7 8	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
351	Primo Impalcat o	46-8 1	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
352	Primo Impalcat o	77-4 7	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
353	Primo Impalcat o	80-4 8	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
354	Primo Impalcat o	49-7 7	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
355	Primo Impalcat o	50-8 0	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
356	Primo Impalcat o	76-5 1	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
357	Primo Impalcat o	53-7 6	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
358	Primo Impalcat o	75-5 5	0	3	2	2	2	2	2	2	2
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
359	Primo Impalcat o	56-7 9	0	3	2	2	2	2	2	2	2
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
360	Primo Impalcat o	57-7 5	0	3	2	2	2	2	2	2	2
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
361	Primo	57-9	0	3	3	3	3	3	3	3	3

	Impalcat o	3									
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
362	Primo Impalcat o	93-5 8	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
363	Primo Impalcat o	61-9 5	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2
364	Primo Impalcat o	95-6 2	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2
365	Primo Impalcat o	96-6 5	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2
366	Primo Impalcat o	66-9 6	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2
367	Primo Impalcat o	69-9 4	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
368	Primo Impalcat o	79-7 0	0	3	2	2	2	2	2	2	2
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
369	Primo Impalcat o	94-7 0	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
370	Primo Impalcat o	1-71	0	3	2	2	2	2	2	2	2
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
371	Primo Impalcat o	1-92	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
372	Primo Impalcat o	92-2	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
373	Primo Impalcat o	6-89	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2
374	Primo Impalcat o	89-7	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2
375	Primo Impalcat o	9-90	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2

376	Primo Impalcato	90-10	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2
377	Primo Impalcato	13-91	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
378	Primo Impalcato	88-14	0	3	2	2	2	2	2	2	2
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
379	Primo Impalcato	91-14	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
380	Primo Impalcato	71-15	0	3	2	2	2	2	2	2	2
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
381	Primo Impalcato	16-88	0	3	2	2	2	2	2	2	2
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
382	Primo Impalcato	17-72	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
383	Primo Impalcato	87-18	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
384	Primo Impalcato	72-19	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
385	Primo Impalcato	20-87	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
386	Primo Impalcato	21-73	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
387	Primo Impalcato	86-22	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
388	Primo Impalcato	73-23	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
389	Primo Impalcato	24-86	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
390	Primo Impalcato	25-74	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0

			206	-3	-3	-3	-3	-3	-3	-3	-3
391	Primo Impalcato	85-26	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
392	Primo Impalcato	27-85	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
393	Primo Impalcato	74-28	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
394	Primo Impalcato	84-29	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
395	Primo Impalcato	31-84	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
396	Primo Impalcato	83-33	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
397	Primo Impalcato	35-83	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
398	Primo Impalcato	82-37	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
399	Primo Impalcato	39-82	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
400	Primo Impalcato	78-43	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
401	Primo Impalcato	81-44	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
402	Primo Impalcato	45-78	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
403	Primo Impalcato	46-81	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
404	Primo Impalcato	77-47	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
405	Primo Impalcato	80-48	0	3	2	2	2	2	2	2	2

			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
406	Primo Impalcato	49-77	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
407	Primo Impalcato	50-80	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
408	Primo Impalcato	76-51	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
409	Primo Impalcato	53-76	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			199	-2	-3	-2	-2	-2	-2	-2	-2
410	Primo Impalcato	75-55	0	3	2	2	2	2	2	2	2
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
411	Primo Impalcato	56-79	0	3	2	2	2	2	2	2	2
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
412	Primo Impalcato	57-75	0	3	2	2	2	2	2	2	2
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
413	Primo Impalcato	57-93	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
414	Primo Impalcato	93-58	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
415	Primo Impalcato	61-95	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2
416	Primo Impalcato	95-62	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2
417	Primo Impalcato	96-65	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2
418	Primo Impalcato	66-96	0	3	2	2	2	2	2	2	2
			100	0	0	0	0	0	0	0	0
			200	-2	-3	-2	-2	-2	-2	-2	-2
419	Primo Impalcato	69-94	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
420	Primo Impalcato	79-70	0	3	2	2	2	2	2	2	2

	o										
			102	0	0	0	0	0	0	0	0
			204	-2	-3	-2	-2	-2	-2	-2	-2
421	Primo Impalcato	94-70	0	3	3	3	3	3	3	3	3
			103	0	0	0	0	0	0	0	0
			206	-3	-3	-3	-3	-3	-3	-3	-3
422	Copertura	1-2	0	1716	-1726	391	-371	96	-56	-5	-5
			83	1497	-1945	105	-658	-169	-322	-224	-224
			166	1277	-2164	-182	-945	-434	-587	-443	-443
423	Copertura	15-1	0	670	-2298	-728	-1192	-728	-904	-728	-728
			80	545	-2423	-853	-1317	-853	-1029	-853	-853
			159	421	-2548	-977	-1442	-977	-1154	-977	-977
424	Copertura	2-3	0	1211	-1423	21	-217	-64	-112	-109	-109
			69	1024	-1606	-217	-455	-284	-332	-291	-291
			138	842	-1861	-455	-694	-473	-552	-473	-473
425	Copertura	3-4	0	1268	-1068	349	-70	171	87	100	100
			69	1086	-1250	111	-308	-49	-133	-82	-82
			138	904	-1432	-127	-546	-264	-353	-264	-264
426	Copertura	4-5	0	1198	-773	480	52	287	201	212	212
			69	1016	-955	242	-186	67	-19	30	30
			138	834	-1137	4	-424	-152	-239	-152	-152
427	Copertura	5-6	0	965	-555	396	114	261	205	205	205
			69	783	-737	158	-124	41	-15	23	23
			138	601	-919	-80	-362	-159	-235	-159	-159
428	Copertura	6-7	0	1882	-1395	599	11	340	223	243	243
			69	1700	-1577	361	-227	120	3	61	61
			138	1518	-1759	123	-465	-100	-217	-121	-121
429	Copertura	7-8	0	1024	-598	417	134	284	213	213	213
			69	842	-780	179	-104	64	8	31	31
			138	660	-962	-59	-342	-151	-213	-151	-151
430	Copertura	8-9	0	946	-755	293	-15	159	95	95	95
			69	764	-937	55	-253	-61	-123	-87	-87
			138	582	-1119	-183	-491	-269	-343	-269	-269
431	Copertura	9-10	0	1559	-1394	382	-126	171	69	82	82
			69	1377	-1576	144	-364	-49	-151	-100	-100
			138	1195	-1758	-94	-602	-269	-371	-282	-282
432	Copertura	10-11	0	1173	-788	452	68	281	192	192	192
			69	991	-970	214	-170	61	-16	10	10
			138	809	-1152	-24	-408	-159	-236	-172	-172
433	Copertura	11-12	0	1607	-1025	621	119	392	291	291	291
			69	1425	-1207	383	-119	172	71	109	109
			138	1243	-1389	145	-357	-48	-149	-73	-73
434	Copertura	12-13	0	1711	-729	748	447	579	491	491	491
			69	1529	-911	510	209	359	299	309	309
			138	1347	-1094	271	-29	139	79	127	127
435	Copertura	13-14	0	2124	-1187	955	220	606	459	462	462
			83	1893	-1406	668	-67	340	193	243	243
			166	1673	-1625	381	-354	75	-72	24	24
436	Copertura	16-14	0	941	-2349	-704	-1167	-704	-875	-704	-704
			80	816	-2474	-829	-1292	-829	-999	-829	-829
			159	691	-2599	-954	-1417	-954	-1124	-954	-954
437	Copertura	15-17	0	6392	-5909	452	103	282	198	198	198
			66	6288	-6013	349	-1	178	95	95	95
			132	6184	-6117	245	-104	74	-9	-9	-9
438	Copertura	16-1	0	2109	-1778	386	172	269	199	199	199

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			66	2006	-1881	282	68	165	95	95	95
			132	1902	-1985	179	-36	61	-8	-8	-8
439	Copertura	17-19	0	4456	-4745	-18	-342	-112	-177	-117	-117
			66	4352	-4849	-122	-445	-216	-280	-221	-221
			132	4249	-4953	-225	-549	-319	-384	-325	-325
440	Copertura	18-20	0	892	-1195	-99	-255	-114	-157	-114	-114
			66	788	-1299	-203	-358	-218	-261	-218	-218
			132	684	-1402	-307	-462	-322	-365	-322	-322
441	Copertura	19-21	0	5717	-6282	-123	-592	-235	-344	-235	-235
			66	5614	-6385	-226	-695	-339	-447	-339	-339
			132	5510	-6489	-330	-799	-443	-551	-443	-443
442	Copertura	20-22	0	1628	-2117	-112	-511	-201	-297	-201	-201
			66	1524	-2220	-216	-615	-304	-400	-304	-304
			132	1420	-2324	-320	-718	-408	-504	-408	-408
443	Copertura	21-23	0	3037	-3660	-253	-498	-253	-343	-253	-253
			66	2934	-3763	-356	-601	-356	-447	-356	-356
			132	2830	-3867	-460	-705	-460	-550	-460	-460
444	Copertura	22-24	0	1405	-1826	-210	-396	-210	-283	-210	-210
			66	1302	-1929	-314	-499	-314	-387	-314	-314
			132	1198	-2033	-418	-603	-418	-491	-418	-418
445	Copertura	23-25	0	3989	-4373	-103	-378	-143	-223	-143	-143
			66	3885	-4477	-207	-482	-247	-327	-247	-247
			132	3781	-4580	-311	-586	-351	-430	-351	-351
446	Copertura	24-26	0	1419	-1655	-47	-350	-118	-192	-118	-118
			66	1315	-1759	-150	-454	-222	-295	-222	-222
			132	1211	-1863	-254	-557	-326	-399	-326	-326
447	Copertura	25-28	0	1339	-1104	118	84	118	103	118	118
			85	1206	-1238	-16	-49	-16	-31	-16	-16
			170	1072	-1371	-149	-183	-149	-164	-149	-149
448	Copertura	26-27	0	1200	-1095	52	-2	52	32	52	52
			66	1096	-1198	-51	-106	-51	-71	-51	-51
			132	992	-1302	-155	-210	-155	-175	-155	-155
449	Copertura	27-29	0	1613	-1368	271	34	179	132	154	154
			66	1509	-1472	168	-70	75	28	50	50
			132	1406	-1575	64	-174	-28	-76	-53	-53
450	Copertura	28-30	0	3565	-3002	381	184	289	250	252	252
			73	3451	-3117	266	69	175	136	137	137
			146	3336	-3231	151	-45	60	21	23	23
451	Copertura	29-31	0	1369	-1093	145	134	142	138	138	138
			66	1266	-1197	41	31	38	35	35	35
			132	1162	-1300	-63	-73	-66	-69	-69	-69
452	Copertura	30-32	0	3934	-3469	354	135	256	212	218	218
			69	3826	-3576	247	27	148	104	110	110
			137	3718	-3684	139	-80	40	-4	3	3
453	Copertura	31-33	0	1476	-1281	198	-15	117	74	98	98
			66	1373	-1385	95	-118	13	-29	-6	-6
			132	1269	-1489	-9	-222	-90	-133	-110	-110
454	Copertura	32-34	0	3385	-3024	274	87	193	156	166	166
			69	3276	-3132	165	-21	85	47	58	58
			138	3168	-3240	57	-129	-24	-61	-51	-51
455	Copertura	33-35	0	1339	-1218	61	35	61	52	61	61
			66	1236	-1322	-43	-68	-43	-52	-43	-43
			132	1132	-1425	-147	-172	-147	-156	-147	-147
456	Copertura	34-36	0	3522	-3209	241	68	166	131	143	143

			69	3414	-3318	133	-41	58	23	35	35
			138	3305	-3426	24	-149	-51	-85	-74	-74
457	Copertura	35-37	0	1672	-1629	101	-99	30	-10	22	22
			66	1569	-1733	-3	-203	-74	-114	-82	-82
			132	1465	-1836	-107	-307	-177	-217	-186	-186
458	Copertura	36-38	0	3226	-2912	258	70	173	135	146	146
			69	3117	-3021	149	-38	64	27	38	38
			138	3009	-3129	41	-147	-44	-82	-70	-70
459	Copertura	37-39	0	1062	-1031	15	-18	15	0	15	15
			66	959	-1135	-88	-122	-88	-103	-88	-88
			132	855	-1239	-192	-225	-192	-207	-192	-192
460	Copertura	38-40	0	4053	-3700	283	55	176	130	141	141
			69	3946	-3807	175	-52	68	23	33	33
			137	3838	-3915	67	-160	-39	-85	-74	-74
461	Copertura	39-41	0	2272	-2238	129	-127	32	-19	17	17
			66	2169	-2342	25	-231	-72	-123	-87	-87
			132	2065	-2446	-78	-335	-175	-227	-190	-190
462	Copertura	40-42	0	3887	-3684	214	-23	104	57	69	69
			69	3779	-3792	106	-132	-4	-52	-40	-40
			138	3671	-3901	-3	-240	-113	-160	-148	-148
463	Copertura	41-44	0	1810	-1769	96	-76	31	-3	21	21
			66	1707	-1873	-7	-179	-72	-107	-83	-83
			132	1603	-1976	-111	-283	-176	-210	-187	-187
464	Copertura	42-43	0	2899	-2772	104	25	64	47	47	47
			23	2863	-2808	68	-11	28	11	11	11
			46	2827	-2844	32	-47	-8	-25	-25	-25
465	Copertura	43-45	0	2208	-1714	289	228	256	236	236	236
			66	2105	-1818	185	124	152	132	132	132
			132	2001	-1922	82	21	49	29	29	29
466	Copertura	44-46	0	1539	-1107	294	211	245	216	216	216
			66	1435	-1211	190	108	141	112	112	112
			132	1332	-1315	86	4	37	8	8	8
467	Copertura	45-47	0	4771	-4147	495	186	347	284	284	284
			66	4667	-4251	391	83	243	181	181	181
			132	4563	-4355	287	-21	140	77	77	77
468	Copertura	46-48	0	1651	-903	536	374	437	374	374	374
			66	1548	-1007	432	270	333	270	270	270
			132	1444	-1111	328	167	230	167	167	167
469	Copertura	47-49	0	4289	-3499	552	308	413	341	341	341
			66	4185	-3603	449	204	309	237	237	237
			132	4081	-3707	345	100	205	133	133	133
470	Copertura	48-50	0	1549	-697	618	426	501	426	426	426
			66	1445	-801	514	322	397	322	322	322
			132	1342	-905	410	218	293	218	218	218
471	Copertura	49-51	0	6705	-5892	680	212	442	346	346	346
			66	6602	-5996	577	108	339	243	243	243
			132	6498	-6100	473	4	235	139	139	139
472	Copertura	50-52	0	2264	-1404	700	397	519	430	430	430
			66	2160	-1508	596	293	415	326	326	326
			132	2057	-1611	492	189	312	223	223	223
473	Copertura	51-53	0	4869	-4192	528	209	364	300	306	306
			66	4765	-4296	424	105	261	197	202	202
			132	4661	-4399	320	2	157	93	99	99
474	Copertura	52-54	0	2039	-1716	519	94	318	233	257	257
			66	1935	-1819	416	-9	215	130	154	154

			132	1832	-1923	312	-113	111	26	50	50
475	Copertura	53-55	0	6312	-6301	129	-218	27	-52	27	27
			66	6208	-6405	26	-322	-77	-156	-77	-77
			132	6105	-6509	-78	-426	-181	-260	-181	-181
476	Copertura	54-56	0	1509	-1687	-48	-198	-48	-113	-48	-48
			66	1405	-1791	-152	-302	-152	-216	-152	-152
			132	1302	-1895	-255	-405	-255	-320	-255	-255
477	Copertura	55-57	0	1226	-2586	-680	-1125	-680	-846	-680	-680
			80	1101	-2711	-805	-1250	-805	-971	-805	-805
			159	976	-2836	-930	-1375	-930	-1096	-930	-930
478	Copertura	56-70	0	918	-2355	-718	-1198	-718	-892	-718	-718
			80	793	-2480	-843	-1322	-843	-1017	-843	-843
			159	668	-2605	-968	-1447	-968	-1141	-968	-968
479	Copertura	57-58	0	1833	-1834	378	-347	97	-48	0	0
			83	1614	-2053	91	-634	-168	-313	-220	-220
			166	1394	-2272	-195	-921	-433	-578	-439	-439
480	Copertura	58-59	0	1252	-1487	39	-258	-69	-128	-118	-118
			69	1070	-1709	-199	-497	-289	-348	-300	-300
			138	888	-1946	-437	-735	-482	-568	-482	-482
481	Copertura	59-60	0	1461	-1309	354	-132	151	54	76	76
			69	1279	-1491	116	-370	-69	-167	-106	-106
			138	1097	-1673	-122	-608	-288	-387	-288	-288
482	Copertura	60-61	0	1170	-826	394	41	234	163	172	172
			69	988	-1008	156	-197	14	-57	-10	-10
			138	806	-1190	-82	-435	-192	-277	-192	-192
483	Copertura	61-62	0	1918	-1345	634	72	381	269	286	286
			69	1736	-1527	396	-166	161	49	104	104
			138	1554	-1709	158	-404	-59	-171	-78	-78
484	Copertura	62-63	0	1096	-525	481	233	356	285	285	285
			69	914	-707	243	-5	135	86	103	103
			138	732	-889	5	-243	-79	-134	-79	-79
485	Copertura	63-64	0	1226	-865	419	54	255	181	181	181
			69	1044	-1047	181	-184	35	-38	-1	-1
			138	862	-1229	-57	-422	-183	-258	-183	-183
486	Copertura	64-65	0	889	-736	241	-7	132	77	77	77
			69	707	-918	3	-245	-88	-138	-105	-105
			138	525	-1100	-235	-483	-287	-358	-287	-287
487	Copertura	65-66	0	1771	-1623	400	-162	167	55	74	74
			69	1589	-1805	162	-400	-53	-165	-108	-108
			138	1407	-1987	-76	-638	-273	-385	-290	-290
488	Copertura	66-67	0	1212	-827	435	85	278	193	193	193
			69	1030	-1009	197	-153	58	-12	11	11
			138	848	-1191	-41	-391	-162	-232	-171	-171
489	Copertura	67-68	0	1657	-1077	609	126	389	290	290	290
			69	1475	-1259	371	-112	169	72	108	108
			138	1293	-1441	133	-350	-52	-148	-74	-74
490	Copertura	68-69	0	1640	-668	738	442	573	486	486	486
			69	1458	-850	500	204	353	294	304	304
			138	1276	-1032	262	-34	133	73	122	122
491	Copertura	69-70	0	2255	-1356	935	206	590	444	450	450
			83	2036	-1575	648	-81	325	179	230	230
			166	1817	-1794	361	-368	60	-86	11	11
492	Copertura	1-1	0	3222	-3267	35	-108	-9	-37	-18	-18
			220	3222	-3267	79	-130	0	-42	-18	-18
			440	3222	-3267	168	-175	18	-51	-18	-18

493	Copertura	2-2	0	914	-968	6	-159	-26	-59	-30	-30
			220	857	-928	-30	-73	-30	-42	-30	-30
			440	959	-928	102	-124	-7	-52	-30	-30
494	Copertura	3-3	0	396	-423	58	-154	5	-38	-7	-7
			220	333	-348	16	-71	-4	-21	-7	-7
			440	427	-311	99	-69	13	-21	-7	-7
495	Copertura	4-4	0	282	-285	63	-125	14	-24	2	2
			220	219	-209	22	-42	6	-7	2	2
			440	357	-185	129	-63	27	-11	2	2
496	Copertura	5-5	0	297	-293	53	-100	13	-18	3	3
			220	294	-284	11	-16	4	-1	3	3
			440	425	-284	154	-74	33	-13	3	3
497	Copertura	6-6	0	268	-264	43	-84	10	-15	2	2
			220	206	-202	5	-1	2	1	2	2
			440	434	-202	170	-84	35	-15	2	2
498	Copertura	7-7	0	249	-248	38	-76	8	-14	1	1
			220	234	-231	8	-4	2	0	1	1
			440	440	-231	178	-89	36	-17	1	1
499	Copertura	8-8	0	248	-251	39	-77	9	-14	1	1
			220	236	-234	7	-3	2	0	1	1
			440	443	-234	177	-88	36	-17	1	1
500	Copertura	9-9	0	191	-197	43	-83	10	-15	2	2
			220	164	-158	5	-1	2	1	2	2
			440	375	-158	171	-84	36	-15	2	2
501	Copertura	10-10	0	280	-291	54	-102	13	-18	3	3
			220	217	-216	12	-18	5	-1	3	3
			440	427	-204	152	-73	33	-12	3	3
502	Copertura	11-11	0	168	-189	65	-126	14	-24	2	2
			220	126	-117	23	-43	6	-7	2	2
			440	266	-117	127	-62	27	-11	2	2
503	Copertura	12-12	0	147	-375	61	-158	5	-39	-8	-8
			220	147	-249	20	-74	-3	-22	-8	-8
			440	231	-248	96	-66	12	-20	-8	-8
504	Copertura	13-13	0	155	-293	21	-174	-23	-62	-30	-30
			220	155	-216	-22	-89	-30	-45	-30	-30
			440	273	-215	86	-109	-10	-49	-30	-30
505	Copertura	57-57	0	3250	-3214	108	-34	38	10	18	18
			220	3250	-3214	130	-78	43	1	18	18
			440	3250	-3214	175	-167	51	-17	18	18
506	Copertura	58-58	0	1042	-842	159	-6	59	26	30	30
			220	913	-842	73	30	42	30	30	30
			440	907	-842	124	-101	52	7	30	30
507	Copertura	59-59	0	454	-267	155	-58	38	-5	7	7
			220	328	-267	71	-16	21	4	7	7
			440	294	-267	69	-99	21	-13	7	7
508	Copertura	60-60	0	332	-184	125	-63	24	-14	-2	-2
			220	206	-181	41	-21	7	-6	-2	-2
			440	216	-181	64	-129	11	-27	-2	-2
509	Copertura	61-61	0	399	-277	100	-53	18	-13	-3	-3
			220	274	-255	17	-11	1	-4	-3	-3
			440	334	-255	74	-154	13	-33	-3	-3
510	Copertura	62-62	0	356	-253	82	-42	15	-10	-2	-2
			220	230	-236	1	-4	-1	-2	-2	-2
			440	335	-236	85	-171	16	-36	-2	-2
511	Copertura	63-6	0	352	-258	77	-38	15	-8	-1	-1

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			220	235	-239	4	-7	0	-2	-1	-1
			440	351	-239	89	-177	17	-36	-1	-1
512	Copertur a	64-6 4	0	298	-230	77	-39	15	-8	-1	-1
			220	228	-230	3	-7	0	-2	-1	-1
			440	302	-230	88	-177	17	-36	-1	-1
513	Copertur a	65-6 5	0	267	-177	83	-43	15	-10	-2	-2
			220	175	-177	1	-4	-1	-2	-2	-2
			440	261	-177	84	-170	15	-35	-2	-2
514	Copertur a	66-6 6	0	259	-168	102	-54	18	-13	-3	-3
			220	165	-168	18	-12	1	-5	-3	-3
			440	215	-168	73	-152	12	-33	-3	-3
515	Copertur a	67-6 7	0	287	-159	126	-64	24	-14	-2	-2
			220	161	-122	43	-23	7	-6	-2	-2
			440	195	-102	62	-127	11	-27	-2	-2
516	Copertur a	68-6 8	0	289	-120	158	-61	39	-5	8	8
			220	163	-110	75	-19	22	4	8	8
			440	162	-110	66	-96	21	-12	8	8
517	Copertur a	69-6 9	0	374	-181	176	-19	64	25	32	32
			220	247	-144	90	24	47	32	32	32
			440	323	-144	111	-84	51	12	32	32
518	Copertur a	1-74	0	3	3	3	3	3	3	3	3
			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
519	Copertur a	74-2	0	3	3	3	3	3	3	3	3
			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
520	Copertur a	6-71	0	3	2	2	2	2	2	2	2
			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
521	Copertur a	71-7	0	3	2	2	2	2	2	2	2
			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
522	Copertur a	9-72	0	3	2	2	2	2	2	2	2
			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
523	Copertur a	72-1 0	0	3	2	2	2	2	2	2	2
			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
524	Copertur a	73-1 3	0	3	3	3	3	3	3	3	3
			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
525	Copertur a	14-7 3	0	3	3	3	3	3	3	3	3
			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
526	Copertur a	57-7 5	0	3	3	3	3	3	3	3	3
			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
527	Copertur a	75-5 8	0	3	3	3	3	3	3	3	3
			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
528	Copertur a	77-6 1	0	3	2	2	2	2	2	2	2
			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
529	Copertur a	62-7 7	0	3	2	2	2	2	2	2	2

			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
530	Copertura	65-78	0	3	2	2	2	2	2	2	2
			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
531	Copertura	78-66	0	3	2	2	2	2	2	2	2
			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
532	Copertura	69-76	0	3	3	3	3	3	3	3	3
			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
533	Copertura	76-70	0	3	3	3	3	3	3	3	3
			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
534	Copertura	1-74	0	3	3	3	3	3	3	3	3
			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
535	Copertura	74-2	0	3	3	3	3	3	3	3	3
			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
536	Copertura	6-71	0	3	2	2	2	2	2	2	2
			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
537	Copertura	71-7	0	3	2	2	2	2	2	2	2
			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
538	Copertura	9-72	0	3	2	2	2	2	2	2	2
			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
539	Copertura	72-10	0	3	2	2	2	2	2	2	2
			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
540	Copertura	73-13	0	3	3	3	3	3	3	3	3
			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
541	Copertura	14-73	0	3	3	3	3	3	3	3	3
			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
542	Copertura	15-125	0	2238	-2535	-110	-280	-148	-190	-148	-148
			75	2060	-2759	-327	-524	-327	-397	-327	-327
			150	1881	-2999	-505	-781	-505	-612	-505	-505
543	Copertura	127-16	0	2786	-1703	834	542	655	542	542	542
			75	2607	-1881	578	363	440	363	363	363
			150	2429	-2060	330	165	232	184	184	184
544	Copertura	17-129	0	2174	-2186	64	-187	4	-46	-6	-6
			75	2006	-2353	-157	-408	-174	-242	-174	-174
			150	1838	-2521	-341	-629	-341	-437	-341	-341
545	Copertura	130-18	0	2775	-2093	631	341	437	341	341	341
			75	2608	-2261	410	159	242	173	173	173
			150	2440	-2429	189	-62	47	-3	6	6
546	Copertura	19-135	0	3540	-3564	154	-289	17	-72	-12	-12
			75	3372	-3732	-67	-509	-178	-267	-180	-180
			150	3205	-3899	-287	-730	-347	-462	-347	-347
547	Copertura	134-20	0	4029	-3340	732	289	460	345	345	345
			75	3861	-3507	512	68	265	176	177	177

			150	3694	-3675	291	-153	70	-19	9	9
548	Copertura	21-136	0	3861	-3928	200	-386	7	-111	-33	-33
			75	3693	-4095	-21	-607	-189	-306	-201	-201
			150	3525	-4263	-242	-828	-369	-501	-369	-369
549	Copertura	138-22	0	4260	-3524	834	250	502	368	368	368
			75	4092	-3692	613	29	306	190	200	200
			150	3925	-3859	392	-192	111	-6	33	33
550	Copertura	23-141	0	4096	-4181	234	-443	5	-130	-43	-43
			75	3928	-4349	13	-663	-190	-325	-210	-210
			150	3760	-4516	-208	-884	-378	-521	-378	-378
551	Copertura	142-24	0	4656	-3901	897	214	523	377	377	377
			75	4488	-4069	676	-6	328	191	210	210
			150	4321	-4236	455	-227	132	-4	42	42
552	Copertura	25-145	0	5288	-5384	234	-466	0	-140	-48	-48
			75	5120	-5551	13	-687	-195	-335	-216	-216
			150	4953	-5719	-208	-908	-383	-530	-383	-383
553	Copertura	146-26	0	5558	-4799	926	191	530	379	379	379
			75	5390	-4967	705	-30	335	188	212	212
			150	5223	-5135	484	-251	140	-7	44	44
554	Copertura	150-27	0	6076	-5324	938	171	530	376	376	376
			75	5908	-5492	717	-50	334	181	208	208
			150	5741	-5660	496	-271	139	-14	40	40
555	Copertura	28-149	0	5670	-5756	243	-468	7	-136	-43	-43
			75	5502	-5924	22	-689	-189	-331	-211	-211
			150	5334	-6091	-198	-909	-378	-526	-378	-378
556	Copertura	154-29	0	6459	-5721	932	160	522	368	369	369
			75	6291	-5888	711	-61	327	173	201	201
			150	6123	-6056	490	-282	132	-23	34	34
557	Copertura	30-153	0	6240	-6306	278	-468	23	-127	-33	-33
			75	6072	-6474	58	-689	-173	-322	-201	-201
			150	5905	-6641	-163	-909	-368	-517	-368	-368
558	Copertura	158-31	0	6517	-5782	926	159	520	367	368	368
			75	6349	-5949	705	-62	325	171	200	200
			150	6181	-6117	484	-282	129	-24	32	32
559	Copertura	32-157	0	6446	-6508	285	-468	26	-125	-31	-31
			75	6279	-6676	64	-689	-170	-320	-199	-199
			150	6111	-6844	-156	-910	-365	-516	-366	-366
560	Copertura	162-33	0	6712	-5980	915	161	516	365	366	366
			75	6544	-6148	695	-60	321	170	198	198
			150	6376	-6315	474	-281	126	-25	31	31
561	Copertura	34-161	0	6279	-6342	276	-464	23	-125	-31	-31
			75	6111	-6509	55	-685	-172	-320	-199	-199
			150	5944	-6677	-166	-906	-367	-515	-367	-367
562	Copertura	166-35	0	6627	-5897	903	165	513	365	365	365
			75	6459	-6065	682	-56	317	170	197	197
			150	6292	-6233	461	-276	122	-25	29	29
563	Copertura	36-165	0	6419	-6482	263	-458	21	-123	-32	-32
			75	6251	-6649	42	-678	-175	-319	-199	-199
			150	6083	-6817	-179	-899	-367	-514	-367	-367
564	Copertura	170-37	0	6785	-6057	890	170	510	364	364	364
			75	6617	-6224	669	-51	314	170	196	196
			150	6449	-6392	448	-271	119	-25	29	29
565	Copertura	38-169	0	6343	-6402	253	-449	20	-120	-30	-30
			75	6175	-6570	32	-670	-175	-315	-197	-197
			150	6007	-6738	-188	-890	-365	-511	-365	-365

566	Copertura	175-39	0	6664	-5937	877	176	506	363	363	363
			75	6496	-6105	656	-45	311	171	196	196
			150	6328	-6272	435	-266	116	-25	28	28
567	Copertura	40-173	0	6052	-6103	263	-444	26	-115	-25	-25
			75	5885	-6270	42	-664	-169	-310	-193	-193
			150	5717	-6438	-179	-885	-360	-505	-360	-360
568	Copertura	178-41	0	5952	-5217	877	186	510	368	368	368
			75	5785	-5385	656	-35	315	177	200	200
			150	5617	-5552	435	-256	119	-19	32	32
569	Copertura	42-177	0	6025	-6075	306	-462	36	-118	-25	-25
			75	5858	-6243	85	-683	-160	-313	-193	-193
			150	5690	-6410	-136	-904	-355	-509	-360	-360
570	Copertura	43-181	0	5706	-5776	291	-475	23	-130	-35	-35
			75	5538	-5944	70	-696	-172	-325	-203	-203
			150	5370	-6112	-151	-917	-367	-521	-371	-371
571	Copertura	182-44	0	6048	-5296	890	194	520	376	376	376
			75	5880	-5463	669	-27	325	185	208	208
			150	5712	-5631	449	-248	129	-10	41	41
572	Copertura	45-185	0	5269	-5343	236	-446	11	-126	-37	-37
			75	5102	-5510	15	-667	-185	-321	-204	-204
			150	4934	-5678	-205	-888	-372	-516	-372	-372
573	Copertura	186-46	0	5763	-5013	872	209	516	375	375	375
			75	5595	-5180	651	-12	321	188	207	207
			150	5428	-5348	430	-233	125	-7	40	40
574	Copertura	47-189	0	4743	-4822	197	-419	1	-123	-39	-39
			75	4576	-4990	-24	-640	-195	-318	-207	-207
			150	4408	-5157	-244	-861	-375	-514	-375	-375
575	Copertura	190-48	0	4849	-4106	846	229	508	372	372	372
			75	4681	-4273	625	8	312	189	204	204
			150	4514	-4441	404	-213	117	-7	36	36
576	Copertura	49-193	0	4100	-4168	166	-373	-1	-109	-34	-34
			75	3932	-4336	-54	-594	-196	-304	-202	-202
			150	3764	-4504	-275	-814	-370	-500	-370	-370
577	Copertura	195-50	0	4593	-3863	801	260	493	365	365	365
			75	4425	-4030	580	39	297	189	197	197
			150	4257	-4198	360	-182	102	-6	30	30
578	Copertura	51-197	0	3777	-3807	131	-283	10	-73	-15	-15
			75	3610	-3974	-89	-504	-182	-268	-182	-182
			150	3442	-4142	-310	-725	-350	-464	-350	-350
579	Copertura	199-52	0	3932	-3250	707	295	452	341	341	341
			75	3764	-3418	486	74	257	173	173	173
			150	3596	-3586	265	-147	61	-21	5	5
580	Copertura	53-201	0	2639	-2653	53	-184	1	-47	-7	-7
			75	2471	-2820	-168	-405	-175	-242	-175	-175
			150	2303	-2988	-342	-626	-342	-438	-342	-342
581	Copertura	202-54	0	2783	-2102	622	340	435	340	340	340
			75	2615	-2270	401	161	240	172	172	172
			150	2447	-2438	180	-59	44	-4	5	5
582	Copertura	55-205	0	2734	-3037	-114	-282	-152	-193	-152	-152
			75	2555	-3216	-330	-528	-330	-401	-330	-330
			150	2377	-3394	-509	-784	-509	-616	-509	-509
583	Copertura	206-56	0	3328	-2271	811	528	639	528	528	528
			75	3149	-2450	555	350	424	350	350	350
			150	2971	-2628	306	149	215	171	171	171
584	Copertura	57-7	0	3	3	3	3	3	3	3	3

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			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
585	Copertura	75-58	0	3	3	3	3	3	3	3	3
			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
586	Copertura	77-61	0	3	2	2	2	2	2	2	2
			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
587	Copertura	62-77	0	3	2	2	2	2	2	2	2
			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
588	Copertura	65-78	0	3	2	2	2	2	2	2	2
			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
589	Copertura	78-66	0	3	2	2	2	2	2	2	2
			115	0	0	0	0	0	0	0	0
			231	-2	-3	-2	-2	-2	-2	-2	-2
590	Copertura	69-76	0	3	3	3	3	3	3	3	3
			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
591	Copertura	76-70	0	3	3	3	3	3	3	3	3
			118	0	0	0	0	0	0	0	0
			235	-3	-3	-3	-3	-3	-3	-3	-3
592	Copertura	79-81	0	555	-511	117	-32	52	22	32	32
			80	547	-519	109	-40	44	14	24	24
			159	538	-528	100	-49	35	5	15	15
593	Copertura	80-82	0	541	-547	105	-59	38	5	18	18
			66	534	-554	98	-66	31	-2	11	11
			132	527	-561	91	-73	24	-9	4	4
594	Copertura	83-84	0	500	-526	88	-66	26	-5	10	10
			66	493	-533	81	-73	19	-12	3	3
			132	486	-540	74	-80	12	-19	-4	-4
595	Copertura	85-86	0	491	-524	86	-68	24	-7	8	8
			66	484	-531	79	-75	17	-14	1	1
			132	477	-538	72	-82	10	-21	-6	-6
596	Copertura	87-88	0	490	-513	100	-55	36	5	19	19
			66	483	-520	93	-62	29	-2	12	12
			132	477	-527	86	-69	22	-9	5	5
597	Copertura	89-90	0	493	-509	110	-46	45	14	26	26
			66	486	-516	103	-53	38	7	19	19
			132	479	-523	96	-60	31	0	12	12
598	Copertura	91-92	0	481	-490	111	-40	47	17	28	28
			66	474	-497	104	-47	40	10	22	22
			132	467	-504	97	-54	33	3	15	15
599	Copertura	93-94	0	489	-496	106	-47	42	11	24	24
			66	482	-503	99	-54	35	4	17	17
			132	475	-510	92	-61	28	-3	10	10
600	Copertura	95-96	0	487	-493	91	-56	31	2	15	15
			66	480	-500	84	-63	24	-5	8	8
			132	473	-507	77	-70	17	-12	1	1
601	Copertura	97-106	0	487	-503	77	-69	19	-10	5	5
			66	480	-510	70	-76	12	-17	-2	-2
			132	473	-517	63	-83	5	-24	-9	-9
602	Copertura	98-99	0	712	-736	127	-86	40	-3	16	16

			66	705	-743	120	-92	33	-10	9	9
			132	698	-750	113	-99	26	-17	2	2
603	Copertura	100-101	0	703	-759	115	-106	27	-17	5	5
			66	696	-766	108	-113	20	-24	-2	-2
			132	689	-773	101	-120	13	-31	-9	-9
604	Copertura	102-103	0	696	-755	117	-106	28	-16	6	6
			66	689	-762	110	-113	21	-23	-1	-1
			132	682	-769	103	-119	14	-30	-8	-8
605	Copertura	104-105	0	692	-744	122	-99	33	-11	10	10
			66	685	-751	115	-106	26	-18	3	3
			132	678	-758	108	-113	19	-25	-4	-4
606	Copertura	107-108	0	491	-535	66	-84	8	-22	-4	-4
			66	484	-542	59	-91	1	-29	-11	-11
			132	477	-549	52	-98	-6	-36	-18	-18
607	Copertura	109-110	0	345	-392	42	-68	0	-22	-8	-8
			80	336	-401	34	-77	-8	-30	-16	-16
			159	328	-409	25	-85	-17	-39	-25	-25
608	Copertura	111-112	0	695	-740	123	-99	34	-11	11	11
			66	688	-747	116	-105	27	-18	4	4
			132	681	-754	109	-112	20	-25	-3	-3
609	Copertura	113-114	0	695	-731	123	-98	34	-11	11	11
			66	688	-737	116	-105	27	-18	4	4
			132	681	-744	109	-112	20	-25	-3	-3
610	Copertura	115-116	0	705	-731	118	-104	30	-15	7	7
			66	698	-738	111	-111	23	-22	0	0
			132	691	-745	104	-118	16	-29	-7	-7
611	Copertura	117-118	0	716	-740	113	-106	26	-18	5	5
			66	709	-747	106	-113	19	-25	-2	-2
			132	702	-754	99	-120	12	-32	-9	-9
612	Copertura	119-120	0	712	-759	103	-114	18	-25	-2	-2
			66	705	-766	96	-121	11	-32	-8	-8
			132	698	-773	89	-128	4	-39	-15	-15
613	Copertura	121-122	0	687	-773	72	-131	-3	-44	-18	-18
			66	680	-780	65	-138	-10	-51	-25	-25
			132	673	-787	58	-145	-17	-58	-32	-32
614	Copertura	124-125	0	246	25	183	128	152	128	128	128
			99	237	16	174	119	143	119	119	119
			198	228	7	165	110	134	110	110	110
615	Copertura	125-127	0	3321	1436	2647	1841	2218	1841	1841	1841
			775	401	-409	-2	-8	-4	-5	-4	-4
			1550	-1444	-3336	-1849	-2659	-1849	-2228	-1849	-1849
616	Copertura	126-127	0	249	10	183	128	152	128	128	128
			99	240	1	174	119	143	119	119	119
			198	231	-8	165	110	134	110	110	110
617	Copertura	128-129	0	256	-1	186	127	153	127	127	127
			99	246	-10	177	118	144	118	118	118
			198	237	-19	168	109	134	109	109	109
618	Copertura	129-130	0	3172	1347	2507	1732	2105	1732	1732	1732
			775	386	-386	16	-17	3	-4	0	0
			1550	-1347	-3172	-1733	-2508	-1733	-2105	-1733	-1733
619	Copertura	131-130	0	297	-43	186	127	152	127	127	127
			99	288	-52	177	118	143	118	118	118
			198	279	-61	168	109	134	109	109	109
620	Copertura	132-135	0	289	-32	191	129	154	129	129	129
			99	280	-41	182	120	145	120	120	120

			198	271	-50	172	111	136	111	111	111
621	Copertura	133-134	0	317	-60	191	129	154	129	129	129
			99	308	-69	182	120	145	120	120	120
			198	299	-78	173	111	136	111	111	111
622	Copertura	135-134	0	3173	1103	2518	1733	2105	1733	1733	1733
			775	630	-630	34	-34	7	-6	0	0
			1550	-1102	-3171	-1732	-2518	-1732	-2105	-1732	-1732
623	Copertura	137-136	0	320	-61	194	129	155	129	129	129
			99	311	-70	185	120	146	120	120	120
			198	302	-79	176	111	137	111	111	111
624	Copertura	136-138	0	3172	1037	2526	1733	2105	1733	1733	1733
			775	695	-695	46	-47	9	-9	0	0
			1550	-1037	-3172	-1732	-2526	-1732	-2105	-1732	-1732
625	Copertura	139-138	0	322	-64	194	129	155	129	129	129
			99	313	-73	185	120	146	120	120	120
			198	304	-82	176	111	137	111	111	111
626	Copertura	140-141	0	356	-97	195	130	156	130	130	130
			99	347	-106	186	121	146	121	121	121
			198	338	-115	177	112	137	112	112	112
627	Copertura	141-142	0	3172	991	2530	1733	2105	1733	1733	1733
			775	742	-742	54	-56	11	-11	0	0
			1550	-991	-3172	-1733	-2531	-1733	-2105	-1733	-1733
628	Copertura	143-142	0	351	-92	196	130	156	130	130	130
			99	342	-101	187	121	146	121	121	121
			198	333	-110	178	112	137	112	112	112
629	Copertura	144-145	0	407	-147	197	130	156	130	130	130
			99	398	-156	188	121	147	121	121	121
			198	389	-165	178	112	138	112	112	112
630	Copertura	145-146	0	3206	808	2533	1733	2105	1733	1733	1733
			775	925	-925	58	-59	12	-12	0	0
			1550	-807	-3173	-1732	-2533	-1732	-2105	-1732	-1732
631	Copertura	147-146	0	389	-130	197	130	156	130	130	130
			99	380	-139	188	121	147	121	121	121
			198	371	-148	179	112	138	112	112	112
632	Copertura	148-149	0	433	-173	197	130	156	130	130	130
			99	424	-182	188	121	147	121	121	121
			198	415	-191	179	112	138	112	112	112
633	Copertura	149-150	0	3173	723	2535	1733	2106	1733	1733	1733
			775	1011	-1010	60	-60	12	-12	0	0
			1550	-722	-3186	-1733	-2534	-1733	-2105	-1733	-1733
634	Copertura	151-150	0	415	-155	197	130	156	130	130	130
			99	405	-164	188	121	147	121	121	121
			198	396	-173	179	112	137	112	112	112
635	Copertura	152-153	0	443	-184	196	129	155	129	129	129
			99	434	-193	187	120	146	120	120	120
			198	425	-202	178	111	137	111	111	111
636	Copertura	153-154	0	3193	636	2536	1733	2106	1733	1733	1733
			775	1098	-1098	62	-63	12	-13	0	0
			1551	-636	-3173	-1733	-2537	-1733	-2106	-1733	-1733
637	Copertura	155-154	0	437	-178	197	130	155	130	130	130
			99	428	-187	188	120	146	120	120	120
			198	418	-196	179	111	137	111	111	111
638	Copertura	156-157	0	457	-198	196	129	155	129	129	129
			99	448	-207	187	120	146	120	120	120
			198	439	-216	178	111	137	111	111	111

639	Copertura	157-158	0	3173	615	2536	1734	2106	1734	1734	1734
			775	1119	-1119	62	-63	12	-13	0	0
			1551	-615	-3173	-1734	-2537	-1734	-2106	-1734	-1734
640	Copertura	159-158	0	444	-185	197	129	155	129	129	129
			99	435	-195	188	120	146	120	120	120
			198	426	-204	179	111	137	111	111	111
641	Copertura	160-161	0	444	-185	196	130	155	130	130	130
			99	435	-194	187	121	146	121	121	121
			198	426	-203	178	111	137	111	111	111
642	Copertura	161-162	0	3188	615	2536	1734	2106	1734	1734	1734
			776	1119	-1119	61	-62	12	-12	0	0
			1551	-615	-3180	-1734	-2536	-1734	-2106	-1734	-1734
643	Copertura	163-162	0	458	-199	197	129	155	129	129	129
			99	449	-208	187	120	146	120	120	120
			198	440	-217	178	111	137	111	111	111
644	Copertura	164-165	0	455	-195	196	130	156	130	130	130
			99	446	-204	187	121	146	121	121	121
			198	437	-214	178	112	137	112	112	112
645	Copertura	165-166	0	3174	621	2536	1734	2107	1734	1734	1734
			776	1113	-1113	60	-59	12	-12	0	0
			1551	-621	-3186	-1734	-2535	-1734	-2106	-1734	-1734
646	Copertura	167-166	0	447	-188	196	130	155	130	130	130
			99	438	-197	187	120	146	120	120	120
			198	429	-206	178	111	137	111	111	111
647	Copertura	168-169	0	456	-197	196	130	156	130	130	130
			99	447	-206	187	121	147	121	121	121
			198	438	-215	178	112	137	112	112	112
648	Copertura	169-170	0	3175	611	2536	1734	2107	1734	1734	1734
			776	1123	-1123	59	-58	12	-11	0	0
			1552	-611	-3174	-1734	-2534	-1734	-2107	-1734	-1734
649	Copertura	171-170	0	457	-197	196	130	155	130	130	130
			99	448	-206	187	121	146	121	121	121
			198	438	-216	178	111	137	111	111	111
650	Copertura	172-173	0	437	-178	196	130	155	130	130	130
			99	428	-187	187	120	146	120	120	120
			198	419	-196	178	111	137	111	111	111
651	Copertura	173-175	0	3175	650	2535	1734	2107	1734	1734	1734
			776	1084	-1085	59	-57	12	-12	0	0
			1552	-650	-3175	-1735	-2535	-1735	-2107	-1735	-1735
652	Copertura	174-175	0	453	-193	196	130	156	130	130	130
			99	443	-202	187	121	146	121	121	121
			198	434	-211	178	112	137	112	112	112
653	Copertura	176-177	0	423	-164	196	130	155	130	130	130
			99	414	-173	187	121	146	121	121	121
			198	405	-182	178	111	137	111	111	111
654	Copertura	177-178	0	3175	744	2537	1735	2107	1735	1735	1735
			776	991	-991	60	-61	12	-12	0	0
			1552	-744	-3176	-1735	-2538	-1735	-2107	-1735	-1735
655	Copertura	179-178	0	449	-190	196	130	156	130	130	130
			99	440	-199	187	121	147	121	121	121
			198	431	-208	178	112	137	112	112	112
656	Copertura	180-181	0	419	-160	196	129	155	129	129	129
			99	410	-169	187	120	146	120	120	120
			198	401	-178	178	111	137	111	111	111
657	Copertura	181-	0	3171	742	2533	1732	2104	1732	1732	1732

	a	182									
			775	990	-990	60	-62	12	-13	0	0
			1550	-743	-3173	-1733	-2535	-1733	-2105	-1733	-1733
658	Copertura	183-182	0	419	-159	196	130	156	130	130	130
			99	410	-168	187	121	147	121	121	121
			198	400	-177	178	112	138	112	112	112
659	Copertura	184-185	0	402	-144	195	129	155	129	129	129
			99	393	-153	186	120	146	120	120	120
			198	384	-162	177	111	137	111	111	111
660	Copertura	185-186	0	3172	779	2531	1732	2105	1732	1732	1732
			775	954	-954	56	-54	11	-11	0	0
			1550	-779	-3199	-1733	-2530	-1733	-2105	-1733	-1733
661	Copertura	187-186	0	419	-160	195	130	156	130	130	130
			99	410	-169	186	121	146	121	121	121
			198	401	-178	177	111	137	111	111	111
662	Copertura	188-189	0	379	-120	195	130	155	130	130	130
			99	370	-129	186	121	146	121	121	121
			198	361	-138	177	111	137	111	111	111
663	Copertura	189-190	0	3172	917	2529	1733	2105	1733	1733	1733
			775	816	-815	51	-48	10	-9	0	0
			1550	-917	-3172	-1732	-2527	-1732	-2105	-1732	-1732
664	Copertura	191-190	0	379	-120	194	129	155	129	129	129
			99	370	-129	185	120	146	120	120	120
			198	361	-139	176	111	137	111	111	111
665	Copertura	192-193	0	338	-79	193	129	155	129	129	129
			99	329	-88	184	120	146	120	120	120
			198	320	-97	175	111	137	111	111	111
666	Copertura	193-195	0	3173	988	2524	1733	2105	1733	1733	1733
			775	745	-745	44	-41	9	-8	0	0
			1550	-987	-3171	-1732	-2522	-1732	-2104	-1732	-1732
667	Copertura	194-195	0	335	-77	193	129	155	129	129	129
			99	326	-86	184	120	146	120	120	120
			198	317	-95	175	111	137	111	111	111
668	Copertura	196-197	0	323	-65	191	129	155	129	129	129
			99	314	-74	182	120	146	120	120	120
			198	305	-83	172	111	136	111	111	111
669	Copertura	197-199	0	3173	1087	2518	1733	2106	1733	1733	1733
			775	647	-646	32	-30	7	-5	1	1
			1550	-1086	-3174	-1732	-2515	-1732	-2104	-1732	-1732
670	Copertura	198-199	0	296	-39	190	128	154	128	128	128
			99	287	-48	181	119	145	119	119	119
			198	277	-57	172	110	136	110	110	110
671	Copertura	200-201	0	318	-64	186	127	153	127	127	127
			99	309	-73	177	118	144	118	118	118
			198	300	-82	168	109	135	109	109	109
672	Copertura	201-202	0	3172	1321	2507	1733	2105	1733	1733	1733
			775	412	-412	16	-15	3	-3	0	0
			1550	-1321	-3172	-1733	-2507	-1733	-2105	-1733	-1733
673	Copertura	203-202	0	282	-28	185	127	153	127	127	127
			99	273	-37	176	118	143	118	118	118
			198	264	-46	167	109	134	109	109	109
674	Copertura	204-205	0	266	-10	184	128	153	128	128	128
			99	257	-19	175	119	144	119	119	119
			198	248	-28	166	110	134	110	110	110
675	Copertura	205-206	0	3325	1344	2650	1843	2221	1843	1843	1843

			775	497	-501	0	-4	-2	-3	-2	-2
			1550	-1348	-3332	-1847	-2655	-1847	-2225	-1847	-1847
676	Copertura	207-206	0	250	7	184	129	153	129	129	129
			99	241	-2	175	120	144	120	120	120
			198	232	-11	166	110	135	110	110	110
677	Copertura	79-14	0	407	-452	-1	-74	-20	-35	-23	-23
			125	448	-452	48	-98	-11	-40	-23	-23
			250	521	-452	97	-123	-1	-45	-23	-23
678	Copertura	124-15	0	1431	-1443	42	-55	4	-15	-4	-4
			155	1431	-1443	42	-55	4	-15	-4	-4
			310	1431	-1443	42	-55	4	-15	-4	-4
679	Copertura	80-16	0	329	-349	25	-62	-5	-22	-10	-10
			45	329	-349	25	-62	-5	-22	-10	-10
			90	329	-349	25	-62	-5	-22	-10	-10
680	Copertura	128-17	0	1424	-1433	44	-53	6	-14	-3	-3
			155	1424	-1433	44	-53	6	-14	-3	-3
			310	1424	-1433	44	-53	6	-14	-3	-3
681	Copertura	82-18	0	537	-479	81	-92	10	-25	-7	-7
			43	537	-479	81	-92	10	-25	-7	-7
			85	537	-479	81	-92	10	-25	-7	-7
682	Copertura	132-19	0	1436	-1441	46	-52	8	-12	-2	-2
			155	1436	-1441	46	-52	8	-12	-2	-2
			310	1436	-1441	46	-52	8	-12	-2	-2
683	Copertura	83-20	0	391	-382	44	-67	2	-20	-8	-8
			43	391	-382	44	-67	2	-20	-8	-8
			85	391	-382	44	-67	2	-20	-8	-8
684	Copertura	137-21	0	1441	-1443	48	-50	9	-11	-1	-1
			155	1441	-1443	48	-50	9	-11	-1	-1
			310	1441	-1443	48	-50	9	-11	-1	-1
685	Copertura	84-22	0	426	-382	68	-57	16	-9	3	3
			43	426	-382	68	-57	16	-9	3	3
			85	426	-382	68	-57	16	-9	3	3
686	Copertura	140-23	0	1443	-1443	50	-49	10	-10	0	0
			155	1443	-1443	50	-49	10	-10	0	0
			310	1443	-1443	50	-49	10	-10	0	0
687	Copertura	85-24	0	398	-378	43	-72	0	-23	-10	-10
			43	398	-378	43	-72	0	-23	-10	-10
			85	398	-378	43	-72	0	-23	-10	-10
688	Copertura	144-25	0	1441	-1442	49	-50	10	-10	0	0
			155	1441	-1442	49	-50	10	-10	0	0
			310	1441	-1442	49	-50	10	-10	0	0
689	Copertura	86-26	0	413	-370	68	-53	18	-6	5	5
			43	413	-370	68	-53	18	-6	5	5
			85	413	-370	68	-53	18	-6	5	5
690	Copertura	87-27	0	389	-386	25	-93	-17	-41	-25	-25
			43	389	-386	25	-93	-17	-41	-25	-25
			85	389	-386	25	-93	-17	-41	-25	-25
691	Copertura	148-28	0	1450	-1430	62	-36	21	2	10	10
			155	1450	-1430	62	-36	21	2	10	10
			310	1450	-1430	62	-36	21	2	10	10
692	Copertura	88-29	0	404	-367	63	-56	14	-10	2	2
			43	404	-367	63	-56	14	-10	2	2
			85	404	-367	63	-56	14	-10	2	2
693	Copertura	152-30	0	1470	-1443	68	-32	26	6	13	13
			155	1470	-1443	68	-32	26	6	13	13

			310	1470	-1443	68	-32	26	6	13	13
694	Copertura	89-31	0	399	-397	27	-98	-19	-43	-27	-27
			43	399	-397	27	-98	-19	-43	-27	-27
			85	399	-397	27	-98	-19	-43	-27	-27
695	Copertura	156-32	0	1470	-1439	70	-30	28	8	15	15
			155	1470	-1439	70	-30	28	8	15	15
			310	1470	-1439	70	-30	28	8	15	15
696	Copertura	90-33	0	395	-369	43	-74	-3	-26	-12	-12
			43	395	-369	43	-74	-3	-26	-12	-12
			85	395	-369	43	-74	-3	-26	-12	-12
697	Copertura	160-34	0	1476	-1442	72	-27	30	10	17	17
			155	1476	-1442	72	-27	30	10	17	17
			310	1476	-1442	72	-27	30	10	17	17
698	Copertura	91-35	0	381	-384	24	-98	-20	-45	-28	-28
			43	381	-384	24	-98	-20	-45	-28	-28
			85	381	-384	24	-98	-20	-45	-28	-28
699	Copertura	164-36	0	1480	-1442	74	-25	32	12	19	19
			155	1480	-1442	74	-25	32	12	19	19
			310	1480	-1442	74	-25	32	12	19	19
700	Copertura	92-37	0	368	-347	33	-75	-8	-30	-17	-17
			43	368	-347	33	-75	-8	-30	-17	-17
			85	368	-347	33	-75	-8	-30	-17	-17
701	Copertura	168-38	0	1484	-1443	77	-22	34	14	21	21
			155	1484	-1443	77	-22	34	14	21	21
			310	1484	-1443	77	-22	34	14	21	21
702	Copertura	93-39	0	376	-365	45	-70	1	-22	-9	-9
			43	376	-365	45	-70	1	-22	-9	-9
			85	376	-365	45	-70	1	-22	-9	-9
703	Copertura	172-40	0	1490	-1446	79	-21	36	16	22	22
			155	1490	-1446	79	-21	36	16	22	22
			310	1490	-1446	79	-21	36	16	22	22
704	Copertura	94-41	0	396	-378	31	-91	-15	-39	-23	-23
			43	396	-378	31	-91	-15	-39	-23	-23
			85	396	-378	31	-91	-15	-39	-23	-23
705	Copertura	176-42	0	1488	-1439	82	-17	39	19	25	25
			155	1488	-1439	82	-17	39	19	25	25
			310	1488	-1439	82	-17	39	19	25	25
706	Copertura	180-43	0	1428	-1428	49	-49	10	-9	0	0
			155	1428	-1428	49	-49	10	-9	0	0
			310	1428	-1428	49	-49	10	-9	0	0
707	Copertura	95-44	0	393	-360	70	-49	22	-2	9	9
			43	393	-360	70	-49	22	-2	9	9
			85	393	-360	70	-49	22	-2	9	9
708	Copertura	184-45	0	1439	-1439	50	-49	10	-10	0	0
			155	1439	-1439	50	-49	10	-10	0	0
			310	1439	-1439	50	-49	10	-10	0	0
709	Copertura	96-46	0	384	-388	23	-90	-19	-42	-27	-27
			43	384	-388	23	-90	-19	-42	-27	-27
			85	384	-388	23	-90	-19	-42	-27	-27
710	Copertura	188-47	0	1438	-1436	50	-48	11	-9	1	1
			155	1438	-1436	50	-48	11	-9	1	1
			310	1438	-1436	50	-48	11	-9	1	1
711	Copertura	97-48	0	402	-380	62	-63	12	-12	0	0
			43	402	-380	62	-63	12	-12	0	0
			85	402	-380	62	-63	12	-12	0	0

712	Copertura	192-49	0	1438	-1436	51	-47	12	-8	1	1
			155	1438	-1436	51	-47	12	-8	1	1
			310	1438	-1436	51	-47	12	-8	1	1
713	Copertura	106-50	0	389	-365	57	-48	13	-8	2	2
			43	389	-365	57	-48	13	-8	2	2
			85	389	-365	57	-48	13	-8	2	2
714	Copertura	196-51	0	1437	-1432	53	-45	13	-7	3	3
			155	1437	-1432	53	-45	13	-7	3	3
			310	1437	-1432	53	-45	13	-7	3	3
715	Copertura	107-52	0	423	-392	66	-66	14	-12	1	1
			43	423	-392	66	-66	14	-12	1	1
			85	423	-392	66	-66	14	-12	1	1
716	Copertura	200-53	0	1428	-1420	54	-43	14	-5	4	4
			155	1428	-1420	54	-43	14	-5	4	4
			310	1428	-1420	54	-43	14	-5	4	4
717	Copertura	108-54	0	413	-356	75	-28	30	9	16	16
			43	413	-356	75	-28	30	9	16	16
			85	413	-356	75	-28	30	9	16	16
718	Copertura	204-55	0	1437	-1427	56	-41	16	-3	5	5
			155	1437	-1427	56	-41	16	-3	5	5
			310	1437	-1427	56	-41	16	-3	5	5
719	Copertura	109-56	0	496	-427	97	-97	24	-15	2	2
			43	496	-427	97	-97	24	-15	2	2
			85	496	-427	97	-97	24	-15	2	2
720	Copertura	110-70	0	390	-303	85	-7	46	28	34	34
			43	403	-303	94	-24	48	24	34	34
			85	415	-303	102	-40	49	21	34	34
721	Copertura	14-79	0	532	-578	20	-101	-17	-41	-23	-23
			95	532	-578	29	-105	-15	-42	-23	-23
			190	569	-578	55	-118	-10	-45	-23	-23
722	Copertura	15-124	0	1317	-1316	48	-46	11	-8	1	1
			65	1317	-1316	48	-46	11	-8	1	1
			130	1317	-1316	48	-46	11	-8	1	1
723	Copertura	16-126	0	264	-229	43	-15	21	10	14	14
			65	264	-229	43	-15	21	10	14	14
			130	264	-229	43	-15	21	10	14	14
724	Copertura	17-128	0	1306	-1314	43	-50	7	-12	-2	-2
			65	1306	-1314	43	-50	7	-12	-2	-2
			130	1306	-1314	43	-50	7	-12	-2	-2
725	Copertura	18-131	0	365	-339	48	-63	5	-18	-5	-5
			65	365	-339	48	-63	5	-18	-5	-5
			130	365	-339	48	-63	5	-18	-5	-5
726	Copertura	19-132	0	1319	-1326	45	-50	7	-12	-2	-2
			65	1319	-1326	45	-50	7	-12	-2	-2
			130	1319	-1326	45	-50	7	-12	-2	-2
727	Copertura	20-133	0	361	-333	48	-59	7	-14	-3	-3
			65	361	-333	48	-59	7	-14	-3	-3
			130	361	-333	48	-59	7	-14	-3	-3
728	Copertura	21-137	0	1326	-1329	47	-49	9	-10	-1	-1
			65	1326	-1329	47	-49	9	-10	-1	-1
			130	1326	-1329	47	-49	9	-10	-1	-1
729	Copertura	22-139	0	377	-335	58	-57	12	-11	0	0
			65	377	-335	58	-57	12	-11	0	0
			130	377	-335	58	-57	12	-11	0	0
730	Copertura	23-1	0	1330	-1331	48	-48	10	-9	0	0

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			65	1330	-1331	48	-48	10	-9	0	0
			130	1330	-1331	48	-48	10	-9	0	0
731	Copertura	24-1 43	0	375	-331	58	-56	13	-10	2	2
			65	375	-331	58	-56	13	-10	2	2
			130	375	-331	58	-56	13	-10	2	2
732	Copertura	25-1 44	0	1330	-1331	48	-48	9	-10	0	0
			65	1330	-1331	48	-48	9	-10	0	0
			130	1330	-1331	48	-48	9	-10	0	0
733	Copertura	26-1 47	0	384	-332	73	-42	25	2	11	11
			65	384	-332	73	-42	25	2	11	11
			130	384	-332	73	-42	25	2	11	11
734	Copertura	27-1 51	0	394	-331	89	-25	40	17	25	25
			65	394	-331	89	-25	40	17	25	25
			130	394	-331	89	-25	40	17	25	25
735	Copertura	28-1 48	0	1304	-1388	0	-95	-32	-51	-36	-36
			65	1304	-1388	0	-95	-32	-51	-36	-36
			130	1304	-1388	0	-95	-32	-51	-36	-36
736	Copertura	29-1 55	0	455	-335	119	5	66	43	46	46
			65	455	-335	119	5	66	43	46	46
			130	455	-335	119	5	66	43	46	46
737	Copertura	30-1 52	0	1312	-1427	-16	-112	-47	-67	-49	-49
			65	1312	-1427	-16	-112	-47	-67	-49	-49
			130	1312	-1427	-16	-112	-47	-67	-49	-49
738	Copertura	31-1 59	0	459	-337	119	5	67	44	48	48
			65	459	-337	119	5	67	44	48	48
			130	459	-337	119	5	67	44	48	48
739	Copertura	32-1 56	0	1304	-1429	-23	-118	-52	-71	-53	-53
			65	1304	-1429	-23	-118	-52	-71	-53	-53
			130	1304	-1429	-23	-118	-52	-71	-53	-53
740	Copertura	33-1 63	0	464	-351	128	21	76	55	56	56
			65	464	-351	128	21	76	55	56	56
			130	464	-351	128	21	76	55	56	56
741	Copertura	34-1 60	0	1302	-1440	-30	-124	-58	-78	-58	-58
			65	1302	-1440	-30	-124	-58	-78	-58	-58
			130	1302	-1440	-30	-124	-58	-78	-58	-58
742	Copertura	35-1 67	0	502	-383	137	17	80	56	59	59
			65	502	-383	137	17	80	56	59	59
			130	502	-383	137	17	80	56	59	59
743	Copertura	36-1 64	0	1302	-1452	-37	-131	-64	-84	-64	-64
			65	1302	-1452	-37	-131	-64	-84	-64	-64
			130	1302	-1452	-37	-131	-64	-84	-64	-64
744	Copertura	37-1 71	0	522	-391	143	30	87	65	65	65
			65	522	-391	143	30	87	65	65	65
			130	522	-391	143	30	87	65	65	65
745	Copertura	38-1 68	0	1299	-1462	-44	-138	-69	-90	-69	-69
			65	1299	-1462	-44	-138	-69	-90	-69	-69
			130	1299	-1462	-44	-138	-69	-90	-69	-69
746	Copertura	39-1 74	0	538	-400	147	34	92	69	69	69
			65	538	-400	147	34	92	69	69	69
			130	538	-400	147	34	92	69	69	69
747	Copertura	40-1 72	0	1295	-1468	-50	-144	-74	-95	-74	-74
			65	1295	-1468	-50	-144	-74	-95	-74	-74
			130	1295	-1468	-50	-144	-74	-95	-74	-74
748	Copertura	41-1 79	0	473	-360	124	12	71	49	51	51

			65	473	-360	124	12	71	49	51	51
			130	473	-360	124	12	71	49	51	51
749	Copertura	42-176	0	1276	-1460	-57	-150	-78	-100	-78	-78
			65	1276	-1460	-57	-150	-78	-100	-78	-78
			130	1276	-1460	-57	-150	-78	-100	-78	-78
750	Copertura	43-180	0	1325	-1324	48	-47	10	-9	0	0
			65	1325	-1324	48	-47	10	-9	0	0
			130	1325	-1324	48	-47	10	-9	0	0
751	Copertura	44-183	0	410	-347	90	-25	40	17	25	25
			65	410	-347	90	-25	40	17	25	25
			130	410	-347	90	-25	40	17	25	25
752	Copertura	45-184	0	1336	-1335	48	-48	10	-9	0	0
			65	1336	-1335	48	-48	10	-9	0	0
			130	1336	-1335	48	-48	10	-9	0	0
753	Copertura	46-187	0	367	-348	57	-55	11	-11	0	0
			65	367	-348	57	-55	11	-11	0	0
			130	367	-348	57	-55	11	-11	0	0
754	Copertura	47-188	0	1336	-1334	49	-47	10	-9	1	1
			65	1336	-1334	49	-47	10	-9	1	1
			130	1336	-1334	49	-47	10	-9	1	1
755	Copertura	48-191	0	370	-347	61	-52	15	-7	3	3
			65	370	-347	61	-52	15	-7	3	3
			130	370	-347	61	-52	15	-7	3	3
756	Copertura	49-192	0	1336	-1333	50	-46	11	-8	2	2
			65	1336	-1333	50	-46	11	-8	2	2
			130	1336	-1333	50	-46	11	-8	2	2
757	Copertura	50-194	0	373	-351	61	-50	16	-6	4	4
			65	373	-351	61	-50	16	-6	4	4
			130	373	-351	61	-50	16	-6	4	4
758	Copertura	51-196	0	1332	-1327	51	-44	13	-6	3	3
			65	1332	-1327	51	-44	13	-6	3	3
			130	1332	-1327	51	-44	13	-6	3	3
759	Copertura	52-198	0	378	-348	65	-47	19	-4	6	6
			65	378	-348	65	-47	19	-4	6	6
			130	378	-348	65	-47	19	-4	6	6
760	Copertura	53-200	0	1318	-1312	51	-42	13	-6	3	3
			65	1318	-1312	51	-42	13	-6	3	3
			130	1318	-1312	51	-42	13	-6	3	3
761	Copertura	54-203	0	361	-333	60	-35	19	0	7	7
			65	361	-333	60	-35	19	0	7	7
			130	361	-333	60	-35	19	0	7	7
762	Copertura	55-204	0	1322	-1324	46	-47	9	-10	-1	-1
			65	1322	-1324	46	-47	9	-10	-1	-1
			130	1322	-1324	46	-47	9	-10	-1	-1
763	Copertura	56-207	0	367	-334	63	-44	19	-3	7	7
			65	367	-334	63	-44	19	-3	7	7
			130	367	-334	63	-44	19	-3	7	7
764	Copertura	70-123	0	430	-380	65	15	32	21	21	21
			95	430	-380	70	6	33	20	21	21
			190	445	-380	83	-20	36	15	21	21
765	Copertura	81-80	0	495	-465	66	-91	3	-28	-10	-10
			80	495	-465	66	-91	3	-28	-10	-10
			160	495	-465	66	-91	3	-28	-10	-10
766	Copertura	126-81	0	259	-279	9	-46	-8	-19	-10	-10
			30	259	-279	9	-46	-8	-19	-10	-10

			60	259	-279	9	-46	-8	-19	-10	-10
767	Copertura	98-82	0	377	-374	40	-62	2	-19	-6	-6
			82	377	-374	40	-62	2	-19	-6	-6
			165	377	-374	40	-62	2	-19	-6	-6
768	Copertura	99-83	0	421	-391	57	-64	9	-16	-3	-3
			82	421	-391	57	-64	9	-16	-3	-3
			165	421	-391	57	-64	9	-16	-3	-3
769	Copertura	100-84	0	408	-378	55	-60	10	-13	-1	-1
			82	408	-378	55	-60	10	-13	-1	-1
			165	408	-378	55	-60	10	-13	-1	-1
770	Copertura	101-85	0	416	-376	64	-55	16	-8	4	4
			82	416	-376	64	-55	16	-8	4	4
			165	416	-376	64	-55	16	-8	4	4
771	Copertura	102-86	0	405	-379	47	-71	1	-22	-9	-9
			82	405	-379	47	-71	1	-22	-9	-9
			165	405	-379	47	-71	1	-22	-9	-9
772	Copertura	103-87	0	408	-374	58	-60	10	-13	-1	-1
			82	408	-374	58	-60	10	-13	-1	-1
			165	408	-374	58	-60	10	-13	-1	-1
773	Copertura	104-88	0	395	-382	30	-88	-14	-37	-22	-22
			82	395	-382	30	-88	-14	-37	-22	-22
			165	395	-382	30	-88	-14	-37	-22	-22
774	Copertura	105-89	0	392	-371	39	-78	-6	-29	-15	-15
			82	392	-371	39	-78	-6	-29	-15	-15
			165	392	-371	39	-78	-6	-29	-15	-15
775	Copertura	111-90	0	413	-399	31	-94	-15	-40	-24	-24
			80	413	-399	31	-94	-15	-40	-24	-24
			160	413	-399	31	-94	-15	-40	-24	-24
776	Copertura	112-91	0	373	-356	30	-81	-11	-34	-19	-19
			82	373	-356	30	-81	-11	-34	-19	-19
			165	373	-356	30	-81	-11	-34	-19	-19
777	Copertura	113-92	0	386	-382	27	-93	-17	-41	-25	-25
			82	386	-382	27	-93	-17	-41	-25	-25
			165	386	-382	27	-93	-17	-41	-25	-25
778	Copertura	114-93	0	382	-377	23	-93	-19	-43	-27	-27
			82	382	-377	23	-93	-19	-43	-27	-27
			165	382	-377	23	-93	-19	-43	-27	-27
779	Copertura	115-94	0	397	-378	52	-68	6	-18	-5	-5
			82	397	-378	52	-68	6	-18	-5	-5
			165	397	-378	52	-68	6	-18	-5	-5
780	Copertura	116-95	0	387	-384	29	-85	-14	-37	-22	-22
			82	387	-384	29	-85	-14	-37	-22	-22
			165	387	-384	29	-85	-14	-37	-22	-22
781	Copertura	117-96	0	400	-378	64	-53	17	-7	4	4
			82	400	-378	64	-53	17	-7	4	4
			165	400	-378	64	-53	17	-7	4	4
782	Copertura	118-97	0	398	-379	56	-56	11	-12	-1	-1
			82	398	-379	56	-56	11	-12	-1	-1
			165	398	-379	56	-56	11	-12	-1	-1
783	Copertura	131-98	0	388	-372	48	-66	3	-19	-7	-7
			30	388	-372	48	-66	3	-19	-7	-7
			60	388	-372	48	-66	3	-19	-7	-7
784	Copertura	133-99	0	379	-359	49	-60	7	-15	-3	-3
			30	379	-359	49	-60	7	-15	-3	-3
			60	379	-359	49	-60	7	-15	-3	-3

785	Copertura	139-100	0	397	-364	60	-58	12	-11	1	1
			30	397	-364	60	-58	12	-11	1	1
			60	397	-364	60	-58	12	-11	1	1
786	Copertura	143-101	0	397	-360	60	-57	13	-10	2	2
			30	397	-360	60	-57	13	-10	2	2
			60	397	-360	60	-57	13	-10	2	2
787	Copertura	147-102	0	403	-356	75	-43	25	2	12	12
			30	403	-356	75	-43	25	2	12	12
			60	403	-356	75	-43	25	2	12	12
788	Copertura	151-103	0	380	-367	30	-88	-14	-37	-22	-22
			30	380	-367	30	-88	-14	-37	-22	-22
			60	380	-367	30	-88	-14	-37	-22	-22
789	Copertura	155-104	0	379	-359	38	-79	-7	-30	-16	-16
			30	379	-359	38	-79	-7	-30	-16	-16
			60	379	-359	38	-79	-7	-30	-16	-16
790	Copertura	159-105	0	380	-363	31	-87	-13	-36	-21	-21
			30	380	-363	31	-87	-13	-36	-21	-21
			60	380	-363	31	-87	-13	-36	-21	-21
791	Copertura	119-106	0	407	-379	62	-55	15	-8	3	3
			82	407	-379	62	-55	15	-8	3	3
			165	407	-379	62	-55	15	-8	3	3
792	Copertura	120-107	0	414	-376	66	-45	20	-2	7	7
			82	414	-376	66	-45	20	-2	7	7
			165	414	-376	66	-45	20	-2	7	7
793	Copertura	121-108	0	438	-387	75	-48	25	0	10	10
			82	438	-387	75	-48	25	0	10	10
			165	438	-387	75	-48	25	0	10	10
794	Copertura	122-109	0	387	-338	66	-19	27	10	15	15
			82	387	-338	66	-19	27	10	15	15
			165	387	-338	66	-19	27	10	15	15
795	Copertura	123-110	0	466	-403	83	-20	36	15	21	21
			82	491	-403	99	-52	39	9	21	21
			165	515	-403	115	-85	42	2	21	21
796	Copertura	163-111	0	360	-343	30	-81	-11	-33	-19	-19
			33	360	-343	30	-81	-11	-33	-19	-19
			65	360	-343	30	-81	-11	-33	-19	-19
797	Copertura	167-112	0	400	-384	30	-94	-16	-41	-24	-24
			30	400	-384	30	-94	-16	-41	-24	-24
			60	400	-384	30	-94	-16	-41	-24	-24
798	Copertura	171-113	0	375	-362	26	-91	-17	-40	-25	-25
			30	375	-362	26	-91	-17	-40	-25	-25
			60	375	-362	26	-91	-17	-40	-25	-25
799	Copertura	174-114	0	372	-370	24	-95	-20	-43	-27	-27
			30	372	-370	24	-95	-20	-43	-27	-27
			60	372	-370	24	-95	-20	-43	-27	-27
800	Copertura	179-115	0	378	-414	-10	-127	-50	-73	-53	-53
			30	378	-414	-10	-127	-50	-73	-53	-53
			60	378	-414	-10	-127	-50	-73	-53	-53
801	Copertura	183-116	0	428	-363	92	-26	41	18	25	25
			30	428	-363	92	-26	41	18	25	25
			60	428	-363	92	-26	41	18	25	25
802	Copertura	187-117	0	386	-366	58	-56	12	-11	0	0
			30	386	-366	58	-56	12	-11	0	0
			60	386	-366	58	-56	12	-11	0	0
803	Copertura	191-	0	390	-364	63	-54	16	-8	4	4

	a	118									
			30	390	-364	63	-54	16	-8	4	4
			60	390	-364	63	-54	16	-8	4	4
804	Copertura	194-119	0	395	-364	62	-51	16	-7	3	3
			30	395	-364	62	-51	16	-7	3	3
			60	395	-364	62	-51	16	-7	3	3
805	Copertura	198-120	0	402	-363	66	-49	19	-4	6	6
			30	402	-363	66	-49	19	-4	6	6
			60	402	-363	66	-49	19	-4	6	6
806	Copertura	203-121	0	391	-345	67	-33	24	4	11	11
			30	391	-345	67	-33	24	4	11	11
			60	391	-345	67	-33	24	4	11	11
807	Copertura	207-122	0	409	-350	75	-35	28	6	15	15
			30	409	-350	75	-35	28	6	15	15
			60	409	-350	75	-35	28	6	15	15

1.2.6 Involuppi dei diagrammi delle sollecitazioni: Momento Flettente X-Y.

I dati seguenti riportano i valori del Momento Flettente X-Y relativamente alle aste che definiscono la struttura ed in modo particolare:

Asta : numerazione interna dell'asta.
X : distanza dal nodo iniziale misurata lungo l'asse dell'asta.
Momento Flettente (M_{xy}) : valore del Momento Flettente X-Y nel punto considerato:
Max : valore massimo (rispetto al sistema di riferimento globale) dell'involuppo.
Min : valore minimo (rispetto al sistema di riferimento globale) dell'involuppo.
Comb : combinazione di appartenenza del valore considerato nell'involuppo.

Tabella 31.I

Momento Flettente (M_{xy}) [daNm]											
				SLU		SLE					
Asta	Imp.	Fili	X [cm]	Max	Min	Caratteristiche		Frequenti		Quasi Permanenti	
						Max	Min	Max	Min	Max	Min
1	Fondazione	1-2	0	171	-124	29	-2	12	6	8	8
			42	58	-40	13	8	9	8	8	8
			83	97	-81	17	-5	10	5	7	7
2	Fondazione	1-2	0	96	-81	17	-5	9	5	7	7
			42	88	-67	15	9	11	9	9	9
			83	95	-67	33	6	17	11	11	11
3	Fondazione	1-15	0	87	-65	30	6	19	14	14	14
			40	67	-57	9	4	6	5	5	5
			80	75	-88	12	-19	-2	-8	-5	-5
4	Fondazione	1-15	0	75	-88	12	-19	-2	-8	-5	-5
			40	45	-35	12	5	7	5	5	5
			80	89	-54	32	0	20	14	15	15
5	Fondazione	2-3	0	90	-66	32	2	15	9	9	9
			35	54	-42	8	5	6	5	5	5
			69	43	-66	13	-22	4	-3	1	1
6	Fondazione	2-3	0	43	-66	13	-22	4	-3	1	1
			35	22	-17	5	2	3	2	2	2
			69	85	-40	30	-8	9	2	4	4
7	Fondazione	3-4	0	80	-44	33	-11	9	1	3	3
			35	25	-20	4	2	2	2	2	2
			69	53	-89	15	-27	4	-5	1	1
8	Fondazione	3-4	0	52	-89	15	-27	4	-5	1	1
			35	20	-18	2	1	1	1	1	1
			69	90	-46	30	-13	7	-1	1	1

9	Fondazio ne	4-5	0	92	-44	33	-15	8	-2	1	1
			35	20	-18	2	1	1	1	1	1
			69	51	-92	16	-29	4	-5	1	1
10	Fondazio ne	4-5	0	51	-92	16	-29	4	-5	1	1
			35	23	-22	1	0	1	1	1	1
			69	78	-44	30	-14	7	-2	1	1
11	Fondazio ne	5-6	0	80	-42	33	-15	7	-3	1	1
			35	21	-21	2	0	1	1	1	1
			69	47	-90	17	-30	4	-5	1	1
12	Fondazio ne	5-6	0	47	-90	17	-30	4	-5	1	1
			35	20	-21	2	-2	1	0	0	0
			69	72	-34	26	-13	5	-2	0	0
13	Fondazio ne	6-7	0	98	-44	37	-18	8	-3	0	0
			35	15	-14	3	-1	0	0	0	0
			69	42	-86	16	-32	3	-7	0	0
14	Fondazio ne	6-7	0	41	-86	16	-32	3	-7	0	0
			35	14	-15	2	-1	0	0	0	0
			69	106	-52	37	-18	8	-3	0	0
15	Fondazio ne	7-8	0	72	-31	27	-13	6	-2	0	0
			35	19	-19	2	-1	1	0	0	0
			69	59	-64	17	-30	4	-5	1	1
16	Fondazio ne	7-8	0	59	-64	17	-30	4	-5	1	1
			35	18	-17	1	0	1	1	1	1
			69	83	-36	32	-15	7	-2	1	1
17	Fondazio ne	8-9	0	80	-34	31	-15	7	-2	1	1
			35	17	-16	2	0	1	0	0	0
			69	57	-60	15	-29	4	-5	1	1
18	Fondazio ne	8-9	0	57	-59	15	-29	4	-5	1	1
			35	17	-19	2	-1	1	0	0	0
			69	62	-33	25	-12	6	-2	1	1
19	Fondazio ne	9-10	0	79	-36	33	-16	7	-3	1	1
			35	16	-14	2	-1	1	0	0	0
			69	55	-61	14	-29	3	-6	0	0
20	Fondazio ne	9-10	0	55	-61	14	-29	3	-6	0	0
			35	18	-17	3	-1	1	0	0	0
			69	91	-49	35	-17	7	-3	0	0
21	Fondazio ne	10-1 1	0	63	-35	24	-12	5	-2	0	0
			35	18	-20	2	-2	1	0	1	1
			69	56	-58	16	-28	4	-4	1	1
22	Fondazio ne	10-1 1	0	56	-58	16	-28	4	-4	1	1
			35	17	-13	3	1	2	1	1	1
			69	73	-33	33	-14	8	-2	1	1
23	Fondazio ne	11-1 2	0	65	-31	30	-12	7	-1	1	1
			35	17	-14	2	1	1	1	1	1
			69	55	-55	15	-26	4	-5	1	1
24	Fondazio ne	11-1 2	0	55	-55	15	-26	4	-5	1	1
			35	19	-13	4	2	3	2	2	2
			69	71	-35	34	-10	10	1	3	3
25	Fondazio ne	12-1 3	0	64	-30	30	-7	10	2	4	4
			35	22	-15	5	3	3	3	3	3
			69	47	-45	13	-21	4	-3	1	1
26	Fondazio ne	12-1 3	0	47	-45	13	-21	4	-3	1	1
			35	23	-10	8	5	6	5	5	5
			69	72	-33	34	2	15	9	9	9
27	Fondazio	13-1	0	83	-42	34	5	17	11	11	11

	ne	4									
			42	47	-19	16	10	12	10	10	10
			83	66	-49	18	-4	11	6	8	8
28	Fondazio ne	13-1 4	0	66	-49	18	-4	11	6	8	8
			42	49	-27	13	8	10	8	8	8
			83	75	-45	28	-1	12	6	8	8
29	Fondazio ne	14-1 6	0	30	-60	-7	-31	-15	-20	-15	-15
			40	31	-42	-6	-10	-6	-7	-6	-6
			80	81	-75	17	-14	7	1	3	3
30	Fondazio ne	14-1 6	0	82	-75	17	-14	7	1	4	4
			40	24	-35	-5	-13	-6	-7	-6	-6
			80	62	-93	0	-31	-14	-20	-15	-15
31	Fondazio ne	15-1 7	0	105	-56	47	8	31	24	25	25
			33	21	-23	3	-1	1	0	0	0
			66	42	-89	-7	-45	-23	-30	-24	-24
32	Fondazio ne	15-1 7	0	42	-89	-7	-46	-23	-30	-24	-24
			33	36	-20	10	7	8	7	7	7
			66	112	-36	64	25	47	38	38	38
33	Fondazio ne	16-1 8	0	67	-115	-8	-46	-23	-31	-24	-24
			33	15	-16	0	-4	0	-1	-1	-1
			66	91	-46	44	7	29	22	23	23
34	Fondazio ne	16-1 8	0	91	-46	44	7	29	22	23	23
			33	12	-25	-6	-10	-6	-8	-6	-6
			66	57	-129	-24	-61	-36	-44	-36	-36
35	Fondazio ne	17-1 9	0	147	-60	77	28	55	44	44	44
			33	33	-16	10	7	8	7	7	7
			66	46	-106	-13	-56	-30	-38	-30	-30
36	Fondazio ne	17-1 9	0	46	-106	-13	-56	-30	-38	-30	-30
			33	28	-17	6	4	5	4	4	4
			66	134	-56	70	23	49	39	39	39
37	Fondazio ne	18-2 0	0	83	-167	-27	-74	-42	-53	-42	-42
			33	10	-23	-6	-9	-6	-8	-6	-6
			66	114	-56	55	12	37	29	29	29
38	Fondazio ne	18-2 0	0	115	-56	55	12	37	29	29	29
			33	8	-17	-5	-7	-5	-6	-5	-5
			66	70	-148	-23	-70	-39	-50	-39	-39
39	Fondazio ne	19-2 1	0	130	-61	65	17	44	35	35	35
			33	21	-19	2	1	1	1	1	1
			66	58	-121	-14	-60	-32	-41	-32	-32
40	Fondazio ne	19-2 1	0	58	-121	-14	-60	-32	-41	-32	-32
			33	19	-18	1	0	0	0	0	0
			66	127	-61	62	16	42	33	33	33
41	Fondazio ne	20-2 2	0	70	-139	-18	-65	-35	-45	-35	-35
			33	14	-17	-1	-2	-1	-1	-1	-1
			66	122	-59	60	14	41	32	32	32
42	Fondazio ne	20-2 2	0	122	-59	60	14	41	32	32	32
			33	16	-16	1	0	0	0	0	0
			66	67	-132	-15	-61	-32	-41	-32	-32
43	Fondazio ne	21-2 3	0	173	-100	70	16	47	36	36	36
			33	21	-14	5	3	4	3	3	3
			66	75	-134	-10	-58	-29	-38	-29	-29
44	Fondazio ne	21-2 3	0	75	-134	-10	-58	-29	-38	-29	-29
			33	26	-18	7	2	5	4	4	4
			66	194	-118	74	15	49	37	38	38
45	Fondazio ne	22-2 4	0	103	-175	-16	-70	-35	-46	-36	-36

			33	12	-18	-2	-5	-3	-4	-3	-3
			66	131	-73	58	10	38	28	29	29
46	Fondazio ne	22-2 4	0	131	-73	58	10	38	28	29	29
			33	10	-18	-2	-6	-4	-4	-4	-4
			66	110	-184	-15	-72	-36	-48	-37	-37
47	Fondazio ne	23-2 5	0	190	-122	68	12	44	33	34	34
			33	25	-19	5	1	4	3	3	3
			66	76	-132	-10	-54	-27	-36	-28	-28
48	Fondazio ne	23-2 5	0	76	-132	-10	-54	-27	-36	-28	-28
			33	48	-63	-5	-16	-9	-11	-9	-9
			66	114	-93	25	0	15	10	11	11
49	Fondazio ne	24-2 6	0	111	-177	-12	-65	-32	-43	-33	-33
			33	10	-15	-1	-5	-2	-3	-3	-3
			66	126	-71	53	11	35	27	27	27
50	Fondazio ne	24-2 6	0	126	-71	53	11	35	27	27	27
			33	45	-26	17	5	12	9	9	9
			66	71	-89	-1	-21	-9	-13	-9	-9
51	Fondazio ne	25-2 6	0	175	-186	2	-13	-4	-7	-5	-5
			49	76	-79	-1	-3	-1	-2	-1	-1
			97	98	-94	4	0	2	2	2	2
52	Fondazio ne	25-2 6	0	97	-93	3	0	2	2	2	2
			49	53	-52	3	-2	1	0	1	1
			97	55	-56	0	-2	-1	-1	-1	-1
53	Fondazio ne	25-2 6	0	56	-57	0	-2	-1	-1	-1	-1
			49	32	-32	1	-2	0	-1	0	0
			97	54	-53	1	-1	0	0	0	0
54	Fondazio ne	25-2 6	0	55	-54	1	-1	0	0	0	0
			49	32	-32	1	-1	0	0	0	0
			97	54	-52	2	-1	1	0	0	0
55	Fondazio ne	25-2 6	0	55	-53	1	-1	1	0	0	0
			49	31	-30	1	-1	0	0	0	0
			97	54	-52	2	-1	1	0	0	0
56	Fondazio ne	25-2 6	0	55	-53	2	-1	1	0	0	0
			49	30	-29	1	0	1	0	0	0
			97	54	-51	2	-1	1	0	0	0
57	Fondazio ne	25-2 6	0	54	-52	2	-1	1	0	0	0
			49	29	-28	1	0	1	0	0	0
			97	52	-51	2	-1	1	0	0	0
58	Fondazio ne	25-2 6	0	52	-51	2	-1	1	0	0	0
			49	28	-28	1	0	1	0	0	0
			97	51	-50	2	-1	1	0	0	0
59	Fondazio ne	25-2 6	0	52	-51	2	-1	1	0	0	0
			49	28	-27	1	0	1	0	0	0
			97	52	-51	2	0	1	0	1	1
60	Fondazio ne	25-2 6	0	52	-51	2	0	1	0	1	1
			49	27	-26	1	0	1	0	0	0
			97	51	-50	2	-1	1	0	0	0
61	Fondazio ne	25-2 6	0	51	-50	2	-1	1	0	0	0
			49	27	-26	1	0	0	0	0	0
			97	52	-51	2	-1	1	0	0	0
62	Fondazio ne	25-2 6	0	52	-51	2	-1	1	0	0	0
			49	27	-26	1	0	1	0	0	0
			97	52	-51	2	-1	1	0	0	0
63	Fondazio ne	25-2 6	0	52	-51	2	-1	1	0	0	0
			49	27	-27	1	0	1	0	0	0

			97	53	-51	2	-1	1	0	0	0
64	Fondazio ne	25-2 6	0	52	-51	2	-1	1	0	0	0
			49	28	-28	1	0	1	0	0	0
			97	55	-52	2	-1	1	0	0	0
65	Fondazio ne	25-2 6	0	53	-52	2	-1	1	0	0	0
			49	28	-29	1	-1	1	0	0	0
			97	55	-53	2	-1	1	0	0	0
66	Fondazio ne	25-2 6	0	55	-52	2	-1	1	0	0	0
			49	28	-29	1	-1	0	0	0	0
			97	55	-53	1	-1	0	0	0	0
67	Fondazio ne	25-2 6	0	55	-53	1	-1	0	0	0	0
			49	28	-31	1	-1	0	0	0	0
			97	55	-54	0	-2	-1	-1	-1	-1
68	Fondazio ne	25-2 6	0	54	-54	0	-2	-1	-1	-1	-1
			49	29	-30	3	-1	1	0	1	1
			97	64	-59	3	2	2	2	2	2
69	Fondazio ne	25-2 6	0	64	-59	3	2	2	2	2	2
			49	49	-52	0	-1	0	-1	-1	-1
			97	42	-49	2	-10	-2	-5	-3	-3
70	Fondazio ne	25-2 8	0	173	-146	40	6	26	19	19	19
			43	53	-62	-1	-10	-4	-6	-5	-5
			85	106	-161	-6	-57	-26	-36	-28	-28
71	Fondazio ne	25-2 8	0	106	-161	-6	-57	-26	-36	-28	-28
			43	33	-25	7	0	5	3	4	4
			85	226	-154	74	9	47	34	36	36
72	Fondazio ne	26-2 7	0	73	-105	-7	-33	-16	-21	-16	-16
			33	41	-31	10	1	7	5	5	5
			66	138	-88	51	8	33	24	25	25
73	Fondazio ne	26-2 7	0	138	-88	51	8	33	25	25	25
			33	24	-34	-2	-9	-5	-6	-5	-5
			66	135	-207	-13	-72	-35	-47	-36	-36
74	Fondazio ne	27-2 9	0	127	-192	-12	-65	-32	-42	-33	-33
			33	14	-15	0	-1	0	0	0	0
			66	173	-110	62	12	41	31	31	31
75	Fondazio ne	27-2 9	0	173	-110	62	12	41	31	31	31
			33	16	-14	2	1	1	1	1	1
			66	127	-188	-10	-61	-30	-40	-30	-30
76	Fondazio ne	28-3 0	0	206	-143	65	7	42	30	32	32
			37	19	-21	-1	-2	-1	-2	-1	-1
			73	118	-185	-9	-67	-32	-44	-34	-34
77	Fondazio ne	28-3 0	0	118	-185	-9	-67	-32	-44	-34	-34
			37	23	-23	0	-1	0	0	0	0
			73	224	-156	69	10	45	33	34	34
78	Fondazio ne	29-3 1	0	162	-230	-12	-69	-33	-45	-34	-34
			33	20	-24	-1	-3	-2	-2	-2	-2
			66	184	-125	60	9	39	29	30	30
79	Fondazio ne	29-3 1	0	184	-125	60	9	39	29	30	30
			33	18	-21	-1	-3	-2	-2	-2	-2
			66	164	-233	-12	-69	-33	-45	-34	-34
80	Fondazio ne	30-3 2	0	230	-162	69	10	45	33	34	34
			34	21	-20	1	0	1	0	1	1
			69	118	-183	-10	-64	-31	-42	-32	-32
81	Fondazio ne	30-3 2	0	118	-183	-10	-64	-31	-42	-32	-32
			34	11	-10	1	0	1	1	1	1
			69	218	-150	69	11	44	33	34	34

82	Fondazio ne	31-3 3	0	142	-203	-11	-61	-30	-40	-30	-30
			33	14	-12	2	1	1	1	1	1
			66	184	-121	62	12	41	31	31	31
83	Fondazio ne	31-3 3	0	184	-121	62	12	41	31	31	31
			33	15	-12	3	1	2	1	1	1
			66	138	-196	-10	-59	-28	-38	-29	-29
84	Fondazio ne	32-3 4	0	223	-155	69	11	44	33	34	34
			35	10	-10	0	0	0	0	0	0
			69	122	-187	-10	-65	-32	-43	-33	-33
85	Fondazio ne	32-3 4	0	122	-187	-10	-65	-32	-43	-33	-33
			35	17	-17	0	-1	0	0	0	0
			69	227	-161	67	11	43	32	33	33
86	Fondazio ne	33-3 5	0	166	-231	-12	-67	-32	-43	-33	-33
			33	20	-23	-1	-2	-1	-2	-1	-1
			66	182	-123	59	9	38	28	29	29
87	Fondazio ne	33-3 5	0	182	-123	59	9	38	28	29	29
			33	20	-23	-1	-3	-2	-2	-2	-2
			66	172	-240	-13	-67	-33	-44	-34	-34
88	Fondazio ne	34-3 6	0	229	-162	67	11	43	32	33	33
			35	17	-17	0	0	0	0	0	0
			69	120	-185	-10	-64	-31	-42	-32	-32
89	Fondazio ne	34-3 6	0	120	-185	-10	-64	-31	-42	-32	-32
			35	18	-18	0	0	0	0	0	0
			69	222	-156	66	11	43	32	33	33
90	Fondazio ne	35-3 7	0	147	-207	-11	-60	-29	-39	-30	-30
			33	17	-15	2	1	1	1	1	1
			66	181	-118	61	12	41	31	32	32
91	Fondazio ne	35-3 7	0	181	-118	61	12	41	31	32	32
			33	11	-9	2	1	2	1	1	1
			66	144	-204	-10	-59	-29	-39	-30	-30
92	Fondazio ne	36-3 8	0	220	-154	66	11	43	32	33	33
			35	16	-16	0	0	0	0	0	0
			69	126	-190	-11	-64	-31	-42	-32	-32
93	Fondazio ne	36-3 8	0	126	-190	-11	-64	-31	-42	-32	-32
			35	15	-16	0	-1	0	0	0	0
			69	214	-149	65	11	42	31	32	32
94	Fondazio ne	37-3 9	0	163	-230	-12	-66	-33	-43	-33	-33
			33	16	-19	-1	-2	-2	-2	-2	-2
			66	179	-120	59	9	39	29	30	30
95	Fondazio ne	37-3 9	0	179	-120	59	9	39	29	30	30
			33	15	-19	-2	-3	-2	-3	-2	-2
			66	171	-240	-13	-68	-34	-45	-35	-35
96	Fondazio ne	38-4 0	0	213	-148	65	11	42	32	32	32
			34	16	-15	1	0	0	0	0	0
			69	122	-184	-11	-61	-30	-40	-31	-31
97	Fondazio ne	38-4 0	0	122	-185	-11	-61	-30	-40	-31	-31
			34	16	-16	0	0	0	0	0	0
			69	214	-151	63	11	41	31	32	32
98	Fondazio ne	39-4 1	0	145	-207	-12	-61	-30	-40	-31	-31
			33	10	-9	1	0	1	1	1	1
			66	180	-118	61	12	40	31	31	31
99	Fondazio ne	39-4 1	0	181	-118	61	12	40	31	31	31
			33	17	-19	0	-2	-1	-1	-1	-1
			66	170	-237	-12	-67	-33	-44	-34	-34
100	Fondazio	40-4	0	209	-146	63	12	41	31	32	32

	ne	2									
			35	17	-20	-1	-2	-1	-2	-1	-1
			69	122	-190	-16	-65	-34	-43	-34	-34
101	Fondazio ne	40-4 2	0	123	-190	-16	-65	-34	-43	-34	-34
			35	20	-20	2	-2	0	-1	0	0
			69	206	-139	64	20	43	34	34	34
102	Fondazio ne	41-4 4	0	160	-227	-12	-67	-33	-44	-34	-34
			33	23	-29	-1	-6	-3	-4	-3	-3
			66	150	-96	53	10	35	26	27	27
103	Fondazio ne	41-4 4	0	150	-96	53	10	35	26	27	27
			33	54	-36	17	5	11	9	9	9
			66	73	-92	-2	-22	-9	-13	-10	-10
104	Fondazio ne	42-4 3	0	198	-131	63	21	43	34	34	34
			23	99	-73	24	9	16	13	13	13
			46	88	-101	-3	-14	-7	-10	-8	-8
105	Fondazio ne	43-4 4	0	155	-185	-10	-28	-15	-19	-15	-15
			49	71	-81	-3	-10	-5	-7	-5	-5
			97	88	-78	7	4	5	5	5	5
106	Fondazio ne	43-4 4	0	88	-78	7	4	5	5	5	5
			49	47	-42	5	1	3	2	2	2
			97	58	-58	1	-2	0	-1	0	0
107	Fondazio ne	43-4 4	0	58	-59	1	-2	0	0	0	0
			49	29	-29	1	-1	0	0	0	0
			97	55	-55	1	-1	0	0	0	0
108	Fondazio ne	43-4 4	0	56	-56	1	-1	0	0	0	0
			49	30	-30	1	-1	0	0	0	0
			97	54	-54	1	-1	0	0	0	0
109	Fondazio ne	43-4 4	0	54	-55	1	-1	0	0	0	0
			49	29	-29	1	-1	0	0	0	0
			97	53	-53	1	-2	0	0	0	0
110	Fondazio ne	43-4 4	0	54	-54	1	-2	0	0	0	0
			49	28	-29	1	-1	0	0	0	0
			97	52	-53	1	-2	0	-1	0	0
111	Fondazio ne	43-4 4	0	53	-53	1	-2	0	-1	0	0
			49	28	-29	1	-1	0	0	0	0
			97	51	-52	1	-2	0	-1	0	0
112	Fondazio ne	43-4 4	0	52	-52	1	-2	0	-1	0	0
			49	27	-28	0	-1	0	0	0	0
			97	51	-51	1	-2	0	-1	0	0
113	Fondazio ne	43-4 4	0	51	-52	1	-2	0	-1	0	0
			49	27	-27	0	-1	0	0	0	0
			97	50	-51	1	-2	0	-1	0	0
114	Fondazio ne	43-4 4	0	51	-51	1	-2	0	-1	0	0
			49	26	-27	0	-1	0	0	0	0
			97	51	-52	1	-2	0	-1	0	0
115	Fondazio ne	43-4 4	0	51	-52	1	-2	0	-1	0	0
			49	26	-27	0	-1	0	0	0	0
			97	51	-52	1	-2	0	-1	0	0
116	Fondazio ne	43-4 4	0	51	-52	1	-2	0	-1	0	0
			49	26	-27	0	-1	0	0	0	0
			97	51	-52	1	-2	0	-1	0	0
117	Fondazio ne	43-4 4	0	51	-52	1	-2	0	-1	0	0
			49	27	-27	1	-1	0	0	0	0
			97	52	-53	1	-2	0	-1	0	0
118	Fondazio ne	43-4 4	0	52	-52	1	-2	0	-1	0	0

			49	27	-27	1	-1	0	0	0	0
			97	54	-53	1	-2	0	-1	0	0
119	Fondazio ne	43-4 4	0	52	-53	1	-2	0	-1	0	0
			49	27	-28	1	-1	0	0	0	0
			97	54	-53	1	-1	0	0	0	0
120	Fondazio ne	43-4 4	0	54	-53	1	-1	0	0	0	0
			49	28	-28	1	-1	0	0	0	0
			97	55	-53	1	-1	0	0	0	0
121	Fondazio ne	43-4 4	0	55	-53	1	-1	0	0	0	0
			49	28	-29	1	-1	0	0	0	0
			97	55	-54	1	-2	0	-1	-1	-1
122	Fondazio ne	43-4 4	0	55	-54	1	-2	0	-1	-1	-1
			49	29	-26	4	0	2	1	1	1
			97	67	-60	5	3	4	3	3	3
123	Fondazio ne	43-4 4	0	67	-59	5	3	4	3	3	3
			49	45	-43	2	1	1	1	1	1
			97	43	-37	4	-7	0	-3	-1	-1
124	Fondazio ne	43-4 5	0	105	-83	21	9	14	11	11	11
			33	38	-55	-2	-18	-8	-11	-9	-9
			66	103	-159	-12	-54	-28	-36	-28	-28
125	Fondazio ne	43-4 5	0	103	-159	-12	-54	-28	-36	-28	-28
			33	31	-25	6	1	4	3	3	3
			66	221	-150	69	15	46	35	35	35
126	Fondazio ne	44-4 6	0	80	-110	-6	-30	-15	-20	-15	-15
			33	39	-27	11	1	7	5	6	6
			66	141	-91	50	9	33	25	25	25
127	Fondazio ne	44-4 6	0	141	-91	50	9	33	25	25	25
			33	29	-39	-2	-9	-5	-6	-5	-5
			66	159	-231	-14	-71	-35	-47	-36	-36
128	Fondazio ne	45-4 7	0	179	-116	62	13	41	31	31	31
			33	20	-21	-1	-2	-1	-1	-1	-1
			66	98	-163	-14	-62	-32	-42	-32	-32
129	Fondazio ne	45-4 7	0	98	-163	-14	-62	-32	-42	-32	-32
			33	11	-13	-1	-2	-1	-1	-1	-1
			66	182	-120	61	12	40	31	31	31
130	Fondazio ne	46-4 8	0	127	-192	-13	-63	-32	-42	-32	-32
			33	14	-16	0	-2	-1	-1	-1	-1
			66	152	-92	58	12	39	29	30	30
131	Fondazio ne	46-4 8	0	152	-92	58	12	39	29	30	30
			33	15	-13	1	1	1	1	1	1
			66	121	-179	-11	-57	-28	-38	-29	-29
132	Fondazio ne	47-4 9	0	190	-121	67	15	45	34	35	35
			33	17	-13	3	2	3	2	2	2
			66	81	-140	-11	-58	-29	-38	-29	-29
133	Fondazio ne	47-4 9	0	81	-140	-11	-58	-29	-38	-29	-29
			33	19	-13	4	2	3	3	3	3
			66	184	-112	69	16	46	35	36	36
134	Fondazio ne	48-5 0	0	119	-184	-14	-64	-32	-42	-33	-33
			33	17	-20	-1	-2	-2	-2	-2	-2
			66	137	-80	57	10	37	28	29	29
135	Fondazio ne	48-5 0	0	137	-80	57	10	37	28	29	29
			33	12	-19	-3	-5	-3	-4	-3	-3
			66	105	-177	-17	-70	-36	-47	-36	-36
136	Fondazio ne	49-5 1	0	137	-73	60	16	41	32	32	32
			33	18	-19	0	-1	0	-1	0	0

			66	63	-128	-15	-60	-32	-41	-32	-32
137	Fondazio ne	49-5 1	0	63	-128	-15	-60	-32	-41	-32	-32
			33	21	-19	1	1	1	1	1	1
			66	141	-72	65	18	44	35	35	35
138	Fondazio ne	50-5 2	0	64	-130	-16	-62	-33	-42	-33	-33
			33	17	-16	1	0	0	0	0	0
			66	126	-61	61	15	42	32	33	33
139	Fondazio ne	50-5 2	0	127	-62	61	15	42	32	33	33
			33	18	-21	-2	-3	-2	-2	-2	-2
			66	69	-143	-19	-68	-37	-47	-37	-37
140	Fondazio ne	51-5 3	0	149	-71	70	23	49	39	39	39
			33	28	-18	6	4	5	4	4	4
			66	64	-123	-13	-56	-29	-38	-30	-30
141	Fondazio ne	51-5 3	0	64	-123	-13	-55	-29	-38	-30	-30
			33	31	-17	10	6	8	6	6	6
			66	172	-87	75	28	54	43	43	43
142	Fondazio ne	52-5 4	0	53	-128	-22	-67	-37	-47	-37	-37
			33	12	-18	-3	-4	-3	-3	-3	-3
			66	122	-60	57	15	40	31	31	31
143	Fondazio ne	52-5 4	0	122	-60	57	15	40	31	31	31
			33	13	-23	-5	-7	-5	-6	-5	-5
			66	55	-137	-26	-72	-41	-51	-41	-41
144	Fondazio ne	53-5 5	0	134	-61	62	25	46	37	37	37
			33	35	-20	10	7	8	7	7	7
			66	60	-106	-7	-44	-22	-30	-23	-23
145	Fondazio ne	53-5 5	0	60	-106	-7	-44	-22	-30	-23	-23
			33	22	-22	3	-1	1	0	0	0
			66	118	-70	46	8	31	23	24	24
146	Fondazio ne	54-5 6	0	39	-117	-26	-66	-39	-48	-39	-39
			33	10	-26	-8	-12	-8	-9	-8	-8
			66	100	-54	44	7	29	22	23	23
147	Fondazio ne	54-5 6	0	99	-54	44	7	29	22	23	23
			33	15	-17	0	-4	0	-1	-1	-1
			66	60	-109	-8	-46	-24	-31	-24	-24
148	Fondazio ne	55-5 7	0	101	-67	31	0	20	13	15	15
			40	46	-34	13	5	7	5	5	5
			80	82	-89	14	-18	-1	-7	-4	-4
149	Fondazio ne	55-5 7	0	82	-89	14	-17	-1	-7	-4	-4
			40	75	-60	10	5	7	6	6	6
			80	99	-63	31	7	20	15	15	15
150	Fondazio ne	56-7 0	0	57	-87	0	-31	-13	-20	-15	-15
			40	24	-35	-5	-12	-5	-7	-5	-5
			80	82	-75	18	-14	7	1	4	4
151	Fondazio ne	56-7 0	0	82	-75	18	-14	7	1	4	4
			40	29	-40	-5	-10	-5	-7	-5	-5
			80	41	-70	-7	-30	-14	-19	-14	-14
152	Fondazio ne	57-5 8	0	132	-145	3	-29	-6	-12	-7	-7
			42	38	-61	-8	-13	-8	-9	-8	-8
			83	85	-107	4	-19	-6	-11	-8	-8
153	Fondazio ne	57-5 8	0	85	-106	4	-18	-6	-11	-8	-8
			42	69	-96	-10	-16	-10	-12	-10	-10
			83	68	-122	-6	-33	-11	-17	-11	-11
154	Fondazio ne	58-5 9	0	65	-117	-2	-33	-9	-15	-9	-9
			35	41	-53	-5	-8	-5	-6	-5	-5
			69	43	-59	21	-13	3	-4	-1	-1

155	Fondazio ne	58-5 9	0	43	-59	21	-13	3	-4	-1	-1
			35	17	-26	-3	-5	-3	-3	-3	-3
			69	42	-47	8	-31	-2	-10	-4	-4
156	Fondazio ne	59-6 0	0	47	-49	10	-34	-1	-10	-4	-4
			35	20	-27	-2	-4	-2	-3	-2	-2
			69	51	-68	27	-15	5	-4	-1	-1
157	Fondazio ne	59-6 0	0	51	-68	27	-15	5	-4	-1	-1
			35	19	-23	-1	-2	-1	-1	-1	-1
			69	53	-47	13	-31	1	-8	-2	-2
158	Fondazio ne	60-6 1	0	55	-45	14	-33	2	-8	-1	-1
			35	18	-23	-1	-3	-1	-2	-1	-1
			69	48	-68	28	-16	5	-4	-1	-1
159	Fondazio ne	60-6 1	0	48	-68	29	-16	5	-4	-1	-1
			35	21	-25	1	-2	0	-1	-1	-1
			69	47	-40	12	-25	2	-6	-1	-1
160	Fondazio ne	61-6 2	0	75	-53	17	-37	3	-8	-1	-1
			35	18	-22	1	-3	0	-1	0	0
			69	45	-62	31	-16	6	-3	0	0
161	Fondazio ne	61-6 2	0	45	-62	31	-16	6	-3	0	0
			35	15	-18	1	-3	0	0	0	0
			69	66	-47	18	-36	3	-7	0	0
162	Fondazio ne	62-6 3	0	46	-33	13	-28	2	-6	0	0
			35	19	-20	1	-2	0	-1	0	0
			69	42	-63	30	-17	5	-4	-1	-1
163	Fondazio ne	62-6 3	0	41	-63	30	-17	5	-4	-1	-1
			35	17	-18	0	-1	-1	-1	-1	-1
			69	62	-41	15	-32	3	-7	-1	-1
164	Fondazio ne	63-6 4	0	58	-35	15	-32	3	-7	-1	-1
			35	17	-18	0	-1	0	-1	0	0
			69	82	-52	31	-16	6	-4	0	0
165	Fondazio ne	63-6 4	0	82	-52	31	-16	6	-4	0	0
			35	15	-16	0	-1	0	-1	0	0
			69	60	-39	15	-32	3	-7	0	0
166	Fondazio ne	64-6 5	0	59	-37	15	-32	3	-7	0	0
			35	15	-16	0	-1	0	-1	0	0
			69	80	-48	30	-16	5	-4	-1	-1
167	Fondazio ne	64-6 5	0	80	-48	30	-16	5	-4	-1	-1
			35	15	-16	1	-1	0	-1	0	0
			69	55	-36	14	-28	3	-6	0	0
168	Fondazio ne	65-6 6	0	64	-38	18	-36	3	-7	0	0
			35	13	-13	1	-2	0	0	0	0
			69	79	-45	31	-15	7	-3	0	0
169	Fondazio ne	65-6 6	0	79	-45	31	-15	7	-3	0	0
			35	15	-15	1	-3	0	-1	0	0
			69	60	-45	18	-36	3	-8	0	0
170	Fondazio ne	66-6 7	0	41	-32	12	-25	2	-5	0	0
			35	17	-19	1	-2	0	-1	-1	-1
			69	76	-48	28	-16	5	-4	-1	-1
171	Fondazio ne	66-6 7	0	76	-48	28	-16	5	-4	-1	-1
			35	13	-16	-1	-3	-1	-1	-1	-1
			69	56	-35	14	-32	2	-8	-1	-1
172	Fondazio ne	67-6 8	0	52	-34	12	-30	1	-7	-1	-1
			35	14	-16	-1	-2	-1	-1	-1	-1
			69	68	-40	26	-14	5	-3	-1	-1
173	Fondazio	67-6	0	68	-40	26	-14	5	-3	-1	-1

	ne	8									
			35	12	-17	-2	-4	-2	-2	-2	-2
			69	55	-41	10	-33	-1	-10	-3	-3
174	Fondazio ne	68-6 9	0	48	-39	8	-30	-2	-9	-4	-4
			35	13	-19	-2	-5	-2	-3	-2	-2
			69	66	-43	20	-13	3	-4	-1	-1
175	Fondazio ne	68-6 9	0	66	-43	20	-13	3	-4	-1	-1
			35	11	-22	-5	-7	-5	-6	-5	-5
			69	43	-55	-1	-32	-8	-14	-9	-9
176	Fondazio ne	69-7 0	0	46	-65	-5	-32	-11	-16	-11	-11
			42	21	-42	-9	-15	-9	-11	-9	-9
			83	73	-74	4	-19	-6	-11	-8	-8
177	Fondazio ne	69-7 0	0	73	-74	4	-19	-6	-11	-8	-8
			42	26	-44	-8	-13	-8	-10	-8	-8
			83	36	-57	0	-29	-7	-13	-9	-9
178	Primo Impalcat o	1-2	0	1490	-897	462	64	312	232	248	248
			83	627	-320	214	85	159	131	131	131
			166	1331	-1301	65	-14	27	11	15	15
179	Primo Impalcat o	1-15	0	762	-1472	-141	-513	-289	-363	-294	-294
			80	648	-660	87	-106	-9	-47	-29	-29
			159	800	-213	346	236	281	236	236	236
180	Primo Impalcat o	2-3	0	1286	-1248	69	-7	31	16	19	19
			69	567	-531	62	-37	13	-6	1	1
			138	916	-956	26	-52	-10	-26	-18	-18
181	Primo Impalcat o	3-4	0	903	-941	28	-51	-9	-25	-17	-17
			69	682	-695	35	-47	-5	-22	-14	-14
			138	413	-434	12	-29	-8	-16	-12	-12
182	Primo Impalcat o	4-5	0	429	-448	15	-30	-7	-16	-11	-11
			69	355	-318	32	-30	0	-13	-8	-8
			138	944	-920	19	-15	1	-6	-4	-4
183	Primo Impalcat o	5-6	0	947	-919	21	-16	1	-6	-4	-4
			69	393	-340	38	-22	6	-6	-2	-2
			138	298	-288	26	-12	5	-3	0	0
184	Primo Impalcat o	6-7	0	296	-285	26	-12	5	-3	0	0
			69	545	-530	44	-20	9	-4	0	0
			138	781	-766	32	-14	7	-2	1	1
185	Primo Impalcat o	7-8	0	785	-771	34	-15	7	-2	0	0
			69	106	-55	50	-23	11	-4	0	0
			138	816	-764	37	-17	8	-3	1	1
186	Primo Impalcat o	8-9	0	806	-755	37	-16	8	-3	1	1
			69	566	-497	48	-23	10	-4	0	0
			138	253	-252	30	-14	6	-3	0	0
187	Primo Impalcat o	9-10	0	259	-257	26	-13	5	-3	0	0
			69	373	-371	36	-21	6	-6	-2	-2
			138	907	-912	16	-14	0	-6	-4	-4
188	Primo Impalcat o	10-1 1	0	913	-920	16	-15	0	-6	-4	-4
			69	271	-290	30	-29	-1	-13	-8	-8
			138	419	-409	14	-29	-7	-16	-12	-12

189	Primo Impalcato	11-12	0	404	-400	11	-28	-8	-16	-12	-12
			69	575	-533	31	-44	-6	-21	-14	-14
			138	657	-690	22	-44	-10	-23	-17	-17
190	Primo Impalcato	12-13	0	667	-702	20	-45	-11	-24	-18	-18
			69	185	-182	54	-26	12	-4	1	1
			138	865	-841	58	7	30	20	20	20
191	Primo Impalcato	13-14	0	851	-840	53	2	25	15	16	16
			83	523	-279	217	90	163	135	135	135
			166	801	-295	453	85	315	241	253	253
192	Primo Impalcato	14-16	0	809	-269	462	133	332	266	270	270
			80	338	-289	88	-84	39	4	23	23
			159	253	-815	-224	-329	-224	-267	-224	-224
193	Primo Impalcato	15-17	0	767	-240	311	212	253	212	212	212
			66	369	-39	219	146	175	146	146	146
			132	477	-284	122	80	98	80	80	80
194	Primo Impalcato	16-18	0	258	-763	-201	-296	-201	-240	-201	-201
			66	92	-372	-140	-210	-140	-168	-140	-140
			132	236	-434	-78	-117	-78	-95	-78	-78
195	Primo Impalcato	17-19	0	451	-274	112	74	90	74	74	74
			66	385	-295	61	31	46	37	37	37
			132	343	-353	6	-6	2	-1	0	0
196	Primo Impalcato	18-20	0	238	-440	-80	-119	-80	-97	-80	-80
			66	251	-343	-35	-66	-40	-50	-40	-40
			132	327	-322	5	-7	0	-2	0	0
197	Primo Impalcato	19-21	0	369	-372	10	-2	5	3	3	3
			66	129	-131	10	-14	1	-4	-1	-1
			132	384	-394	-1	-8	-5	-6	-5	-5
198	Primo Impalcato	20-22	0	321	-323	1	-10	-3	-5	-3	-3
			66	125	-123	15	-11	4	-2	1	1
			132	380	-368	8	1	6	5	5	5
199	Primo Impalcato	21-23	0	364	-377	-4	-9	-6	-8	-6	-6
			66	291	-299	3	-14	-3	-6	-4	-4
			132	287	-291	4	-3	-1	-2	-2	-2
200	Primo Impalcato	22-24	0	389	-372	10	3	8	7	7	7
			66	291	-280	19	-5	8	3	5	5
			132	245	-240	4	-1	3	2	2	2
201	Primo Impalcato	23-25	0	290	-289	6	0	1	0	0	0
			66	214	-214	7	-8	1	-2	0	0
			132	455	-456	2	-1	0	-1	-1	-1
202	Primo Impalcato	24-26	0	246	-244	1	-4	0	0	0	0
			66	139	-138	11	-8	2	-1	0	0
			132	413	-414	1	-3	0	0	0	0
203	Primo Impalcato	25-28	0	439	-445	1	-4	-2	-3	-3	-3
			85	211	-247	10	-24	0	-7	-2	-2

			170	266	-269	2	-3	-1	-2	-1	-1
204	Primo Impalcato	26-27	0	430	-425	4	-1	3	2	2	2
			66	244	-249	10	-6	3	0	1	1
			132	274	-274	1	-4	0	-1	0	0
205	Primo Impalcato	27-29	0	264	-267	-2	-5	-2	-2	-2	-2
			66	192	-196	6	-9	0	-3	-2	-2
			132	388	-392	-1	-7	-1	-3	-1	-1
206	Primo Impalcato	28-30	0	263	-262	3	1	1	1	1	1
			73	234	-233	7	-9	2	-1	1	1
			146	426	-431	12	-4	3	0	1	1
207	Primo Impalcato	29-31	0	411	-410	1	-5	0	-1	0	0
			66	223	-222	7	-4	2	0	1	1
			132	313	-312	3	-6	1	-1	1	1
208	Primo Impalcato	30-32	0	434	-438	11	-4	3	0	1	1
			69	208	-207	3	-3	1	0	0	0
			137	281	-281	10	-4	2	-1	0	0
209	Primo Impalcato	31-33	0	299	-302	0	-8	-1	-3	-1	-1
			66	236	-244	4	-5	0	-2	-1	-1
			132	347	-356	1	-8	-1	-2	-1	-1
210	Primo Impalcato	32-34	0	282	-282	10	-4	2	-1	0	0
			69	262	-268	3	-5	1	-1	0	0
			138	390	-394	9	-4	2	-1	0	0
211	Primo Impalcato	33-35	0	374	-379	4	-7	2	0	1	1
			66	199	-197	5	-1	2	1	1	1
			132	327	-336	5	-7	2	-1	1	1
212	Primo Impalcato	34-36	0	400	-405	9	-5	2	-1	0	0
			69	202	-203	2	-6	0	-1	0	0
			138	306	-308	8	-5	1	-1	0	0
213	Primo Impalcato	35-37	0	300	-313	2	-9	0	-2	-1	-1
			66	272	-273	3	-3	0	-1	-1	-1
			132	296	-310	3	-9	0	-3	-1	-1
214	Primo Impalcato	36-38	0	309	-310	8	-5	1	-1	0	0
			69	259	-259	3	-8	0	-2	0	0
			138	294	-295	4	-3	1	-1	0	0
215	Primo Impalcato	37-39	0	335	-325	6	-7	2	-1	1	1
			66	166	-164	5	1	2	1	1	1
			132	383	-380	7	-8	2	-1	1	1
216	Primo Impalcato	38-40	0	300	-295	4	-3	0	-1	-1	-1
			69	206	-207	7	-13	1	-3	0	0
			137	385	-384	2	-2	1	0	0	0
217	Primo Impalcato	39-41	0	347	-350	5	-10	0	-3	-1	-1
			66	256	-260	3	-3	0	-1	-1	-1
			132	245	-248	2	-9	-1	-3	-1	-1
218	Primo Impalcato	40-42	0	376	-373	3	-4	1	-1	0	0

			69	245	-242	4	1	2	2	2	2
			138	267	-261	35	-9	10	1	3	3
219	Primo Impalcato	41-44	0	260	-263	2	-9	-1	-3	-1	-1
			66	161	-161	5	-3	1	-1	0	0
			132	234	-232	4	-5	2	0	1	1
220	Primo Impalcato	42-43	0	264	-258	34	-9	10	1	3	3
			23	213	-208	34	-10	9	0	3	3
			46	257	-228	34	-12	9	-1	2	2
221	Primo Impalcato	43-45	0	226	-226	33	-15	7	-3	0	0
			66	260	-262	1	-1	0	-1	0	0
			132	364	-366	5	-8	0	-2	-1	-1
222	Primo Impalcato	44-46	0	216	-211	7	-4	4	2	3	3
			66	260	-251	9	-3	3	1	2	2
			132	376	-375	1	-3	1	0	0	0
223	Primo Impalcato	45-47	0	382	-379	8	-5	3	0	1	1
			66	144	-144	12	-18	3	-3	0	0
			132	261	-267	5	-6	0	-2	-1	-1
224	Primo Impalcato	46-48	0	407	-410	-1	-4	-1	-2	-1	-1
			66	220	-221	11	-9	2	-2	0	0
			132	313	-312	1	-3	1	0	0	0
225	Primo Impalcato	47-49	0	248	-257	2	-7	-2	-4	-3	-3
			66	264	-294	5	-21	-3	-9	-5	-5
			132	308	-322	-4	-11	-7	-9	-7	-7
226	Primo Impalcato	48-50	0	294	-290	3	0	3	2	2	2
			66	276	-275	18	-4	8	3	5	5
			132	315	-299	10	4	8	7	7	7
227	Primo Impalcato	49-51	0	328	-340	-1	-10	-5	-7	-6	-6
			66	122	-126	10	-16	1	-5	-2	-2
			132	347	-342	10	-3	5	2	2	2
228	Primo Impalcato	50-52	0	343	-331	9	2	7	6	6	6
			66	121	-119	16	-12	4	-2	1	1
			132	340	-347	1	-13	-3	-6	-3	-3
229	Primo Impalcato	51-53	0	326	-328	6	-7	1	-1	-1	-1
			66	337	-254	61	30	45	36	36	36
			132	412	-228	111	73	89	73	73	73
230	Primo Impalcato	52-54	0	310	-312	3	-9	-1	-4	-1	-1
			66	221	-305	-32	-64	-38	-48	-38	-38
			132	156	-353	-75	-113	-75	-91	-75	-75
231	Primo Impalcato	53-55	0	436	-233	121	80	97	80	80	80
			66	411	-109	220	146	175	146	146	146
			132	778	-254	312	212	253	212	212	212
232	Primo Impalcato	54-56	0	177	-369	-81	-122	-81	-99	-81	-81
			66	40	-372	-146	-220	-146	-176	-146	-146
			132	231	-768	-211	-312	-211	-252	-211	-211
233	Primo Impalcato	55-57	0	814	-233	347	236	282	236	236	236

	o										
			80	551	-680	87	-105	-8	-47	-29	-29
			159	785	-1611	-141	-512	-289	-363	-293	-293
234	Primo Impalcat o	56-70	0	206	-730	-206	-303	-206	-246	-206	-206
			80	344	-391	89	-77	41	7	25	25
			159	687	-161	440	124	315	252	256	256
235	Primo Impalcat o	57-58	0	883	-1607	-64	-461	-232	-311	-247	-247
			83	240	-611	-86	-213	-131	-159	-131	-131
			166	1118	-1154	14	-66	-11	-27	-15	-15
236	Primo Impalcat o	58-59	0	1061	-1107	7	-70	-16	-31	-19	-19
			69	518	-521	37	-63	6	-14	-1	-1
			138	802	-756	52	-27	25	10	17	17
237	Primo Impalcat o	59-60	0	790	-746	51	-29	24	8	16	16
			69	568	-516	47	-36	22	5	14	14
			138	356	-333	29	-12	16	8	12	12
238	Primo Impalcat o	60-61	0	362	-340	30	-15	16	7	11	11
			69	260	-243	29	-30	12	1	8	8
			138	706	-697	14	-15	6	0	4	4
239	Primo Impalcat o	61-62	0	707	-699	14	-16	6	0	4	4
			69	267	-264	20	-35	6	-5	2	2
			138	247	-247	12	-25	2	-5	0	0
240	Primo Impalcat o	62-63	0	244	-244	13	-28	3	-6	0	0
			69	398	-398	22	-47	4	-10	0	0
			138	573	-574	16	-36	3	-8	-1	-1
241	Primo Impalcat o	63-64	0	578	-579	16	-37	3	-8	-1	-1
			69	82	-134	24	-52	4	-11	-1	-1
			138	604	-605	16	-37	3	-8	-1	-1
242	Primo Impalcat o	64-65	0	595	-597	16	-37	3	-8	-1	-1
			69	390	-390	22	-48	4	-10	0	0
			138	219	-219	14	-29	3	-6	0	0
243	Primo Impalcat o	65-66	0	221	-221	12	-26	3	-5	0	0
			69	269	-266	21	-36	6	-5	2	2
			138	700	-693	14	-16	6	0	4	4
244	Primo Impalcat o	66-67	0	705	-697	14	-16	6	0	4	4
			69	237	-260	29	-29	13	1	8	8
			138	341	-317	30	-14	16	8	12	12
245	Primo Impalcat o	67-68	0	335	-310	29	-10	17	9	12	12
			69	423	-394	44	-31	22	7	15	15
			138	569	-495	45	-21	24	11	17	17
246	Primo Impalcat o	68-69	0	579	-503	46	-19	25	12	18	18
			69	161	-150	26	-52	4	-11	-1	-1
			138	682	-721	-8	-57	-19	-29	-20	-20
247	Primo Impalcat o	69-70	0	676	-708	-2	-51	-15	-25	-16	-16
			83	172	-531	-91	-221	-137	-166	-137	-137
			166	206	-752	-89	-461	-247	-321	-258	-258
248	Primo	1-1	0	674	-860	-4	-114	-34	-55	-38	-38

	Impalcat o										
			188	279	-150	79	55	68	63	64	64
			376	982	-649	351	53	207	148	166	166
249	Primo Impalcat o	2-2	0	35	-41	4	-11	-1	-4	-3	-3
			188	1	-2	0	0	0	0	0	0
			376	41	-36	10	-4	4	1	3	3
250	Primo Impalcat o	3-3	0	43	-44	8	-10	1	-2	-1	-1
			188	0	-1	0	0	0	0	0	0
			376	43	-43	9	-8	2	-2	0	0
251	Primo Impalcat o	4-4	0	44	-43	9	-8	2	-1	0	0
			188	0	0	0	0	0	0	0	0
			376	43	-45	8	-10	1	-3	-1	-1
252	Primo Impalcat o	5-5	0	46	-45	10	-9	2	-1	0	0
			188	1	-1	0	0	0	0	0	0
			376	44	-45	8	-10	1	-2	-1	-1
253	Primo Impalcat o	6-6	0	38	-38	8	-7	2	-1	0	0
			188	1	-1	0	0	0	0	0	0
			376	39	-40	7	-8	1	-2	0	0
254	Primo Impalcat o	7-7	0	39	-38	7	-7	2	-1	0	0
			188	1	-1	0	0	0	0	0	0
			376	39	-40	8	-8	1	-2	0	0
255	Primo Impalcat o	8-8	0	48	-48	10	-10	2	-2	0	0
			188	1	-1	0	0	0	0	0	0
			376	46	-46	9	-9	2	-2	0	0
256	Primo Impalcat o	9-9	0	38	-39	7	-8	1	-2	0	0
			188	1	-1	0	0	0	0	0	0
			376	40	-39	8	-7	2	-1	0	0
257	Primo Impalcat o	10-1 0	0	38	-39	7	-8	1	-2	0	0
			188	1	-1	0	0	0	0	0	0
			376	40	-39	8	-7	2	-1	1	1
258	Primo Impalcat o	11-1 1	0	46	-47	9	-10	1	-2	0	0
			188	1	0	0	0	0	0	0	0
			376	46	-45	10	-8	3	-1	1	1
259	Primo Impalcat o	12-1 2	0	46	-45	9	-8	2	-1	1	1
			188	1	0	0	0	0	0	0	0
			376	45	-45	9	-9	2	-2	0	0
260	Primo Impalcat o	13-1 3	0	42	-37	11	-4	4	1	3	3
			188	1	0	0	0	0	0	0	0
			376	36	-42	4	-10	-1	-4	-3	-3
261	Primo Impalcat o	14-1 4	0	746	-630	122	24	69	50	52	52
			188	85	-205	-49	-76	-59	-64	-60	-60
			376	683	-1115	-62	-358	-155	-214	-172	-172
262	Primo Impalcat o	15-1 5	0	1492	-871	378	93	254	197	198	198
			188	388	-1030	-321	-547	-321	-401	-321	-321
			376	1143	-2823	-512	-1541	-840	-1071	-840	-840

263	Primo Impalcato	16-16	0	1184	-1598	-104	-377	-207	-263	-207	-207
			188	1037	-409	539	314	394	314	314	314
			376	3295	-1622	1539	509	1067	836	836	836
264	Primo Impalcato	17-17	0	1775	-401	1042	656	825	687	687	687
			188	899	-1565	-256	-651	-333	-437	-333	-333
			376	1701	-4407	-955	-2406	-1353	-1706	-1353	-1353
265	Primo Impalcato	18-18	0	1126	-2490	-650	-1034	-682	-819	-682	-682
			188	1573	-908	653	257	436	333	333	333
			376	5088	-2395	2402	951	1699	1347	1347	1347
266	Primo Impalcato	19-19	0	1528	-115	1065	686	848	704	704	704
			188	1419	-2070	-178	-710	-325	-442	-325	-325
			376	2614	-5322	-830	-2545	-1354	-1740	-1354	-1354
267	Primo Impalcato	20-20	0	675	-2088	-688	-1070	-707	-852	-707	-707
			188	2084	-1435	713	181	442	325	325	325
			376	5712	-3000	2555	838	1744	1356	1356	1356
268	Primo Impalcato	21-21	0	1900	-351	1006	645	802	665	665	665
			188	1925	-2561	-117	-751	-317	-444	-318	-318
			376	3834	-6436	-666	-2572	-1301	-1698	-1301	-1301
269	Primo Impalcato	22-22	0	463	-2158	-645	-1009	-666	-804	-666	-666
			188	2552	-1917	756	122	445	318	318	318
			376	6543	-3940	2585	677	1701	1302	1302	1302
270	Primo Impalcato	23-23	0	2235	-767	989	619	785	651	651	651
			188	2375	-3010	-78	-785	-309	-450	-318	-318
			376	5019	-7592	-563	-2626	-1283	-1695	-1286	-1286
271	Primo Impalcato	24-24	0	429	-2156	-629	-988	-653	-787	-653	-653
			188	2997	-2365	791	86	450	309	316	316
			376	7372	-4801	2634	588	1696	1285	1285	1285
272	Primo Impalcato	25-25	0	2466	-1160	1000	592	787	653	653	653
			188	2830	-3483	-61	-824	-314	-466	-327	-327
			376	6174	-8788	-478	-2731	-1284	-1734	-1307	-1307
273	Primo Impalcato	26-26	0	623	-1934	-632	-992	-655	-790	-655	-655
			188	3470	-2828	824	66	461	310	321	321
			376	8405	-5809	2704	552	1721	1291	1298	1298
274	Primo Impalcato	27-27	0	641	-1951	-634	-990	-655	-790	-655	-655
			188	3783	-3152	823	53	456	302	315	315
			376	9060	-6488	2700	527	1709	1275	1286	1286
275	Primo Impalcato	28-28	0	2211	-905	1005	579	788	653	653	653
			188	3197	-3841	-49	-824	-307	-462	-322	-322
			376	6695	-9290	-432	-2745	-1267	-1729	-1298	-1298
276	Primo Impalcato	29-29	0	985	-2300	-635	-994	-657	-793	-657	-657
			188	4039	-3412	823	49	454	300	314	314
			376	9873	-7304	2704	519	1709	1272	1284	1284
277	Primo Impalcato	30-30	0	2432	-959	1012	609	798	662	662	662
			188	3446	-4082	-43	-821	-303	-458	-318	-318

			376	7349	-9944	-469	-2730	-1274	-1727	-1298	-1298
278	Primo Impalcato	31-31	0	1144	-2461	-634	-996	-658	-793	-658	-658
			188	4200	-3575	819	49	453	299	313	313
			376	10292	-7724	2699	520	1708	1272	1284	1284
279	Primo Impalcato	32-32	0	1985	-658	1010	624	799	663	663	663
			188	3610	-4243	-45	-817	-302	-456	-317	-317
			376	7346	-9939	-495	-2714	-1278	-1722	-1296	-1296
280	Primo Impalcato	33-33	0	941	-2258	-635	-997	-658	-793	-658	-658
			188	4299	-3674	812	52	451	299	312	312
			376	10326	-7759	2685	525	1705	1273	1283	1283
281	Primo Impalcato	34-34	0	2232	-905	1010	625	800	664	664	664
			188	3688	-4321	-51	-814	-303	-455	-316	-316
			376	7787	-10380	-507	-2709	-1281	-1721	-1296	-1296
282	Primo Impalcato	35-35	0	999	-2316	-635	-996	-658	-793	-658	-658
			188	4279	-3655	804	55	449	300	312	312
			376	10372	-7808	2668	533	1700	1273	1282	1282
283	Primo Impalcato	36-36	0	2068	-740	1012	622	801	664	664	664
			188	3702	-4334	-59	-809	-304	-454	-316	-316
			376	7664	-10256	-519	-2702	-1283	-1719	-1296	-1296
284	Primo Impalcato	37-37	0	869	-2186	-635	-997	-659	-794	-659	-659
			188	4263	-3640	794	59	447	300	312	312
			376	10156	-7593	2650	540	1696	1274	1282	1282
285	Primo Impalcato	38-38	0	2283	-951	1014	626	803	666	666	666
			188	3661	-4289	-66	-802	-304	-451	-314	-314
			376	7710	-10299	-537	-2690	-1285	-1715	-1294	-1294
286	Primo Impalcato	39-39	0	1080	-2398	-634	-1000	-659	-794	-659	-659
			188	4156	-3533	786	63	445	301	312	312
			376	10188	-7623	2638	547	1694	1276	1282	1282
287	Primo Impalcato	40-40	0	2386	-1048	1009	663	806	669	669	669
			188	3540	-4162	-72	-791	-301	-445	-311	-311
			376	7590	-10170	-586	-2654	-1290	-1704	-1290	-1290
288	Primo Impalcato	41-41	0	1161	-2487	-636	-1008	-663	-800	-663	-663
			188	4016	-3391	783	66	445	302	313	313
			376	9937	-7360	2640	556	1700	1283	1289	1289
289	Primo Impalcato	42-42	0	1809	-478	991	666	803	666	666	666
			188	3351	-3955	-64	-775	-292	-434	-302	-302
			376	6752	-9290	-682	-2560	-1269	-1666	-1269	-1269
290	Primo Impalcato	43-43	0	1902	-574	990	664	801	664	664	664
			188	3282	-3894	-67	-782	-296	-439	-306	-306
			376	6671	-9222	-691	-2572	-1276	-1674	-1276	-1276
291	Primo Impalcato	44-44	0	702	-2020	-635	-1001	-659	-795	-659	-659
			188	3927	-3290	791	71	452	308	318	318
			376	9383	-6792	2648	563	1707	1290	1296	1296
292	Primo Impalcato	45-45	0	2263	-943	990	660	796	660	660	660

			188	2980	-3595	-87	-770	-301	-438	-307	-307
			376	6337	-8886	-628	-2589	-1275	-1677	-1275	-1275
293	Primo Impalcato	46-46	0	1078	-2388	-631	-993	-655	-790	-655	-655
			188	3619	-2998	767	77	441	302	311	311
			376	9020	-6467	2594	572	1680	1275	1276	1276
294	Primo Impalcato	47-47	0	2201	-807	997	633	793	657	657	657
			188	2564	-3187	-104	-761	-309	-440	-311	-311
			376	5410	-7970	-628	-2584	-1280	-1682	-1280	-1280
295	Primo Impalcato	48-48	0	1030	-2412	-631	-995	-656	-791	-656	-656
			188	3193	-2572	751	94	437	306	310	310
			376	8181	-5628	2563	607	1674	1277	1277	1277
296	Primo Impalcato	49-49	0	2024	-561	1011	643	805	667	667	667
			188	2082	-2713	-136	-738	-316	-440	-316	-316
			376	4328	-6925	-702	-2551	-1299	-1692	-1299	-1299
297	Primo Impalcato	50-50	0	369	-1985	-646	-1012	-668	-806	-668	-668
			188	2731	-2103	729	128	436	314	314	314
			376	6786	-4195	2535	689	1686	1296	1296	1296
298	Primo Impalcato	51-51	0	2067	-658	1067	685	849	705	705	705
			188	1590	-2238	-191	-702	-324	-440	-324	-324
			376	3325	-6031	-854	-2531	-1353	-1736	-1353	-1353
299	Primo Impalcato	52-52	0	385	-1810	-693	-1078	-712	-859	-712	-712
			188	2224	-1580	696	184	437	322	322	322
			376	5898	-3185	2530	849	1739	1357	1357	1357
300	Primo Impalcato	53-53	0	2712	-1335	1044	657	827	688	688	688
			188	1031	-1697	-263	-648	-333	-436	-333	-333
			376	2707	-5415	-971	-2401	-1354	-1706	-1354	-1354
301	Primo Impalcato	54-54	0	635	-2021	-660	-1052	-693	-833	-693	-693
			188	1711	-1049	643	259	433	331	331	331
			376	4911	-2201	2400	965	1707	1355	1355	1355
302	Primo Impalcato	55-55	0	1977	-1581	378	92	254	197	198	198
			188	464	-1107	-322	-547	-322	-402	-322	-322
			376	2015	-3698	-519	-1542	-842	-1072	-842	-842
303	Primo Impalcato	56-56	0	900	-1304	-97	-369	-202	-256	-202	-202
			188	1124	-493	537	316	394	316	316	316
			376	3136	-1457	1528	508	1062	833	833	833
304	Primo Impalcato	57-57	0	695	-777	-8	-116	-37	-58	-41	-41
			188	275	-148	79	54	68	63	64	64
			376	1043	-706	355	55	210	150	168	168
305	Primo Impalcato	58-58	0	39	-45	4	-11	-2	-5	-3	-3
			188	1	-1	0	0	0	0	0	0
			376	45	-39	10	-4	4	1	3	3
306	Primo Impalcato	59-59	0	48	-49	8	-10	1	-2	-1	-1
			188	0	-1	0	0	0	0	0	0
			376	48	-48	9	-9	2	-2	0	0
307	Primo Impalcato	60-60	0	51	-50	10	-9	2	-1	0	0

	o										
			188	0	-1	0	0	0	0	0	0
			376	49	-50	8	-10	1	-3	-1	-1
308	Primo Impalcato	61-61	0	43	-42	8	-7	2	-1	0	0
			188	1	-1	0	0	0	0	0	0
			376	43	-44	7	-8	1	-2	-1	-1
309	Primo Impalcato	62-62	0	42	-42	8	-7	2	-1	0	0
			188	1	-1	0	0	0	0	0	0
			376	43	-44	7	-8	1	-2	0	0
310	Primo Impalcato	63-63	0	51	-50	9	-9	2	-2	0	0
			188	1	-1	0	0	0	0	0	0
			376	49	-49	9	-9	2	-2	0	0
311	Primo Impalcato	64-64	0	50	-51	9	-9	2	-2	0	0
			188	1	-1	0	0	0	0	0	0
			376	50	-49	9	-9	2	-2	0	0
312	Primo Impalcato	65-65	0	42	-42	7	-8	1	-2	0	0
			188	1	-1	0	0	0	0	0	0
			376	44	-43	8	-7	2	-1	0	0
313	Primo Impalcato	66-66	0	42	-42	7	-8	1	-2	0	0
			188	1	-1	0	0	0	0	0	0
			376	44	-43	9	-7	2	-1	1	1
314	Primo Impalcato	67-67	0	50	-51	9	-10	1	-2	-1	-1
			188	1	0	0	0	0	0	0	0
			376	50	-49	10	-8	3	-1	1	1
315	Primo Impalcato	68-68	0	49	-48	9	-8	2	-1	0	0
			188	1	0	0	0	0	0	0	0
			376	48	-49	9	-9	2	-2	0	0
316	Primo Impalcato	69-69	0	45	-39	11	-4	4	1	3	3
			188	1	0	0	0	0	0	0	0
			376	39	-44	4	-10	-1	-4	-3	-3
317	Primo Impalcato	70-70	0	743	-644	117	20	66	47	50	50
			188	85	-207	-50	-77	-59	-65	-61	-61
			376	694	-1105	-59	-356	-153	-213	-171	-171
318	Primo Impalcato	1-71	0	19	-18	2	-1	1	0	1	1
			102	6	-15	-3	-8	-4	-6	-4	-4
			204	6	-25	-9	-16	-10	-12	-10	-10
319	Primo Impalcato	1-92	0	15	-21	-2	-4	-2	-3	-2	-2
			103	24	-33	1	-7	-1	-3	-2	-2
			206	43	-58	5	-12	0	-3	-1	-1
320	Primo Impalcato	92-2	0	33	-19	9	0	4	2	2	2
			103	14	-16	0	-2	-1	-1	-1	-1
			206	41	-60	-1	-14	-4	-6	-4	-4
321	Primo Impalcato	6-89	0	57	-90	15	-30	3	-6	0	0
			100	36	-65	11	-23	2	-5	0	0
			200	29	-51	8	-15	1	-3	0	0
322	Primo	89-7	0	46	-62	7	-13	1	-3	0	0

	Impalcat o										
			100	37	-67	11	-22	2	-5	0	0
			200	57	-92	16	-31	3	-6	0	0
323	Primo Impalcat o	9-90	0	36	-72	15	-30	3	-6	0	0
			100	24	-50	10	-20	2	-4	0	0
			200	15	-26	5	-10	1	-2	0	0
324	Primo Impalcat o	90-1 0	0	39	-60	8	-15	1	-3	0	0
			100	24	-53	11	-21	2	-4	0	0
			200	40	-71	14	-28	3	-6	0	0
325	Primo Impalcat o	13-9 1	0	31	-41	-1	-13	-4	-6	-4	-4
			103	3	-6	0	-2	-1	-1	-1	-1
			206	28	-21	9	0	4	2	2	2
326	Primo Impalcat o	88-1 4	0	6	-25	-8	-16	-10	-12	-10	-10
			102	7	-17	-3	-8	-4	-6	-4	-4
			204	15	-12	2	-1	1	0	1	1
327	Primo Impalcat o	91-1 4	0	12	-26	5	-12	0	-3	-1	-1
			103	9	-16	1	-7	-1	-3	-2	-2
			206	16	-21	-2	-4	-2	-3	-2	-2
328	Primo Impalcat o	71-1 5	0	30	-11	11	6	8	7	7	7
			102	4	-4	1	0	0	0	0	0
			204	17	-31	-4	-11	-6	-8	-6	-6
329	Primo Impalcat o	16-8 8	0	19	-34	-4	-11	-6	-8	-6	-6
			102	4	-4	1	-1	0	0	0	0
			204	29	-13	11	6	8	7	7	7
330	Primo Impalcat o	17-7 2	0	26	-52	-10	-23	-13	-16	-13	-13
			100	17	-33	-5	-15	-8	-10	-8	-8
			199	29	-35	0	-7	-3	-4	-3	-3
331	Primo Impalcat o	87-1 8	0	35	-40	-1	-7	-3	-4	-3	-3
			100	19	-35	-5	-15	-8	-10	-8	-8
			199	36	-63	-10	-23	-13	-17	-13	-13
332	Primo Impalcat o	72-1 9	0	10	-15	-2	-5	-3	-3	-3	-3
			100	13	-28	-6	-14	-8	-10	-8	-8
			199	32	-58	-9	-23	-13	-16	-13	-13
333	Primo Impalcat o	20-8 7	0	41	-66	-9	-24	-13	-16	-13	-13
			100	15	-31	-6	-14	-8	-10	-8	-8
			199	13	-18	-2	-5	-3	-3	-3	-3
334	Primo Impalcat o	21-7 3	0	45	-69	-7	-23	-12	-16	-12	-12
			100	33	-47	-3	-16	-7	-10	-7	-7
			199	34	-40	0	-8	-3	-4	-3	-3
335	Primo Impalcat o	86-2 2	0	36	-41	0	-8	-3	-4	-3	-3
			100	32	-47	-3	-16	-7	-10	-7	-7
			199	46	-70	-7	-24	-12	-16	-12	-12
336	Primo Impalcat o	73-2 3	0	22	-28	-1	-7	-3	-4	-3	-3
			100	28	-42	-4	-15	-7	-10	-7	-7
			199	54	-78	-6	-24	-12	-16	-12	-12

337	Primo Impalcato	24-86	0	53	-76	-6	-24	-12	-16	-12	-12
			100	28	-43	-4	-15	-7	-10	-7	-7
			199	20	-26	-1	-7	-3	-4	-3	-3
338	Primo Impalcato	25-74	0	68	-90	-5	-24	-11	-15	-11	-11
			103	42	-56	-2	-15	-7	-9	-7	-7
			206	45	-50	0	-7	-2	-4	-3	-3
339	Primo Impalcato	85-26	0	42	-48	0	-8	-3	-4	-3	-3
			100	44	-59	-3	-16	-7	-10	-7	-7
			199	64	-89	-6	-25	-12	-16	-12	-12
340	Primo Impalcato	27-85	0	68	-91	-6	-24	-12	-16	-12	-12
			100	40	-55	-3	-16	-7	-10	-7	-7
			199	28	-33	0	-7	-3	-4	-3	-3
341	Primo Impalcato	74-28	0	30	-35	-1	-7	-3	-4	-3	-3
			103	39	-53	-2	-15	-7	-9	-7	-7
			206	69	-91	-4	-23	-11	-15	-11	-11
342	Primo Impalcato	84-29	0	44	-50	0	-8	-3	-4	-3	-3
			100	52	-67	-3	-16	-7	-10	-7	-7
			199	80	-104	-5	-25	-12	-16	-12	-12
343	Primo Impalcato	31-84	0	83	-107	-6	-25	-12	-16	-12	-12
			100	50	-64	-3	-16	-7	-10	-7	-7
			199	39	-45	0	-8	-3	-4	-3	-3
344	Primo Impalcato	83-33	0	43	-48	0	-7	-3	-4	-3	-3
			100	53	-67	-3	-16	-7	-10	-7	-7
			199	82	-105	-6	-24	-12	-16	-12	-12
345	Primo Impalcato	35-83	0	83	-106	-6	-24	-12	-16	-12	-12
			100	52	-67	-3	-16	-7	-10	-7	-7
			199	45	-50	0	-8	-3	-4	-3	-3
346	Primo Impalcato	82-37	0	39	-45	0	-7	-3	-4	-3	-3
			100	51	-66	-3	-16	-7	-10	-7	-7
			199	79	-102	-6	-24	-12	-16	-12	-12
347	Primo Impalcato	39-82	0	80	-104	-6	-24	-12	-16	-12	-12
			100	51	-66	-3	-16	-7	-10	-7	-7
			199	46	-52	0	-8	-3	-4	-3	-3
348	Primo Impalcato	78-43	0	35	-29	7	0	4	3	3	3
			100	58	-43	15	3	10	7	7	7
			199	96	-73	24	7	15	12	12	12
349	Primo Impalcato	81-44	0	31	-36	0	-7	-3	-4	-3	-3
			100	44	-59	-3	-16	-7	-10	-7	-7
			199	73	-97	-6	-24	-12	-16	-12	-12
350	Primo Impalcato	45-78	0	94	-70	24	7	15	12	12	12
			100	60	-45	15	4	10	7	7	7
			199	50	-45	7	1	4	3	3	3
351	Primo Impalcato	46-81	0	71	-94	-6	-23	-12	-15	-12	-12
			100	45	-60	-3	-15	-7	-10	-7	-7

			199	46	-51	0	-7	-3	-4	-3	-3
352	Primo Impalcato	77-47	0	30	-24	7	1	4	3	3	3
			100	45	-30	15	4	10	7	7	7
			199	82	-59	23	6	15	12	12	12
353	Primo Impalcato	80-48	0	25	-31	-1	-7	-3	-4	-3	-3
			100	30	-45	-4	-15	-7	-10	-7	-7
			199	60	-83	-6	-23	-12	-15	-12	-12
354	Primo Impalcato	49-77	0	75	-51	23	7	16	12	12	12
			100	50	-36	15	4	10	7	7	7
			199	44	-38	7	0	4	3	3	3
355	Primo Impalcato	50-80	0	50	-74	-7	-23	-12	-16	-12	-12
			100	36	-51	-3	-15	-7	-10	-7	-7
			199	36	-41	0	-7	-3	-4	-3	-3
356	Primo Impalcato	76-51	0	19	-13	5	2	3	3	3	3
			100	33	-17	14	6	10	8	8	8
			199	69	-44	23	9	16	13	13	13
357	Primo Impalcato	53-76	0	66	-39	23	10	17	13	13	13
			100	37	-21	15	5	10	8	8	8
			199	43	-37	7	1	4	3	3	3
358	Primo Impalcato	75-55	0	16	-33	-6	-11	-7	-8	-7	-7
			102	4	-5	0	-1	0	0	0	0
			204	36	-23	11	4	8	6	6	6
359	Primo Impalcato	56-79	0	32	-17	11	4	8	6	6	6
			102	4	-5	1	-1	0	0	0	0
			204	12	-28	-6	-11	-7	-8	-7	-7
360	Primo Impalcato	57-75	0	18	-20	1	-2	0	-1	-1	-1
			102	18	-9	8	3	6	4	4	4
			204	26	-7	16	9	12	10	10	10
361	Primo Impalcato	57-93	0	19	-13	4	2	3	2	2	2
			103	27	-24	7	-1	3	1	1	1
			206	45	-44	13	-5	3	0	1	1
362	Primo Impalcato	93-58	0	16	-22	0	-9	-2	-4	-2	-2
			103	16	-14	2	0	1	1	1	1
			206	47	-38	13	1	6	4	4	4
363	Primo Impalcato	61-95	0	58	-65	28	-14	6	-3	0	0
			100	38	-48	22	-11	4	-2	0	0
			200	36	-45	15	-8	3	-1	0	0
364	Primo Impalcato	95-62	0	39	-39	11	-6	2	-1	0	0
			100	42	-50	20	-10	4	-2	0	0
			200	49	-68	30	-15	6	-3	0	0
365	Primo Impalcato	96-65	0	23	-15	5	-10	1	-2	0	0
			100	38	-23	10	-20	2	-4	0	0
			200	55	-34	15	-30	3	-6	0	0
366	Primo Impalcato	66-96	0	56	-35	14	-28	3	-6	0	0

			100	39	-24	11	-21	2	-4	0	0
			200	38	-36	8	-15	1	-3	0	0
367	Primo Impalcat o	69-9 4	0	32	-20	13	1	6	4	4	4
			103	5	-4	2	0	1	1	1	1
			206	20	-22	0	-9	-2	-4	-2	-2
368	Primo Impalcat o	79-7 0	0	26	-7	15	8	12	9	9	9
			102	16	-7	8	3	6	4	4	4
			204	14	-14	1	-2	0	-1	-1	-1
369	Primo Impalcat o	94-7 0	0	12	-18	12	-4	3	0	1	1
			103	11	-11	7	-1	3	1	2	2
			206	17	-12	4	2	3	2	2	2
370	Primo Impalcat o	1-71	0	35	-26	9	-1	3	1	2	2
			102	28	-14	10	4	6	5	5	5
			204	30	-11	11	7	9	7	7	7
371	Primo Impalcat o	1-92	0	29	-15	11	5	8	6	6	6
			103	24	-11	9	3	6	4	4	4
			206	35	-22	9	0	4	2	2	2
372	Primo Impalcat o	92-2	0	43	-57	6	-12	1	-3	0	0
			103	65	-67	7	-6	3	0	2	2
			206	88	-79	8	-1	5	3	4	4
373	Primo Impalcat o	6-89	0	26	-27	4	-2	1	-1	0	0
			100	33	-37	2	-5	0	-1	0	0
			200	46	-63	7	-13	1	-3	0	0
374	Primo Impalcat o	89-7	0	30	-51	8	-15	1	-3	0	0
			100	23	-33	4	-8	1	-2	0	0
			200	16	-16	0	0	0	0	0	0
375	Primo Impalcat o	9-90	0	25	-25	0	-1	0	0	0	0
			100	26	-36	4	-8	1	-2	0	0
			200	41	-61	7	-15	1	-3	0	0
376	Primo Impalcat o	90-1 0	0	16	-28	5	-11	1	-2	0	0
			100	11	-12	1	-2	0	-1	0	0
			200	15	-15	7	-4	1	-1	0	0
377	Primo Impalcat o	13-9 1	0	28	-20	7	0	5	3	4	4
			103	19	-22	6	-5	3	0	2	2
			206	12	-25	5	-11	1	-2	0	0
378	Primo Impalcat o	88-1 4	0	31	-13	11	7	9	7	7	7
			102	19	-7	10	4	6	5	5	5
			204	25	-21	9	0	4	2	2	2
379	Primo Impalcat o	91-1 4	0	29	-23	9	0	4	2	2	2
			103	20	-8	9	3	6	4	4	4
			206	29	-15	11	5	8	6	6	6
380	Primo Impalcat o	71-1 5	0	6	-26	-9	-17	-10	-12	-10	-10
			102	10	-22	-6	-10	-6	-8	-6	-6
			204	16	-20	-1	-4	-2	-3	-2	-2
381	Primo Impalcat	16-8 8	0	18	-21	-1	-4	-2	-3	-2	-2

	o										
			102	9	-21	-6	-10	-6	-7	-6	-6
			204	6	-26	-9	-16	-10	-12	-10	-10
382	Primo Impalcato	17-72	0	22	-7	13	5	10	8	8	8
			100	12	-7	4	1	3	2	2	2
			199	10	-16	-3	-5	-3	-4	-3	-3
383	Primo Impalcato	87-18	0	13	-19	-2	-5	-3	-4	-3	-3
			100	14	-9	4	2	3	2	2	2
			199	23	-7	13	6	10	8	8	8
384	Primo Impalcato	72-19	0	28	-34	0	-7	-3	-4	-3	-3
			100	23	-19	3	1	2	2	2	2
			199	21	-7	10	7	8	7	7	7
385	Primo Impalcato	20-87	0	20	-7	10	7	8	7	7	7
			100	25	-21	3	1	2	2	2	2
			199	34	-40	-1	-7	-3	-4	-3	-3
386	Primo Impalcato	21-73	0	21	-9	10	4	7	6	6	6
			100	10	-7	2	1	2	1	1	1
			199	24	-30	-1	-7	-3	-4	-3	-3
387	Primo Impalcato	86-22	0	21	-27	-1	-7	-3	-4	-3	-3
			100	11	-8	2	1	2	1	1	1
			199	21	-9	10	4	7	6	6	6
388	Primo Impalcato	73-23	0	33	-39	0	-8	-3	-4	-3	-3
			100	25	-22	3	0	2	1	2	2
			199	20	-8	9	6	7	6	6	6
389	Primo Impalcato	24-86	0	18	-6	9	6	7	6	6	6
			100	25	-22	3	0	2	1	2	2
			199	35	-41	0	-8	-3	-4	-3	-3
390	Primo Impalcato	25-74	0	25	-13	9	4	7	6	6	6
			103	14	-12	2	1	2	1	1	1
			206	31	-36	-1	-7	-3	-4	-3	-3
391	Primo Impalcato	85-26	0	28	-34	0	-8	-3	-4	-3	-3
			100	14	-11	2	1	2	1	2	2
			199	20	-8	9	5	7	6	6	6
392	Primo Impalcato	27-85	0	17	-5	9	5	7	6	6	6
			100	27	-24	3	0	2	1	2	2
			199	42	-48	0	-8	-3	-4	-3	-3
393	Primo Impalcato	74-28	0	45	-51	0	-8	-3	-4	-3	-3
			103	27	-25	2	1	2	1	1	1
			206	21	-9	9	4	7	6	6	6
394	Primo Impalcato	84-29	0	40	-46	0	-8	-3	-4	-3	-3
			100	21	-18	3	1	2	1	2	2
			199	17	-5	9	5	7	6	6	6
395	Primo Impalcato	31-84	0	14	-2	9	5	7	6	6	6
			100	27	-24	3	1	2	2	2	2
			199	45	-50	0	-8	-3	-4	-3	-3
396	Primo	83-3	0	45	-51	0	-8	-3	-4	-3	-3

	Impalcat o	3									
			100	24	-21	3	1	2	1	2	2
			199	15	-2	9	5	7	6	6	6
397	Primo Impalcat o	35-8 3	0	16	-1	10	5	7	6	6	6
			100	25	-22	2	1	2	2	2	2
			199	43	-49	0	-8	-3	-4	-3	-3
398	Primo Impalcat o	82-3 7	0	46	-52	0	-8	-3	-4	-3	-3
			100	27	-23	3	1	2	1	2	2
			199	15	-1	9	5	7	6	6	6
399	Primo Impalcat o	39-8 2	0	17	-4	10	5	7	6	6	6
			100	21	-18	2	1	2	2	2	2
			199	40	-45	0	-7	-3	-4	-3	-3
400	Primo Impalcat o	78-4 3	0	50	-45	7	1	4	3	3	3
			100	24	-27	-1	-3	-2	-2	-2	-2
			199	3	-15	-6	-9	-6	-7	-6	-6
401	Primo Impalcat o	81-4 4	0	46	-52	0	-8	-3	-4	-3	-3
			100	27	-24	3	1	2	1	2	2
			199	16	-4	9	5	7	6	6	6
402	Primo Impalcat o	45-7 8	0	9	-21	-5	-10	-6	-7	-6	-6
			100	13	-17	-1	-3	-2	-2	-2	-2
			199	36	-30	7	0	4	3	3	3
403	Primo Impalcat o	46-8 1	0	20	-8	10	5	7	6	6	6
			100	16	-13	2	1	2	2	2	2
			199	31	-37	-1	-7	-3	-4	-3	-3
404	Primo Impalcat o	77-4 7	0	43	-37	8	0	4	3	3	3
			100	24	-27	-1	-3	-1	-2	-2	-2
			199	6	-19	-6	-9	-6	-7	-6	-6
405	Primo Impalcat o	80-4 8	0	34	-40	0	-7	-3	-4	-3	-3
			100	26	-23	3	1	2	2	2	2
			199	21	-8	9	6	7	6	6	6
406	Primo Impalcat o	49-7 7	0	9	-21	-4	-10	-6	-7	-6	-6
			100	7	-10	-1	-2	-1	-2	-1	-1
			199	31	-25	7	1	4	3	3	3
407	Primo Impalcat o	50-8 0	0	22	-10	10	4	7	6	6	6
			100	11	-8	2	1	2	1	1	1
			199	27	-33	-1	-7	-3	-4	-3	-3
408	Primo Impalcat o	76-5 1	0	42	-37	7	1	4	3	3	3
			100	23	-27	-1	-3	-2	-2	-2	-2
			199	9	-22	-7	-10	-7	-8	-7	-7
409	Primo Impalcat o	53-7 6	0	10	-26	-6	-13	-8	-10	-8	-8
			100	10	-15	-2	-4	-2	-3	-2	-2
			199	20	-14	5	3	4	3	3	3
410	Primo Impalcat o	75-5 5	0	28	-8	17	9	12	10	10	10
			102	24	-11	10	6	8	6	6	6
			204	26	-22	4	1	3	2	2	2

411	Primo Impalcato	56-79	0	22	-17	4	2	3	2	2	2
			102	23	-10	10	6	8	6	6	6
			204	26	-6	16	9	12	10	10	10
412	Primo Impalcato	57-75	0	29	-33	1	-9	-1	-3	-2	-2
			102	14	-24	-4	-10	-5	-6	-5	-5
			204	15	-33	-7	-11	-7	-9	-7	-7
413	Primo Impalcato	57-93	0	19	-32	-5	-10	-6	-7	-6	-6
			103	11	-20	-3	-9	-4	-5	-4	-4
			206	18	-23	0	-9	-2	-4	-2	-2
414	Primo Impalcato	93-58	0	44	-45	12	-6	3	-1	0	0
			103	60	-63	6	-7	0	-3	-2	-2
			206	77	-85	1	-8	-3	-5	-4	-4
415	Primo Impalcato	61-95	0	31	-40	4	-7	1	-1	0	0
			100	30	-30	2	-1	1	0	0	0
			200	39	-40	11	-6	2	-1	0	0
416	Primo Impalcato	95-62	0	38	-47	15	-8	3	-1	0	0
			100	23	-27	8	-4	2	-1	0	0
			200	17	-16	1	0	0	0	0	0
417	Primo Impalcato	96-65	0	37	-36	7	-15	1	-3	0	0
			100	25	-25	4	-8	1	-2	0	0
			200	25	-25	1	-1	0	0	0	0
418	Primo Impalcato	66-96	0	15	-13	7	-4	1	-1	0	0
			100	11	-10	1	-2	0	-1	0	0
			200	24	-16	5	-11	1	-2	0	0
419	Primo Impalcato	69-94	0	19	-31	-1	-8	-3	-5	-4	-4
			103	13	-24	5	-6	-1	-3	-2	-2
			206	10	-18	11	-5	2	-1	0	0
420	Primo Impalcato	79-70	0	12	-29	-7	-11	-7	-8	-7	-7
			102	7	-16	-4	-10	-5	-6	-5	-5
			204	18	-22	0	-9	-2	-4	-2	-2
421	Primo Impalcato	94-70	0	22	-23	0	-9	-2	-4	-2	-2
			103	8	-17	-3	-10	-4	-6	-4	-4
			206	13	-26	-5	-11	-6	-8	-6	-6
422	Copertura	1-2	0	2294	-3590	1171	-2598	205	-548	-26	-26
			83	1739	-2742	850	-1814	163	-369	-3	-3
			166	2189	-2151	535	-1043	122	-193	19	19
423	Copertura	15-1	0	2600	-2233	258	-77	75	8	26	26
			80	2142	-2379	534	-1182	96	-248	-10	-10
			159	2303	-3590	1144	-2622	183	-570	-45	-45
424	Copertura	2-3	0	2180	-2144	536	-1048	122	-195	18	18
			69	2214	-2178	316	-590	78	-103	18	18
			138	2335	-2300	229	-187	61	-22	18	18
425	Copertura	3-4	0	2336	-2301	228	-188	61	-22	17	17
			69	1913	-1890	194	-165	50	-22	12	12
			138	1758	-1507	516	-235	110	-40	6	6
426	Copertura	4-5	0	1750	-1511	510	-233	108	-40	6	6
			69	2077	-1267	741	-351	152	-67	2	2

			138	2829	-1700	965	-466	193	-93	-2	-2
427	Copertura	5-6	0	2823	-1701	960	-464	192	-93	-2	-2
			69	3146	-1854	1106	-538	220	-109	-4	-4
			138	3462	-2025	1244	-608	246	-125	-7	-7
428	Copertura	6-7	0	3455	-2035	1239	-605	244	-124	-6	-6
			69	2651	-1585	1311	-642	258	-132	-7	-7
			138	2716	-1290	1375	-674	270	-139	-8	-8
429	Copertura	7-8	0	2729	-1305	1375	-674	270	-139	-8	-8
			69	2768	-899	1379	-676	271	-140	-8	-8
			138	3088	-1158	1375	-674	270	-140	-8	-8
430	Copertura	8-9	0	3094	-1164	1376	-675	270	-140	-8	-8
			69	3128	-1374	1310	-642	258	-133	-8	-8
			138	2310	-1738	1236	-605	244	-125	-7	-7
431	Copertura	9-10	0	2333	-1742	1239	-607	244	-125	-7	-7
			69	1957	-1572	1100	-536	218	-109	-5	-5
			138	1571	-1427	953	-461	190	-93	-3	-3
432	Copertura	10-11	0	1587	-1427	961	-465	191	-94	-3	-3
			69	1027	-1025	735	-349	149	-67	1	1
			138	1462	-1453	501	-228	106	-40	5	5
433	Copertura	11-12	0	1457	-1446	508	-231	107	-41	5	5
			69	2004	-1983	194	-165	48	-23	10	10
			138	2564	-2533	228	-188	59	-24	16	16
434	Copertura	12-13	0	2563	-2531	229	-188	60	-23	16	16
			69	2571	-2634	330	-610	79	-109	16	16
			138	2593	-3429	554	-1073	123	-202	16	16
435	Copertura	13-14	0	2595	-3409	553	-1067	124	-200	17	17
			83	2388	-4648	885	-1859	167	-381	-7	-7
			166	3089	-6368	1223	-2663	212	-565	-30	-30
436	Copertura	16-14	0	1205	-1566	-5	-305	-68	-128	-75	-75
			80	3530	-2014	1210	-570	252	-104	8	8
			159	6381	-3020	2726	-1136	632	-140	91	91
437	Copertura	15-17	0	1582	-1808	96	-242	6	-61	-14	-14
			66	1141	-1379	100	-160	18	-34	-2	-2
			132	1680	-1665	227	-196	54	-30	11	11
438	Copertura	16-18	0	2329	-2095	231	-44	73	18	30	30
			66	1331	-1171	156	-81	44	-3	14	14
			132	954	-958	211	-212	41	-44	-2	-2
439	Copertura	17-19	0	1410	-1360	146	-108	40	-11	13	13
			66	779	-761	194	-171	45	-28	7	7
			132	1892	-1737	238	-227	49	-43	2	2
440	Copertura	18-20	0	1624	-1565	126	-130	22	-29	-4	-4
			66	761	-766	181	-182	34	-39	-3	-3
			132	1404	-1289	230	-231	45	-48	-2	-2
441	Copertura	19-21	0	1429	-1271	173	-159	37	-30	2	2
			66	903	-819	188	-184	38	-37	0	0
			132	1515	-1700	201	-203	38	-42	-2	-2
442	Copertura	20-22	0	1214	-1216	168	-166	32	-34	-1	-1
			66	900	-826	189	-186	37	-38	-1	-1
			132	1269	-1440	202	-203	40	-41	-1	-1
443	Copertura	21-23	0	1562	-1426	155	-154	29	-33	-2	-2
			66	747	-752	157	-162	29	-34	-2	-2
			132	1316	-1467	155	-164	29	-35	-3	-3
444	Copertura	22-24	0	1180	-1149	158	-154	32	-31	0	0
			66	778	-779	159	-160	31	-33	-1	-1
			132	1133	-1137	153	-163	29	-34	-2	-2

445	Copertura	23-25	0	1444	-1446	126	-131	23	-28	-2	-2
			66	1299	-1304	127	-141	23	-30	-2	-2
			132	1963	-1968	126	-144	23	-31	-3	-3
446	Copertura	24-26	0	1092	-1212	126	-132	24	-28	-1	-1
			66	887	-888	118	-131	21	-28	-2	-2
			132	953	-959	103	-127	18	-28	-3	-3
447	Copertura	25-28	0	2485	-2490	109	-126	20	-27	-2	-2
			85	1056	-1061	83	-105	14	-23	-2	-2
			170	1685	-1788	48	-69	7	-16	-2	-2
448	Copertura	26-27	0	1828	-1928	85	-107	14	-24	-3	-3
			66	1015	-1021	93	-117	16	-26	-3	-3
			132	1986	-1992	93	-124	16	-28	-3	-3
449	Copertura	27-29	0	1598	-1604	86	-118	14	-26	-3	-3
			66	1507	-1513	68	-92	11	-21	-3	-3
			132	1856	-1860	42	-62	7	-14	-2	-2
450	Copertura	28-30	0	661	-627	42	-62	6	-15	-2	-2
			73	866	-956	41	-62	6	-14	-2	-2
			146	1846	-1915	36	-52	5	-12	-2	-2
451	Copertura	29-31	0	1610	-1614	41	-63	6	-15	-2	-2
			66	1352	-1356	32	-49	5	-11	-2	-2
			132	1404	-1407	17	-31	2	-7	-1	-1
452	Copertura	30-32	0	1397	-1403	34	-53	5	-13	-2	-2
			69	1164	-1168	28	-44	4	-10	-2	-2
			137	1571	-1573	18	-27	2	-7	-1	-1
453	Copertura	31-33	0	1566	-1569	19	-36	2	-9	-2	-2
			66	1305	-1307	16	-28	2	-7	-1	-1
			132	1571	-1572	6	-16	1	-4	-1	-1
454	Copertura	32-34	0	1511	-1514	19	-33	3	-8	-1	-1
			69	1232	-1234	15	-27	2	-6	-1	-1
			138	1675	-1687	7	-12	1	-3	-1	-1
455	Copertura	33-35	0	1770	-1777	10	-24	1	-6	-1	-1
			66	1360	-1360	9	-17	2	-4	0	0
			132	1511	-1511	2	-7	1	-1	0	0
456	Copertura	34-36	0	1836	-1842	10	-21	1	-5	-1	-1
			69	1255	-1256	8	-16	1	-4	0	0
			138	1580	-1580	3	-4	1	-1	0	0
457	Copertura	35-37	0	1651	-1652	6	-17	1	-4	0	0
			66	1248	-1247	8	-8	2	-1	1	1
			132	1607	-1603	5	-1	3	1	2	2
458	Copertura	36-38	0	1525	-1525	7	-14	1	-3	0	0
			69	1102	-1101	6	-8	2	-1	1	1
			138	1701	-1699	7	-3	3	1	1	1
459	Copertura	37-39	0	1456	-1453	8	-7	3	0	1	1
			66	1114	-1109	7	1	3	2	2	2
			132	1164	-1158	25	-5	8	2	3	3
460	Copertura	38-40	0	1637	-1632	6	-5	2	0	1	1
			69	1039	-1035	6	1	3	2	2	2
			137	1317	-1312	19	-1	6	2	3	3
461	Copertura	39-41	0	1310	-1303	15	2	6	3	3	3
			66	1290	-1263	42	-17	11	0	3	3
			132	2982	-2909	72	-35	17	-4	3	3
462	Copertura	40-42	0	1447	-1441	10	2	4	3	3	3
			69	1669	-1662	22	-4	8	3	4	4
			138	3224	-3213	32	-9	10	2	4	4
463	Copertura	41-4	0	2370	-2285	66	-29	16	-2	4	4

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			66	904	-898	21	3	7	3	3	3
			132	2761	-2756	60	-40	14	-6	2	2
464	Copertura	42-43	0	2425	-2415	39	-16	12	1	5	5
			23	1447	-1438	29	3	10	5	5	5
			46	1149	-1116	36	-8	12	3	5	5
465	Copertura	43-45	0	2729	-2709	28	-1	10	4	5	5
			66	1173	-1166	57	-22	15	-1	4	4
			132	2015	-2073	84	-65	19	-11	2	2
466	Copertura	44-46	0	3651	-3688	67	-45	16	-7	3	3
			66	2214	-2209	79	-58	18	-9	3	3
			132	1738	-1733	85	-68	19	-12	2	2
467	Copertura	45-47	0	1825	-1820	98	-77	22	-13	3	3
			66	1344	-1342	116	-108	24	-21	1	1
			132	1873	-2003	131	-131	26	-27	0	0
468	Copertura	46-48	0	1983	-1978	98	-78	22	-13	3	3
			66	1385	-1383	117	-105	25	-20	1	1
			132	1439	-1565	128	-128	26	-26	0	0
469	Copertura	47-49	0	1574	-1580	156	-153	31	-31	0	0
			66	1073	-1076	163	-168	31	-35	-1	-1
			132	1283	-1452	166	-177	31	-38	-3	-3
470	Copertura	48-50	0	1437	-1436	154	-150	31	-29	1	1
			66	1012	-1012	164	-165	33	-33	0	0
			132	1129	-1131	168	-176	33	-36	-1	-1
471	Copertura	49-51	0	1521	-1525	208	-215	40	-45	-2	-2
			66	890	-893	197	-205	38	-42	-1	-1
			132	1612	-1447	183	-189	36	-38	0	0
472	Copertura	50-52	0	1398	-1400	207	-213	41	-43	-1	-1
			66	890	-886	196	-206	37	-43	-2	-2
			132	1441	-1447	179	-195	33	-42	-3	-3
473	Copertura	51-53	0	2005	-2008	245	-248	49	-49	0	0
			66	917	-907	201	-195	44	-35	5	5
			132	1302	-1283	154	-136	38	-19	9	9
474	Copertura	52-54	0	1512	-1790	239	-254	45	-54	-3	-3
			66	880	-893	188	-209	32	-47	-6	-6
			132	1404	-1423	131	-160	18	-40	-9	-9
475	Copertura	53-55	0	1646	-1631	232	-217	53	-37	8	8
			66	1155	-1170	102	-169	13	-41	-7	-7
			132	1624	-1669	87	-255	-3	-71	-22	-22
476	Copertura	54-56	0	962	-863	217	-229	41	-48	-3	-3
			66	1198	-1170	155	-98	43	-7	14	14
			132	2413	-2344	232	-44	73	18	30	30
477	Copertura	55-57	0	2370	-2437	70	-269	-16	-84	-33	-33
			80	2538	-1830	1178	-535	245	-97	8	8
			159	2618	-3117	2625	-1139	574	-179	49	49
478	Copertura	56-70	0	1513	-1422	264	-33	93	34	45	45
			80	2351	-2248	569	-1219	101	-256	-11	-11
			159	3641	-3480	1172	-2703	169	-606	-67	-67
479	Copertura	57-58	0	2545	-3185	2601	-1165	552	-202	29	29
			83	2101	-2065	1816	-846	372	-160	6	6
			166	2257	-2293	1044	-533	195	-121	-18	-18
480	Copertura	58-59	0	2249	-2283	1049	-533	196	-120	-17	-17
			69	2329	-2363	591	-314	104	-77	-17	-17
			138	2463	-2497	182	-225	21	-60	-17	-17
481	Copertura	59-60	0	2464	-2497	182	-225	22	-59	-17	-17

			69	2025	-2048	160	-191	21	-49	-11	-11
			138	1616	-1628	235	-516	40	-110	-6	-6
482	Copertura	60-61	0	1619	-1631	233	-510	40	-108	-6	-6
			69	1426	-1382	351	-742	67	-152	-2	-2
			138	2061	-2040	466	-966	93	-194	2	2
483	Copertura	61-62	0	2069	-2047	462	-958	92	-192	2	2
			69	2248	-2243	536	-1104	108	-220	4	4
			138	2456	-2447	606	-1243	124	-246	6	6
484	Copertura	62-63	0	2453	-2444	605	-1240	124	-245	6	6
			69	2073	-1946	641	-1313	131	-259	6	6
			138	1929	-1465	674	-1379	139	-272	7	7
485	Copertura	63-64	0	1936	-1476	674	-1378	139	-272	7	7
			69	1720	-1234	676	-1382	139	-272	7	7
			138	2253	-1310	674	-1377	139	-272	7	7
486	Copertura	64-65	0	2255	-1313	674	-1378	139	-272	7	7
			69	2518	-1574	641	-1312	132	-259	7	7
			138	2805	-1894	604	-1238	124	-245	6	6
487	Copertura	65-66	0	2826	-1912	606	-1241	124	-245	6	6
			69	2365	-1631	535	-1102	109	-219	4	4
			138	1910	-1491	460	-954	92	-190	2	2
488	Copertura	66-67	0	1917	-1490	464	-962	93	-192	2	2
			69	1079	-1159	348	-736	67	-150	-1	-1
			138	1513	-1523	227	-502	40	-106	-5	-5
489	Copertura	67-68	0	1507	-1518	230	-508	40	-107	-5	-5
			69	2068	-2089	163	-189	23	-48	-10	-10
			138	2640	-2781	185	-222	23	-58	-16	-16
490	Copertura	68-69	0	2638	-2774	185	-223	23	-59	-16	-16
			69	2658	-2828	610	-330	109	-79	-16	-16
			138	2694	-2918	1075	-554	203	-122	-15	-15
491	Copertura	69-70	0	2696	-2909	1069	-553	201	-123	-16	-16
			83	2490	-2748	1862	-882	384	-164	9	9
			166	3475	-3719	2668	-1218	570	-207	35	35
492	Copertura	1-1	0	2029	-2123	14	-98	-36	-58	-47	-47
			220	259	-296	26	-79	-10	-30	-19	-19
			440	1580	-1561	91	-38	27	1	10	10
493	Copertura	2-2	0	32	-37	2	-8	-2	-4	-3	-3
			220	2	-1	1	0	0	0	0	0
			440	39	-32	9	-1	5	3	4	4
494	Copertura	3-3	0	36	-40	3	-8	-1	-3	-2	-2
			220	1	-1	0	0	0	0	0	0
			440	41	-37	8	-4	3	1	2	2
495	Copertura	4-4	0	37	-40	4	-8	0	-3	-1	-1
			220	0	0	0	0	0	0	0	0
			440	40	-38	7	-5	2	0	1	1
496	Copertura	5-5	0	39	-41	5	-8	0	-2	-1	-1
			220	1	-1	0	0	0	0	0	0
			440	42	-40	8	-6	2	0	1	1
497	Copertura	6-6	0	36	-37	5	-6	0	-2	-1	-1
			220	1	-1	0	0	0	0	0	0
			440	36	-35	6	-5	2	0	1	1
498	Copertura	7-7	0	37	-37	5	-6	1	-1	0	0
			220	1	-1	0	0	0	0	0	0
			440	36	-35	5	-5	1	-1	0	0
499	Copertura	8-8	0	41	-41	7	-7	1	-1	0	0
			220	1	-1	0	0	0	0	0	0

			440	43	-43	7	-7	1	-2	0	0
500	Copertura	9-9	0	37	-36	6	-5	1	-1	0	0
			220	1	-1	0	0	0	0	0	0
			440	35	-36	5	-6	1	-1	0	0
501	Copertura	10-10	0	37	-36	7	-5	2	0	1	1
			220	1	-1	0	0	0	0	0	0
			440	35	-36	4	-6	0	-2	-1	-1
502	Copertura	11-11	0	41	-38	8	-5	3	0	1	1
			220	1	-1	0	0	0	0	0	0
			440	39	-41	5	-8	0	-3	-1	-1
503	Copertura	12-12	0	40	-36	8	-3	3	1	2	2
			220	1	-1	0	0	0	0	0	0
			440	37	-41	4	-8	-1	-3	-2	-2
504	Copertura	13-13	0	37	-31	8	-2	4	2	3	3
			220	0	-1	0	-1	0	0	0	0
			440	31	-38	1	-9	-3	-5	-4	-4
505	Copertura	57-57	0	1966	-2058	18	-102	-34	-58	-46	-46
			220	262	-350	26	-79	-10	-31	-19	-19
			440	1530	-1499	93	-41	26	0	8	8
506	Copertura	58-58	0	32	-37	2	-8	-2	-4	-3	-3
			220	2	-1	1	0	0	0	0	0
			440	39	-32	9	-1	5	3	4	4
507	Copertura	59-59	0	36	-40	4	-8	-1	-3	-2	-2
			220	1	-1	0	0	0	0	0	0
			440	41	-37	8	-4	3	1	2	2
508	Copertura	60-60	0	39	-42	5	-8	0	-3	-1	-1
			220	1	-1	0	0	0	0	0	0
			440	43	-40	8	-5	2	0	1	1
509	Copertura	61-61	0	37	-39	5	-6	0	-2	-1	-1
			220	1	-1	0	0	0	0	0	0
			440	38	-36	6	-4	2	0	1	1
510	Copertura	62-62	0	39	-39	5	-6	1	-1	0	0
			220	1	-1	0	0	0	0	0	0
			440	38	-37	6	-5	1	-1	0	0
511	Copertura	63-63	0	43	-43	6	-7	1	-1	0	0
			220	1	-1	0	0	0	0	0	0
			440	44	-44	7	-7	1	-1	0	0
512	Copertura	64-64	0	43	-43	7	-6	1	-1	0	0
			220	1	-1	0	0	0	0	0	0
			440	44	-44	7	-7	1	-1	0	0
513	Copertura	65-65	0	40	-39	6	-5	2	-1	0	0
			220	1	-1	0	0	0	0	0	0
			440	38	-38	5	-6	1	-1	0	0
514	Copertura	66-66	0	40	-38	7	-5	2	0	1	1
			220	1	-1	0	0	0	0	0	0
			440	37	-39	4	-6	0	-2	-1	-1
515	Copertura	67-67	0	43	-41	8	-5	3	0	1	1
			220	1	-1	0	0	0	0	0	0
			440	42	-44	5	-8	0	-3	-1	-1
516	Copertura	68-68	0	42	-38	8	-3	3	1	2	2
			220	1	-1	0	0	0	0	0	0
			440	39	-44	4	-9	-1	-3	-2	-2
517	Copertura	69-69	0	39	-33	8	-2	4	2	3	3
			220	0	-1	0	-1	0	0	0	0
			440	33	-40	1	-9	-3	-5	-4	-4

518	Copertura	1-74	0	293	-277	20	-6	10	5	6	6
			118	94	-85	9	-1	5	3	4	4
			235	125	-122	4	-1	2	1	1	1
519	Copertura	74-2	0	104	-102	4	-2	2	1	1	1
			118	67	-62	7	1	3	2	2	2
			235	55	-45	16	0	6	3	4	4
520	Copertura	6-71	0	37	-38	0	0	0	0	0	0
			115	13	-14	1	0	0	0	0	0
			231	46	-46	2	-1	0	0	0	0
521	Copertura	71-7	0	43	-44	6	-3	1	-1	0	0
			115	26	-27	4	-2	1	0	0	0
			231	36	-37	3	-1	0	0	0	0
522	Copertura	9-72	0	32	-32	5	-3	1	-1	0	0
			115	8	-8	7	-3	1	-1	0	0
			231	38	-39	8	-4	2	-1	0	0
523	Copertura	72-10	0	26	-26	0	-1	0	0	0	0
			115	20	-21	0	0	0	0	0	0
			231	28	-28	0	0	0	0	0	0
524	Copertura	73-13	0	31	-31	0	-3	-1	-1	-1	-1
			118	9	-18	-1	-8	-2	-4	-2	-2
			235	11	-22	1	-16	-3	-6	-4	-4
525	Copertura	14-73	0	51	-64	2	-15	-5	-9	-6	-6
			118	15	-21	0	-8	-4	-5	-4	-4
			235	46	-48	-1	-2	-1	-2	-1	-1
526	Copertura	57-75	0	269	-284	6	-20	-5	-10	-7	-7
			118	84	-93	1	-9	-3	-5	-4	-4
			235	113	-116	1	-4	-1	-2	-1	-1
527	Copertura	75-58	0	95	-97	2	-4	-1	-2	-1	-1
			118	61	-72	-2	-7	-2	-3	-2	-2
			235	38	-61	0	-16	-3	-6	-3	-3
528	Copertura	77-61	0	26	-26	0	0	0	0	0	0
			115	12	-13	0	0	0	0	0	0
			231	34	-34	0	0	0	0	0	0
529	Copertura	62-77	0	65	-59	5	-2	1	-1	0	0
			115	25	-19	6	-3	1	-1	0	0
			231	49	-49	8	-4	1	-1	0	0
530	Copertura	65-78	0	44	-43	3	-5	1	-1	0	0
			115	8	-13	3	-7	1	-1	0	0
			231	48	-48	4	-8	1	-2	0	0
531	Copertura	78-66	0	35	-35	0	0	0	0	0	0
			115	19	-19	0	0	0	0	0	0
			231	37	-36	0	0	0	0	0	0
532	Copertura	69-76	0	14	-20	1	-17	-3	-7	-4	-4
			118	10	-15	-1	-8	-2	-4	-2	-2
			235	28	-30	0	-3	-1	-1	-1	-1
533	Copertura	76-70	0	38	-41	-1	-2	-1	-2	-1	-1
			118	12	-26	0	-8	-4	-5	-4	-4
			235	40	-67	1	-16	-6	-9	-7	-7
534	Copertura	1-74	0	300	-310	-2	-13	-4	-6	-4	-4
			118	100	-104	-1	-5	-2	-3	-2	-2
			235	106	-105	3	-1	1	0	1	1
535	Copertura	74-2	0	120	-118	3	0	2	1	1	1
			118	50	-50	0	-1	0	0	0	0
			235	43	-51	-1	-4	-1	-2	-1	-1
536	Copertura	6-71	0	55	-44	8	-4	2	-1	0	0

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			115	16	-15	7	-3	1	-1	0	0
			231	44	-44	6	-3	1	-1	0	0
537	Copertura	71-7	0	45	-45	2	-1	0	0	0	0
			115	9	-7	3	-1	1	0	0	0
			231	47	-44	4	-2	1	0	0	0
538	Copertura	9-72	0	35	-34	1	-1	0	0	0	0
			115	16	-16	0	0	0	0	0	0
			231	27	-28	0	0	0	0	0	0
539	Copertura	72-10	0	35	-36	8	-4	2	-1	0	0
			115	21	-10	8	-4	2	-1	0	0
			231	32	-29	9	-4	2	-1	0	0
540	Copertura	73-13	0	42	-46	-1	-2	-2	-2	-2	-2
			118	10	-10	2	-1	0	0	0	0
			235	51	-45	5	0	2	1	1	1
541	Copertura	14-73	0	64	-55	7	4	5	4	4	4
			118	19	-15	4	1	2	2	2	2
			235	32	-33	1	-2	0	-1	-1	-1
542	Copertura	15-125	0	1756	-1897	81	-100	10	-27	-7	-7
			75	722	-826	78	-86	13	-20	-3	-3
			150	678	-675	75	-71	17	-13	2	2
543	Copertura	127-16	0	655	-634	88	-59	27	-2	11	11
			75	683	-698	72	-90	8	-25	-7	-7
			150	907	-963	57	-122	-12	-47	-26	-26
544	Copertura	17-129	0	1834	-1946	79	-84	15	-18	-1	-1
			75	739	-833	72	-74	14	-15	0	0
			150	721	-720	65	-65	13	-12	0	0
545	Copertura	130-18	0	697	-694	67	-63	14	-11	1	1
			75	810	-809	74	-72	15	-14	0	0
			150	1179	-1183	80	-81	15	-17	-1	-1
546	Copertura	19-135	0	1778	-1856	63	-65	12	-13	0	0
			75	691	-777	56	-59	11	-12	0	0
			150	722	-723	50	-52	10	-11	0	0
547	Copertura	134-20	0	699	-698	53	-50	11	-9	1	1
			75	792	-791	58	-55	12	-11	1	1
			150	1142	-1151	64	-61	13	-12	1	1
548	Copertura	21-136	0	1559	-1606	44	-47	9	-10	0	0
			75	610	-668	39	-42	8	-9	0	0
			150	690	-691	35	-38	7	-8	0	0
549	Copertura	138-22	0	665	-664	37	-35	8	-7	0	0
			75	672	-682	42	-39	9	-7	1	1
			150	861	-870	47	-44	10	-8	1	1
550	Copertura	23-141	0	1612	-1634	29	-31	5	-7	0	0
			75	626	-660	26	-28	5	-6	0	0
			150	656	-657	23	-25	4	-5	0	0
551	Copertura	142-24	0	631	-630	25	-23	5	-4	0	0
			75	691	-701	28	-25	6	-5	0	0
			150	917	-926	31	-28	7	-5	0	0
552	Copertura	25-145	0	1751	-1755	16	-18	3	-4	0	0
			75	680	-694	15	-16	3	-3	0	0
			150	636	-637	13	-15	3	-3	0	0
553	Copertura	146-26	0	585	-586	14	-14	3	-3	0	0
			75	784	-796	16	-15	3	-3	0	0
			150	1172	-1181	19	-17	4	-3	0	0
554	Copertura	150-27	0	547	-560	7	-9	1	-2	-1	-1

			75	795	-807	7	-8	1	-2	0	0
			150	1230	-1240	7	-7	1	-1	0	0
555	Copertura	28-149	0	1827	-1828	6	-6	1	-1	0	0
			75	712	-712	6	-5	2	-1	0	0
			150	614	-609	7	-4	2	0	1	1
556	Copertura	154-29	0	488	-503	6	-9	0	-3	-1	-1
			75	631	-643	6	-8	1	-2	-1	-1
			150	854	-864	7	-7	1	-1	0	0
557	Copertura	30-153	0	1528	-1528	5	-5	1	-1	0	0
			75	562	-560	4	-3	2	0	1	1
			150	580	-574	4	0	2	1	1	1
558	Copertura	158-31	0	459	-474	6	-10	0	-3	-1	-1
			75	588	-600	6	-8	1	-2	-1	-1
			150	784	-794	7	-7	1	-1	0	0
559	Copertura	32-157	0	1536	-1537	5	-5	1	-1	0	0
			75	567	-566	6	-3	2	0	1	1
			150	558	-551	6	0	3	2	2	2
560	Copertura	162-33	0	462	-478	5	-10	-1	-4	-2	-2
			75	664	-672	6	-9	0	-3	-1	-1
			150	1036	-1044	7	-8	1	-2	0	0
561	Copertura	34-161	0	1669	-1677	8	-5	2	-1	0	0
			75	590	-590	8	-2	3	0	1	1
			150	561	-554	8	0	3	2	2	2
562	Copertura	166-35	0	458	-474	6	-10	-1	-4	-2	-2
			75	751	-762	6	-10	0	-3	-1	-1
			150	1246	-1256	7	-9	1	-2	0	0
563	Copertura	36-165	0	1792	-1796	9	-5	2	-1	0	0
			75	634	-635	9	-2	3	0	1	1
			150	554	-546	10	0	4	2	2	2
564	Copertura	170-37	0	451	-464	5	-11	-1	-4	-2	-2
			75	676	-687	6	-11	0	-3	-1	-1
			150	1017	-1026	7	-10	1	-2	0	0
565	Copertura	38-169	0	1590	-1598	10	-6	2	-1	0	0
			75	548	-552	10	-3	3	0	1	1
			150	551	-539	10	-1	4	2	2	2
566	Copertura	175-39	0	440	-453	5	-11	-1	-4	-2	-2
			75	605	-615	6	-10	1	-3	-1	-1
			150	808	-816	7	-9	2	-2	0	0
567	Copertura	40-173	0	1484	-1492	9	-6	2	-1	0	0
			75	537	-540	10	-3	3	0	1	1
			150	542	-531	10	-1	4	2	2	2
568	Copertura	178-41	0	420	-429	5	-8	0	-3	-1	-1
			75	630	-636	6	-7	1	-2	0	0
			150	925	-931	7	-6	2	-1	0	0
569	Copertura	42-177	0	1639	-1648	7	-7	1	-2	-1	-1
			75	587	-591	8	-4	2	0	1	1
			150	599	-589	8	-2	3	1	2	2
570	Copertura	43-181	0	1824	-1833	7	-7	1	-2	0	0
			75	674	-680	7	-6	1	-1	0	0
			150	631	-623	6	-6	1	-1	0	0
571	Copertura	182-44	0	471	-478	6	-8	1	-2	-1	-1
			75	766	-771	6	-7	1	-1	0	0
			150	1244	-1248	7	-6	2	-1	0	0
572	Copertura	45-185	0	1835	-1845	11	-13	2	-3	0	0
			75	693	-700	10	-12	2	-3	0	0

			150	667	-657	8	-10	1	-2	0	0
573	Copertura	186-46	0	568	-578	11	-9	2	-1	0	0
			75	818	-827	12	-10	3	-2	0	0
			150	1251	-1260	13	-10	3	-2	0	0
574	Copertura	47-189	0	1581	-1591	21	-24	4	-5	-1	-1
			75	585	-589	19	-22	3	-5	-1	-1
			150	690	-672	16	-19	3	-4	0	0
575	Copertura	190-48	0	581	-599	19	-17	4	-3	0	0
			75	738	-755	22	-19	5	-3	0	0
			150	988	-1007	25	-21	5	-4	1	1
576	Copertura	49-193	0	1627	-1638	37	-41	7	-9	-1	-1
			75	618	-626	33	-36	6	-8	-1	-1
			150	722	-691	29	-32	6	-7	0	0
577	Copertura	195-50	0	639	-638	33	-30	7	-6	0	0
			75	722	-768	36	-33	7	-6	0	0
			150	901	-933	39	-36	8	-7	0	0
578	Copertura	51-197	0	1710	-1722	57	-60	11	-13	-1	-1
			75	653	-654	51	-54	10	-11	0	0
			150	774	-728	45	-47	9	-10	0	0
579	Copertura	199-52	0	691	-691	47	-46	9	-9	0	0
			75	799	-869	53	-52	11	-10	0	0
			150	1106	-1176	59	-57	12	-11	0	0
580	Copertura	53-201	0	1891	-1896	78	-77	16	-15	1	1
			75	752	-749	69	-70	14	-14	0	0
			150	793	-734	60	-63	11	-13	-1	-1
581	Copertura	202-54	0	695	-705	60	-64	10	-15	-2	-2
			75	873	-957	71	-68	15	-13	1	1
			150	1289	-1391	81	-71	20	-11	3	3
582	Copertura	55-205	0	1826	-1814	95	-81	24	-11	6	6
			75	743	-739	81	-78	18	-14	2	2
			150	746	-686	67	-75	11	-18	-3	-3
583	Copertura	206-56	0	640	-649	67	-75	11	-18	-3	-3
			75	753	-841	83	-75	19	-13	3	3
			150	1036	-1134	99	-76	28	-7	9	9
584	Copertura	57-75	0	298	-289	13	2	7	4	4	4
			118	103	-99	5	1	3	2	2	2
			235	98	-99	1	-3	0	-1	-1	-1
585	Copertura	75-58	0	109	-113	0	-3	-1	-2	-1	-1
			118	52	-51	1	0	0	0	0	0
			235	35	-32	4	1	2	1	1	1
586	Copertura	77-61	0	47	-47	8	-4	1	-1	0	0
			115	20	-11	8	-4	2	-1	0	0
			231	32	-32	9	-4	2	-1	0	0
587	Copertura	62-77	0	36	-37	2	-1	0	0	0	0
			115	7	-7	1	0	0	0	0	0
			231	28	-28	0	0	0	0	0	0
588	Copertura	65-78	0	41	-41	1	-1	0	0	0	0
			115	15	-15	0	0	0	0	0	0
			231	37	-36	0	0	0	0	0	0
589	Copertura	78-66	0	46	-46	4	-8	1	-2	0	0
			115	14	-11	4	-8	1	-2	0	0
			231	35	-37	4	-9	1	-2	0	0
590	Copertura	69-76	0	39	-35	5	0	2	1	1	1
			118	12	-11	2	-1	0	0	0	0
			235	36	-38	-1	-2	-1	-2	-1	-1

591	Copertura	76-70	0	30	-32	1	-2	0	-1	-1	-1
			118	19	-13	4	2	3	2	2	2
			235	51	-41	8	5	6	5	5	5
592	Copertura	79-81	0	136	13	110	67	86	71	71	71
			80	33	-43	15	-10	7	3	5	5
			159	-29	-127	-61	-92	-61	-74	-61	-61
593	Copertura	80-82	0	24	-85	-24	-36	-24	-29	-24	-24
			66	5	-43	-19	-28	-19	-22	-19	-19
			132	19	-53	-12	-20	-13	-16	-13	-13
594	Copertura	83-84	0	34	-36	0	-2	-1	-1	-1	-1
			66	14	-14	2	-2	0	0	0	0
			132	41	-40	3	-1	1	0	1	1
595	Copertura	85-86	0	26	-25	1	-1	0	0	0	0
			66	17	-17	1	-1	0	0	0	0
			132	45	-47	1	-1	0	0	0	0
596	Copertura	87-88	0	29	-29	1	-1	0	0	0	0
			66	25	-25	1	-1	0	0	0	0
			132	44	-44	0	-1	0	0	0	0
597	Copertura	89-90	0	33	-33	0	-1	0	0	0	0
			66	27	-28	0	0	0	0	0	0
			132	39	-40	0	0	0	0	0	0
598	Copertura	91-92	0	34	-34	0	0	0	0	0	0
			66	30	-30	0	0	0	0	0	0
			132	32	-32	0	0	0	0	0	0
599	Copertura	93-94	0	42	-42	0	0	0	0	0	0
			66	27	-27	0	0	0	0	0	0
			132	26	-27	0	0	0	0	0	0
600	Copertura	95-96	0	32	-31	1	0	0	0	0	0
			66	29	-29	1	0	0	0	0	0
			132	45	-44	1	0	0	0	0	0
601	Copertura	97-106	0	37	-36	2	-1	1	0	0	0
			66	29	-30	2	-1	1	0	0	0
			132	33	-33	2	-1	1	0	0	0
602	Copertura	98-99	0	30	-38	-4	-6	-4	-5	-4	-4
			66	15	-20	-1	-5	-3	-3	-3	-3
			132	31	-33	3	-6	0	-2	-1	-1
603	Copertura	100-101	0	37	-36	1	0	0	0	0	0
			66	17	-16	2	-1	1	0	0	0
			132	36	-36	3	-2	1	0	0	0
604	Copertura	102-103	0	50	-50	1	-1	0	0	0	0
			66	16	-16	1	-1	0	0	0	0
			132	45	-45	1	-1	0	0	0	0
605	Copertura	104-105	0	43	-44	0	-1	0	0	0	0
			66	18	-18	0	-1	0	0	0	0
			132	37	-36	0	0	0	0	0	0
606	Copertura	107-108	0	33	-37	0	-5	-2	-3	-2	-2
			66	24	-33	-3	-8	-4	-5	-4	-4
			132	25	-37	-6	-10	-6	-8	-6	-6
607	Copertura	109-110	0	5	-114	-43	-66	-43	-52	-43	-43
			80	51	-26	21	-5	13	8	10	10
			159	135	-4	97	52	75	62	62	62
608	Copertura	111-112	0	46	-47	0	-1	0	0	0	0
			66	16	-16	0	0	0	0	0	0
			132	42	-42	0	0	0	0	0	0
609	Copertura	113-	0	39	-39	0	0	0	0	0	0

	a	114									
			66	13	-13	0	0	0	0	0	0
			132	41	-40	1	0	0	0	0	0
610	Copertura	115-116	0	23	-23	0	-1	0	0	0	0
			66	13	-13	0	0	0	0	0	0
			132	22	-22	1	0	0	0	0	0
611	Copertura	117-118	0	52	-52	2	-1	0	0	0	0
			66	18	-18	1	-1	0	0	0	0
			132	35	-35	1	-1	0	0	0	0
612	Copertura	119-120	0	47	-48	4	-3	1	0	1	1
			66	9	-9	2	-2	0	-1	0	0
			132	43	-45	-1	-2	-1	-1	-1	-1
613	Copertura	121-122	0	28	-49	-6	-16	-8	-11	-8	-8
			66	5	-25	-9	-14	-9	-11	-9	-9
			132	42	-68	-10	-15	-10	-12	-10	-10
614	Copertura	124-125	0	65	-45	14	8	10	8	8	8
			99	119	-114	8	-1	4	2	3	3
			198	181	-188	1	-10	-3	-5	-3	-3
615	Copertura	125-127	0	772	-773	76	-78	15	-16	0	0
			775	114	-111	4	-4	1	0	1	1
			1550	678	-674	80	-74	18	-13	2	2
616	Copertura	126-127	0	-10	-80	-36	-54	-36	-43	-36	-36
			99	14	-39	-11	-19	-12	-14	-12	-12
			198	55	-30	20	12	15	13	13	13
617	Copertura	128-129	0	63	-60	4	-1	2	1	1	1
			99	123	-122	5	-4	1	-1	0	0
			198	188	-190	5	-7	0	-2	-1	-1
618	Copertura	129-130	0	819	-819	68	-69	13	-14	0	0
			775	103	-103	0	0	0	0	0	0
			1550	728	-727	70	-67	14	-13	1	1
619	Copertura	131-130	0	36	-40	-1	-3	-2	-2	-2	-2
			99	34	-32	2	-3	0	-1	0	0
			198	47	-45	6	-3	2	0	1	1
620	Copertura	132-135	0	65	-66	3	-4	0	-1	0	0
			99	124	-125	4	-5	1	-1	0	0
			198	188	-189	6	-6	1	-1	0	0
621	Copertura	133-134	0	37	-36	2	-2	0	0	0	0
			99	34	-31	2	-2	1	0	0	0
			198	45	-45	4	-3	1	0	0	0
622	Copertura	135-134	0	826	-827	52	-55	10	-11	-1	-1
			775	103	-103	1	0	0	0	0	0
			1550	732	-731	55	-52	11	-10	0	0
623	Copertura	137-136	0	63	-63	3	-4	0	-1	0	0
			99	122	-123	5	-5	1	-1	0	0
			198	190	-190	6	-6	1	-1	0	0
624	Copertura	136-138	0	795	-796	37	-40	7	-8	0	0
			775	103	-103	0	0	0	0	0	0
			1550	699	-698	40	-37	8	-7	0	0
625	Copertura	139-138	0	29	-28	1	0	1	0	0	0
			99	28	-27	2	-2	1	0	0	0
			198	45	-45	3	-4	1	-1	0	0
626	Copertura	140-141	0	64	-64	3	-3	1	-1	0	0
			99	123	-123	5	-5	1	-1	0	0
			198	189	-189	6	-6	1	-1	0	0
627	Copertura	141-142	0	776	-777	24	-27	5	-6	0	0

			775	103	-103	0	0	0	0	0	0
			1550	661	-661	27	-24	6	-5	0	0
628	Copertura	143-142	0	33	-31	1	-1	0	0	0	0
			99	29	-28	2	-2	0	0	0	0
			198	40	-40	3	-4	0	-1	0	0
629	Copertura	144-145	0	65	-65	3	-3	1	-1	0	0
			99	123	-123	5	-5	1	-1	0	0
			198	185	-185	6	-6	1	-1	0	0
630	Copertura	145-146	0	752	-753	14	-15	3	-3	0	0
			775	98	-98	0	0	0	0	0	0
			1550	615	-614	16	-14	3	-3	0	0
631	Copertura	147-146	0	37	-37	1	-1	0	0	0	0
			99	32	-29	2	-3	0	-1	0	0
			198	41	-43	3	-4	0	-1	-1	-1
632	Copertura	148-149	0	68	-68	4	-3	1	0	0	0
			99	123	-125	4	-6	0	-2	-1	-1
			198	181	-184	4	-8	0	-3	-1	-1
633	Copertura	149-150	0	722	-717	6	-6	1	-1	0	0
			775	98	-97	0	0	0	0	0	0
			1550	564	-567	6	-6	1	-1	0	0
634	Copertura	151-150	0	43	-41	1	-1	0	0	0	0
			99	34	-31	2	-3	0	-1	0	0
			198	35	-36	3	-4	0	-2	-1	-1
635	Copertura	152-153	0	61	-60	4	-3	1	0	0	0
			99	119	-121	4	-6	0	-2	-1	-1
			198	180	-185	4	-9	-1	-3	-2	-2
636	Copertura	153-154	0	690	-681	6	-6	1	-1	0	0
			775	102	-102	0	0	0	0	0	0
			1551	503	-511	5	-6	1	-1	0	0
637	Copertura	155-154	0	34	-34	1	0	0	0	0	0
			99	26	-25	1	-3	0	-1	-1	-1
			198	36	-39	1	-6	-1	-3	-2	-2
638	Copertura	156-157	0	65	-65	4	-3	1	0	0	0
			99	120	-122	4	-6	0	-2	-1	-1
			198	179	-184	4	-9	-1	-3	-2	-2
639	Copertura	157-158	0	668	-659	6	-6	2	-1	0	0
			775	102	-103	0	0	0	0	0	0
			1551	476	-483	5	-6	1	-1	0	0
640	Copertura	159-158	0	33	-33	1	-1	0	0	0	0
			99	26	-25	1	-3	0	-1	-1	-1
			198	27	-31	1	-6	-1	-3	-2	-2
641	Copertura	160-161	0	65	-65	4	-3	1	0	0	0
			99	120	-122	4	-6	0	-2	-1	-1
			198	176	-182	3	-9	-1	-4	-2	-2
642	Copertura	161-162	0	667	-660	7	-6	2	-1	0	0
			776	102	-102	0	0	0	0	0	0
			1551	479	-485	5	-7	1	-2	0	0
643	Copertura	163-162	0	41	-41	1	0	1	0	0	0
			99	29	-28	1	-3	-1	-1	-1	-1
			198	27	-31	1	-6	-2	-3	-2	-2
644	Copertura	164-165	0	69	-68	4	-3	1	0	0	0
			99	121	-123	3	-6	0	-2	-1	-1
			198	176	-182	3	-9	-1	-4	-2	-2
645	Copertura	165-166	0	656	-651	8	-6	2	-1	0	0
			776	102	-102	0	0	0	0	0	0

			1551	471	-477	5	-8	1	-2	0	0
646	Copertura	167-166	0	44	-43	1	0	1	0	0	0
			99	32	-31	1	-3	-1	-1	-1	-1
			198	24	-25	1	-6	-2	-3	-2	-2
647	Copertura	168-169	0	65	-64	4	-3	1	0	0	0
			99	118	-120	3	-6	0	-2	-1	-1
			198	177	-183	3	-9	-2	-4	-2	-2
648	Copertura	169-170	0	656	-644	9	-6	2	-1	0	0
			776	101	-101	0	0	0	0	0	0
			1552	457	-469	5	-9	1	-2	0	0
649	Copertura	171-170	0	39	-38	1	0	1	0	0	0
			99	26	-26	1	-3	-1	-2	-1	-1
			198	23	-24	0	-6	-2	-3	-2	-2
650	Copertura	172-173	0	63	-62	4	-3	1	0	0	0
			99	117	-120	3	-6	0	-2	-1	-1
			198	179	-185	3	-10	-2	-4	-3	-3
651	Copertura	173-175	0	651	-638	8	-6	2	-1	0	0
			776	101	-101	0	0	0	0	0	0
			1552	451	-463	5	-8	1	-2	0	0
652	Copertura	174-175	0	35	-33	1	0	1	0	0	0
			99	21	-23	1	-3	-1	-2	-1	-1
			198	20	-22	0	-7	-2	-4	-2	-2
653	Copertura	176-177	0	63	-62	4	-3	1	0	0	0
			99	117	-120	3	-6	0	-2	-1	-1
			198	180	-186	3	-10	-2	-4	-3	-3
654	Copertura	177-178	0	708	-699	7	-6	1	-1	0	0
			776	138	-137	1	-1	0	0	0	0
			1552	430	-438	5	-6	1	-1	0	0
655	Copertura	179-178	0	31	-30	1	-1	1	0	0	0
			99	21	-22	1	-3	0	-1	-1	-1
			198	14	-16	1	-5	-1	-3	-2	-2
656	Copertura	180-181	0	63	-63	3	-3	1	-1	0	0
			99	120	-120	5	-5	1	-1	0	0
			198	182	-182	6	-6	1	-1	0	0
657	Copertura	181-182	0	742	-736	6	-6	1	-1	0	0
			775	136	-135	1	-1	0	0	0	0
			1550	482	-486	5	-5	1	-1	0	0
658	Copertura	183-182	0	34	-34	1	-1	0	0	0	0
			99	24	-26	2	-3	0	-1	0	0
			198	17	-19	2	-5	-1	-2	-1	-1
659	Copertura	184-185	0	64	-64	3	-3	1	-1	0	0
			99	122	-122	5	-5	1	-1	0	0
			198	185	-185	6	-6	1	-1	0	0
660	Copertura	185-186	0	779	-771	9	-11	1	-3	0	0
			775	102	-101	0	0	0	0	0	0
			1550	581	-590	11	-9	3	-1	0	0
661	Copertura	187-186	0	39	-39	1	-1	0	0	0	0
			99	29	-29	2	-2	0	-1	0	0
			198	24	-24	3	-3	1	-1	0	0
662	Copertura	188-189	0	62	-62	3	-3	1	-1	0	0
			99	121	-121	5	-5	1	-1	0	0
			198	187	-187	6	-6	1	-1	0	0
663	Copertura	189-190	0	808	-791	18	-21	3	-5	0	0
			775	102	-102	0	0	0	0	0	0
			1550	602	-618	21	-18	5	-3	0	0

664	Copertura	191-190	0	36	-36	1	-1	0	0	0	0
			99	26	-26	2	-2	0	-1	0	0
			198	31	-31	3	-4	0	-1	0	0
665	Copertura	192-193	0	62	-61	4	-3	1	0	0	0
			99	122	-122	5	-5	1	-1	0	0
			198	189	-189	6	-6	1	-1	0	0
666	Copertura	193-195	0	844	-814	31	-34	6	-7	0	0
			775	103	-103	0	0	0	0	0	0
			1550	665	-664	34	-31	7	-6	0	0
667	Copertura	194-195	0	37	-36	1	-2	0	-1	0	0
			99	27	-27	2	-2	0	-1	0	0
			198	31	-32	3	-3	1	-1	0	0
668	Copertura	196-197	0	65	-64	4	-3	1	0	0	0
			99	123	-122	5	-4	1	-1	0	0
			198	188	-187	6	-6	1	-1	0	0
669	Copertura	197-199	0	895	-848	48	-50	9	-10	0	0
			775	103	-103	1	-1	0	0	0	0
			1550	718	-718	50	-48	10	-9	0	0
670	Copertura	198-199	0	39	-40	0	-1	0	-1	-1	-1
			99	30	-31	1	-3	0	-1	0	0
			198	34	-35	3	-4	0	-1	0	0
671	Copertura	200-201	0	61	-64	1	-4	-1	-2	-1	-1
			99	122	-122	4	-5	1	-1	0	0
			198	190	-187	7	-5	2	0	1	1
672	Copertura	201-202	0	911	-849	64	-66	13	-13	0	0
			775	103	-103	0	-1	0	0	0	0
			1550	721	-722	65	-65	13	-13	0	0
673	Copertura	203-202	0	46	-37	8	4	6	5	5	5
			99	36	-31	4	-1	2	1	1	1
			198	35	-40	0	-7	-2	-4	-2	-2
674	Copertura	204-205	0	47	-69	-8	-14	-8	-10	-8	-8
			99	114	-119	1	-8	-2	-4	-2	-2
			198	188	-180	10	-1	5	3	3	3
675	Copertura	205-206	0	867	-799	74	-76	14	-16	-1	-1
			775	118	-110	5	-3	1	-1	0	0
			1550	667	-667	75	-74	15	-15	0	0
676	Copertura	207-206	0	59	-30	17	11	13	11	11	11
			99	36	-27	7	1	4	3	3	3
			198	27	-36	-2	-10	-5	-6	-5	-5
677	Copertura	79-14	0	249	-323	38	-96	-17	-44	-25	-25
			125	286	-291	19	-23	0	-8	-2	-2
			250	833	-793	82	-63	34	5	20	20
678	Copertura	124-15	0	4563	538	3520	2389	2879	2389	2389	2389
			155	2404	573	1938	1284	1549	1284	1284	1284
			310	1481	-895	356	71	235	178	180	180
679	Copertura	80-16	0	141	-2012	-808	-1239	-808	-975	-808	-808
			45	654	-1652	-448	-780	-499	-604	-499	-499
			90	1206	-1588	-84	-356	-190	-244	-191	-191
680	Copertura	128-17	0	4927	-415	3405	2256	2742	2256	2256	2256
			155	2714	407	2253	1474	1787	1474	1474	1474
			310	1792	-407	1051	659	832	692	692	692
681	Copertura	82-18	0	223	-2571	-1123	-1720	-1123	-1358	-1123	-1123
			43	658	-2468	-903	-1383	-905	-1091	-905	-905
			85	1133	-2506	-653	-1043	-687	-825	-687	-687
682	Copertura	132-	0	5547	-1015	3486	2266	2755	2266	2266	2266

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			155	3017	-41	2305	1488	1805	1488	1488	1488
			310	1535	-105	1073	693	856	710	710	710
683	Copertura	83-20	0	169	-2545	-1140	-1760	-1140	-1380	-1140	-1140
			43	371	-2223	-923	-1421	-926	-1120	-926	-926
			85	664	-2090	-696	-1078	-713	-860	-713	-713
684	Copertura	137-21	0	6364	-1810	3550	2277	2768	2277	2277	2277
			155	3375	-427	2308	1474	1788	1474	1474	1474
			310	1907	-353	1015	650	809	671	671	671
685	Copertura	84-22	0	367	-2852	-1114	-1737	-1114	-1350	-1114	-1114
			43	370	-2499	-876	-1379	-893	-1080	-893	-893
			85	466	-2166	-650	-1018	-672	-811	-672	-672
686	Copertura	140-23	0	7266	-2705	3587	2280	2772	2280	2280	2280
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687	Copertura	85-24	0	527	-2872	-1089	-1731	-1105	-1339	-1105	-1105
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			85	424	-2165	-636	-996	-659	-794	-659	-659
688	Copertura	144-25	0	8269	-3704	3607	2283	2775	2283	2283	2283
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689	Copertura	86-26	0	802	-3015	-1082	-1740	-1107	-1341	-1107	-1107
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			85	627	-1948	-637	-1000	-661	-797	-661	-661
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			85	631	-1953	-639	-999	-661	-797	-661	-661
691	Copertura	148-28	0	8716	-4152	3614	2282	2774	2282	2282	2282
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692	Copertura	88-29	0	1221	-3436	-1077	-1745	-1108	-1342	-1108	-1108
			43	1026	-2797	-852	-1376	-885	-1071	-885	-885
			85	983	-2309	-640	-1003	-663	-799	-663	-663
693	Copertura	152-30	0	9024	-4467	3614	2278	2770	2278	2278	2278
			155	4584	-1644	2340	1447	1786	1470	1470	1470
			310	2426	-954	1012	609	798	662	662	662
694	Copertura	89-31	0	1354	-3570	-1077	-1746	-1108	-1342	-1108	-1108
			43	1171	-2943	-852	-1377	-886	-1071	-886	-886
			85	1137	-2465	-639	-1005	-664	-800	-664	-664
695	Copertura	156-32	0	9209	-4653	3614	2278	2769	2278	2278	2278
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			310	1983	-657	1010	624	799	663	663	663
696	Copertura	90-33	0	1322	-3539	-1078	-1744	-1108	-1342	-1108	-1108
			43	1053	-2825	-852	-1377	-886	-1071	-886	-886
			85	938	-2266	-640	-1006	-664	-800	-664	-664
697	Copertura	160-34	0	9128	-4570	3613	2279	2770	2279	2279	2279
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698	Copertura	91-35	0	1351	-3567	-1080	-1742	-1108	-1342	-1108	-1108
			43	1098	-2870	-854	-1375	-886	-1071	-886	-886
			85	992	-2320	-640	-1005	-664	-800	-664	-664
699	Copertura	164-36	0	9210	-4650	3610	2280	2772	2280	2280	2280
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700	Copertura	92-37	0	1247	-3463	-1082	-1740	-1108	-1342	-1108	-1108

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701	Copertura	168-38	0	9288	-4728	3605	2280	2771	2280	2280	2280
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702	Copertura	93-39	0	1348	-3566	-1083	-1741	-1109	-1343	-1109	-1109
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			85	1074	-2404	-639	-1009	-665	-801	-665	-665
703	Copertura	172-40	0	9021	-4464	3601	2278	2769	2278	2278	2278
			155	4690	-1743	2331	1473	1788	1473	1473	1473
			310	2383	-1045	1008	663	806	669	669	669
704	Copertura	94-41	0	1279	-3495	-1082	-1740	-1108	-1342	-1108	-1108
			43	1158	-2929	-853	-1376	-886	-1071	-886	-886
			85	1167	-2494	-636	-1008	-663	-800	-663	-663
705	Copertura	176-42	0	8702	-4148	3600	2277	2768	2277	2277	2277
			155	4561	-1618	2313	1472	1785	1472	1472	1472
			310	1808	-476	992	666	803	666	666	666
706	Copertura	180-43	0	8589	-4036	3598	2277	2768	2277	2277	2277
			155	4511	-1565	2315	1473	1788	1473	1473	1473
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707	Copertura	95-44	0	989	-3207	-1085	-1740	-1109	-1344	-1109	-1109
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708	Copertura	184-45	0	8314	-3759	3587	2277	2769	2277	2277	2277
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			310	2278	-947	999	666	803	666	666	666
709	Copertura	96-46	0	1073	-3284	-1087	-1731	-1106	-1339	-1106	-1106
			43	1006	-2773	-855	-1369	-883	-1068	-883	-883
			85	1077	-2399	-636	-1003	-661	-797	-661	-661
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			155	3877	-934	2314	1471	1785	1471	1471	1471
			310	2210	-800	1005	639	800	663	663	663
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			43	883	-2650	-860	-1367	-884	-1069	-884	-884
			85	1022	-2420	-637	-1003	-662	-798	-662	-662
712	Copertura	192-49	0	6777	-2220	3542	2278	2770	2278	2278	2278
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			43	323	-2286	-878	-1378	-894	-1081	-894	-894
			85	372	-1995	-651	-1021	-674	-813	-674	-674
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			310	2067	-646	1075	692	857	711	711	711
715	Copertura	107-52	0	227	-2507	-1140	-1758	-1140	-1380	-1140	-1140
			43	262	-2114	-924	-1419	-926	-1119	-926	-926
			85	382	-1806	-694	-1077	-712	-858	-712	-712
716	Copertura	200-53	0	5936	-1422	3403	2257	2743	2257	2257	2257
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			310	2733	-1345	1053	661	833	694	694	694
717	Copertura	108-54	0	36	-2275	-1119	-1712	-1119	-1353	-1119	-1119
			43	309	-2119	-904	-1383	-905	-1092	-905	-905
			85	642	-2024	-658	-1049	-691	-830	-691	-691
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			155	2420	480	1941	1287	1552	1287	1287	1287

			310	1973	-1612	356	70	235	178	181	181
719	Copertura	109-56	0	42	-1844	-755	-1159	-755	-912	-755	-755
			43	455	-1490	-414	-736	-470	-568	-470	-470
			85	931	-1301	-76	-347	-183	-237	-185	-185
720	Copertura	110-70	0	412	-453	-20	-43	-20	-28	-20	-20
			43	609	-614	22	-45	1	-12	-3	-3
			85	806	-776	75	-68	28	-1	15	15
721	Copertura	14-79	0	1096	-892	164	62	119	99	102	102
			95	669	-590	110	-20	54	28	39	39
			190	251	-319	40	-94	-14	-41	-23	-23
722	Copertura	15-124	0	80	-475	-162	-259	-167	-201	-167	-167
			65	1916	188	1500	1021	1231	1021	1021	1021
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			65	-7	-2106	-1027	-1510	-1027	-1239	-1027	-1027
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			65	2152	-223	1451	964	1173	964	964	964
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725	Copertura	18-131	0	431	-121	247	136	188	155	155	155
			65	519	-2446	-963	-1452	-963	-1172	-963	-963
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726	Copertura	19-132	0	140	-452	-131	-254	-156	-191	-156	-156
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727	Copertura	20-133	0	469	-154	256	134	192	157	157	157
			65	711	-2644	-966	-1485	-966	-1176	-966	-966
			130	1369	-5549	-2090	-3221	-2090	-2542	-2090	-2090
728	Copertura	21-137	0	185	-497	-126	-259	-156	-191	-156	-156
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729	Copertura	22-139	0	515	-203	261	126	192	156	156	156
			65	825	-2770	-973	-1516	-973	-1184	-973	-973
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732	Copertura	25-144	0	359	-686	-122	-279	-163	-202	-163	-163
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733	Copertura	26-147	0	613	-291	273	126	199	161	161	161
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737	Copertura	30-152	0	718	-1047	-107	-259	-149	-186	-149	-149
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738	Copertura	31-159	0	703	-406	258	110	185	149	149	149
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739	Copertura	32-156	0	778	-1099	-107	-255	-147	-183	-147	-147
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740	Copertura	33-163	0	730	-438	253	108	182	146	146	146
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742	Copertura	35-167	0	731	-440	251	107	180	145	145	145
			65	2113	-4070	-979	-1547	-979	-1191	-979	-979
			130	4431	-8637	-2103	-3335	-2103	-2557	-2103	-2103
743	Copertura	36-164	0	913	-1225	-106	-252	-146	-181	-146	-146
			65	4126	-2167	1547	980	1192	980	980	980
			130	8549	-4339	3337	2105	2559	2105	2105	2105
744	Copertura	37-171	0	731	-443	248	106	179	144	144	144
			65	2146	-4105	-980	-1544	-980	-1192	-980	-980
			130	4520	-8726	-2103	-3327	-2103	-2557	-2103	-2103
745	Copertura	38-168	0	991	-1296	-105	-249	-144	-179	-144	-144
			65	4173	-2212	1546	981	1193	981	981	981
			130	8610	-4401	3332	2105	2559	2105	2105	2105
746	Copertura	39-174	0	750	-464	246	106	178	143	143	143
			65	2096	-4057	-980	-1542	-980	-1192	-980	-980
			130	4408	-8615	-2103	-3321	-2103	-2557	-2103	-2103
747	Copertura	40-172	0	1064	-1364	-104	-243	-140	-174	-140	-140
			65	4064	-2101	1547	981	1194	981	981	981
			130	8360	-4154	3328	2103	2557	2103	2103	2103
748	Copertura	41-179	0	670	-377	249	112	181	147	147	147
			65	2065	-4022	-979	-1540	-979	-1191	-979	-979
			130	4274	-8483	-2104	-3322	-2104	-2558	-2104	-2104
749	Copertura	42-176	0	1126	-1421	-116	-235	-140	-173	-140	-140
			65	3870	-1908	1549	981	1193	981	981	981
			130	8067	-3863	3327	2102	2556	2102	2102	2102
750	Copertura	43-180	0	316	-631	-139	-259	-157	-193	-157	-157
			65	3727	-1782	1536	972	1183	972	972	972
			130	7955	-3752	3326	2102	2556	2102	2102	2102
751	Copertura	44-183	0	772	-449	274	126	200	162	162	162
			65	1809	-3752	-971	-1528	-971	-1182	-971	-971
			130	3915	-8122	-2104	-3321	-2104	-2558	-2104	-2104
752	Copertura	45-184	0	363	-678	-126	-266	-157	-195	-157	-157
			65	3573	-1628	1529	973	1183	973	973	973
			130	7708	-3503	3316	2103	2557	2103	2103	2103
753	Copertura	46-187	0	654	-334	268	128	197	160	160	160
			65	1762	-3705	-971	-1522	-971	-1182	-971	-971
			130	3678	-7882	-2102	-3306	-2102	-2556	-2102	-2102
754	Copertura	47-188	0	292	-607	-127	-265	-158	-194	-158	-158
			65	3334	-1386	1522	974	1184	974	974	974
			130	7135	-2926	3301	2105	2559	2105	2105	2105
755	Copertura	48-1	0	593	-279	263	126	194	157	157	157

	a	91									
			65	1429	-3373	-972	-1517	-972	-1183	-972	-972
			130	3007	-7209	-2101	-3289	-2101	-2555	-2101	-2101
756	Copertura	49-192	0	229	-542	-129	-260	-156	-192	-156	-156
			65	2939	-992	1510	973	1184	973	973	973
			130	6277	-2070	3274	2103	2558	2103	2103	2103
757	Copertura	50-194	0	513	-200	258	129	192	156	156	156
			65	954	-2896	-971	-1504	-971	-1182	-971	-971
			130	2011	-6209	-2099	-3262	-2099	-2552	-2099	-2099
758	Copertura	51-196	0	182	-498	-135	-257	-158	-193	-158	-158
			65	2717	-782	1482	968	1178	968	968	968
			130	5755	-1567	3218	2094	2546	2094	2094	2094
759	Copertura	52-198	0	474	-165	251	130	188	154	154	154
			65	581	-2514	-966	-1479	-966	-1176	-966	-966
			130	1203	-5376	-2087	-3205	-2087	-2538	-2087	-2087
760	Copertura	53-200	0	140	-452	-138	-248	-156	-189	-156	-156
			65	2648	-720	1450	964	1173	964	964	964
			130	5479	-1311	3146	2084	2534	2084	2084	2084
761	Copertura	54-203	0	404	-93	246	138	188	155	155	155
			65	443	-2370	-963	-1448	-963	-1172	-963	-963
			130	807	-4971	-2082	-3140	-2082	-2531	-2082	-2082
762	Copertura	55-204	0	77	-491	-164	-261	-168	-202	-168	-168
			65	2176	-131	1502	1022	1233	1022	1022	1022
			130	4538	-111	3262	2213	2668	2213	2213	2213
763	Copertura	56-207	0	381	-38	256	159	198	165	165	165
			65	-25	-2069	-1028	-1510	-1028	-1240	-1028	-1028
			130	-215	-4403	-2222	-3274	-2222	-2679	-2222	-2222
764	Copertura	70-123	0	1059	-930	115	11	77	56	65	65
			95	663	-581	110	-17	56	31	41	41
			190	273	-237	88	-37	31	6	18	18
765	Copertura	81-80	0	-398	-3843	-1918	-2850	-1918	-2313	-1918	-1918
			80	-588	-2765	-1363	-2052	-1363	-1644	-1363	-1363
			160	144	-2016	-808	-1240	-808	-976	-808	-808
766	Copertura	126-81	0	-204	-4834	-2387	-3517	-2387	-2877	-2387	-2387
			30	-304	-4340	-2154	-3186	-2154	-2596	-2154	-2154
			60	-403	-3845	-1921	-2853	-1921	-2316	-1921	-1921
767	Copertura	98-82	0	391	-4316	-1951	-2965	-1951	-2370	-1951	-1951
			82	-366	-3189	-1537	-2349	-1537	-1864	-1537	-1537
			165	219	-2569	-1123	-1720	-1123	-1358	-1123	-1123
768	Copertura	99-83	0	863	-4793	-1965	-3036	-1965	-2387	-1965	-1965
			82	129	-3432	-1552	-2406	-1552	-1883	-1552	-1552
			165	173	-2546	-1140	-1761	-1140	-1380	-1140	-1140
769	Copertura	100-84	0	1251	-5183	-1966	-3080	-1966	-2389	-1966	-1966
			82	518	-3599	-1540	-2415	-1540	-1869	-1540	-1540
			165	363	-2851	-1114	-1737	-1114	-1350	-1114	-1114
770	Copertura	101-85	0	1829	-5762	-1967	-3107	-1967	-2389	-1967	-1967
			82	876	-3948	-1536	-2426	-1536	-1864	-1536	-1536
			165	530	-2873	-1089	-1732	-1105	-1339	-1105	-1105
771	Copertura	102-86	0	2469	-6403	-1967	-3124	-1967	-2390	-1967	-1967
			82	1305	-4379	-1537	-2439	-1537	-1865	-1537	-1537
			165	799	-3012	-1082	-1739	-1107	-1341	-1107	-1107
772	Copertura	103-87	0	2908	-6841	-1967	-3130	-1967	-2390	-1967	-1967
			82	1582	-4655	-1537	-2443	-1537	-1866	-1537	-1537
			165	909	-3122	-1079	-1741	-1107	-1340	-1107	-1107
773	Copertura	104-88	0	3276	-7208	-1966	-3133	-1966	-2391	-1966	-1966

			82	1834	-4908	-1537	-2446	-1537	-1867	-1537	-1537
			165	1219	-3435	-1077	-1745	-1108	-1342	-1108	-1108
774	Copertura	105-89	0	3515	-7448	-1966	-3132	-1966	-2390	-1966	-1966
			82	1946	-5021	-1537	-2446	-1537	-1867	-1537	-1537
			165	1355	-3571	-1077	-1746	-1108	-1342	-1108	-1108
775	Copertura	111-90	0	3568	-7445	-1939	-3084	-1939	-2355	-1939	-1939
			80	2029	-5077	-1524	-2421	-1524	-1849	-1524	-1524
			160	1322	-3538	-1078	-1744	-1108	-1342	-1108	-1108
776	Copertura	112-91	0	3562	-7494	-1966	-3120	-1966	-2388	-1966	-1966
			82	2044	-5118	-1537	-2438	-1537	-1865	-1537	-1537
			165	1351	-3567	-1080	-1742	-1108	-1342	-1108	-1108
777	Copertura	113-92	0	3641	-7572	-1966	-3113	-1966	-2388	-1966	-1966
			82	2017	-5091	-1537	-2434	-1537	-1865	-1537	-1537
			165	1247	-3463	-1082	-1740	-1108	-1342	-1108	-1108
778	Copertura	114-93	0	3525	-7458	-1966	-3109	-1966	-2389	-1966	-1966
			82	1951	-5027	-1538	-2432	-1538	-1866	-1538	-1538
			165	1346	-3564	-1083	-1740	-1109	-1343	-1109	-1109
779	Copertura	115-94	0	3380	-7313	-1967	-3110	-1967	-2389	-1967	-1967
			82	1761	-4836	-1537	-2432	-1537	-1866	-1537	-1537
			165	1281	-3497	-1082	-1740	-1108	-1342	-1108	-1108
780	Copertura	116-95	0	3121	-7054	-1967	-3109	-1967	-2389	-1967	-1967
			82	1640	-4716	-1538	-2432	-1538	-1866	-1538	-1538
			165	987	-3206	-1085	-1740	-1109	-1344	-1109	-1109
781	Copertura	117-96	0	2854	-6783	-1964	-3094	-1964	-2387	-1964	-1964
			82	1468	-4538	-1535	-2420	-1535	-1863	-1535	-1535
			165	1076	-3287	-1087	-1731	-1106	-1339	-1106	-1106
782	Copertura	118-97	0	2263	-6190	-1964	-3080	-1964	-2386	-1964	-1964
			82	1051	-4120	-1535	-2411	-1535	-1863	-1535	-1535
			165	866	-3078	-1095	-1727	-1106	-1340	-1106	-1106
783	Copertura	131-98	0	1000	-5509	-2255	-3406	-2255	-2740	-2255	-2255
			30	692	-4897	-2103	-3186	-2103	-2555	-2103	-2103
			60	392	-4316	-1951	-2965	-1951	-2370	-1951	-1951
784	Copertura	133-99	0	1478	-6006	-2264	-3485	-2264	-2752	-2264	-2264
			30	1168	-5397	-2114	-3262	-2114	-2570	-2114	-2114
			60	861	-4791	-1965	-3036	-1965	-2387	-1965	-1965
785	Copertura	139-100	0	1859	-6412	-2277	-3555	-2277	-2767	-2277	-2277
			30	1554	-5796	-2121	-3318	-2121	-2578	-2121	-2121
			60	1253	-5185	-1966	-3080	-1966	-2389	-1966	-1966
786	Copertura	143-101	0	2573	-7134	-2280	-3594	-2280	-2772	-2280	-2280
			30	2199	-6446	-2124	-3351	-2124	-2581	-2124	-2124
			60	1827	-5760	-1967	-3107	-1967	-2389	-1967	-1967
787	Copertura	147-102	0	3329	-7892	-2281	-3614	-2281	-2773	-2281	-2281
			30	2895	-7143	-2124	-3370	-2124	-2581	-2124	-2124
			60	2471	-6406	-1967	-3124	-1967	-2390	-1967	-1967
788	Copertura	151-103	0	3941	-8502	-2280	-3622	-2280	-2772	-2280	-2280
			30	3423	-7670	-2124	-3377	-2124	-2581	-2124	-2124
			60	2906	-6839	-1967	-3130	-1967	-2390	-1967	-1967
789	Copertura	155-104	0	4451	-9009	-2279	-3624	-2279	-2770	-2279	-2279
			30	3861	-8106	-2122	-3379	-2122	-2580	-2122	-2122
			60	3278	-7210	-1966	-3133	-1966	-2390	-1966	-1966
790	Copertura	159-105	0	4765	-9322	-2279	-3622	-2279	-2770	-2279	-2279
			30	4138	-8383	-2123	-3378	-2123	-2580	-2123	-2123
			60	3514	-7447	-1966	-3132	-1966	-2390	-1966	-1966
791	Copertura	119-106	0	1501	-5430	-1965	-3060	-1965	-2387	-1965	-1965
			82	691	-3770	-1540	-2403	-1540	-1869	-1540	-1540

			165	375	-2614	-1115	-1732	-1115	-1350	-1115	-1115
792	Copertura	120-107	0	799	-4720	-1961	-3021	-1961	-2382	-1961	-1961
			82	245	-3345	-1550	-2396	-1550	-1881	-1550	-1550
			165	222	-2503	-1140	-1757	-1140	-1381	-1140	-1140
793	Copertura	121-108	0	360	-4263	-1951	-2957	-1951	-2369	-1951	-1951
			82	-233	-3030	-1535	-2342	-1535	-1861	-1535	-1535
			165	41	-2279	-1119	-1713	-1119	-1353	-1119	-1119
794	Copertura	122-109	0	-364	-3789	-1963	-2915	-1963	-2366	-1963	-1963
			82	-490	-2636	-1358	-2043	-1358	-1638	-1358	-1358
			165	42	-1840	-753	-1156	-753	-909	-753	-753
795	Copertura	123-110	0	273	-237	88	-37	31	6	18	18
			82	215	-185	42	-41	5	-12	-2	-2
			165	409	-454	-22	-46	-22	-30	-22	-22
796	Copertura	163-111	0	4871	-9428	-2278	-3616	-2278	-2769	-2278	-2278
			33	4212	-8429	-2108	-3350	-2108	-2562	-2108	-2108
			65	3566	-7444	-1939	-3083	-1939	-2355	-1939	-1939
797	Copertura	167-112	0	4756	-9312	-2278	-3608	-2278	-2769	-2278	-2278
			30	4148	-8392	-2122	-3365	-2122	-2579	-2122	-2122
			60	3563	-7495	-1966	-3120	-1966	-2388	-1966	-1966
798	Copertura	171-113	0	4858	-9414	-2278	-3599	-2278	-2769	-2278	-2278
			30	4248	-8492	-2122	-3357	-2122	-2578	-2122	-2122
			60	3640	-7571	-1966	-3113	-1966	-2388	-1966	-1966
799	Copertura	174-114	0	4739	-9296	-2278	-3593	-2278	-2769	-2278	-2278
			30	4131	-8376	-2122	-3352	-2122	-2579	-2122	-2122
			60	3526	-7458	-1966	-3109	-1966	-2389	-1966	-1966
800	Copertura	179-115	0	4601	-9161	-2280	-3595	-2280	-2771	-2280	-2280
			30	3988	-8235	-2123	-3353	-2123	-2580	-2123	-2123
			60	3378	-7311	-1967	-3110	-1967	-2389	-1967	-1967
801	Copertura	183-116	0	4196	-8754	-2279	-3593	-2279	-2770	-2279	-2279
			30	3658	-7904	-2123	-3352	-2123	-2580	-2123	-2123
			60	3121	-7054	-1967	-3109	-1967	-2389	-1967	-1967
802	Copertura	187-117	0	3956	-8511	-2277	-3577	-2277	-2768	-2277	-2277
			30	3403	-7645	-2121	-3336	-2121	-2578	-2121	-2121
			60	2853	-6781	-1964	-3094	-1964	-2387	-1964	-1964
803	Copertura	191-118	0	3228	-7780	-2276	-3559	-2276	-2767	-2276	-2276
			30	2745	-6985	-2120	-3321	-2120	-2576	-2120	-2120
			60	2265	-6192	-1964	-3080	-1964	-2386	-1964	-1964
804	Copertura	194-119	0	2156	-6704	-2274	-3529	-2274	-2764	-2274	-2274
			30	1827	-6065	-2119	-3296	-2119	-2576	-2119	-2119
			60	1498	-5427	-1965	-3060	-1965	-2387	-1965	-1965
805	Copertura	198-120	0	1287	-5808	-2260	-3468	-2260	-2748	-2260	-2260
			30	1043	-5264	-2111	-3246	-2111	-2565	-2111	-2111
			60	801	-4723	-1961	-3021	-1961	-2382	-1961	-1961
806	Copertura	203-121	0	869	-5379	-2255	-3397	-2255	-2740	-2255	-2255
			30	612	-4818	-2103	-3179	-2103	-2555	-2103	-2103
			60	356	-4261	-1952	-2958	-1952	-2370	-1952	-1952
807	Copertura	207-122	0	-225	-4757	-2403	-3538	-2403	-2896	-2403	-2403
			30	-301	-4247	-2182	-3227	-2182	-2631	-2182	-2182
			60	-360	-3789	-1961	-2913	-1961	-2365	-1961	-1961

1.2.7 Involuppi dei diagrammi delle sollecitazioni: Taglio X-Y.

I dati seguenti riportano i valori del Taglio X-Y relativamente alle aste che definiscono la struttura ed in modo particolare:

Asta : numerazione interna dell'asta.
X : distanza dal nodo iniziale misurata lungo l'asse dell'asta.

Taglio (T_{xy}) : valore del Taglio X-Y nel punto considerato:
 Max : valore massimo (rispetto al sistema di riferimento globale) dell'involuppo.
 Min : valore minimo (rispetto al sistema di riferimento globale) dell'involuppo.
 Comb : combinazione di appartenenza del valore considerato nell'involuppo.

Tabella 32.I

				Taglio (T _{xy}) [daN]							
				SLU		SLE					
						Caratteristiche		Frequenti		Quasi Permanenti	
Asta	Imp.	Fili	X [cm]	Max	Min	Max	Min	Max	Min	Max	Min
1	Fondazio ne	1-2	0	436	-435	39	-27	8	-6	1	1
			42	267	-235	40	-22	9	-4	2	2
			83	410	-409	43	-19	10	-3	2	2
2	Fondazio ne	1-2	0	344	-363	11	-50	-3	-15	-6	-6
			42	48	-69	13	-45	-2	-14	-5	-5
			83	292	-307	13	-39	-2	-12	-5	-5
3	Fondazio ne	1-15	0	305	-257	67	-7	36	21	24	24
			40	165	-117	62	-8	35	21	24	24
			80	325	-278	56	-10	33	20	23	23
4	Fondazio ne	1-15	0	224	-273	18	-59	-19	-34	-25	-25
			40	94	-145	16	-64	-20	-36	-25	-25
			80	308	-360	13	-70	-22	-38	-26	-26
5	Fondazio ne	2-3	0	310	-230	75	-16	26	7	12	12
			35	113	-73	78	-15	26	7	12	12
			69	296	-258	81	-14	26	7	12	12
6	Fondazio ne	2-3	0	271	-296	30	-77	3	-19	-3	-3
			35	65	-172	31	-75	3	-18	-4	-4
			69	283	-342	32	-72	3	-18	-4	-4
7	Fondazio ne	3-4	0	375	-302	85	-39	20	-4	4	4
			35	205	-100	88	-38	20	-5	3	3
			69	299	-274	90	-38	21	-5	3	3
8	Fondazio ne	3-4	0	280	-299	40	-85	8	-17	0	0
			35	99	-216	41	-83	8	-17	-1	-1
			69	301	-376	41	-81	7	-17	-1	-1
9	Fondazio ne	4-5	0	386	-289	88	-45	19	-8	1	1
			35	206	-76	90	-45	19	-8	1	1
			69	305	-286	92	-44	19	-9	0	0
10	Fondazio ne	4-5	0	279	-296	44	-89	9	-17	1	1
			35	100	-223	44	-86	9	-17	0	0
			69	278	-395	45	-85	8	-17	-1	-1
11	Fondazio ne	5-6	0	380	-270	89	-47	18	-9	0	0
			35	224	-92	90	-46	18	-10	0	0
			69	297	-283	92	-46	18	-10	-1	-1
12	Fondazio ne	5-6	0	274	-287	42	-83	10	-15	1	1
			35	59	-177	42	-81	9	-15	1	1
			69	262	-361	43	-79	9	-16	0	0
13	Fondazio ne	6-7	0	414	-272	99	-49	21	-8	2	2
			35	227	-81	100	-49	21	-9	1	1
			69	313	-291	102	-49	21	-9	1	1
14	Fondazio ne	6-7	0	288	-309	48	-102	9	-21	0	0
			35	95	-241	49	-100	9	-21	-1	-1
			69	271	-414	49	-98	8	-21	-2	-2
15	Fondazio ne	7-8	0	365	-246	82	-43	16	-9	0	0
			35	169	-47	83	-43	16	-9	-1	-1
			69	283	-267	85	-43	16	-10	-1	-1
16	Fondazio	7-8	0	281	-302	45	-92	10	-18	1	1

	ne										
			35	64	-193	46	-90	9	-18	0	0
			69	254	-364	46	-88	9	-18	0	0
17	Fondazio ne	8-9	0	352	-249	85	-44	18	-8	1	1
			35	197	-68	87	-44	17	-9	0	0
			69	293	-276	89	-43	17	-9	0	0
18	Fondazio ne	8-9	0	265	-284	39	-81	8	-16	1	1
			35	52	-157	39	-79	8	-16	0	0
			69	248	-335	40	-77	7	-16	-1	-1
19	Fondazio ne	9-10	0	360	-247	89	-44	19	-7	2	2
			35	164	-43	91	-44	19	-8	1	1
			69	313	-288	93	-43	19	-8	1	1
20	Fondazio ne	9-10	0	297	-320	45	-95	9	-19	0	0
			35	75	-191	46	-93	9	-19	-1	-1
			69	246	-369	46	-91	8	-19	-1	-1
21	Fondazio ne	10-1 1	0	328	-233	72	-41	13	-9	-1	-1
			35	141	-47	74	-40	13	-10	-2	-2
			69	296	-281	77	-40	13	-10	-2	-2
22	Fondazio ne	10-1 1	0	261	-282	43	-89	9	-17	0	0
			35	44	-151	44	-87	9	-17	0	0
			69	244	-372	44	-85	9	-17	0	0
23	Fondazio ne	11-1 2	0	363	-244	79	-40	17	-7	2	2
			35	152	-45	82	-39	17	-7	1	1
			69	299	-281	84	-39	17	-7	1	1
24	Fondazio ne	11-1 2	0	278	-307	36	-90	4	-21	-4	-4
			35	52	-164	36	-87	4	-21	-4	-4
			69	245	-373	37	-85	4	-21	-4	-4
25	Fondazio ne	12-1 3	0	348	-238	72	-30	18	-2	4	4
			35	131	-30	75	-30	19	-2	4	4
			69	299	-272	78	-29	19	-2	4	4
26	Fondazio ne	12-1 3	0	247	-304	15	-82	-7	-27	-12	-12
			35	25	-134	16	-79	-7	-26	-12	-12
			69	235	-314	18	-76	-7	-26	-12	-12
27	Fondazio ne	13-1 4	0	293	-276	39	-16	11	0	4	4
			42	83	-70	45	-16	13	1	4	4
			83	339	-310	50	-14	14	1	5	5
28	Fondazio ne	13-1 4	0	329	-328	20	-42	4	-9	-1	-1
			42	71	-130	23	-38	5	-7	-1	-1
			83	269	-324	28	-36	7	-6	1	1
29	Fondazio ne	14-1 6	0	252	-297	7	-66	-20	-35	-23	-23
			40	122	-168	8	-60	-20	-34	-23	-23
			80	296	-341	9	-55	-19	-32	-23	-23
30	Fondazio ne	14-1 6	0	292	-247	55	-19	32	17	23	23
			40	155	-109	61	-17	34	18	23	23
			80	351	-302	67	-14	36	20	24	24
31	Fondazio ne	15-1 7	0	434	-286	146	25	96	72	74	74
			33	246	-100	140	24	94	71	73	73
			66	298	-154	133	23	92	69	72	72
32	Fondazio ne	15-1 7	0	157	-341	-48	-159	-92	-114	-92	-92
			33	76	-262	-49	-166	-93	-117	-93	-93
			66	245	-434	-51	-173	-95	-120	-95	-95
33	Fondazio ne	16-1 8	0	306	-449	-24	-141	-69	-93	-72	-72
			33	152	-293	-23	-135	-68	-91	-71	-71
			66	178	-317	-22	-129	-67	-88	-69	-69
34	Fondazio ne	16-1 8	0	348	-174	152	45	109	87	87	87

			33	322	-145	159	46	111	89	89	89
			66	455	-274	166	48	114	90	90	90
35	Fondazio ne	17-1 9	0	498	-272	208	63	144	113	113	113
			33	351	-128	201	62	141	112	112	112
			66	428	-209	194	60	138	110	110	110
36	Fondazio ne	17-1 9	0	219	-424	-52	-184	-103	-130	-103	-103
			33	124	-332	-54	-191	-104	-133	-104	-104
			66	258	-470	-56	-199	-106	-136	-106	-106
37	Fondazio ne	18-2 0	0	310	-529	-61	-203	-110	-139	-110	-110
			33	198	-414	-59	-195	-108	-136	-108	-108
			66	206	-418	-58	-188	-106	-133	-106	-106
38	Fondazio ne	18-2 0	0	405	-202	183	53	128	102	102	102
			33	387	-180	190	54	132	103	103	103
			66	495	-284	197	56	135	105	105	105
39	Fondazio ne	19-2 1	0	486	-281	196	49	132	102	102	102
			33	349	-148	188	47	129	100	100	100
			66	437	-240	181	45	125	98	99	99
40	Fondazio ne	19-2 1	0	237	-430	-43	-177	-96	-122	-96	-96
			33	154	-350	-45	-184	-98	-126	-98	-98
			66	281	-481	-47	-192	-100	-129	-100	-100
41	Fondazio ne	20-2 2	0	307	-513	-51	-197	-103	-133	-103	-103
			33	178	-380	-49	-189	-101	-129	-101	-101
			66	214	-413	-47	-182	-99	-126	-99	-99
42	Fondazio ne	20-2 2	0	391	-201	176	43	121	95	95	95
			33	367	-172	183	45	125	97	97	97
			66	512	-313	191	47	128	99	99	99
43	Fondazio ne	21-2 3	0	584	-381	202	40	132	100	101	101
			33	447	-248	195	39	129	98	99	99
			66	500	-305	187	37	126	96	98	98
44	Fondazio ne	21-2 3	0	321	-521	-36	-193	-98	-129	-100	-100
			33	275	-478	-38	-200	-100	-132	-102	-102
			66	405	-613	-40	-208	-102	-135	-104	-104
45	Fondazio ne	22-2 4	0	395	-595	-41	-200	-99	-131	-100	-100
			33	247	-443	-39	-193	-97	-127	-98	-98
			66	262	-454	-37	-185	-94	-124	-96	-96
46	Fondazio ne	22-2 4	0	451	-256	188	36	126	96	98	98
			33	447	-248	196	38	129	98	100	100
			66	614	-411	204	40	133	100	102	102
47	Fondazio ne	23-2 5	0	593	-401	192	35	125	94	96	96
			33	474	-286	184	34	122	91	94	94
			66	510	-326	177	32	119	89	92	92
48	Fondazio ne	23-2 5	0	298	-411	-14	-112	-54	-74	-56	-56
			33	243	-359	-16	-119	-56	-77	-58	-58
			66	346	-466	-18	-127	-58	-80	-60	-60
49	Fondazio ne	24-2 6	0	417	-604	-37	-188	-92	-122	-94	-94
			33	250	-433	-35	-180	-90	-119	-91	-91
			66	263	-442	-33	-172	-88	-115	-90	-90
50	Fondazio ne	24-2 6	0	354	-248	106	15	70	52	53	53
			33	311	-201	113	17	73	54	55	55
			66	463	-349	120	19	76	56	57	57
51	Fondazio ne	25-2 6	0	487	-501	11	-26	-4	-11	-7	-7
			49	251	-266	1	-17	-5	-9	-6	-6
			97	467	-481	-6	-8	-6	-7	-6	-6
52	Fondazio ne	25-2 6	0	332	-327	9	-3	4	2	3	3
			49	66	-60	6	0	3	2	3	3

			97	386	-380	14	-9	5	0	3	3
53	Fondazio ne	25-2 6	0	350	-352	8	-10	1	-3	-1	-1
			49	6	-9	-1	-1	-1	-1	-1	-1
			97	342	-344	7	-10	1	-3	-1	-1
54	Fondazio ne	25-2 6	0	343	-343	9	-8	2	-2	0	0
			49	3	-3	0	0	0	0	0	0
			97	339	-340	8	-10	1	-2	0	0
55	Fondazio ne	25-2 6	0	338	-337	9	-8	2	-2	0	0
			49	3	-3	0	0	0	0	0	0
			97	333	-334	8	-10	1	-2	0	0
56	Fondazio ne	25-2 6	0	341	-332	9	-8	2	-1	0	0
			49	3	-3	0	0	0	0	0	0
			97	328	-337	8	-10	1	-2	0	0
57	Fondazio ne	25-2 6	0	337	-327	10	-8	2	-1	0	0
			49	3	-3	0	0	0	0	0	0
			97	323	-324	8	-10	1	-2	0	0
58	Fondazio ne	25-2 6	0	324	-322	10	-8	2	-1	0	0
			49	3	-3	0	0	0	0	0	0
			97	320	-320	8	-10	1	-2	0	0
59	Fondazio ne	25-2 6	0	320	-319	10	-8	2	-1	0	0
			49	4	-5	0	0	0	0	0	0
			97	317	-318	7	-10	1	-2	-1	-1
60	Fondazio ne	25-2 6	0	318	-317	10	-7	3	-1	1	1
			49	5	-4	0	0	0	0	0	0
			97	316	-317	8	-10	1	-2	0	0
61	Fondazio ne	25-2 6	0	316	-316	10	-8	2	-1	0	0
			49	3	-3	0	0	0	0	0	0
			97	317	-319	8	-10	1	-2	0	0
62	Fondazio ne	25-2 6	0	318	-317	10	-8	2	-1	0	0
			49	3	-3	0	0	0	0	0	0
			97	319	-320	8	-10	1	-2	0	0
63	Fondazio ne	25-2 6	0	320	-319	10	-8	2	-1	0	0
			49	3	-3	0	0	0	0	0	0
			97	321	-322	8	-10	1	-2	0	0
64	Fondazio ne	25-2 6	0	322	-321	10	-8	2	-1	0	0
			49	3	-3	0	0	0	0	0	0
			97	323	-337	8	-9	1	-2	0	0
65	Fondazio ne	25-2 6	0	338	-323	10	-8	2	-1	0	0
			49	3	-3	0	0	0	0	0	0
			97	325	-339	8	-9	2	-2	0	0
66	Fondazio ne	25-2 6	0	340	-326	10	-8	2	-2	0	0
			49	3	-3	0	0	0	0	0	0
			97	327	-341	9	-9	2	-2	0	0
67	Fondazio ne	25-2 6	0	343	-327	10	-7	3	-1	1	1
			49	5	-3	1	1	1	1	1	1
			97	330	-342	10	-8	3	-1	1	1
68	Fondazio ne	25-2 6	0	341	-331	8	-14	-1	-5	-3	-3
			49	12	-16	-1	-5	-3	-4	-3	-3
			97	331	-348	4	-11	-2	-4	-3	-3
69	Fondazio ne	25-2 6	0	382	-369	9	5	6	5	5	5
			49	94	-71	14	0	8	5	6	6
			97	315	-327	23	-9	10	3	6	6
70	Fondazio ne	25-2 8	0	500	-385	121	20	77	56	57	57
			43	362	-254	114	14	73	53	55	55
			85	466	-360	106	8	70	50	53	53

71	Fondazio ne	25-2 8	0	365	-510	-12	-146	-68	-95	-72	-72
			43	287	-436	-17	-154	-71	-98	-75	-75
			85	434	-588	-23	-162	-75	-102	-77	-77
72	Fondazio ne	26-2 7	0	361	-489	-25	-134	-64	-86	-64	-64
			33	223	-348	-23	-127	-62	-82	-63	-63
			66	267	-389	-21	-119	-59	-79	-61	-61
73	Fondazio ne	26-2 7	0	543	-361	180	30	118	89	91	91
			33	515	-329	187	32	122	91	93	93
			66	640	-450	195	34	125	93	95	95
74	Fondazio ne	27-2 9	0	456	-654	-37	-200	-97	-129	-99	-99
			33	353	-546	-35	-192	-94	-126	-97	-97
			66	389	-578	-33	-185	-92	-122	-95	-95
75	Fondazio ne	27-2 9	0	571	-389	178	31	118	89	91	91
			33	542	-355	186	33	122	91	93	93
			66	628	-437	194	35	125	94	96	96
76	Fondazio ne	28-3 0	0	653	-469	189	26	121	88	92	92
			37	521	-342	182	23	117	85	89	89
			73	536	-362	174	20	114	83	87	87
77	Fondazio ne	28-3 0	0	376	-557	-23	-179	-86	-117	-90	-90
			37	361	-545	-26	-187	-89	-121	-92	-92
			73	496	-685	-29	-195	-91	-124	-95	-95
78	Fondazio ne	29-3 1	0	500	-697	-34	-203	-96	-130	-99	-99
			33	431	-624	-32	-195	-94	-126	-96	-96
			66	447	-635	-30	-187	-91	-123	-94	-94
79	Fondazio ne	29-3 1	0	624	-435	187	31	123	92	94	94
			33	628	-435	195	33	126	94	96	96
			66	689	-492	203	35	130	96	99	99
80	Fondazio ne	30-3 2	0	725	-527	203	31	130	95	99	99
			34	595	-402	195	29	126	93	97	97
			69	586	-397	187	26	123	91	94	94
81	Fondazio ne	30-3 2	0	378	-567	-28	-186	-91	-123	-94	-94
			34	377	-570	-30	-194	-93	-126	-97	-97
			69	511	-708	-32	-202	-96	-130	-99	-99
82	Fondazio ne	31-3 3	0	456	-648	-36	-194	-94	-126	-96	-96
			33	398	-586	-34	-186	-92	-122	-94	-94
			66	399	-582	-32	-178	-89	-118	-91	-91
83	Fondazio ne	31-3 3	0	583	-404	175	30	116	87	90	90
			33	575	-391	183	32	120	90	92	92
			66	655	-466	192	35	124	92	94	94
84	Fondazio ne	32-3 4	0	714	-516	202	34	130	96	99	99
			35	583	-390	194	31	126	94	97	97
			69	582	-392	186	29	123	91	95	95
85	Fondazio ne	32-3 4	0	403	-590	-28	-184	-90	-121	-93	-93
			35	404	-595	-31	-192	-93	-125	-96	-96
			69	511	-706	-33	-200	-95	-129	-98	-98
86	Fondazio ne	33-3 5	0	519	-713	-34	-198	-94	-127	-97	-97
			33	431	-620	-32	-190	-92	-124	-94	-94
			66	435	-619	-30	-182	-89	-120	-92	-92
87	Fondazio ne	33-3 5	0	615	-428	184	31	121	91	93	93
			33	625	-433	192	33	125	93	96	96
			66	723	-527	200	35	129	96	98	98
88	Fondazio ne	34-3 6	0	702	-509	198	33	127	94	97	97
			35	590	-401	190	31	124	92	95	95
			69	596	-411	182	28	120	89	92	92
89	Fondazio	34-3	0	418	-602	-28	-181	-89	-119	-92	-92

	ne	6									
			35	388	-576	-30	-189	-91	-123	-94	-94
			69	492	-685	-33	-197	-94	-127	-97	-97
90	Fondazio ne	35-3 7	0	487	-679	-37	-191	-94	-125	-96	-96
			33	391	-577	-35	-183	-91	-121	-93	-93
			66	391	-573	-33	-175	-89	-117	-91	-91
91	Fondazio ne	35-3 7	0	560	-379	175	32	117	88	90	90
			33	572	-386	183	34	120	91	93	93
			66	679	-489	191	36	124	93	95	95
92	Fondazio ne	36-3 8	0	679	-486	197	34	127	94	97	97
			35	583	-395	189	31	123	92	94	94
			69	619	-435	181	29	119	89	92	92
93	Fondazio ne	36-3 8	0	438	-620	-28	-179	-88	-118	-91	-91
			35	396	-583	-31	-187	-91	-122	-93	-93
			69	474	-665	-33	-195	-93	-126	-96	-96
94	Fondazio ne	37-3 9	0	526	-721	-35	-198	-95	-128	-97	-97
			33	416	-606	-33	-190	-93	-124	-95	-95
			66	391	-577	-31	-182	-90	-121	-93	-93
95	Fondazio ne	37-3 9	0	587	-398	185	32	123	92	95	95
			33	628	-434	193	34	126	95	97	97
			66	737	-539	201	36	130	97	99	99
96	Fondazio ne	38-4 0	0	645	-455	193	35	125	93	95	95
			34	578	-392	185	33	121	90	93	93
			69	608	-427	177	30	117	88	91	91
97	Fondazio ne	38-4 0	0	424	-603	-30	-174	-87	-115	-89	-89
			34	394	-577	-33	-182	-89	-119	-91	-91
			69	476	-663	-35	-190	-92	-123	-94	-94
98	Fondazio ne	39-4 1	0	495	-687	-37	-192	-95	-125	-96	-96
			33	392	-580	-35	-184	-92	-122	-94	-94
			66	362	-546	-33	-176	-90	-118	-92	-92
99	Fondazio ne	39-4 1	0	589	-396	186	34	125	94	97	97
			33	625	-428	194	36	128	96	99	99
			66	728	-527	202	38	131	99	101	101
100	Fondazio ne	40-4 2	0	668	-475	193	43	126	96	97	97
			35	576	-387	185	40	123	94	95	95
			69	596	-412	177	38	119	91	92	92
101	Fondazio ne	40-4 2	0	411	-602	-48	-178	-95	-122	-95	-95
			35	374	-569	-51	-186	-98	-126	-98	-98
			69	470	-670	-54	-194	-100	-130	-100	-100
102	Fondazio ne	41-4 4	0	475	-664	-36	-189	-92	-123	-94	-94
			33	372	-556	-34	-181	-90	-120	-92	-92
			66	360	-541	-32	-174	-88	-116	-90	-90
103	Fondazio ne	41-4 4	0	392	-285	105	16	70	52	54	54
			33	354	-243	113	18	73	54	56	56
			66	466	-351	120	20	77	57	58	58
104	Fondazio ne	42-4 3	0	570	-385	176	47	118	92	92	92
			23	505	-324	168	51	115	91	91	91
			46	516	-337	160	54	112	89	89	89
105	Fondazio ne	43-4 4	0	451	-497	-11	-43	-20	-27	-20	-20
			49	205	-247	-14	-35	-21	-25	-21	-21
			97	423	-473	-15	-36	-21	-26	-21	-21
106	Fondazio ne	43-4 4	0	340	-327	13	0	7	4	5	5
			49	61	-49	9	4	6	5	5	5
			97	384	-373	18	-5	8	3	5	5
107	Fondazio ne	43-4 4	0	351	-352	9	-10	1	-2	0	0

			49	10	-11	0	-1	0	-1	0	0
			97	342	-343	8	-9	1	-2	0	0
108	Fondazio ne	43-4 4	0	344	-344	9	-8	2	-1	0	0
			49	4	-3	1	0	0	0	0	0
			97	339	-338	10	-8	2	-1	0	0
109	Fondazio ne	43-4 4	0	338	-338	8	-9	2	-2	0	0
			49	4	-3	0	0	0	0	0	0
			97	334	-340	9	-8	2	-1	0	0
110	Fondazio ne	43-4 4	0	340	-333	8	-9	2	-2	0	0
			49	3	-3	0	0	0	0	0	0
			97	328	-335	9	-8	2	-1	0	0
111	Fondazio ne	43-4 4	0	335	-328	8	-9	1	-2	0	0
			49	3	-3	0	0	0	0	0	0
			97	324	-323	9	-8	2	-1	0	0
112	Fondazio ne	43-4 4	0	323	-324	8	-9	1	-2	0	0
			49	3	-3	0	0	0	0	0	0
			97	320	-320	9	-8	2	-1	0	0
113	Fondazio ne	43-4 4	0	319	-320	8	-9	1	-2	0	0
			49	3	-3	0	0	0	0	0	0
			97	318	-317	9	-8	2	-1	0	0
114	Fondazio ne	43-4 4	0	317	-317	8	-9	1	-2	0	0
			49	4	-3	0	0	0	0	0	0
			97	317	-316	9	-8	2	-1	0	0
115	Fondazio ne	43-4 4	0	316	-317	8	-9	1	-2	0	0
			49	3	-3	0	0	0	0	0	0
			97	318	-317	9	-8	2	-1	0	0
116	Fondazio ne	43-4 4	0	317	-318	8	-9	1	-2	0	0
			49	3	-3	0	0	0	0	0	0
			97	320	-319	9	-8	2	-1	0	0
117	Fondazio ne	43-4 4	0	319	-320	8	-9	1	-2	0	0
			49	3	-3	0	0	0	0	0	0
			97	322	-321	9	-8	2	-1	0	0
118	Fondazio ne	43-4 4	0	321	-322	8	-9	1	-2	0	0
			49	3	-3	0	0	0	0	0	0
			97	323	-323	9	-8	2	-1	0	0
119	Fondazio ne	43-4 4	0	323	-324	8	-9	1	-2	0	0
			49	3	-3	0	0	0	0	0	0
			97	325	-338	9	-8	2	-2	0	0
120	Fondazio ne	43-4 4	0	338	-326	8	-10	1	-2	0	0
			49	3	-4	0	-1	0	0	0	0
			97	327	-340	9	-9	2	-2	0	0
121	Fondazio ne	43-4 4	0	341	-327	9	-8	2	-1	1	1
			49	5	-4	1	0	1	1	1	1
			97	330	-342	10	-8	3	-1	1	1
122	Fondazio ne	43-4 4	0	338	-331	6	-16	-2	-7	-4	-4
			49	12	-21	-3	-7	-4	-5	-4	-4
			97	330	-349	2	-12	-3	-6	-4	-4
123	Fondazio ne	43-4 4	0	377	-363	8	3	6	5	5	5
			49	87	-66	12	-1	7	4	5	5
			97	313	-325	22	-10	9	2	5	5
124	Fondazio ne	43-4 5	0	506	-384	121	34	80	61	61	61
			33	390	-272	113	32	76	59	59	59
			66	428	-315	106	30	73	57	57	57
125	Fondazio ne	43-4 5	0	397	-584	-39	-179	-92	-120	-93	-93
			33	382	-573	-41	-187	-95	-124	-96	-96

			66	485	-681	-44	-195	-97	-128	-98	-98
126	Fondazio ne	44-4 6	0	355	-480	-24	-129	-62	-83	-63	-63
			33	252	-373	-22	-121	-60	-80	-61	-61
			66	299	-417	-21	-114	-58	-76	-59	-59
127	Fondazio ne	44-4 6	0	549	-367	176	32	118	89	91	91
			33	562	-376	183	34	121	91	93	93
			66	647	-457	191	36	124	93	95	95
128	Fondazio ne	45-4 7	0	631	-434	195	42	128	98	99	99
			33	514	-320	187	40	125	95	97	97
			66	517	-328	179	38	121	93	94	94
129	Fondazio ne	45-4 7	0	313	-500	-37	-179	-92	-121	-94	-94
			33	315	-507	-40	-186	-95	-124	-96	-96
			66	443	-640	-42	-194	-97	-128	-98	-98
130	Fondazio ne	46-4 8	0	417	-610	-39	-191	-95	-125	-96	-96
			33	328	-517	-37	-183	-93	-122	-94	-94
			66	334	-519	-35	-175	-91	-119	-92	-92
131	Fondazio ne	46-4 8	0	504	-329	166	32	112	85	87	87
			33	499	-321	174	34	116	88	89	89
			66	612	-429	182	36	119	90	91	91
132	Fondazio ne	47-4 9	0	620	-421	197	41	129	98	99	99
			33	477	-283	189	39	126	96	97	97
			66	475	-285	182	37	122	93	95	95
133	Fondazio ne	47-4 9	0	289	-482	-39	-184	-95	-124	-96	-96
			33	276	-473	-41	-192	-98	-128	-99	-99
			66	406	-607	-43	-200	-100	-131	-101	-101
134	Fondazio ne	48-5 0	0	415	-605	-38	-190	-94	-124	-95	-95
			33	296	-482	-36	-182	-92	-121	-93	-93
			66	312	-494	-34	-175	-89	-118	-91	-91
135	Fondazio ne	48-5 0	0	492	-299	184	38	124	95	97	97
			33	470	-272	191	40	128	97	99	99
			66	605	-404	199	42	131	100	101	101
136	Fondazio ne	49-5 1	0	505	-305	191	48	128	100	100	100
			33	387	-191	183	46	125	98	98	98
			66	420	-229	175	44	122	95	96	96
137	Fondazio ne	49-5 1	0	236	-436	-48	-182	-100	-127	-100	-100
			33	194	-398	-50	-189	-102	-130	-102	-102
			66	304	-511	-52	-197	-104	-133	-104	-104
138	Fondazio ne	50-5 2	0	310	-512	-49	-193	-101	-130	-101	-101
			33	170	-368	-47	-185	-99	-127	-99	-99
			66	227	-421	-45	-178	-97	-123	-97	-97
139	Fondazio ne	50-5 2	0	462	-256	188	50	131	103	103	103
			33	395	-184	195	52	134	105	105	105
			66	511	-297	203	53	137	107	107	107
140	Fondazio ne	51-5 3	0	483	-271	198	57	135	106	106	106
			33	406	-198	190	55	132	104	104	104
			66	421	-217	183	53	129	102	102	102
141	Fondazio ne	51-5 3	0	225	-441	-60	-190	-108	-135	-108	-108
			33	222	-441	-61	-198	-110	-138	-110	-110
			66	293	-516	-63	-205	-111	-141	-111	-111
142	Fondazio ne	52-5 4	0	236	-447	-57	-195	-105	-134	-105	-105
			33	155	-362	-55	-188	-104	-131	-104	-104
			66	246	-450	-53	-181	-102	-128	-102	-102
143	Fondazio ne	52-5 4	0	464	-249	188	59	134	107	107	107
			33	372	-153	196	61	137	109	109	109
			66	476	-255	203	63	140	111	111	111

144	Fondazio ne	53-5 5	0	453	-268	169	50	117	92	92	92
			33	356	-175	162	48	114	91	91	91
			66	371	-192	155	47	111	89	89	89
145	Fondazio ne	53-5 5	0	194	-335	-23	-130	-68	-89	-70	-70
			33	185	-327	-24	-136	-69	-92	-71	-71
			66	306	-451	-25	-142	-70	-94	-72	-72
146	Fondazio ne	54-5 6	0	231	-421	-51	-174	-95	-120	-95	-95
			33	116	-303	-49	-167	-93	-117	-93	-93
			66	217	-401	-48	-160	-92	-115	-92	-92
147	Fondazio ne	54-5 6	0	337	-197	130	21	89	67	70	70
			33	271	-122	136	23	92	69	71	71
			66	415	-271	143	23	94	70	72	72
148	Fondazio ne	55-5 7	0	365	-317	67	-14	36	19	24	24
			40	191	-179	61	-17	33	18	23	23
			80	288	-243	55	-20	32	17	22	22
149	Fondazio ne	55-5 7	0	309	-354	10	-55	-19	-32	-23	-23
			40	138	-184	8	-60	-20	-34	-23	-23
			80	269	-315	7	-66	-20	-35	-23	-23
150	Fondazio ne	56-7 0	0	278	-326	15	-68	-20	-36	-24	-24
			40	101	-160	18	-62	-18	-34	-23	-23
			80	250	-295	20	-56	-17	-32	-23	-23
151	Fondazio ne	56-7 0	0	368	-323	55	-10	32	19	22	22
			40	186	-140	61	-8	34	20	23	23
			80	296	-250	66	-7	35	20	23	23
152	Fondazio ne	57-5 8	0	457	-451	30	-37	8	-5	2	2
			42	249	-241	25	-39	6	-7	0	0
			83	406	-412	22	-42	5	-8	-1	-1
153	Fondazio ne	57-5 8	0	324	-304	49	-13	14	1	5	5
			42	108	-58	44	-15	12	1	4	4
			83	316	-306	38	-16	11	0	4	4
154	Fondazio ne	58-5 9	0	239	-261	17	-75	-7	-25	-11	-11
			35	63	-164	16	-78	-7	-26	-11	-11
			69	267	-377	15	-81	-7	-26	-11	-11
155	Fondazio ne	58-5 9	0	314	-227	78	-29	19	-2	4	4
			35	69	-94	75	-30	19	-3	4	4
			69	291	-318	72	-31	18	-3	4	4
156	Fondazio ne	59-6 0	0	343	-304	38	-86	4	-21	-4	-4
			35	126	-98	37	-89	4	-21	-4	-4
			69	275	-376	36	-91	4	-21	-4	-4
157	Fondazio ne	59-6 0	0	376	-286	86	-40	18	-7	1	1
			35	94	-132	84	-41	18	-7	1	1
			69	298	-343	82	-41	18	-7	2	2
158	Fondazio ne	60-6 1	0	343	-288	45	-88	8	-18	-1	-1
			35	131	-79	44	-90	8	-18	-1	-1
			69	285	-382	44	-92	9	-18	0	0
159	Fondazio ne	60-6 1	0	356	-272	80	-40	15	-9	-1	-1
			35	78	-120	78	-40	15	-9	-1	-1
			69	274	-327	76	-41	15	-8	0	0
160	Fondazio ne	61-6 2	0	350	-291	48	-96	8	-21	-2	-2
			35	161	-99	48	-98	8	-21	-1	-1
			69	286	-389	47	-100	9	-21	-1	-1
161	Fondazio ne	61-6 2	0	384	-281	99	-48	20	-9	0	0
			35	82	-139	97	-48	20	-9	1	1
			69	283	-332	95	-48	20	-9	1	1
162	Fondazio	62-6	0	296	-258	44	-82	9	-16	0	0

	ne	3									
			35	112	-75	43	-84	9	-16	1	1
			69	250	-339	43	-86	10	-16	1	1
163	Fondazio ne	62-6 3	0	355	-263	92	-45	17	-10	-1	-1
			35	79	-142	90	-46	18	-9	0	0
			69	263	-303	88	-46	18	-9	0	0
164	Fondazio ne	63-6 4	0	302	-252	46	-89	8	-19	-1	-1
			35	121	-82	45	-91	9	-18	0	0
			69	258	-356	45	-93	9	-18	0	0
165	Fondazio ne	63-6 4	0	352	-257	93	-45	18	-10	0	0
			35	75	-126	91	-46	18	-9	0	0
			69	256	-320	89	-46	19	-8	1	1
166	Fondazio ne	64-6 5	0	320	-252	46	-88	9	-18	0	0
			35	119	-83	46	-90	9	-18	0	0
			69	247	-344	45	-91	10	-17	1	1
167	Fondazio ne	64-6 5	0	334	-245	86	-43	16	-10	-1	-1
			35	69	-122	84	-43	16	-9	-1	-1
			69	251	-317	82	-44	16	-9	0	0
168	Fondazio ne	65-6 6	0	304	-251	48	-95	8	-20	-2	-2
			35	116	-99	48	-97	9	-20	-1	-1
			69	249	-352	47	-99	9	-20	0	0
169	Fondazio ne	65-6 6	0	385	-279	100	-47	20	-9	1	1
			35	82	-137	98	-48	21	-9	1	1
			69	251	-298	96	-48	21	-8	2	2
170	Fondazio ne	66-6 7	0	272	-233	41	-75	8	-15	0	0
			35	98	-79	40	-77	9	-15	1	1
			69	264	-345	40	-79	9	-15	1	1
171	Fondazio ne	66-6 7	0	334	-241	90	-43	18	-9	0	0
			35	102	-95	88	-44	18	-9	0	0
			69	245	-310	85	-44	18	-8	1	1
172	Fondazio ne	67-6 8	0	303	-245	39	-79	6	-17	-2	-2
			35	97	-86	39	-81	7	-17	-1	-1
			69	227	-316	38	-83	7	-17	-1	-1
173	Fondazio ne	67-6 8	0	318	-221	88	-35	21	-4	3	3
			35	84	-100	86	-36	21	-4	4	4
			69	254	-306	83	-36	20	-3	4	4
174	Fondazio ne	68-6 9	0	290	-247	30	-70	2	-18	-4	-4
			35	75	-83	29	-73	2	-18	-4	-4
			69	222	-295	28	-75	2	-18	-4	-4
175	Fondazio ne	68-6 9	0	330	-235	79	-16	25	6	11	11
			35	69	-69	76	-17	25	6	11	11
			69	263	-239	73	-17	24	6	11	11
176	Fondazio ne	69-7 0	0	273	-281	17	-38	0	-11	-4	-4
			42	48	-103	16	-44	0	-12	-4	-4
			83	307	-363	15	-49	0	-13	-4	-4
177	Fondazio ne	69-7 0	0	393	-351	43	-20	9	-3	2	2
			42	79	-94	39	-23	8	-4	1	1
			83	263	-264	38	-27	7	-6	0	0
178	Primo Impalcat o	1-2	0	1655	-1493	309	-46	186	115	140	140
			83	1655	-1428	288	-3	181	123	140	140
			166	1655	-1344	259	53	176	134	140	140
179	Primo Impalcat o	1-15	0	525	-1286	-286	-522	-333	-398	-333	-333
			80	451	-1286	-286	-522	-333	-398	-333	-333
			159	451	-1286	-286	-522	-333	-398	-333	-333

180	Primo Impalcato	2-3	0	1266	-1189	54	-12	34	21	26	26
			69	1234	-1175	43	24	32	26	26	26
			138	1268	-1175	74	11	38	26	26	26
181	Primo Impalcato	3-4	0	391	-397	6	-31	-2	-9	-3	-3
			69	391	-397	12	-16	-1	-6	-3	-3
			138	391	-397	55	-37	8	-10	-3	-3
182	Primo Impalcato	4-5	0	949	-1019	11	-45	-3	-14	-6	-6
			69	950	-963	-3	-11	-6	-7	-6	-6
			138	988	-994	40	-32	3	-11	-6	-6
183	Primo Impalcato	5-6	0	880	-895	18	-46	2	-11	-2	-2
			69	850	-856	-2	-4	-2	-3	-2	-2
			138	913	-855	39	-24	6	-7	-2	-2
184	Primo Impalcato	6-7	0	365	-366	23	-47	4	-10	-1	-1
			69	365	-366	1	-4	0	-1	-1	-1
			138	365	-366	38	-20	7	-4	-1	-1
185	Primo Impalcato	7-8	0	1080	-1147	23	-45	4	-9	0	0
			69	1080	-1083	1	-3	0	-1	0	0
			138	1116	-1109	40	-20	8	-4	0	0
186	Primo Impalcato	8-9	0	418	-421	20	-38	5	-7	1	1
			69	394	-387	5	-1	2	0	1	1
			138	458	-387	48	-23	10	-4	1	1
187	Primo Impalcato	9-10	0	855	-853	23	-35	7	-5	3	3
			69	831	-820	7	1	4	3	3	3
			138	895	-820	50	-20	12	-2	3	3
188	Primo Impalcato	10-11	0	928	-988	32	-41	11	-3	6	6
			69	928	-924	11	1	7	5	6	6
			138	964	-939	44	-11	14	3	6	6
189	Primo Impalcato	11-12	0	238	-240	33	-51	9	-7	3	3
			69	238	-233	12	-9	5	1	3	3
			138	238	-233	34	-10	10	1	3	3
190	Primo Impalcato	12-13	0	1062	-1126	-17	-70	-27	-38	-27	-27
			69	1042	-1102	-25	-44	-27	-33	-27	-27
			138	1092	-1102	15	-59	-21	-36	-27	-27
191	Primo Impalcato	13-14	0	569	-954	-74	-245	-141	-175	-143	-143
			83	617	-996	-17	-273	-130	-181	-143	-143
			166	656	-1028	26	-294	-121	-185	-143	-143
192	Primo Impalcato	14-16	0	836	-215	483	273	371	311	311	311
			80	836	-215	483	273	371	311	311	311
			159	836	-215	483	273	371	311	311	311
193	Primo Impalcato	15-17	0	722	-459	156	100	117	100	100	100
			66	722	-459	156	100	117	100	100	100
			132	722	-459	156	74	117	100	100	100
194	Primo Impalcato	16-18	0	415	-671	-93	-146	-93	-110	-93	-93
			66	415	-671	-93	-146	-93	-110	-93	-93

			132	415	-671	-65	-147	-93	-110	-93	-93
195	Primo Impalcato	17-19	0	287	-175	105	56	71	56	56	56
			66	287	-175	84	56	68	56	56	56
			132	287	-175	93	30	69	56	56	56
196	Primo Impalcato	18-20	0	185	-305	-60	-109	-60	-76	-60	-60
			66	185	-305	-60	-88	-60	-73	-60	-60
			132	185	-305	-34	-99	-60	-74	-60	-60
197	Primo Impalcato	19-21	0	547	-541	44	-10	14	4	6	6
			66	550	-541	11	3	8	6	6	6
			132	578	-541	27	-31	11	0	6	6
198	Primo Impalcato	20-22	0	482	-497	10	-45	-4	-15	-6	-6
			66	482	-497	-4	-11	-6	-8	-6	-6
			132	534	-497	29	-27	0	-11	-6	-6
199	Primo Impalcato	21-23	0	240	-247	29	-21	3	-7	-3	-3
			66	240	-247	-2	-8	-3	-4	-3	-3
			132	240	-247	17	-45	0	-12	-3	-3
200	Primo Impalcato	22-24	0	219	-212	22	-32	7	-3	3	3
			66	219	-212	6	3	4	3	3	3
			132	219	-212	43	-15	12	0	3	3
201	Primo Impalcato	23-25	0	500	-526	41	-18	9	-3	0	0
			66	500	-499	3	0	1	0	0	0
			132	500	-499	19	-34	4	-6	0	0
202	Primo Impalcato	24-26	0	467	-517	16	-34	3	-7	0	0
			66	467	-467	3	-3	1	0	0	0
			132	467	-467	40	-21	8	-4	0	0
203	Primo Impalcato	25-28	0	316	-339	61	-31	12	-7	-1	-1
			85	316	-318	0	-1	-1	-1	-1	-1
			170	316	-403	30	-62	5	-13	-1	-1
204	Primo Impalcato	26-27	0	347	-373	21	-35	5	-6	2	2
			66	347	-344	3	1	2	2	2	2
			132	347	-369	39	-17	9	-2	2	2
205	Primo Impalcato	27-29	0	341	-373	18	-36	3	-7	0	0
			66	341	-342	1	-1	0	0	0	0
			132	341	-370	38	-20	8	-4	0	0
206	Primo Impalcato	28-30	0	325	-332	40	-20	8	-4	0	0
			73	325	-325	3	-6	1	-1	0	0
			146	325	-391	26	-52	5	-10	0	0
207	Primo Impalcato	29-31	0	411	-465	17	-36	3	-7	0	0
			66	411	-411	1	-2	0	-1	0	0
			132	411	-411	38	-20	7	-4	0	0
208	Primo Impalcato	30-32	0	424	-453	41	-20	8	-4	0	0
			69	424	-423	1	0	0	0	0	0
			137	424	-423	21	-40	4	-8	0	0
209	Primo Impalcato	31-33	0	278	-278	18	-37	3	-8	0	0

			66	278	-278	0	-1	0	0	0	0
			132	278	-278	38	-20	7	-4	0	0
210	Primo Impalcato	32-34	0	292	-292	42	-20	9	-4	0	0
			69	292	-292	1	0	0	0	0	0
			138	292	-292	20	-40	4	-8	0	0
211	Primo Impalcato	33-35	0	471	-471	18	-37	4	-7	0	0
			66	471	-471	0	-1	0	0	0	0
			132	527	-471	38	-19	7	-4	0	0
212	Primo Impalcato	34-36	0	456	-456	41	-20	8	-4	0	0
			69	456	-456	1	0	0	0	0	0
			138	486	-456	20	-41	4	-8	0	0
213	Primo Impalcato	35-37	0	255	-255	18	-37	4	-7	0	0
			66	255	-255	0	-1	0	0	0	0
			132	255	-255	38	-20	7	-4	0	0
214	Primo Impalcato	36-38	0	286	-286	43	-22	9	-4	0	0
			69	286	-286	3	-1	1	0	0	0
			138	286	-286	19	-38	4	-8	0	0
215	Primo Impalcato	37-39	0	534	-508	18	-37	4	-7	0	0
			66	508	-508	1	-1	0	0	0	0
			132	542	-508	38	-19	8	-4	0	0
216	Primo Impalcato	38-40	0	533	-468	45	-24	8	-5	-1	-1
			69	473	-468	4	-4	0	-1	-1	-1
			137	480	-468	16	-36	3	-8	-1	-1
217	Primo Impalcato	39-41	0	280	-280	20	-38	4	-7	0	0
			66	280	-280	2	-1	1	0	0	0
			132	280	-280	37	-17	8	-3	0	0
218	Primo Impalcato	40-42	0	289	-294	13	-12	0	-4	-2	-2
			69	289	-294	9	-28	0	-8	-2	-2
			138	289	-294	29	-69	4	-16	-2	-2
219	Primo Impalcato	41-44	0	291	-330	17	-40	2	-10	-2	-2
			66	291	-296	0	-5	-2	-3	-2	-2
			132	291	-321	34	-20	5	-6	-2	-2
220	Primo Impalcato	42-43	0	680	-674	7	0	4	3	3	3
			23	680	-676	7	0	4	3	3	3
			46	680	-679	7	-2	4	2	3	3
221	Primo Impalcato	43-45	0	272	-271	68	-34	14	-6	1	1
			66	272	-271	31	-15	7	-2	1	1
			132	272	-271	4	-6	1	-1	1	1
222	Primo Impalcato	44-46	0	291	-288	23	-38	6	-6	2	2
			66	291	-288	5	-1	3	1	2	2
			132	291	-288	37	-14	9	-1	2	2
223	Primo Impalcato	45-47	0	506	-450	38	-16	9	-2	2	2
			66	453	-450	3	1	2	2	2	2
			132	470	-450	21	-37	6	-6	2	2
224	Primo Impalcato	46-48	0	509	-483	19	-41	2	-10	-1	-1

	o										
			66	481	-483	0	-4	-1	-2	-1	-1
			132	511	-483	33	-18	5	-5	-1	-1
225	Primo Impalcato	47-49	0	208	-201	39	-14	11	0	3	3
			66	208	-201	5	2	4	3	3	3
			132	208	-201	23	-35	8	-4	3	3
226	Primo Impalcato	48-50	0	208	-216	16	-43	0	-12	-4	-4
			66	208	-216	-3	-6	-4	-4	-4	-4
			132	208	-216	32	-22	3	-8	-4	-4
227	Primo Impalcato	49-51	0	479	-510	29	-27	0	-11	-6	-6
			66	479	-494	-3	-12	-6	-8	-6	-6
			132	479	-549	10	-46	-4	-15	-6	-6
228	Primo Impalcato	50-52	0	487	-501	30	-30	13	1	7	7
			66	487	-471	12	5	9	7	7	7
			132	487	-492	45	-7	16	5	7	7
229	Primo Impalcato	51-53	0	181	-293	-30	-93	-56	-69	-56	-56
			66	181	-293	-56	-84	-56	-68	-56	-56
			132	181	-293	-56	-105	-56	-71	-56	-56
230	Primo Impalcato	52-54	0	232	-120	94	29	69	56	56	56
			66	232	-120	82	56	67	56	56	56
			132	232	-120	103	56	71	56	56	56
231	Primo Impalcato	53-55	0	443	-651	-75	-157	-100	-118	-100	-100
			66	397	-651	-100	-157	-100	-118	-100	-100
			132	397	-651	-100	-157	-100	-118	-100	-100
232	Primo Impalcato	54-56	0	653	-382	156	72	116	99	99	99
			66	637	-382	156	99	116	99	99	99
			132	629	-382	156	99	116	99	99	99
233	Primo Impalcato	55-57	0	1326	-518	523	287	398	333	333	333
			80	1335	-518	523	287	398	333	333	333
			159	1358	-518	523	287	398	333	333	333
234	Primo Impalcato	56-70	0	132	-749	-252	-453	-291	-348	-291	-291
			80	132	-773	-252	-453	-291	-348	-291	-291
			159	132	-796	-252	-453	-291	-348	-291	-291
235	Primo Impalcato	57-58	0	1167	-1508	46	-308	-114	-185	-140	-140
			83	1167	-1508	3	-287	-123	-181	-140	-140
			166	1167	-1508	-53	-259	-134	-175	-140	-140
236	Primo Impalcato	58-59	0	911	-973	12	-54	-21	-34	-26	-26
			69	911	-973	-24	-43	-26	-32	-26	-26
			138	911	-973	-11	-74	-26	-38	-26	-26
237	Primo Impalcato	59-60	0	348	-342	30	-6	9	2	3	3
			69	348	-342	16	-12	6	0	3	3
			138	348	-342	37	-55	10	-8	3	3
238	Primo Impalcato	60-61	0	723	-712	43	-10	13	3	6	6
			69	723	-712	12	0	7	5	6	6
			138	723	-712	33	-43	12	-4	6	6
239	Primo	61-6	0	662	-657	50	-20	12	-2	2	2

	Impalcat o	2									
			69	662	-657	7	1	4	2	2	2
			138	662	-657	23	-36	7	-5	2	2
240	Primo Impalcat o	62-6 3	0	342	-314	48	-23	10	-4	1	1
			69	316	-314	6	-2	2	0	1	1
			138	316	-314	20	-37	5	-7	1	1
241	Primo Impalcat o	63-6 4	0	842	-842	43	-22	9	-4	0	0
			69	842	-842	1	-1	0	0	0	0
			138	842	-842	21	-43	4	-9	0	0
242	Primo Impalcat o	64-6 5	0	310	-312	37	-20	7	-5	-1	-1
			69	310	-312	1	-5	0	-2	-1	-1
			138	310	-312	23	-48	4	-10	-1	-1
243	Primo Impalcat o	65-6 6	0	630	-636	36	-23	5	-7	-3	-3
			69	630	-636	-2	-7	-3	-4	-3	-3
			138	630	-636	20	-50	2	-12	-3	-3
244	Primo Impalcat o	66-6 7	0	713	-727	41	-32	3	-12	-6	-6
			69	713	-727	-2	-11	-5	-7	-6	-6
			138	713	-727	10	-44	-3	-14	-6	-6
245	Primo Impalcat o	67-6 8	0	183	-221	51	-33	7	-10	-3	-3
			69	183	-190	8	-12	-1	-5	-3	-3
			138	183	-212	9	-35	-1	-10	-3	-3
246	Primo Impalcat o	68-6 9	0	879	-807	70	17	39	28	28	28
			69	879	-807	45	25	34	28	28	28
			138	879	-807	60	-15	37	22	28	28
247	Primo Impalcat o	69-7 0	0	806	-526	249	77	179	144	146	146
			83	832	-611	277	20	185	133	146	146
			166	851	-675	299	-23	189	125	146	146
248	Primo Impalcat o	1-1	0	342	-451	-43	-101	-54	-65	-54	-54
			188	342	-451	-17	-110	-49	-67	-54	-54
			376	362	-451	22	-188	-41	-83	-54	-54
249	Primo Impalcat o	2-2	0	19	-22	2	-6	-1	-2	-2	-2
			188	19	-22	2	-6	-1	-2	-2	-2
			376	19	-22	2	-6	-1	-2	-2	-2
250	Primo Impalcat o	3-3	0	23	-23	4	-5	1	-1	0	0
			188	23	-23	4	-5	1	-1	0	0
			376	23	-23	4	-5	1	-1	0	0
251	Primo Impalcat o	4-4	0	23	-23	5	-4	1	-1	0	0
			188	23	-23	5	-4	1	-1	0	0
			376	23	-23	5	-4	1	-1	0	0
252	Primo Impalcat o	5-5	0	24	-24	5	-5	1	-1	0	0
			188	24	-24	5	-5	1	-1	0	0
			376	24	-24	5	-5	1	-1	0	0
253	Primo Impalcat o	6-6	0	21	-20	4	-4	1	-1	0	0
			188	21	-20	4	-4	1	-1	0	0
			376	21	-20	4	-4	1	-1	0	0

254	Primo Impalcato	7-7	0	21	-21	4	-4	1	-1	0	0
			188	21	-21	4	-4	1	-1	0	0
			376	21	-21	4	-4	1	-1	0	0
255	Primo Impalcato	8-8	0	25	-25	5	-5	1	-1	0	0
			188	25	-25	5	-5	1	-1	0	0
			376	25	-25	5	-5	1	-1	0	0
256	Primo Impalcato	9-9	0	21	-21	4	-4	1	-1	0	0
			188	21	-21	4	-4	1	-1	0	0
			376	21	-21	4	-4	1	-1	0	0
257	Primo Impalcato	10-10	0	21	-21	4	-4	0	-1	0	0
			188	21	-21	4	-4	0	-1	0	0
			376	21	-21	4	-4	0	-1	0	0
258	Primo Impalcato	11-11	0	24	-25	4	-5	1	-1	0	0
			188	24	-25	4	-5	1	-1	0	0
			376	24	-25	4	-5	1	-1	0	0
259	Primo Impalcato	12-12	0	24	-24	5	-5	1	-1	0	0
			188	24	-24	5	-5	1	-1	0	0
			376	24	-24	5	-5	1	-1	0	0
260	Primo Impalcato	13-13	0	22	-19	6	-2	2	1	1	1
			188	22	-19	6	-2	2	1	1	1
			376	22	-19	6	-2	2	1	1	1
261	Primo Impalcato	14-14	0	468	-349	105	51	71	60	60	60
			188	490	-349	115	25	73	55	60	60
			376	561	-349	193	-14	89	47	60	60
262	Primo Impalcato	15-15	0	1034	-482	450	266	340	276	276	276
			188	1034	-482	495	169	349	276	276	276
			376	1034	-482	568	23	364	255	276	276
263	Primo Impalcato	16-16	0	724	-1279	-268	-453	-277	-341	-277	-277
			188	724	-1279	-171	-497	-277	-351	-277	-277
			376	724	-1279	-25	-570	-257	-366	-277	-277
264	Primo Impalcato	17-17	0	1599	-514	869	527	660	542	542	542
			188	1599	-514	901	436	669	542	542	542
			376	1599	-514	969	300	682	542	542	542
265	Primo Impalcato	18-18	0	898	-1977	-524	-865	-539	-656	-539	-539
			188	898	-1977	-433	-898	-539	-665	-539	-539
			376	898	-1977	-298	-966	-539	-679	-539	-539
266	Primo Impalcato	19-19	0	1773	-679	899	501	675	547	547	547
			188	1773	-679	944	411	684	547	547	547
			376	1773	-679	1012	275	697	547	547	547
267	Primo Impalcato	20-20	0	924	-2022	-504	-903	-549	-677	-549	-549
			188	924	-2022	-414	-948	-549	-686	-549	-549
			376	924	-2022	-278	-1016	-549	-699	-549	-549
268	Primo Impalcato	21-21	0	2111	-1065	891	447	652	523	523	523
			188	2111	-1065	936	356	661	523	523	523

			376	2111	-1065	1004	220	674	517	523	523
269	Primo Impalcato	22-22	0	1120	-2167	-450	-895	-523	-653	-523	-523
			188	1120	-2167	-359	-941	-523	-662	-523	-523
			376	1120	-2167	-223	-1008	-519	-676	-523	-523
270	Primo Impalcato	23-23	0	2503	-1472	902	412	647	515	515	515
			188	2503	-1472	947	322	656	515	515	515
			376	2503	-1472	1015	186	669	504	515	515
271	Primo Impalcato	24-24	0	1330	-2361	-422	-903	-515	-647	-515	-515
			188	1330	-2361	-331	-948	-515	-656	-515	-515
			376	1330	-2361	-195	-1016	-506	-670	-515	-515
272	Primo Impalcato	25-25	0	2915	-1873	929	394	657	521	521	521
			188	2915	-1873	979	293	667	521	521	521
			376	2915	-1873	1055	142	682	500	521	521
273	Primo Impalcato	26-26	0	1651	-2690	-413	-923	-520	-655	-520	-520
			188	1651	-2690	-322	-968	-520	-664	-520	-520
			376	1651	-2690	-187	-1036	-507	-677	-520	-520
274	Primo Impalcato	27-27	0	1831	-2864	-407	-921	-516	-651	-516	-516
			188	1831	-2864	-316	-966	-516	-660	-516	-516
			376	1831	-2864	-180	-1034	-503	-674	-516	-516
275	Primo Impalcato	28-28	0	2983	-1946	932	382	656	519	519	519
			188	2983	-1946	985	278	666	519	519	519
			376	2983	-1946	1063	121	682	494	519	519
276	Primo Impalcato	29-29	0	2128	-3161	-405	-923	-516	-652	-516	-516
			188	2128	-3161	-314	-968	-516	-661	-516	-516
			376	2128	-3161	-179	-1036	-503	-675	-516	-516
277	Primo Impalcato	30-30	0	3178	-2136	934	391	658	521	521	521
			188	3178	-2136	982	295	668	521	521	521
			376	3178	-2136	1053	151	682	502	521	521
278	Primo Impalcato	31-31	0	2273	-3306	-405	-922	-516	-652	-516	-516
			188	2273	-3306	-315	-968	-516	-661	-516	-516
			376	2273	-3306	-179	-1036	-503	-675	-516	-516
279	Primo Impalcato	32-32	0	3091	-2049	929	399	657	521	521	521
			188	3091	-2049	976	305	667	521	521	521
			376	3091	-2049	1046	165	681	504	521	521
280	Primo Impalcato	33-33	0	2234	-3266	-407	-919	-516	-651	-516	-516
			188	2234	-3266	-316	-964	-516	-660	-516	-516
			376	2234	-3266	-180	-1032	-503	-674	-516	-516
281	Primo Impalcato	34-34	0	3274	-2232	928	403	657	521	521	521
			188	3274	-2232	975	309	667	521	521	521
			376	3274	-2232	1045	168	681	505	521	521
282	Primo Impalcato	35-35	0	2263	-3295	-409	-914	-516	-650	-516	-516
			188	2263	-3295	-318	-959	-516	-659	-516	-516
			376	2263	-3295	-182	-1027	-504	-673	-516	-516
283	Primo Impalcato	36-36	0	3198	-2155	927	405	657	521	521	521

			188	3198	-2155	974	311	667	521	521	521
			376	3198	-2155	1044	170	681	506	521	521
284	Primo Impalcato	37-37	0	2168	-3201	-411	-910	-516	-649	-516	-516
			188	2168	-3201	-320	-955	-516	-658	-516	-516
			376	2168	-3201	-184	-1023	-504	-672	-516	-516
285	Primo Impalcato	38-38	0	3262	-2220	924	411	657	521	521	521
			188	3262	-2220	971	317	666	521	521	521
			376	3262	-2220	1041	176	680	507	521	521
286	Primo Impalcato	39-39	0	2236	-3269	-412	-908	-516	-649	-516	-516
			188	2236	-3269	-322	-953	-516	-658	-516	-516
			376	2236	-3269	-186	-1021	-504	-671	-516	-516
287	Primo Impalcato	40-40	0	3254	-2212	911	434	654	521	521	521
			188	3254	-2212	958	340	663	521	521	521
			376	3254	-2212	1028	199	677	511	521	521
288	Primo Impalcato	41-41	0	2191	-3230	-415	-910	-519	-652	-519	-519
			188	2191	-3230	-325	-956	-519	-661	-519	-519
			376	2191	-3230	-189	-1024	-507	-674	-519	-519
289	Primo Impalcato	42-42	0	2887	-1857	897	434	645	515	515	515
			188	2887	-1857	928	373	651	515	515	515
			376	2887	-1857	974	281	660	515	515	515
290	Primo Impalcato	43-43	0	2888	-1856	901	434	647	516	516	516
			188	2888	-1856	931	374	653	516	516	516
			376	2888	-1856	975	284	662	516	516	516
291	Primo Impalcato	44-44	0	1918	-2958	-417	-910	-520	-652	-520	-520
			188	1918	-2958	-326	-956	-520	-661	-520	-520
			376	1918	-2958	-190	-1024	-508	-675	-520	-520
292	Primo Impalcato	45-45	0	2887	-1858	890	443	644	515	515	515
			188	2887	-1858	936	352	653	515	515	515
			376	2887	-1858	1003	216	666	509	515	515
293	Primo Impalcato	46-46	0	1926	-2953	-418	-894	-514	-644	-514	-514
			188	1926	-2953	-327	-939	-514	-653	-514	-514
			376	1926	-2953	-192	-1007	-503	-666	-514	-514
294	Primo Impalcato	47-47	0	2618	-1588	892	433	645	515	515	515
			188	2618	-1588	937	343	654	515	515	515
			376	2618	-1588	1005	207	668	508	515	515
295	Primo Impalcato	48-48	0	1699	-2727	-427	-886	-514	-642	-514	-514
			188	1699	-2727	-337	-931	-514	-652	-514	-514
			376	1699	-2727	-201	-999	-505	-665	-514	-514
296	Primo Impalcato	49-49	0	2292	-1246	887	456	651	523	523	523
			188	2292	-1246	932	365	660	523	523	523
			376	2292	-1246	1000	229	673	519	523	523
297	Primo Impalcato	50-50	0	1167	-2211	-453	-883	-522	-650	-522	-522
			188	1167	-2211	-363	-928	-522	-659	-522	-522
			376	1167	-2211	-227	-996	-518	-672	-522	-522
298	Primo Impalcato	51-51	0	2098	-1003	896	508	674	547	547	547

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			188	2098	-1003	941	417	683	547	547	547
			376	2098	-1003	1009	281	697	547	547	547
299	Primo Impalcato	52-52	0	902	-2002	-508	-899	-550	-677	-550	-550
			188	902	-2002	-418	-943	-550	-686	-550	-550
			376	902	-2002	-282	-1011	-550	-700	-550	-550
300	Primo Impalcato	53-53	0	2115	-1029	869	531	660	543	543	543
			188	2115	-1029	901	440	669	543	543	543
			376	2115	-1029	969	305	683	543	543	543
301	Primo Impalcato	54-54	0	710	-1799	-530	-871	-545	-662	-545	-545
			188	710	-1799	-440	-903	-545	-671	-545	-545
			376	710	-1799	-304	-971	-545	-685	-545	-545
302	Primo Impalcato	55-55	0	1486	-933	450	268	340	276	276	276
			188	1486	-933	495	171	350	276	276	276
			376	1486	-933	568	25	364	256	276	276
303	Primo Impalcato	56-56	0	595	-1146	-266	-448	-275	-338	-275	-275
			188	595	-1146	-169	-493	-275	-348	-275	-275
			376	595	-1239	-23	-566	-254	-363	-275	-275
304	Primo Impalcato	57-57	0	368	-479	-45	-103	-55	-67	-56	-56
			188	368	-479	-19	-112	-50	-69	-56	-56
			376	368	-479	20	-190	-42	-84	-56	-56
305	Primo Impalcato	58-58	0	21	-24	2	-6	-1	-2	-2	-2
			188	21	-24	2	-6	-1	-2	-2	-2
			376	21	-24	2	-6	-1	-2	-2	-2
306	Primo Impalcato	59-59	0	25	-26	4	-5	1	-1	0	0
			188	25	-26	4	-5	1	-1	0	0
			376	25	-26	4	-5	1	-1	0	0
307	Primo Impalcato	60-60	0	27	-26	5	-5	1	-1	0	0
			188	27	-26	5	-5	1	-1	0	0
			376	27	-26	5	-5	1	-1	0	0
308	Primo Impalcato	61-61	0	23	-23	4	-4	1	-1	0	0
			188	23	-23	4	-4	1	-1	0	0
			376	23	-23	4	-4	1	-1	0	0
309	Primo Impalcato	62-62	0	23	-23	4	-4	1	-1	0	0
			188	23	-23	4	-4	1	-1	0	0
			376	23	-23	4	-4	1	-1	0	0
310	Primo Impalcato	63-63	0	27	-27	5	-5	1	-1	0	0
			188	27	-27	5	-5	1	-1	0	0
			376	27	-27	5	-5	1	-1	0	0
311	Primo Impalcato	64-64	0	27	-27	5	-5	1	-1	0	0
			188	27	-27	5	-5	1	-1	0	0
			376	27	-27	5	-5	1	-1	0	0
312	Primo Impalcato	65-65	0	23	-23	4	-4	1	-1	0	0
			188	23	-23	4	-4	1	-1	0	0
			376	23	-23	4	-4	1	-1	0	0
313	Primo	66-66	0	22	-23	4	-4	0	-1	0	0

	Impalcat o	6									
			188	22	-23	4	-4	0	-1	0	0
			376	22	-23	4	-4	0	-1	0	0
314	Primo Impalcat o	67-6 7	0	26	-27	4	-5	1	-1	0	0
			188	26	-27	4	-5	1	-1	0	0
			376	26	-27	4	-5	1	-1	0	0
315	Primo Impalcat o	68-6 8	0	26	-26	5	-5	1	-1	0	0
			188	26	-26	5	-5	1	-1	0	0
			376	26	-26	5	-5	1	-1	0	0
316	Primo Impalcat o	69-6 9	0	24	-21	6	-2	2	1	1	1
			188	24	-21	6	-2	2	1	1	1
			376	24	-21	6	-2	2	1	1	1
317	Primo Impalcat o	70-7 0	0	473	-355	103	49	70	59	59	59
			188	480	-355	114	23	72	54	59	59
			376	571	-355	192	-16	87	46	59	59
318	Primo Impalcat o	1-71	0	19	-7	8	5	6	5	5	5
			102	19	-7	8	5	6	5	5	5
			204	19	-7	8	5	6	5	5	5
319	Primo Impalcat o	1-92	0	29	-27	5	-4	0	-1	-1	-1
			103	29	-27	5	-4	0	-1	-1	-1
			206	29	-27	5	-4	0	-1	-1	-1
320	Primo Impalcat o	92-2	0	44	-28	11	0	5	3	3	3
			103	44	-28	11	0	5	3	3	3
			206	44	-28	11	0	5	3	3	3
321	Primo Impalcat o	6-89	0	23	-27	4	-7	1	-1	0	0
			100	23	-27	4	-7	1	-1	0	0
			200	23	-27	4	-7	1	-1	0	0
322	Primo Impalcat o	89-7	0	33	-32	9	-5	2	-1	0	0
			100	33	-32	9	-5	2	-1	0	0
			200	33	-32	9	-5	2	-1	0	0
323	Primo Impalcat o	9-90	0	12	-22	5	-10	1	-2	0	0
			100	12	-22	5	-10	1	-2	0	0
			200	12	-22	5	-10	1	-2	0	0
324	Primo Impalcat o	90-1 0	0	28	-27	6	-3	1	-1	0	0
			100	28	-27	6	-3	1	-1	0	0
			200	28	-27	6	-3	1	-1	0	0
325	Primo Impalcat o	13-9 1	0	27	-35	-1	-11	-3	-5	-3	-3
			103	27	-35	-1	-11	-3	-5	-3	-3
			206	27	-35	-1	-11	-3	-5	-3	-3
326	Primo Impalcat o	88-1 4	0	4	-16	-5	-8	-5	-6	-5	-5
			102	4	-16	-5	-8	-5	-6	-5	-5
			204	4	-16	-5	-8	-5	-6	-5	-5
327	Primo Impalcat o	91-1 4	0	13	-16	4	-4	1	0	1	1
			103	13	-16	4	-4	1	0	1	1
			206	13	-16	4	-4	1	0	1	1

328	Primo Impalcato	71-15	0	30	-14	11	5	8	6	6	6
			102	30	-14	11	5	8	6	6	6
			204	30	-14	11	5	8	6	6	6
329	Primo Impalcato	16-88	0	15	-31	-5	-11	-6	-8	-6	-6
			102	15	-31	-5	-11	-6	-8	-6	-6
			204	15	-31	-5	-11	-6	-8	-6	-6
330	Primo Impalcato	17-72	0	12	-22	-5	-8	-5	-6	-5	-5
			100	12	-22	-5	-8	-5	-6	-5	-5
			199	12	-22	-5	-8	-5	-6	-5	-5
331	Primo Impalcato	87-18	0	31	-21	8	5	6	5	5	5
			100	31	-21	8	5	6	5	5	5
			199	31	-21	8	5	6	5	5	5
332	Primo Impalcato	72-19	0	30	-20	9	3	6	5	5	5
			100	30	-20	9	3	6	5	5	5
			199	30	-20	9	3	6	5	5	5
333	Primo Impalcato	20-87	0	26	-36	-3	-9	-5	-6	-5	-5
			100	26	-36	-3	-9	-5	-6	-5	-5
			199	26	-36	-3	-9	-5	-6	-5	-5
334	Primo Impalcato	21-73	0	15	-26	-3	-8	-5	-6	-5	-5
			100	15	-26	-3	-8	-5	-6	-5	-5
			199	15	-26	-3	-8	-5	-6	-5	-5
335	Primo Impalcato	86-22	0	30	-17	8	3	6	5	5	5
			100	30	-17	8	3	6	5	5	5
			199	30	-17	8	3	6	5	5	5
336	Primo Impalcato	73-23	0	37	-28	9	2	6	4	4	4
			100	37	-28	9	2	6	4	4	4
			199	37	-28	9	2	6	4	4	4
337	Primo Impalcato	24-86	0	26	-35	-2	-9	-4	-6	-4	-4
			100	26	-35	-2	-9	-4	-6	-4	-4
			199	26	-35	-2	-9	-4	-6	-4	-4
338	Primo Impalcato	25-74	0	27	-36	-2	-8	-4	-5	-4	-4
			103	27	-36	-2	-8	-4	-5	-4	-4
			206	27	-36	-2	-8	-4	-5	-4	-4
339	Primo Impalcato	85-26	0	31	-22	9	3	6	5	5	5
			100	31	-22	9	3	6	5	5	5
			199	31	-22	9	3	6	5	5	5
340	Primo Impalcato	27-85	0	29	-38	-3	-9	-4	-6	-4	-4
			100	29	-38	-3	-9	-4	-6	-4	-4
			199	29	-38	-3	-9	-4	-6	-4	-4
341	Primo Impalcato	74-28	0	40	-32	8	2	5	4	4	4
			103	40	-32	8	2	5	4	4	4
			206	40	-32	8	2	5	4	4	4
342	Primo Impalcato	84-29	0	39	-30	9	3	6	5	5	5
			100	39	-30	9	3	6	5	5	5

			199	39	-30	9	3	6	5	5	5
343	Primo Impalcato	31-84	0	36	-45	-3	-9	-5	-6	-5	-5
			100	36	-45	-3	-9	-5	-6	-5	-5
			199	36	-45	-3	-9	-5	-6	-5	-5
344	Primo Impalcato	83-33	0	40	-31	9	3	6	5	5	5
			100	40	-31	9	3	6	5	5	5
			199	40	-31	9	3	6	5	5	5
345	Primo Impalcato	35-83	0	34	-43	-3	-8	-5	-6	-5	-5
			100	34	-43	-3	-8	-5	-6	-5	-5
			199	34	-43	-3	-8	-5	-6	-5	-5
346	Primo Impalcato	82-37	0	40	-31	8	3	6	5	5	5
			100	40	-31	8	3	6	5	5	5
			199	40	-31	8	3	6	5	5	5
347	Primo Impalcato	39-82	0	31	-40	-3	-8	-5	-6	-5	-5
			100	31	-40	-3	-8	-5	-6	-5	-5
			199	31	-40	-3	-8	-5	-6	-5	-5
348	Primo Impalcato	78-43	0	30	-39	-3	-8	-5	-6	-5	-5
			100	30	-39	-3	-8	-5	-6	-5	-5
			199	30	-39	-3	-8	-5	-6	-5	-5
349	Primo Impalcato	81-44	0	39	-30	9	3	6	5	5	5
			100	39	-30	9	3	6	5	5	5
			199	39	-30	9	3	6	5	5	5
350	Primo Impalcato	45-78	0	36	-27	8	3	6	5	5	5
			100	36	-27	8	3	6	5	5	5
			199	36	-27	8	3	6	5	5	5
351	Primo Impalcato	46-81	0	28	-37	-3	-8	-4	-6	-4	-4
			100	28	-37	-3	-8	-4	-6	-4	-4
			199	28	-37	-3	-8	-4	-6	-4	-4
352	Primo Impalcato	77-47	0	30	-39	-2	-8	-4	-6	-4	-4
			100	30	-39	-2	-8	-4	-6	-4	-4
			199	30	-39	-2	-8	-4	-6	-4	-4
353	Primo Impalcato	80-48	0	40	-31	8	2	6	4	4	4
			100	40	-31	8	2	6	4	4	4
			199	40	-31	8	2	6	4	4	4
354	Primo Impalcato	49-77	0	27	-18	8	3	6	5	5	5
			100	27	-18	8	3	6	5	5	5
			199	27	-18	8	3	6	5	5	5
355	Primo Impalcato	50-80	0	16	-27	-3	-8	-5	-6	-5	-5
			100	16	-27	-3	-8	-5	-6	-5	-5
			199	16	-27	-3	-8	-5	-6	-5	-5
356	Primo Impalcato	76-51	0	27	-37	-3	-9	-5	-6	-5	-5
			100	27	-37	-3	-9	-5	-6	-5	-5
			199	27	-37	-3	-9	-5	-6	-5	-5
357	Primo Impalcato	53-76	0	32	-22	8	5	6	5	5	5

			100	32	-22	8	5	6	5	5	5
			199	32	-22	8	5	6	5	5	5
358	Primo Impalcato	75-55	0	19	-33	-5	-11	-6	-8	-6	-6
			102	19	-33	-5	-11	-6	-8	-6	-6
			204	19	-33	-5	-11	-6	-8	-6	-6
359	Primo Impalcato	56-79	0	29	-14	11	5	8	6	6	6
			102	29	-14	11	5	8	6	6	6
			204	29	-14	11	5	8	6	6	6
360	Primo Impalcato	57-75	0	6	-18	-5	-8	-5	-6	-5	-5
			102	6	-18	-5	-8	-5	-6	-5	-5
			204	6	-18	-5	-8	-5	-6	-5	-5
361	Primo Impalcato	57-93	0	25	-24	4	-5	1	0	1	1
			103	25	-24	4	-5	1	0	1	1
			206	25	-24	4	-5	1	0	1	1
362	Primo Impalcato	93-58	0	25	-32	0	-11	-3	-5	-3	-3
			103	25	-32	0	-11	-3	-5	-3	-3
			206	25	-32	0	-11	-3	-5	-3	-3
363	Primo Impalcato	61-95	0	23	-23	6	-3	1	-1	0	0
			100	23	-23	6	-3	1	-1	0	0
			200	23	-23	6	-3	1	-1	0	0
364	Primo Impalcato	95-62	0	17	-10	5	-10	1	-2	0	0
			100	17	-10	5	-10	1	-2	0	0
			200	17	-10	5	-10	1	-2	0	0
365	Primo Impalcato	96-65	0	11	-15	10	-5	2	-1	0	0
			100	11	-15	10	-5	2	-1	0	0
			200	11	-15	10	-5	2	-1	0	0
366	Primo Impalcato	66-96	0	18	-19	3	-6	1	-1	0	0
			100	18	-19	3	-6	1	-1	0	0
			200	18	-19	3	-6	1	-1	0	0
367	Primo Impalcato	69-94	0	27	-18	11	1	5	3	3	3
			103	27	-18	11	1	5	3	3	3
			206	27	-18	11	1	5	3	3	3
368	Primo Impalcato	79-70	0	15	-5	8	5	6	5	5	5
			102	15	-5	8	5	6	5	5	5
			204	15	-5	8	5	6	5	5	5
369	Primo Impalcato	94-70	0	9	-14	4	-4	0	-1	-1	-1
			103	9	-14	4	-4	0	-1	-1	-1
			206	9	-14	4	-4	0	-1	-1	-1
370	Primo Impalcato	1-71	0	14	-20	-1	-5	-3	-3	-3	-3
			102	14	-20	-1	-5	-3	-3	-3	-3
			204	14	-20	-1	-5	-3	-3	-3	-3
371	Primo Impalcato	1-92	0	23	-18	4	1	3	2	2	2
			103	23	-18	4	1	3	2	2	2
			206	23	-18	4	1	3	2	2	2
372	Primo Impalcato	92-2	0	19	-24	-1	-5	-2	-3	-2	-2

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			103	19	-24	-1	-5	-2	-3	-2	-2
			206	19	-24	-1	-5	-2	-3	-2	-2
373	Primo Impalcato	6-89	0	27	-14	9	-4	2	-1	0	0
			100	27	-14	9	-4	2	-1	0	0
			200	27	-14	9	-4	2	-1	0	0
374	Primo Impalcato	89-7	0	10	-21	4	-8	1	-2	0	0
			100	10	-21	4	-8	1	-2	0	0
			200	10	-21	4	-8	1	-2	0	0
375	Primo Impalcato	9-90	0	18	-17	7	-3	1	-1	0	0
			100	18	-17	7	-3	1	-1	0	0
			200	18	-17	7	-3	1	-1	0	0
376	Primo Impalcato	90-10	0	12	-25	5	-9	1	-2	0	0
			100	12	-25	5	-9	1	-2	0	0
			200	12	-25	5	-9	1	-2	0	0
377	Primo Impalcato	13-91	0	12	-6	6	1	3	2	2	2
			103	12	-6	6	1	3	2	2	2
			206	12	-6	6	1	3	2	2	2
378	Primo Impalcato	88-14	0	20	-15	4	1	3	2	3	3
			102	20	-15	4	1	3	2	3	3
			204	20	-15	4	1	3	2	3	3
379	Primo Impalcato	91-14	0	17	-22	-1	-3	-2	-2	-2	-2
			103	17	-22	-1	-3	-2	-2	-2	-2
			206	17	-22	-1	-3	-2	-2	-2	-2
380	Primo Impalcato	71-15	0	2	-12	-3	-6	-4	-5	-4	-4
			102	2	-12	-3	-6	-4	-5	-4	-4
			204	2	-12	-3	-6	-4	-5	-4	-4
381	Primo Impalcato	16-88	0	11	-3	6	3	5	4	4	4
			102	11	-3	6	3	5	4	4	4
			204	11	-3	6	3	5	4	4	4
382	Primo Impalcato	17-72	0	16	-5	9	4	7	5	5	5
			100	16	-5	9	4	7	5	5	5
			199	16	-5	9	4	7	5	5	5
383	Primo Impalcato	87-18	0	7	-17	-4	-9	-5	-7	-5	-5
			100	7	-17	-4	-9	-5	-7	-5	-5
			199	7	-17	-4	-9	-5	-7	-5	-5
384	Primo Impalcato	72-19	0	6	-16	-4	-8	-5	-6	-5	-5
			100	6	-16	-4	-8	-5	-6	-5	-5
			199	6	-16	-4	-8	-5	-6	-5	-5
385	Primo Impalcato	20-87	0	19	-10	8	4	6	5	5	5
			100	19	-10	8	4	6	5	5	5
			199	19	-10	8	4	6	5	5	5
386	Primo Impalcato	21-73	0	25	-15	8	3	6	5	5	5
			100	25	-15	8	3	6	5	5	5
			199	25	-15	8	3	6	5	5	5
387	Primo	86-2	0	14	-23	-3	-9	-5	-6	-5	-5

	Impalcat o	2									
			100	14	-23	-3	-9	-5	-6	-5	-5
			199	14	-23	-3	-9	-5	-6	-5	-5
388	Primo Impalcat o	73-2 3	0	9	-18	-3	-8	-4	-6	-4	-4
			100	9	-18	-3	-8	-4	-6	-4	-4
			199	9	-18	-3	-8	-4	-6	-4	-4
389	Primo Impalcat o	24-8 6	0	19	-10	8	3	6	4	4	4
			100	19	-10	8	3	6	4	4	4
			199	19	-10	8	3	6	4	4	4
390	Primo Impalcat o	25-7 4	0	28	-20	8	2	5	4	4	4
			103	28	-20	8	2	5	4	4	4
			206	28	-20	8	2	5	4	4	4
391	Primo Impalcat o	85-2 6	0	15	-24	-3	-9	-5	-6	-5	-5
			100	15	-24	-3	-9	-5	-6	-5	-5
			199	15	-24	-3	-9	-5	-6	-5	-5
392	Primo Impalcat o	27-8 5	0	25	-15	9	3	6	5	5	5
			100	25	-15	9	3	6	5	5	5
			199	25	-15	9	3	6	5	5	5
393	Primo Impalcat o	74-2 8	0	20	-28	-2	-8	-4	-5	-4	-4
			103	20	-28	-2	-8	-4	-5	-4	-4
			206	20	-28	-2	-8	-4	-5	-4	-4
394	Primo Impalcat o	84-2 9	0	20	-29	-3	-9	-5	-6	-5	-5
			100	20	-29	-3	-9	-5	-6	-5	-5
			199	20	-29	-3	-9	-5	-6	-5	-5
395	Primo Impalcat o	31-8 4	0	27	-18	9	3	6	5	5	5
			100	27	-18	9	3	6	5	5	5
			199	27	-18	9	3	6	5	5	5
396	Primo Impalcat o	83-3 3	0	21	-30	-3	-8	-5	-6	-5	-5
			100	21	-30	-3	-8	-5	-6	-5	-5
			199	21	-30	-3	-8	-5	-6	-5	-5
397	Primo Impalcat o	35-8 3	0	29	-20	8	3	6	5	5	5
			100	29	-20	8	3	6	5	5	5
			199	29	-20	8	3	6	5	5	5
398	Primo Impalcat o	82-3 7	0	21	-30	-3	-8	-5	-6	-5	-5
			100	21	-30	-3	-8	-5	-6	-5	-5
			199	21	-30	-3	-8	-5	-6	-5	-5
399	Primo Impalcat o	39-8 2	0	28	-19	8	3	6	5	5	5
			100	28	-19	8	3	6	5	5	5
			199	28	-19	8	3	6	5	5	5
400	Primo Impalcat o	78-4 3	0	27	-18	8	4	6	5	5	5
			100	27	-18	8	4	6	5	5	5
			199	27	-18	8	4	6	5	5	5
401	Primo Impalcat o	81-4 4	0	18	-27	-3	-8	-5	-6	-5	-5
			100	18	-27	-3	-8	-5	-6	-5	-5
			199	18	-27	-3	-8	-5	-6	-5	-5

402	Primo Impalcato	45-78	0	16	-25	-3	-8	-4	-6	-4	-4
			100	16	-25	-3	-8	-4	-6	-4	-4
			199	16	-25	-3	-8	-4	-6	-4	-4
403	Primo Impalcato	46-81	0	26	-17	8	3	6	5	5	5
			100	26	-17	8	3	6	5	5	5
			199	26	-17	8	3	6	5	5	5
404	Primo Impalcato	77-47	0	20	-11	8	3	6	5	5	5
			100	20	-11	8	3	6	5	5	5
			199	20	-11	8	3	6	5	5	5
405	Primo Impalcato	80-48	0	10	-19	-3	-8	-4	-6	-4	-4
			100	10	-19	-3	-8	-4	-6	-4	-4
			199	10	-19	-3	-8	-4	-6	-4	-4
406	Primo Impalcato	49-77	0	16	-25	-3	-8	-5	-6	-5	-5
			100	16	-25	-3	-8	-5	-6	-5	-5
			199	16	-25	-3	-8	-5	-6	-5	-5
407	Primo Impalcato	50-80	0	26	-17	8	3	6	5	5	5
			100	26	-17	8	3	6	5	5	5
			199	26	-17	8	3	6	5	5	5
408	Primo Impalcato	76-51	0	21	-11	8	4	6	5	5	5
			100	21	-11	8	4	6	5	5	5
			199	21	-11	8	4	6	5	5	5
409	Primo Impalcato	53-76	0	7	-18	-4	-9	-5	-7	-5	-5
			100	7	-18	-4	-9	-5	-7	-5	-5
			199	7	-18	-4	-9	-5	-7	-5	-5
410	Primo Impalcato	75-55	0	14	-5	6	3	5	4	4	4
			102	14	-5	6	3	5	4	4	4
			204	14	-5	6	3	5	4	4	4
411	Primo Impalcato	56-79	0	2	-10	-3	-6	-4	-4	-4	-4
			102	2	-10	-3	-6	-4	-4	-4	-4
			204	2	-10	-3	-6	-4	-4	-4	-4
412	Primo Impalcato	57-75	0	23	-17	5	1	3	3	3	3
			102	23	-17	5	1	3	3	3	3
			204	23	-17	5	1	3	3	3	3
413	Primo Impalcato	57-93	0	18	-22	-1	-3	-2	-2	-2	-2
			103	18	-22	-1	-3	-2	-2	-2	-2
			206	18	-22	-1	-3	-2	-2	-2	-2
414	Primo Impalcato	93-58	0	26	-17	6	1	3	2	2	2
			103	26	-17	6	1	3	2	2	2
			206	26	-17	6	1	3	2	2	2
415	Primo Impalcato	61-95	0	21	-14	5	-9	1	-2	0	0
			100	21	-14	5	-9	1	-2	0	0
			200	21	-14	5	-9	1	-2	0	0
416	Primo Impalcato	95-62	0	17	-21	7	-4	1	-1	0	0
			100	17	-21	7	-4	1	-1	0	0

			200	17	-21	7	-4	1	-1	0	0
417	Primo Impalcato	96-65	0	17	-25	3	-7	1	-1	0	0
			100	17	-25	3	-7	1	-1	0	0
			200	17	-25	3	-7	1	-1	0	0
418	Primo Impalcato	66-96	0	11	-18	9	-5	2	-1	0	0
			100	11	-18	9	-5	2	-1	0	0
			200	11	-18	9	-5	2	-1	0	0
419	Primo Impalcato	69-94	0	7	-15	-1	-6	-2	-3	-2	-2
			103	7	-15	-1	-6	-2	-3	-2	-2
			206	7	-15	-1	-6	-2	-3	-2	-2
420	Primo Impalcato	79-70	0	12	-17	-1	-4	-2	-3	-2	-2
			102	12	-17	-1	-4	-2	-3	-2	-2
			204	12	-17	-1	-4	-2	-3	-2	-2
421	Primo Impalcato	94-70	0	19	-15	4	1	3	2	2	2
			103	19	-15	4	1	3	2	2	2
			206	19	-15	4	1	3	2	2	2
422	Copertura	1-2	0	1179	-1387	390	-951	52	-217	-27	-27
			83	1179	-1363	382	-935	50	-214	-27	-27
			166	1179	-1340	374	-919	48	-210	-27	-27
423	Copertura	15-1	0	3770	-1644	1811	-768	406	-110	45	45
			80	3770	-1644	1811	-768	406	-110	45	45
			159	3770	-1644	1811	-768	406	-110	45	45
424	Copertura	2-3	0	534	-1342	321	-670	64	-135	1	1
			69	534	-1324	315	-658	62	-132	1	1
			138	534	-1306	309	-646	61	-130	1	1
425	Copertura	3-4	0	774	-1079	251	-491	56	-92	8	8
			69	774	-1061	245	-479	55	-90	8	8
			138	774	-1043	239	-467	54	-87	8	8
426	Copertura	4-5	0	1061	-1117	175	-342	40	-64	6	6
			69	1052	-1107	169	-330	39	-61	6	6
			138	1052	-1096	163	-318	37	-59	6	6
427	Copertura	5-6	0	554	-548	111	-218	25	-41	3	3
			69	554	-548	104	-206	23	-39	3	3
			138	554	-548	98	-194	22	-36	3	3
428	Copertura	6-7	0	692	-689	56	-111	12	-21	1	1
			69	692	-689	50	-99	11	-19	1	1
			138	692	-689	44	-87	10	-16	1	1
429	Copertura	7-8	0	1160	-1159	28	-28	6	-5	0	0
			69	1160	-1159	28	-28	6	-5	0	0
			138	1160	-1159	28	-28	6	-5	0	0
430	Copertura	8-9	0	730	-732	89	-44	17	-10	-1	-1
			69	730	-732	101	-51	19	-11	-1	-1
			138	730	-732	113	-57	22	-12	-1	-1
431	Copertura	9-10	0	778	-662	196	-99	37	-22	-3	-3
			69	796	-662	208	-105	39	-23	-3	-3
			138	814	-662	220	-111	42	-24	-3	-3
432	Copertura	10-11	0	1391	-1154	321	-166	60	-38	-6	-6
			69	1409	-1154	333	-172	62	-39	-6	-6
			138	1427	-1154	345	-178	65	-40	-6	-6
433	Copertura	11-12	0	1387	-840	472	-242	88	-54	-8	-8
			69	1406	-840	484	-248	91	-56	-8	-8
			138	1424	-840	496	-254	93	-57	-8	-8

434	Copertura	12-13	0	1527	-645	654	-316	132	-62	0	0
			69	1545	-645	666	-322	134	-63	0	0
			138	1563	-645	678	-328	137	-64	0	0
435	Copertura	13-14	0	1694	-1287	944	-395	216	-51	29	29
			83	1718	-1287	960	-403	220	-53	29	29
			166	1741	-1287	975	-411	223	-55	29	29
436	Copertura	16-14	0	1719	-4150	711	-1906	46	-478	-105	-105
			80	1719	-4150	711	-1906	46	-478	-105	-105
			159	1719	-4150	711	-1906	46	-478	-105	-105
437	Copertura	15-17	0	1978	-1822	154	-201	14	-57	-19	-19
			66	1962	-1822	144	-196	12	-56	-19	-19
			132	1947	-1822	134	-190	10	-54	-19	-19
438	Copertura	16-18	0	1750	-1745	206	-147	62	-8	24	24
			66	1750	-1745	201	-137	61	-6	24	24
			132	1750	-1745	196	-126	60	-4	24	24
439	Copertura	17-19	0	2144	-1999	100	-74	27	-8	8	8
			66	2128	-1999	89	-71	25	-7	8	8
			132	2113	-1999	79	-71	23	-7	8	8
440	Copertura	18-20	0	1949	-1829	81	-89	15	-19	-2	-2
			66	1942	-1829	76	-79	14	-17	-2	-2
			132	1934	-1829	71	-68	13	-15	-2	-2
441	Copertura	19-21	0	1493	-1458	43	-26	12	-2	3	3
			66	1477	-1458	33	-21	10	-1	3	3
			132	1465	-1458	23	-16	8	0	3	3
442	Copertura	20-22	0	1173	-1192	33	-37	6	-8	0	0
			66	1173	-1192	28	-26	5	-6	0	0
			132	1173	-1192	23	-16	4	-4	0	0
443	Copertura	21-23	0	1876	-1875	18	-5	4	-1	0	0
			66	1876	-1875	7	-3	2	0	0	0
			132	1880	-1875	6	-3	2	0	0	0
444	Copertura	22-24	0	1485	-1495	12	-7	4	0	2	2
			66	1485	-1495	10	-7	3	0	2	2
			132	1485	-1495	13	-7	4	0	2	2
445	Copertura	23-25	0	1572	-1572	20	-13	4	-2	0	0
			66	1572	-1572	13	-13	3	-2	0	0
			132	1572	-1572	13	-13	3	-2	0	0
446	Copertura	24-26	0	893	-890	7	0	3	1	1	1
			66	893	-890	17	-4	5	0	1	1
			132	893	-890	28	-9	7	-1	1	1
447	Copertura	25-28	0	2292	-2292	26	-15	5	-3	0	0
			85	2292	-2292	36	-34	7	-7	0	0
			170	2292	-2292	45	-53	9	-10	0	0
448	Copertura	26-27	0	2632	-2655	18	-16	4	-3	0	0
			66	2632	-2655	16	-15	3	-3	0	0
			132	2632	-2655	16	-15	3	-3	0	0
449	Copertura	27-29	0	1048	-1053	23	-37	4	-8	-1	-1
			66	1048	-1053	33	-42	6	-9	-1	-1
			132	1060	-1053	44	-47	8	-10	-1	-1
450	Copertura	28-30	0	1412	-1412	6	-7	1	-2	0	0
			73	1416	-1412	6	-7	1	-2	0	0
			146	1422	-1412	11	-20	2	-4	0	0
451	Copertura	29-31	0	1220	-1225	8	-20	1	-4	-1	-1
			66	1226	-1225	18	-25	3	-5	-1	-1
			132	1241	-1225	29	-30	5	-6	-1	-1
452	Copertura	30-3	0	1668	-1663	6	-7	1	-2	-1	-1

	a	2									
			69	1673	-1663	12	-19	2	-4	-1	-1
			137	1678	-1663	18	-30	3	-7	-1	-1
453	Copertur a	31-3 3	0	952	-963	4	-11	0	-3	-1	-1
			66	952	-971	9	-16	1	-4	-1	-1
			132	952	-978	20	-21	3	-5	-1	-1
454	Copertur a	32-3 4	0	1414	-1414	4	-5	0	-2	-1	-1
			69	1414	-1414	9	-15	1	-4	-1	-1
			138	1414	-1414	15	-27	2	-6	-1	-1
455	Copertur a	33-3 5	0	1686	-1692	4	-7	0	-2	-1	-1
			66	1686	-1692	5	-13	0	-3	-1	-1
			132	1686	-1692	16	-18	2	-4	-1	-1
456	Copertur a	34-3 6	0	1888	-1893	4	-6	0	-2	-1	-1
			69	1888	-1893	5	-12	0	-3	-1	-1
			138	1888	-1893	11	-24	1	-5	-1	-1
457	Copertur a	35-3 7	0	1554	-1561	4	-10	0	-3	-1	-1
			66	1554	-1561	4	-15	0	-4	-1	-1
			132	1554	-1561	13	-20	1	-5	-1	-1
458	Copertur a	36-3 8	0	1716	-1719	5	-8	0	-3	-1	-1
			69	1716	-1719	5	-14	0	-4	-1	-1
			138	1716	-1719	10	-26	1	-6	-1	-1
459	Copertur a	37-3 9	0	1224	-1243	8	-19	1	-5	-1	-1
			66	1224	-1251	8	-24	1	-6	-1	-1
			132	1224	-1258	16	-29	2	-7	-1	-1
460	Copertur a	38-4 0	0	1541	-1544	4	-7	0	-2	-1	-1
			69	1544	-1544	4	-17	0	-5	-1	-1
			137	1549	-1544	8	-29	0	-7	-1	-1
461	Copertur a	39-4 1	0	2672	-2706	29	-38	6	-8	0	0
			66	2672	-2711	29	-43	6	-9	0	0
			132	2672	-2715	37	-49	7	-10	0	0
462	Copertur a	40-4 2	0	2857	-2856	8	-23	1	-6	-1	-1
			69	2854	-2856	8	-18	1	-5	-1	-1
			138	2854	-2856	8	-16	1	-4	-1	-1
463	Copertur a	41-4 4	0	3369	-3253	85	-75	18	-14	1	1
			66	3361	-3253	80	-65	17	-12	1	1
			132	3354	-3253	75	-54	16	-10	1	1
464	Copertur a	42-4 3	0	4705	-4706	78	-79	15	-16	0	0
			23	4705	-4706	78	-79	15	-16	0	0
			46	4705	-4706	78	-79	15	-16	0	0
465	Copertur a	43-4 5	0	3279	-3321	81	-48	18	-8	2	2
			66	3279	-3315	71	-43	16	-7	2	2
			132	3279	-3310	61	-38	14	-6	2	2
466	Copertur a	44-4 6	0	3198	-3197	28	-26	6	-5	1	1
			66	3198	-3197	28	-26	6	-5	1	1
			132	3198	-3197	28	-26	6	-5	1	1
467	Copertur a	45-4 7	0	1711	-1724	52	-30	12	-4	2	2
			66	1711	-1720	41	-25	10	-3	2	2
			132	1711	-1715	31	-20	8	-2	2	2
468	Copertur a	46-4 8	0	1570	-1566	43	-33	10	-5	2	2
			66	1570	-1566	38	-23	9	-3	2	2
			132	1570	-1566	33	-13	8	-1	2	2
469	Copertur a	47-4 9	0	1919	-1917	28	-12	8	0	2	2
			66	1919	-1912	18	-7	6	1	2	2
			132	1919	-1908	9	-5	4	1	2	2
470	Copertur a	48-5 0	0	1610	-1608	25	-21	6	-3	1	1

			66	1610	-1608	20	-11	5	-1	1	1
			132	1610	-1608	15	-8	4	-1	1	1
471	Copertura	49-51	0	1651	-1648	13	-9	1	-3	-1	-1
			66	1651	-1648	19	-20	3	-5	-1	-1
			132	1651	-1648	24	-30	4	-7	-1	-1
472	Copertura	50-52	0	1327	-1333	16	-9	5	0	2	2
			66	1327	-1337	22	-14	6	-1	2	2
			132	1327	-1342	32	-19	8	-2	2	2
473	Copertura	51-53	0	2073	-1986	74	-75	9	-21	-7	-7
			66	2073	-1986	74	-85	9	-23	-7	-7
			132	2073	-1986	75	-95	9	-25	-7	-7
474	Copertura	52-54	0	1845	-1936	72	-66	18	-10	4	4
			66	1845	-1943	82	-71	20	-11	4	4
			132	1845	-1951	93	-77	22	-12	4	4
475	Copertura	53-55	0	2230	-2152	195	-129	59	-6	23	23
			66	2230	-2152	200	-139	60	-8	23	23
			132	2230	-2152	205	-149	61	-10	23	23
476	Copertura	54-56	0	2048	-2314	123	-196	3	-61	-25	-25
			66	2048	-2322	134	-201	5	-62	-25	-25
			132	2048	-2330	144	-207	7	-63	-25	-25
477	Copertura	55-57	0	2694	-1571	760	-1820	102	-414	-52	-52
			80	2694	-1571	760	-1820	102	-414	-52	-52
			159	2694	-1571	760	-1820	102	-414	-52	-52
478	Copertura	56-70	0	1854	-1910	1866	-757	440	-85	71	71
			80	1854	-1922	1866	-757	440	-85	71	71
			159	1854	-1933	1866	-757	440	-85	71	71
479	Copertura	57-58	0	1356	-1300	952	-388	218	-50	28	28
			83	1356	-1300	937	-381	215	-49	28	28
			166	1356	-1300	921	-373	212	-47	28	28
480	Copertura	58-59	0	645	-1123	670	-320	135	-63	0	0
			69	645	-1114	658	-314	133	-62	0	0
			138	645	-1105	646	-308	130	-60	0	0
481	Copertura	59-60	0	1323	-963	492	-250	93	-56	-7	-7
			69	1305	-963	480	-244	90	-55	-7	-7
			138	1287	-963	468	-238	88	-53	-7	-7
482	Copertura	60-61	0	1270	-1250	343	-175	64	-39	-6	-6
			69	1270	-1250	331	-169	62	-38	-6	-6
			138	1270	-1250	319	-163	59	-37	-6	-6
483	Copertura	61-62	0	553	-559	219	-110	42	-24	-3	-3
			69	553	-559	206	-104	39	-23	-3	-3
			138	553	-559	194	-98	37	-22	-3	-3
484	Copertura	62-63	0	759	-844	113	-56	22	-12	-1	-1
			69	759	-835	101	-50	19	-11	-1	-1
			138	759	-826	89	-44	17	-10	-1	-1
485	Copertura	63-64	0	1184	-1189	27	-27	5	-6	0	0
			69	1184	-1184	27	-27	5	-6	0	0
			138	1186	-1184	27	-27	5	-6	0	0
486	Copertura	64-65	0	834	-854	45	-89	10	-17	1	1
			69	840	-872	51	-102	11	-20	1	1
			138	845	-890	57	-114	12	-22	1	1
487	Copertura	65-66	0	728	-705	99	-196	22	-37	3	3
			69	728	-705	106	-208	23	-40	3	3
			138	728	-705	112	-220	24	-42	3	3
488	Copertura	66-67	0	1427	-1389	166	-322	37	-60	6	6
			69	1427	-1389	172	-334	39	-62	6	6

			138	1427	-1389	178	-346	40	-65	6	6
489	Copertura	67-68	0	1038	-990	242	-472	54	-89	7	7
			69	1038	-990	248	-484	55	-91	7	7
			138	1038	-990	254	-496	56	-94	7	7
490	Copertura	68-69	0	972	-782	315	-655	61	-133	-1	-1
			69	982	-782	321	-667	63	-135	-1	-1
			138	991	-782	327	-679	64	-137	-1	-1
491	Copertura	69-70	0	1455	-2255	393	-946	49	-219	-31	-31
			83	1455	-2278	401	-962	51	-222	-31	-31
			166	1455	-2302	408	-978	52	-225	-31	-31
492	Copertura	1-1	0	815	-849	10	-34	-9	-18	-13	-13
			220	815	-841	8	-35	-9	-18	-13	-13
			440	815	-841	54	-127	0	-36	-13	-13
493	Copertura	2-2	0	14	-17	1	-4	-1	-2	-1	-1
			220	14	-17	1	-4	-1	-2	-1	-1
			440	14	-17	1	-4	-1	-2	-1	-1
494	Copertura	3-3	0	17	-18	2	-4	0	-2	-1	-1
			220	17	-18	2	-4	0	-2	-1	-1
			440	17	-18	2	-4	0	-2	-1	-1
495	Copertura	4-4	0	17	-18	2	-3	0	-1	-1	-1
			220	17	-18	2	-3	0	-1	-1	-1
			440	17	-18	2	-3	0	-1	-1	-1
496	Copertura	5-5	0	18	-19	3	-3	0	-1	0	0
			220	18	-19	3	-3	0	-1	0	0
			440	18	-19	3	-3	0	-1	0	0
497	Copertura	6-6	0	16	-17	2	-3	0	-1	0	0
			220	16	-17	2	-3	0	-1	0	0
			440	16	-17	2	-3	0	-1	0	0
498	Copertura	7-7	0	16	-16	2	-3	0	-1	0	0
			220	16	-16	2	-3	0	-1	0	0
			440	16	-16	2	-3	0	-1	0	0
499	Copertura	8-8	0	19	-19	3	-3	1	-1	0	0
			220	19	-19	3	-3	1	-1	0	0
			440	19	-19	3	-3	1	-1	0	0
500	Copertura	9-9	0	17	-16	3	-2	1	0	0	0
			220	17	-16	3	-2	1	0	0	0
			440	17	-16	3	-2	1	0	0	0
501	Copertura	10-10	0	17	-16	3	-2	1	0	0	0
			220	17	-16	3	-2	1	0	0	0
			440	17	-16	3	-2	1	0	0	0
502	Copertura	11-11	0	19	-17	4	-2	1	0	1	1
			220	19	-17	4	-2	1	0	1	1
			440	19	-17	4	-2	1	0	1	1
503	Copertura	12-12	0	18	-16	4	-2	2	0	1	1
			220	18	-16	4	-2	2	0	1	1
			440	18	-16	4	-2	2	0	1	1
504	Copertura	13-13	0	17	-14	4	-1	2	1	1	1
			220	17	-14	4	-1	2	1	1	1
			440	17	-14	4	-1	2	1	1	1
505	Copertura	57-57	0	787	-814	9	-33	-9	-17	-12	-12
			220	787	-812	10	-37	-8	-18	-12	-12
			440	787	-915	55	-128	1	-36	-12	-12
506	Copertura	58-58	0	15	-17	1	-4	-1	-2	-1	-1
			220	15	-17	1	-4	-1	-2	-1	-1
			440	15	-17	1	-4	-1	-2	-1	-1

507	Copertura	59-59	0	17	-19	2	-4	0	-1	-1	-1
			220	17	-19	2	-4	0	-1	-1	-1
			440	17	-19	2	-4	0	-1	-1	-1
508	Copertura	60-60	0	18	-19	2	-4	0	-1	-1	-1
			220	18	-19	2	-4	0	-1	-1	-1
			440	18	-19	2	-4	0	-1	-1	-1
509	Copertura	61-61	0	17	-17	2	-3	0	-1	0	0
			220	17	-17	2	-3	0	-1	0	0
			440	17	-17	2	-3	0	-1	0	0
510	Copertura	62-62	0	17	-18	2	-3	0	-1	0	0
			220	17	-18	2	-3	0	-1	0	0
			440	17	-18	2	-3	0	-1	0	0
511	Copertura	63-63	0	20	-20	3	-3	1	-1	0	0
			220	20	-20	3	-3	1	-1	0	0
			440	20	-20	3	-3	1	-1	0	0
512	Copertura	64-64	0	20	-20	3	-3	1	-1	0	0
			220	20	-20	3	-3	1	-1	0	0
			440	20	-20	3	-3	1	-1	0	0
513	Copertura	65-65	0	18	-17	3	-2	1	0	0	0
			220	18	-17	3	-2	1	0	0	0
			440	18	-17	3	-2	1	0	0	0
514	Copertura	66-66	0	18	-17	3	-2	1	0	0	0
			220	18	-17	3	-2	1	0	0	0
			440	18	-17	3	-2	1	0	0	0
515	Copertura	67-67	0	20	-19	4	-2	1	0	1	1
			220	20	-19	4	-2	1	0	1	1
			440	20	-19	4	-2	1	0	1	1
516	Copertura	68-68	0	20	-18	4	-2	2	0	1	1
			220	20	-18	4	-2	2	0	1	1
			440	20	-18	4	-2	2	0	1	1
517	Copertura	69-69	0	18	-15	4	-1	2	1	1	1
			220	18	-15	4	-1	2	1	1	1
			440	18	-15	4	-1	2	1	1	1
518	Copertura	1-74	0	176	-170	9	-4	4	1	2	2
			118	176	-170	9	-4	4	1	2	2
			235	176	-170	9	-4	4	1	2	2
519	Copertura	74-2	0	33	-35	2	-7	-1	-2	-1	-1
			118	33	-35	2	-7	-1	-2	-1	-1
			235	33	-35	2	-7	-1	-2	-1	-1
520	Copertura	6-71	0	35	-35	0	-1	0	0	0	0
			115	35	-35	0	-1	0	0	0	0
			231	35	-35	0	-1	0	0	0	0
521	Copertura	71-7	0	26	-26	1	-1	0	0	0	0
			115	26	-26	1	-1	0	0	0	0
			231	26	-26	1	-1	0	0	0	0
522	Copertura	9-72	0	29	-29	1	-1	0	0	0	0
			115	29	-29	1	-1	0	0	0	0
			231	29	-29	1	-1	0	0	0	0
523	Copertura	72-10	0	15	-15	0	0	0	0	0	0
			115	15	-15	0	0	0	0	0	0
			231	15	-15	0	0	0	0	0	0
524	Copertura	73-13	0	27	-16	7	-1	2	1	1	1
			118	27	-16	7	-1	2	1	1	1
			235	27	-16	7	-1	2	1	1	1
525	Copertura	14-7	0	41	-51	2	-6	-2	-3	-2	-2

	a	3									
			118	41	-51	2	-6	-2	-3	-2	-2
			235	41	-51	2	-6	-2	-3	-2	-2
526	Copertura	57-75	0	163	-168	4	-9	-1	-4	-2	-2
			118	163	-168	4	-9	-1	-4	-2	-2
			235	163	-168	4	-9	-1	-4	-2	-2
527	Copertura	75-58	0	30	-31	7	-2	2	1	1	1
			118	30	-31	7	-2	2	1	1	1
			235	30	-31	7	-2	2	1	1	1
528	Copertura	77-61	0	25	-25	0	0	0	0	0	0
			115	25	-25	0	0	0	0	0	0
			231	25	-25	0	0	0	0	0	0
529	Copertura	62-77	0	41	-41	1	-1	0	0	0	0
			115	41	-41	1	-1	0	0	0	0
			231	41	-41	1	-1	0	0	0	0
530	Copertura	65-78	0	39	-39	1	-1	0	0	0	0
			115	39	-39	1	-1	0	0	0	0
			231	39	-39	1	-1	0	0	0	0
531	Copertura	78-66	0	22	-22	0	0	0	0	0	0
			115	22	-22	0	0	0	0	0	0
			231	22	-22	0	0	0	0	0	0
532	Copertura	69-76	0	15	-16	1	-7	-1	-2	-1	-1
			118	15	-16	1	-7	-1	-2	-1	-1
			235	15	-16	1	-7	-1	-2	-1	-1
533	Copertura	76-70	0	37	-32	6	-1	3	2	2	2
			118	37	-32	6	-1	3	2	2	2
			235	37	-32	6	-1	3	2	2	2
534	Copertura	1-74	0	171	-176	0	-7	-2	-3	-2	-2
			118	171	-176	0	-7	-2	-3	-2	-2
			235	171	-176	0	-7	-2	-3	-2	-2
535	Copertura	74-2	0	64	-61	3	0	2	1	1	1
			118	64	-61	3	0	2	1	1	1
			235	64	-61	3	0	2	1	1	1
536	Copertura	6-71	0	34	-33	1	0	0	0	0	0
			115	34	-33	1	0	0	0	0	0
			231	34	-33	1	0	0	0	0	0
537	Copertura	71-7	0	36	-37	1	-1	0	0	0	0
			115	36	-37	1	-1	0	0	0	0
			231	36	-37	1	-1	0	0	0	0
538	Copertura	9-72	0	19	-19	1	0	0	0	0	0
			115	19	-19	1	0	0	0	0	0
			231	19	-19	1	0	0	0	0	0
539	Copertura	72-10	0	24	-25	0	0	0	0	0	0
			115	24	-25	0	0	0	0	0	0
			231	24	-25	0	0	0	0	0	0
540	Copertura	73-13	0	35	-39	-1	-3	-1	-2	-1	-1
			118	35	-39	-1	-3	-1	-2	-1	-1
			235	35	-39	-1	-3	-1	-2	-1	-1
541	Copertura	14-73	0	41	-36	4	2	3	2	2	2
			118	41	-36	4	2	3	2	2	2
			235	41	-36	4	2	3	2	2	2
542	Copertura	15-125	0	1527	-1536	4	-20	-4	-9	-6	-6
			75	1527	-1536	4	-20	-4	-9	-6	-6
			150	1527	-1536	4	-20	-4	-9	-6	-6
543	Copertura	127-16	0	510	-461	42	21	30	24	24	24

			75	510	-461	42	21	30	24	24	24
			150	510	-461	42	21	30	24	24	24
544	Copertura	17-129	0	1593	-1589	10	-13	1	-4	-1	-1
			75	1593	-1589	10	-13	1	-4	-1	-1
			150	1593	-1589	10	-13	1	-4	-1	-1
545	Copertura	130-18	0	683	-670	12	-9	4	-1	1	1
			75	683	-670	12	-9	4	-1	1	1
			150	683	-670	12	-9	4	-1	1	1
546	Copertura	19-135	0	1553	-1548	9	-9	2	-2	0	0
			75	1553	-1548	9	-9	2	-2	0	0
			150	1553	-1548	9	-9	2	-2	0	0
547	Copertura	134-20	0	624	-617	8	-7	2	-1	0	0
			75	624	-617	8	-7	2	-1	0	0
			150	624	-617	8	-7	2	-1	0	0
548	Copertura	21-136	0	1367	-1365	6	-6	1	-1	0	0
			75	1367	-1365	6	-6	1	-1	0	0
			150	1367	-1365	6	-6	1	-1	0	0
549	Copertura	138-22	0	354	-354	6	-7	1	-2	0	0
			75	354	-354	6	-7	1	-2	0	0
			150	354	-354	6	-7	1	-2	0	0
550	Copertura	23-141	0	1404	-1404	4	-4	1	-1	0	0
			75	1404	-1404	4	-4	1	-1	0	0
			150	1404	-1404	4	-4	1	-1	0	0
551	Copertura	142-24	0	407	-408	3	-4	0	-1	0	0
			75	407	-408	3	-4	0	-1	0	0
			150	407	-408	3	-4	0	-1	0	0
552	Copertura	25-145	0	1504	-1505	2	-2	0	0	0	0
			75	1504	-1505	2	-2	0	0	0	0
			150	1504	-1505	2	-2	0	0	0	0
553	Copertura	146-26	0	630	-629	2	-3	0	-1	0	0
			75	630	-629	2	-3	0	-1	0	0
			150	630	-629	2	-3	0	-1	0	0
554	Copertura	150-27	0	705	-705	0	-1	0	-1	0	0
			75	705	-705	0	-1	0	-1	0	0
			150	705	-705	0	-1	0	-1	0	0
555	Copertura	28-149	0	1533	-1538	1	-3	0	-1	-1	-1
			75	1533	-1538	1	-3	0	-1	-1	-1
			150	1533	-1538	1	-3	0	-1	-1	-1
556	Copertura	154-29	0	389	-391	-1	-2	-1	-1	-1	-1
			75	389	-391	-1	-2	-1	-1	-1	-1
			150	389	-391	-1	-2	-1	-1	-1	-1
557	Copertura	30-153	0	1323	-1329	1	-3	-1	-2	-1	-1
			75	1323	-1329	1	-3	-1	-2	-1	-1
			150	1323	-1329	1	-3	-1	-2	-1	-1
558	Copertura	158-31	0	326	-328	-1	-2	-1	-1	-1	-1
			75	326	-328	-1	-2	-1	-1	-1	-1
			150	326	-328	-1	-2	-1	-1	-1	-1
559	Copertura	32-157	0	1324	-1327	1	-3	-1	-2	-1	-1
			75	1324	-1327	1	-3	-1	-2	-1	-1
			150	1324	-1327	1	-3	-1	-2	-1	-1
560	Copertura	162-33	0	530	-532	-1	-2	-1	-1	-1	-1
			75	530	-532	-1	-2	-1	-1	-1	-1
			150	530	-532	-1	-2	-1	-1	-1	-1
561	Copertura	34-161	0	1449	-1452	1	-4	-1	-2	-1	-1
			75	1449	-1452	1	-4	-1	-2	-1	-1

			150	1449	-1452	1	-4	-1	-2	-1	-1
562	Copertura	166-35	0	690	-694	-1	-2	-1	-1	-1	-1
			75	690	-694	-1	-2	-1	-1	-1	-1
			150	690	-694	-1	-2	-1	-1	-1	-1
563	Copertura	36-165	0	1549	-1552	1	-4	-1	-2	-1	-1
			75	1549	-1552	1	-4	-1	-2	-1	-1
			150	1549	-1552	1	-4	-1	-2	-1	-1
564	Copertura	170-37	0	475	-478	-1	-2	-1	-2	-1	-1
			75	475	-478	-1	-2	-1	-2	-1	-1
			150	475	-478	-1	-2	-1	-2	-1	-1
565	Copertura	38-169	0	1405	-1412	0	-4	-1	-2	-1	-1
			75	1405	-1412	0	-4	-1	-2	-1	-1
			150	1405	-1412	0	-4	-1	-2	-1	-1
566	Copertura	175-39	0	276	-279	-1	-2	-1	-2	-1	-1
			75	276	-279	-1	-2	-1	-2	-1	-1
			150	276	-279	-1	-2	-1	-2	-1	-1
567	Copertura	40-173	0	1296	-1301	0	-4	-1	-2	-1	-1
			75	1296	-1301	0	-4	-1	-2	-1	-1
			150	1296	-1301	0	-4	-1	-2	-1	-1
568	Copertura	178-41	0	405	-407	-1	-2	-1	-1	-1	-1
			75	405	-407	-1	-2	-1	-1	-1	-1
			150	405	-407	-1	-2	-1	-1	-1	-1
569	Copertura	42-177	0	1449	-1454	0	-4	-1	-2	-2	-2
			75	1449	-1454	0	-4	-1	-2	-2	-2
			150	1449	-1454	0	-4	-1	-2	-2	-2
570	Copertura	43-181	0	1555	-1559	2	-2	0	0	0	0
			75	1555	-1559	2	-2	0	0	0	0
			150	1555	-1559	2	-2	0	0	0	0
571	Copertura	182-44	0	667	-669	0	-2	-1	-1	-1	-1
			75	667	-669	0	-2	-1	-1	-1	-1
			150	667	-669	0	-2	-1	-1	-1	-1
572	Copertura	45-185	0	1547	-1549	2	-2	0	0	0	0
			75	1547	-1549	2	-2	0	0	0	0
			150	1547	-1549	2	-2	0	0	0	0
573	Copertura	186-46	0	635	-636	1	-1	0	0	0	0
			75	635	-636	1	-1	0	0	0	0
			150	635	-636	1	-1	0	0	0	0
574	Copertura	47-189	0	1372	-1375	3	-3	1	-1	0	0
			75	1372	-1375	3	-3	1	-1	0	0
			150	1372	-1375	3	-3	1	-1	0	0
575	Copertura	190-48	0	383	-381	3	-3	0	-1	0	0
			75	383	-381	3	-3	0	-1	0	0
			150	383	-381	3	-3	0	-1	0	0
576	Copertura	49-193	0	1387	-1392	5	-6	1	-1	0	0
			75	1387	-1392	5	-6	1	-1	0	0
			150	1387	-1392	5	-6	1	-1	0	0
577	Copertura	195-50	0	294	-294	4	-4	1	-1	0	0
			75	294	-294	4	-4	1	-1	0	0
			150	294	-294	4	-4	1	-1	0	0
578	Copertura	51-197	0	1477	-1481	8	-8	1	-2	0	0
			75	1477	-1481	8	-8	1	-2	0	0
			150	1477	-1481	8	-8	1	-2	0	0
579	Copertura	199-52	0	516	-509	8	-8	2	-2	0	0
			75	516	-509	8	-8	2	-2	0	0
			150	516	-509	8	-8	2	-2	0	0

580	Copertura	53-201	0	1599	-1606	12	-9	3	-1	1	1
			75	1599	-1606	12	-9	3	-1	1	1
			150	1599	-1606	12	-9	3	-1	1	1
581	Copertura	202-54	0	683	-699	4	-14	-3	-6	-4	-4
			75	683	-699	4	-14	-3	-6	-4	-4
			150	683	-699	4	-14	-3	-6	-4	-4
582	Copertura	55-205	0	1540	-1535	19	-4	9	4	6	6
			75	1540	-1535	19	-4	9	4	6	6
			150	1540	-1535	19	-4	9	4	6	6
583	Copertura	206-56	0	480	-500	0	-21	-7	-12	-8	-8
			75	480	-500	0	-21	-7	-12	-8	-8
			150	480	-500	0	-21	-7	-12	-8	-8
584	Copertura	57-75	0	169	-164	7	0	3	2	2	2
			118	169	-164	7	0	3	2	2	2
			235	169	-164	7	0	3	2	2	2
585	Copertura	75-58	0	53	-55	0	-3	-1	-2	-1	-1
			118	53	-55	0	-3	-1	-2	-1	-1
			235	53	-55	0	-3	-1	-2	-1	-1
586	Copertura	77-61	0	32	-32	0	0	0	0	0	0
			115	32	-32	0	0	0	0	0	0
			231	32	-32	0	0	0	0	0	0
587	Copertura	62-77	0	27	-27	1	0	0	0	0	0
			115	27	-27	1	0	0	0	0	0
			231	27	-27	1	0	0	0	0	0
588	Copertura	65-78	0	27	-27	0	-1	0	0	0	0
			115	27	-27	0	-1	0	0	0	0
			231	27	-27	0	-1	0	0	0	0
589	Copertura	78-66	0	32	-32	0	0	0	0	0	0
			115	32	-32	0	0	0	0	0	0
			231	32	-32	0	0	0	0	0	0
590	Copertura	69-76	0	29	-27	2	1	2	1	1	1
			118	29	-27	2	1	2	1	1	1
			235	29	-27	2	1	2	1	1	1
591	Copertura	76-70	0	27	-34	-2	-4	-2	-3	-2	-2
			118	27	-34	-2	-4	-2	-3	-2	-2
			235	27	-34	-2	-4	-2	-3	-2	-2
592	Copertura	79-81	0	150	38	124	83	100	83	83	83
			80	150	38	124	83	100	83	83	83
			159	150	38	124	83	100	83	83	83
593	Copertura	80-82	0	45	-66	-9	-14	-9	-10	-9	-9
			66	45	-66	-9	-14	-9	-10	-9	-9
			132	45	-66	-9	-14	-9	-10	-9	-9
594	Copertura	83-84	0	51	-54	-1	-2	-1	-1	-1	-1
			66	51	-54	-1	-2	-1	-1	-1	-1
			132	51	-54	-1	-2	-1	-1	-1	-1
595	Copertura	85-86	0	51	-51	0	0	0	0	0	0
			66	51	-51	0	0	0	0	0	0
			132	51	-51	0	0	0	0	0	0
596	Copertura	87-88	0	39	-39	0	0	0	0	0	0
			66	39	-39	0	0	0	0	0	0
			132	39	-39	0	0	0	0	0	0
597	Copertura	89-90	0	30	-30	0	0	0	0	0	0
			66	30	-30	0	0	0	0	0	0
			132	30	-30	0	0	0	0	0	0
598	Copertura	91-9	0	27	-27	0	0	0	0	0	0

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			66	27	-27	0	0	0	0	0	0
			132	27	-27	0	0	0	0	0	0
599	Copertura	93-94	0	37	-37	0	0	0	0	0	0
			66	37	-37	0	0	0	0	0	0
			132	37	-37	0	0	0	0	0	0
600	Copertura	95-96	0	40	-40	0	0	0	0	0	0
			66	40	-40	0	0	0	0	0	0
			132	40	-40	0	0	0	0	0	0
601	Copertura	97-106	0	29	-29	0	0	0	0	0	0
			66	29	-29	0	0	0	0	0	0
			132	29	-29	0	0	0	0	0	0
602	Copertura	98-99	0	42	-47	0	-6	-2	-3	-2	-2
			66	42	-47	0	-6	-2	-3	-2	-2
			132	42	-47	0	-6	-2	-3	-2	-2
603	Copertura	100-101	0	49	-49	2	-2	0	0	0	0
			66	49	-49	2	-2	0	0	0	0
			132	49	-49	2	-2	0	0	0	0
604	Copertura	102-103	0	63	-63	0	0	0	0	0	0
			66	63	-63	0	0	0	0	0	0
			132	63	-63	0	0	0	0	0	0
605	Copertura	104-105	0	55	-56	0	-1	0	0	0	0
			66	55	-56	0	-1	0	0	0	0
			132	55	-56	0	-1	0	0	0	0
606	Copertura	107-108	0	30	-23	5	3	4	3	3	3
			66	30	-23	5	3	4	3	3	3
			132	30	-23	5	3	4	3	3	3
607	Copertura	109-110	0	-11	-138	-66	-99	-66	-79	-66	-66
			80	-11	-138	-66	-99	-66	-79	-66	-66
			159	-11	-138	-66	-99	-66	-79	-66	-66
608	Copertura	111-112	0	62	-64	0	-1	0	0	0	0
			66	62	-64	0	-1	0	0	0	0
			132	62	-64	0	-1	0	0	0	0
609	Copertura	113-114	0	60	-60	0	-1	0	0	0	0
			66	60	-60	0	-1	0	0	0	0
			132	60	-60	0	-1	0	0	0	0
610	Copertura	115-116	0	21	-21	0	-1	0	-1	0	0
			66	21	-21	0	-1	0	-1	0	0
			132	21	-21	0	-1	0	-1	0	0
611	Copertura	117-118	0	63	-63	1	-1	0	0	0	0
			66	63	-63	1	-1	0	0	0	0
			132	63	-63	1	-1	0	0	0	0
612	Copertura	119-120	0	65	-65	4	-1	2	1	1	1
			66	65	-65	4	-1	2	1	1	1
			132	65	-65	4	-1	2	1	1	1
613	Copertura	121-122	0	67	-69	5	-3	1	0	1	1
			66	67	-69	5	-3	1	0	1	1
			132	67	-69	5	-3	1	0	1	1
614	Copertura	124-125	0	79	-66	9	5	7	6	6	6
			99	79	-66	9	5	7	6	6	6
			198	79	-66	9	5	7	6	6	6
615	Copertura	125-127	0	91	-92	10	-10	2	-2	0	0
			775	91	-92	10	-10	2	-2	0	0
			1550	91	-92	10	-10	2	-2	0	0
616	Copertura	126-127	0	-2	-49	-25	-36	-25	-30	-25	-25

			99	-2	-49	-25	-36	-25	-30	-25	-25
			198	-2	-49	-25	-36	-25	-30	-25	-25
617	Copertura	128-129	0	73	-70	4	-1	2	1	1	1
			99	73	-70	4	-1	2	1	1	1
			198	73	-70	4	-1	2	1	1	1
618	Copertura	129-130	0	98	-98	9	-9	2	-2	0	0
			775	98	-98	9	-9	2	-2	0	0
			1550	98	-98	9	-9	2	-2	0	0
619	Copertura	131-130	0	24	-27	0	-4	-1	-2	-1	-1
			99	24	-27	0	-4	-1	-2	-1	-1
			198	24	-27	0	-4	-1	-2	-1	-1
620	Copertura	132-135	0	72	-72	2	-2	0	-1	0	0
			99	72	-72	2	-2	0	-1	0	0
			198	72	-72	2	-2	0	-1	0	0
621	Copertura	133-134	0	25	-25	1	-2	0	0	0	0
			99	25	-25	1	-2	0	0	0	0
			198	25	-25	1	-2	0	0	0	0
622	Copertura	135-134	0	98	-98	7	-7	1	-1	0	0
			775	98	-98	7	-7	1	-1	0	0
			1550	98	-98	7	-7	1	-1	0	0
623	Copertura	137-136	0	71	-71	1	-2	0	0	0	0
			99	71	-71	1	-2	0	0	0	0
			198	71	-71	1	-2	0	0	0	0
624	Copertura	136-138	0	94	-94	5	-5	1	-1	0	0
			775	94	-94	5	-5	1	-1	0	0
			1550	94	-94	5	-5	1	-1	0	0
625	Copertura	139-138	0	26	-25	2	-1	1	0	0	0
			99	26	-25	2	-1	1	0	0	0
			198	26	-25	2	-1	1	0	0	0
626	Copertura	140-141	0	70	-71	1	-1	0	0	0	0
			99	70	-71	1	-1	0	0	0	0
			198	70	-71	1	-1	0	0	0	0
627	Copertura	141-142	0	89	-89	3	-3	1	-1	0	0
			775	89	-89	3	-3	1	-1	0	0
			1550	89	-89	3	-3	1	-1	0	0
628	Copertura	143-142	0	22	-22	1	-1	0	0	0	0
			99	22	-22	1	-1	0	0	0	0
			198	22	-22	1	-1	0	0	0	0
629	Copertura	144-145	0	67	-67	1	-1	0	0	0	0
			99	67	-67	1	-1	0	0	0	0
			198	67	-67	1	-1	0	0	0	0
630	Copertura	145-146	0	86	-86	2	-2	0	0	0	0
			775	86	-86	2	-2	0	0	0	0
			1550	86	-86	2	-2	0	0	0	0
631	Copertura	147-146	0	27	-27	2	-1	1	0	0	0
			99	27	-27	2	-1	1	0	0	0
			198	27	-27	2	-1	1	0	0	0
632	Copertura	148-149	0	66	-64	2	0	1	1	1	1
			99	66	-64	2	0	1	1	1	1
			198	66	-64	2	0	1	1	1	1
633	Copertura	149-150	0	83	-83	1	-1	0	0	0	0
			775	83	-83	1	-1	0	0	0	0
			1550	83	-83	1	-1	0	0	0	0
634	Copertura	151-150	0	23	-22	2	-1	1	0	0	0
			99	23	-22	2	-1	1	0	0	0

			198	23	-22	2	-1	1	0	0	0
635	Copertura	152-153	0	66	-63	3	0	1	1	1	1
			99	66	-63	3	0	1	1	1	1
			198	66	-63	3	0	1	1	1	1
636	Copertura	153-154	0	77	-76	1	-1	0	0	0	0
			775	77	-76	1	-1	0	0	0	0
			1551	77	-76	1	-1	0	0	0	0
637	Copertura	155-154	0	27	-25	3	0	1	1	1	1
			99	27	-25	3	0	1	1	1	1
			198	27	-25	3	0	1	1	1	1
638	Copertura	156-157	0	67	-64	3	0	2	1	1	1
			99	67	-64	3	0	2	1	1	1
			198	67	-64	3	0	2	1	1	1
639	Copertura	157-158	0	74	-73	1	-1	0	0	0	0
			775	74	-73	1	-1	0	0	0	0
			1551	74	-73	1	-1	0	0	0	0
640	Copertura	159-158	0	19	-17	3	0	1	1	1	1
			99	19	-17	3	0	1	1	1	1
			198	19	-17	3	0	1	1	1	1
641	Copertura	160-161	0	65	-62	3	0	2	1	1	1
			99	65	-62	3	0	2	1	1	1
			198	65	-62	3	0	2	1	1	1
642	Copertura	161-162	0	74	-73	1	-1	0	0	0	0
			776	74	-73	1	-1	0	0	0	0
			1551	74	-73	1	-1	0	0	0	0
643	Copertura	163-162	0	23	-21	3	0	2	1	1	1
			99	23	-21	3	0	2	1	1	1
			198	23	-21	3	0	2	1	1	1
644	Copertura	164-165	0	67	-64	3	0	2	1	1	1
			99	67	-64	3	0	2	1	1	1
			198	67	-64	3	0	2	1	1	1
645	Copertura	165-166	0	73	-72	1	-1	0	0	0	0
			776	73	-72	1	-1	0	0	0	0
			1551	73	-72	1	-1	0	0	0	0
646	Copertura	167-166	0	21	-20	3	0	2	1	1	1
			99	21	-20	3	0	2	1	1	1
			198	21	-20	3	0	2	1	1	1
647	Copertura	168-169	0	67	-64	3	0	2	1	1	1
			99	67	-64	3	0	2	1	1	1
			198	67	-64	3	0	2	1	1	1
648	Copertura	169-170	0	73	-71	1	-1	0	0	0	0
			776	73	-71	1	-1	0	0	0	0
			1552	73	-71	1	-1	0	0	0	0
649	Copertura	171-170	0	21	-18	3	0	2	1	1	1
			99	21	-18	3	0	2	1	1	1
			198	21	-18	3	0	2	1	1	1
650	Copertura	172-173	0	67	-64	3	1	2	1	2	2
			99	67	-64	3	1	2	1	2	2
			198	67	-64	3	1	2	1	2	2
651	Copertura	173-175	0	72	-70	1	-1	0	0	0	0
			776	72	-70	1	-1	0	0	0	0
			1552	72	-70	1	-1	0	0	0	0
652	Copertura	174-175	0	18	-16	3	1	2	1	1	1
			99	18	-16	3	1	2	1	1	1
			198	18	-16	3	1	2	1	1	1

653	Copertura	176-177	0	72	-69	3	1	2	2	2	2
			99	72	-69	3	1	2	2	2	2
			198	72	-69	3	1	2	2	2	2
654	Copertura	177-178	0	74	-73	1	-1	0	0	0	0
			776	74	-73	1	-1	0	0	0	0
			1552	74	-73	1	-1	0	0	0	0
655	Copertura	179-178	0	13	-11	2	0	1	1	1	1
			99	13	-11	2	0	1	1	1	1
			198	13	-11	2	0	1	1	1	1
656	Copertura	180-181	0	70	-70	1	-1	0	0	0	0
			99	70	-70	1	-1	0	0	0	0
			198	70	-70	1	-1	0	0	0	0
657	Copertura	181-182	0	79	-78	1	-1	0	0	0	0
			775	79	-78	1	-1	0	0	0	0
			1550	79	-78	1	-1	0	0	0	0
658	Copertura	183-182	0	16	-12	2	0	1	1	1	1
			99	16	-12	2	0	1	1	1	1
			198	16	-12	2	0	1	1	1	1
659	Copertura	184-185	0	67	-67	1	-1	0	0	0	0
			99	67	-67	1	-1	0	0	0	0
			198	67	-67	1	-1	0	0	0	0
660	Copertura	185-186	0	88	-87	1	-1	0	0	0	0
			775	88	-87	1	-1	0	0	0	0
			1550	88	-87	1	-1	0	0	0	0
661	Copertura	187-186	0	17	-15	1	-1	0	0	0	0
			99	17	-15	1	-1	0	0	0	0
			198	17	-15	1	-1	0	0	0	0
662	Copertura	188-189	0	69	-69	1	-1	0	0	0	0
			99	69	-69	1	-1	0	0	0	0
			198	69	-69	1	-1	0	0	0	0
663	Copertura	189-190	0	92	-90	2	-3	0	-1	0	0
			775	92	-90	2	-3	0	-1	0	0
			1550	92	-90	2	-3	0	-1	0	0
664	Copertura	191-190	0	22	-22	1	-1	0	0	0	0
			99	22	-22	1	-1	0	0	0	0
			198	22	-22	1	-1	0	0	0	0
665	Copertura	192-193	0	71	-71	2	-1	0	0	0	0
			99	71	-71	2	-1	0	0	0	0
			198	71	-71	2	-1	0	0	0	0
666	Copertura	193-195	0	96	-93	4	-4	1	-1	0	0
			775	96	-93	4	-4	1	-1	0	0
			1550	96	-93	4	-4	1	-1	0	0
667	Copertura	194-195	0	20	-20	1	-1	0	0	0	0
			99	20	-20	1	-1	0	0	0	0
			198	20	-20	1	-1	0	0	0	0
668	Copertura	196-197	0	72	-72	2	-2	0	0	0	0
			99	72	-72	2	-2	0	0	0	0
			198	72	-72	2	-2	0	0	0	0
669	Copertura	197-199	0	103	-97	6	-6	1	-1	0	0
			775	103	-97	6	-6	1	-1	0	0
			1550	103	-97	6	-6	1	-1	0	0
670	Copertura	198-199	0	23	-23	1	-2	0	0	0	0
			99	23	-23	1	-2	0	0	0	0
			198	23	-23	1	-2	0	0	0	0
671	Copertura	200-	0	71	-74	1	-4	-1	-2	-1	-1

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			99	71	-74	1	-4	-1	-2	-1	-1
			198	71	-74	1	-4	-1	-2	-1	-1
672	Copertura	201-202	0	105	-97	8	-8	2	-2	0	0
			775	105	-97	8	-8	2	-2	0	0
			1550	105	-97	8	-8	2	-2	0	0
673	Copertura	203-202	0	26	-19	6	3	5	4	4	4
			99	26	-19	6	3	5	4	4	4
			198	26	-19	6	3	5	4	4	4
674	Copertura	204-205	0	67	-81	-6	-10	-6	-7	-6	-6
			99	67	-81	-6	-10	-6	-7	-6	-6
			198	67	-81	-6	-10	-6	-7	-6	-6
675	Copertura	205-206	0	99	-90	10	-10	2	-2	0	0
			775	99	-90	10	-10	2	-2	0	0
			1550	99	-90	10	-10	2	-2	0	0
676	Copertura	207-206	0	34	-13	12	8	10	8	8	8
			99	34	-13	12	8	10	8	8	8
			198	34	-13	12	8	10	8	8	8
677	Copertura	79-14	0	411	-446	-10	-46	-18	-26	-18	-18
			125	411	-446	40	-71	-9	-31	-18	-18
			250	411	-466	91	-96	1	-36	-18	-18
678	Copertura	124-15	0	1699	-149	1101	712	858	712	712	712
			155	1699	-149	1041	712	858	712	712	712
			310	1699	-149	1073	712	858	712	712	712
679	Copertura	80-16	0	359	-1729	-685	-1014	-685	-826	-685	-685
			45	359	-1729	-685	-1024	-685	-826	-685	-685
			90	359	-1729	-685	-1034	-685	-826	-685	-685
680	Copertura	128-17	0	1653	-644	797	504	616	504	504	504
			155	1653	-644	759	504	616	504	504	504
			310	1653	-644	792	504	616	504	504	504
681	Copertura	82-18	0	975	-1998	-512	-785	-512	-624	-512	-512
			43	975	-1998	-512	-794	-512	-624	-512	-512
			85	975	-1998	-512	-803	-512	-624	-512	-512
682	Copertura	132-19	0	1722	-718	771	502	613	502	502	502
			155	1722	-718	778	502	613	502	502	502
			310	1722	-718	811	502	615	502	502	502
683	Copertura	83-20	0	1016	-2016	-500	-791	-500	-610	-500	-500
			43	1016	-2016	-500	-800	-500	-610	-500	-500
			85	1016	-2016	-500	-809	-500	-613	-500	-500
684	Copertura	137-21	0	2038	-1002	785	518	632	518	518	518
			155	2038	-1002	818	518	632	518	518	518
			310	2038	-1002	852	510	639	518	518	518
685	Copertura	84-22	0	1022	-2059	-518	-834	-518	-634	-518	-518
			43	1022	-2059	-518	-843	-518	-637	-518	-518
			85	1022	-2059	-514	-855	-518	-640	-518	-518
686	Copertura	140-23	0	2451	-1404	803	524	639	524	524	524
			155	2451	-1404	835	524	639	524	524	524
			310	2451	-1404	875	501	649	524	524	524
687	Copertura	85-24	0	1240	-2286	-523	-853	-523	-643	-523	-523
			43	1240	-2286	-523	-865	-523	-646	-523	-523
			85	1240	-2286	-502	-880	-523	-649	-523	-523
688	Copertura	144-25	0	2878	-1830	802	524	639	524	524	524
			155	2878	-1830	838	524	639	524	524	524
			310	2878	-1830	886	491	651	524	524	524
689	Copertura	86-26	0	1489	-2534	-523	-859	-523	-645	-523	-523

			43	1489	-2534	-521	-874	-523	-648	-523	-523
			85	1489	-2534	-491	-889	-523	-651	-523	-523
690	Copertura	87-27	0	1724	-2769	-522	-865	-522	-646	-522	-522
			43	1724	-2769	-515	-880	-522	-649	-522	-522
			85	1724	-2769	-485	-895	-522	-652	-522	-522
691	Copertura	148-28	0	2901	-1854	801	524	639	524	524	524
			155	2901	-1854	839	524	639	524	524	524
			310	2901	-1854	890	486	652	524	524	524
692	Copertura	88-29	0	1958	-3000	-521	-865	-521	-645	-521	-521
			43	1958	-3000	-512	-880	-521	-648	-521	-521
			85	1958	-3000	-482	-895	-521	-651	-521	-521
693	Copertura	152-30	0	3021	-1978	805	522	636	522	522	522
			155	3021	-1978	840	522	638	522	522	522
			310	3021	-1978	888	483	650	522	522	522
694	Copertura	89-31	0	2085	-3127	-521	-863	-521	-644	-521	-521
			43	2085	-3127	-513	-878	-521	-647	-521	-521
			85	2085	-3127	-483	-893	-521	-650	-521	-521
695	Copertura	156-32	0	2979	-1937	806	521	635	521	521	521
			155	2979	-1937	840	521	638	521	521	521
			310	2979	-1937	888	481	649	521	521	521
696	Copertura	90-33	0	2061	-3102	-521	-860	-521	-643	-521	-521
			43	2061	-3102	-514	-875	-521	-646	-521	-521
			85	2061	-3102	-484	-890	-521	-649	-521	-521
697	Copertura	160-34	0	3002	-1960	806	521	636	521	521	521
			155	3002	-1960	839	521	638	521	521	521
			310	3002	-1960	887	484	649	521	521	521
698	Copertura	91-35	0	2039	-3081	-521	-856	-521	-642	-521	-521
			43	2039	-3081	-516	-871	-521	-645	-521	-521
			85	2039	-3081	-486	-886	-521	-648	-521	-521
699	Copertura	164-36	0	2977	-1934	804	521	636	521	521	521
			155	2977	-1934	838	521	637	521	521	521
			310	2977	-1934	884	489	649	521	521	521
700	Copertura	92-37	0	2045	-3086	-520	-851	-520	-641	-520	-520
			43	2045	-3086	-518	-866	-520	-644	-520	-520
			85	2045	-3086	-488	-881	-520	-647	-520	-520
701	Copertura	168-38	0	3067	-2025	802	521	635	521	521	521
			155	3067	-2025	836	521	636	521	521	521
			310	3067	-2025	881	493	647	521	521	521
702	Copertura	93-39	0	2042	-3083	-521	-849	-521	-640	-521	-521
			43	2042	-3083	-520	-861	-521	-643	-521	-521
			85	2042	-3083	-491	-876	-521	-646	-521	-521
703	Copertura	172-40	0	3030	-1992	802	519	633	519	519	519
			155	3030	-1992	836	519	635	519	519	519
			310	3030	-1992	883	482	647	519	519	519
704	Copertura	94-41	0	2011	-3054	-521	-849	-521	-641	-521	-521
			43	2011	-3054	-521	-861	-521	-644	-521	-521
			85	2011	-3054	-492	-876	-521	-647	-521	-521
705	Copertura	176-42	0	2795	-1756	819	520	634	520	520	520
			155	2795	-1756	841	520	637	520	520	520
			310	2795	-1756	872	506	645	520	520	520
706	Copertura	180-43	0	2781	-1744	817	518	632	518	518	518
			155	2781	-1744	839	518	636	518	518	518
			310	2781	-1744	868	508	643	518	518	518
707	Copertura	95-44	0	1821	-2862	-521	-848	-521	-640	-521	-521
			43	1821	-2862	-521	-861	-521	-643	-521	-521

			85	1821	-2862	-491	-876	-521	-646	-521	-521
708	Copertura	184-45	0	2793	-1753	802	520	634	520	520	520
			155	2793	-1753	835	520	635	520	520	520
			310	2793	-1753	879	490	646	520	520	520
709	Copertura	96-46	0	1824	-2867	-521	-845	-521	-640	-521	-521
			43	1824	-2867	-521	-854	-521	-643	-521	-521
			85	1824	-2867	-499	-869	-521	-646	-521	-521
710	Copertura	188-47	0	2594	-1551	795	522	636	522	522	522
			155	2594	-1551	828	522	636	522	522	522
			310	2594	-1551	865	512	645	522	522	522
711	Copertura	97-48	0	1600	-2641	-521	-839	-521	-637	-521	-521
			43	1600	-2641	-521	-848	-521	-640	-521	-521
			85	1600	-2641	-507	-860	-521	-643	-521	-521
712	Copertura	192-49	0	2245	-1209	783	518	632	518	518	518
			155	2245	-1209	814	518	632	518	518	518
			310	2245	-1209	846	518	638	518	518	518
713	Copertura	106-50	0	1105	-2137	-516	-824	-516	-630	-516	-516
			43	1105	-2137	-516	-833	-516	-632	-516	-516
			85	1105	-2137	-516	-842	-516	-635	-516	-516
714	Copertura	196-51	0	2112	-1107	776	502	613	502	502	502
			155	2112	-1107	776	502	613	502	502	502
			310	2112	-1107	809	502	615	502	502	502
715	Copertura	107-52	0	839	-1842	-502	-789	-502	-612	-502	-502
			43	839	-1842	-502	-798	-502	-612	-502	-502
			85	839	-1842	-502	-807	-502	-614	-502	-502
716	Copertura	200-53	0	2272	-1263	799	504	616	504	504	504
			155	2272	-1263	758	504	616	504	504	504
			310	2272	-1263	791	504	616	504	504	504
717	Copertura	108-54	0	814	-1818	-502	-769	-502	-613	-502	-502
			43	814	-1818	-502	-777	-502	-613	-502	-502
			85	814	-1818	-502	-786	-502	-613	-502	-502
718	Copertura	204-55	0	2075	-647	1104	714	860	714	714	714
			155	2075	-647	1043	714	860	714	714	714
			310	2075	-647	1075	714	860	714	714	714
719	Copertura	109-56	0	303	-1639	-668	-988	-668	-805	-668	-668
			43	303	-1639	-668	-997	-668	-805	-668	-668
			85	303	-1639	-668	-1007	-668	-805	-668	-668
720	Copertura	110-70	0	382	-465	30	-113	-32	-60	-42	-42
			43	382	-465	47	-122	-28	-62	-42	-42
			85	382	-465	64	-130	-25	-64	-42	-42
721	Copertura	14-79	0	451	-320	100	52	79	65	65	65
			95	451	-320	100	61	79	65	65	65
			190	451	-320	100	65	79	65	65	65
722	Copertura	15-124	0	-483	-3544	-1828	-2707	-1828	-2203	-1828	-1828
			65	-483	-3544	-1828	-2705	-1828	-2203	-1828	-1828
			130	-483	-3544	-1828	-2700	-1828	-2203	-1828	-1828
723	Copertura	16-126	0	3647	288	2687	1814	2186	1814	1814	1814
			65	3645	288	2685	1814	2186	1814	1814	1814
			130	3637	288	2680	1814	2186	1814	1814	1814
724	Copertura	17-128	0	262	-3706	-1722	-2612	-1722	-2092	-1722	-1722
			65	262	-3706	-1722	-2611	-1722	-2092	-1722	-1722
			130	262	-3706	-1722	-2606	-1722	-2092	-1722	-1722
725	Copertura	18-131	0	4062	-621	2614	1721	2091	1721	1721	1721
			65	4062	-621	2612	1721	2091	1721	1721	1721
			130	4062	-621	2607	1721	2091	1721	1721	1721

726	Copertura	19-132	0	739	-4197	-1729	-2674	-1729	-2101	-1729	-1729
			65	739	-4197	-1729	-2673	-1729	-2101	-1729	-1729
			130	739	-4197	-1729	-2668	-1729	-2101	-1729	-1729
727	Copertura	20-133	0	4473	-1015	2676	1729	2101	1729	1729	1729
			65	4473	-1015	2674	1729	2101	1729	1729	1729
			130	4473	-1015	2670	1729	2101	1729	1729	1729
728	Copertura	21-137	0	1361	-4835	-1737	-2722	-1737	-2111	-1737	-1737
			65	1361	-4835	-1737	-2721	-1737	-2111	-1737	-1737
			130	1361	-4835	-1737	-2716	-1737	-2111	-1737	-1737
729	Copertura	22-139	0	4877	-1404	2727	1737	2110	1737	1737	1737
			65	4877	-1404	2725	1737	2110	1737	1737	1737
			130	4877	-1404	2720	1737	2110	1737	1737	1737
730	Copertura	23-140	0	2046	-5529	-1741	-2753	-1741	-2116	-1741	-1741
			65	2046	-5529	-1741	-2752	-1741	-2116	-1741	-1741
			130	2046	-5529	-1741	-2747	-1741	-2116	-1741	-1741
731	Copertura	24-143	0	5427	-1945	2759	1741	2116	1741	1741	1741
			65	5427	-1945	2757	1741	2116	1741	1741	1741
			130	5427	-1945	2753	1741	2116	1741	1741	1741
732	Copertura	25-144	0	2784	-6277	-1747	-2776	-1747	-2122	-1747	-1747
			65	2784	-6277	-1747	-2774	-1747	-2122	-1747	-1747
			130	2784	-6277	-1747	-2769	-1747	-2122	-1747	-1747
733	Copertura	26-147	0	6015	-2528	2777	1743	2120	1743	1743	1743
			65	6015	-2528	2775	1743	2119	1743	1743	1743
			130	6015	-2528	2770	1743	2119	1743	1743	1743
734	Copertura	27-151	0	6436	-2956	2779	1740	2118	1740	1740	1740
			65	6436	-2956	2778	1740	2118	1740	1740	1740
			130	6436	-2956	2773	1740	2116	1740	1740	1740
735	Copertura	28-148	0	3138	-6622	-1742	-2775	-1742	-2118	-1742	-1742
			65	3138	-6622	-1742	-2774	-1742	-2118	-1742	-1742
			130	3138	-6622	-1742	-2768	-1742	-2116	-1742	-1742
736	Copertura	29-155	0	6799	-3332	2773	1734	2112	1734	1734	1734
			65	6799	-3332	2771	1734	2111	1734	1734	1734
			130	6799	-3332	2767	1734	2110	1734	1734	1734
737	Copertura	30-152	0	3481	-6946	-1733	-2765	-1733	-2109	-1733	-1733
			65	3481	-6946	-1733	-2764	-1733	-2108	-1733	-1733
			130	3481	-6946	-1733	-2759	-1733	-2106	-1733	-1733
738	Copertura	31-159	0	7035	-3570	2770	1733	2110	1733	1733	1733
			65	7035	-3570	2768	1733	2110	1733	1733	1733
			130	7035	-3570	2764	1733	2108	1733	1733	1733
739	Copertura	32-156	0	3671	-7133	-1731	-2763	-1731	-2106	-1731	-1731
			65	3671	-7133	-1731	-2761	-1731	-2106	-1731	-1731
			130	3671	-7133	-1731	-2756	-1731	-2104	-1731	-1731
740	Copertura	33-163	0	7123	-3662	2762	1730	2106	1730	1730	1730
			65	7123	-3662	2760	1730	2105	1730	1730	1730
			130	7123	-3662	2756	1730	2104	1730	1730	1730
741	Copertura	34-160	0	3697	-7160	-1731	-2760	-1731	-2106	-1731	-1731
			65	3697	-7160	-1731	-2759	-1731	-2105	-1731	-1731
			130	3697	-7160	-1731	-2754	-1731	-2104	-1731	-1731
742	Copertura	35-167	0	7082	-3623	2755	1729	2103	1729	1729	1729
			65	7082	-3623	2753	1729	2102	1729	1729	1729
			130	7082	-3623	2749	1729	2102	1729	1729	1729
743	Copertura	36-164	0	3750	-7212	-1731	-2757	-1731	-2105	-1731	-1731
			65	3750	-7212	-1731	-2755	-1731	-2104	-1731	-1731
			130	3750	-7212	-1731	-2750	-1731	-2104	-1731	-1731
744	Copertura	37-1	0	7132	-3675	2746	1728	2100	1728	1728	1728

	a	71									
			65	7132	-3675	2745	1728	2100	1728	1728	1728
			130	7132	-3675	2740	1728	2100	1728	1728	1728
745	Copertura	38-168	0	3740	-7200	-1730	-2751	-1730	-2102	-1730	-1730
			65	3740	-7200	-1730	-2750	-1730	-2102	-1730	-1730
			130	3740	-7200	-1730	-2745	-1730	-2102	-1730	-1730
746	Copertura	39-174	0	7026	-3570	2741	1728	2100	1728	1728	1728
			65	7026	-3570	2739	1728	2100	1728	1728	1728
			130	7026	-3570	2735	1728	2100	1728	1728	1728
747	Copertura	40-172	0	3579	-7031	-1726	-2744	-1726	-2097	-1726	-1726
			65	3579	-7031	-1726	-2742	-1726	-2097	-1726	-1726
			130	3579	-7031	-1726	-2737	-1726	-2097	-1726	-1726
748	Copertura	41-179	0	6883	-3419	2745	1732	2104	1732	1732	1732
			65	6883	-3419	2743	1732	2104	1732	1732	1732
			130	6883	-3419	2739	1732	2104	1732	1732	1732
749	Copertura	42-176	0	3406	-6855	-1725	-2738	-1725	-2096	-1725	-1725
			65	3406	-6855	-1725	-2737	-1725	-2096	-1725	-1725
			130	3406	-6855	-1725	-2734	-1725	-2096	-1725	-1725
750	Copertura	43-180	0	3047	-6523	-1738	-2756	-1738	-2112	-1738	-1738
			65	3047	-6523	-1738	-2755	-1738	-2112	-1738	-1738
			130	3047	-6523	-1738	-2752	-1738	-2112	-1738	-1738
751	Copertura	44-183	0	6731	-3246	2763	1743	2117	1743	1743	1743
			65	6731	-3246	2761	1743	2117	1743	1743	1743
			130	6731	-3246	2756	1743	2117	1743	1743	1743
752	Copertura	45-184	0	2890	-6367	-1738	-2753	-1738	-2113	-1738	-1738
			65	2890	-6367	-1738	-2752	-1738	-2113	-1738	-1738
			130	2890	-6367	-1738	-2747	-1738	-2113	-1738	-1738
753	Copertura	46-187	0	6430	-2949	2748	1740	2115	1740	1740	1740
			65	6430	-2949	2746	1740	2115	1740	1740	1740
			130	6430	-2949	2741	1740	2115	1740	1740	1740
754	Copertura	47-188	0	2371	-5851	-1740	-2742	-1740	-2115	-1740	-1740
			65	2371	-5851	-1740	-2740	-1740	-2115	-1740	-1740
			130	2371	-5851	-1740	-2735	-1740	-2115	-1740	-1740
755	Copertura	48-191	0	5904	-2430	2731	1737	2111	1737	1737	1737
			65	5904	-2430	2730	1737	2111	1737	1737	1737
			130	5904	-2430	2725	1737	2111	1737	1737	1737
756	Copertura	49-192	0	1671	-5148	-1738	-2717	-1738	-2113	-1738	-1738
			65	1671	-5148	-1738	-2716	-1738	-2113	-1738	-1738
			130	1671	-5148	-1738	-2711	-1738	-2113	-1738	-1738
757	Copertura	50-194	0	5098	-1628	2708	1735	2108	1735	1735	1735
			65	5098	-1628	2706	1735	2108	1735	1735	1735
			130	5098	-1628	2701	1735	2108	1735	1735	1735
758	Copertura	51-196	0	1212	-4676	-1732	-2674	-1732	-2105	-1732	-1732
			65	1212	-4676	-1732	-2672	-1732	-2105	-1732	-1732
			130	1212	-4676	-1732	-2667	-1732	-2105	-1732	-1732
759	Copertura	52-198	0	4408	-960	2659	1724	2095	1724	1724	1724
			65	4408	-960	2658	1724	2095	1724	1724	1724
			130	4408	-960	2653	1724	2095	1724	1724	1724
760	Copertura	53-200	0	913	-4359	-1723	-2613	-1723	-2093	-1723	-1723
			65	913	-4359	-1723	-2611	-1723	-2093	-1723	-1723
			130	913	-4359	-1723	-2606	-1723	-2093	-1723	-1723
761	Copertura	54-203	0	4005	-562	2607	1721	2091	1721	1721	1721
			65	4005	-562	2606	1721	2091	1721	1721	1721
			130	4005	-562	2601	1721	2091	1721	1721	1721
762	Copertura	55-204	0	-25	-3727	-1832	-2712	-1832	-2208	-1832	-1832

			65	-25	-3727	-1832	-2710	-1832	-2208	-1832	-1832
			130	-25	-3727	-1832	-2705	-1832	-2208	-1832	-1832
763	Copertura	56-207	0	3593	289	2718	1836	2213	1836	1836	1836
			65	3593	289	2716	1836	2213	1836	1836	1836
			130	3593	289	2711	1836	2213	1836	1836	1836
764	Copertura	70-123	0	418	-369	40	2	29	22	25	25
			95	418	-369	40	11	29	23	25	25
			190	418	-369	41	13	29	24	25	25
765	Copertura	81-80	0	433	-1821	-694	-1050	-694	-836	-694	-694
			80	433	-1821	-694	-1014	-694	-836	-694	-694
			160	433	-1821	-694	-1025	-694	-836	-694	-694
766	Copertura	126-81	0	377	-1931	-777	-1190	-777	-936	-777	-777
			30	377	-1931	-777	-1176	-777	-936	-777	-777
			60	377	-1931	-777	-1163	-777	-936	-777	-777
767	Copertura	98-82	0	1097	-2103	-503	-770	-503	-615	-503	-503
			82	1097	-2103	-503	-756	-503	-615	-503	-503
			165	1097	-2103	-503	-774	-503	-615	-503	-503
768	Copertura	99-83	0	1061	-2063	-501	-757	-501	-611	-501	-501
			82	1061	-2063	-501	-774	-501	-611	-501	-501
			165	1061	-2063	-501	-792	-501	-611	-501	-501
769	Copertura	100-84	0	1062	-2097	-517	-798	-517	-631	-517	-517
			82	1062	-2097	-517	-816	-517	-631	-517	-517
			165	1062	-2097	-517	-833	-517	-633	-517	-517
770	Copertura	101-85	0	1263	-2310	-523	-818	-523	-638	-523	-523
			82	1263	-2310	-523	-835	-523	-638	-523	-523
			165	1263	-2310	-523	-852	-523	-643	-523	-523
771	Copertura	102-86	0	1531	-2576	-523	-823	-523	-637	-523	-523
			82	1531	-2576	-523	-840	-523	-639	-523	-523
			165	1531	-2576	-523	-859	-523	-645	-523	-523
772	Copertura	103-87	0	1764	-2809	-522	-826	-522	-637	-522	-522
			82	1764	-2809	-522	-844	-522	-640	-522	-522
			165	1764	-2809	-522	-865	-522	-646	-522	-522
773	Copertura	104-88	0	2017	-3059	-521	-825	-521	-636	-521	-521
			82	2017	-3059	-521	-843	-521	-639	-521	-521
			165	2017	-3059	-521	-865	-521	-645	-521	-521
774	Copertura	105-89	0	2145	-3187	-521	-824	-521	-635	-521	-521
			82	2145	-3187	-521	-842	-521	-638	-521	-521
			165	2145	-3187	-521	-863	-521	-644	-521	-521
775	Copertura	111-90	0	2099	-3140	-521	-823	-521	-635	-521	-521
			80	2099	-3140	-521	-840	-521	-638	-521	-521
			160	2099	-3140	-521	-860	-521	-643	-521	-521
776	Copertura	112-91	0	2106	-3148	-521	-820	-521	-635	-521	-521
			82	2106	-3148	-521	-837	-521	-637	-521	-521
			165	2106	-3148	-521	-856	-521	-642	-521	-521
777	Copertura	113-92	0	2086	-3127	-520	-816	-520	-635	-520	-520
			82	2086	-3127	-520	-834	-520	-635	-520	-520
			165	2086	-3127	-520	-851	-520	-641	-520	-520
778	Copertura	114-93	0	2112	-3154	-521	-814	-521	-635	-521	-521
			82	2112	-3154	-521	-831	-521	-635	-521	-521
			165	2112	-3154	-521	-849	-521	-640	-521	-521
779	Copertura	115-94	0	2090	-3133	-521	-814	-521	-636	-521	-521
			82	2090	-3133	-521	-832	-521	-636	-521	-521
			165	2090	-3133	-521	-849	-521	-641	-521	-521
780	Copertura	116-95	0	1878	-2919	-521	-814	-521	-635	-521	-521
			82	1878	-2919	-521	-831	-521	-635	-521	-521

			165	1878	-2919	-521	-848	-521	-640	-521	-521
781	Copertura	117-96	0	1879	-2922	-521	-810	-521	-636	-521	-521
			82	1879	-2922	-521	-828	-521	-636	-521	-521
			165	1879	-2922	-521	-845	-521	-640	-521	-521
782	Copertura	118-97	0	1673	-2714	-521	-805	-521	-635	-521	-521
			82	1673	-2714	-521	-822	-521	-635	-521	-521
			165	1673	-2714	-521	-839	-521	-637	-521	-521
783	Copertura	131-98	0	1085	-2096	-505	-800	-505	-617	-505	-505
			30	1085	-2096	-505	-788	-505	-617	-505	-505
			60	1085	-2096	-505	-775	-505	-617	-505	-505
784	Copertura	133-99	0	1070	-2067	-499	-766	-499	-609	-499	-499
			30	1070	-2067	-499	-753	-499	-609	-499	-499
			60	1070	-2067	-499	-756	-499	-609	-499	-499
785	Copertura	139-100	0	1042	-2076	-517	-785	-517	-631	-517	-517
			30	1042	-2076	-517	-791	-517	-631	-517	-517
			60	1042	-2076	-517	-797	-517	-631	-517	-517
786	Copertura	143-101	0	1263	-2309	-523	-806	-523	-638	-523	-523
			30	1263	-2309	-523	-812	-523	-638	-523	-523
			60	1263	-2309	-523	-819	-523	-638	-523	-523
787	Copertura	147-102	0	1501	-2546	-523	-810	-523	-637	-523	-523
			30	1501	-2546	-523	-817	-523	-637	-523	-523
			60	1501	-2546	-523	-823	-523	-637	-523	-523
788	Copertura	151-103	0	1748	-2793	-522	-814	-522	-637	-522	-522
			30	1748	-2793	-522	-820	-522	-637	-522	-522
			60	1748	-2793	-522	-827	-522	-637	-522	-522
789	Copertura	155-104	0	1994	-3037	-521	-813	-521	-636	-521	-521
			30	1994	-3037	-521	-820	-521	-636	-521	-521
			60	1994	-3037	-521	-826	-521	-636	-521	-521
790	Copertura	159-105	0	2120	-3162	-521	-811	-521	-635	-521	-521
			30	2120	-3162	-521	-818	-521	-635	-521	-521
			60	2120	-3162	-521	-824	-521	-635	-521	-521
791	Copertura	119-106	0	1135	-2167	-516	-789	-516	-630	-516	-516
			82	1135	-2167	-516	-807	-516	-630	-516	-516
			165	1135	-2167	-516	-824	-516	-630	-516	-516
792	Copertura	120-107	0	898	-1894	-498	-750	-498	-608	-498	-498
			82	898	-1894	-498	-767	-498	-608	-498	-498
			165	898	-1894	-498	-785	-498	-608	-498	-498
793	Copertura	121-108	0	874	-1884	-505	-776	-505	-617	-505	-505
			82	874	-1884	-505	-755	-505	-617	-505	-505
			165	874	-1884	-505	-773	-505	-617	-505	-505
794	Copertura	122-109	0	316	-1785	-734	-1103	-734	-885	-734	-734
			82	316	-1785	-734	-1070	-734	-885	-734	-734
			165	316	-1785	-734	-1086	-734	-885	-734	-734
795	Copertura	123-110	0	431	-382	41	13	29	24	25	25
			82	431	-382	72	-3	35	20	25	25
			165	431	-382	105	-20	42	17	25	25
796	Copertura	163-111	0	2075	-3117	-521	-810	-521	-635	-521	-521
			33	2075	-3117	-521	-817	-521	-635	-521	-521
			65	2075	-3117	-521	-824	-521	-635	-521	-521
797	Copertura	167-112	0	2066	-3106	-520	-806	-520	-635	-520	-520
			30	2066	-3106	-520	-813	-520	-635	-520	-520
			60	2066	-3106	-520	-819	-520	-635	-520	-520
798	Copertura	171-113	0	2061	-3103	-521	-804	-521	-635	-521	-521
			30	2061	-3103	-521	-811	-521	-635	-521	-521
			60	2061	-3103	-521	-817	-521	-635	-521	-521

799	Copertura	174-114	0	2072	-3113	-520	-800	-520	-635	-520	-520
			30	2072	-3113	-520	-807	-520	-635	-520	-520
			60	2072	-3113	-520	-813	-520	-635	-520	-520
800	Copertura	179-115	0	2073	-3116	-522	-802	-522	-636	-522	-522
			30	2073	-3116	-522	-808	-522	-636	-522	-522
			60	2073	-3116	-522	-815	-522	-636	-522	-522
801	Copertura	183-116	0	1863	-2904	-520	-801	-520	-635	-520	-520
			30	1863	-2904	-520	-807	-520	-635	-520	-520
			60	1863	-2904	-520	-813	-520	-635	-520	-520
802	Copertura	187-117	0	1882	-2925	-522	-798	-522	-636	-522	-522
			30	1882	-2925	-522	-804	-522	-636	-522	-522
			60	1882	-2925	-522	-811	-522	-636	-522	-522
803	Copertura	191-118	0	1639	-2681	-521	-792	-521	-635	-521	-521
			30	1639	-2681	-521	-798	-521	-635	-521	-521
			60	1639	-2681	-521	-804	-521	-635	-521	-521
804	Copertura	194-119	0	1135	-2165	-515	-776	-515	-628	-515	-515
			30	1135	-2165	-515	-783	-515	-628	-515	-515
			60	1135	-2165	-515	-789	-515	-628	-515	-515
805	Copertura	198-120	0	874	-1873	-499	-771	-499	-609	-499	-499
			30	874	-1873	-499	-759	-499	-609	-499	-499
			60	874	-1873	-499	-750	-499	-609	-499	-499
806	Copertura	203-121	0	884	-1892	-504	-797	-504	-616	-504	-504
			30	884	-1892	-504	-784	-504	-616	-504	-504
			60	884	-1892	-504	-771	-504	-616	-504	-504
807	Copertura	207-122	0	284	-1756	-736	-1135	-736	-886	-736	-736
			30	284	-1756	-736	-1121	-736	-886	-736	-736
			60	284	-1756	-736	-1108	-736	-886	-736	-736

1.2.8 Involuppi Piastre

- Piastra : numerazione interna della Piastra intesa come insieme di elementi bidimensionali;
- Sollecitazioni : N1-1 : valore dello Sforzo Normale sulla faccia di normale parallela all'asse 1 in direzione 1 nel punto considerato;
- : N2-2 : valore dello Sforzo Normale sulla faccia di normale parallela all'asse 2 in direzione 2 nel punto considerato;
- : N1-2 : valore dello Sforzo Normale sulla faccia di normale parallela all'asse 1 in direzione 2 nel punto considerato;
- : M1-1 : valore dello Momento Flettente sulla faccia di normale parallela all'asse 1 nel punto considerato;
- : M2-2 : valore dello Momento Flettente sulla faccia di normale parallela all'asse 2 nel punto considerato;
- : M1-2 : valore dello Momento Torcente sulle faccie nel punto considerato;
- : T1-3 : valore del Taglio sulla faccia di normale parallela all'asse 1 in direzione 3 nel punto considerato;
- : T2-3 : valore del Taglio sulla faccia di normale parallela all'asse 2 in direzione 3 nel punto considerato;

1.2.8.1 Involuppi SLV.

Tabella 33.I

MASSIMI										
Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	30.69	37.78	22.66	5694.60	1993.33	1113.37	95.47	51.71
2	Fondazione	43, 45, 47, 49, 51, 53,	32.96	27.39	17.76	6091.17	3019.11	1581.64	114.38	82.21

		55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44								
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	23.04	19.30	19.91	3496.21	3086.60	2824.31	76.12	94.91

Tabella 33.II

MINIMI										
Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	-18.40	-34.90	-20.56	-8686.63	-2072.98	-1369.31	-101.67	-60.70
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	-24.46	-22.54	-19.44	-9122.32	-3795.38	-2352.24	-107.50	-94.78
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	-22.71	-16.09	-18.40	-6362.79	-3511.58	-2454.41	-81.12	-81.53

1.2.8.2 Involuppi SLD.

Tabella 34.I

MASSIMI										
Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	15.02	14.14	8.26	1090.78	808.93	426.05	38.04	18.90
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	16.17	11.16	5.94	1232.71	860.28	697.67	47.29	29.37

3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	11.95	9.18	7.60	344.60	829.28	1095.55	27.09	37.79
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Tabella 34.II

MINIMI										
Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/c m]	M2-2 [daNcm/c m]	M1-2 [daNcm/c m]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	-3.13	-11.78	-7.19	-4157.79	-1023.07	-585.74	-40.20	-23.72
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	-9.51	-6.30	-7.33	-4263.87	-1436.58	-1048.05	-41.04	-33.28
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	-9.18	-5.76	-6.19	-3210.13	-1391.61	-735.05	-32.03	-31.69

1.2.8.3 Involuppi SLO.

Tabella 35.I

MASSIMI										
Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/c m]	M2-2 [daNcm/c m]	M1-2 [daNcm/c m]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	16.47	15.04	8.70	1554.92	849.95	481.37	43.58	19.68
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	17.71	11.79	6.30	1720.33	924.37	745.06	53.87	30.45
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	12.98	9.55	7.97	664.63	888.42	1150.19	30.90	39.29

Tabella 35.II

MINIMI										
Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	-4.54	-12.55	-7.60	-4616.69	-1086.42	-659.68	-46.09	-24.96
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	-10.11	-6.94	-7.72	-4751.49	-1500.66	-1084.63	-47.06	-34.85
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	-9.76	-6.15	-6.57	-3531.20	-1450.76	-789.69	-36.22	-32.89

1.2.8.4 Involuppi SLE

Tabella 36.I

MASSIMI - Combinazione Caratteristica										
Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	9.74	2.86	1.62	101.62	278.63	267.90	19.76	11.07
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	10.75	5.34	2.77	167.10	982.91	562.87	28.46	13.81
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	9.57	5.23	2.46	398.27	1075.07	587.83	19.42	16.80

Tabella 36.II

MASSIMI - Combinazione Frequente										
Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36,	6.70	2.19	0.93	73.11	196.71	219.44	13.72	9.04

		38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26								
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	7.20	4.28	1.96	72.40	171.26	452.62	20.75	11.44
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	6.88	4.26	1.82	91.41	180.77	469.75	14.08	10.21

Tabella 36.III

MASSIMI - Combinazione Quasi Permanente										
Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/c m]	M2-2 [daNcm/c m]	M1-2 [daNcm/c m]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	6.14	2.11	0.79	68.13	182.07	212.21	12.60	8.70
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	6.54	4.11	1.86	68.69	56.93	434.34	19.37	11.09
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	6.42	4.09	1.71	57.29	54.82	450.94	13.15	8.88

Tabella 36.IV

MINIMI - Combinazione Caratteristica										
Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/c m]	M2-2 [daNcm/c m]	M1-2 [daNcm/c m]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	0.54	-2.13	-1.68	-2620.00	-704.03	-344.77	-16.62	-11.04
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52,	-3.99	-4.71	-2.54	-2637.66	-720.62	-592.09	-20.33	-15.79

		50, 48, 46, 44								
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	-3.85	-4.59	-1.78	-2345.00	-610.90	-596.04	-16.45	-12.95

Tabella 36.V

MINIMI - Combinazione Frequente										
Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	1.71	-0.78	-1.23	-1786.32	-553.65	-253.50	-11.87	-9.03
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	-2.46	-1.57	-1.91	-1769.71	-549.09	-477.12	-13.76	-10.06
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	-2.35	-1.74	-1.38	-1586.95	-428.29	-478.15	-11.79	-9.17

Tabella 36.VI

MINIMI - Combinazione Quasi Permanente										
Piastra	Impalcato	Fili	N1-1 [daN/cm]	N2-2 [daN/cm]	N1-2 [daN/cm]	M1-1 [daNcm/cm]	M2-2 [daNcm/cm]	M1-2 [daNcm/cm]	T1-3 [daN/cm]	T2-3 [daN/cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	2.07	-0.51	-1.16	-1628.65	-528.59	-237.50	-10.99	-8.74
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	-2.13	-0.97	-1.80	-1603.76	-519.39	-458.04	-12.51	-8.93
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	-2.02	-1.11	-1.32	-1462.96	-409.09	-459.11	-11.01	-8.79

1.3 Tensioni sul Terreno.

I dati seguenti riportano i valori delle tensioni esercitate dalla fondazione sul terreno.

Asta/Piastra : numerazione interna dell'asta/piastra.

X : distanza dal nodo iniziale misurata lungo l'asse dell'asta/piastra.

Comb : combinazione di appartenenza del valore considerato nell'involuppo.

Tensioni (σ_T) : valore della tensione dovuta alla pressione dell'asta/piastra di fondazione:

Tabella 37.I

Tensioni Terreno									
				SLV	SLD	SLO	SLE		
				AI	AI		Caratt.	Freq.	Q. Perm.
Asta	Imp.	Fili	X [cm]	σ_T [daN/cm ²]	σ_T [daN/cm ²]	σ_T [daN/cm ²]	σ_T [daN/cm ²]	σ_T [daN/cm ²]	σ_T [daN/cm ²]
1	Fondazione	1-2	0.00	0.66(42)	0.42(26)	0.36(26)	0.28(17)	0.25(8)	0.22(1)
			41.56	0.57(42)	0.37(26)	0.32(26)	0.26(17)	0.23(8)	0.20(1)
			83.12	0.49(42)	0.32(26)	0.28(26)	0.24(17)	0.22(8)	0.19(1)
2	Fondazione	1-2	0.00	0.49(50)	0.32(34)	0.28(34)	0.24(17)	0.22(8)	0.19(1)
			41.56	0.42(50)	0.29(34)	0.26(34)	0.23(17)	0.21(8)	0.18(1)
			83.12	0.37(50)	0.26(34)	0.23(34)	0.22(17)	0.20(8)	0.17(1)
3	Fondazione	1-15	0.00	0.66(51)	0.42(37)	0.36(37)	0.28(9)	0.25(6)	0.22(1)
			39.75	0.59(51)	0.38(37)	0.34(37)	0.28(9)	0.25(6)	0.22(1)
			79.50	0.51(51)	0.35(37)	0.31(37)	0.28(9)	0.25(6)	0.22(1)
4	Fondazione	1-15	0.00	0.51(51)	0.35(37)	0.31(21)	0.28(9)	0.25(9)	0.22(1)
			39.75	0.46(51)	0.32(37)	0.30(21)	0.29(9)	0.26(9)	0.22(1)
			79.50	0.42(51)	0.30(37)	0.29(21)	0.30(9)	0.26(9)	0.22(1)
5	Fondazione	2-3	0.00	0.37(42)	0.26(26)	0.23(26)	0.22(17)	0.20(8)	0.17(1)
			34.50	0.34(42)	0.24(26)	0.22(26)	0.21(17)	0.19(8)	0.16(1)
			69.00	0.31(42)	0.22(26)	0.21(26)	0.21(17)	0.19(8)	0.16(1)
6	Fondazione	2-3	0.00	0.31(1)	0.22(26)	0.21(1)	0.21(17)	0.19(8)	0.16(1)
			34.50	0.28(1)	0.21(26)	0.20(1)	0.21(17)	0.18(8)	0.16(1)
			69.00	0.28(1)	0.20(26)	0.20(1)	0.20(17)	0.18(8)	0.16(1)
7	Fondazione	3-4	0.00	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.15(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.15(1)
8	Fondazione	3-4	0.00	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.15(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.15(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.15(1)
9	Fondazione	4-5	0.00	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.15(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.15(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.18(8)	0.15(1)
10	Fondazione	4-5	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.18(8)	0.15(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.18(8)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.18(8)	0.16(1)
11	Fondazione	5-6	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.18(8)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
12	Fondazione	5-6	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
13	Fondazione	6-7	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
14	Fondazione	6-7	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
15	Fondazione	7-8	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
16	Fondazione	7-8	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
17	Fondazione	8-9	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
18	Fondazione	8-9	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
19	Fondazione	9-10	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)

			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
20	Fondazione	9-10	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
21	Fondazione	10-11	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.18(8)	0.16(1)
22	Fondazione	10-11	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.18(8)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.18(8)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.15(1)
23	Fondazione	11-12	0.00	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.15(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.15(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.15(1)
24	Fondazione	11-12	0.00	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.15(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.15(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.16(1)
25	Fondazione	12-13	0.00	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(8)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.18(8)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
26	Fondazione	12-13	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(17)	0.19(8)	0.16(1)
			34.50	0.29(1)	0.21(1)	0.21(1)	0.21(17)	0.19(8)	0.16(1)
			69.00	0.30(1)	0.21(1)	0.21(1)	0.22(17)	0.20(8)	0.17(1)
27	Fondazione	13-14	0.00	0.30(1)	0.21(18)	0.21(1)	0.22(17)	0.20(8)	0.17(1)
			41.56	0.31(1)	0.22(18)	0.22(1)	0.23(17)	0.21(8)	0.18(1)
			83.12	0.33(1)	0.24(18)	0.23(1)	0.24(17)	0.22(8)	0.19(1)
28	Fondazione	13-14	0.00	0.33(1)	0.24(18)	0.23(18)	0.24(17)	0.22(8)	0.19(1)
			41.56	0.35(1)	0.26(18)	0.26(18)	0.26(17)	0.23(8)	0.20(1)
			83.12	0.37(1)	0.29(18)	0.29(18)	0.28(17)	0.25(8)	0.22(1)
29	Fondazione	14-16	0.00	0.37(1)	0.29(18)	0.29(18)	0.28(5)	0.25(5)	0.22(1)
			39.75	0.38(1)	0.29(18)	0.28(18)	0.28(5)	0.25(5)	0.22(1)
			79.50	0.38(1)	0.29(18)	0.29(18)	0.29(5)	0.25(5)	0.22(1)
30	Fondazione	14-16	0.00	0.38(1)	0.29(18)	0.29(18)	0.29(5)	0.25(9)	0.22(1)
			39.75	0.39(1)	0.29(18)	0.29(18)	0.29(5)	0.26(9)	0.22(1)
			79.50	0.40(1)	0.30(18)	0.29(18)	0.30(5)	0.26(9)	0.22(1)
31	Fondazione	15-17	0.00	0.42(1)	0.30(21)	0.29(21)	0.30(9)	0.26(9)	0.22(1)
			33.00	0.41(1)	0.30(21)	0.29(21)	0.30(9)	0.27(9)	0.23(1)
			66.00	0.41(1)	0.30(21)	0.30(21)	0.31(9)	0.27(9)	0.23(1)
32	Fondazione	15-17	0.00	0.41(1)	0.30(21)	0.30(21)	0.31(9)	0.27(9)	0.23(1)
			33.00	0.42(1)	0.31(21)	0.30(21)	0.31(9)	0.28(9)	0.23(1)
			66.00	0.42(1)	0.31(21)	0.31(21)	0.32(9)	0.28(9)	0.24(1)
33	Fondazione	16-18	0.00	0.40(1)	0.30(10)	0.29(18)	0.30(5)	0.26(9)	0.22(1)
			33.00	0.40(1)	0.30(10)	0.30(18)	0.30(5)	0.27(9)	0.23(1)
			66.00	0.41(1)	0.31(10)	0.30(18)	0.31(5)	0.27(9)	0.23(1)
34	Fondazione	16-18	0.00	0.41(1)	0.31(10)	0.30(10)	0.31(5)	0.27(9)	0.23(1)
			33.00	0.42(1)	0.32(10)	0.31(10)	0.31(5)	0.28(9)	0.24(1)
			66.00	0.42(1)	0.32(10)	0.32(10)	0.32(5)	0.28(9)	0.24(1)
35	Fondazione	17-19	0.00	0.42(1)	0.31(17)	0.31(17)	0.32(9)	0.28(9)	0.24(1)
			33.00	0.43(1)	0.32(17)	0.31(17)	0.32(9)	0.28(9)	0.24(1)
			66.00	0.43(1)	0.32(17)	0.31(17)	0.33(9)	0.29(9)	0.24(1)
36	Fondazione	17-19	0.00	0.43(1)	0.32(17)	0.31(17)	0.33(9)	0.29(9)	0.24(1)
			33.00	0.44(1)	0.33(17)	0.32(17)	0.33(9)	0.29(9)	0.25(1)
			66.00	0.44(1)	0.33(17)	0.32(17)	0.34(9)	0.29(9)	0.25(1)
37	Fondazione	18-20	0.00	0.42(1)	0.32(10)	0.32(10)	0.32(5)	0.28(9)	0.24(1)
			33.00	0.43(1)	0.33(10)	0.32(10)	0.32(5)	0.28(9)	0.24(1)
			66.00	0.43(1)	0.33(10)	0.32(10)	0.33(5)	0.29(9)	0.24(1)
38	Fondazione	18-20	0.00	0.43(1)	0.33(10)	0.32(10)	0.33(5)	0.29(9)	0.24(1)
			33.00	0.44(1)	0.34(10)	0.33(10)	0.33(5)	0.29(9)	0.25(1)
			66.00	0.44(1)	0.34(10)	0.33(10)	0.34(5)	0.29(9)	0.25(1)
39	Fondazione	19-21	0.00	0.44(1)	0.33(17)	0.32(17)	0.34(9)	0.29(9)	0.25(1)
			33.00	0.45(1)	0.34(17)	0.33(17)	0.34(9)	0.29(9)	0.25(1)
			66.00	0.45(1)	0.34(17)	0.33(17)	0.34(9)	0.29(9)	0.25(1)
40	Fondazione	19-21	0.00	0.45(1)	0.34(17)	0.33(17)	0.34(9)	0.29(9)	0.25(1)
			33.00	0.45(1)	0.34(17)	0.33(17)	0.34(9)	0.30(9)	0.25(1)
			66.00	0.45(1)	0.34(17)	0.33(17)	0.34(9)	0.30(9)	0.25(1)
41	Fondazione	20-22	0.00	0.44(1)	0.34(10)	0.33(10)	0.34(5)	0.29(9)	0.25(1)
			33.00	0.45(1)	0.35(10)	0.34(10)	0.34(5)	0.29(9)	0.25(1)
			66.00	0.45(1)	0.35(10)	0.34(10)	0.34(5)	0.30(9)	0.25(1)
42	Fondazione	20-22	0.00	0.45(10)	0.35(10)	0.34(10)	0.34(5)	0.30(9)	0.25(1)
			33.00	0.45(10)	0.35(10)	0.34(10)	0.34(5)	0.30(9)	0.25(1)
			66.00	0.45(10)	0.35(10)	0.34(10)	0.34(5)	0.30(9)	0.25(1)
43	Fondazione	21-23	0.00	0.45(48)	0.34(17)	0.33(17)	0.34(9)	0.30(9)	0.25(1)

			33.00	0.45(48)	0.34(17)	0.33(17)	0.34(9)	0.30(9)	0.25(1)
			66.00	0.45(48)	0.35(17)	0.33(17)	0.34(9)	0.29(9)	0.25(1)
44	Fondazione	21-23	0.00	0.45(48)	0.35(17)	0.33(17)	0.34(9)	0.29(9)	0.25(1)
			33.00	0.46(48)	0.35(17)	0.33(17)	0.34(9)	0.29(9)	0.25(1)
			66.00	0.46(48)	0.35(17)	0.33(17)	0.34(9)	0.29(9)	0.25(1)
45	Fondazione	22-24	0.00	0.45(10)	0.35(10)	0.34(10)	0.34(5)	0.30(9)	0.25(1)
			33.00	0.46(10)	0.35(10)	0.34(10)	0.34(5)	0.30(9)	0.25(1)
			66.00	0.46(10)	0.36(10)	0.34(10)	0.34(5)	0.30(9)	0.25(1)
46	Fondazione	22-24	0.00	0.46(10)	0.36(10)	0.34(10)	0.34(5)	0.30(9)	0.25(1)
			33.00	0.46(10)	0.36(10)	0.34(10)	0.34(5)	0.30(9)	0.25(1)
			66.00	0.47(10)	0.36(10)	0.35(10)	0.34(5)	0.30(9)	0.25(1)
47	Fondazione	23-25	0.00	0.46(17)	0.35(17)	0.33(17)	0.34(9)	0.29(9)	0.25(1)
			33.00	0.45(17)	0.35(17)	0.33(17)	0.33(9)	0.29(9)	0.25(1)
			66.00	0.45(17)	0.35(17)	0.33(17)	0.33(9)	0.29(9)	0.24(1)
48	Fondazione	23-25	0.00	0.45(17)	0.35(17)	0.33(17)	0.33(9)	0.29(9)	0.24(1)
			33.00	0.45(17)	0.35(17)	0.33(17)	0.33(9)	0.28(9)	0.24(1)
			66.00	0.45(17)	0.35(17)	0.33(17)	0.32(9)	0.28(9)	0.24(1)
49	Fondazione	24-26	0.00	0.47(10)	0.36(10)	0.35(10)	0.34(5)	0.30(9)	0.25(1)
			33.00	0.47(10)	0.36(10)	0.35(10)	0.34(5)	0.29(9)	0.25(1)
			66.00	0.48(10)	0.36(10)	0.35(10)	0.34(5)	0.29(9)	0.25(1)
50	Fondazione	24-26	0.00	0.48(10)	0.36(10)	0.35(10)	0.34(5)	0.29(9)	0.25(1)
			33.00	0.48(10)	0.36(10)	0.35(10)	0.34(5)	0.29(9)	0.25(1)
			66.00	0.49(10)	0.37(10)	0.35(10)	0.34(5)	0.29(9)	0.25(1)
51	Fondazione	25-26	0.00	0.45(1)	0.35(1)	0.33(1)	0.32(13)	0.28(9)	0.24(1)
			48.68	0.36(1)	0.27(1)	0.26(1)	0.27(13)	0.24(9)	0.20(1)
			97.37	0.31(1)	0.22(1)	0.22(1)	0.23(13)	0.20(9)	0.17(1)
52	Fondazione	25-26	0.00	0.31(1)	0.22(1)	0.22(1)	0.23(5)	0.20(5)	0.17(1)
			48.68	0.27(1)	0.20(1)	0.20(1)	0.20(5)	0.18(5)	0.14(1)
			97.37	0.25(1)	0.18(1)	0.18(1)	0.18(5)	0.16(5)	0.12(1)
53	Fondazione	25-26	0.00	0.25(1)	0.18(1)	0.18(1)	0.18(5)	0.16(5)	0.12(1)
			48.68	0.23(1)	0.16(1)	0.16(1)	0.17(5)	0.15(5)	0.11(1)
			97.37	0.22(1)	0.16(1)	0.16(1)	0.16(5)	0.14(5)	0.11(1)
54	Fondazione	25-26	0.00	0.22(1)	0.16(1)	0.16(1)	0.16(5)	0.14(5)	0.11(1)
			48.68	0.21(1)	0.15(1)	0.15(1)	0.16(5)	0.14(5)	0.10(1)
			97.37	0.21(1)	0.15(1)	0.15(1)	0.16(5)	0.13(5)	0.10(1)
55	Fondazione	25-26	0.00	0.21(1)	0.15(1)	0.15(1)	0.16(5)	0.13(5)	0.10(1)
			48.68	0.22(1)	0.16(1)	0.16(1)	0.16(5)	0.14(5)	0.10(1)
			97.37	0.22(1)	0.16(1)	0.16(1)	0.16(5)	0.14(5)	0.10(1)
56	Fondazione	25-26	0.00	0.22(1)	0.16(1)	0.16(1)	0.16(5)	0.14(5)	0.10(1)
			48.68	0.22(1)	0.16(1)	0.16(1)	0.16(5)	0.14(5)	0.11(1)
			97.37	0.23(1)	0.16(1)	0.16(1)	0.16(5)	0.14(5)	0.11(1)
57	Fondazione	25-26	0.00	0.23(1)	0.16(1)	0.16(1)	0.16(1)	0.14(8)	0.11(1)
			48.68	0.23(1)	0.17(1)	0.17(1)	0.17(1)	0.14(8)	0.11(1)
			97.37	0.23(1)	0.17(1)	0.17(1)	0.17(1)	0.15(8)	0.11(1)
58	Fondazione	25-26	0.00	0.23(1)	0.17(1)	0.17(1)	0.17(17)	0.15(8)	0.11(1)
			48.68	0.23(1)	0.17(1)	0.17(1)	0.17(17)	0.15(8)	0.11(1)
			97.37	0.24(1)	0.17(1)	0.17(1)	0.17(17)	0.15(8)	0.11(1)
59	Fondazione	25-26	0.00	0.24(1)	0.17(1)	0.17(1)	0.17(17)	0.15(9)	0.11(1)
			48.68	0.24(1)	0.17(1)	0.17(1)	0.17(17)	0.15(9)	0.12(1)
			97.37	0.24(1)	0.17(1)	0.17(1)	0.17(17)	0.15(9)	0.12(1)
60	Fondazione	25-26	0.00	0.24(1)	0.17(1)	0.17(1)	0.17(17)	0.15(9)	0.12(1)
			48.68	0.24(1)	0.17(1)	0.17(1)	0.17(17)	0.15(9)	0.12(1)
			97.37	0.24(1)	0.17(1)	0.17(1)	0.17(17)	0.15(9)	0.12(1)
61	Fondazione	25-26	0.00	0.24(1)	0.17(1)	0.17(1)	0.17(5)	0.15(5)	0.12(1)
			48.68	0.24(1)	0.17(1)	0.17(1)	0.17(5)	0.15(5)	0.12(1)
			97.37	0.24(1)	0.17(1)	0.17(1)	0.17(5)	0.15(5)	0.11(1)
62	Fondazione	25-26	0.00	0.24(1)	0.17(1)	0.17(1)	0.17(1)	0.15(8)	0.11(1)
			48.68	0.23(1)	0.17(1)	0.17(1)	0.17(1)	0.15(8)	0.11(1)
			97.37	0.23(1)	0.17(1)	0.17(1)	0.17(1)	0.15(8)	0.11(1)
63	Fondazione	25-26	0.00	0.23(1)	0.17(1)	0.17(1)	0.17(9)	0.15(6)	0.11(1)
			48.68	0.23(1)	0.17(1)	0.17(1)	0.17(9)	0.14(6)	0.11(1)
			97.37	0.23(1)	0.16(1)	0.16(1)	0.16(9)	0.14(6)	0.11(1)
64	Fondazione	25-26	0.00	0.23(1)	0.16(1)	0.16(1)	0.16(9)	0.14(6)	0.11(1)
			48.68	0.22(1)	0.16(1)	0.16(1)	0.16(9)	0.14(6)	0.11(1)
			97.37	0.22(1)	0.16(1)	0.16(1)	0.16(9)	0.14(6)	0.10(1)
65	Fondazione	25-26	0.00	0.22(1)	0.16(1)	0.16(1)	0.16(9)	0.14(6)	0.10(1)
			48.68	0.21(1)	0.15(1)	0.15(1)	0.16(9)	0.13(6)	0.10(1)
			97.37	0.21(1)	0.15(1)	0.15(1)	0.16(9)	0.13(6)	0.10(1)
66	Fondazione	25-26	0.00	0.21(1)	0.15(1)	0.15(1)	0.16(9)	0.13(6)	0.10(1)
			48.68	0.21(1)	0.15(1)	0.15(1)	0.16(9)	0.13(6)	0.10(1)
			97.37	0.22(1)	0.16(1)	0.16(1)	0.16(9)	0.14(6)	0.10(1)
67	Fondazione	25-26	0.00	0.22(1)	0.16(1)	0.16(1)	0.16(9)	0.14(6)	0.10(1)

			48.68	0.23(1)	0.16(1)	0.16(1)	0.17(9)	0.15(6)	0.11(1)
			97.37	0.25(1)	0.18(1)	0.18(1)	0.18(9)	0.16(6)	0.12(1)
68	Fondazione	25-26	0.00	0.25(1)	0.18(1)	0.18(1)	0.18(13)	0.16(9)	0.12(1)
			48.68	0.28(1)	0.20(1)	0.20(1)	0.20(13)	0.18(9)	0.14(1)
			97.37	0.32(1)	0.23(1)	0.23(1)	0.23(13)	0.21(9)	0.17(1)
69	Fondazione	25-26	0.00	0.32(10)	0.23(10)	0.23(10)	0.23(5)	0.21(9)	0.17(1)
			48.68	0.37(10)	0.28(10)	0.27(10)	0.28(5)	0.24(9)	0.21(1)
			97.37	0.49(10)	0.37(10)	0.35(10)	0.34(5)	0.29(9)	0.25(1)
70	Fondazione	25-28	0.00	0.45(17)	0.35(17)	0.33(17)	0.32(9)	0.28(9)	0.24(1)
			42.50	0.46(17)	0.35(17)	0.33(17)	0.32(9)	0.28(9)	0.24(1)
			85.00	0.47(17)	0.35(17)	0.34(17)	0.32(9)	0.28(9)	0.24(1)
71	Fondazione	25-28	0.00	0.47(17)	0.35(17)	0.34(17)	0.32(9)	0.28(9)	0.24(1)
			42.50	0.49(17)	0.37(17)	0.35(17)	0.33(9)	0.28(9)	0.24(1)
			85.00	0.50(17)	0.38(17)	0.35(17)	0.33(9)	0.29(9)	0.24(1)
72	Fondazione	26-27	0.00	0.49(10)	0.37(10)	0.35(10)	0.34(5)	0.29(9)	0.25(1)
			33.00	0.49(10)	0.37(10)	0.35(10)	0.34(5)	0.29(9)	0.25(1)
			66.00	0.50(10)	0.38(10)	0.36(10)	0.34(5)	0.29(9)	0.25(1)
73	Fondazione	26-27	0.00	0.50(10)	0.38(10)	0.36(10)	0.34(5)	0.29(9)	0.25(1)
			33.00	0.51(10)	0.38(10)	0.36(10)	0.34(5)	0.30(9)	0.25(1)
			66.00	0.52(10)	0.39(10)	0.37(10)	0.34(5)	0.30(9)	0.25(1)
74	Fondazione	27-29	0.00	0.52(10)	0.39(10)	0.37(10)	0.34(5)	0.30(9)	0.25(1)
			33.00	0.53(10)	0.39(10)	0.37(10)	0.35(5)	0.30(9)	0.25(1)
			66.00	0.53(10)	0.40(10)	0.37(10)	0.35(5)	0.30(9)	0.26(1)
75	Fondazione	27-29	0.00	0.53(10)	0.40(10)	0.37(10)	0.35(5)	0.30(9)	0.26(1)
			33.00	0.54(10)	0.40(10)	0.38(10)	0.35(5)	0.30(9)	0.26(1)
			66.00	0.55(10)	0.40(10)	0.38(10)	0.35(5)	0.30(9)	0.26(1)
76	Fondazione	28-30	0.00	0.50(17)	0.38(17)	0.35(17)	0.33(9)	0.29(9)	0.24(1)
			36.50	0.51(17)	0.38(17)	0.36(17)	0.33(9)	0.29(9)	0.25(1)
			73.00	0.52(17)	0.38(17)	0.36(17)	0.33(9)	0.29(9)	0.25(1)
77	Fondazione	28-30	0.00	0.52(17)	0.38(17)	0.36(17)	0.33(9)	0.29(9)	0.25(1)
			36.50	0.52(17)	0.39(17)	0.37(17)	0.34(9)	0.29(9)	0.25(1)
			73.00	0.53(17)	0.39(17)	0.37(17)	0.34(9)	0.30(9)	0.25(1)
78	Fondazione	29-31	0.00	0.55(10)	0.40(10)	0.38(10)	0.35(5)	0.30(9)	0.26(1)
			33.00	0.55(10)	0.41(10)	0.38(10)	0.35(5)	0.31(9)	0.26(1)
			66.00	0.55(10)	0.41(10)	0.38(10)	0.35(5)	0.31(9)	0.26(1)
79	Fondazione	29-31	0.00	0.55(10)	0.41(10)	0.38(10)	0.35(5)	0.31(9)	0.26(1)
			33.00	0.56(10)	0.41(10)	0.39(10)	0.35(5)	0.31(9)	0.26(1)
			66.00	0.56(10)	0.41(10)	0.39(10)	0.36(5)	0.31(9)	0.26(1)
80	Fondazione	30-32	0.00	0.53(17)	0.39(17)	0.37(17)	0.34(9)	0.30(9)	0.25(1)
			34.25	0.53(17)	0.39(17)	0.37(17)	0.34(9)	0.30(9)	0.25(1)
			68.50	0.53(17)	0.39(17)	0.37(17)	0.34(9)	0.30(9)	0.25(1)
81	Fondazione	30-32	0.00	0.53(17)	0.39(17)	0.37(17)	0.34(9)	0.30(9)	0.25(1)
			34.25	0.53(17)	0.40(17)	0.37(17)	0.34(9)	0.30(9)	0.25(1)
			68.50	0.53(17)	0.40(17)	0.37(17)	0.35(9)	0.30(9)	0.26(1)
82	Fondazione	31-33	0.00	0.56(10)	0.41(10)	0.39(10)	0.36(5)	0.31(9)	0.26(1)
			33.00	0.56(10)	0.41(10)	0.39(10)	0.36(5)	0.31(9)	0.26(1)
			66.00	0.56(10)	0.41(10)	0.39(10)	0.36(5)	0.31(9)	0.26(1)
83	Fondazione	31-33	0.00	0.56(10)	0.41(10)	0.39(10)	0.36(5)	0.31(9)	0.26(1)
			33.00	0.56(10)	0.41(10)	0.39(10)	0.36(5)	0.31(9)	0.26(1)
			66.00	0.56(10)	0.41(10)	0.39(10)	0.36(5)	0.31(9)	0.26(1)
84	Fondazione	32-34	0.00	0.53(17)	0.40(17)	0.37(17)	0.35(9)	0.30(9)	0.26(1)
			34.50	0.53(17)	0.40(17)	0.37(17)	0.35(9)	0.30(9)	0.26(1)
			69.00	0.53(17)	0.40(17)	0.37(17)	0.35(9)	0.30(9)	0.26(1)
85	Fondazione	32-34	0.00	0.53(17)	0.40(17)	0.37(17)	0.35(9)	0.30(9)	0.26(1)
			34.50	0.53(17)	0.40(17)	0.37(17)	0.35(9)	0.30(9)	0.26(1)
			69.00	0.53(17)	0.40(17)	0.37(17)	0.35(9)	0.30(9)	0.26(1)
86	Fondazione	33-35	0.00	0.56(10)	0.41(10)	0.39(10)	0.36(5)	0.31(9)	0.26(1)
			33.00	0.56(10)	0.41(10)	0.39(10)	0.36(5)	0.31(9)	0.26(1)
			66.00	0.56(10)	0.41(10)	0.39(10)	0.36(5)	0.31(9)	0.26(1)
87	Fondazione	33-35	0.00	0.56(10)	0.41(10)	0.39(10)	0.36(5)	0.31(9)	0.26(1)
			33.00	0.56(10)	0.41(10)	0.39(10)	0.36(5)	0.31(9)	0.26(1)
			66.00	0.56(10)	0.41(10)	0.39(10)	0.36(5)	0.31(9)	0.26(1)
88	Fondazione	34-36	0.00	0.53(17)	0.40(17)	0.37(17)	0.35(9)	0.30(9)	0.26(1)
			34.50	0.53(17)	0.40(17)	0.37(17)	0.35(9)	0.30(9)	0.26(1)
			69.00	0.53(17)	0.40(17)	0.37(17)	0.35(9)	0.30(9)	0.26(1)
89	Fondazione	34-36	0.00	0.53(18)	0.40(18)	0.37(18)	0.35(9)	0.30(9)	0.26(1)
			34.50	0.53(18)	0.40(18)	0.37(18)	0.35(9)	0.30(9)	0.26(1)
			69.00	0.53(18)	0.40(18)	0.37(18)	0.35(9)	0.30(9)	0.26(1)
90	Fondazione	35-37	0.00	0.56(13)	0.41(13)	0.39(13)	0.36(5)	0.31(9)	0.26(1)
			33.00	0.55(13)	0.41(13)	0.38(13)	0.36(5)	0.31(9)	0.26(1)
			66.00	0.55(13)	0.41(13)	0.38(13)	0.35(5)	0.31(9)	0.26(1)
91	Fondazione	35-37	0.00	0.55(13)	0.41(13)	0.38(13)	0.35(5)	0.31(9)	0.26(1)

			33.00	0.55(13)	0.41(13)	0.38(13)	0.35(5)	0.31(9)	0.26(1)
			66.00	0.55(13)	0.41(13)	0.38(13)	0.35(5)	0.31(9)	0.26(1)
92	Fondazione	36-38	0.00	0.53(18)	0.40(18)	0.37(18)	0.35(9)	0.30(9)	0.26(1)
			34.50	0.54(18)	0.40(18)	0.37(18)	0.35(9)	0.30(9)	0.26(1)
			69.00	0.54(18)	0.40(18)	0.38(18)	0.35(9)	0.30(9)	0.26(1)
93	Fondazione	36-38	0.00	0.54(18)	0.40(18)	0.38(18)	0.35(9)	0.30(9)	0.26(1)
			34.50	0.54(18)	0.40(18)	0.38(18)	0.35(9)	0.30(9)	0.26(1)
			69.00	0.54(18)	0.40(18)	0.38(18)	0.35(9)	0.31(9)	0.26(1)
94	Fondazione	37-39	0.00	0.55(13)	0.41(13)	0.38(13)	0.35(5)	0.31(9)	0.26(1)
			33.00	0.55(13)	0.41(13)	0.38(13)	0.35(5)	0.31(9)	0.26(1)
			66.00	0.54(13)	0.40(13)	0.38(13)	0.35(5)	0.31(9)	0.26(1)
95	Fondazione	37-39	0.00	0.54(13)	0.40(13)	0.38(13)	0.35(5)	0.31(9)	0.26(1)
			33.00	0.54(13)	0.40(13)	0.38(13)	0.35(5)	0.30(9)	0.26(1)
			66.00	0.54(13)	0.40(13)	0.38(13)	0.35(5)	0.30(9)	0.26(1)
96	Fondazione	38-40	0.00	0.54(18)	0.40(18)	0.38(18)	0.35(9)	0.31(9)	0.26(1)
			34.25	0.55(18)	0.41(18)	0.38(18)	0.35(9)	0.31(9)	0.26(1)
			68.50	0.55(18)	0.41(18)	0.38(18)	0.35(9)	0.31(9)	0.26(1)
97	Fondazione	38-40	0.00	0.55(18)	0.41(18)	0.38(18)	0.35(9)	0.31(9)	0.26(1)
			34.25	0.55(18)	0.41(18)	0.38(18)	0.35(9)	0.31(9)	0.26(1)
			68.50	0.55(18)	0.41(18)	0.39(18)	0.36(9)	0.31(9)	0.26(1)
98	Fondazione	39-41	0.00	0.54(9)	0.40(9)	0.38(9)	0.35(5)	0.30(9)	0.26(1)
			33.00	0.53(9)	0.40(9)	0.37(9)	0.35(5)	0.30(9)	0.26(1)
			66.00	0.53(9)	0.39(9)	0.37(9)	0.35(5)	0.30(9)	0.25(1)
99	Fondazione	39-41	0.00	0.53(9)	0.39(9)	0.37(9)	0.35(5)	0.30(9)	0.25(1)
			33.00	0.52(9)	0.39(9)	0.37(9)	0.34(5)	0.30(9)	0.25(1)
			66.00	0.52(9)	0.39(9)	0.36(9)	0.34(5)	0.30(9)	0.25(1)
100	Fondazione	40-42	0.00	0.55(18)	0.41(18)	0.39(18)	0.36(9)	0.31(9)	0.26(1)
			34.50	0.56(18)	0.41(18)	0.39(18)	0.36(9)	0.31(9)	0.26(1)
			69.00	0.56(18)	0.41(18)	0.39(18)	0.36(9)	0.31(9)	0.26(1)
101	Fondazione	40-42	0.00	0.56(18)	0.41(18)	0.39(18)	0.36(9)	0.31(9)	0.26(1)
			34.50	0.56(18)	0.42(18)	0.39(18)	0.36(9)	0.31(9)	0.26(1)
			69.00	0.57(18)	0.42(18)	0.39(18)	0.36(9) *	0.31(9)	0.27(1)
102	Fondazione	41-44	0.00	0.52(9)	0.39(9)	0.36(9)	0.34(5)	0.30(9)	0.25(1)
			33.00	0.51(9)	0.38(9)	0.36(9)	0.34(5)	0.29(9)	0.25(1)
			66.00	0.50(9)	0.38(9)	0.36(9)	0.34(5)	0.29(9)	0.25(1)
103	Fondazione	41-44	0.00	0.50(9)	0.38(9)	0.36(9)	0.34(5)	0.29(9)	0.25(1)
			33.00	0.50(9)	0.38(9)	0.36(9)	0.34(5)	0.29(9)	0.25(1)
			66.00	0.50(9)	0.37(9)	0.35(9)	0.34(5)	0.29(9)	0.25(1)
104	Fondazione	42-43	0.00	0.57(18)	0.42(18)	0.39(18)	0.36(9) *	0.31(9)	0.27(1)
			23.00	0.56(18)	0.42(18)	0.39(18)	0.36(9) *	0.31(9)	0.27(1)
			46.00	0.56(18)	0.42(18)	0.39(18)	0.36(9) *	0.31(9)	0.27(1)
105	Fondazione	43-44	0.00	0.56(1)	0.42(1)	0.39(1)	0.36(17) *	0.31(9)	0.27(1)
			48.68	0.41(1)	0.31(1)	0.29(1)	0.29(17)	0.26(9)	0.22(1)
			97.37	0.33(1)	0.24(1)	0.24(1)	0.24(17)	0.21(9)	0.18(1)
106	Fondazione	43-44	0.00	0.33(1)	0.24(1)	0.24(1)	0.24(5)	0.21(5)	0.18(1)
			48.68	0.28(1)	0.20(1)	0.20(1)	0.21(5)	0.18(5)	0.15(1)
			97.37	0.25(1)	0.18(1)	0.18(1)	0.19(5)	0.16(5)	0.13(1)
107	Fondazione	43-44	0.00	0.25(1)	0.18(1)	0.18(1)	0.19(5)	0.16(5)	0.13(1)
			48.68	0.23(1)	0.16(1)	0.16(1)	0.17(5)	0.15(5)	0.11(1)
			97.37	0.22(1)	0.16(1)	0.16(1)	0.16(5)	0.14(5)	0.10(1)
108	Fondazione	43-44	0.00	0.22(1)	0.16(1)	0.16(1)	0.16(5)	0.14(5)	0.10(1)
			48.68	0.21(1)	0.15(1)	0.15(1)	0.16(5)	0.13(5)	0.10(1)
			97.37	0.21(1)	0.15(1)	0.15(1)	0.15(5)	0.13(5)	0.10(1)
109	Fondazione	43-44	0.00	0.21(1)	0.15(1)	0.15(1)	0.15(5)	0.13(5)	0.10(1)
			48.68	0.21(1)	0.15(1)	0.15(1)	0.16(5)	0.13(5)	0.10(1)
			97.37	0.22(1)	0.16(1)	0.16(1)	0.16(5)	0.14(5)	0.10(1)
110	Fondazione	43-44	0.00	0.22(1)	0.16(1)	0.16(1)	0.16(5)	0.14(5)	0.10(1)
			48.68	0.22(1)	0.16(1)	0.16(1)	0.16(5)	0.14(5)	0.11(1)
			97.37	0.23(1)	0.16(1)	0.16(1)	0.16(5)	0.14(5)	0.11(1)
111	Fondazione	43-44	0.00	0.23(1)	0.16(1)	0.16(1)	0.16(1)	0.14(7)	0.11(1)
			48.68	0.23(1)	0.16(1)	0.16(1)	0.16(1)	0.14(7)	0.11(1)
			97.37	0.23(1)	0.17(1)	0.17(1)	0.17(1)	0.15(7)	0.11(1)
112	Fondazione	43-44	0.00	0.23(1)	0.17(1)	0.17(1)	0.17(13)	0.15(7)	0.11(1)
			48.68	0.23(1)	0.17(1)	0.17(1)	0.17(13)	0.15(7)	0.11(1)
			97.37	0.24(1)	0.17(1)	0.17(1)	0.17(13)	0.15(7)	0.11(1)
113	Fondazione	43-44	0.00	0.24(1)	0.17(1)	0.17(1)	0.17(13)	0.15(9)	0.11(1)
			48.68	0.24(1)	0.17(1)	0.17(1)	0.17(13)	0.15(9)	0.12(1)
			97.37	0.24(1)	0.17(1)	0.17(1)	0.17(13)	0.15(9)	0.12(1)
114	Fondazione	43-44	0.00	0.24(1)	0.17(1)	0.17(1)	0.17(13)	0.15(9)	0.12(1)
			48.68	0.24(1)	0.17(1)	0.17(1)	0.17(13)	0.15(9)	0.12(1)
			97.37	0.24(1)	0.17(1)	0.17(1)	0.17(13)	0.15(9)	0.12(1)
115	Fondazione	43-44	0.00	0.24(1)	0.17(1)	0.17(1)	0.17(5)	0.15(5)	0.12(1)

			48.68	0.24(1)	0.17(1)	0.17(1)	0.17(5)	0.15(5)	0.12(1)
			97.37	0.24(1)	0.17(1)	0.17(1)	0.17(5)	0.15(5)	0.11(1)
116	Fondazione	43-44	0.00	0.24(1)	0.17(1)	0.17(1)	0.17(1)	0.15(7)	0.11(1)
			48.68	0.23(1)	0.17(1)	0.17(1)	0.17(1)	0.15(7)	0.11(1)
			97.37	0.23(1)	0.17(1)	0.17(1)	0.17(1)	0.15(7)	0.11(1)
117	Fondazione	43-44	0.00	0.23(1)	0.17(1)	0.17(1)	0.17(9)	0.15(6)	0.11(1)
			48.68	0.23(1)	0.17(1)	0.17(1)	0.17(9)	0.14(6)	0.11(1)
			97.37	0.23(1)	0.16(1)	0.16(1)	0.16(9)	0.14(6)	0.11(1)
118	Fondazione	43-44	0.00	0.23(1)	0.16(1)	0.16(1)	0.16(9)	0.14(6)	0.11(1)
			48.68	0.22(1)	0.16(1)	0.16(1)	0.16(9)	0.14(6)	0.11(1)
			97.37	0.22(1)	0.16(1)	0.16(1)	0.16(9)	0.14(6)	0.10(1)
119	Fondazione	43-44	0.00	0.22(1)	0.16(1)	0.16(1)	0.16(9)	0.14(6)	0.10(1)
			48.68	0.22(1)	0.15(1)	0.15(1)	0.16(9)	0.13(6)	0.10(1)
			97.37	0.21(1)	0.15(1)	0.15(1)	0.16(9)	0.13(6)	0.10(1)
120	Fondazione	43-44	0.00	0.21(1)	0.15(1)	0.15(1)	0.16(9)	0.13(6)	0.10(1)
			48.68	0.21(1)	0.15(1)	0.15(1)	0.16(9)	0.13(6)	0.10(1)
			97.37	0.22(1)	0.16(1)	0.16(1)	0.16(9)	0.14(6)	0.10(1)
121	Fondazione	43-44	0.00	0.22(1)	0.16(1)	0.16(1)	0.16(9)	0.14(6)	0.10(1)
			48.68	0.23(1)	0.16(1)	0.16(1)	0.17(9)	0.15(6)	0.11(1)
			97.37	0.25(1)	0.18(1)	0.18(1)	0.18(9)	0.16(6)	0.12(1)
122	Fondazione	43-44	0.00	0.25(1)	0.18(1)	0.18(1)	0.18(17)	0.16(9)	0.12(1)
			48.68	0.28(1)	0.20(1)	0.20(1)	0.20(17)	0.18(9)	0.14(1)
			97.37	0.32(1)	0.23(1)	0.23(1)	0.23(17)	0.21(9)	0.17(1)
123	Fondazione	43-44	0.00	0.32(9)	0.23(9)	0.23(9)	0.23(5)	0.21(9)	0.17(1)
			48.68	0.37(9)	0.28(9)	0.27(9)	0.28(5)	0.25(9)	0.21(1)
			97.37	0.50(9)	0.37(9)	0.35(9)	0.34(5)	0.29(9)	0.25(1)
124	Fondazione	43-45	0.00	0.56(18)	0.42(18)	0.39(18)	0.36(9) *	0.31(9)	0.27(1)
			33.00	0.55(18)	0.41(18)	0.39(18)	0.36(9)	0.31(9)	0.27(1)
			66.00	0.54(18)	0.41(18)	0.38(18)	0.36(9)	0.31(9)	0.26(1)
125	Fondazione	43-45	0.00	0.54(18)	0.41(18)	0.38(18)	0.36(9)	0.31(9)	0.26(1)
			33.00	0.54(18)	0.40(18)	0.38(18)	0.36(9)	0.31(9)	0.26(1)
			66.00	0.53(18)	0.40(18)	0.38(18)	0.36(9)	0.31(9)	0.26(1)
126	Fondazione	44-46	0.00	0.50(9)	0.37(9)	0.35(9)	0.34(5)	0.29(9)	0.25(1)
			33.00	0.49(9)	0.37(9)	0.35(9)	0.34(5)	0.29(9)	0.25(1)
			66.00	0.49(9)	0.37(9)	0.35(9)	0.34(5)	0.29(9)	0.25(1)
127	Fondazione	44-46	0.00	0.49(9)	0.37(9)	0.35(9)	0.34(5)	0.29(9)	0.25(1)
			33.00	0.49(9)	0.37(9)	0.35(9)	0.34(5)	0.30(9)	0.25(1)
			66.00	0.49(9)	0.37(9)	0.35(9)	0.34(5)	0.30(9)	0.25(1)
128	Fondazione	45-47	0.00	0.53(18)	0.40(18)	0.38(18)	0.36(9)	0.31(9)	0.26(1)
			33.00	0.52(18)	0.39(18)	0.37(18)	0.36(9)	0.31(9)	0.26(1)
			66.00	0.52(18)	0.39(18)	0.37(18)	0.36(9)	0.31(9)	0.26(1)
129	Fondazione	45-47	0.00	0.52(18)	0.39(18)	0.37(18)	0.36(9)	0.31(9)	0.26(1)
			33.00	0.51(18)	0.39(18)	0.37(18)	0.36(9)	0.31(9)	0.26(1)
			66.00	0.51(18)	0.39(18)	0.37(18)	0.36(9)	0.31(9)	0.26(1)
130	Fondazione	46-48	0.00	0.49(39)	0.37(9)	0.35(9)	0.34(5)	0.30(9)	0.25(1)
			33.00	0.48(39)	0.37(9)	0.35(9)	0.35(5)	0.30(9)	0.26(1)
			66.00	0.48(39)	0.37(9)	0.35(9)	0.35(5)	0.30(9)	0.26(1)
131	Fondazione	46-48	0.00	0.48(39)	0.37(9)	0.35(9)	0.35(5)	0.30(9)	0.26(1)
			33.00	0.48(39)	0.37(9)	0.35(9)	0.35(5)	0.30(9)	0.26(1)
			66.00	0.48(39)	0.37(9)	0.35(9)	0.35(5)	0.31(9)	0.26(1)
132	Fondazione	47-49	0.00	0.51(18)	0.39(18)	0.37(18)	0.36(9)	0.31(9)	0.26(1)
			33.00	0.50(18)	0.38(18)	0.36(18)	0.35(9)	0.31(9)	0.26(1)
			66.00	0.49(18)	0.37(18)	0.36(18)	0.35(9)	0.31(9)	0.26(1)
133	Fondazione	47-49	0.00	0.49(18)	0.37(18)	0.36(18)	0.35(9)	0.31(9)	0.26(1)
			33.00	0.48(18)	0.37(18)	0.36(18)	0.35(9)	0.31(9)	0.26(1)
			66.00	0.47(18)	0.37(18)	0.35(18)	0.35(9)	0.31(9)	0.26(1)
134	Fondazione	48-50	0.00	0.48(39)	0.37(9)	0.35(9)	0.35(5)	0.31(9)	0.26(1)
			33.00	0.48(39)	0.37(9)	0.35(9)	0.35(5)	0.31(9)	0.26(1)
			66.00	0.48(39)	0.36(9)	0.35(9)	0.35(5)	0.30(9)	0.26(1)
135	Fondazione	48-50	0.00	0.48(39)	0.36(9)	0.35(9)	0.35(5)	0.30(9)	0.26(1)
			33.00	0.47(39)	0.36(9)	0.35(9)	0.35(5)	0.30(9)	0.26(1)
			66.00	0.47(39)	0.36(9)	0.34(9)	0.35(5)	0.30(9)	0.26(1)
136	Fondazione	49-51	0.00	0.47(51)	0.37(18)	0.35(18)	0.35(9)	0.31(9)	0.26(1)
			33.00	0.46(51)	0.36(18)	0.35(18)	0.35(9)	0.30(9)	0.26(1)
			66.00	0.46(51)	0.35(18)	0.34(18)	0.34(9)	0.30(9)	0.26(1)
137	Fondazione	49-51	0.00	0.46(51)	0.35(18)	0.34(18)	0.34(9)	0.30(9)	0.26(1)
			33.00	0.46(51)	0.35(18)	0.34(18)	0.34(9)	0.30(9)	0.25(1)
			66.00	0.45(51)	0.35(18)	0.33(18)	0.34(9)	0.30(9)	0.25(1)
138	Fondazione	50-52	0.00	0.47(39)	0.36(9)	0.34(9)	0.35(5)	0.30(9)	0.26(1)
			33.00	0.46(39)	0.35(9)	0.34(9)	0.35(5)	0.30(9)	0.26(1)
			66.00	0.46(39)	0.35(9)	0.34(9)	0.34(5)	0.30(9)	0.25(1)
139	Fondazione	50-52	0.00	0.46(1)	0.35(9)	0.34(9)	0.34(5)	0.30(9)	0.25(1)

			33.00	0.45(1)	0.34(9)	0.33(9)	0.34(5)	0.30(9)	0.25(1)
			66.00	0.45(1)	0.34(9)	0.33(9)	0.34(5)	0.29(9)	0.25(1)
140	Fondazione	51-53	0.00	0.45(1)	0.35(18)	0.33(18)	0.34(9)	0.30(9)	0.25(1)
			33.00	0.44(1)	0.34(18)	0.33(18)	0.33(9)	0.29(9)	0.25(1)
			66.00	0.44(1)	0.33(18)	0.32(18)	0.33(9)	0.29(9)	0.25(1)
141	Fondazione	51-53	0.00	0.44(48)	0.33(14)	0.32(18)	0.33(9)	0.29(9)	0.25(1)
			33.00	0.43(48)	0.33(14)	0.32(18)	0.33(9)	0.29(9)	0.24(1)
			66.00	0.43(48)	0.33(14)	0.32(18)	0.32(9)	0.28(9)	0.24(1)
142	Fondazione	52-54	0.00	0.45(1)	0.34(9)	0.33(9)	0.34(5)	0.29(9)	0.25(1)
			33.00	0.44(1)	0.33(9)	0.32(9)	0.33(5)	0.29(9)	0.25(1)
			66.00	0.43(1)	0.33(9)	0.32(9)	0.33(5)	0.29(9)	0.24(1)
143	Fondazione	52-54	0.00	0.43(1)	0.33(9)	0.32(9)	0.33(5)	0.29(9)	0.24(1)
			33.00	0.43(1)	0.32(9)	0.31(9)	0.32(5)	0.28(9)	0.24(1)
			66.00	0.42(1)	0.32(9)	0.31(9)	0.32(5)	0.28(9)	0.24(1)
144	Fondazione	53-55	0.00	0.43(46)	0.33(14)	0.32(14)	0.32(9)	0.28(9)	0.24(1)
			33.00	0.43(46)	0.32(14)	0.31(14)	0.32(9)	0.28(9)	0.24(1)
			66.00	0.43(46)	0.32(14)	0.31(14)	0.31(9)	0.27(9)	0.23(1)
145	Fondazione	53-55	0.00	0.43(46)	0.32(14)	0.31(14)	0.31(9)	0.27(9)	0.23(1)
			33.00	0.44(46)	0.32(14)	0.31(14)	0.30(9)	0.27(9)	0.23(1)
			66.00	0.46(46)	0.32(14)	0.31(14)	0.30(9)	0.26(9)	0.22(1)
146	Fondazione	54-56	0.00	0.42(1)	0.32(9)	0.31(9)	0.32(5)	0.28(9)	0.24(1)
			33.00	0.42(1)	0.31(9)	0.30(9)	0.31(5)	0.27(9)	0.23(1)
			66.00	0.41(1)	0.30(9)	0.30(9)	0.31(5)	0.27(9)	0.23(1)
147	Fondazione	54-56	0.00	0.41(1)	0.30(9)	0.30(9)	0.31(5)	0.27(9)	0.23(1)
			33.00	0.40(1)	0.30(9)	0.29(9)	0.30(5)	0.26(9)	0.23(1)
			66.00	0.39(1)	0.30(9)	0.29(9)	0.30(5)	0.26(9)	0.22(1)
148	Fondazione	55-57	0.00	0.46(46)	0.32(30)	0.31(30)	0.30(9)	0.26(6)	0.22(1)
			39.75	0.50(46)	0.33(30)	0.31(30)	0.29(9)	0.26(6)	0.22(1)
			79.50	0.55(46)	0.36(30)	0.33(30)	0.28(9)	0.25(6)	0.22(1)
149	Fondazione	55-57	0.00	0.55(46)	0.36(30)	0.33(30)	0.28(13)	0.25(7)	0.22(1)
			39.75	0.63(46)	0.40(30)	0.35(30)	0.28(13)	0.25(7)	0.22(1)
			79.50	0.71(46) *	0.44(30) *	0.38(30)	0.28(13)	0.25(7)	0.22(1)
150	Fondazione	56-70	0.00	0.39(1)	0.30(9)	0.29(9)	0.30(5)	0.26(5)	0.22(1)
			39.75	0.39(1)	0.29(9)	0.29(9)	0.29(5)	0.26(5)	0.22(1)
			79.50	0.38(1)	0.29(9)	0.29(9)	0.28(5)	0.25(5)	0.22(1)
151	Fondazione	56-70	0.00	0.38(9)	0.29(9)	0.29(9)	0.28(5)	0.25(5)	0.22(1)
			39.75	0.37(9)	0.29(9)	0.29(9)	0.28(5)	0.25(5)	0.22(1)
			79.50	0.38(9)	0.30(9)	0.29(9)	0.28(5)	0.25(5)	0.22(1)
152	Fondazione	57-58	0.00	0.71(46) *	0.44(33) *	0.38(33)	0.28(13)	0.25(7)	0.22(1)
			41.56	0.61(46)	0.38(33)	0.33(33)	0.26(13)	0.23(7)	0.20(1)
			83.12	0.52(46)	0.33(33)	0.30(33)	0.24(13)	0.22(7)	0.19(1)
153	Fondazione	57-58	0.00	0.52(46)	0.33(33)	0.30(33)	0.24(13)	0.22(7)	0.19(1)
			41.56	0.45(46)	0.30(33)	0.27(33)	0.23(13)	0.21(7)	0.18(1)
			83.12	0.39(46)	0.27(33)	0.24(33)	0.22(13)	0.20(7)	0.17(1)
154	Fondazione	58-59	0.00	0.39(46)	0.27(33)	0.24(33)	0.22(13)	0.20(7)	0.17(1)
			34.50	0.35(46)	0.25(33)	0.23(33)	0.21(13)	0.19(7)	0.16(1)
			69.00	0.32(46)	0.23(33)	0.21(33)	0.21(13)	0.19(7)	0.16(1)
155	Fondazione	58-59	0.00	0.32(46)	0.23(33)	0.21(1)	0.21(13)	0.19(7)	0.16(1)
			34.50	0.30(46)	0.22(33)	0.20(1)	0.21(13)	0.18(7)	0.16(1)
			69.00	0.28(46)	0.21(33)	0.20(1)	0.20(13)	0.18(7)	0.16(1)
156	Fondazione	59-60	0.00	0.28(1)	0.21(1)	0.20(1)	0.20(13)	0.18(7)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.20(13)	0.18(7)	0.15(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.20(13)	0.18(7)	0.15(1)
157	Fondazione	59-60	0.00	0.28(1)	0.20(1)	0.20(1)	0.20(13)	0.18(7)	0.15(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.20(13)	0.18(7)	0.15(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.20(13)	0.18(7)	0.15(1)
158	Fondazione	60-61	0.00	0.28(1)	0.20(1)	0.20(1)	0.20(13)	0.18(7)	0.15(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.18(7)	0.15(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.18(7)	0.16(1)
159	Fondazione	60-61	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.18(7)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.18(7)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
160	Fondazione	61-62	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
161	Fondazione	61-62	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
162	Fondazione	62-63	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
163	Fondazione	62-63	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)

			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
164	Fondazione	63-64	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
165	Fondazione	63-64	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
166	Fondazione	64-65	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
167	Fondazione	64-65	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
168	Fondazione	65-66	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
169	Fondazione	65-66	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
170	Fondazione	66-67	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.18(7)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.18(7)	0.16(1)
171	Fondazione	66-67	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.18(7)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.18(7)	0.15(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.20(13)	0.18(7)	0.15(1)
172	Fondazione	67-68	0.00	0.28(1)	0.20(1)	0.20(1)	0.20(13)	0.18(7)	0.15(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.20(13)	0.18(7)	0.15(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.20(13)	0.18(7)	0.15(1)
173	Fondazione	67-68	0.00	0.28(1)	0.20(1)	0.20(1)	0.20(13)	0.18(7)	0.15(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.20(13)	0.18(7)	0.15(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.20(13)	0.18(7)	0.16(1)
174	Fondazione	68-69	0.00	0.28(1)	0.20(1)	0.20(1)	0.20(13)	0.18(7)	0.16(1)
			34.50	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.18(7)	0.16(1)
			69.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
175	Fondazione	68-69	0.00	0.28(1)	0.20(1)	0.20(1)	0.21(13)	0.19(7)	0.16(1)
			34.50	0.29(1)	0.21(1)	0.21(1)	0.21(13)	0.19(7)	0.16(1)
			69.00	0.30(1)	0.21(1)	0.21(1)	0.22(13)	0.20(7)	0.17(1)
176	Fondazione	69-70	0.00	0.30(1)	0.21(9)	0.21(1)	0.22(13)	0.20(7)	0.17(1)
			41.56	0.31(1)	0.22(9)	0.22(1)	0.23(13)	0.21(7)	0.18(1)
			83.12	0.33(1)	0.24(9)	0.23(1)	0.24(13)	0.22(7)	0.19(1)
177	Fondazione	69-70	0.00	0.33(9)	0.24(9)	0.23(9)	0.24(5)	0.22(5)	0.19(1)
			41.56	0.35(9)	0.27(9)	0.26(9)	0.26(5)	0.23(5)	0.20(1)
			83.12	0.38(9)	0.30(9)	0.29(9)	0.28(5)	0.25(5)	0.22(1)

Tabella 37.II

Tensioni Terreno						
		SLV	SLD	SLO	SLE	
		A1	A1		Caratt.	Freq.
Piastra	Fili	σ_t [daN/cm ²]	σ_t [daN/cm ²]	σ_t [daN/cm ²]	σ_t [daN/cm ²]	σ_t [daN/cm ²]
1	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	0.61(18)	0.46(18)	0.44(18) *	0.36(9)	0.32(1) *
2	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	0.71(46) *	0.46(30)	0.43(18)	0.36(9)	0.32(1) *
3	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8,	0.66(43)	0.45(29)	0.39(29)	0.34(5)	0.30(1)

	7, 6, 5, 4, 3, 2					
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* valore massimo.

1.4 Verifiche Nodi.

1.4.1 Verifiche SLV - Verifica Nodo.

Nodo : numerazione interna del nodo;
 Filo : filo fisso al quale appartiene il nodo considerato;
 D staffe : passo delle staffe;
 \varnothing : diametro delle staffe;
 S traz : coefficiente di sicurezza per integrità per fessurazione;
 S comp : coefficiente di sicurezza per compressione puntone diagonale;
 Esito : Esito della verifica : V = VERIFICATA;
 : NV = NON VERIFICATA;

Tabella 38.I

Nodo	Imp.	Filo	D staffe [cm]	\varnothing [mm]	η	vd	VjbdX [daN]	S comp X	VjbdY [daN]	S comp Y	Esito comp	S traz	Esito traz
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* numero nodo relativo alla numerazione del modello di calcolo.

1.5 Verifica Aste.

1.5.1 Verifiche Travi di Fondazione in C.A. .

Qui di seguito vengono riportate le tabelle riportanti i risultati delle verifiche relative alle travi di fondazione della struttura.

1.5.1.1 Verifiche SLV - Flessione Composta

Camp : campata alla quale appartengono le aste riportate;
 Asta : numerazione interna dell'asta;
 Imp. : impalcato al quale appartiene l'asta considerata;
 Fili : fili fissi ai quali appartiene l'asta considerata;
 Tipo Sez. : tipo di sezione dell'asta considerata;
 ε_{c2} : deformazione di contrazione del calcestruzzo al raggiungimento della massima tensione;
 ε_{cu2} : deformazione ultima di contrazione del calcestruzzo;
 X : distanza dal nodo iniziale misurata lungo l'asse dell'asta
 Cop : distanza tra la superficie esterna dell'armatura più prossima alla superficie del calcestruzzo e la superficie stessa del calcestruzzo;
 A_{sup} : valore dell'area di armatura presente all'estradosso;
 A_{inf} : valore dell'area di armatura presente all'intradosso;
 A_{fl} : valore dell'area di armatura presente nella sezione;

Azioni Sollecitanti:

N_{sd} : Sforzo Normale Sollecitante;
 M_{sdXZ} : valore del Momento Flettente X-Z sollecitante di calcolo;
 M_{sdXY} : valore del Momento Flettente X-Y sollecitante di calcolo;

ε_{cls} : deformazione massima del calcestruzzo compresso
 ε_{acc} : deformazione massima dell'armatura tesa

Azioni Resistenti:

N_{Rd} : Sforzo Normale Resistente;
 M_{RdXZ} : valore del Momento Flettente X-Z resistente di calcolo;
 M_{RdXY} : valore del Momento Flettente X-Y resistente di calcolo;

C : campo di rottura
 S : valore del coefficiente di sicurezza minimo della sezione;
 Esito : Esito della verifica : V = VERIFICATA;
 : NV = NON VERIFICATA;

Tabella 39.I

Camp	Asta	Imp.	Fili	Tipo Sez.	Azioni Sollecitanti										Azioni Resistenti		Azioni Resistenti			C	S	Esit o
					g _{cu} [%]	g _{cu} 2 [%]	X [cm]	Cop [cm]	A _{sup} [cm²]	A _{inf} [cm²]	A _n [cm²]	N _{sd} [daN]	M _{sdz} [daNm]	M _{sdxy} [daNm]	g _{cls} [%]	g _{acc} [%]	N _{rd} [daN]	M _{rdz} [daNm]	M _{rdxy} [daNm]			
404	1	Fondazi one	1-2	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	-674	-	0.68	1.86	1	-10202	-	2	15.13	V
					2.00	3.50	51	2.5	8.04	8.04	16.08	0	-1829	-	0.68	1.86	1	-10202	-	2	5.58	V
					2.00	3.50	166	2.5	8.04	8.04	16.08	0	-1687	-	0.68	1.86	1	-10202	-	2	6.05	V
405	3	Fondazi one	1-15	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	-696	-	0.68	1.86	1	-10202	-	2	14.66	V
					2.00	3.50	122	2.5	8.04	8.04	16.08	0	2367	-	0.68	1.86	1	10202	-	2	4.31	V
					2.00	3.50	159	2.5	8.04	8.04	16.08	0	2877	-	0.68	1.86	1	10202	-	2	3.55	V
406	5	Fondazi one	2-3	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	-1315	-	0.68	1.86	1	-10202	-	2	7.76	V
					2.00	3.50	31	2.5	8.04	8.04	16.08	0	-1394	-	0.68	1.86	1	-10202	-	2	7.32	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	-699	-	0.68	1.86	1	-10202	-	2	14.59	V
407	7	Fondazi one	3-4	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	-562	-	0.68	1.86	1	-10202	-	2	18.17	V
					2.00	3.50	47	2.5	8.04	8.04	16.08	0	-657	-	0.68	1.86	1	-10202	-	2	15.53	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	218	-	0.68	1.86	1	10202	-	2	46.89	V
408	9	Fondazi one	4-5	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	166	-	0.68	1.86	1	10202	-	2	61.51	V
					2.00	3.50	63	2.5	8.04	8.04	16.08	0	-292	-	0.68	1.86	1	-10202	-	2	34.96	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	226	-	0.68	1.86	1	10202	-	2	45.20	V
409	11	Fondazi one	5-6	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	209	-	0.68	1.86	1	10202	-	2	48.93	V
					2.00	3.50	110	2.5	8.04	8.04	16.08	0	420	-	0.68	1.86	1	10202	-	2	24.30	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	545	-	0.68	1.86	1	10202	-	2	18.73	V
410	13	Fondazi one	6-7	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	538	-	0.68	1.86	1	10202	-	2	18.95	V
					2.00	3.50	110	2.5	8.04	8.04	16.08	0	373	-	0.68	1.86	1	10202	-	2	27.36	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	533	-	0.68	1.86	1	10202	-	2	19.15	V
411	15	Fondazi one	7-8	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	550	-	0.68	1.86	1	10202	-	2	18.54	V
					2.00	3.50	16	2.5	8.04	8.04	16.08	0	416	-	0.68	1.86	1	10202	-	2	24.51	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	125	-	0.68	1.86	1	10202	-	2	81.88	V
412	17	Fondazi one	8-9	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	154	-	0.68	1.86	1	10202	-	2	66.23	V
					2.00	3.50	110	2.5	8.04	8.04	16.08	0	399	-	0.68	1.86	1	10202	-	2	25.57	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	542	-	0.68	1.86	1	10202	-	2	18.83	V
413	19	Fondazi one	9-10	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	537	-	0.68	1.86	1	10202	-	2	19.01	V
					2.00	3.50	110	2.5	8.04	8.04	16.08	0	382	-	0.68	1.86	1	10202	-	2	26.69	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	543	-	0.68	1.86	1	10202	-	2	18.79	V
414	21	Fondazi one	10-11	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	561	-	0.68	1.86	1	10202	-	2	18.19	V
					2.00	3.50	16	2.5	8.04	8.04	16.08	0	449	-	0.68	1.86	1	10202	-	2	22.72	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	170	-	0.68	1.86	1	10202	-	2	60.04	V
415	23	Fondazi one	11-12	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	199	-	0.68	1.86	1	10202	-	2	51.22	V
					2.00	3.50	110	2.5	8.04	8.04	16.08	0	-333	-	0.68	1.86	1	-10202	-	2	30.65	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	-331	-	0.68	1.86	1	-10202	-	2	30.79	V
416	25	Fondazi one	12-13	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	-276	-	0.68	1.86	1	-10202	-	2	37.02	V
					2.00	3.50	110	2.5	8.04	8.04	16.08	0	-879	-	0.68	1.86	1	-10202	-	2	11.60	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	-973	-	0.68	1.86	1	-10202	-	2	10.49	V
417	27	Fondazi one	13-14	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	-861	-	0.68	1.86	1	-10202	-	2	11.84	V
					2.00	3.50	68	2.5	8.04	8.04	16.08	0	-980	-	0.68	1.86	1	-10202	-	2	10.41	V
					2.00	3.50	166	2.5	8.04	8.04	16.08	0	-695	-	0.68	1.86	1	-10202	-	2	14.68	V
418	29	Fondazi one	14-16	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	-320	-	0.68	1.86	1	-10202	-	2	31.84	V
					2.00	3.50	70	2.5	8.04	8.04	16.08	0	-619	-	0.68	1.86	1	-10202	-	2	16.48	V
					2.00	3.50	159	2.5	8.04	8.04	16.08	0	733	-	0.68	1.86	1	10202	-	2	13.92	V
419	31	Fondazi one	15-17	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	2453	-	0.68	1.86	1	10202	-	2	4.16	V
					2.00	3.50	15	2.5	8.04	8.04	16.08	0	-2122	-	0.68	1.86	1	-10202	-	2	4.81	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	1203	-	0.68	1.86	1	10202	-	2	8.48	V
420	33	Fondazi one	16-18	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	682	-	0.68	1.86	1	10202	-	2	14.95	V
					2.00	3.50	15	2.5	8.04	8.04	16.08	0	451	-	0.68	1.86	1	10202	-	2	22.62	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	648	-	0.68	1.86	1	10202	-	2	15.75	V
421	35	Fondazi one	17-19	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	1004	-	0.68	1.86	1	10202	-	2	10.16	V
					2.00	3.50	102	2.5	8.04	8.04	16.08	0	1262	-	0.68	1.86	1	10202	-	2	8.08	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	1772	-	0.68	1.86	1	10202	-	2	5.76	V
422	37	Fondazi one	18-20	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	445	-	0.68	1.86	1	10202	-	2	22.93	V
					2.00	3.50	102	2.5	8.04	8.04	16.08	0	469	-	0.68	1.86	1	10202	-	2	21.74	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	818	-	0.68	1.86	1	10202	-	2	12.47	V
423	39	Fondazi one	19-21	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	1745	-	0.68	1.86	1	10202	-	2	5.85	V
					2.00	3.50	15	2.5	8.04	8.04	16.08	0	1243	-	0.68	1.86	1	10202	-	2	8.21	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	1567	-	0.68	1.86	1	10202	-	2	6.51	V
424	41	Fondazi one	20-22	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	773	-	0.68	1.86	1	10202	-	2	13.20	V

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					2.00	3.50	15	2.5	8.04	8.04	16.08	0	483	-	0.68	1.86	1	10202	-	2	21.10	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	633	-	0.68	1.86	1	10202	-	2	16.13	V
425	43	Fondazi one	21-2 3	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	1362	-	0.68	1.86	1	10202	-	2	7.49	V
					2.00	3.50	102	2.5	8.04	8.04	16.08	0	1009	-	0.68	1.86	1	10202	-	2	10.11	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	1539	-	0.68	1.86	1	10202	-	2	6.63	V
426	45	Fondazi one	22-2 4	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	535	-	0.68	1.86	1	10202	-	2	19.06	V
					2.00	3.50	102	2.5	8.04	8.04	16.08	0	381	-	0.68	1.86	1	10202	-	2	26.80	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	709	-	0.68	1.86	1	10202	-	2	14.38	V
427	47	Fondazi one	23-2 5	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	1699	-	0.68	1.86	1	10202	-	2	6.00	V
					2.00	3.50	102	2.5	8.04	8.04	16.08	0	-1388	-	0.68	1.86	1	-10202	-	2	7.35	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	-1701	-	0.68	1.86	1	-10202	-	2	6.00	V
428	49	Fondazi one	24-2 6	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	693	-	0.68	1.86	1	10202	-	2	14.72	V
					2.00	3.50	73	2.5	8.04	8.04	16.08	0	-445	-	0.68	1.86	1	-10202	-	2	22.93	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	402	-	0.68	1.86	1	10202	-	2	25.36	V
429	51	Fondazi one	25-2 6	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	-2975	-	0.68	1.86	1	-10202	-	2	3.43	V
					2.00	3.50	157 5	2.5	8.04	8.04	16.08	0	-1240	-	0.68	1.86	1	-10202	-	2	8.23	V
					2.00	3.50	185 0	2.5	8.04	8.04	16.08	0	-3187	-	0.68	1.86	1	-10202	-	2	3.20	V
430	70	Fondazi one	25-2 8	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	1400	-	0.68	1.86	1	10202	-	2	7.29	V
					2.00	3.50	19	2.5	8.04	8.04	16.08	0	-1240	-	0.68	1.86	1	-10202	-	2	8.23	V
					2.00	3.50	170	2.5	8.04	8.04	16.08	0	1848	-	0.68	1.86	1	10202	-	2	5.52	V
431	72	Fondazi one	26-2 7	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	-237	-	0.68	1.86	1	-10202	-	2	43.00	V
					2.00	3.50	73	2.5	8.04	8.04	16.08	0	-448	-	0.68	1.86	1	-10202	-	2	22.79	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	734	-	0.68	1.86	1	10202	-	2	13.90	V
432	74	Fondazi one	27-2 9	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	731	-	0.68	1.86	1	10202	-	2	13.96	V
					2.00	3.50	15	2.5	8.04	8.04	16.08	0	399	-	0.68	1.86	1	10202	-	2	25.54	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	757	-	0.68	1.86	1	10202	-	2	13.48	V
433	76	Fondazi one	28-3 0	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	2083	-	0.68	1.86	1	10202	-	2	4.90	V
					2.00	3.50	16	2.5	8.04	8.04	16.08	0	1491	-	0.68	1.86	1	10202	-	2	6.84	V
					2.00	3.50	146	2.5	8.04	8.04	16.08	0	825	-	0.68	1.86	1	10202	-	2	12.36	V
434	78	Fondazi one	29-3 1	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	618	-	0.68	1.86	1	10202	-	2	16.50	V
					2.00	3.50	102	2.5	8.04	8.04	16.08	0	353	-	0.68	1.86	1	10202	-	2	28.94	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	734	-	0.68	1.86	1	10202	-	2	13.90	V
435	80	Fondazi one	30-3 2	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	713	-	0.68	1.86	1	10202	-	2	14.30	V
					2.00	3.50	106	2.5	8.04	8.04	16.08	0	488	-	0.68	1.86	1	10202	-	2	20.90	V
					2.00	3.50	137	2.5	8.04	8.04	16.08	0	910	-	0.68	1.86	1	10202	-	2	11.21	V
436	82	Fondazi one	31-3 3	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	757	-	0.68	1.86	1	10202	-	2	13.48	V
					2.00	3.50	15	2.5	8.04	8.04	16.08	0	405	-	0.68	1.86	1	10202	-	2	25.16	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	668	-	0.68	1.86	1	10202	-	2	15.27	V
437	84	Fondazi one	32-3 4	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	720	-	0.68	1.86	1	10202	-	2	14.17	V
					2.00	3.50	61	2.5	8.04	8.04	16.08	0	-430	-	0.68	1.86	1	-10202	-	2	23.74	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	779	-	0.68	1.86	1	10202	-	2	13.10	V
438	86	Fondazi one	33-3 5	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	647	-	0.68	1.86	1	10202	-	2	15.77	V
					2.00	3.50	15	2.5	8.04	8.04	16.08	0	315	-	0.68	1.86	1	10202	-	2	32.35	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	667	-	0.68	1.86	1	10202	-	2	15.28	V
439	88	Fondazi one	34-3 6	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	658	-	0.68	1.86	1	10202	-	2	15.50	V
					2.00	3.50	61	2.5	8.04	8.04	16.08	0	-385	-	0.68	1.86	1	-10202	-	2	26.52	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	675	-	0.68	1.86	1	10202	-	2	15.11	V
440	90	Fondazi one	35-3 7	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	767	-	0.68	1.86	1	10202	-	2	13.29	V
					2.00	3.50	15	2.5	8.04	8.04	16.08	0	388	-	0.68	1.86	1	10202	-	2	26.28	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	684	-	0.68	1.86	1	10202	-	2	14.92	V
441	92	Fondazi one	36-3 8	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	639	-	0.68	1.86	1	10202	-	2	15.97	V
					2.00	3.50	61	2.5	8.04	8.04	16.08	0	-448	-	0.68	1.86	1	-10202	-	2	22.77	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	610	-	0.68	1.86	1	10202	-	2	16.73	V
442	94	Fondazi one	37-3 9	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	746	-	0.68	1.86	1	10202	-	2	13.67	V
					2.00	3.50	102	2.5	8.04	8.04	16.08	0	422	-	0.68	1.86	1	10202	-	2	24.16	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	759	-	0.68	1.86	1	10202	-	2	13.45	V
443	96	Fondazi one	38-4 0	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	611	-	0.68	1.86	1	10202	-	2	16.69	V
					2.00	3.50	61	2.5	8.04	8.04	16.08	0	-436	-	0.68	1.86	1	-10202	-	2	23.41	V
					2.00	3.50	137	2.5	8.04	8.04	16.08	0	577	-	0.68	1.86	1	10202	-	2	17.68	V
444	98	Fondazi one	39-4 1	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	941	-	0.68	1.86	1	10202	-	2	10.84	V
					2.00	3.50	15	2.5	8.04	8.04	16.08	0	528	-	0.68	1.86	1	10202	-	2	19.33	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	475	-	0.68	1.86	1	10202	-	2	21.48	V
445	100	Fondazi one	40-4 2	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	510	-	0.68	1.86	1	10202	-	2	19.98	V
					2.00	3.50	107	2.5	8.04	8.04	16.08	0	947	-	0.68	1.86	1	10202	-	2	10.78	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	1506	-	0.68	1.86	1	10202	-	2	6.78	V
446	102	Fondazi one	41-4 4	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	586	-	0.68	1.86	1	10202	-	2	17.42	V
					2.00	3.50	58	2.5	8.04	8.04	16.08	0	-712	-	0.68	1.86	1	-10202	-	2	14.33	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	605	-	0.68	1.86	1	10202	-	2	16.87	V
447	104	Fondazi one	42-4 3	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	1343	-	0.68	1.86	1	10202	-	2	7.59	V
					2.00	3.50	26	2.5	8.04	8.04	16.08	0	1406	-	0.68	1.86	1	10202	-	2	7.25	V
					2.00	3.50	46	2.5	8.04	8.04	16.08	0	1440	-	0.68	1.86	1	10202	-	2	7.08	V
448	105	Fondazi	43-4	7	2.00	3.50	0	2.5	8.04	8.04	16.08	0	-4199	-</								

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		one	4		2.00	3.50	225	2.5	8.04	8.04	16.08	0	-1431	-	0.68	1.86	1	-10202	-	2	7.13	V
					2.00	3.50	185	2.5	8.04	8.04	16.08	0	-3501	-	0.68	1.86	1	-10202	-	2	2.91	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	1383	-	0.68	1.86	1	10202	-	2	7.38	V
					2.00	3.50	102	2.5	8.04	8.04	16.08	0	1029	-	0.68	1.86	1	10202	-	2	9.91	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	1569	-	0.68	1.86	1	10202	-	2	6.50	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	417	-	0.68	1.86	1	10202	-	2	24.46	V
					2.00	3.50	58	2.5	8.04	8.04	16.08	0	-506	-	0.68	1.86	1	-10202	-	2	20.17	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	748	-	0.68	1.86	1	10202	-	2	13.64	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	1840	-	0.68	1.86	1	10202	-	2	5.55	V
					2.00	3.50	15	2.5	8.04	8.04	16.08	0	1246	-	0.68	1.86	1	10202	-	2	8.19	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	1651	-	0.68	1.86	1	10202	-	2	6.18	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	905	-	0.68	1.86	1	10202	-	2	11.27	V
					2.00	3.50	15	2.5	8.04	8.04	16.08	0	501	-	0.68	1.86	1	10202	-	2	20.36	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	696	-	0.68	1.86	1	10202	-	2	14.67	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	1445	-	0.68	1.86	1	10202	-	2	7.06	V
					2.00	3.50	15	2.5	8.04	8.04	16.08	0	905	-	0.68	1.86	1	10202	-	2	11.27	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	1339	-	0.68	1.86	1	10202	-	2	7.62	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	767	-	0.68	1.86	1	10202	-	2	13.30	V
					2.00	3.50	15	2.5	8.04	8.04	16.08	0	430	-	0.68	1.86	1	10202	-	2	23.75	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	665	-	0.68	1.86	1	10202	-	2	15.34	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	1573	-	0.68	1.86	1	10202	-	2	6.48	V
					2.00	3.50	102	2.5	8.04	8.04	16.08	0	1228	-	0.68	1.86	1	10202	-	2	8.31	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	1767	-	0.68	1.86	1	10202	-	2	5.77	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	895	-	0.68	1.86	1	10202	-	2	11.40	V
					2.00	3.50	15	2.5	8.04	8.04	16.08	0	522	-	0.68	1.86	1	10202	-	2	19.56	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	488	-	0.68	1.86	1	10202	-	2	20.92	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	1745	-	0.68	1.86	1	10202	-	2	5.85	V
					2.00	3.50	15	2.5	8.04	8.04	16.08	0	1234	-	0.68	1.86	1	10202	-	2	8.26	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	972	-	0.68	1.86	1	10202	-	2	10.50	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	644	-	0.68	1.86	1	10202	-	2	15.85	V
					2.00	3.50	58	2.5	8.04	8.04	16.08	0	-497	-	0.68	1.86	1	-10202	-	2	20.54	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	482	-	0.68	1.86	1	10202	-	2	21.16	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	1167	-	0.68	1.86	1	10202	-	2	8.74	V
					2.00	3.50	102	2.5	8.04	8.04	16.08	0	-2207	-	0.68	1.86	1	-10202	-	2	4.62	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	-2476	-	0.68	1.86	1	-10202	-	2	4.12	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	632	-	0.68	1.86	1	10202	-	2	16.14	V
					2.00	3.50	58	2.5	8.04	8.04	16.08	0	-700	-	0.68	1.86	1	-10202	-	2	14.58	V
					2.00	3.50	132	2.5	8.04	8.04	16.08	0	625	-	0.68	1.86	1	10202	-	2	16.32	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	2715	-	0.68	1.86	1	10202	-	2	3.76	V
					2.00	3.50	17	2.5	8.04	8.04	16.08	0	-2392	-	0.68	1.86	1	-10202	-	2	4.27	V
					2.00	3.50	159	2.5	8.04	8.04	16.08	0	-666	-	0.68	1.86	1	-10202	-	2	15.31	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	713	-	0.68	1.86	1	10202	-	2	14.32	V
					2.00	3.50	70	2.5	8.04	8.04	16.08	0	-770	-	0.68	1.86	1	-10202	-	2	13.26	V
					2.00	3.50	159	2.5	8.04	8.04	16.08	0	-311	-	0.68	1.86	1	-10202	-	2	32.77	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	-749	-	0.68	1.86	1	-10202	-	2	13.62	V
					2.00	3.50	118	2.5	8.04	8.04	16.08	0	-1884	-	0.68	1.86	1	-10202	-	2	5.41	V
					2.00	3.50	166	2.5	8.04	8.04	16.08	0	-1820	-	0.68	1.86	1	-10202	-	2	5.60	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	-1414	-	0.68	1.86	1	-10202	-	2	7.22	V
					2.00	3.50	47	2.5	8.04	8.04	16.08	0	-1550	-	0.68	1.86	1	-10202	-	2	6.58	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	-760	-	0.68	1.86	1	-10202	-	2	13.42	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	-629	-	0.68	1.86	1	-10202	-	2	16.23	V
					2.00	3.50	32	2.5	8.04	8.04	16.08	0	-716	-	0.68	1.86	1	-10202	-	2	14.25	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	271	-	0.68	1.86	1	10202	-	2	37.65	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	195	-	0.68	1.86	1	10202	-	2	52.33	V
					2.00	3.50	110	2.5	8.04	8.04	16.08	0	490	-	0.68	1.86	1	10202	-	2	20.83	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	618	-	0.68	1.86	1	10202	-	2	16.51	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	634	-	0.68	1.86	1	10202	-	2	16.08	V
					2.00	3.50	16	2.5	8.04	8.04	16.08	0	445	-	0.68	1.86	1	10202	-	2	22.91	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	575	-	0.68	1.86	1	10202	-	2	17.75	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	588	-	0.68	1.86	1	10202	-	2	17.35	V
					2.00	3.50	16	2.5	8.04	8.04	16.08	0	455	-	0.68	1.86	1	10202	-	2	22.44	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	143	-	0.68	1.86	1	10202	-	2	71.33	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	217	-	0.68	1.86	1	10202	-	2	47.01	V
					2.00	3.50	63	2.5	8.04	8.04	16.08	0	-137	-	0.68	1.86	1	-10202	-	2	74.52	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	222	-	0.68	1.86	1	10202	-	2	45.94	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	207	-	0.68	1.86	1	10202	-	2	49.39	V
					2.00	3.50	110	2.5	8.04	8.04	16.08	0	456	-	0.68	1.86	1	10202	-	2	22.37	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	597	-	0.68	1.86	1	10202	-	2	17.08	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	586	-	0.68	1.86	1	10202	-	2	17.42	V
					2.00	3.50	110	2.5	8.04	8.04	16.08	0	436	-	0.68	1.86	1	10202	-	2	23.37	V
					2.00	3.50	138	2.5	8.04	8.04	16.08	0	608	-	0.68	1.86	1	10202	-	2	16.78	V
					2.00	3.50	0	2.5	8.04	8.04	16.08	0	602	-	0.68	1.86	1	10202	-	2	16.95	V

1.5.1.2 Verifiche SLV - Taglio

Tabella 40.I

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414	21	Fondazio ne	10-11	7	2.5	Ini	2.5	0.00	0	924	-	31775	8	4	20	126	-	34.40	V
415	23	Fondazio ne	11-12	7	2.5	Ini	2.5	0.00	0	863	-	31775	8	4	20	126	-	36.84	V
416	25	Fondazio ne	12-13	7	2.5	Ini	2.5	0.00	0	1294	-	31775	8	4	20	126	-	24.56	V
417	27	Fondazio ne	13-14	7	2.5	Ini	2.5	0.00	0	1350	-	31775	8	4	20	135	-	23.54	V
418	29	Fondazio ne	14-16	7	2.5	Ini	2.5	0.00	0	2106	-	31775	8	4	20	140	-	15.09	V
419	31	Fondazio ne	15-17	7	2.5	Ini	2.5	0.00	0	5116	-	31775	8	4	20	116	-	6.21	V
420	33	Fondazio ne	16-18	7	2.5	Ini	2.5	0.00	0	2431	-	31775	8	4	20	116	-	13.07	V
421	35	Fondazio ne	17-19	7	2.5	Ini	2.5	0.00	0	3887	-	31775	8	4	20	116	-	8.17	V
422	37	Fondazio ne	18-20	7	2.5	Ini	2.5	0.00	0	2678	-	31775	8	4	20	116	-	11.87	V
423	39	Fondazio ne	19-21	7	2.5	Ini	2.5	0.00	0	3982	-	31775	8	4	20	116	-	7.98	V
424	41	Fondazio ne	20-22	7	2.5	Ini	2.5	0.00	0	2444	-	31775	8	4	20	116	-	13.00	V
425	43	Fondazio ne	21-23	7	2.5	Ini	2.5	0.00	0	3959	-	31775	8	4	20	116	-	8.03	V
426	45	Fondazio ne	22-24	7	2.5	Ini	2.5	0.00	0	2613	-	31775	8	4	20	116	-	12.16	V
427	47	Fondazio ne	23-25	7	2.5	Ini	2.5	0.00	0	4718	-	31775	8	4	20	116	-	6.74	V
428	49	Fondazio ne	24-26	7	2.5	Ini	2.5	0.00	0	2689	-	31775	8	4	20	116	-	11.82	V
429	51	Fondazio ne	25-26	7	2.5	Ini	2.5	0.00	0	1650	-	31775	8	4	20	1800	-	19.26	V
430	70	Fondazio ne	25-28	7	2.5	Ini	2.5	0.00	0	4734	-	31775	8	4	20	154	-	6.71	V
431	72	Fondazio ne	26-27	7	2.5	Ini	2.5	0.00	0	3372	-	31775	8	4	20	116	-	9.42	V
432	74	Fondazio ne	27-29	7	2.5	Ini	2.5	0.00	0	2991	-	31775	8	4	20	116	-	10.62	V
433	76	Fondazio ne	28-30	7	2.5	Ini	2.5	0.00	0	4037	-	31775	8	4	20	130	-	7.87	V
434	78	Fondazio ne	29-31	7	2.5	Ini	2.5	0.00	0	2963	-	31775	8	4	20	116	-	10.72	V
435	80	Fondazio ne	30-32	7	2.5	Ini	2.5	0.00	0	3152	-	31775	8	4	20	121	-	10.08	V
436	82	Fondazio ne	31-33	7	2.5	Ini	2.5	0.00	0	2890	-	31775	8	4	20	116	-	11.00	V
437	84	Fondazio ne	32-34	7	2.5	Ini	2.5	0.00	0	3015	-	31775	8	4	20	122	-	10.54	V
438	86	Fondazio ne	33-35	7	2.5	Ini	2.5	0.00	0	2825	-	31775	8	4	20	116	-	11.25	V
439	88	Fondazio ne	34-36	7	2.5	Ini	2.5	0.00	0	2910	-	31775	8	4	20	122	-	10.92	V
440	90	Fondazio ne	35-37	7	2.5	Ini	2.5	0.00	0	3065	-	31775	8	4	20	116	-	10.37	V
441	92	Fondazio ne	36-38	7	2.5	Ini	2.5	0.00	0	2894	-	31775	8	4	20	122	-	10.98	V
442	94	Fondazio ne	37-39	7	2.5	Ini	2.5	0.00	0	2804	-	31775	8	4	20	116	-	11.33	V
443	96	Fondazio ne	38-40	7	2.5	Ini	2.5	0.00	0	2940	-	31775	8	4	20	121	-	10.81	V
444	98	Fondazio ne	39-41	7	2.5	Ini	2.5	0.00	0	3205	-	31775	8	4	20	116	-	9.91	V
445	100	Fondazio ne	40-42	7	2.5	Ini	2.5	0.00	0	4026	-	31775	8	4	20	122	-	7.89	V
446	102	Fondazio ne	41-44	7	2.5	Ini	2.5	0.00	0	3227	-	31775	8	4	20	116	-	9.85	V
447	104	Fondazio ne	42-43	7	2.5	Ini	2.5	0.00	0	1956	-	31775	8	4	20	30	-	16.25	V
448	105	Fondazio ne	43-44	7	2.5	Ini	2.5	0.00	0	1952	-	31775	8	4	20	1800	-	16.28	V
449	124	Fondazio ne	43-45	7	2.5	Ini	2.5	0.00	0	4889	-	31775	8	4	20	116	-	6.50	V
450	126	Fondazio ne	44-46	7	2.5	Ini	2.5	0.00	0	3087	-	31775	8	4	20	116	-	10.29	V
451	128	Fondazio ne	45-47	7	2.5	Ini	2.5	0.00	0	4431	-	31775	8	4	20	116	-	7.17	V
452	130	Fondazio ne	46-48	7	2.5	Ini	2.5	0.00	0	3103	-	31775	8	4	20	116	-	10.24	V
453	132	Fondazio ne	47-49	7	2.5	Ini	2.5	0.00	0	4147	-	31775	8	4	20	116	-	7.66	V
454	134	Fondazio ne	48-50	7	2.5	Ini	2.5	0.00	0	2704	-	31775	8	4	20	116	-	11.75	V
455	136	Fondazio ne	49-51	7	2.5	Ini	2.5	0.00	0	4074	-	31775	8	4	20	116	-	7.80	V
456	138	Fondazio ne	50-52	7	2.5	Ini	2.5	0.00	0	2857	-	31775	8	4	20	116	-	11.12	V
457	140	Fondazio ne	51-53	7	2.5	Ini	2.5	0.00	0	3972	-	31775	8	4	20	116	-	8.00	V
458	142	Fondazio ne	52-54	7	2.5	Ini	2.5	0.00	0	2642	-	31775	8	4	20	116	-	12.03	V
459	144	Fondazio ne	53-55	7	2.5	Ini	2.5	0.00	0	4997	-	31775	8	4	20	116	-	6.36	V
460	146	Fondazio ne	54-56	7	2.5	Ini	2.5	0.00	0	2518	-	31775	8	4	20	116	-	12.62	V
461	148	Fondazio ne	55-57	7	2.5	Ini	2.5	0.00	0	5504	-	31775	8	4	20	140	-	5.77	V
462	150	Fondazio ne	56-70	7	2.5	Ini	2.5	0.00	0	2098	-	31775	8	4	20	140	-	15.14	V

463	152	Fondazio ne	57-58	7	2.5	Ini	2.5	0.00	0	4526	-	31775	8	4	20	135	-	7.02	V
464	154	Fondazio ne	58-59	7	2.5	Ini	2.5	0.00	0	1724	-	31775	8	4	20	126	-	18.43	V
465	156	Fondazio ne	59-60	7	2.5	Ini	2.5	0.00	0	1278	-	31775	8	4	20	126	-	24.86	V
466	158	Fondazio ne	60-61	7	2.5	Ini	2.5	0.00	0	1094	-	31775	8	4	20	126	-	29.05	V
467	160	Fondazio ne	61-62	7	2.5	Ini	2.5	0.00	0	1397	-	31775	8	4	20	126	-	22.74	V
468	162	Fondazio ne	62-63	7	2.5	Ini	2.5	0.00	0	1081	-	31775	8	4	20	126	-	29.40	V
469	164	Fondazio ne	63-64	7	2.5	Ini	2.5	0.00	0	923	-	31775	8	4	20	126	-	34.44	V
470	166	Fondazio ne	64-65	7	2.5	Ini	2.5	0.00	0	1066	-	31775	8	4	20	126	-	29.80	V
471	168	Fondazio ne	65-66	7	2.5	Ini	2.5	0.00	0	1324	-	31775	8	4	20	126	-	24.00	V
472	170	Fondazio ne	66-67	7	2.5	Ini	2.5	0.00	0	924	-	31775	8	4	20	126	-	34.39	V
473	172	Fondazio ne	67-68	7	2.5	Ini	2.5	0.00	0	853	-	31775	8	4	20	126	-	37.24	V
474	174	Fondazio ne	68-69	7	2.5	Ini	2.5	0.00	0	1448	-	31775	8	4	20	126	-	21.94	V
475	176	Fondazio ne	69-70	7	2.5	Ini	2.5	0.00	0	1544	-	31775	8	4	20	135	-	20.58	V

1.5.1.2.1 Verifiche SLD - Flessione Composta.

Camp : campata alla quale appartengono le aste riportate;
 Asta : numerazione interna dell'asta;
 Imp. : impalcato al quale appartiene l'asta considerata;
 Fili : fili fissi ai quali appartiene l'asta considerata;
 Tipo Sez. : tipo di sezione dell'asta considerata;
 X : distanza dal nodo iniziale misurata lungo l'asse dell'asta

Azioni Sollecitanti:

N_{sd} : Sforzo Normale Sollecitante;
 M_{sdXZ} : valore del Momento Flettente X-Z sollecitante di calcolo;
 M_{sdXY} : valore del Momento Flettente X-Y sollecitante di calcolo;

Azioni Resistenti:

N_{Rd} : Sforzo Normale Resistente;
 M_{RdXZ} : valore del Momento Flettente X-Z resistente di calcolo;
 M_{RdXY} : valore del Momento Flettente X-Y resistente di calcolo;

S : valore del coefficiente di sicurezza minimo della sezione;
 Esito : Esito della verifica : V = VERIFICATA;
 : NV = NON VERIFICATA;

Vedi tabella 41.I

Camp	Asta	Imp.	Fili	Tipo Sez.	X [cm]	Azioni Sollecitanti			Azioni Resistenti			S	Esito
						N_{sd} [daN]	M_{sdXZ} [daNm]	M_{sdXY} [daNm]	N_{Rd} [daN]	M_{RdXZ} [daNm]	M_{RdXY} [daNm]		
404	1	F	1-2	7	0	0	-357	-	0	-11889	-	33.32	V
					51	0	-839	-	0	-11889	-	14.16	V
					166	0	-662	-	0	-11889	-	17.96	V
405	3	F	1-15	7	0	0	-335	-	0	-11889	-	35.53	V
					122	0	-812	-	0	-11889	-	14.65	V
					159	0	1036	-	0	11889	-	11.48	V
406	5	F	2-3	7	0	0	-569	-	0	-11889	-	20.90	V
					31	0	-635	-	0	-11889	-	18.72	V
					138	0	-272	-	0	-11889	-	43.77	V
407	7	F	3-4	7	0	0	-232	-	0	-11889	-	51.34	V
					47	0	-306	-	0	-11889	-	38.84	V
					138	0	95	-	0	11889	-	124.86	V
408	9	F	4-5	7	0	0	79	-	0	11889	-	151.07	V
					63	0	-143	-	0	-11889	-	83.27	V
					138	0	122	-	0	11889	-	97.47	V
409	11	F	5-6	7	0	0	118	-	0	11889	-	101.05	V
					110	0	179	-	0	11889	-	66.57	V
					138	0	255	-	0	11889	-	46.59	V
410	13	F	6-7	7	0	0	254	-	0	11889	-	46.73	V
					110	0	156	-	0	11889	-	76.31	V
					138	0	243	-	0	11889	-	48.99	V
411	15	F	7-8	7	0	0	251	-	0	11889	-	47.43	V
					16	0	169	-	0	11889	-	70.23	V
					138	0	76	-	0	11889	-	156.95	V
412	17	F	8-9	7	0	0	85	-	0	11889	-	140.30	V
					110	0	166	-	0	11889	-	71.72	V
					138	0	252	-	0	11889	-	47.27	V
413	19	F	9-10	7	0	0	247	-	0	11889	-	48.14	V

					110	0	169	-	0	11889	-	70.24	V
					138	0	259	-	0	11889	-	45.84	V
414	21	F	10-11	7	0	0	266	-	0	11889	-	44.63	V
					16	0	190	-	0	11889	-	62.43	V
					138	0	82	-	0	11889	-	145.77	V
415	23	F	11-12	7	0	0	93	-	0	11889	-	128.50	V
					110	0	-188	-	0	-11889	-	63.40	V
					138	0	-166	-	0	-11889	-	71.70	V
416	25	F	12-13	7	0	0	-138	-	0	-11889	-	85.94	V
					110	0	-454	-	0	-11889	-	26.18	V
					138	0	-464	-	0	-11889	-	25.64	V
417	27	F	13-14	7	0	0	-388	-	0	-11889	-	30.64	V
					68	0	-608	-	0	-11889	-	19.55	V
					166	0	-360	-	0	-11889	-	33.05	V
418	29	F	14-16	7	0	0	-205	-	0	-11889	-	57.98	V
					70	0	-431	-	0	-11889	-	27.60	V
					159	0	276	-	0	11889	-	43.10	V
419	31	F	15-17	7	0	0	-834	-	0	-11889	-	14.25	V
					15	0	-766	-	0	-11889	-	15.51	V
					132	0	580	-	0	11889	-	20.50	V
420	33	F	16-18	7	0	0	-173	-	0	-11889	-	68.53	V
					15	0	-187	-	0	-11889	-	63.51	V
					132	0	390	-	0	11889	-	30.50	V
421	35	F	17-19	7	0	0	445	-	0	11889	-	26.74	V
					102	0	510	-	0	11889	-	23.31	V
					132	0	777	-	0	11889	-	15.30	V
422	37	F	18-20	7	0	0	280	-	0	11889	-	42.42	V
					102	0	226	-	0	11889	-	52.55	V
					132	0	437	-	0	11889	-	27.19	V
423	39	F	19-21	7	0	0	729	-	0	11889	-	16.31	V
					15	0	493	-	0	11889	-	24.10	V
					132	0	695	-	0	11889	-	17.10	V
424	41	F	20-22	7	0	0	364	-	0	11889	-	32.62	V
					15	0	207	-	0	11889	-	57.51	V
					132	0	399	-	0	11889	-	29.83	V
425	43	F	21-23	7	0	0	614	-	0	11889	-	19.36	V
					102	0	435	-	0	11889	-	27.35	V
					132	0	694	-	0	11889	-	17.12	V
426	45	F	22-24	7	0	0	329	-	0	11889	-	36.15	V
					102	0	189	-	0	11889	-	63.01	V
					132	0	385	-	0	11889	-	30.84	V
427	47	F	23-25	7	0	0	768	-	0	11889	-	15.49	V
					102	0	-531	-	0	-11889	-	22.39	V
					132	0	-598	-	0	-11889	-	19.90	V
428	49	F	24-26	7	0	0	355	-	0	11889	-	33.45	V
					73	0	-284	-	0	-11889	-	41.93	V
					132	0	151	-	0	11889	-	78.77	V
429	51	F	25-26	7	0	0	-1452	-	0	-11889	-	8.19	V
					1575	0	-741	-	0	-11889	-	16.05	V
					1850	0	-1555	-	0	-11889	-	7.64	V
430	70	F	25-28	7	0	0	493	-	0	11889	-	24.12	V
					19	0	-510	-	0	-11889	-	23.32	V
					170	0	779	-	0	11889	-	15.26	V
431	72	F	26-27	7	0	0	-86	-	0	-11889	-	138.73	V
					73	0	-271	-	0	-11889	-	43.87	V
					132	0	385	-	0	11889	-	30.86	V
432	74	F	27-29	7	0	0	358	-	0	11889	-	33.17	V
					15	0	178	-	0	11889	-	66.64	V
					132	0	413	-	0	11889	-	28.78	V
433	76	F	28-30	7	0	0	873	-	0	11889	-	13.62	V
					16	0	576	-	0	11889	-	20.63	V
					146	0	447	-	0	11889	-	26.58	V
434	78	F	29-31	7	0	0	362	-	0	11889	-	32.80	V
					102	0	169	-	0	11889	-	70.52	V
					132	0	386	-	0	11889	-	30.77	V
435	80	F	30-32	7	0	0	398	-	0	11889	-	29.88	V
					106	0	233	-	0	11889	-	51.01	V
					137	0	479	-	0	11889	-	24.84	V
436	82	F	31-33	7	0	0	388	-	0	11889	-	30.62	V
					15	0	180	-	0	11889	-	66.19	V
					132	0	357	-	0	11889	-	33.34	V
437	84	F	32-34	7	0	0	403	-	0	11889	-	29.47	V
					61	0	-241	-	0	-11889	-	49.29	V
					138	0	415	-	0	11889	-	28.67	V
438	86	F	33-35	7	0	0	354	-	0	11889	-	33.57	V
					15	0	152	-	0	11889	-	77.99	V
					132	0	354	-	0	11889	-	33.60	V
439	88	F	34-36	7	0	0	362	-	0	11889	-	32.87	V
					61	0	-236	-	0	-11889	-	50.36	V
					138	0	366	-	0	11889	-	32.48	V
440	90	F	35-37	7	0	0	397	-	0	11889	-	29.96	V
					15	0	179	-	0	11889	-	66.33	V
					132	0	369	-	0	11889	-	32.21	V
441	92	F	36-38	7	0	0	344	-	0	11889	-	34.60	V
					61	0	-263	-	0	-11889	-	45.18	V
					138	0	339	-	0	11889	-	35.06	V
442	94	F	37-39	7	0	0	399	-	0	11889	-	29.78	V
					102	0	208	-	0	11889	-	57.22	V
					132	0	412	-	0	11889	-	28.87	V
443	96	F	38-40	7	0	0	320	-	0	11889	-	37.18	V
					61	0	-255	-	0	-11889	-	46.59	V
					137	0	323	-	0	11889	-	36.86	V
444	98	F	39-41	7	0	0	485	-	0	11889	-	24.52	V
					15	0	249	-	0	11889	-	47.80	V
					132	0	268	-	0	11889	-	44.35	V

445	100	F	40-42	7	0	0	274	-	0	11889	-	43.37	V
					107	0	376	-	0	11889	-	31.59	V
					138	0	664	-	0	11889	-	17.92	V
446	102	F	41-44	7	0	0	308	-	0	11889	-	38.56	V
					58	0	-411	-	0	-11889	-	28.90	V
					132	0	190	-	0	11889	-	62.50	V
447	104	F	42-43	7	0	0	604	-	0	11889	-	19.67	V
					26	0	580	-	0	11889	-	20.51	V
					46	0	589	-	0	11889	-	20.19	V
448	105	F	43-44	7	0	0	-1979	-	0	-11889	-	6.01	V
					225	0	-834	-	0	-11889	-	14.26	V
					1850	0	-1665	-	0	-11889	-	7.14	V
449	124	F	43-45	7	0	0	587	-	0	11889	-	20.27	V
					102	0	390	-	0	11889	-	30.51	V
					132	0	647	-	0	11889	-	18.37	V
450	126	F	44-46	7	0	0	150	-	0	11889	-	79.25	V
					58	0	-316	-	0	-11889	-	37.62	V
					132	0	422	-	0	11889	-	28.15	V
451	128	F	45-47	7	0	0	763	-	0	11889	-	15.59	V
					15	0	468	-	0	11889	-	25.41	V
					132	0	669	-	0	11889	-	17.77	V
452	130	F	46-48	7	0	0	473	-	0	11889	-	25.15	V
					15	0	244	-	0	11889	-	48.80	V
					132	0	390	-	0	11889	-	30.51	V
453	132	F	47-49	7	0	0	621	-	0	11889	-	19.14	V
					15	0	359	-	0	11889	-	33.10	V
					132	0	582	-	0	11889	-	20.42	V
454	134	F	48-50	7	0	0	431	-	0	11889	-	27.61	V
					15	0	229	-	0	11889	-	52.02	V
					132	0	393	-	0	11889	-	30.25	V
455	136	F	49-51	7	0	0	692	-	0	11889	-	17.17	V
					102	0	465	-	0	11889	-	25.56	V
					132	0	709	-	0	11889	-	16.77	V
456	138	F	50-52	7	0	0	509	-	0	11889	-	23.36	V
					15	0	279	-	0	11889	-	42.65	V
					132	0	272	-	0	11889	-	43.65	V
457	140	F	51-53	7	0	0	742	-	0	11889	-	16.01	V
					15	0	478	-	0	11889	-	24.85	V
					132	0	438	-	0	11889	-	27.16	V
458	142	F	52-54	7	0	0	390	-	0	11889	-	30.48	V
					58	0	-282	-	0	-11889	-	42.21	V
					132	0	246	-	0	11889	-	48.43	V
459	144	F	53-55	7	0	0	558	-	0	11889	-	21.30	V
					102	0	-798	-	0	-11889	-	14.89	V
					132	0	-869	-	0	-11889	-	13.68	V
460	146	F	54-56	7	0	0	341	-	0	11889	-	34.90	V
					58	0	-400	-	0	-11889	-	29.72	V
					132	0	226	-	0	11889	-	52.55	V
461	148	F	55-57	7	0	0	996	-	0	11889	-	11.93	V
					17	0	-840	-	0	-11889	-	14.16	V
					159	0	-325	-	0	-11889	-	36.61	V
462	150	F	56-70	7	0	0	332	-	0	11889	-	35.84	V
					70	0	-479	-	0	-11889	-	24.80	V
					159	0	-203	-	0	-11889	-	58.52	V
463	152	F	57-58	7	0	0	-383	-	0	-11889	-	31.01	V
					118	0	-752	-	0	-11889	-	15.82	V
					166	0	-674	-	0	-11889	-	17.63	V
464	154	F	58-59	7	0	0	-566	-	0	-11889	-	20.99	V
					47	0	-659	-	0	-11889	-	18.04	V
					138	0	-300	-	0	-11889	-	39.69	V
465	156	F	59-60	7	0	0	-256	-	0	-11889	-	46.44	V
					32	0	-314	-	0	-11889	-	37.84	V
					138	0	108	-	0	11889	-	109.62	V
466	158	F	60-61	7	0	0	94	-	0	11889	-	126.63	V
					110	0	206	-	0	11889	-	57.85	V
					138	0	286	-	0	11889	-	41.56	V
467	160	F	61-62	7	0	0	295	-	0	11889	-	40.24	V
					16	0	195	-	0	11889	-	60.93	V
					138	0	263	-	0	11889	-	45.15	V
468	162	F	62-63	7	0	0	273	-	0	11889	-	43.51	V
					16	0	191	-	0	11889	-	62.36	V
					138	0	80	-	0	11889	-	149.00	V
469	164	F	63-64	7	0	0	108	-	0	11889	-	109.65	V
					63	0	-82	-	0	-11889	-	144.46	V
					138	0	109	-	0	11889	-	109.25	V
470	166	F	64-65	7	0	0	87	-	0	11889	-	136.20	V
					110	0	190	-	0	11889	-	62.59	V
					138	0	275	-	0	11889	-	43.24	V
471	168	F	65-66	7	0	0	266	-	0	11889	-	44.73	V
					110	0	192	-	0	11889	-	61.96	V
					138	0	286	-	0	11889	-	41.51	V
472	170	F	66-67	7	0	0	281	-	0	11889	-	42.36	V
					16	0	207	-	0	11889	-	57.49	V
					138	0	88	-	0	11889	-	135.83	V
473	172	F	67-68	7	0	0	98	-	0	11889	-	120.84	V
					110	0	-193	-	0	-11889	-	61.69	V
					138	0	-172	-	0	-11889	-	69.31	V
474	174	F	68-69	7	0	0	-166	-	0	-11889	-	71.78	V
					110	0	-490	-	0	-11889	-	24.25	V
					138	0	-502	-	0	-11889	-	23.66	V
475	176	F	69-70	7	0	0	-447	-	0	-11889	-	26.58	V
					51	0	-625	-	0	-11889	-	19.02	V
					166	0	-364	-	0	-11889	-	32.64	V

1.5.1.3 Verifiche SLD - Taglio

Tabella 42.I

Camp	: campata alla quale appartengono le aste riportate;
Asta	: numerazione interna dell'asta;
Imp.	: impalcato al quale appartiene l'asta considerata;
Fili	: fili fissi ai quali appartiene l'asta considerata;
Tipo Sez.	: tipo di sezione dell'asta considerata;
Cop	: distanza tra la superficie esterna dell'armatura più prossima alla superficie del calcestruzzo e la superficie stessa del calcestruzzo;
Blocco	: Ini : tratto (iniziale) nel quale le staffe vengono mantenute costanti; Med : tratto (mediano) nel quale le staffe vengono mantenute costanti; Fin : tratto (finale) nel quale le staffe vengono mantenute costanti;
cot(θ)	: cotangente dell'angolo θ;
A _{Sag}	: area del singolo sagomato;

Tagli Sollecitanti:

V _{SdXY}	: valore del Taglio X-Y sollecitante di calcolo;
V _{SdXZ}	: valore del Taglio X-Z sollecitante di calcolo;

Tagli Resistenti:

V _{RdXZ}	: valore del Taglio X-Z resistente di calcolo;
V _{RdXY}	: valore del Taglio X-Y resistente di calcolo;

φ	: diametro della staffa;
N _{br}	: numero di bracci di cui è composta la staffa;
D _{Staffe}	: interasse tra le staffe;
L _{TR}	: lunghezza dei tratti per cui si ha D _{Staffe} ;
S _{XY}	: coefficiente di sicurezza relativo a V _{SdXY}
S _{XZ}	: coefficiente di sicurezza relativo a V _{SdXZ}
Esito	: Esito della verifica : V = VERIFICATA; : NV = NON VERIFICATA; : NV_min = Minimi di normativa non rispettati;

Tabella 42.I

Camp	Asta	Imp.	Fili	Tipo Sez.	Cop [cm]	Blocco	cot(θ)	A _{Sag} [cm²]	Tagli Sollecitanti		Tagli Resistenti		φ [mm]	N _{br}	D _{Staffe} [cm]	L _{TR} [cm]	S _{XY}	S _{XZ}	Esito
									V _{SdXY} [daN]	V _{SdXZ} [daN]	V _{RdXY} [daN]	V _{RdXZ} [daN]							
404	1	Fondazione	1-2	7	2.5	Ini	2.50	0.00	118	1783	-	36542	8	4	20	135	-	20.49	V
405	3	Fondazione	1-15	7	2.5	Ini	2.50	0.00	102	2035	-	36542	8	4	20	140	-	17.95	V
406	5	Fondazione	2-3	7	2.5	Ini	2.50	0.00	87	774	-	36542	8	4	20	126	-	47.21	V
407	7	Fondazione	3-4	7	2.5	Ini	2.50	0.00	101	622	-	36542	8	4	20	126	-	58.70	V
408	9	Fondazione	4-5	7	2.5	Ini	2.50	0.00	93	520	-	36542	8	4	20	126	-	70.24	V
409	11	Fondazione	5-6	7	2.5	Ini	2.50	0.00	85	564	-	36542	8	4	20	126	-	64.75	V
410	13	Fondazione	6-7	7	2.5	Ini	2.50	0.00	88	654	-	36542	8	4	20	126	-	55.86	V
411	15	Fondazione	7-8	7	2.5	Ini	2.50	0.00	77	614	-	36542	8	4	20	126	-	59.53	V
412	17	Fondazione	8-9	7	2.5	Ini	2.50	0.00	79	622	-	36542	8	4	20	126	-	58.78	V
413	19	Fondazione	9-10	7	2.5	Ini	2.50	0.00	80	597	-	36542	8	4	20	126	-	61.18	V
414	21	Fondazione	10-11	7	2.5	Ini	2.50	0.00	73	576	-	36542	8	4	20	126	-	63.42	V
415	23	Fondazione	11-12	7	2.5	Ini	2.50	0.00	78	580	-	36542	8	4	20	126	-	63.03	V
416	25	Fondazione	12-13	7	2.5	Ini	2.50	0.00	80	715	-	36542	8	4	20	126	-	51.08	V
417	27	Fondazione	13-14	7	2.5	Ini	2.50	0.00	94	905	-	36542	8	4	20	135	-	40.36	V
418	29	Fondazione	14-16	7	2.5	Ini	2.50	0.00	101	1447	-	36542	8	4	20	140	-	25.25	V
419	31	Fondazione	15-17	7	2.5	Ini	2.50	0.00	189	2486	-	36542	8	4	20	116	-	14.70	V
420	33	Fondazione	16-18	7	2.5	Ini	2.50	0.00	195	1673	-	36542	8	4	20	116	-	21.84	V
421	35	Fondazione	17-19	7	2.5	Ini	2.50	0.00	238	1992	-	36542	8	4	20	116	-	18.35	V
422	37	Fondazione	18-20	7	2.5	Ini	2.50	0.00	251	1647	-	36542	8	4	20	116	-	22.18	V
423	39	Fondazione	19-21	7	2.5	Ini	2.50	0.00	226	1934	-	36542	8	4	20	116	-	18.90	V
424	41	Fondazione	20-22	7	2.5	Ini	2.50	0.00	237	1551	-	36542	8	4	20	116	-	23.56	V
425	43	Fondazione	21-23	7	2.5	Ini	2.50	0.00	263	1951	-	36542	8	4	20	116	-	18.73	V
426	45	Fondazione	22-24	7	2.5	Ini	2.50	0.00	266	1551	-	36542	8	4	20	116	-	23.56	V
427	47	Fondazione	23-25	7	2.5	Ini	2.50	0.00	264	2368	-	36542	8	4	20	116	-	15.43	V
428	49	Fondazione	24-26	7	2.5	Ini	2.50	0.00	264	1691	-	36542	8	4	20	116	-	21.61	V
429	51	Fondazione	25-26	7	2.5	Ini	2.50	0.00	122	869	-	36542	8	4	20	1800	-	42.04	V
430	70	Fondazione	25-28	7	2.5	Ini	2.50	0.00	204	2332	-	36542	8	4	20	154	-	15.67	V
431	72	Fondazione	26-27	7	2.5	Ini	2.50	0.00	204	1947	-	36542	8	4	20	116	-	18.76	V
432	74	Fondazione	27-29	7	2.5	Ini	2.50	0.00	286	1735	-	36542	8	4	20	116	-	21.06	V
433	76	Fondazione	28-30	7	2.5	Ini	2.50	0.00	281	1989	-	36542	8	4	20	130	-	18.37	V
434	78	Fondazione	29-31	7	2.5	Ini	2.50	0.00	305	1695	-	36542	8	4	20	116	-	21.56	V
435	80	Fondazione	30-32	7	2.5	Ini	2.50	0.00	313	1819	-	36542	8	4	20	121	-	20.09	V
436	82	Fondazione	31-33	7	2.5	Ini	2.50	0.00	289	1685	-	36542	8	4	20	116	-	21.69	V
437	84	Fondazione	32-34	7	2.5	Ini	2.50	0.00	309	1754	-	36542	8	4	20	122	-	20.83	V
438	86	Fondazione	33-35	7	2.5	Ini	2.50	0.00	310	1654	-	36542	8	4	20	116	-	22.10	V
439	88	Fondazione	34-36	7	2.5	Ini	2.50	0.00	305	1712	-	36542	8	4	20	122	-	21.35	V
440	90	Fondazione	35-37	7	2.5	Ini	2.50	0.00	298	1739	-	36542	8	4	20	116	-	21.01	V

441	92	Fondazione	36-38	7	2.5	Ini	2.50	0.00	297	1715	-	36542	8	4	20	122	-	21.31	V
442	94	Fondazione	37-39	7	2.5	Ini	2.50	0.00	312	1639	-	36542	8	4	20	116	-	22.29	V
443	96	Fondazione	38-40	7	2.5	Ini	2.50	0.00	282	1746	-	36542	8	4	20	121	-	20.93	V
444	98	Fondazione	39-41	7	2.5	Ini	2.50	0.00	299	1829	-	36542	8	4	20	116	-	19.98	V
445	100	Fondazione	40-42	7	2.5	Ini	2.50	0.00	293	2109	-	36542	8	4	20	122	-	17.32	V
446	102	Fondazione	41-44	7	2.5	Ini	2.50	0.00	291	1866	-	36542	8	4	20	116	-	19.58	V
447	104	Fondazione	42-43	7	2.5	Ini	2.50	0.00	253	1057	-	36542	8	4	20	30	-	34.58	V
448	105	Fondazione	43-44	7	2.5	Ini	2.50	0.00	128	1077	-	36542	8	4	20	1800	-	33.92	V
449	124	Fondazione	43-45	7	2.5	Ini	2.50	0.00	210	2526	-	36542	8	4	20	116	-	14.47	V
450	126	Fondazione	44-46	7	2.5	Ini	2.50	0.00	201	1940	-	36542	8	4	20	116	-	18.84	V
451	128	Fondazione	45-47	7	2.5	Ini	2.50	0.00	280	2178	-	36542	8	4	20	116	-	16.78	V
452	130	Fondazione	46-48	7	2.5	Ini	2.50	0.00	270	1765	-	36542	8	4	20	116	-	20.70	V
453	132	Fondazione	47-49	7	2.5	Ini	2.50	0.00	276	1999	-	36542	8	4	20	116	-	18.28	V
454	134	Fondazione	48-50	7	2.5	Ini	2.50	0.00	267	1644	-	36542	8	4	20	116	-	22.23	V
455	136	Fondazione	49-51	7	2.5	Ini	2.50	0.00	231	2013	-	36542	8	4	20	116	-	18.15	V
456	138	Fondazione	50-52	7	2.5	Ini	2.50	0.00	234	1762	-	36542	8	4	20	116	-	20.74	V
457	140	Fondazione	51-53	7	2.5	Ini	2.50	0.00	230	1981	-	36542	8	4	20	116	-	18.45	V
458	142	Fondazione	52-54	7	2.5	Ini	2.50	0.00	216	1683	-	36542	8	4	20	116	-	21.71	V
459	144	Fondazione	53-55	7	2.5	Ini	2.50	0.00	210	2437	-	36542	8	4	20	116	-	15.00	V
460	146	Fondazione	54-56	7	2.5	Ini	2.50	0.00	201	1686	-	36542	8	4	20	116	-	21.68	V
461	148	Fondazione	55-57	7	2.5	Ini	2.50	0.00	131	2067	-	36542	8	4	20	140	-	17.68	V
462	150	Fondazione	56-70	7	2.5	Ini	2.50	0.00	119	1466	-	36542	8	4	20	140	-	24.92	V
463	152	Fondazione	57-58	7	2.5	Ini	2.50	0.00	117	1758	-	36542	8	4	20	135	-	20.78	V
464	154	Fondazione	58-59	7	2.5	Ini	2.50	0.00	88	765	-	36542	8	4	20	126	-	47.77	V
465	156	Fondazione	59-60	7	2.5	Ini	2.50	0.00	98	684	-	36542	8	4	20	126	-	53.39	V
466	158	Fondazione	60-61	7	2.5	Ini	2.50	0.00	91	615	-	36542	8	4	20	126	-	59.42	V
467	160	Fondazione	61-62	7	2.5	Ini	2.50	0.00	93	666	-	36542	8	4	20	126	-	54.90	V
468	162	Fondazione	62-63	7	2.5	Ini	2.50	0.00	81	635	-	36542	8	4	20	126	-	57.56	V
469	164	Fondazione	63-64	7	2.5	Ini	2.50	0.00	80	491	-	36542	8	4	20	126	-	74.43	V
470	166	Fondazione	64-65	7	2.5	Ini	2.50	0.00	79	625	-	36542	8	4	20	126	-	58.48	V
471	168	Fondazione	65-66	7	2.5	Ini	2.50	0.00	80	646	-	36542	8	4	20	126	-	56.53	V
472	170	Fondazione	66-67	7	2.5	Ini	2.50	0.00	73	576	-	36542	8	4	20	126	-	63.41	V
473	172	Fondazione	67-68	7	2.5	Ini	2.50	0.00	78	559	-	36542	8	4	20	126	-	65.39	V
474	174	Fondazione	68-69	7	2.5	Ini	2.50	0.00	80	717	-	36542	8	4	20	126	-	50.97	V
475	176	Fondazione	69-70	7	2.5	Ini	2.50	0.00	92	886	-	36542	8	4	20	135	-	41.25	V

1.5.1.4 Verifiche SLE - Stato Tensionale.

Camp : campata alla quale appartengono le aste riportate;
 Asta : numerazione interna dell'asta;
 Imp. : impalcato al quale appartiene l'asta considerata;
 Fili : fili fissi ai quali appartiene l'asta considerata;
 Tipo Sez. : tipo di sezione dell'asta considerata;
 Cop : distanza tra la superficie esterna dell'armatura più prossima alla superficie del calcestruzzo e la superficie stessa del calcestruzzo;
 Comb : tipo di combinazione a cui la verifica è riferita;
 X : distanza dal nodo iniziale misurata lungo l'asse dell'asta;

Azioni Sollecitanti:

N_{sd} : Sforzo Normale Sollecitante;
 M_{sdXZ} : valore del Momento Flettente X-Z sollecitante di calcolo;
 M_{sdXY} : valore del Momento Flettente X-Y sollecitante di calcolo;

Tensioni:

σ_c : tensioni d'esercizio del calcestruzzo;
 σ_s : tensioni d'esercizio dell'acciaio;

Tensioni Limite:

$\sigma_{c,lim}$: Tensioni limite del calcestruzzo;
 $\sigma_{s,lim}$: Tensioni limite dell'acciaio;

S : valore del coefficiente di sicurezza minimo della sezione;

Esito : Esito della verifica : V = VERIFICATA;
 : NV = NON VERIFICATA;

Tabella 43.I

Camp	Asta	Imp.	Fili	Tipo Sez.	Cop [cm]	Comb	X [cm]	Azioni Sollecitanti			Tensioni		Tensioni Limite		S	Esito
								N_{sd} [daN]	M_{sdXZ} [daNm]	M_{sdXY} [daNm]	σ_c [daN/cm²]	σ_s [daN/cm²]	$\sigma_{c,lim}$ [daN/cm²]	$\sigma_{s,lim}$ [daN/cm²]		
404	1	Fondazione	1-2	7	2.5	Caratt.	0	0	-299	-	2.65	-114.07	150.00	3600.00	31.56	V
							51	0	-507	-	4.50	-193.49	150.00	3600.00	18.61	V
							166	0	-324	-	2.87	-123.63	150.00	3600.00	29.12	V
							0	0	-175	-	1.55	-66.56	112.50	3600.00	54.08	V
							51	0	-309	-	2.74	-118.00	112.50	3600.00	30.51	V
							166	0	-112	-	0.99	-42.67	112.50	3600.00	84.36	V
405	3	Fondazione	1-15	7	2.5	Caratt.	0	0	-182	-	1.61	-69.21	150.00	3600.00	52.02	V
							122	0	153	-	1.36	-58.29	150.00	3600.00	61.77	V

TABULATI DI CALCOLO -

							159	0	381	-	3.38	-145.14	150.00	3600.00	24.80	V
						Q.Perm	0	0	-143	-	1.27	-54.43	112.50	3600.00	66.14	V
							122	0	-32	-	0.29	-12.37	112.50	3600.00	290.95	V
							159	0	148	-	1.32	-56.59	112.50	3600.00	63.62	V
406	5	Fondazione	2-3	7	2.5	Caratt.	0	0	-369	-	3.27	-140.58	150.00	3600.00	25.61	V
							31	0	-400	-	3.54	-152.36	150.00	3600.00	23.63	V
							138	0	-91	-	0.81	-34.82	150.00	3600.00	103.39	V
						Q.Perm	0	0	-164	-	1.45	-62.37	112.50	3600.00	57.72	V
							31	0	-228	-	2.02	-86.81	112.50	3600.00	41.47	V
							138	0	-43	-	0.38	-16.24	112.50	3600.00	221.68	V
407	7	Fondazione	3-4	7	2.5	Caratt.	0	0	-104	-	0.92	-39.49	150.00	3600.00	91.15	V
							47	0	-158	-	1.40	-60.39	150.00	3600.00	59.61	V
							138	0	63	-	0.56	-24.03	150.00	3600.00	149.84	V
						Q.Perm	0	0	-54	-	0.48	-20.45	112.50	3600.00	176.05	V
							47	0	-124	-	1.10	-47.18	112.50	3600.00	76.31	V
							138	0	33	-	0.30	-12.72	112.50	3600.00	283.10	V
408	9	Fondazione	4-5	7	2.5	Caratt.	0	0	57	-	0.51	-21.80	150.00	3600.00	165.15	V
							63	0	-79	-	0.70	-29.98	150.00	3600.00	120.07	V
							138	0	101	-	0.90	-38.55	150.00	3600.00	93.39	V
						Q.Perm	0	0	37	-	0.33	-14.18	112.50	3600.00	253.87	V
							63	0	-62	-	0.55	-23.64	112.50	3600.00	152.26	V
							138	0	62	-	0.55	-23.69	112.50	3600.00	151.94	V
409	11	Fondazione	5-6	7	2.5	Caratt.	0	0	98	-	0.87	-37.21	150.00	3600.00	96.74	V
							110	0	121	-	1.07	-46.05	150.00	3600.00	78.18	V
							138	0	193	-	1.71	-73.62	150.00	3600.00	48.90	V
						Q.Perm	0	0	67	-	0.59	-25.45	112.50	3600.00	141.47	V
							110	0	41	-	0.36	-15.58	112.50	3600.00	231.01	V
							138	0	90	-	0.80	-34.34	112.50	3600.00	104.84	V
410	13	Fondazione	6-7	7	2.5	Caratt.	0	0	196	-	1.74	-74.78	150.00	3600.00	48.14	V
							110	0	103	-	0.91	-39.33	150.00	3600.00	91.54	V
							138	0	183	-	1.62	-69.59	150.00	3600.00	51.73	V
						Q.Perm	0	0	93	-	0.82	-35.47	112.50	3600.00	101.50	V
							110	0	32	-	0.28	-12.11	112.50	3600.00	297.18	V
							138	0	77	-	0.68	-29.34	112.50	3600.00	122.71	V
411	15	Fondazione	7-8	7	2.5	Caratt.	0	0	189	-	1.67	-71.94	150.00	3600.00	50.04	V
							16	0	110	-	0.97	-41.84	150.00	3600.00	86.04	V
							138	0	73	-	0.65	-27.97	150.00	3600.00	128.72	V
						Q.Perm	0	0	79	-	0.70	-30.20	112.50	3600.00	119.21	V
							16	0	28	-	0.25	-10.72	112.50	3600.00	335.87	V
							138	0	47	-	0.42	-18.01	112.50	3600.00	199.86	V
412	17	Fondazione	8-9	7	2.5	Caratt.	0	0	80	-	0.71	-30.58	150.00	3600.00	117.72	V
							110	0	110	-	0.98	-41.98	150.00	3600.00	85.75	V
							138	0	191	-	1.69	-72.77	150.00	3600.00	49.47	V
						Q.Perm	0	0	46	-	0.41	-17.60	112.50	3600.00	204.49	V
							110	0	33	-	0.29	-12.46	112.50	3600.00	288.91	V
							138	0	86	-	0.76	-32.76	112.50	3600.00	109.89	V
413	19	Fondazione	9-10	7	2.5	Caratt.	0	0	186	-	1.65	-71.02	150.00	3600.00	50.69	V
							110	0	119	-	1.06	-45.56	150.00	3600.00	79.01	V
							138	0	204	-	1.81	-77.93	150.00	3600.00	46.20	V
						Q.Perm	0	0	82	-	0.73	-31.37	112.50	3600.00	114.78	V
							110	0	48	-	0.42	-18.13	112.50	3600.00	198.56	V
							138	0	97	-	0.86	-37.13	112.50	3600.00	96.96	V
414	21	Fondazione	10-11	7	2.5	Caratt.	0	0	205	-	1.81	-77.99	150.00	3600.00	46.16	V
							16	0	127	-	1.13	-48.51	150.00	3600.00	74.21	V
							138	0	59	-	0.52	-22.50	150.00	3600.00	160.00	V
						Q.Perm	0	0	97	-	0.86	-37.16	112.50	3600.00	96.88	V
							16	0	42	-	0.38	-16.15	112.50	3600.00	222.89	V
							138	0	30	-	0.27	-11.55	112.50	3600.00	311.70	V
415	23	Fondazione	11-12	7	2.5	Caratt.	0	0	64	-	0.56	-24.24	150.00	3600.00	148.54	V
							110	0	-151	-	1.34	-57.70	150.00	3600.00	62.39	V
							138	0	-123	-	1.09	-46.75	150.00	3600.00	77.00	V
						Q.Perm	0	0	31	-	0.27	-11.74	112.50	3600.00	306.64	V
							110	0	-103	-	0.92	-39.43	112.50	3600.00	91.31	V
							138	0	-71	-	0.63	-27.01	112.50	3600.00	133.28	V

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416	25	Fondazione	12-13	7	2.5	Caratt.	0	0	-112	-	0.99	-42.72	150.00	3600.00	84.27	V
							110	0	-406	-	3.60	-154.83	150.00	3600.00	23.25	V
							138	0	-381	-	3.38	-145.37	150.00	3600.00	24.76	V
						Q.Perm	0	0	-60	-	0.53	-22.75	112.50	3600.00	158.25	V
							110	0	-212	-	1.88	-80.72	112.50	3600.00	44.60	V
							138	0	-173	-	1.53	-65.95	112.50	3600.00	54.58	V
417	27	Fondazione	13-14	7	2.5	Caratt.	0	0	-336	-	2.98	-127.97	150.00	3600.00	28.13	V
							68	0	-599	-	5.31	-228.36	150.00	3600.00	15.76	V
							166	0	-294	-	2.60	-111.96	150.00	3600.00	32.15	V
						Q.Perm	0	0	-118	-	1.05	-45.01	112.50	3600.00	79.99	V
							68	0	-396	-	3.51	-151.05	112.50	3600.00	23.83	V
							166	0	-170	-	1.51	-64.85	112.50	3600.00	55.51	V
418	29	Fondazione	14-16	7	2.5	Caratt.	0	0	-177	-	1.57	-67.37	150.00	3600.00	53.44	V
							70	0	-461	-	4.09	-175.90	150.00	3600.00	20.47	V
							159	0	315	-	2.79	-120.11	150.00	3600.00	29.97	V
						Q.Perm	0	0	-139	-	1.23	-53.05	112.50	3600.00	67.87	V
							70	0	-346	-	3.07	-132.00	112.50	3600.00	27.27	V
							159	0	117	-	1.04	-44.59	112.50	3600.00	80.74	V
419	31	Fondazione	15-17	7	2.5	Caratt.	0	0	185	-	1.64	-70.36	150.00	3600.00	51.16	V
							15	0	-152	-	1.35	-58.13	150.00	3600.00	61.93	V
							132	0	454	-	4.02	-173.01	150.00	3600.00	20.81	V
						Q.Perm	0	0	-1	-	0.01	-0.30	112.50	3600.00	11951.75	V
							15	0	-50	-	0.45	-19.21	112.50	3600.00	187.37	V
							132	0	311	-	2.76	-118.74	112.50	3600.00	30.32	V
420	33	Fondazione	16-18	7	2.5	Caratt.	0	0	152	-	1.35	-57.91	150.00	3600.00	62.17	V
							15	0	-140	-	1.24	-53.21	150.00	3600.00	67.66	V
							132	0	410	-	3.63	-156.28	150.00	3600.00	23.04	V
						Q.Perm	0	0	-8	-	0.07	-2.95	112.50	3600.00	1221.40	V
							15	0	-55	-	0.48	-20.85	112.50	3600.00	172.64	V
							132	0	282	-	2.50	-107.40	112.50	3600.00	33.52	V
421	35	Fondazione	17-19	7	2.5	Caratt.	0	0	299	-	2.65	-114.18	150.00	3600.00	31.53	V
							102	0	224	-	1.98	-85.36	150.00	3600.00	42.17	V
							132	0	419	-	3.71	-159.71	150.00	3600.00	22.54	V
						Q.Perm	0	0	197	-	1.75	-75.20	112.50	3600.00	47.87	V
							102	0	134	-	1.19	-51.09	112.50	3600.00	70.46	V
							132	0	279	-	2.48	-106.57	112.50	3600.00	33.78	V
422	37	Fondazione	18-20	7	2.5	Caratt.	0	0	288	-	2.56	-109.92	150.00	3600.00	32.75	V
							102	0	196	-	1.74	-74.72	150.00	3600.00	48.18	V
							132	0	379	-	3.36	-144.59	150.00	3600.00	24.90	V
						Q.Perm	0	0	191	-	1.69	-72.85	112.50	3600.00	49.41	V
							102	0	117	-	1.04	-44.76	112.50	3600.00	80.43	V
							132	0	255	-	2.26	-97.30	112.50	3600.00	37.00	V
423	39	Fondazione	19-21	7	2.5	Caratt.	0	0	342	-	3.04	-130.54	150.00	3600.00	27.58	V
							15	0	186	-	1.65	-70.81	150.00	3600.00	50.84	V
							132	0	393	-	3.48	-149.83	150.00	3600.00	24.03	V
						Q.Perm	0	0	223	-	1.98	-85.20	112.50	3600.00	42.25	V
							15	0	110	-	0.98	-42.01	112.50	3600.00	85.70	V
							132	0	271	-	2.41	-103.50	112.50	3600.00	34.78	V
424	41	Fondazione	20-22	7	2.5	Caratt.	0	0	316	-	2.80	-120.32	150.00	3600.00	29.92	V
							15	0	165	-	1.47	-63.02	150.00	3600.00	57.12	V
							132	0	380	-	3.37	-144.76	150.00	3600.00	24.87	V
						Q.Perm	0	0	209	-	1.85	-79.76	112.50	3600.00	45.14	V
							15	0	99	-	0.88	-37.80	112.50	3600.00	95.24	V
							132	0	264	-	2.34	-100.82	112.50	3600.00	35.71	V
425	43	Fondazione	21-23	7	2.5	Caratt.	0	0	371	-	3.29	-141.31	150.00	3600.00	25.48	V
							102	0	203	-	1.80	-77.54	150.00	3600.00	46.43	V
							132	0	385	-	3.41	-146.63	150.00	3600.00	24.55	V
						Q.Perm	0	0	259	-	2.29	-98.62	112.50	3600.00	36.50	V
							102	0	139	-	1.23	-52.87	112.50	3600.00	68.09	V
							132	0	267	-	2.37	-101.97	112.50	3600.00	35.31	V
426	45	Fondazione	22-24	7	2.5	Caratt.	0	0	349	-	3.09	-133.07	150.00	3600.00	27.05	V
							102	0	148	-	1.32	-56.57	150.00	3600.00	63.64	V
							132	0	317	-	2.81	-120.75	150.00	3600.00	29.81	V
						Q.Perm	0	0	246	-	2.18	-93.74	112.50	3600.00	38.40	V
							102	0	97	-	0.86	-36.97	112.50	3600.00	97.37	V
							132	0	219	-	1.94	-83.34	112.50	3600.00	43.20	V
427	47	Fondazione	23-25	7	2.5	Caratt.	0	0	409	-	3.62	-155.82	150.00	3600.00	23.10	V
							102	0	-155	-	1.37	-59.10	150.00	3600.00	60.91	V
							132	0	-72	-	0.64	-27.38	150.00	3600.00	131.48	V
						Q.Perm	0	0	281	-	2.49	-107.14	112.50	3600.00	33.60	V
							102	0	-83	-	0.73	-31.51	112.50	3600.00	114.26	V
							132	0	-6	-	0.05	-2.28	112.50	3600.00	1578.84	V
428	49	Fondazione	24-26	7	2.5	Caratt.	0	0	308	-	2.73	-117.42	150.00	3600.00	30.66	V
							73	0	-254	-	2.25	-96.82	150.00	3600.00	37.18	V
							132	0	62	-	0.55	-23.72	150.00	3600.00	151.79	V
						Q.Perm	0	0	209	-	1.86	-79.83	112.50	3600.00	45.10	V
							73	0	-190	-	1.69	-72.53	112.50	3600.00	49.64	V
							132	0	7	-	0.06	-2.66	112.50	3600.00	1354.58	V
429	51	Fondazione	25-26	7	2.5	Caratt.	0	0	-1085	-	9.62	-413.59	150.00	3600.00	8.70	V
							1575	0	-627	-	5.56	-239.00	150.00	3600.00	15.06	V
							1850	0	-1173	-	10.40	-447.17	150.00	3600.00	8.05	V
						Q.Perm	0	0	-593	-	5.26	-226.08	112.50	3600.00	15.92	V
							1575	0	-456	-	4.04	-173.91	112.50	3600.00	20.70	V
							1850	0	-638	-	5.66	-243.33	112.50	3600.00	14.79	V
430	70	Fondazione	25-28	7	2.5	Caratt.	0	0	89	-	0.79	-34.02	150.00	3600.00	105.81	V

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							19	0	-206	-	1.83	-78.56	150.00	3600.00	45.83	V
							170	0	341	-	3.03	-130.10	150.00	3600.00	27.67	V
						Q.Perm	0	0	16	-	0.15	-6.28	112.50	3600.00	572.90	V
							19	0	-131	-	1.17	-50.13	112.50	3600.00	71.82	V
							170	0	224	-	1.99	-85.49	112.50	3600.00	42.11	V
431	72	Fondazione	26-27	7	2.5	Caratt.	0	0	44	-	0.39	-16.85	150.00	3600.00	213.61	V
							73	0	-232	-	2.06	-88.48	150.00	3600.00	40.69	V
							132	0	271	-	2.41	-103.48	150.00	3600.00	34.79	V
						Q.Perm	0	0	0	-	0.00	-0.14	112.50	3600.00	26227.46	V
							73	0	-169	-	1.50	-64.56	112.50	3600.00	55.76	V
							132	0	186	-	1.65	-71.01	112.50	3600.00	50.70	V
432	74	Fondazione	27-29	7	2.5	Caratt.	0	0	278	-	2.46	-105.98	150.00	3600.00	33.97	V
							15	0	115	-	1.02	-43.88	150.00	3600.00	82.04	V
							132	0	312	-	2.76	-118.84	150.00	3600.00	30.29	V
						Q.Perm	0	0	184	-	1.63	-70.26	112.50	3600.00	51.24	V
							15	0	66	-	0.58	-25.08	112.50	3600.00	143.55	V
							132	0	216	-	1.91	-82.22	112.50	3600.00	43.79	V
433	76	Fondazione	28-30	7	2.5	Caratt.	0	0	362	-	3.21	-138.19	150.00	3600.00	26.05	V
							16	0	164	-	1.45	-62.48	150.00	3600.00	57.62	V
							146	0	326	-	2.89	-124.24	150.00	3600.00	28.98	V
						Q.Perm	0	0	232	-	2.06	-88.59	112.50	3600.00	40.64	V
							16	0	87	-	0.77	-33.23	112.50	3600.00	108.32	V
							146	0	230	-	2.04	-87.61	112.50	3600.00	41.09	V
434	78	Fondazione	29-31	7	2.5	Caratt.	0	0	304	-	2.69	-115.82	150.00	3600.00	31.08	V
							102	0	101	-	0.90	-38.52	150.00	3600.00	93.45	V
							132	0	267	-	2.37	-101.98	150.00	3600.00	35.30	V
						Q.Perm	0	0	214	-	1.90	-81.63	112.50	3600.00	44.10	V
							102	0	62	-	0.55	-23.80	112.50	3600.00	151.28	V
							132	0	187	-	1.66	-71.18	112.50	3600.00	50.57	V
435	80	Fondazione	30-32	7	2.5	Caratt.	0	0	303	-	2.69	-115.48	150.00	3600.00	31.17	V
							106	0	120	-	1.06	-45.62	150.00	3600.00	78.91	V
							137	0	324	-	2.87	-123.43	150.00	3600.00	29.17	V
						Q.Perm	0	0	217	-	1.92	-82.68	112.50	3600.00	43.54	V
							106	0	88	-	0.78	-33.67	112.50	3600.00	106.91	V
							137	0	231	-	2.05	-88.23	112.50	3600.00	40.80	V
436	82	Fondazione	31-33	7	2.5	Caratt.	0	0	283	-	2.51	-107.84	150.00	3600.00	33.38	V
							15	0	110	-	0.97	-41.90	150.00	3600.00	85.91	V
							132	0	265	-	2.35	-101.15	150.00	3600.00	35.59	V
						Q.Perm	0	0	191	-	1.69	-72.72	112.50	3600.00	49.50	V
							15	0	63	-	0.56	-24.11	112.50	3600.00	149.34	V
							132	0	177	-	1.57	-67.43	112.50	3600.00	53.39	V
437	84	Fondazione	32-34	7	2.5	Caratt.	0	0	304	-	2.69	-115.88	150.00	3600.00	31.07	V
							61	0	-207	-	1.84	-79.09	150.00	3600.00	45.52	V
							138	0	294	-	2.61	-112.14	150.00	3600.00	32.10	V
						Q.Perm	0	0	219	-	1.94	-83.45	112.50	3600.00	43.14	V
							61	0	-153	-	1.36	-58.32	112.50	3600.00	61.72	V
							138	0	207	-	1.84	-79.04	112.50	3600.00	45.55	V
438	86	Fondazione	33-35	7	2.5	Caratt.	0	0	268	-	2.37	-102.12	150.00	3600.00	35.25	V
							15	0	98	-	0.87	-37.45	150.00	3600.00	96.13	V
							132	0	249	-	2.21	-95.03	150.00	3600.00	37.88	V
						Q.Perm	0	0	185	-	1.64	-70.61	112.50	3600.00	50.98	V
							15	0	58	-	0.51	-22.10	112.50	3600.00	162.90	V
							132	0	173	-	1.54	-66.14	112.50	3600.00	54.43	V
439	88	Fondazione	34-36	7	2.5	Caratt.	0	0	267	-	2.37	-101.96	150.00	3600.00	35.31	V
							61	0	-209	-	1.85	-79.51	150.00	3600.00	45.28	V
							138	0	265	-	2.35	-101.18	150.00	3600.00	35.58	V
						Q.Perm	0	0	191	-	1.69	-72.88	112.50	3600.00	49.40	V
							61	0	-151	-	1.34	-57.67	112.50	3600.00	62.42	V
							138	0	189	-	1.67	-72.00	112.50	3600.00	50.00	V
440	90	Fondazione	35-37	7	2.5	Caratt.	0	0	273	-	2.42	-104.02	150.00	3600.00	34.61	V
							15	0	103	-	0.91	-39.27	150.00	3600.00	91.67	V
							132	0	278	-	2.47	-106.17	150.00	3600.00	33.91	V
						Q.Perm	0	0	185	-	1.64	-70.45	112.50	3600.00	51.10	V
							15	0	59	-	0.52	-22.57	112.50	3600.00	159.48	V
							132	0	186	-	1.65	-70.95	112.50	3600.00	50.74	V
441	92	Fondazione	36-38	7	2.5	Caratt.	0	0	245	-	2.17	-93.33	150.00	3600.00	38.57	V
							61	0	-220	-	1.95	-83.76	150.00	3600.00	42.98	V
							138	0	256	-	2.27	-97.73	150.00	3600.00	36.84	V
						Q.Perm	0	0	175	-	1.55	-66.73	112.50	3600.00	53.95	V
							61	0	-157	-	1.40	-60.00	112.50	3600.00	60.00	V
							138	0	183	-	1.63	-69.93	112.50	3600.00	51.48	V
442	94	Fondazione	37-39	7	2.5	Caratt.	0	0	285	-	2.53	-108.75	150.00	3600.00	33.10	V
							102	0	132	-	1.17	-50.29	150.00	3600.00	71.59	V
							132	0	305	-	2.70	-116.31	150.00	3600.00	30.95	V
						Q.Perm	0	0	198	-	1.76	-75.52	112.50	3600.00	47.67	V
							102	0	83	-	0.73	-31.59	112.50	3600.00	113.96	V
							132	0	211	-	1.87	-80.60	112.50	3600.00	44.67	V
443	96	Fondazione	38-40	7	2.5	Caratt.	0	0	212	-	1.88	-80.93	150.00	3600.00	44.48	V
							61	0	-214	-	1.90	-81.56	150.00	3600.00	44.14	V
							137	0	253	-	2.24	-96.42	150.00	3600.00	37.34	V
						Q.Perm	0	0	154	-	1.36	-58.55	112.50	3600.00	61.48	V
							61	0	-152	-	1.35	-58.07	112.50	3600.00	61.99	V
							137	0	181	-	1.60	-68.82	112.50	3600.00	52.31	V
444	98	Fondazione	39-41	7	2.5	Caratt.	0	0	328	-	2.91	-125.12	150.00	3600.00	28.77	V
							15	0	149	-	1.32	-56.98	150.00	3600.00	63.18	V

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							132	0	209	-	1.85	-79.62	150.00	3600.00	45.21	V
						Q.Perm	0	0	223	-	1.97	-84.91	112.50	3600.00	42.40	V
							15	0	88	-	0.78	-33.50	112.50	3600.00	107.46	V
							132	0	148	-	1.31	-56.36	112.50	3600.00	63.88	V
445	100	Fondazione	40-42	7	2.5	Caratt.	0	0	194	-	1.72	-74.01	150.00	3600.00	48.64	V
							107	0	146	-	1.29	-55.53	150.00	3600.00	64.83	V
							138	0	383	-	3.40	-146.07	150.00	3600.00	24.65	V
						Q.Perm	0	0	139	-	1.23	-53.08	112.50	3600.00	67.82	V
							107	0	87	-	0.77	-33.13	112.50	3600.00	108.66	V
							138	0	256	-	2.27	-97.61	112.50	3600.00	36.88	V
446	102	Fondazione	41-44	7	2.5	Caratt.	0	0	219	-	1.94	-83.45	150.00	3600.00	43.14	V
							58	0	-324	-	2.87	-123.45	150.00	3600.00	29.16	V
							132	0	80	-	0.71	-30.52	150.00	3600.00	117.97	V
						Q.Perm	0	0	150	-	1.33	-57.10	112.50	3600.00	63.05	V
							58	0	-239	-	2.12	-91.27	112.50	3600.00	39.44	V
							132	0	10	-	0.09	-3.66	112.50	3600.00	984.51	V
447	104	Fondazione	42-43	7	2.5	Caratt.	0	0	374	-	3.31	-142.44	150.00	3600.00	25.27	V
							26	0	272	-	2.41	-103.58	150.00	3600.00	34.76	V
							46	0	270	-	2.39	-102.89	150.00	3600.00	34.99	V
						Q.Perm	0	0	256	-	2.27	-97.56	112.50	3600.00	36.90	V
							26	0	168	-	1.49	-63.88	112.50	3600.00	56.36	V
							46	0	164	-	1.45	-62.50	112.50	3600.00	57.60	V
448	105	Fondazione	43-44	7	2.5	Caratt.	0	0	-1332	-	11.81	-507.90	150.00	3600.00	7.09	V
							225	0	-684	-	6.07	-260.93	150.00	3600.00	13.80	V
							1850	0	-1148	-	10.17	-437.55	150.00	3600.00	8.23	V
						Q.Perm	0	0	-731	-	6.48	-278.64	112.50	3600.00	12.92	V
							225	0	-496	-	4.40	-189.26	112.50	3600.00	19.02	V
							1850	0	-634	-	5.62	-241.65	112.50	3600.00	14.90	V
449	124	Fondazione	43-45	7	2.5	Caratt.	0	0	332	-	2.94	-126.48	150.00	3600.00	28.46	V
							102	0	97	-	0.86	-36.83	150.00	3600.00	97.76	V
							132	0	275	-	2.44	-104.93	150.00	3600.00	34.31	V
						Q.Perm	0	0	205	-	1.81	-78.03	112.50	3600.00	46.13	V
							102	0	49	-	0.43	-18.56	112.50	3600.00	193.95	V
							132	0	180	-	1.60	-68.75	112.50	3600.00	52.36	V
450	126	Fondazione	44-46	7	2.5	Caratt.	0	0	63	-	0.56	-24.09	150.00	3600.00	149.41	V
							58	0	-276	-	2.45	-105.35	150.00	3600.00	34.17	V
							132	0	342	-	3.03	-130.32	150.00	3600.00	27.62	V
						Q.Perm	0	0	2	-	0.02	-0.75	112.50	3600.00	4768.63	V
							58	0	-207	-	1.83	-78.76	112.50	3600.00	45.71	V
							132	0	237	-	2.10	-90.44	112.50	3600.00	39.81	V
451	128	Fondazione	45-47	7	2.5	Caratt.	0	0	313	-	2.78	-119.48	150.00	3600.00	30.13	V
							15	0	111	-	0.99	-42.39	150.00	3600.00	84.93	V
							132	0	299	-	2.65	-114.13	150.00	3600.00	31.54	V
						Q.Perm	0	0	202	-	1.79	-76.86	112.50	3600.00	46.84	V
							15	0	52	-	0.46	-19.86	112.50	3600.00	181.25	V
							132	0	195	-	1.73	-74.23	112.50	3600.00	48.50	V
452	130	Fondazione	46-48	7	2.5	Caratt.	0	0	331	-	2.94	-126.34	150.00	3600.00	28.50	V
							15	0	153	-	1.36	-58.31	150.00	3600.00	61.74	V
							132	0	350	-	3.10	-133.32	150.00	3600.00	27.00	V
						Q.Perm	0	0	227	-	2.01	-86.60	112.50	3600.00	41.57	V
							15	0	97	-	0.86	-36.99	112.50	3600.00	97.32	V
							132	0	242	-	2.15	-92.44	112.50	3600.00	38.95	V
453	132	Fondazione	47-49	7	2.5	Caratt.	0	0	309	-	2.74	-117.77	150.00	3600.00	30.57	V
							15	0	127	-	1.12	-48.38	150.00	3600.00	74.41	V
							132	0	312	-	2.77	-119.10	150.00	3600.00	30.23	V
						Q.Perm	0	0	209	-	1.85	-79.73	112.50	3600.00	45.15	V
							15	0	77	-	0.68	-29.33	112.50	3600.00	122.74	V
							132	0	214	-	1.90	-81.68	112.50	3600.00	44.08	V
454	134	Fondazione	48-50	7	2.5	Caratt.	0	0	379	-	3.36	-144.36	150.00	3600.00	24.94	V
							15	0	192	-	1.70	-73.15	150.00	3600.00	49.22	V
							132	0	363	-	3.22	-138.49	150.00	3600.00	25.99	V
						Q.Perm	0	0	265	-	2.35	-101.20	112.50	3600.00	35.57	V
							15	0	131	-	1.16	-49.85	112.50	3600.00	72.22	V
							132	0	251	-	2.23	-95.74	112.50	3600.00	37.60	V
455	136	Fondazione	49-51	7	2.5	Caratt.	0	0	367	-	3.26	-140.08	150.00	3600.00	25.70	V
							102	0	140	-	1.24	-53.54	150.00	3600.00	67.24	V
							132	0	296	-	2.63	-112.94	150.00	3600.00	31.88	V
						Q.Perm	0	0	250	-	2.21	-95.24	112.50	3600.00	37.80	V
							102	0	74	-	0.66	-28.18	112.50	3600.00	127.74	V
							132	0	186	-	1.65	-70.97	112.50	3600.00	50.73	V
456	138	Fondazione	50-52	7	2.5	Caratt.	0	0	419	-	3.72	-159.94	150.00	3600.00	22.51	V
							15	0	220	-	1.95	-83.94	150.00	3600.00	42.89	V
							132	0	277	-	2.45	-105.54	150.00	3600.00	34.11	V
						Q.Perm	0	0	289	-	2.56	-110.08	112.50	3600.00	32.70	V
							15	0	140	-	1.24	-53.24	112.50	3600.00	67.61	V
							132	0	196	-	1.74	-74.86	112.50	3600.00	48.09	V
457	140	Fondazione	51-53	7	2.5	Caratt.	0	0	372	-	3.30	-141.95	150.00	3600.00	25.36	V
							15	0	186	-	1.65	-70.96	150.00	3600.00	50.73	V
							132	0	285	-	2.53	-108.67	150.00	3600.00	33.13	V
						Q.Perm	0	0	245	-	2.17	-93.39	112.50	3600.00	38.55	V
							15	0	104	-	0.92	-39.61	112.50	3600.00	90.88	V
							132	0	186	-	1.65	-70.79	112.50	3600.00	50.85	V
458	142	Fondazione	52-54	7	2.5	Caratt.	0	0	375	-	3.33	-143.08	150.00	3600.00	25.16	V
							58	0	-206	-	1.82	-78.42	150.00	3600.00	45.91	V
							132	0	248	-	2.20	-94.62	150.00	3600.00	38.05	V
						Q.Perm	0	0	260	-	2.31	-99.24	112.50	3600.00	36.28	V

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							58	0	-160	-	1.42	-61.02	112.50	3600.00	59.00	V
							132	0	145	-	1.29	-55.39	112.50	3600.00	64.99	V
459	144	Fondazione	53-55	7	2.5	Caratt.	0	0	420	-	3.72	-160.04	150.00	3600.00	22.49	V
							102	0	-167	-	1.48	-63.61	150.00	3600.00	56.59	V
							132	0	170	-	1.51	-64.76	150.00	3600.00	55.59	V
						Q.Perm	0	0	286	-	2.53	-108.92	112.50	3600.00	33.05	V
							102	0	-61	-	0.54	-23.10	112.50	3600.00	155.88	V
							132	0	-14	-	0.12	-5.28	112.50	3600.00	681.20	V
460	146	Fondazione	54-56	7	2.5	Caratt.	0	0	391	-	3.47	-149.06	150.00	3600.00	24.15	V
							58	0	-334	-	2.96	-127.46	150.00	3600.00	28.24	V
							132	0	181	-	1.60	-68.87	150.00	3600.00	52.27	V
						Q.Perm	0	0	252	-	2.23	-96.08	112.50	3600.00	37.47	V
							58	0	-243	-	2.16	-92.83	112.50	3600.00	38.78	V
							132	0	4	-	0.03	-1.33	112.50	3600.00	2697.68	V
461	148	Fondazione	55-57	7	2.5	Caratt.	0	0	341	-	3.02	-129.91	150.00	3600.00	27.71	V
							17	0	-172	-	1.52	-65.58	150.00	3600.00	54.90	V
							159	0	-181	-	1.61	-69.14	150.00	3600.00	52.07	V
						Q.Perm	0	0	117	-	1.03	-44.47	112.50	3600.00	80.96	V
							17	0	-53	-	0.47	-20.06	112.50	3600.00	179.46	V
							159	0	-142	-	1.26	-54.30	112.50	3600.00	66.30	V
462	150	Fondazione	56-70	7	2.5	Caratt.	0	0	357	-	3.16	-135.97	150.00	3600.00	26.48	V
							70	0	-468	-	4.15	-178.62	150.00	3600.00	20.15	V
							159	0	-179	-	1.59	-68.34	150.00	3600.00	52.68	V
						Q.Perm	0	0	139	-	1.23	-52.94	112.50	3600.00	68.00	V
							70	0	-350	-	3.11	-133.61	112.50	3600.00	26.94	V
							159	0	-141	-	1.25	-53.57	112.50	3600.00	67.20	V
463	152	Fondazione	57-58	7	2.5	Caratt.	0	0	-299	-	2.65	-113.85	150.00	3600.00	31.62	V
							118	0	-439	-	3.89	-167.21	150.00	3600.00	21.53	V
							166	0	-334	-	2.96	-127.31	150.00	3600.00	28.28	V
						Q.Perm	0	0	-174	-	1.54	-66.36	112.50	3600.00	54.25	V
							118	0	-217	-	1.92	-82.69	112.50	3600.00	43.54	V
							166	0	-117	-	1.04	-44.67	112.50	3600.00	80.59	V
464	154	Fondazione	58-59	7	2.5	Caratt.	0	0	-380	-	3.37	-145.01	150.00	3600.00	24.83	V
							47	0	-397	-	3.52	-151.46	150.00	3600.00	23.77	V
							138	0	-112	-	1.00	-42.82	150.00	3600.00	84.07	V
						Q.Perm	0	0	-173	-	1.53	-65.86	112.50	3600.00	54.66	V
							47	0	-243	-	2.15	-92.66	112.50	3600.00	38.85	V
							138	0	-59	-	0.52	-22.54	112.50	3600.00	159.73	V
465	156	Fondazione	59-60	7	2.5	Caratt.	0	0	-124	-	1.10	-47.33	150.00	3600.00	76.07	V
							32	0	-164	-	1.45	-62.47	150.00	3600.00	57.63	V
							138	0	64	-	0.57	-24.57	150.00	3600.00	146.49	V
						Q.Perm	0	0	-72	-	0.63	-27.30	112.50	3600.00	131.86	V
							32	0	-123	-	1.09	-46.96	112.50	3600.00	76.66	V
							138	0	30	-	0.27	-11.50	112.50	3600.00	312.94	V
466	158	Fondazione	60-61	7	2.5	Caratt.	0	0	64	-	0.57	-24.56	150.00	3600.00	146.58	V
							110	0	130	-	1.15	-49.38	150.00	3600.00	72.91	V
							138	0	205	-	1.82	-78.31	150.00	3600.00	45.97	V
						Q.Perm	0	0	35	-	0.31	-13.42	112.50	3600.00	268.30	V
							110	0	42	-	0.38	-16.16	112.50	3600.00	222.73	V
							138	0	96	-	0.85	-36.63	112.50	3600.00	98.28	V
467	160	Fondazione	61-62	7	2.5	Caratt.	0	0	216	-	1.91	-82.26	150.00	3600.00	43.76	V
							16	0	129	-	1.15	-49.35	150.00	3600.00	72.95	V
							138	0	192	-	1.70	-73.28	150.00	3600.00	49.13	V
						Q.Perm	0	0	102	-	0.91	-39.07	112.50	3600.00	92.14	V
							16	0	52	-	0.46	-19.88	112.50	3600.00	181.08	V
							138	0	86	-	0.76	-32.71	112.50	3600.00	110.05	V
468	162	Fondazione	62-63	7	2.5	Caratt.	0	0	202	-	1.79	-77.03	150.00	3600.00	46.73	V
							16	0	123	-	1.09	-46.73	150.00	3600.00	77.04	V
							138	0	72	-	0.64	-27.53	150.00	3600.00	130.75	V
						Q.Perm	0	0	93	-	0.83	-35.60	112.50	3600.00	101.12	V
							16	0	40	-	0.35	-15.26	112.50	3600.00	235.92	V
							138	0	44	-	0.39	-16.60	112.50	3600.00	216.85	V
469	164	Fondazione	63-64	7	2.5	Caratt.	0	0	84	-	0.75	-32.17	150.00	3600.00	111.89	V
							63	0	-65	-	0.58	-24.88	150.00	3600.00	144.72	V
							138	0	84	-	0.74	-31.90	150.00	3600.00	112.85	V
						Q.Perm	0	0	47	-	0.42	-18.03	112.50	3600.00	199.65	V
							63	0	-55	-	0.49	-20.94	112.50	3600.00	171.91	V
							138	0	47	-	0.41	-17.84	112.50	3600.00	201.78	V
470	166	Fondazione	64-65	7	2.5	Caratt.	0	0	72	-	0.64	-27.45	150.00	3600.00	131.17	V
							110	0	121	-	1.07	-46.03	150.00	3600.00	78.22	V
							138	0	200	-	1.77	-76.25	150.00	3600.00	47.21	V
						Q.Perm	0	0	43	-	0.38	-16.49	112.50	3600.00	218.30	V

							110	0	38	-	0.34	-14.67	112.50	3600.00	245.36	V
							138	0	92	-	0.81	-34.96	112.50	3600.00	102.97	V
471	168	Fondazione	65-66	7	2.5	Caratt.	0	0	190	-	1.69	-72.61	150.00	3600.00	49.58	V
							110	0	129	-	1.14	-49.15	150.00	3600.00	73.25	V
							138	0	216	-	1.91	-82.28	150.00	3600.00	43.75	V
						Q.Perm	0	0	84	-	0.75	-32.11	112.50	3600.00	112.13	V
							110	0	52	-	0.46	-19.87	112.50	3600.00	181.18	V
							138	0	103	-	0.91	-39.26	112.50	3600.00	91.70	V
472	170	Fondazione	66-67	7	2.5	Caratt.	0	0	205	-	1.82	-78.32	150.00	3600.00	45.97	V
							16	0	129	-	1.14	-49.07	150.00	3600.00	73.36	V
							138	0	61	-	0.54	-23.22	150.00	3600.00	155.06	V
						Q.Perm	0	0	97	-	0.86	-36.82	112.50	3600.00	97.77	V
							16	0	42	-	0.37	-16.02	112.50	3600.00	224.69	V
							138	0	32	-	0.28	-12.15	112.50	3600.00	296.25	V
473	172	Fondazione	67-68	7	2.5	Caratt.	0	0	61	-	0.54	-23.14	150.00	3600.00	155.57	V
							110	0	-149	-	1.32	-56.80	150.00	3600.00	63.38	V
							138	0	-121	-	1.07	-46.16	150.00	3600.00	77.99	V
						Q.Perm	0	0	28	-	0.25	-10.80	112.50	3600.00	333.38	V
							110	0	-102	-	0.90	-38.78	112.50	3600.00	92.84	V
							138	0	-70	-	0.62	-26.60	112.50	3600.00	135.36	V
474	174	Fondazione	68-69	7	2.5	Caratt.	0	0	-116	-	1.03	-44.10	150.00	3600.00	81.64	V
							110	0	-402	-	3.56	-153.25	150.00	3600.00	23.49	V
							138	0	-378	-	3.35	-143.94	150.00	3600.00	25.01	V
						Q.Perm	0	0	-63	-	0.56	-23.96	112.50	3600.00	150.27	V
							110	0	-210	-	1.86	-79.97	112.50	3600.00	45.02	V
							138	0	-172	-	1.52	-65.44	112.50	3600.00	55.01	V
475	176	Fondazione	69-70	7	2.5	Caratt.	0	0	-338	-	3.00	-128.81	150.00	3600.00	27.95	V
							51	0	-575	-	5.10	-219.15	150.00	3600.00	16.43	V
							166	0	-299	-	2.65	-113.86	150.00	3600.00	31.62	V
						Q.Perm	0	0	-122	-	1.09	-46.70	112.50	3600.00	77.09	V
							51	0	-361	-	3.20	-137.55	112.50	3600.00	26.17	V
							166	0	-174	-	1.55	-66.51	112.50	3600.00	54.13	V

1.5.1.5 Verifiche SLE - Fessurazione.

Camp : campata alla quale appartengono le aste riportate;
 Asta : numerazione interna dell'asta;
 Imp. : impalcato al quale appartiene l'asta considerata;
 Fili : fili fissi ai quali appartiene l'asta considerata;
 Tipo Sez. : tipo di sezione dell'asta considerata;
 Cop : distanza tra la superficie esterna dell'armatura più prossima alla superficie del calcestruzzo e la superficie stessa del calcestruzzo;
 Comb : tipo di combinazione a cui la verifica è riferita;
 X : distanza dal nodo iniziale misurata lungo l'asse dell'asta;

Sollecitazione : M_{XZ} : valore del Momento Flettente X-Z sollecitante di calcolo;
 Fessura di calcolo: W_k : valore dell'apertura della fessura calcolata;
 Fessura max : $W_{k,max}$: valore della massima apertura ammissibile delle fessure;

Esito : Esito della verifica : V = VERIFICATA;
 : NV = NON VERIFICATA;

Tabella 44.I

Camp	Asta	Imp.	Fili	Tipo Sez.	Cop [cm]	Comb	166 X [cm]	Soll. M_{XZ} [daNm]	Fess. di calc. W_k [mm]	Fessura max $W_{k,max}$ [mm]	S	Esito
404	1	Fondazione	1-2	7	2.5	Freq	0	-205	0.00	0.40	-	V
							51	-365	0.00	0.40	-	V
							166	-159	0.00	0.40	-	V
						Q.Perm	0	-175	0.00	0.30	-	V
							51	-309	0.00	0.30	-	V
							166	-112	0.00	0.30	-	V
405	3	Fondazione	1-15	7	2.5	Freq	0	-150	0.00	0.40	-	V
							122	-48	0.00	0.40	-	V

							159	214	0.00	0.40	-	V
						Q.Perm	0	-143	0.00	0.30	-	V
							122	-32	0.00	0.30	-	V
							159	148	0.00	0.30	-	V
406	5	Fondazio ne	2-3	7	2.5	Freq	0	-203	0.00	0.40	-	V
							31	-269	0.00	0.40	-	V
							138	-50	0.00	0.40	-	V
						Q.Perm	0	-164	0.00	0.30	-	V
							31	-228	0.00	0.30	-	V
							138	-43	0.00	0.30	-	V
407	7	Fondazio ne	3-4	7	2.5	Freq	0	-58	0.00	0.40	-	V
							47	-133	0.00	0.40	-	V
							138	45	0.00	0.40	-	V
						Q.Perm	0	-54	0.00	0.30	-	V
							47	-124	0.00	0.30	-	V
							138	33	0.00	0.30	-	V
408	9	Fondazio ne	4-5	7	2.5	Freq	0	48	0.00	0.40	-	V
							63	-64	0.00	0.40	-	V
							138	75	0.00	0.40	-	V
						Q.Perm	0	37	0.00	0.30	-	V
							63	-62	0.00	0.30	-	V
							138	62	0.00	0.30	-	V
409	11	Fondazio ne	5-6	7	2.5	Freq	0	78	0.00	0.40	-	V
							110	58	0.00	0.40	-	V
							138	117	0.00	0.40	-	V
						Q.Perm	0	67	0.00	0.30	-	V
							110	41	0.00	0.30	-	V
							138	90	0.00	0.30	-	V
410	13	Fondazio ne	6-7	7	2.5	Freq	0	120	0.00	0.40	-	V
							110	46	0.00	0.40	-	V
							138	103	0.00	0.40	-	V
						Q.Perm	0	93	0.00	0.30	-	V
							110	32	0.00	0.30	-	V
							138	77	0.00	0.30	-	V
411	15	Fondazio ne	7-8	7	2.5	Freq	0	107	0.00	0.40	-	V
							16	45	0.00	0.40	-	V
							138	56	0.00	0.40	-	V
						Q.Perm	0	79	0.00	0.30	-	V
							16	28	0.00	0.30	-	V
							138	47	0.00	0.30	-	V
412	17	Fondazio ne	8-9	7	2.5	Freq	0	56	0.00	0.40	-	V
							110	48	0.00	0.40	-	V
							138	113	0.00	0.40	-	V
						Q.Perm	0	46	0.00	0.30	-	V
							110	33	0.00	0.30	-	V
							138	86	0.00	0.30	-	V
413	19	Fondazio ne	9-10	7	2.5	Freq	0	108	0.00	0.40	-	V
							110	63	0.00	0.40	-	V
							138	126	0.00	0.40	-	V
						Q.Perm	0	82	0.00	0.30	-	V
							110	48	0.00	0.30	-	V
							138	97	0.00	0.30	-	V
414	21	Fondazio ne	10-11	7	2.5	Freq	0	126	0.00	0.40	-	V
							16	61	0.00	0.40	-	V
							138	43	0.00	0.40	-	V
						Q.Perm	0	97	0.00	0.30	-	V
							16	42	0.00	0.30	-	V
							138	30	0.00	0.30	-	V
415	23	Fondazio ne	11-12	7	2.5	Freq	0	43	0.00	0.40	-	V
							110	-113	0.00	0.40	-	V
							138	-76	0.00	0.40	-	V
						Q.Perm	0	31	0.00	0.30	-	V
							110	-103	0.00	0.30	-	V

							138	-71	0.00	0.30	-	V
416	25	Fondazio ne	12-13	7	2.5	Freq	0	-68	0.00	0.40	-	V
							110	-256	0.00	0.40	-	V
							138	-214	0.00	0.40	-	V
						Q.Perm	0	-60	0.00	0.30	-	V
							110	-212	0.00	0.30	-	V
							138	-173	0.00	0.30	-	V
417	27	Fondazio ne	13-14	7	2.5	Freq	0	-167	0.00	0.40	-	V
							68	-449	0.00	0.40	-	V
							166	-200	0.00	0.40	-	V
						Q.Perm	0	-118	0.00	0.30	-	V
							68	-396	0.00	0.30	-	V
							166	-170	0.00	0.30	-	V
418	29	Fondazio ne	14-16	7	2.5	Freq	0	-145	0.00	0.40	-	V
							70	-371	0.00	0.40	-	V
							159	174	0.00	0.40	-	V
						Q.Perm	0	-139	0.00	0.30	-	V
							70	-346	0.00	0.30	-	V
							159	117	0.00	0.30	-	V
419	31	Fondazio ne	15-17	7	2.5	Freq	0	51	0.00	0.40	-	V
							15	-62	0.00	0.40	-	V
							132	378	0.00	0.40	-	V
						Q.Perm	0	-1	0.00	0.30	-	V
							15	-50	0.00	0.30	-	V
							132	311	0.00	0.30	-	V
420	33	Fondazio ne	16-18	7	2.5	Freq	0	38	0.00	0.40	-	V
							15	-63	0.00	0.40	-	V
							132	344	0.00	0.40	-	V
						Q.Perm	0	-8	0.00	0.30	-	V
							15	-55	0.00	0.30	-	V
							132	282	0.00	0.30	-	V
421	35	Fondazio ne	17-19	7	2.5	Freq	0	246	0.00	0.40	-	V
							102	167	0.00	0.40	-	V
							132	334	0.00	0.40	-	V
						Q.Perm	0	197	0.00	0.30	-	V
							102	134	0.00	0.30	-	V
							132	279	0.00	0.30	-	V
422	37	Fondazio ne	18-20	7	2.5	Freq	0	239	0.00	0.40	-	V
							102	146	0.00	0.40	-	V
							132	303	0.00	0.40	-	V
						Q.Perm	0	191	0.00	0.30	-	V
							102	117	0.00	0.30	-	V
							132	255	0.00	0.30	-	V
423	39	Fondazio ne	19-21	7	2.5	Freq	0	268	0.00	0.40	-	V
							15	136	0.00	0.40	-	V
							132	318	0.00	0.40	-	V
						Q.Perm	0	223	0.00	0.30	-	V
							15	110	0.00	0.30	-	V
							132	271	0.00	0.30	-	V
424	41	Fondazio ne	20-22	7	2.5	Freq	0	250	0.00	0.40	-	V
							15	122	0.00	0.40	-	V
							132	310	0.00	0.40	-	V
						Q.Perm	0	209	0.00	0.30	-	V
							15	99	0.00	0.30	-	V
							132	264	0.00	0.30	-	V
425	43	Fondazio ne	21-23	7	2.5	Freq	0	301	0.00	0.40	-	V
							102	161	0.00	0.40	-	V
							132	311	0.00	0.40	-	V
						Q.Perm	0	259	0.00	0.30	-	V
							102	139	0.00	0.30	-	V
							132	267	0.00	0.30	-	V
426	45	Fondazio ne	22-24	7	2.5	Freq	0	286	0.00	0.40	-	V

							102	113	0.00	0.40	-	V
							132	255	0.00	0.40	-	V
						Q.Perm	0	246	0.00	0.30	-	V
							102	97	0.00	0.30	-	V
							132	219	0.00	0.30	-	V
427	47	Fondazio ne	23-25	7	2.5	Freq	0	327	0.00	0.40	-	V
							102	-104	0.00	0.40	-	V
							132	-18	0.00	0.40	-	V
						Q.Perm	0	281	0.00	0.30	-	V
							102	-83	0.00	0.30	-	V
							132	-6	0.00	0.30	-	V
428	49	Fondazio ne	24-26	7	2.5	Freq	0	244	0.00	0.40	-	V
							73	-219	0.00	0.40	-	V
							132	21	0.00	0.40	-	V
						Q.Perm	0	209	0.00	0.30	-	V
							73	-190	0.00	0.30	-	V
							132	7	0.00	0.30	-	V
429	51	Fondazio ne	25-26	7	2.5	Freq	0	-738	0.00	0.40	-	V
							1575	-503	0.00	0.40	-	V
							1850	-797	0.00	0.40	-	V
						Q.Perm	0	-593	0.00	0.30	-	V
							1575	-456	0.00	0.30	-	V
							1850	-638	0.00	0.30	-	V
430	70	Fondazio ne	25-28	7	2.5	Freq	0	36	0.00	0.40	-	V
							19	-158	0.00	0.40	-	V
							170	265	0.00	0.40	-	V
						Q.Perm	0	16	0.00	0.30	-	V
							19	-131	0.00	0.30	-	V
							170	224	0.00	0.30	-	V
431	72	Fondazio ne	26-27	7	2.5	Freq	0	11	0.00	0.40	-	V
							73	-196	0.00	0.40	-	V
							132	216	0.00	0.40	-	V
						Q.Perm	0	0	0.00	0.30	-	V
							73	-169	0.00	0.30	-	V
							132	186	0.00	0.30	-	V
432	74	Fondazio ne	27-29	7	2.5	Freq	0	218	0.00	0.40	-	V
							15	79	0.00	0.40	-	V
							132	251	0.00	0.40	-	V
						Q.Perm	0	184	0.00	0.30	-	V
							15	66	0.00	0.30	-	V
							132	216	0.00	0.30	-	V
433	76	Fondazio ne	28-30	7	2.5	Freq	0	277	0.00	0.40	-	V
							16	107	0.00	0.40	-	V
							146	267	0.00	0.40	-	V
						Q.Perm	0	232	0.00	0.30	-	V
							16	87	0.00	0.30	-	V
							146	230	0.00	0.30	-	V
434	78	Fondazio ne	29-31	7	2.5	Freq	0	249	0.00	0.40	-	V
							102	74	0.00	0.40	-	V
							132	217	0.00	0.40	-	V
						Q.Perm	0	214	0.00	0.30	-	V
							102	62	0.00	0.30	-	V
							132	187	0.00	0.30	-	V
435	80	Fondazio ne	30-32	7	2.5	Freq	0	252	0.00	0.40	-	V
							106	100	0.00	0.40	-	V
							137	267	0.00	0.40	-	V
						Q.Perm	0	217	0.00	0.30	-	V
							106	88	0.00	0.30	-	V
							137	231	0.00	0.30	-	V
436	82	Fondazio ne	31-33	7	2.5	Freq	0	225	0.00	0.40	-	V
							15	76	0.00	0.40	-	V
							132	208	0.00	0.40	-	V
						Q.Perm	0	191	0.00	0.30	-	V

							15	63	0.00	0.30	-	V
							132	177	0.00	0.30	-	V
437	84	Fondazio ne	32-34	7	2.5	Freq	0	253	0.00	0.40	-	V
							61	-171	0.00	0.40	-	V
							138	242	0.00	0.40	-	V
						Q.Perm	0	219	0.00	0.30	-	V
							61	-153	0.00	0.30	-	V
							138	207	0.00	0.30	-	V
438	86	Fondazio ne	33-35	7	2.5	Freq	0	216	0.00	0.40	-	V
							15	69	0.00	0.40	-	V
							132	202	0.00	0.40	-	V
						Q.Perm	0	185	0.00	0.30	-	V
							15	58	0.00	0.30	-	V
							132	173	0.00	0.30	-	V
439	88	Fondazio ne	34-36	7	2.5	Freq	0	221	0.00	0.40	-	V
							61	-170	0.00	0.40	-	V
							138	220	0.00	0.40	-	V
						Q.Perm	0	191	0.00	0.30	-	V
							61	-151	0.00	0.30	-	V
							138	189	0.00	0.30	-	V
440	90	Fondazio ne	35-37	7	2.5	Freq	0	217	0.00	0.40	-	V
							15	71	0.00	0.40	-	V
							132	220	0.00	0.40	-	V
						Q.Perm	0	185	0.00	0.30	-	V
							15	59	0.00	0.30	-	V
							132	186	0.00	0.30	-	V
441	92	Fondazio ne	36-38	7	2.5	Freq	0	203	0.00	0.40	-	V
							61	-177	0.00	0.40	-	V
							138	214	0.00	0.40	-	V
						Q.Perm	0	175	0.00	0.30	-	V
							61	-157	0.00	0.30	-	V
							138	183	0.00	0.30	-	V
442	94	Fondazio ne	37-39	7	2.5	Freq	0	231	0.00	0.40	-	V
							102	98	0.00	0.40	-	V
							132	247	0.00	0.40	-	V
						Q.Perm	0	198	0.00	0.30	-	V
							102	83	0.00	0.30	-	V
							132	211	0.00	0.30	-	V
443	96	Fondazio ne	38-40	7	2.5	Freq	0	177	0.00	0.40	-	V
							61	-172	0.00	0.40	-	V
							137	211	0.00	0.40	-	V
						Q.Perm	0	154	0.00	0.30	-	V
							61	-152	0.00	0.30	-	V
							137	181	0.00	0.30	-	V
444	98	Fondazio ne	39-41	7	2.5	Freq	0	261	0.00	0.40	-	V
							15	105	0.00	0.40	-	V
							132	172	0.00	0.40	-	V
						Q.Perm	0	223	0.00	0.30	-	V
							15	88	0.00	0.30	-	V
							132	148	0.00	0.30	-	V
445	100	Fondazio ne	40-42	7	2.5	Freq	0	161	0.00	0.40	-	V
							107	105	0.00	0.40	-	V
							138	305	0.00	0.40	-	V
						Q.Perm	0	139	0.00	0.30	-	V
							107	87	0.00	0.30	-	V
							138	256	0.00	0.30	-	V
446	102	Fondazio ne	41-44	7	2.5	Freq	0	174	0.00	0.40	-	V
							58	-271	0.00	0.40	-	V
							132	27	0.00	0.40	-	V
						Q.Perm	0	150	0.00	0.30	-	V
							58	-239	0.00	0.30	-	V
							132	10	0.00	0.30	-	V
447	104	Fondazio	42-43	7	2.5	Freq	0	301	0.00	0.40	-	V

		ne										
							26	205	0.00	0.40	-	V
							46	203	0.00	0.40	-	V
						Q.Perm	0	256	0.00	0.30	-	V
							26	168	0.00	0.30	-	V
							46	164	0.00	0.30	-	V
448	105	Fondazio ne	43-44	7	2.5	Freq	0	-913	0.00	0.40	-	V
							225	-550	0.00	0.40	-	V
							1850	-788	0.00	0.40	-	V
						Q.Perm	0	-731	0.00	0.30	-	V
							225	-496	0.00	0.30	-	V
							1850	-634	0.00	0.30	-	V
449	124	Fondazio ne	43-45	7	2.5	Freq	0	250	0.00	0.40	-	V
							102	58	0.00	0.40	-	V
							132	211	0.00	0.40	-	V
						Q.Perm	0	205	0.00	0.30	-	V
							102	49	0.00	0.30	-	V
							132	180	0.00	0.30	-	V
450	126	Fondazio ne	44-46	7	2.5	Freq	0	18	0.00	0.40	-	V
							58	-237	0.00	0.40	-	V
							132	275	0.00	0.40	-	V
						Q.Perm	0	2	0.00	0.30	-	V
							58	-207	0.00	0.30	-	V
							132	237	0.00	0.30	-	V
451	128	Fondazio ne	45-47	7	2.5	Freq	0	240	0.00	0.40	-	V
							15	66	0.00	0.40	-	V
							132	232	0.00	0.40	-	V
						Q.Perm	0	202	0.00	0.30	-	V
							15	52	0.00	0.30	-	V
							132	195	0.00	0.30	-	V
452	130	Fondazio ne	46-48	7	2.5	Freq	0	266	0.00	0.40	-	V
							15	114	0.00	0.40	-	V
							132	282	0.00	0.40	-	V
						Q.Perm	0	227	0.00	0.30	-	V
							15	97	0.00	0.30	-	V
							132	242	0.00	0.30	-	V
453	132	Fondazio ne	47-49	7	2.5	Freq	0	247	0.00	0.40	-	V
							15	92	0.00	0.40	-	V
							132	251	0.00	0.40	-	V
						Q.Perm	0	209	0.00	0.30	-	V
							15	77	0.00	0.30	-	V
							132	214	0.00	0.30	-	V
454	134	Fondazio ne	48-50	7	2.5	Freq	0	308	0.00	0.40	-	V
							15	151	0.00	0.40	-	V
							132	293	0.00	0.40	-	V
						Q.Perm	0	265	0.00	0.30	-	V
							15	131	0.00	0.30	-	V
							132	251	0.00	0.30	-	V
455	136	Fondazio ne	49-51	7	2.5	Freq	0	294	0.00	0.40	-	V
							102	95	0.00	0.40	-	V
							132	226	0.00	0.40	-	V
						Q.Perm	0	250	0.00	0.30	-	V
							102	74	0.00	0.30	-	V
							132	186	0.00	0.30	-	V
456	138	Fondazio ne	50-52	7	2.5	Freq	0	338	0.00	0.40	-	V
							15	167	0.00	0.40	-	V
							132	236	0.00	0.40	-	V
						Q.Perm	0	289	0.00	0.30	-	V
							15	140	0.00	0.30	-	V
							132	196	0.00	0.30	-	V
457	140	Fondazio ne	51-53	7	2.5	Freq	0	293	0.00	0.40	-	V
							15	132	0.00	0.40	-	V
							132	233	0.00	0.40	-	V

						Q.Perm	0	245	0.00	0.30	-	V
							15	104	0.00	0.30	-	V
							132	186	0.00	0.30	-	V
458	142	Fondazio ne	52-54	7	2.5	Freq	0	311	0.00	0.40	-	V
							58	-167	0.00	0.40	-	V
							132	189	0.00	0.40	-	V
						Q.Perm	0	260	0.00	0.30	-	V
							58	-160	0.00	0.30	-	V
							132	145	0.00	0.30	-	V
459	144	Fondazio ne	53-55	7	2.5	Freq	0	348	0.00	0.40	-	V
							102	-74	0.00	0.40	-	V
							132	36	0.00	0.40	-	V
						Q.Perm	0	286	0.00	0.30	-	V
							102	-61	0.00	0.30	-	V
							132	-14	0.00	0.30	-	V
460	146	Fondazio ne	54-56	7	2.5	Freq	0	309	0.00	0.40	-	V
							58	-258	0.00	0.40	-	V
							132	54	0.00	0.40	-	V
						Q.Perm	0	252	0.00	0.30	-	V
							58	-243	0.00	0.30	-	V
							132	4	0.00	0.30	-	V
461	148	Fondazio ne	55-57	7	2.5	Freq	0	179	0.00	0.40	-	V
							17	-71	0.00	0.40	-	V
							159	-149	0.00	0.40	-	V
						Q.Perm	0	117	0.00	0.30	-	V
							17	-53	0.00	0.30	-	V
							159	-142	0.00	0.30	-	V
462	150	Fondazio ne	56-70	7	2.5	Freq	0	201	0.00	0.40	-	V
							70	-376	0.00	0.40	-	V
							159	-147	0.00	0.40	-	V
						Q.Perm	0	139	0.00	0.30	-	V
							70	-350	0.00	0.30	-	V
							159	-141	0.00	0.30	-	V
463	152	Fondazio ne	57-58	7	2.5	Freq	0	-205	0.00	0.40	-	V
							118	-273	0.00	0.40	-	V
							166	-166	0.00	0.40	-	V
						Q.Perm	0	-174	0.00	0.30	-	V
							118	-217	0.00	0.30	-	V
							166	-117	0.00	0.30	-	V
464	154	Fondazio ne	58-59	7	2.5	Freq	0	-214	0.00	0.40	-	V
							47	-282	0.00	0.40	-	V
							138	-68	0.00	0.40	-	V
						Q.Perm	0	-173	0.00	0.30	-	V
							47	-243	0.00	0.30	-	V
							138	-59	0.00	0.30	-	V
465	156	Fondazio ne	59-60	7	2.5	Freq	0	-77	0.00	0.40	-	V
							32	-134	0.00	0.40	-	V
							138	43	0.00	0.40	-	V
						Q.Perm	0	-72	0.00	0.30	-	V
							32	-123	0.00	0.30	-	V
							138	30	0.00	0.30	-	V
466	158	Fondazio ne	60-61	7	2.5	Freq	0	47	0.00	0.40	-	V
							110	62	0.00	0.40	-	V
							138	125	0.00	0.40	-	V
						Q.Perm	0	35	0.00	0.30	-	V
							110	42	0.00	0.30	-	V
							138	96	0.00	0.30	-	V
467	160	Fondazio ne	61-62	7	2.5	Freq	0	133	0.00	0.40	-	V
							16	70	0.00	0.40	-	V
							138	113	0.00	0.40	-	V
						Q.Perm	0	102	0.00	0.30	-	V
							16	52	0.00	0.30	-	V
							138	86	0.00	0.30	-	V

468	162	Fondazio ne	62-63	7	2.5	Freq	0	121	0.00	0.40	-	V
							16	57	0.00	0.40	-	V
							138	53	0.00	0.40	-	V
						Q.Perm	0	93	0.00	0.30	-	V
							16	40	0.00	0.30	-	V
							138	44	0.00	0.30	-	V
469	164	Fondazio ne	63-64	7	2.5	Freq	0	58	0.00	0.40	-	V
							63	-57	0.00	0.40	-	V
							138	58	0.00	0.40	-	V
						Q.Perm	0	47	0.00	0.30	-	V
							63	-55	0.00	0.30	-	V
							138	47	0.00	0.30	-	V
470	166	Fondazio ne	64-65	7	2.5	Freq	0	52	0.00	0.40	-	V
							110	55	0.00	0.40	-	V
							138	120	0.00	0.40	-	V
						Q.Perm	0	43	0.00	0.30	-	V
							110	38	0.00	0.30	-	V
							138	92	0.00	0.30	-	V
471	168	Fondazio ne	65-66	7	2.5	Freq	0	111	0.00	0.40	-	V
							110	69	0.00	0.40	-	V
							138	133	0.00	0.40	-	V
						Q.Perm	0	84	0.00	0.30	-	V
							110	52	0.00	0.30	-	V
							138	103	0.00	0.30	-	V
472	170	Fondazio ne	66-67	7	2.5	Freq	0	125	0.00	0.40	-	V
							16	61	0.00	0.40	-	V
							138	44	0.00	0.40	-	V
						Q.Perm	0	97	0.00	0.30	-	V
							16	42	0.00	0.30	-	V
							138	32	0.00	0.30	-	V
473	172	Fondazio ne	67-68	7	2.5	Freq	0	40	0.00	0.40	-	V
							110	-111	0.00	0.40	-	V
							138	-75	0.00	0.40	-	V
						Q.Perm	0	28	0.00	0.30	-	V
							110	-102	0.00	0.30	-	V
							138	-70	0.00	0.30	-	V
474	174	Fondazio ne	68-69	7	2.5	Freq	0	-71	0.00	0.40	-	V
							110	-253	0.00	0.40	-	V
							138	-212	0.00	0.40	-	V
						Q.Perm	0	-63	0.00	0.30	-	V
							110	-210	0.00	0.30	-	V
							138	-172	0.00	0.30	-	V
475	176	Fondazio ne	69-70	7	2.5	Freq	0	-171	0.00	0.40	-	V
							51	-418	0.00	0.40	-	V
							166	-205	0.00	0.40	-	V
						Q.Perm	0	-122	0.00	0.30	-	V
							51	-361	0.00	0.30	-	V
							166	-174	0.00	0.30	-	V

1.5.2 Aste in Legno.

Dati 45 del Tabulato.

Colonna 1 Primo Impa[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x220** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 3760 mm] - **R 500x220**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.128 (fs=7.79)
 Sforzo Normale di Progetto [daN] : 7623 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 359
 Momento Flettente Mz di Progetto [daNm] : -860

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.69
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.047
 fs : 21.41
 Tensione di Progetto relativa a My [N/mm²] : 0.89
 Tensione di Progetto relativa a Mz [N/mm²] : 0.94
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.082
 fs : 12.25
 Coefficiente di Sfruttamento : 0.128
 fs : 7.79

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 3760 mm] - **R 500x220**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.063 (fs=15.942)
 Taglio Ty di Progetto [daN] : -47
 Taglio Tz di Progetto [daN] : -126
 Momento Torcente Mt di Progetto [daNm] : -860

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.01
 Tensione di Progetto relativa a Tz [N/mm²] : 0.02
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.007
 fs : 144.91
 Tensione di Progetto [N/mm²] : 0.22
 Modulo di resistenza a torsione [mm³] : 6381856.5
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.063
 fs : 15.95
 Coefficiente di Sfruttamento a taglio+torsione : 0.063
 fs : 15.94

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 41.44
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.66
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 50
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.74
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.94
Coefficiente di sfruttamento nel piano XY	: 0.127	Coefficiente di sfruttamento nel piano XZ	: 0.130
fs	: 7.671		

Colonna 2 Primo Impa[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.366 (fs=2.733)

Sforzo Normale di Progetto [daN] : -1191 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -2164
 Momento Flettente Mz di Progetto [daNm] : -25

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.25
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.014
 fs : 73.4
 Tensione di Progetto relativa a My [N/mm²] : 6.76
 Tensione di Progetto relativa a Mz [N/mm²] : 0.26
 Tensione Resistente relativa a My [N/mm²] : 18.96
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.366
 fs : 2.73
 Coefficiente di Sfruttamento a pressoflessione : 0.366
 fs : 2.73

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 31 [CAR] [ST] " - Coeff. Sfruttamento : 0.054 (fs=18.641)

Taglio Ty di Progetto [daN] : -2
 Taglio Tz di Progetto [daN] : 373
 Momento Torcente Mt di Progetto [daNm] : 3

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.12
 Tensione tang. Resistente [N/mm²] : 2.17
 Coefficiente di Sfruttamento a taglio : 0.054
 fs : 18.64

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.420	Coefficiente di sfruttamento nel piano XZ	: 0.397
fs	: 2.382		

Colonna 2 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.385 (fs=2.599)

Sforzo Normale di Progetto [daN] : 391 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -2296
 Momento Flettente Mz di Progetto [daNm] : 3

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.08

Tensione Resistente [N/mm ²]	: 15.17
Coefficiente di Sfruttamento a trazione	: 0.005
fs	: 186.1
Tensione di Progetto relativa a My [N/mm ²]	: 7.18
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.03
Tensione Resistente relativa a My [N/mm ²]	: 18.96
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.379
fs	: 2.64
Coefficiente di Sfruttamento	: 0.385
fs	: 2.6

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.052 (fs=19.385)

Taglio Ty di Progetto [daN]	: -14
Taglio Tz di Progetto [daN]	: -438
Momento Torcente Mt di Progetto [daNm]	: 31

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.14
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.052
fs	: 19.38

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.387	Coefficiente di sfruttamento nel piano XZ	: 0.363
fs	: 2.585		

Colonna 3 Primo Impa[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.584 (fs=1.713)

Sforzo Normale di Progetto [daN]	: -1042 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 3532
Momento Flettente Mz di Progetto [daNm]	: -4

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.22
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.012
fs	: 83.86
Tensione di Progetto relativa a My [N/mm ²]	: 11.04
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.04
Tensione Resistente relativa a My [N/mm ²]	: 18.96
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03

Coefficiente di Sfruttamento a flessione	: 0.584
fs	: 1.71
Coefficiente di Sfruttamento a pressoflessione	: 0.584
fs	: 1.71

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - R 120x400	
<i>Comb. più gravosa : " Comb 31 [CAR] [ST] " - Coeff. Sfruttamento : 0.064 (fs=15.638)</i>	
Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: 445
Momento Torcente Mt di Progetto [daNm]	: 1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0
Tensione di Progetto relativa a Tz [N/mm²]	: 0.14
Tensione tang. Resistente [N/mm²]	: 2.17
Coefficiente di Sfruttamento a taglio	: 0.064
fs	: 15.64

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.604	Coefficiente di sfruttamento nel piano XZ	: 0.596
fs	: 1.657		

Colonna 3 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - R 120x400	
<i>Comb. più gravosa : " Comb 44 [SLV] [IN] " - Coeff. Sfruttamento : 0.183 (fs=5.478)</i>	
Sforzo Normale di Progetto [daN]	: -1096 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -1091
Momento Flettente Mz di Progetto [daNm]	: -7

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.23
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.013
fs	: 79.74
Tensione di Progetto relativa a My [N/mm²]	: 3.41
Tensione di Progetto relativa a Mz [N/mm²]	: 0.07
Tensione Resistente relativa a My [N/mm²]	: 18.96
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.182
fs	: 5.48
Coefficiente di Sfruttamento a pressoflessione	: 0.183
fs	: 5.48

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.05 (fs=19.882)
 Taglio Ty di Progetto [daN] : -10
 Taglio Tz di Progetto [daN] : 427
 Momento Torcente Mt di Progetto [daNm] : 22

Tipo Verifica : TAGLIO
 Tensione di Progetto relativa a Ty [N/mm²] : 0.00
 Tensione di Progetto relativa a Tz [N/mm²] : 0.13
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.05
 fs : 19.88

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 45
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.212	Coefficiente di sfruttamento nel piano XZ	: 0.196
fs	: 4.713		

Colonna 4 Primo Impa[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)
 L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.627 (fs=1.595)
 Sforzo Normale di Progetto [daN] : -1137 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 3761
 Momento Flettente Mz di Progetto [daNm] : 19

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1
 Tensione di Progetto [N/mm²] : -0.24
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.013
 fs : 76.87
 Tensione di Progetto relativa a My [N/mm²] : 11.75
 Tensione di Progetto relativa a Mz [N/mm²] : 0.19
 Tensione Resistente relativa a My [N/mm²] : 18.96
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.627
 fs : 1.6
 Coefficiente di Sfruttamento a pressoflessione : 0.627
 fs : 1.6

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**
Comb. più gravosa : " Comb 31 [CAR] [ST] " - Coeff. Sfruttamento : 0.068 (fs=14.812)
 Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : 469
 Momento Torcente Mt di Progetto [daNm] : 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.15
Tensione tang. Resistente [N/mm ²]	: 2.17
Coefficiente di Sfruttamento a taglio	: 0.068
fs	: 14.81

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.649	Coefficiente di sfruttamento nel piano XZ	: 0.640
fs	: 1.542		

Colonna 4 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)
L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.131 (fs=7.608)

Sforzo Normale di Progetto [daN]	: -248 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 785
Momento Flettente Mz di Progetto [daNm]	: -6

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.05
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.003
fs	: 352.56
Tensione di Progetto relativa a My [N/mm ²]	: 2.45
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.06
Tensione Resistente relativa a My [N/mm ²]	: 18.96
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.131
fs	: 7.61
Coefficiente di Sfruttamento a pressoflessione	: 0.131
fs	: 7.61

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.042 (fs=23.801)

Taglio Ty di Progetto [daN]	: -9
Taglio Tz di Progetto [daN]	: 357
Momento Torcente Mt di Progetto [daNm]	: 19

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.11
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.042
fs	: 23.8

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 44
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.157	Coefficiente di sfruttamento nel piano XZ	: 0.142
fs	: 6.379		

Colonna 5 Primo Impa[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.667 (fs=1.498)

Sforzo Normale di Progetto [daN]	: -1053 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 4005
Momento Flettente Mz di Progetto [daNm]	: 20

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.22
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.012
fs	: 82.98
Tensione di Progetto relativa a My [N/mm²]	: 12.52
Tensione di Progetto relativa a Mz [N/mm²]	: 0.21
Tensione Resistente relativa a My [N/mm²]	: 18.96
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.667
fs	: 1.5
Coefficiente di Sfruttamento a pressoflessione	: 0.667
fs	: 1.5

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.146 (fs=6.848)

Taglio Ty di Progetto [daN]	: -11
Taglio Tz di Progetto [daN]	: 1241
Momento Torcente Mt di Progetto [daNm]	: 20

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm²]	: 0.39
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.146
fs	: 6.85

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99

Coefficiente di sfruttamento nel piano XY : 0.688
fs : 1.454

Coefficiente di sfruttamento nel piano XZ : 0.679

Colonna 5 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 25 [SLD] [IN] " - Coeff. Sfruttamento : 0.166 (fs=6.017)

Sforzo Normale di Progetto [daN] : -229 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : 995
Momento Flettente Mz di Progetto [daNm] : 6

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.05
Tensione Resistente [N/mm²] : 18.21
Coefficiente di Sfruttamento a compressione : 0.003
fs : 381.44
Tensione di Progetto relativa a My [N/mm²] : 3.11
Tensione di Progetto relativa a Mz [N/mm²] : 0.06
Tensione Resistente relativa a My [N/mm²] : 18.96
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.166
fs : 6.02
Coefficiente di Sfruttamento a pressoflessione : 0.166
fs : 6.02

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.05 (fs=19.97)

Taglio Ty di Progetto [daN] : -9
Taglio Tz di Progetto [daN] : 425
Momento Torcente Mt di Progetto [daNm] : 21

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
Tensione di Progetto relativa a Tz [N/mm²] : 0.13
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.05
fs : 19.97

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 50
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.182	Coefficiente di sfruttamento nel piano XZ	: 0.172
fs	: 5.492		

Colonna 6 Primo Impa[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.614 (fs=1.629)
 Sforzo Normale di Progetto [daN] : -709 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 3686
 Momento Flettente Mz di Progetto [daNm] : 18

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.15
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.008
 fs : 123.29
 Tensione di Progetto relativa a My [N/mm²] : 11.52
 Tensione di Progetto relativa a Mz [N/mm²] : 0.18
 Tensione Resistente relativa a My [N/mm²] : 18.96
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.614
 fs : 1.63
 Coefficiente di Sfruttamento a pressoflessione : 0.614
 fs : 1.63

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**
Comb. più gravosa : " Comb 31 [CAR] [ST] " - Coeff. Sfruttamento : 0.07 (fs=14.227)
 Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : 489
 Momento Torcente Mt di Progetto [daNm] : 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.15
 Tensione tang. Resistente [N/mm²] : 2.17
 Coefficiente di Sfruttamento a taglio : 0.07
 fs : 14.23

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.628	Coefficiente di sfruttamento nel piano XZ	: 0.622
fs	: 1.594		

Colonna 6 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**
Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.129 (fs=7.741)
 Sforzo Normale di Progetto [daN] : -84 (COMPRESSIONE)

Momento Flettente My di Progetto [daNm] : 774
 Momento Flettente Mz di Progetto [daNm] : -4

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.02
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.001
 fs : 1000
 Tensione di Progetto relativa a My [N/mm²] : 2.42
 Tensione di Progetto relativa a Mz [N/mm²] : 0.04
 Tensione Resistente relativa a My [N/mm²] : 18.96
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.129
 fs : 7.74
 Coefficiente di Sfruttamento a pressoflessione : 0.129
 fs : 7.74

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.051 (fs=19.564)

Taglio Ty di Progetto [daN] : -8
 Taglio Tz di Progetto [daN] : 434
 Momento Torcente Mt di Progetto [daNm] : 17

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
 Tensione di Progetto relativa a Tz [N/mm²] : 0.14
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.051
 fs : 19.56

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 26
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.146	Coefficiente di sfruttamento nel piano XZ	: 0.136
fs	: 6.870		

Colonna 7 Primo Impa[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.624 (fs=1.602)

Sforzo Normale di Progetto [daN] : -1440 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 3746
 Momento Flettente Mz di Progetto [daNm] : 18

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.3
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.016

fs	: 60.67
Tensione di Progetto relativa a My [N/mm ²]	: 11.71
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.19
Tensione Resistente relativa a My [N/mm ²]	: 18.96
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.624
fs	: 1.6
Coefficiente di Sfruttamento a pressoflessione	: 0.624
fs	: 1.6

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 31 [CAR] [ST] " - Coeff. Sfruttamento : 0.071 (fs=14.022)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: 496
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.15
Tensione tang. Resistente [N/mm ²]	: 2.17
Coefficiente di Sfruttamento a taglio	: 0.071
fs	: 14.02

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.652	Coefficiente di sfruttamento nel piano XZ	: 0.640
fs	: 1.535		

Colonna 7 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.142 (fs=7.022)

Sforzo Normale di Progetto [daN]	: 277 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 769
Momento Flettente Mz di Progetto [daNm]	: 32

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.06
Tensione Resistente [N/mm ²]	: 15.17
Coefficiente di Sfruttamento a trazione	: 0.004
fs	: 262.92
Tensione di Progetto relativa a My [N/mm ²]	: 2.4
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.34
Tensione Resistente relativa a My [N/mm ²]	: 18.96
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.139
fs	: 7.22

Coefficiente di Sfruttamento : 0.142
fs : 7.02

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**
Comb. più gravosa : " Comb 31 [CAR] [ST] " - Coeff. Sfruttamento : 0.026 (fs=39.043)
Taglio Ty di Progetto [daN] : 0
Taglio Tz di Progetto [daN] : 178
Momento Torcente Mt di Progetto [daNm] : 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
Tensione di Progetto relativa a Tz [N/mm²] : 0.06
Tensione tang. Resistente [N/mm²] : 2.17
Coefficiente di Sfruttamento a taglio : 0.026
fs : 39.04

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 37
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.159	Coefficiente di sfruttamento nel piano XZ	: 0.146
fs	: 6.292		

Colonna 8 Primo Impa[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.608 (fs=1.644)
Sforzo Normale di Progetto [daN] : -1144 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : 3645
Momento Flettente Mz di Progetto [daNm] : 20

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.24
Tensione Resistente [N/mm²] : 18.21
Coefficiente di Sfruttamento a compressione : 0.013
fs : 76.41
Tensione di Progetto relativa a My [N/mm²] : 11.39
Tensione di Progetto relativa a Mz [N/mm²] : 0.21
Tensione Resistente relativa a My [N/mm²] : 18.96
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.608
fs : 1.64
Coefficiente di Sfruttamento a pressoflessione : 0.608
fs : 1.64

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**
Comb. più gravosa : " Comb 31 [CAR] [ST] " - Coeff. Sfruttamento : 0.071 (fs=14.027)

Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : 496
 Momento Torcente Mt di Progetto [daNm] : 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.15
 Tensione tang. Resistente [N/mm²] : 2.17
 Coefficiente di Sfruttamento a taglio : 0.071
 fs : 14.03

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.630	Coefficiente di sfruttamento nel piano XZ	: 0.621
fs	: 1.587		

Colonna 8 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.143 (fs=7.002)

Sforzo Normale di Progetto [daN] : -421 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 811
 Momento Flettente Mz di Progetto [daNm] : 25

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.09
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.005
 fs : 207.67
 Tensione di Progetto relativa a My [N/mm²] : 2.53
 Tensione di Progetto relativa a Mz [N/mm²] : 0.26
 Tensione Resistente relativa a My [N/mm²] : 18.96
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.143
 fs : 7
 Coefficiente di Sfruttamento a pressoflessione : 0.143
 fs : 7

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 31 [CAR] [ST] " - Coeff. Sfruttamento : 0.026 (fs=39.206)

Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : 177
 Momento Torcente Mt di Progetto [daNm] : 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.06

Tensione tang. Resistente [N/mm ²]	: 2.17
Coefficiente di Sfruttamento a taglio	: 0.026
fs	: 39.21

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 40
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.153	Coefficiente di sfruttamento nel piano XZ	: 0.148
fs	: 6.519		

Colonna 9 Primo Impa[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.518 (fs=1.93)

Sforzo Normale di Progetto [daN]	: -724 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 3104
Momento Flettente Mz di Progetto [daNm]	: 17

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.15
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.008
fs	: 120.76
Tensione di Progetto relativa a My [N/mm ²]	: 9.7
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.18
Tensione Resistente relativa a My [N/mm ²]	: 18.96
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.518
fs	: 1.93
Coefficiente di Sfruttamento a pressoflessione	: 0.518
fs	: 1.93

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 31 [CAR] [ST] " - Coeff. Sfruttamento : 0.07 (fs=14.223)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: 489
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.15
Tensione tang. Resistente [N/mm ²]	: 2.17
Coefficiente di Sfruttamento a taglio	: 0.07
fs	: 14.22

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
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Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.532	Coefficiente di sfruttamento nel piano XZ	: 0.526
fs	: 1.880		

Colonna 9 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.107 (fs=9.347)

Sforzo Normale di Progetto [daN]	: -873 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 602
Momento Flettente Mz di Progetto [daNm]	: 21

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.18
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.01
fs	: 100.11
Tensione di Progetto relativa a My [N/mm²]	: 1.88
Tensione di Progetto relativa a Mz [N/mm²]	: 0.22
Tensione Resistente relativa a My [N/mm²]	: 18.96
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.107
fs	: 9.36
Coefficiente di Sfruttamento a pressoflessione	: 0.107
fs	: 9.35

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.028 (fs=35.545)

Taglio Ty di Progetto [daN]	: -7
Taglio Tz di Progetto [daN]	: 375
Momento Torcente Mt di Progetto [daNm]	: 16

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm²]	: 0.12
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.044
fs	: 22.66
Tensione di Progetto [N/mm²]	: 0.1
Modulo di resistenza a torsione [mm³]	: 1627118.63
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.026
fs	: 38.19
Coefficiente di Sfruttamento a taglio+torsione	: 0.028
fs	: 35.54

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
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Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 38
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.136	Coefficiente di sfruttamento nel piano XZ	: 0.120
fs	: 7.374		

Colonna 10 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.474 (fs=2.11)

Sforzo Normale di Progetto [daN]	: -1425 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 2836
Momento Flettente Mz di Progetto [daNm]	: 17

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.3
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.016
fs	: 61.31
Tensione di Progetto relativa a My [N/mm²]	: 8.86
Tensione di Progetto relativa a Mz [N/mm²]	: 0.18
Tensione Resistente relativa a My [N/mm²]	: 18.96
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.474
fs	: 2.11
Coefficiente di Sfruttamento a pressoflessione	: 0.474
fs	: 2.11

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 31 [CAR] [ST] " - Coeff. Sfruttamento : 0.068 (fs=14.644)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: 475
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0
Tensione di Progetto relativa a Tz [N/mm²]	: 0.15
Tensione tang. Resistente [N/mm²]	: 2.17
Coefficiente di Sfruttamento a taglio	: 0.068
fs	: 14.64

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.501	Coefficiente di sfruttamento nel piano XZ	: 0.490
fs	: 1.995		

Colonna 10 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)
L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.123 (fs=8.129)

Sforzo Normale di Progetto [daN] : -1002 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : -705
Momento Flettente Mz di Progetto [daNm] : -18

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.21
Tensione Resistente [N/mm²] : 18.21
Coefficiente di Sfruttamento a compressione : 0.011
fs : 87.18
Tensione di Progetto relativa a My [N/mm²] : 2.2
Tensione di Progetto relativa a Mz [N/mm²] : 0.19
Tensione Resistente relativa a My [N/mm²] : 18.96
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.123
fs : 8.14
Coefficiente di Sfruttamento a pressoflessione : 0.123
fs : 8.13

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.034 (fs=29.235)

Taglio Ty di Progetto [daN] : 9
Taglio Tz di Progetto [daN] : -291
Momento Torcente Mt di Progetto [daNm] : 19

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
Tensione di Progetto relativa a Tz [N/mm²] : 0.09
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.034
fs : 29.24

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 45
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.148	Coefficiente di sfruttamento nel piano XZ	: 0.135
fs	: 6.748		

Colonna 11 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)
L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.395 (fs=2.529)
 Sforzo Normale di Progetto [daN] : -1525 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 2354
 Momento Flettente Mz di Progetto [daNm] : 19

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.32
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.017
 fs : 57.3
 Tensione di Progetto relativa a My [N/mm²] : 7.36
 Tensione di Progetto relativa a Mz [N/mm²] : 0.2
 Tensione Resistente relativa a My [N/mm²] : 18.96
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.395
 fs : 2.53
 Coefficiente di Sfruttamento a pressoflessione : 0.395
 fs : 2.53

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**
Comb. più gravosa : " Comb 31 [CAR] [ST] " - Coeff. Sfruttamento : 0.067 (fs=14.997)
 Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : 464
 Momento Torcente Mt di Progetto [daNm] : 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.14
 Tensione tang. Resistente [N/mm²] : 2.17
 Coefficiente di Sfruttamento a taglio : 0.067
 fs : 15

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.425	Coefficiente di sfruttamento nel piano XZ	: 0.413
fs	: 2.356		

Colonna 11 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**
Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.084 (fs=11.841)
 Sforzo Normale di Progetto [daN] : -303 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 433
 Momento Flettente Mz di Progetto [daNm] : 36

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.003
fs	: 288.51
Tensione di Progetto relativa a My [N/mm ²]	: 1.35
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.38
Tensione Resistente relativa a My [N/mm ²]	: 18.96
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.084
fs	: 11.84
Coefficiente di Sfruttamento a pressoflessione	: 0.084
fs	: 11.84

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.034 (fs=29.38)

Taglio Ty di Progetto [daN]	: -8
Taglio Tz di Progetto [daN]	: 266
Momento Torcente Mt di Progetto [daNm]	: 17

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.08
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.031
fs	: 31.92
Tensione di Progetto [N/mm ²]	: 0.13
Modulo di resistenza a torsione [mm ³]	: 1627118.63
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.033
fs	: 30.25
Coefficiente di Sfruttamento a taglio+torsione	: 0.034
fs	: 29.38

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 37
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.103	Coefficiente di sfruttamento nel piano XZ	: 0.091
fs	: 9.690		

Colonna 12 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.336 (fs=2.979)

Sforzo Normale di Progetto [daN]	: -1706 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 1995
Momento Flettente Mz di Progetto [daNm]	: 18

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.36
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.02
fs	: 51.23
Tensione di Progetto relativa a My [N/mm ²]	: 6.23
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.19
Tensione Resistente relativa a My [N/mm ²]	: 18.96
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.335
fs	: 2.98
Coefficiente di Sfruttamento a pressoflessione	: 0.336
fs	: 2.98

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 31 [CAR] [ST] " - Coeff. Sfruttamento : 0.063 (fs=15.77)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: 441
Momento Torcente Mt di Progetto [daNm]	: -1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.14
Tensione tang. Resistente [N/mm ²]	: 2.17
Coefficiente di Sfruttamento a taglio	: 0.063
fs	: 15.77

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.368	Coefficiente di sfruttamento nel piano XZ	: 0.355
fs	: 2.716		

Colonna 12 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.095 (fs=10.477)

Sforzo Normale di Progetto [daN]	: -307 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -507
Momento Flettente Mz di Progetto [daNm]	: -33

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.004
fs	: 285.13
Tensione di Progetto relativa a My [N/mm ²]	: 1.58

Tensione di Progetto relativa a M_z [N/mm ²]	: 0.34
Tensione Resistente relativa a M_y [N/mm ²]	: 18.96
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.095
fs	: 10.48
Coefficiente di Sfruttamento a pressoflessione	: 0.095
fs	: 10.48

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.028 (fs=35.571)

Taglio Ty di Progetto [daN]	: -7
Taglio Tz di Progetto [daN]	: -375
Momento Torcente Mt di Progetto [daNm]	: -15

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.12
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.044
fs	: 22.66
Tensione di Progetto [N/mm ²]	: 0.1
Modulo di resistenza a torsione [mm ³]	: 1627118.63
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.026
fs	: 38.22
Coefficiente di Sfruttamento a taglio+torsione	: 0.028
fs	: 35.57

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 38
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.116	Coefficiente di sfruttamento nel piano XZ	: 0.099
fs	: 8.607		

Colonna 13 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.229 (fs=4.36)

Sforzo Normale di Progetto [daN]	: -1577 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 1359
Momento Flettente Mz di Progetto [daNm]	: 14

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.33
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.018
fs	: 55.41
Tensione di Progetto relativa a My [N/mm ²]	: 4.25

Tensione di Progetto relativa a M_z [N/mm ²]	: 0.15
Tensione Resistente relativa a M_y [N/mm ²]	: 18.96
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.229
f_s	: 4.37
Coefficiente di Sfruttamento a pressoflessione	: 0.229
f_s	: 4.36

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.068 ($f_s=14.713$)

Taglio T_y di Progetto [daN]	: 12
Taglio T_z di Progetto [daN]	: 577
Momento Torcente M_t di Progetto [daNm]	: -22

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.00
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.18
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.068
f_s	: 14.71

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente K_c nel piano XY	: 0.59	Coefficiente K_c nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.259	Coefficiente di sfruttamento nel piano XZ	: 0.247
f_s	: 3.854		

Colonna 13 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.116 ($f_s=8.586$)

Sforzo Normale di Progetto [daN]	: 608 (TRAZIONE)
Momento Flettente M_y di Progetto [daNm]	: -587
Momento Flettente M_z di Progetto [daNm]	: -31

Tipo Verifica : TRAZIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: 0.13
Tensione Resistente [N/mm ²]	: 15.17
Coefficiente di Sfruttamento a trazione	: 0.008
f_s	: 119.72
Tensione di Progetto relativa a M_y [N/mm ²]	: 1.83
Tensione di Progetto relativa a M_z [N/mm ²]	: 0.33
Tensione Resistente relativa a M_y [N/mm ²]	: 18.96
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.108
f_s	: 9.25
Coefficiente di Sfruttamento	: 0.116
f_s	: 8.59

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.035 (fs=28.936)

Taglio Ty di Progetto [daN]	: 10
Taglio Tz di Progetto [daN]	: -293
Momento Torcente Mt di Progetto [daNm]	: 22

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm²]	: 0.09
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.035
fs	: 28.94

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 38
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.122	Coefficiente di sfruttamento nel piano XZ	: 0.096
fs	: 8.180		

Colonna 14 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x220** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x220**

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.069 (fs=14.413)

Sforzo Normale di Progetto [daN]	: -22 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 44
Momento Flettente Mz di Progetto [daNm]	: -1115

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.00
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.000
fs	: 1000
Tensione di Progetto relativa a My [N/mm²]	: 0.11
Tensione di Progetto relativa a Mz [N/mm²]	: 1.22
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.069
fs	: 14.41
Coefficiente di Sfruttamento a pressoflessione	: 0.069
fs	: 14.41

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 3760 mm] - **R 500x220**

Comb. più gravosa : " Comb 39 [SLV] [IN] " - Coeff. Sfruttamento : 0.042 (fs=24)

Taglio Ty di Progetto [daN]	: 354
Taglio Tz di Progetto [daN]	: -60

Momento Torcente Mt di Progetto [daNm]	: 612	
Tipo Verifica		: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.05	
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.01	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a taglio	: 0.018	
fs	: 54.2	
Tensione di Progetto [N/mm ²]	: 0.15	
Modulo di resistenza a torsione [mm ³]	: 6381856.5	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a torsione	: 0.041	
fs	: 24.2	
Coefficiente di Sfruttamento a taglio+torsione	: 0.042	
fs	: 24	

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 41.44
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.66
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.74
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.94
Coefficiente di sfruttamento nel piano XY	: 0.073	Coefficiente di sfruttamento nel piano XZ	: 0.074
fs	: 13.534		

Colonna 79 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)
L= 2500 mm - **R 500x220** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2500 mm / 2500 mm] - **R 500x220**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.132 (fs=7.603)

Sforzo Normale di Progetto [daN]	: -2420 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -828
Momento Flettente Mz di Progetto [daNm]	: -702

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.22
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.012
fs	: 82.77
Tensione di Progetto relativa a My [N/mm ²]	: 2.05
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.77
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.131
fs	: 7.61
Coefficiente di Sfruttamento a pressoflessione	: 0.132
fs	: 7.6

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2500 mm / 2500 mm] - **R 500x220**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.035 (fs=28.203)

Taglio Ty di Progetto [daN]	: -322
Taglio Tz di Progetto [daN]	: 73

Momento Torcente Mt di Progetto [daNm]	: 581	
Tipo Verifica		: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04	
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.01	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a taglio	: 0.017	
fs	: 58.99	
Tensione di Progetto [N/mm ²]	: 0.13	
Modulo di resistenza a torsione [mm ³]	: 6381856.5	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a torsione	: 0.035	
fs	: 28.43	
Coefficiente di Sfruttamento a taglio+torsione	: 0.035	
fs	: 28.2	

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 12.12	Snellezza nel piano XZ	: 27.56
Snellezza relativa nel piano XY	: 0.19	Snellezza relativa nel piano XZ	: 0.44
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 37
Coefficiente K nel piano XY	: 0.51	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.98
Coefficiente di sfruttamento nel piano XY	: 0.143	Coefficiente di sfruttamento nel piano XZ	: 0.144
fs	: 6.960		

Colonna 14 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1900 mm - **R 500x220** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1900 mm] - **R 500x220**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.159 (fs=6.308)

Sforzo Normale di Progetto [daN]	: -1862 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 956
Momento Flettente Mz di Progetto [daNm]	: 975

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.17
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.009
fs	: 107.58
Tensione di Progetto relativa a My [N/mm ²]	: 2.37
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.06
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.158
fs	: 6.31
Coefficiente di Sfruttamento a pressoflessione	: 0.159
fs	: 6.31

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1900 mm / 1900 mm] - **R 500x220**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.074 (fs=13.572)

Taglio Ty di Progetto [daN]	: 115
Taglio Tz di Progetto [daN]	: -43

Momento Torcente Mt di Progetto [daNm]	: -48	
Tipo Verifica		: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02	
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.01	
Tensione tang. Resistente [N/mm ²]	: 1.69	
Coefficiente di Sfruttamento a taglio	: 0.01	
fs	: 100.66	
Tensione di Progetto [N/mm ²]	: 0.17	
Modulo di resistenza a torsione [mm ³]	: 6381856.5	
Tensione tang. Resistente [N/mm ²]	: 1.69	
Coefficiente di Sfruttamento a torsione	: 0.074	
fs	: 13.59	
Coefficiente di Sfruttamento a taglio+torsione	: 0.074	
fs	: 13.57	

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 9.21	Snellezza nel piano XZ	: 20.94
Snellezza relativa nel piano XY	: 0.15	Snellezza relativa nel piano XZ	: 0.33
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 37
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.56
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.168	Coefficiente di sfruttamento nel piano XZ	: 0.168
fs	: 5.960		

Colonna 15 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)
L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 48 [SLV] [IN] " - Coeff. Sfruttamento : 0.264 (fs=3.784)

Sforzo Normale di Progetto [daN]	: -4366 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 342
Momento Flettente Mz di Progetto [daNm]	: -2562

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.55
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.03
fs	: 33.36
Tensione di Progetto relativa a My [N/mm ²]	: 1.61
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.84
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.263
fs	: 3.8
Coefficiente di Sfruttamento a pressoflessione	: 0.264
fs	: 3.78

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.065 (fs=15.449)

Taglio Ty di Progetto [daN]	: 896
Taglio Tz di Progetto [daN]	: 195

Momento Torcente Mt di Progetto [daNm] : -2150

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.17
 Tensione di Progetto relativa a Tz [N/mm²] : 0.04
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.065
 fs : 15.45

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 48
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.293	Coefficiente di sfruttamento nel piano XZ	: 0.299
fs	: 3.343		

Colonna 124 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)
 L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.837 (fs=1.195)

Sforzo Normale di Progetto [daN] : 4371 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 3115
 Momento Flettente Mz di Progetto [daNm] : 1256

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.55
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.037
 fs : 27.15
 Tensione di Progetto relativa a My [N/mm²] : 14.6
 Tensione di Progetto relativa a Mz [N/mm²] : 1.88
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.8
 fs : 1.25
 Coefficiente di Sfruttamento : 0.837
 fs : 1.19

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 34 [SLD] [IN] " - Coeff. Sfruttamento : 0.135 (fs=7.432)

Taglio Ty di Progetto [daN] : 1275
 Taglio Tz di Progetto [daN] : -1416
 Momento Torcente Mt di Progetto [daNm] : -485

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.24
 Tensione di Progetto relativa a Tz [N/mm²] : 0.27
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.135

fs

: 7.43

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 26
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.839	Coefficiente di sfruttamento nel piano XZ	: 0.844
fs	: 1.184		

Colonna 15 Copertura[Colonna]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $-\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.746 (fs=1.341)

Sforzo Normale di Progetto [daN]	: 6399 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -2948
Momento Flettente Mz di Progetto [daNm]	: -30

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.8
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.054
fs	: 18.55
Tensione di Progetto relativa a My [N/mm²]	: 13.82
Tensione di Progetto relativa a Mz [N/mm²]	: 0.05
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.692
fs	: 1.45
Coefficiente di Sfruttamento	: 0.746
fs	: 1.34

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 27 [CAR] [ST] " - Coeff. Sfruttamento : 0.218 (fs=4.588)

Taglio Ty di Progetto [daN]	: -2526
Taglio Tz di Progetto [daN]	: -1
Momento Torcente Mt di Progetto [daNm]	: -252

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.47
Tensione di Progetto relativa a Tz [N/mm²]	: 0
Tensione tang. Resistente [N/mm²]	: 2.17
Coefficiente di Sfruttamento a taglio	: 0.218
fs	: 4.59

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31

Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.750	Coefficiente di sfruttamento nel piano XZ	: 0.751
fs	: 1.332		

Colonna 16 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.285 (fs=3.506)

Sforzo Normale di Progetto [daN]	: -597 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 42
Momento Flettente Mz di Progetto [daNm]	: 3441

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.07
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.004
fs	: 243.79
Tensione di Progetto relativa a My [N/mm²]	: 0.2
Tensione di Progetto relativa a Mz [N/mm²]	: 5.16
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.285
fs	: 3.51
Coefficiente di Sfruttamento a pressoflessione	: 0.285
fs	: 3.51

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.037 (fs=27.255)

Taglio Ty di Progetto [daN]	: -1327
Taglio Tz di Progetto [daN]	: 23
Momento Torcente Mt di Progetto [daNm]	: 3441

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²]	: 0.25
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.094
fs	: 10.67
Tensione di Progetto [N/mm²]	: 0.11
Modulo di resistenza a torsione [mm³]	: 3579418.25
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.028
fs	: 35.83
Coefficiente di Sfruttamento a taglio+torsione	: 0.037
fs	: 27.25

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91

Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.289	Coefficiente di sfruttamento nel piano XZ	: 0.290
fs	: 3.447		

Colonna 80 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 900 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 900 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.187 (fs=5.334)

Sforzo Normale di Progetto [daN]	: -3214 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -1
Momento Flettente Mz di Progetto [daNm]	: -1463

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²]	: -0.4
Tensione Resistente [N/mm²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.035
fs	: 28.84
Tensione di Progetto relativa a My [N/mm²]	: 0.01
Tensione di Progetto relativa a Mz [N/mm²]	: 2.19
Tensione Resistente relativa a My [N/mm²]	: 12.74
Tensione Resistente relativa a Mz [N/mm²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.186
fs	: 5.37
Coefficiente di Sfruttamento a pressoflessione	: 0.187
fs	: 5.33

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=900 mm / 900 mm] - **R 500x160**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.041 (fs=24.171)

Taglio Ty di Progetto [daN]	: 359
Taglio Tz di Progetto [daN]	: -93
Momento Torcente Mt di Progetto [daNm]	: 886

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²]	: 0.07
Tensione di Progetto relativa a Tz [N/mm²]	: 0.02
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.026
fs	: 38.21
Tensione di Progetto [N/mm²]	: 0.16
Modulo di resistenza a torsione [mm³]	: 3579418.25
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.041
fs	: 24.58
Coefficiente di Sfruttamento a taglio+torsione	: 0.041
fs	: 24.17

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.36	Snellezza nel piano XZ	: 13.64
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.22

Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.221	Coefficiente di sfruttamento nel piano XZ	: 0.221
fs	: 4.526		

Colonna 81 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.446 (fs=2.244)

Sforzo Normale di Progetto [daN]	: -3112 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 16
Momento Flettente Mz di Progetto [daNm]	: -3464

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²]	: -0.39
Tensione Resistente [N/mm²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.034
fs	: 29.79
Tensione di Progetto relativa a My [N/mm²]	: 0.07
Tensione di Progetto relativa a Mz [N/mm²]	: 5.2
Tensione Resistente relativa a My [N/mm²]	: 12.74
Tensione Resistente relativa a Mz [N/mm²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.444
fs	: 2.25
Coefficiente di Sfruttamento a pressoflessione	: 0.446
fs	: 2.24

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1600 mm / 1600 mm] - **R 500x160**

Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.083 (fs=12.041)

Taglio Ty di Progetto [daN]	: -1091
Taglio Tz di Progetto [daN]	: 440
Momento Torcente Mt di Progetto [daNm]	: -1894

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.2
Tensione di Progetto relativa a Tz [N/mm²]	: 0.08
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.083
fs	: 12.04

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.76	Snellezza nel piano XZ	: 24.25
Snellezza relativa nel piano XY	: 0.12	Snellezza relativa nel piano XZ	: 0.39
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.478	Coefficiente di sfruttamento nel piano XZ	: 0.478
fs	: 2.091		

Colonna 126 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.55 (fs=1.817)

Sforzo Normale di Progetto [daN] : -3120 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : -5
Momento Flettente Mz di Progetto [daNm] : -4308

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -0.39
Tensione Resistente [N/mm²] : 11.59
Coefficiente di Sfruttamento a compressione : 0.034
fs : 29.71
Tensione di Progetto relativa a My [N/mm²] : 0.02
Tensione di Progetto relativa a Mz [N/mm²] : 6.46
Tensione Resistente relativa a My [N/mm²] : 12.74
Tensione Resistente relativa a Mz [N/mm²] : 11.8
Coefficiente di Sfruttamento a flessione : 0.549
fs : 1.82
Coefficiente di Sfruttamento a pressoflessione : 0.55
fs : 1.82

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.121 (fs=8.28)

Taglio Ty di Progetto [daN] : -1400
Taglio Tz di Progetto [daN] : -19
Momento Torcente Mt di Progetto [daNm] : -3468

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.26
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a taglio : 0.155
fs : 6.44
Tensione di Progetto [N/mm²] : 0.24
Modulo di resistenza a torsione [mm³] : 3579418.25
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a torsione : 0.097
fs : 10.35
Coefficiente di Sfruttamento a taglio+torsione : 0.121
fs : 8.28

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.583	Coefficiente di sfruttamento nel piano XZ	: 0.583
fs	: 1.716		

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.532 (fs=1.88)

Sforzo Normale di Progetto [daN] : 1231 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 36
Momento Flettente Mz di Progetto [daNm] : -3984

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : 0.15
Tensione Resistente [N/mm²] : 9.44
Coefficiente di Sfruttamento a trazione : 0.016
fs : 61.37
Tensione di Progetto relativa a My [N/mm²] : 0.17
Tensione di Progetto relativa a Mz [N/mm²] : 5.98
Tensione Resistente relativa a My [N/mm²] : 12.74
Tensione Resistente relativa a Mz [N/mm²] : 11.8
Coefficiente di Sfruttamento a flessione : 0.516
fs : 1.94
Coefficiente di Sfruttamento : 0.532
fs : 1.88

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.223 (fs=4.487)

Taglio Ty di Progetto [daN] : 3155
Taglio Tz di Progetto [daN] : 69
Momento Torcente Mt di Progetto [daNm] : -3985

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.59
Tensione di Progetto relativa a Tz [N/mm²] : 0.01
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.223
fs : 4.49

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.516	Coefficiente di sfruttamento nel piano XZ	: 0.516
fs	: 1.939		

Colonna 17 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.388 (fs=2.576)
 Sforzo Normale di Progetto [daN] : -2128 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -78
 Momento Flettente Mz di Progetto [daNm] : -4638

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1
 Tensione di Progetto [N/mm²] : -0.27
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.015
 fs : 68.43
 Tensione di Progetto relativa a My [N/mm²] : 0.37
 Tensione di Progetto relativa a Mz [N/mm²] : 6.96
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.388
 fs : 2.58
 Coefficiente di Sfruttamento a pressoflessione : 0.388
 fs : 2.58

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.11 (fs=9.084)
 Taglio Ty di Progetto [daN] : 992
 Taglio Tz di Progetto [daN] : -6
 Momento Torcente Mt di Progetto [daNm] : -2495

Tipo Verifica : TAGLIO
 Tensione di Progetto relativa a Ty [N/mm²] : 0.19
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.11
 fs : 9.08

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.403	Coefficiente di sfruttamento nel piano XZ	: 0.405
fs	: 2.466		

Colonna 128 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
 L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**
Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.795 (fs=1.258)
 Sforzo Normale di Progetto [daN] : -3381 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 3080
 Momento Flettente Mz di Progetto [daNm] : 1300

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.42
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.023
fs	: 43.08
Tensione di Progetto relativa a My [N/mm ²]	: 14.44
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.95
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.794
fs	: 1.26
Coefficiente di Sfruttamento a pressoflessione	: 0.795
fs	: 1.26

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.103 (fs=9.677)

Taglio Ty di Progetto [daN]	: 931
Taglio Tz di Progetto [daN]	: -7
Momento Torcente Mt di Progetto [daNm]	: 1245

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.17
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.103
fs	: 9.68

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.818	Coefficiente di sfruttamento nel piano XZ	: 0.820
fs	: 1.220		

Colonna 17 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.716 (fs=1.397)

Sforzo Normale di Progetto [daN]	: 1356 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 2967
Momento Flettente Mz di Progetto [daNm]	: -175

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.17
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.011
fs	: 87.53
Tensione di Progetto relativa a My [N/mm ²]	: 13.91
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.26
Tensione Resistente relativa a My [N/mm ²]	: 20.03

Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.704
f_s	: 1.42
Coefficiente di Sfruttamento	: 0.716
f_s	: 1.4

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.35 ($f_s=2.86$)

Taglio T_y di Progetto [daN]	: -3151
Taglio T_z di Progetto [daN]	: -4
Momento Torcente M_t di Progetto [daNm]	: 3817

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.59
Tensione di Progetto relativa a T_z [N/mm ²]	: 0
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.35
f_s	: 2.86

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente K_c nel piano XY	: 1.00	Coefficiente K_c nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.709	Coefficiente di sfruttamento nel piano XZ	: 0.709
f_s	: 1.410		

Colonna 18 Primo Imp[Colonna]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $-\gamma_M=1.45$ (FC=1)
L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.437 ($f_s=2.289$)

Sforzo Normale di Progetto [daN]	: -315 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: 41
Momento Flettente M_z di Progetto [daNm]	: 5318

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: -0.04
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.002
f_s	: 462.08
Tensione di Progetto relativa a M_y [N/mm ²]	: 0.19
Tensione di Progetto relativa a M_z [N/mm ²]	: 7.98
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.437
f_s	: 2.29
Coefficiente di Sfruttamento a pressoflessione	: 0.437
f_s	: 2.29

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.109 (fs=9.134)
 Taglio Ty di Progetto [daN] : -987
 Taglio Tz di Progetto [daN] : -8
 Momento Torcente Mt di Progetto [daNm] : 2484

Tipo Verifica : TAGLIO
 Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.109
 fs : 9.13

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.439	Coefficiente di sfruttamento nel piano XZ	: 0.439
fs	: 2.275		

Colonna 82 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.261 (fs=3.834)
 Sforzo Normale di Progetto [daN] : -3636 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : -2040

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7
 Tensione di Progetto [N/mm²] : -0.45
 Tensione Resistente [N/mm²] : 11.59
 Coefficiente di Sfruttamento a compressione : 0.039
 fs : 25.49
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 3.06
 Tensione Resistente relativa a My [N/mm²] : 12.74
 Tensione Resistente relativa a Mz [N/mm²] : 11.8
 Coefficiente di Sfruttamento a flessione : 0.259
 fs : 3.86
 Coefficiente di Sfruttamento a pressoflessione : 0.261
 fs : 3.83

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 853.13 mm] - **R 500x160**
Comb. più gravosa : " Comb 43 [SLV] [IN] " - Coeff. Sfruttamento : 0.096 (fs=10.431)
 Taglio Ty di Progetto [daN] : -1317
 Taglio Tz di Progetto [daN] : -328
 Momento Torcente Mt di Progetto [daNm] : -1114

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.25
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.06
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.096
fs	: 10.43

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.299	Coefficiente di sfruttamento nel piano XZ	: 0.299
fs	: 3.350		

Colonna 98 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.458 (fs=2.185)

Sforzo Normale di Progetto [daN]	: -3579 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 9
Momento Flettente Mz di Progetto [daNm]	: -3570

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.45
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.039
fs	: 25.9
Tensione di Progetto relativa a My [N/mm ²]	: 0.04
Tensione di Progetto relativa a Mz [N/mm ²]	: 5.35
Tensione Resistente relativa a My [N/mm ²]	: 12.74
Tensione Resistente relativa a Mz [N/mm ²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.456
fs	: 2.19
Coefficiente di Sfruttamento a pressoflessione	: 0.458
fs	: 2.19

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.052 (fs=19.256)

Taglio Ty di Progetto [daN]	: -669
Taglio Tz di Progetto [daN]	: -305
Momento Torcente Mt di Progetto [daNm]	: -1081

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.13
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.06
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.052
fs	: 19.26

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.495	Coefficiente di sfruttamento nel piano XZ	: 0.495
fs	: 2.020		

Colonna 131 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.527 (fs=1.898)

Sforzo Normale di Progetto [daN]	: -3525 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 2
Momento Flettente Mz di Progetto [daNm]	: -4129

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²]	: -0.44
Tensione Resistente [N/mm²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.038
fs	: 26.29
Tensione di Progetto relativa a My [N/mm²]	: 0.01
Tensione di Progetto relativa a Mz [N/mm²]	: 6.19
Tensione Resistente relativa a My [N/mm²]	: 12.74
Tensione Resistente relativa a Mz [N/mm²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.525
fs	: 1.9
Coefficiente di Sfruttamento a pressoflessione	: 0.527
fs	: 1.9

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 11 [SLD] [IN] " - Coeff. Sfruttamento : 0.136 (fs=7.341)

Taglio Ty di Progetto [daN]	: -1928
Taglio Tz di Progetto [daN]	: -51
Momento Torcente Mt di Progetto [daNm]	: -3627

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.36
Tensione di Progetto relativa a Tz [N/mm²]	: 0.01
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.136
fs	: 7.34

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50

Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.563	Coefficiente di sfruttamento nel piano XZ	: 0.563
fs	: 1.775		

Colonna 18 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.49 (fs=2.04)

Sforzo Normale di Progetto [daN]	: 315 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 4
Momento Flettente Mz di Progetto [daNm]	: -3815

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: 0.04
Tensione Resistente [N/mm ²]	: 9.44
Coefficiente di Sfruttamento a trazione	: 0.004
fs	: 239.73
Tensione di Progetto relativa a My [N/mm ²]	: 0.02
Tensione di Progetto relativa a Mz [N/mm ²]	: 5.72
Tensione Resistente relativa a My [N/mm ²]	: 12.74
Tensione Resistente relativa a Mz [N/mm ²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.486
fs	: 2.06
Coefficiente di Sfruttamento	: 0.49
fs	: 2.04

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.35 (fs=2.861)

Taglio Ty di Progetto [daN]	: 3150
Taglio Tz di Progetto [daN]	: -10
Momento Torcente Mt di Progetto [daNm]	: -3815

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.59
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.35
fs	: 2.86

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.486	Coefficiente di sfruttamento nel piano XZ	: 0.486
fs	: 2.058		

Colonna 19 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7
VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.463 (fs=2.162)
 Sforzo Normale di Progetto [daN] : -768 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -78
 Momento Flettente Mz di Progetto [daNm] : -5559

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.1
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 189.62
Tensione di Progetto relativa a My [N/mm ²]	: 0.36
Tensione di Progetto relativa a Mz [N/mm ²]	: 8.34
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.462
fs	: 2.16
Coefficiente di Sfruttamento a pressoflessione	: 0.463
fs	: 2.16

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.112 (fs=8.953)
 Taglio Ty di Progetto [daN] : 1007
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : -2511

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.19
Tensione di Progetto relativa a Tz [N/mm ²]	: 0
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.112
fs	: 8.95

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.468	Coefficiente di sfruttamento nel piano XZ	: 0.469
fs	: 2.133		

Colonna 132 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**
Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.793 (fs=1.262)

Sforzo Normale di Progetto [daN]	: 11 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 3106
Momento Flettente Mz di Progetto [daNm]	: 1157

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.00
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 14.56
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.74
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.793
fs	: 1.26
Coefficiente di Sfruttamento	: 0.793
fs	: 1.26

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 48 [SLV] [IN] " - Coeff. Sfruttamento : 0.114 (fs=8.762)

Taglio Ty di Progetto [daN]	: 891
Taglio Tz di Progetto [daN]	: 1348
Momento Torcente Mt di Progetto [daNm]	: 1535

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.17
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.25
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.114
fs	: 8.76

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.810	Coefficiente di sfruttamento nel piano XZ	: 0.814
fs	: 1.229		

Colonna 19 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.722 (fs=1.386)

Sforzo Normale di Progetto [daN]	: 2185 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -2973
Momento Flettente Mz di Progetto [daNm]	: -132

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.27
Tensione Resistente [N/mm ²]	: 14.83

Coefficiente di Sfruttamento a trazione	: 0.018
fs	: 54.32
Tensione di Progetto relativa a My [N/mm ²]	: 13.94
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.2
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.703
fs	: 1.42
Coefficiente di Sfruttamento	: 0.722
fs	: 1.39

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.351 (fs=2.846)

Taglio Ty di Progetto [daN]	: -3166
Taglio Tz di Progetto [daN]	: -4
Momento Torcente Mt di Progetto [daNm]	: 3835

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.59
Tensione di Progetto relativa a Tz [N/mm ²]	: 0
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.351
fs	: 2.85

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.730	Coefficiente di sfruttamento nel piano XZ	: 0.730
fs	: 1.370		

Colonna 20 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.483 (fs=2.072)

Sforzo Normale di Progetto [daN]	: -398 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 8
Momento Flettente Mz di Progetto [daNm]	: 5950

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.05
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.003
fs	: 365.7
Tensione di Progetto relativa a My [N/mm ²]	: 0.04
Tensione di Progetto relativa a Mz [N/mm ²]	: 8.92
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.483

fs	: 2.07
Coefficiente di Sfruttamento a pressoflessione	: 0.483
fs	: 2.07

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - R 500x160	
<i>Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.127 (fs=7.861)</i>	
Taglio Ty di Progetto [daN]	: -1801
Taglio Tz di Progetto [daN]	: 27
Momento Torcente Mt di Progetto [daNm]	: 4643

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.34
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.127
fs	: 7.86

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.485	Coefficiente di sfruttamento nel piano XZ	: 0.486
fs	: 2.058		

Colonna 83 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - R 500x160	
<i>Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.266 (fs=3.754)</i>	
Sforzo Normale di Progetto [daN]	: -4059 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 2
Momento Flettente Mz di Progetto [daNm]	: -2076

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²]	: -0.51
Tensione Resistente [N/mm²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.044
fs	: 22.83
Tensione di Progetto relativa a My [N/mm²]	: 0.01
Tensione di Progetto relativa a Mz [N/mm²]	: 3.11
Tensione Resistente relativa a My [N/mm²]	: 12.74
Tensione Resistente relativa a Mz [N/mm²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.264
fs	: 3.78
Coefficiente di Sfruttamento a pressoflessione	: 0.266
fs	: 3.75

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.102 (fs=9.783)

Taglio Ty di Progetto [daN]	: -921
Taglio Tz di Progetto [daN]	: -14
Momento Torcente Mt di Progetto [daNm]	: -1290

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.17
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.102
fs	: 9.78

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.308	Coefficiente di sfruttamento nel piano XZ	: 0.308
fs	: 3.244		

Colonna 99 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.46 (fs=2.172)

Sforzo Normale di Progetto [daN]	: -3973 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 6
Momento Flettente Mz di Progetto [daNm]	: -3596

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²]	: -0.5
Tensione Resistente [N/mm²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.043
fs	: 23.33
Tensione di Progetto relativa a My [N/mm²]	: 0.03
Tensione di Progetto relativa a Mz [N/mm²]	: 5.39
Tensione Resistente relativa a My [N/mm²]	: 12.74
Tensione Resistente relativa a Mz [N/mm²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.459
fs	: 2.18
Coefficiente di Sfruttamento a pressoflessione	: 0.46
fs	: 2.17

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa : 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.102 (fs=9.762)

Taglio Ty di Progetto [daN]	: -923
Taglio Tz di Progetto [daN]	: -6
Momento Torcente Mt di Progetto [daNm]	: -2076

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.17
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Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.102
f_s	: 9.76

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.501	Coefficiente di sfruttamento nel piano XZ	: 0.502
f_s	: 1.992		

Colonna 133 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.529 ($f_s=1.89$)

Sforzo Normale di Progetto [daN]	: -3956 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: 0
Momento Flettente M_z di Progetto [daNm]	: -4148

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 0.7$

Tensione di Progetto [N/mm ²]	: -0.49
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.043
f_s	: 23.43
Tensione di Progetto relativa a M_y [N/mm ²]	: 0
Tensione di Progetto relativa a M_z [N/mm ²]	: 6.22
Tensione Resistente relativa a M_y [N/mm ²]	: 12.74
Tensione Resistente relativa a M_z [N/mm ²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.527
f_s	: 1.9
Coefficiente di Sfruttamento a pressoflessione	: 0.529
f_s	: 1.89

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.102 ($f_s=9.808$)

Taglio T_y di Progetto [daN]	: -919
Taglio T_z di Progetto [daN]	: -6
Momento Torcente M_t di Progetto [daNm]	: -3597

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.17
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.102
f_s	: 9.81

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.570	Coefficiente di sfruttamento nel piano XZ	: 0.570
fs	: 1.754		

Colonna 20 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.487 (fs=2.053)

Sforzo Normale di Progetto [daN]	: -111 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -3831

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²]	: -0.01
Tensione Resistente [N/mm²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.001
fs	: 835.15
Tensione di Progetto relativa a My [N/mm²]	: 0
Tensione di Progetto relativa a Mz [N/mm²]	: 5.75
Tensione Resistente relativa a My [N/mm²]	: 12.74
Tensione Resistente relativa a Mz [N/mm²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.487
fs	: 2.05
Coefficiente di Sfruttamento a pressoflessione	: 0.487
fs	: 2.05

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.351 (fs=2.847)

Taglio Ty di Progetto [daN]	: 3166
Taglio Tz di Progetto [daN]	: -6
Momento Torcente Mt di Progetto [daNm]	: -3831

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.59
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.351
fs	: 2.85

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.488	Coefficiente di sfruttamento nel piano XZ	: 0.488

fs : 2.048

Colonna 21 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)
L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.564 (fs=1.772)

Sforzo Normale di Progetto [daN] : -889 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : 152
Momento Flettente Mz di Progetto [daNm] : -6666

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.11
Tensione Resistente [N/mm²] : 18.21
Coefficiente di Sfruttamento a compressione : 0.006
fs : 163.92
Tensione di Progetto relativa a My [N/mm²] : 0.71
Tensione di Progetto relativa a Mz [N/mm²] : 10
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 18.54
Coefficiente di Sfruttamento a flessione : 0.564
fs : 1.77
Coefficiente di Sfruttamento a pressoflessione : 0.564
fs : 1.77

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.358)

Taglio Ty di Progetto [daN] : 963
Taglio Tz di Progetto [daN] : 1
Momento Torcente Mt di Progetto [daNm] : -2416

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
Tensione di Progetto relativa a Tz [N/mm²] : 0
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a taglio : 0.107
fs : 9.36

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 17
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.570	Coefficiente di sfruttamento nel piano XZ	: 0.572
fs	: 1.750		

Colonna 137 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)
L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**
Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.827 (fs=1.209)
 Sforzo Normale di Progetto [daN] : -6851 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 3063
 Momento Flettente Mz di Progetto [daNm] : 1907

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.86
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.047
 fs : 21.26
 Tensione di Progetto relativa a My [N/mm²] : 14.36
 Tensione di Progetto relativa a Mz [N/mm²] : 2.86
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.825
 fs : 1.21
 Coefficiente di Sfruttamento a pressoflessione : 0.827
 fs : 1.21

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**
Comb. più gravosa : " Comb 48 [SLV] [IN] " - Coeff. Sfruttamento : 0.112 (fs=8.919)
 Taglio Ty di Progetto [daN] : 830
 Taglio Tz di Progetto [daN] : 1354
 Momento Torcente Mt di Progetto [daNm] : 1461

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.16
 Tensione di Progetto relativa a Tz [N/mm²] : 0.25
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.112
 fs : 8.92

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 41
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.872	Coefficiente di sfruttamento nel piano XZ	: 0.876
fs	: 1.141		

Colonna 21 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)
 L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1300 mm] - **R 500x160**
Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.729 (fs=1.372)
 Sforzo Normale di Progetto [daN] : 3376 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 2949

Momento Flettente Mz di Progetto [daNm] : -181

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.42
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.028
fs	: 35.15
Tensione di Progetto relativa a My [N/mm ²]	: 13.83
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.27
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.701
fs	: 1.43
Coefficiente di Sfruttamento	: 0.729
fs	: 1.37

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.353 (fs=2.834)

Taglio Ty di Progetto [daN]	: -3180
Taglio Tz di Progetto [daN]	: -1
Momento Torcente Mt di Progetto [daNm]	: 3853

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.6
Tensione di Progetto relativa a Tz [N/mm ²]	: 0
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.353
fs	: 2.83

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.732	Coefficiente di sfruttamento nel piano XZ	: 0.732
fs	: 1.366		

Colonna 22 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.55 (fs=1.819)

Sforzo Normale di Progetto [daN]	: -779 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 10
Momento Flettente Mz di Progetto [daNm]	: 6773

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.1
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 186.98

Tensione di Progetto relativa a M_y [N/mm ²]	: 0.05
Tensione di Progetto relativa a M_z [N/mm ²]	: 10.16
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.55
f_s	: 1.82
Coefficiente di Sfruttamento a pressoflessione	: 0.55
f_s	: 1.82

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.146 ($f_s=6.856$)

Taglio T_y di Progetto [daN]	: -2065
Taglio T_z di Progetto [daN]	: 29
Momento Torcente M_t di Progetto [daNm]	: 5376

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.39
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.146
f_s	: 6.86

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente K_c nel piano XY	: 1.00	Coefficiente K_c nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.555	Coefficiente di sfruttamento nel piano XZ	: 0.556
f_s	: 1.799		

Colonna 84 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.261 ($f_s=3.834$)

Sforzo Normale di Progetto [daN]	: -4229 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: -2
Momento Flettente M_z di Progetto [daNm]	: -2032

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 0.7$

Tensione di Progetto [N/mm ²]	: -0.53
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.046
f_s	: 21.92
Tensione di Progetto relativa a M_y [N/mm ²]	: 0.01
Tensione di Progetto relativa a M_z [N/mm ²]	: 3.05
Tensione Resistente relativa a M_y [N/mm ²]	: 12.74
Tensione Resistente relativa a M_z [N/mm ²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.259
f_s	: 3.87
Coefficiente di Sfruttamento a pressoflessione	: 0.261

fs : 3.83

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.445)

Taglio Ty di Progetto [daN] : -954
 Taglio Tz di Progetto [daN] : 5
 Momento Torcente Mt di Progetto [daNm] : -1218

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.106
 fs : 9.45

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.304	Coefficiente di sfruttamento nel piano XZ	: 0.304
fs	: 3.286		

Colonna 100 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.46 (fs=2.174)

Sforzo Normale di Progetto [daN] : -4153 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 2
 Momento Flettente Mz di Progetto [daNm] : -3599

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -0.52
 Tensione Resistente [N/mm²] : 11.59
 Coefficiente di Sfruttamento a compressione : 0.045
 fs : 22.32
 Tensione di Progetto relativa a My [N/mm²] : 0.01
 Tensione di Progetto relativa a Mz [N/mm²] : 5.4
 Tensione Resistente relativa a My [N/mm²] : 12.74
 Tensione Resistente relativa a Mz [N/mm²] : 11.8
 Coefficiente di Sfruttamento a flessione : 0.458
 fs : 2.18
 Coefficiente di Sfruttamento a pressoflessione : 0.46
 fs : 2.17

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.466)

Taglio Ty di Progetto [daN] : -952

Taglio Tz di Progetto [daN] : -3
 Momento Torcente Mt di Progetto [daNm] : -2032

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.106
 fs : 9.47

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.503	Coefficiente di sfruttamento nel piano XZ	: 0.503
fs	: 1.986		

Colonna 139 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
 L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.532 (fs=1.878)

Sforzo Normale di Progetto [daN] : -4121 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 1
 Momento Flettente Mz di Progetto [daNm] : -4171

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -0.52
 Tensione Resistente [N/mm²] : 11.59
 Coefficiente di Sfruttamento a compressione : 0.044
 fs : 22.49
 Tensione di Progetto relativa a My [N/mm²] : 0.01
 Tensione di Progetto relativa a Mz [N/mm²] : 6.26
 Tensione Resistente relativa a My [N/mm²] : 12.74
 Tensione Resistente relativa a Mz [N/mm²] : 11.8
 Coefficiente di Sfruttamento a flessione : 0.53
 fs : 1.89
 Coefficiente di Sfruttamento a pressoflessione : 0.532
 fs : 1.88

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.465)

Taglio Ty di Progetto [daN] : -952
 Taglio Tz di Progetto [daN] : 1
 Momento Torcente Mt di Progetto [daNm] : -3600

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0
 Tensione tang. Resistente [N/mm²] : 1.69

Coefficiente di Sfruttamento a taglio : 0.106
fs : 9.47

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.575	Coefficiente di sfruttamento nel piano XZ	: 0.575
fs	: 1.739		

Colonna 22 Copertura[Colonna]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.505 (fs=1.981)

Sforzo Normale di Progetto [daN]	: 2778 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -7
Momento Flettente Mz di Progetto [daNm]	: -5937

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.35
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.023
fs	: 42.72
Tensione di Progetto relativa a My [N/mm²]	: 0.03
Tensione di Progetto relativa a Mz [N/mm²]	: 8.91
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.481
fs	: 2.08
Coefficiente di Sfruttamento	: 0.505
fs	: 1.98

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.353 (fs=2.834)

Taglio Ty di Progetto [daN]	: 3180
Taglio Tz di Progetto [daN]	: 1
Momento Torcente Mt di Progetto [daNm]	: -3852

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.6
Tensione di Progetto relativa a Tz [N/mm²]	: 0
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.353
fs	: 2.83

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70

Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.492	Coefficiente di sfruttamento nel piano XZ	: 0.492
fs	: 2.031		

Colonna 23 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.644 (fs=1.553)

Sforzo Normale di Progetto [daN]	: -447 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -69
Momento Flettente Mz di Progetto [daNm]	: -7819

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.06
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.003
fs	: 325.99
Tensione di Progetto relativa a My [N/mm²]	: 0.32
Tensione di Progetto relativa a Mz [N/mm²]	: 11.73
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.644
fs	: 1.55
Coefficiente di Sfruttamento a pressoflessione	: 0.644
fs	: 1.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.105 (fs=9.498)

Taglio Ty di Progetto [daN]	: 949
Taglio Tz di Progetto [daN]	: 4
Momento Torcente Mt di Progetto [daNm]	: -2388

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm²]	: 0
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.105
fs	: 9.5

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.647	Coefficiente di sfruttamento nel piano XZ	: 0.647
fs	: 1.544		

Colonna 140 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.858 (fs=1.166)

Sforzo Normale di Progetto [daN] : -2775 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : -3120
Momento Flettente Mz di Progetto [daNm] : 2244

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.35
Tensione Resistente [N/mm²] : 18.21
Coefficiente di Sfruttamento a compressione : 0.019
fs : 52.48
Tensione di Progetto relativa a My [N/mm²] : 14.63
Tensione di Progetto relativa a Mz [N/mm²] : 3.37
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 18.54
Coefficiente di Sfruttamento a flessione : 0.857
fs : 1.17
Coefficiente di Sfruttamento a pressoflessione : 0.858
fs : 1.17

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.111 (fs=9.023)

Taglio Ty di Progetto [daN] : 674
Taglio Tz di Progetto [daN] : -1417
Momento Torcente Mt di Progetto [daNm] : 1332

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.13
Tensione di Progetto relativa a Tz [N/mm²] : 0.27
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.111
fs : 9.02

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.876	Coefficiente di sfruttamento nel piano XZ	: 0.878
fs	: 1.139		

Colonna 23 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.721 (fs=1.387)

Sforzo Normale di Progetto [daN] : 1274 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 2951
 Momento Flettente Mz di Progetto [daNm] : -345

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.16
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.011
 fs : 93.13
 Tensione di Progetto relativa a My [N/mm²] : 13.83
 Tensione di Progetto relativa a Mz [N/mm²] : 0.52
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.71
 fs : 1.41
 Coefficiente di Sfruttamento : 0.721
 fs : 1.39

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.354 (fs=2.826)

Taglio Ty di Progetto [daN] : -3189
 Taglio Tz di Progetto [daN] : 0
 Momento Torcente Mt di Progetto [daNm] : 3858

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.6
 Tensione di Progetto relativa a Tz [N/mm²] : 0
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.354
 fs : 2.83

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.717	Coefficiente di sfruttamento nel piano XZ	: 0.717
fs	: 1.395		

Colonna 24 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.617 (fs=1.621)

Sforzo Normale di Progetto [daN] : -801 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 13
 Momento Flettente Mz di Progetto [daNm] : 7598

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.1
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 181.93
Tensione di Progetto relativa a My [N/mm ²]	: 0.06
Tensione di Progetto relativa a Mz [N/mm ²]	: 11.4
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.617
fs	: 1.62
Coefficiente di Sfruttamento a pressoflessione	: 0.617
fs	: 1.62

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.105 (fs=9.496)

Taglio Ty di Progetto [daN]	: -949
Taglio Tz di Progetto [daN]	: 1
Momento Torcente Mt di Progetto [daNm]	: 2386

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm ²]	: 0
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.105
fs	: 9.5

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.622	Coefficiente di sfruttamento nel piano XZ	: 0.623
fs	: 1.604		

Colonna 85 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.261 (fs=3.835)

Sforzo Normale di Progetto [daN]	: -4433 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 9
Momento Flettente Mz di Progetto [daNm]	: -2014

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.55
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.048
fs	: 20.91
Tensione di Progetto relativa a My [N/mm ²]	: 0.04
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.02

Tensione Resistente relativa a M_y [N/mm ²]	: 12.74
Tensione Resistente relativa a M_z [N/mm ²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.258
f_s	: 3.87
Coefficiente di Sfruttamento a pressoflessione	: 0.261
f_s	: 3.84

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.12 ($f_s=8.304$)

Taglio T_y di Progetto [daN]	: -1690
Taglio T_z di Progetto [daN]	: -231
Momento Torcente M_t di Progetto [daNm]	: -1328

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.32
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.04
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.12
f_s	: 8.3

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente K_c nel piano XY	: 1.00	Coefficiente K_c nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.306	Coefficiente di sfruttamento nel piano XZ	: 0.306
f_s	: 3.265		

Colonna 101 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.496 ($f_s=2.018$)

Sforzo Normale di Progetto [daN]	: -111 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: -180
Momento Flettente M_z di Progetto [daNm]	: -5762

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: -0.01
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.001
f_s	: 1000
Tensione di Progetto relativa a M_y [N/mm ²]	: 0.84
Tensione di Progetto relativa a M_z [N/mm ²]	: 8.64
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.496
f_s	: 2.02
Coefficiente di Sfruttamento a pressoflessione	: 0.496
f_s	: 2.02

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.358)

Taglio Ty di Progetto [daN] : -963
 Taglio Tz di Progetto [daN] : 6
 Momento Torcente Mt di Progetto [daNm] : -2014

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.107
 fs : 9.36

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.506	Coefficiente di sfruttamento nel piano XZ	: 0.506
fs	: 1.976		

Colonna 143 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa: 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.579 (fs=1.728)

Sforzo Normale di Progetto [daN] : -903 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -9
 Momento Flettente Mz di Progetto [daNm] : -7134

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.11
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.006
 fs : 161.35
 Tensione di Progetto relativa a My [N/mm²] : 0.04
 Tensione di Progetto relativa a Mz [N/mm²] : 10.7
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.579
 fs : 1.73
 Coefficiente di Sfruttamento a pressoflessione : 0.579
 fs : 1.73

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.358)

Taglio Ty di Progetto [daN] : -963
 Taglio Tz di Progetto [daN] : 2
 Momento Torcente Mt di Progetto [daNm] : -3600

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm ²]	: 0
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.107
fs	: 9.36

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 10
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.585	Coefficiente di sfruttamento nel piano XZ	: 0.585
fs	: 1.710		

Colonna 24 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.568 (fs=1.762)

Sforzo Normale di Progetto [daN]	: 3731 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -8
Momento Flettente Mz di Progetto [daNm]	: -6610

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.47
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.031
fs	: 31.81
Tensione di Progetto relativa a My [N/mm ²]	: 0.04
Tensione di Progetto relativa a Mz [N/mm ²]	: 9.92
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.536
fs	: 1.87
Coefficiente di Sfruttamento	: 0.568
fs	: 1.76

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.354 (fs=2.826)

Taglio Ty di Progetto [daN]	: 3188
Taglio Tz di Progetto [daN]	: 2
Momento Torcente Mt di Progetto [daNm]	: -3859

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.6
Tensione di Progetto relativa a Tz [N/mm ²]	: 0
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.354
fs	: 2.83

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 10
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.536	Coefficiente di sfruttamento nel piano XZ	: 0.536
fs	: 1.865		

Colonna 25 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.755 (fs=1.324)

Sforzo Normale di Progetto [daN]	: -1401 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 158
Momento Flettente Mz di Progetto [daNm]	: -9017

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.18
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.01
fs	: 103.97
Tensione di Progetto relativa a My [N/mm²]	: 0.74
Tensione di Progetto relativa a Mz [N/mm²]	: 13.53
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.755
fs	: 1.32
Coefficiente di Sfruttamento a pressoflessione	: 0.755
fs	: 1.32

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 48 [SLV] [IN] " - Coeff. Sfruttamento : 0.136 (fs=7.366)

Taglio Ty di Progetto [daN]	: 1912
Taglio Tz di Progetto [daN]	: 197
Momento Torcente Mt di Progetto [daNm]	: -5089

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.36
Tensione di Progetto relativa a Tz [N/mm²]	: 0.04
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.136
fs	: 7.37

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 17

Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.765	Coefficiente di sfruttamento nel piano XZ	: 0.767
fs	: 1.304		

Colonna 144 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.845 (fs=1.183)

Sforzo Normale di Progetto [daN]	: 1038 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -3065
Momento Flettente Mz di Progetto [daNm]	: 2098

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.13
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.009
fs	: 114.38
Tensione di Progetto relativa a My [N/mm²]	: 14.37
Tensione di Progetto relativa a Mz [N/mm²]	: 3.15
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.836
fs	: 1.2
Coefficiente di Sfruttamento	: 0.845
fs	: 1.18

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 48 [SLV] [IN] " - Coeff. Sfruttamento : 0.165 (fs=6.065)

Taglio Ty di Progetto [daN]	: 1902
Taglio Tz di Progetto [daN]	: 1354
Momento Torcente Mt di Progetto [daNm]	: 745

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.36
Tensione di Progetto relativa a Tz [N/mm²]	: 0.25
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.165
fs	: 6.06

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 50
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.836	Coefficiente di sfruttamento nel piano XZ	: 0.836
fs	: 1.196		

Colonna 25 Copertura[Colonna]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $-\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.739 (fs=1.354)

Sforzo Normale di Progetto [daN] : 3963 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 2952
Momento Flettente Mz di Progetto [daNm] : -257

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.5
Tensione Resistente [N/mm²] : 14.83
Coefficiente di Sfruttamento a trazione : 0.033
fs : 29.94
Tensione di Progetto relativa a My [N/mm²] : 13.84
Tensione di Progetto relativa a Mz [N/mm²] : 0.38
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 18.54
Coefficiente di Sfruttamento a flessione : 0.705
fs : 1.42
Coefficiente di Sfruttamento : 0.739
fs : 1.35

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.355 (fs=2.818)

Taglio Ty di Progetto [daN] : -3198
Taglio Tz di Progetto [daN] : 0
Momento Torcente Mt di Progetto [daNm] : 3862

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.6
Tensione di Progetto relativa a Tz [N/mm²] : 0
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a taglio : 0.355
fs : 2.82

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.740	Coefficiente di sfruttamento nel piano XZ	: 0.740
fs	: 1.351		

Colonna 26 Primo Imp[Colonna]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $-\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.7 ($f_s=1.428$)

Sforzo Normale di Progetto [daN] : -500 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 12
 Momento Flettente Mz di Progetto [daNm] : 8633

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.06
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.003
 f_s : 291.15
 Tensione di Progetto relativa a My [N/mm²] : 0.06
 Tensione di Progetto relativa a Mz [N/mm²] : 12.95
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.7
 f_s : 1.43
 Coefficiente di Sfruttamento a pressoflessione : 0.7
 f_s : 1.43

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.108 ($f_s=9.231$)

Taglio Ty di Progetto [daN] : -1534
 Taglio Tz di Progetto [daN] : 31
 Momento Torcente Mt di Progetto [daNm] : 5693

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.29
 Tensione di Progetto relativa a Tz [N/mm²] : 0.01
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.108
 f_s : 9.23

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.704	Coefficiente di sfruttamento nel piano XZ	: 0.704
f_s	: 1.419		

Colonna 86 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.261 ($f_s=3.833$)

Sforzo Normale di Progetto [daN] : -4560 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -8
 Momento Flettente Mz di Progetto [daNm] : -2017

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -0.57

Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.049
fs	: 20.33
Tensione di Progetto relativa a My [N/mm ²]	: 0.04
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.03
Tensione Resistente relativa a My [N/mm ²]	: 12.74
Tensione Resistente relativa a Mz [N/mm ²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.258
fs	: 3.87
Coefficiente di Sfruttamento a pressoflessione	: 0.261
fs	: 3.83

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.369)

Taglio Ty di Progetto [daN]	: -962
Taglio Tz di Progetto [daN]	: 8
Momento Torcente Mt di Progetto [daNm]	: -1197

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.107
fs	: 9.37

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.308	Coefficiente di sfruttamento nel piano XZ	: 0.308
fs	: 3.250		

Colonna 102 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**
Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.543 (fs=1.842)

Sforzo Normale di Progetto [daN]	: 201 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -141
Momento Flettente Mz di Progetto [daNm]	: -6403

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.03
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 589.11
Tensione di Progetto relativa a My [N/mm ²]	: 0.66
Tensione di Progetto relativa a Mz [N/mm ²]	: 9.61
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54

Coefficiente di Sfruttamento a flessione	: 0.541
fs	: 1.85
Coefficiente di Sfruttamento	: 0.543
fs	: 1.84

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.366)

Taglio Ty di Progetto [daN]	: -962
Taglio Tz di Progetto [daN]	: -16
Momento Torcente Mt di Progetto [daNm]	: -2017

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.107
fs	: 9.37

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.541	Coefficiente di sfruttamento nel piano XZ	: 0.541
fs	: 1.848		

Colonna 147 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.64 (fs=1.561)

Sforzo Normale di Progetto [daN]	: 236 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -7892

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.03
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 502.49
Tensione di Progetto relativa a My [N/mm²]	: 0
Tensione di Progetto relativa a Mz [N/mm²]	: 11.84
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.638
fs	: 1.57
Coefficiente di Sfruttamento	: 0.64
fs	: 1.56

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.365)

Taglio Ty di Progetto [daN] : -962
 Taglio Tz di Progetto [daN] : 22
 Momento Torcente Mt di Progetto [daNm] : -3602

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.107
 fs : 9.36

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.638	Coefficiente di sfruttamento nel piano XZ	: 0.638
fs	: 1.566		

Colonna 26 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.629 (fs=1.589)

Sforzo Normale di Progetto [daN] : 4465 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 2
 Momento Flettente Mz di Progetto [daNm] : -7311

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.56
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.038
 fs : 26.58
 Tensione di Progetto relativa a My [N/mm²] : 0.01
 Tensione di Progetto relativa a Mz [N/mm²] : 10.97
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.592
 fs : 1.69
 Coefficiente di Sfruttamento : 0.629
 fs : 1.59

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.354 (fs=2.823)

Taglio Ty di Progetto [daN] : 3192
 Taglio Tz di Progetto [daN] : 21
 Momento Torcente Mt di Progetto [daNm] : -3859

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.6
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.354
f_s	: 2.82

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.592	Coefficiente di sfruttamento nel piano XZ	: 0.592
f_s	: 1.690		

Colonna 27 Primo Imp[Colonna]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $-\gamma_M=1.45$ (FC=1)
L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.753 ($f_s=1.328$)

Sforzo Normale di Progetto [daN]	: -165 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: 10
Momento Flettente M_z di Progetto [daNm]	: 9287

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: -0.02
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.001
f_s	: 884.78
Tensione di Progetto relativa a M_y [N/mm ²]	: 0.04
Tensione di Progetto relativa a M_z [N/mm ²]	: 13.93
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.753
f_s	: 1.33
Coefficiente di Sfruttamento a pressoflessione	: 0.753
f_s	: 1.33

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.114 ($f_s=8.755$)

Taglio T_y di Progetto [daN]	: -1617
Taglio T_z di Progetto [daN]	: 30
Momento Torcente M_t di Progetto [daNm]	: 5920

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.3
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.114
f_s	: 8.76

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.754	Coefficiente di sfruttamento nel piano XZ	: 0.754
fs	: 1.326		

Colonna 87 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.262 (fs=3.812)

Sforzo Normale di Progetto [daN]	: -4467 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 14
Momento Flettente Mz di Progetto [daNm]	: -2017

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²]	: -0.56
Tensione Resistente [N/mm²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.048
fs	: 20.75
Tensione di Progetto relativa a My [N/mm²]	: 0.07
Tensione di Progetto relativa a Mz [N/mm²]	: 3.03
Tensione Resistente relativa a My [N/mm²]	: 12.74
Tensione Resistente relativa a Mz [N/mm²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.26
fs	: 3.85
Coefficiente di Sfruttamento a pressoflessione	: 0.262
fs	: 3.81

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 39 [SLV] [IN] " - Coeff. Sfruttamento : 0.138 (fs=7.268)

Taglio Ty di Progetto [daN]	: -1928
Taglio Tz di Progetto [daN]	: 283
Momento Torcente Mt di Progetto [daNm]	: -1022

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.36
Tensione di Progetto relativa a Tz [N/mm²]	: 0.05
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.138
fs	: 7.27

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00

Coefficiente di sfruttamento nel piano XY : 0.308
fs : 3.245

Coefficiente di sfruttamento nel piano XZ : 0.308

Colonna 103 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.581 (fs=1.722)

Sforzo Normale di Progetto [daN] : -200 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : -167
Momento Flettente Mz di Progetto [daNm] : -6841

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.02
Tensione Resistente [N/mm²] : 18.21
Coefficiente di Sfruttamento a compressione : 0.001
fs : 729.35
Tensione di Progetto relativa a My [N/mm²] : 0.78
Tensione di Progetto relativa a Mz [N/mm²] : 10.26
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 18.54
Coefficiente di Sfruttamento a flessione : 0.581
fs : 1.72
Coefficiente di Sfruttamento a pressoflessione : 0.581
fs : 1.72

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa : 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.372)

Taglio Ty di Progetto [daN] : -962
Taglio Tz di Progetto [daN] : -2
Momento Torcente Mt di Progetto [daNm] : -2017

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
Tensione di Progetto relativa a Tz [N/mm²] : 0
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a taglio : 0.107
fs : 9.37

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.582	Coefficiente di sfruttamento nel piano XZ	: 0.582
fs	: 1.718		

Colonna 151 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**
Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.7 (fs=1.428)
 Sforzo Normale di Progetto [daN] : 628 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 43
 Momento Flettente Mz di Progetto [daNm] : -8502

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.08
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.005
 fs : 188.83
 Tensione di Progetto relativa a My [N/mm²] : 0.2
 Tensione di Progetto relativa a Mz [N/mm²] : 12.75
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.695
 fs : 1.44
 Coefficiente di Sfruttamento : 0.7
 fs : 1.43

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**
Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.198 (fs=5.061)
 Taglio Ty di Progetto [daN] : -2793
 Taglio Tz di Progetto [daN] : 172
 Momento Torcente Mt di Progetto [daNm] : -6839

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.52
 Tensione di Progetto relativa a Tz [N/mm²] : 0.03
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.198
 fs : 5.06

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.695	Coefficiente di sfruttamento nel piano XZ	: 0.695
fs	: 1.439		

Colonna 27 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
 L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**
Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.689 (fs=1.452)
 Sforzo Normale di Progetto [daN] : 5424 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : 35
 Momento Flettente Mz di Progetto [daNm] : -7880

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.68
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.046
 fs : 21.88
 Tensione di Progetto relativa a My [N/mm²] : 0.17
 Tensione di Progetto relativa a Mz [N/mm²] : 11.82
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.643
 fs : 1.55
 Coefficiente di Sfruttamento : 0.689
 fs : 1.45

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.455 (fs=2.198)

Taglio Ty di Progetto [daN] : 6436
 Taglio Tz di Progetto [daN] : 312
 Momento Torcente Mt di Progetto [daNm] : -7880

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 1.21
 Tensione di Progetto relativa a Tz [N/mm²] : 0.06
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.455
 fs : 2.2

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.643	Coefficiente di sfruttamento nel piano XZ	: 0.643
fs	: 1.555		

Colonna 28 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.783 (fs=1.277)

Sforzo Normale di Progetto [daN] : 108 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -75
 Momento Flettente Mz di Progetto [daNm] : -9518

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.01
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.001

fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 0.35
Tensione di Progetto relativa a Mz [N/mm ²]	: 14.28
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.782
fs	: 1.28
Coefficiente di Sfruttamento	: 0.783
fs	: 1.28

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.12 (fs=8.354)

Taglio Ty di Progetto [daN]	: 1683
Taglio Tz di Progetto [daN]	: -202
Momento Torcente Mt di Progetto [daNm]	: -4608

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.32
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.04
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.12
fs	: 8.35

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.782	Coefficiente di sfruttamento nel piano XZ	: 0.782
fs	: 1.278		

Colonna 148 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.816 (fs=1.225)

Sforzo Normale di Progetto [daN]	: -5645 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -3019
Momento Flettente Mz di Progetto [daNm]	: 1910

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.71
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.039
fs	: 25.8
Tensione di Progetto relativa a My [N/mm ²]	: 14.15
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.86
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.815
fs	: 1.23

Coefficiente di Sfruttamento a pressoflessione : 0.816
fs : 1.23

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.348)
Taglio Ty di Progetto [daN] : 964
Taglio Tz di Progetto [daN] : 18
Momento Torcente Mt di Progetto [daNm] : 1192

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a taglio : 0.107
fs : 9.35

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 50
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.853	Coefficiente di sfruttamento nel piano XZ	: 0.857
fs	: 1.167		

Colonna 28 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**
Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.788 (fs=1.269)
Sforzo Normale di Progetto [daN] : 5589 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : -536
Momento Flettente Mz di Progetto [daNm] : 8075

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.7
Tensione Resistente [N/mm²] : 14.83
Coefficiente di Sfruttamento a trazione : 0.047
fs : 21.23
Tensione di Progetto relativa a My [N/mm²] : 2.51
Tensione di Progetto relativa a Mz [N/mm²] : 12.11
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 18.54
Coefficiente di Sfruttamento a flessione : 0.741
fs : 1.35
Coefficiente di Sfruttamento : 0.788
fs : 1.27

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.354 (fs=2.825)

Taglio Ty di Progetto [daN]	: -3189
Taglio Tz di Progetto [daN]	: -66
Momento Torcente Mt di Progetto [daNm]	: 3860

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.6
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.354
fs	: 2.83

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 26
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.760	Coefficiente di sfruttamento nel piano XZ	: 0.760
fs	: 1.316		

Colonna 29 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.823 (fs=1.216)

Sforzo Normale di Progetto [daN]	: -679 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -35
Momento Flettente Mz di Progetto [daNm]	: 10099

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.08
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 214.41
Tensione di Progetto relativa a My [N/mm ²]	: 0.16
Tensione di Progetto relativa a Mz [N/mm ²]	: 15.15
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.823
fs	: 1.22
Coefficiente di Sfruttamento a pressoflessione	: 0.823
fs	: 1.22

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.114 (fs=8.801)

Taglio Ty di Progetto [daN]	: -1609
Taglio Tz di Progetto [daN]	: 31
Momento Torcente Mt di Progetto [daNm]	: 4887

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.3
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.01

Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.114
fs	: 8.8

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 10
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.827	Coefficiente di sfruttamento nel piano XZ	: 0.828
fs	: 1.207		

Colonna 88 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.283 (fs=3.54)

Sforzo Normale di Progetto [daN]	: -134 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -28
Momento Flettente Mz di Progetto [daNm]	: -3436

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.02
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.001
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 0.13
Tensione di Progetto relativa a Mz [N/mm ²]	: 5.15
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.283
fs	: 3.54
Coefficiente di Sfruttamento a pressoflessione	: 0.283
fs	: 3.54

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.393)

Taglio Ty di Progetto [daN]	: -959
Taglio Tz di Progetto [daN]	: 3
Momento Torcente Mt di Progetto [daNm]	: -1201

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm ²]	: 0
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.106
fs	: 9.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
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Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.306	Coefficiente di sfruttamento nel piano XZ	: 0.306
fs	: 3.269		

Colonna 104 Copertur[Colonna]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $-\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.601 (fs=1.664)

Sforzo Normale di Progetto [daN]	: 758 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -69
Momento Flettente Mz di Progetto [daNm]	: -7208

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.09
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.006
fs	: 156.45
Tensione di Progetto relativa a My [N/mm²]	: 0.32
Tensione di Progetto relativa a Mz [N/mm²]	: 10.81
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.594
fs	: 1.68
Coefficiente di Sfruttamento	: 0.601
fs	: 1.66

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.385)

Taglio Ty di Progetto [daN]	: -959
Taglio Tz di Progetto [daN]	: -40
Momento Torcente Mt di Progetto [daNm]	: -2019

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm²]	: 0.01
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.107
fs	: 9.38

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.594	Coefficiente di sfruttamento nel piano XZ	: 0.594
fs	: 1.682		

Colonna 155 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.754 (fs=1.326)

Sforzo Normale di Progetto [daN] : 788 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 114
Momento Flettente Mz di Progetto [daNm] : -9009

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.1
Tensione Resistente [N/mm²] : 14.83
Coefficiente di Sfruttamento a trazione : 0.007
fs : 150.56
Tensione di Progetto relativa a My [N/mm²] : 0.54
Tensione di Progetto relativa a Mz [N/mm²] : 13.51
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 18.54
Coefficiente di Sfruttamento a flessione : 0.748
fs : 1.34
Coefficiente di Sfruttamento : 0.754
fs : 1.33

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.384)

Taglio Ty di Progetto [daN] : -960
Taglio Tz di Progetto [daN] : -29
Momento Torcente Mt di Progetto [daNm] : -3599

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
Tensione di Progetto relativa a Tz [N/mm²] : 0.01
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a taglio : 0.107
fs : 9.38

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.748	Coefficiente di sfruttamento nel piano XZ	: 0.748
fs	: 1.338		

Colonna 29 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**
Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.733 (fs=1.363)
 Sforzo Normale di Progetto [daN] : 5381 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 76
 Momento Flettente Mz di Progetto [daNm] : -8351

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.67
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.045
 fs : 22.05
 Tensione di Progetto relativa a My [N/mm²] : 0.36
 Tensione di Progetto relativa a Mz [N/mm²] : 12.53
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.688
 fs : 1.45
 Coefficiente di Sfruttamento : 0.733
 fs : 1.36

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.352 (fs=2.838)
 Taglio Ty di Progetto [daN] : 3174
 Taglio Tz di Progetto [daN] : 86
 Momento Torcente Mt di Progetto [daNm] : -3856

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.6
 Tensione di Progetto relativa a Tz [N/mm²] : 0.02
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.352
 fs : 2.84

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.688	Coefficiente di sfruttamento nel piano XZ	: 0.688
fs	: 1.453		

Colonna 30 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.85 (fs=1.176)
 Sforzo Normale di Progetto [daN] : -1031 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 167
 Momento Flettente Mz di Progetto [daNm] : -10173

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.13
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.007
fs	: 141.32
Tensione di Progetto relativa a My [N/mm ²]	: 0.78
Tensione di Progetto relativa a Mz [N/mm ²]	: 15.26
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.85
fs	: 1.18
Coefficiente di Sfruttamento a pressoflessione	: 0.85
fs	: 1.18

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.149 (fs=6.7)

Taglio Ty di Progetto [daN]	: 2102
Taglio Tz di Progetto [daN]	: -219
Momento Torcente Mt di Progetto [daNm]	: -3155

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.39
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.04
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.149
fs	: 6.7

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 17
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.857	Coefficiente di sfruttamento nel piano XZ	: 0.859
fs	: 1.164		

Colonna 152 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.842 (fs=1.187)

Sforzo Normale di Progetto [daN]	: -1279 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -3040
Momento Flettente Mz di Progetto [daNm]	: 2303

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.16
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.009
fs	: 113.9
Tensione di Progetto relativa a My [N/mm ²]	: 14.25

Tensione di Progetto relativa a M_z [N/mm ²]	: 3.45
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.842
f_s	: 1.19
Coefficiente di Sfruttamento a pressoflessione	: 0.842
f_s	: 1.19

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 48 [SLV] [IN] " - Coeff. Sfruttamento : 0.175 ($f_s=5.725$)

Taglio T_y di Progetto [daN]	: 2046
Taglio T_z di Progetto [daN]	: 1390
Momento Torcente M_t di Progetto [daNm]	: 370

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.38
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.26
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.175
f_s	: 5.73

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente K_c nel piano XY	: 1.00	Coefficiente K_c nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.850	Coefficiente di sfruttamento nel piano XZ	: 0.852
f_s	: 1.174		

Colonna 30 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.817 ($f_s=1.224$)

Sforzo Normale di Progetto [daN]	: 5643 (TRAZIONE)
Momento Flettente M_y di Progetto [daNm]	: -565
Momento Flettente M_z di Progetto [daNm]	: 8368

Tipo Verifica : TRAZIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: 0.71
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.048
f_s	: 21.03
Tensione di Progetto relativa a M_y [N/mm ²]	: 2.65
Tensione di Progetto relativa a M_z [N/mm ²]	: 12.55
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.77
f_s	: 1.3
Coefficiente di Sfruttamento	: 0.817
f_s	: 1.22

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.352 (fs=2.839)
 Taglio Ty di Progetto [daN] : -3173
 Taglio Tz di Progetto [daN] : -90
 Momento Torcente Mt di Progetto [daNm] : 3855

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.59
 Tensione di Progetto relativa a Tz [N/mm²] : 0.02
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.352
 fs : 2.84

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 17
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.770	Coefficiente di sfruttamento nel piano XZ	: 0.770
fs	: 1.299		

Colonna 31 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
 L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.853 (fs=1.172)
 Sforzo Normale di Progetto [daN] : -667 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 13
 Momento Flettente Mz di Progetto [daNm] : 10518

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.08
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.005
 fs : 218.32
 Tensione di Progetto relativa a My [N/mm²] : 0.06
 Tensione di Progetto relativa a Mz [N/mm²] : 15.78
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.853
 fs : 1.17
 Coefficiente di Sfruttamento a pressoflessione : 0.853
 fs : 1.17

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.13 (fs=7.688)
 Taglio Ty di Progetto [daN] : -1842
 Taglio Tz di Progetto [daN] : -34

Momento Torcente Mt di Progetto [daNm] : 5038

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.35
 Tensione di Progetto relativa a Tz [N/mm²] : 0.01
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.13
 fs : 7.69

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 10
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.858	Coefficiente di sfruttamento nel piano XZ	: 0.859
fs	: 1.165		

Colonna 89 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.295 (fs=3.395)

Sforzo Normale di Progetto [daN] : 126 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 28
 Momento Flettente Mz di Progetto [daNm] : -3570

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.02
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.001
 fs : 940.21
 Tensione di Progetto relativa a My [N/mm²] : 0.13
 Tensione di Progetto relativa a Mz [N/mm²] : 5.36
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.293
 fs : 3.41
 Coefficiente di Sfruttamento : 0.295
 fs : 3.4

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.384)

Taglio Ty di Progetto [daN] : -959
 Taglio Tz di Progetto [daN] : -48
 Momento Torcente Mt di Progetto [daNm] : -1202

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0.01
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.107

fs

: 9.38

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.304	Coefficiente di sfruttamento nel piano XZ	: 0.304
fs	: 3.287		

Colonna 105 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.613 (fs=1.632)

Sforzo Normale di Progetto [daN]	: 752 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 97
Momento Flettente Mz di Progetto [daNm]	: -7299

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.09
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.006
fs	: 157.9
Tensione di Progetto relativa a My [N/mm²]	: 0.45
Tensione di Progetto relativa a Mz [N/mm²]	: 10.95
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.606
fs	: 1.65
Coefficiente di Sfruttamento	: 0.613
fs	: 1.63

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.391)

Taglio Ty di Progetto [daN]	: -959
Taglio Tz di Progetto [daN]	: -28
Momento Torcente Mt di Progetto [daNm]	: -2020

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm²]	: 0.01
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.106
fs	: 9.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40

Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.606	Coefficiente di sfruttamento nel piano XZ	: 0.606
fs	: 1.649		

Colonna 159 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.774 (fs=1.292)

Sforzo Normale di Progetto [daN]	: 111 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 115
Momento Flettente Mz di Progetto [daNm]	: -9322

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.01
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.001
fs	: 1000
Tensione di Progetto relativa a My [N/mm²]	: 0.54
Tensione di Progetto relativa a Mz [N/mm²]	: 13.98
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.773
fs	: 1.29
Coefficiente di Sfruttamento	: 0.774
fs	: 1.29

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.223 (fs=4.479)

Taglio Ty di Progetto [daN]	: -3162
Taglio Tz di Progetto [daN]	: 3
Momento Torcente Mt di Progetto [daNm]	: -7447

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.59
Tensione di Progetto relativa a Tz [N/mm²]	: 0
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.223
fs	: 4.48

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 10
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.773	Coefficiente di sfruttamento nel piano XZ	: 0.773
fs	: 1.294		

Colonna 31 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.764 ($f_s=1.31$)

Sforzo Normale di Progetto [daN] : 5694 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 99
Momento Flettente Mz di Progetto [daNm] : -8645

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.71
Tensione Resistente [N/mm²] : 14.83
Coefficiente di Sfruttamento a trazione : 0.048
 f_s : 20.84
Tensione di Progetto relativa a My [N/mm²] : 0.46
Tensione di Progetto relativa a Mz [N/mm²] : 12.97
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 18.54
Coefficiente di Sfruttamento a flessione : 0.716
 f_s : 1.4
Coefficiente di Sfruttamento : 0.764
 f_s : 1.31

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.483 ($f_s=2.072$)

Taglio Ty di Progetto [daN] : 6822
Taglio Tz di Progetto [daN] : 429
Momento Torcente Mt di Progetto [daNm] : -8331

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 1.28
Tensione di Progetto relativa a Tz [N/mm²] : 0.08
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.483
 f_s : 2.07

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 10
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.716	Coefficiente di sfruttamento nel piano XZ	: 0.716
f_s	: 1.397		

Colonna 32 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.836 (fs=1.197)

Sforzo Normale di Progetto [daN] : -282 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -81
 Momento Flettente Mz di Progetto [daNm] : -10167

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.04
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.002
 fs : 515.69
 Tensione di Progetto relativa a My [N/mm²] : 0.38
 Tensione di Progetto relativa a Mz [N/mm²] : 15.25
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.836
 fs : 1.2
 Coefficiente di Sfruttamento a pressoflessione : 0.836
 fs : 1.2

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.394)

Taglio Ty di Progetto [daN] : 959
 Taglio Tz di Progetto [daN] : 0
 Momento Torcente Mt di Progetto [daNm] : -2406

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.106
 fs : 9.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.838	Coefficiente di sfruttamento nel piano XZ	: 0.838
fs	: 1.193		

Colonna 156 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.847 (fs=1.18)

Sforzo Normale di Progetto [daN] : 53 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -622
 Momento Flettente Mz di Progetto [daNm] : 9209

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.01
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.000
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 2.92
Tensione di Progetto relativa a Mz [N/mm ²]	: 13.81
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.847
fs	: 1.18
Coefficiente di Sfruttamento	: 0.847
fs	: 1.18

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.204 (fs=4.896)

Taglio Ty di Progetto [daN]	: 2884
Taglio Tz di Progetto [daN]	: -221
Momento Torcente Mt di Progetto [daNm]	: 1983

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.54
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.04
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.204
fs	: 4.9

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 17
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.847	Coefficiente di sfruttamento nel piano XZ	: 0.847
fs	: 1.181		

Colonna 32 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.832 (fs=1.202)

Sforzo Normale di Progetto [daN]	: 5477 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -578
Momento Flettente Mz di Progetto [daNm]	: 8540

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.68
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.046
fs	: 21.67
Tensione di Progetto relativa a My [N/mm ²]	: 2.71
Tensione di Progetto relativa a Mz [N/mm ²]	: 12.81
Tensione Resistente relativa a My [N/mm ²]	: 20.03

Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.786
f_s	: 1.27
Coefficiente di Sfruttamento	: 0.832
f_s	: 1.2

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 20 [SLD] [IN] " - Coeff. Sfruttamento : 0.47 ($f_s=2.126$)

Taglio T_y di Progetto [daN]	: -6631
Taglio T_z di Progetto [daN]	: -638
Momento Torcente M_t di Progetto [daNm]	: 8215

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 1.24
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.12
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.47
f_s	: 2.13

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 17
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente K_c nel piano XY	: 1.00	Coefficiente K_c nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.786	Coefficiente di sfruttamento nel piano XZ	: 0.786
f_s	: 1.273		

Colonna 33 Primo Imp[Colonna]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $-\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.856 ($f_s=1.169$)

Sforzo Normale di Progetto [daN]	: -513 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: 13
Momento Flettente M_z di Progetto [daNm]	: 10552

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.004
f_s	: 283.87
Tensione di Progetto relativa a M_y [N/mm ²]	: 0.06
Tensione di Progetto relativa a M_z [N/mm ²]	: 15.83
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.856
f_s	: 1.17
Coefficiente di Sfruttamento a pressoflessione	: 0.856
f_s	: 1.17

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.105 (fs=9.48)
 Taglio Ty di Progetto [daN] : -951
 Taglio Tz di Progetto [daN] : -1
 Momento Torcente Mt di Progetto [daNm] : 2383

Tipo Verifica : TAGLIO
 Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.105
 fs : 9.48

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 10
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.859	Coefficiente di sfruttamento nel piano XZ	: 0.860
fs	: 1.163		

Colonna 90 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**
Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.289 (fs=3.465)
 Sforzo Normale di Progetto [daN] : 203 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -13
 Momento Flettente Mz di Progetto [daNm] : -3519

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1
 Tensione di Progetto [N/mm²] : 0.03
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.002
 fs : 584.45
 Tensione di Progetto relativa a My [N/mm²] : 0.06
 Tensione di Progetto relativa a Mz [N/mm²] : 5.28
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.287
 fs : 3.49
 Coefficiente di Sfruttamento : 0.289
 fs : 3.47

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.397)
 Taglio Ty di Progetto [daN] : -959
 Taglio Tz di Progetto [daN] : -23
 Momento Torcente Mt di Progetto [daNm] : -1202

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.106
fs	: 9.4

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.303	Coefficiente di sfruttamento nel piano XZ	: 0.303
fs	: 3.297		

Colonna 111 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1595.24 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1595.24 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.615 (fs=1.625)

Sforzo Normale di Progetto [daN]	: 115 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 108
Momento Flettente Mz di Progetto [daNm]	: -7378

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.01
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.001
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 0.5
Tensione di Progetto relativa a Mz [N/mm ²]	: 11.07
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.615
fs	: 1.63
Coefficiente di Sfruttamento	: 0.615
fs	: 1.62

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1595.24 mm / 1595.24 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.391)

Taglio Ty di Progetto [daN]	: -959
Taglio Tz di Progetto [daN]	: -44
Momento Torcente Mt di Progetto [daNm]	: -2020

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.106
fs	: 9.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.74	Snellezza nel piano XZ	: 24.18
Snellezza relativa nel piano XY	: 0.12	Snellezza relativa nel piano XZ	: 0.38
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.615	Coefficiente di sfruttamento nel piano XZ	: 0.615
fs	: 1.627		

Colonna 163 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 651.63 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 651.63 mm] - **R 500x160**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.787 (fs=1.271)

Sforzo Normale di Progetto [daN]	: 101 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 141
Momento Flettente Mz di Progetto [daNm]	: -9428

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.01
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.001
fs	: 1000
Tensione di Progetto relativa a My [N/mm²]	: 0.66
Tensione di Progetto relativa a Mz [N/mm²]	: 14.14
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.786
fs	: 1.27
Coefficiente di Sfruttamento	: 0.787
fs	: 1.27

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=651.63 mm / 651.63 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.389)

Taglio Ty di Progetto [daN]	: -959
Taglio Tz di Progetto [daN]	: -35
Momento Torcente Mt di Progetto [daNm]	: -3548

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm²]	: 0.01
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.107
fs	: 9.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 3.16	Snellezza nel piano XZ	: 9.88
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.16
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 10
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.51

Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.786	Coefficiente di sfruttamento nel piano XZ	: 0.786
fs	: 1.273		

Colonna 33 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.773 (fs=1.294)

Sforzo Normale di Progetto [daN]	: 5605 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 114
Momento Flettente Mz di Progetto [daNm]	: -8741

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.7
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.047
fs	: 21.17
Tensione di Progetto relativa a My [N/mm ²]	: 0.53
Tensione di Progetto relativa a Mz [N/mm ²]	: 13.11
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.726
fs	: 1.38
Coefficiente di Sfruttamento	: 0.773
fs	: 1.29

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.489 (fs=2.047)

Taglio Ty di Progetto [daN]	: 6903
Taglio Tz di Progetto [daN]	: 464
Momento Torcente Mt di Progetto [daNm]	: -8444

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 1.29
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.09
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.489
fs	: 2.05

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 10
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.726	Coefficiente di sfruttamento nel piano XZ	: 0.726
fs	: 1.378		

Colonna 34 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7
VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.872 (fs=1.147)

Sforzo Normale di Progetto [daN]	: -501 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -125
Momento Flettente Mz di Progetto [daNm]	: -10522

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.003
fs	: 290.68
Tensione di Progetto relativa a My [N/mm ²]	: 0.58
Tensione di Progetto relativa a Mz [N/mm ²]	: 15.78
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.872
fs	: 1.15
Coefficiente di Sfruttamento a pressoflessione	: 0.872
fs	: 1.15

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.133 (fs=7.524)

Taglio Ty di Progetto [daN]	: 1870
Taglio Tz di Progetto [daN]	: -213
Momento Torcente Mt di Progetto [daNm]	: -5319

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.35
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.04
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.133
fs	: 7.52

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 18
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.875	Coefficiente di sfruttamento nel piano XZ	: 0.876
fs	: 1.142		

Colonna 160 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 3100 mm] - **R 500x160**
Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.84 (fs=1.191)

Sforzo Normale di Progetto [daN]	: 98 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -641
Momento Flettente Mz di Progetto [daNm]	: 9073

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.01
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.001
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 3.01
Tensione di Progetto relativa a Mz [N/mm ²]	: 13.61
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.839
fs	: 1.19
Coefficiente di Sfruttamento	: 0.84
fs	: 1.19

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.216 (fs=4.623)

Taglio Ty di Progetto [daN]	: 3002
Taglio Tz di Progetto [daN]	: 608
Momento Torcente Mt di Progetto [daNm]	: 1950

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.56
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.11
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.216
fs	: 4.62

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 17
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.839	Coefficiente di sfruttamento nel piano XZ	: 0.839
fs	: 1.192		

Colonna 34 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.826 (fs=1.21)

Sforzo Normale di Progetto [daN]	: 5878 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -592
Momento Flettente Mz di Progetto [daNm]	: 8402

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.73
Tensione Resistente [N/mm ²]	: 14.83

Coefficiente di Sfruttamento a trazione	: 0.05
fs	: 20.19
Tensione di Progetto relativa a My [N/mm ²]	: 2.77
Tensione di Progetto relativa a Mz [N/mm ²]	: 12.6
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.777
fs	: 1.29
Coefficiente di Sfruttamento	: 0.826
fs	: 1.21

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 19 [SLD] [IN] " - Coeff. Sfruttamento : 0.483 (fs=2.072)

Taglio Ty di Progetto [daN]	: -6811
Taglio Tz di Progetto [daN]	: -553
Momento Torcente Mt di Progetto [daNm]	: 8464

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 1.28
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.1
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.483
fs	: 2.07

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 17
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.777	Coefficiente di sfruttamento nel piano XZ	: 0.777
fs	: 1.288		

Colonna 35 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.866 (fs=1.155)

Sforzo Normale di Progetto [daN]	: -84 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 58
Momento Flettente Mz di Progetto [daNm]	: 10587

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.01
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.001
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 0.27
Tensione di Progetto relativa a Mz [N/mm ²]	: 15.88
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.866

fs	: 1.15
Coefficiente di Sfruttamento a pressoflessione	: 0.866
fs	: 1.15

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - R 500x160	
Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.239 (fs=4.187)	
Taglio Ty di Progetto [daN]	: -3382
Taglio Tz di Progetto [daN]	: 17
Momento Torcente Mt di Progetto [daNm]	: 10599

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.63
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.239
fs	: 4.19

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.867	Coefficiente di sfruttamento nel piano XZ	: 0.867
fs	: 1.154		

Colonna 91 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - R 500x160	
Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.299 (fs=3.344)	
Sforzo Normale di Progetto [daN]	: 582 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 38
Momento Flettente Mz di Progetto [daNm]	: -3560

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.07
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.005
fs	: 203.95
Tensione di Progetto relativa a My [N/mm²]	: 0.18
Tensione di Progetto relativa a Mz [N/mm²]	: 5.34
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.294
fs	: 3.4
Coefficiente di Sfruttamento	: 0.299
fs	: 3.34

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.389)

Taglio Ty di Progetto [daN] : -959
 Taglio Tz di Progetto [daN] : -50
 Momento Torcente Mt di Progetto [daNm] : -1202

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0.01
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.107
 fs : 9.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.304	Coefficiente di sfruttamento nel piano XZ	: 0.304
fs	: 3.292		

Colonna 112 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.628 (fs=1.593)

Sforzo Normale di Progetto [daN] : 593 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 102
 Momento Flettente Mz di Progetto [daNm] : -7494

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.07
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.005
 fs : 200.25
 Tensione di Progetto relativa a My [N/mm²] : 0.48
 Tensione di Progetto relativa a Mz [N/mm²] : 11.24
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.623
 fs : 1.61
 Coefficiente di Sfruttamento : 0.628
 fs : 1.59

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa : 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.132 (fs=7.58)

Taglio Ty di Progetto [daN] : -1845
 Taglio Tz di Progetto [daN] : -296
 Momento Torcente Mt di Progetto [daNm] : -2023

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.35

Tensione di Progetto relativa a Tz [N/mm ²]	: 0.06
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.132
fs	: 7.58

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.623	Coefficiente di sfruttamento nel piano XZ	: 0.623
fs	: 1.605		

Colonna 167 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.779 (fs=1.284)

Sforzo Normale di Progetto [daN]	: 105 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 151
Momento Flettente Mz di Progetto [daNm]	: -9312

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.01
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.001
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 0.71
Tensione di Progetto relativa a Mz [N/mm ²]	: 13.97
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.778
fs	: 1.29
Coefficiente di Sfruttamento	: 0.779
fs	: 1.28

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 12 [SLD] [IN] " - Coeff. Sfruttamento : 0.219 (fs=4.564)

Taglio Ty di Progetto [daN]	: -3102
Taglio Tz di Progetto [daN]	: -25
Momento Torcente Mt di Progetto [daNm]	: -7482

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.58
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.219
fs	: 4.56

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.778	Coefficiente di sfruttamento nel piano XZ	: 0.778
fs	: 1.285		

Colonna 35 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.766 (fs=1.305)

Sforzo Normale di Progetto [daN]	: 5762 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 123
Momento Flettente Mz di Progetto [daNm]	: -8622

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.72
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.049
fs	: 20.59
Tensione di Progetto relativa a My [N/mm²]	: 0.58
Tensione di Progetto relativa a Mz [N/mm²]	: 12.93
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.718
fs	: 1.39
Coefficiente di Sfruttamento	: 0.766
fs	: 1.31

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.5 (fs=1.999)

Taglio Ty di Progetto [daN]	: 7082
Taglio Tz di Progetto [daN]	: 195
Momento Torcente Mt di Progetto [daNm]	: -8637

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 1.33
Tensione di Progetto relativa a Tz [N/mm²]	: 0.04
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.5
fs	: 2

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.719	Coefficiente di sfruttamento nel piano XZ	: 0.719

fs : 1.391

Colonna 36 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)
L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.868 (fs=1.152)

Sforzo Normale di Progetto [daN] : -610 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : -123
Momento Flettente Mz di Progetto [daNm] : -10484

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.08
Tensione Resistente [N/mm²] : 18.21
Coefficiente di Sfruttamento a compressione : 0.004
fs : 238.77
Tensione di Progetto relativa a My [N/mm²] : 0.58
Tensione di Progetto relativa a Mz [N/mm²] : 15.73
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 18.54
Coefficiente di Sfruttamento a flessione : 0.868
fs : 1.15
Coefficiente di Sfruttamento a pressoflessione : 0.868
fs : 1.15

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.232 (fs=4.308)

Taglio Ty di Progetto [daN] : 3286
Taglio Tz di Progetto [daN] : 65
Momento Torcente Mt di Progetto [daNm] : -10243

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.62
Tensione di Progetto relativa a Tz [N/mm²] : 0.01
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.232
fs : 4.31

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 18
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.873	Coefficiente di sfruttamento nel piano XZ	: 0.873
fs	: 1.145		

Colonna 164 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)
L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.845 (fs=1.183)

Sforzo Normale di Progetto [daN] : 384 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -653
 Momento Flettente Mz di Progetto [daNm] : 9084

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.05
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.003
 fs : 309.2
 Tensione di Progetto relativa a My [N/mm²] : 3.06
 Tensione di Progetto relativa a Mz [N/mm²] : 13.63
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.842
 fs : 1.19
 Coefficiente di Sfruttamento : 0.845
 fs : 1.18

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.21 (fs=4.77)

Taglio Ty di Progetto [daN] : 2905
 Taglio Tz di Progetto [daN] : 615
 Momento Torcente Mt di Progetto [daNm] : -577

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.54
 Tensione di Progetto relativa a Tz [N/mm²] : 0.12
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.21
 fs : 4.77

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 17
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.842	Coefficiente di sfruttamento nel piano XZ	: 0.842
fs	: 1.188		

Colonna 36 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.828 (fs=1.208)

Sforzo Normale di Progetto [daN] : 5804 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -600

Momento Flettente Mz di Progetto [daNm] : 8414

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.73
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.049
 fs : 20.45
 Tensione di Progetto relativa a My [N/mm²] : 2.81
 Tensione di Progetto relativa a Mz [N/mm²] : 12.62
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.779
 fs : 1.28
 Coefficiente di Sfruttamento : 0.828
 fs : 1.21

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.483 (fs=2.072)

Taglio Ty di Progetto [daN] : -6813
 Taglio Tz di Progetto [daN] : -545
 Momento Torcente Mt di Progetto [daNm] : 8532

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 1.28
 Tensione di Progetto relativa a Tz [N/mm²] : 0.1
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.483
 fs : 2.07

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 17
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.779	Coefficiente di sfruttamento nel piano XZ	: 0.779
fs	: 1.284		

Colonna 37 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.845 (fs=1.183)

Sforzo Normale di Progetto [daN] : -213 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 31
 Momento Flettente Mz di Progetto [daNm] : 10382

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.03
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.001
 fs : 682.87

Tensione di Progetto relativa a M_y [N/mm ²]	: 0.15
Tensione di Progetto relativa a M_z [N/mm ²]	: 15.57
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.845
f_s	: 1.18
Coefficiente di Sfruttamento a pressoflessione	: 0.845
f_s	: 1.18

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.142 ($f_s=7.04$)

Taglio T_y di Progetto [daN]	: -2011
Taglio T_z di Progetto [daN]	: 50
Momento Torcente M_t di Progetto [daNm]	: 5637

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.38
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.142
f_s	: 7.04

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente K_c nel piano XY	: 1.00	Coefficiente K_c nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.847	Coefficiente di sfruttamento nel piano XZ	: 0.847
f_s	: 1.181		

Colonna 92 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.286 ($f_s=3.494$)

Sforzo Normale di Progetto [daN]	: 442 (TRAZIONE)
Momento Flettente M_y di Progetto [daNm]	: 14
Momento Flettente M_z di Progetto [daNm]	: -3463

Tipo Verifica : TRAZIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: 0.06
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.004
f_s	: 268.66
Tensione di Progetto relativa a M_y [N/mm ²]	: 0.07
Tensione di Progetto relativa a M_z [N/mm ²]	: 5.2
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.283
f_s	: 3.54
Coefficiente di Sfruttamento	: 0.286

fs

: 3.49

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.218 (fs=4.585)

Taglio Ty di Progetto [daN] : -3086
 Taglio Tz di Progetto [daN] : -124
 Momento Torcente Mt di Progetto [daNm] : -1947

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.58
 Tensione di Progetto relativa a Tz [N/mm²] : 0.02
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.218
 fs : 4.59

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.303	Coefficiente di sfruttamento nel piano XZ	: 0.303
fs	: 3.296		

Colonna 113 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.644 (fs=1.554)

Sforzo Normale di Progetto [daN] : 379 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 171
 Momento Flettente Mz di Progetto [daNm] : -7572

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.05
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.003
 fs : 313.26
 Tensione di Progetto relativa a My [N/mm²] : 0.8
 Tensione di Progetto relativa a Mz [N/mm²] : 11.36
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.64
 fs : 1.56
 Coefficiente di Sfruttamento : 0.644
 fs : 1.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.11 (fs=9.097)

Taglio Ty di Progetto [daN] : -1538

Taglio Tz di Progetto [daN] : 240
 Momento Torcente Mt di Progetto [daNm] : -2855

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.29
 Tensione di Progetto relativa a Tz [N/mm²] : 0.05
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.11
 fs : 9.1

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.640	Coefficiente di sfruttamento nel piano XZ	: 0.640
fs	: 1.561		

Colonna 171 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
 L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.798 (fs=1.253)

Sforzo Normale di Progetto [daN] : 983 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 172
 Momento Flettente Mz di Progetto [daNm] : -9414

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.12
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.008
 fs : 120.76
 Tensione di Progetto relativa a My [N/mm²] : 0.81
 Tensione di Progetto relativa a Mz [N/mm²] : 14.12
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.79
 fs : 1.27
 Coefficiente di Sfruttamento : 0.798
 fs : 1.25

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.389)

Taglio Ty di Progetto [daN] : -959
 Taglio Tz di Progetto [daN] : -45
 Momento Torcente Mt di Progetto [daNm] : -3598

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0.01
 Tensione tang. Resistente [N/mm²] : 1.69

Coefficiente di Sfruttamento a taglio : 0.107
fs : 9.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.790	Coefficiente di sfruttamento nel piano XZ	: 0.790
fs	: 1.266		

Colonna 37 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.777 (fs=1.286)

Sforzo Normale di Progetto [daN]	: 5793 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 138
Momento Flettente Mz di Progetto [daNm]	: -8726

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.72
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.049
fs	: 20.49
Tensione di Progetto relativa a My [N/mm²]	: 0.65
Tensione di Progetto relativa a Mz [N/mm²]	: 13.09
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.729
fs	: 1.37
Coefficiente di Sfruttamento	: 0.777
fs	: 1.29

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.504 (fs=1.985)

Taglio Ty di Progetto [daN]	: 7132
Taglio Tz di Progetto [daN]	: 235
Momento Torcente Mt di Progetto [daNm]	: -8726

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 1.34
Tensione di Progetto relativa a Tz [N/mm²]	: 0.04
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.504
fs	: 1.98

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70

Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.729	Coefficiente di sfruttamento nel piano XZ	: 0.729
fs	: 1.373		

Colonna 38 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.872 (fs=1.147)

Sforzo Normale di Progetto [daN]	: -349 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 124
Momento Flettente Mz di Progetto [daNm]	: -10527

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.04
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.002
fs	: 417.09
Tensione di Progetto relativa a My [N/mm²]	: 0.58
Tensione di Progetto relativa a Mz [N/mm²]	: 15.79
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.872
fs	: 1.15
Coefficiente di Sfruttamento a pressoflessione	: 0.872
fs	: 1.15

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.39)

Taglio Ty di Progetto [daN]	: 960
Taglio Tz di Progetto [daN]	: 0
Momento Torcente Mt di Progetto [daNm]	: -2403

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm²]	: 0
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.106
fs	: 9.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 14
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.874	Coefficiente di sfruttamento nel piano XZ	: 0.875
fs	: 1.143		

Colonna 168 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.843 (fs=1.186)

Sforzo Normale di Progetto [daN] : 545 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : -666
Momento Flettente Mz di Progetto [daNm] : 9018

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.07
Tensione Resistente [N/mm²] : 14.83
Coefficiente di Sfruttamento a trazione : 0.005
fs : 217.67
Tensione di Progetto relativa a My [N/mm²] : 3.12
Tensione di Progetto relativa a Mz [N/mm²] : 13.53
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 18.54
Coefficiente di Sfruttamento a flessione : 0.839
fs : 1.19
Coefficiente di Sfruttamento : 0.843
fs : 1.19

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.394)

Taglio Ty di Progetto [daN] : 959
Taglio Tz di Progetto [daN] : 38
Momento Torcente Mt di Progetto [daNm] : 1205

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
Tensione di Progetto relativa a Tz [N/mm²] : 0.01
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a taglio : 0.106
fs : 9.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 41
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.849	Coefficiente di sfruttamento nel piano XZ	: 0.851
fs	: 1.175		

Colonna 38 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**
Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.826 (fs=1.211)
 Sforzo Normale di Progetto [daN] : 5837 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -611
 Momento Flettente Mz di Progetto [daNm] : 8359

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.73
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.049
 fs : 20.33
 Tensione di Progetto relativa a My [N/mm²] : 2.87
 Tensione di Progetto relativa a Mz [N/mm²] : 12.54
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.776
 fs : 1.29
 Coefficiente di Sfruttamento : 0.826
 fs : 1.21

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**
Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.478 (fs=2.091)
 Taglio Ty di Progetto [daN] : -6732
 Taglio Tz di Progetto [daN] : -731
 Momento Torcente Mt di Progetto [daNm] : 8610

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 1.26
 Tensione di Progetto relativa a Tz [N/mm²] : 0.14
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.478
 fs : 2.09

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 17
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.776	Coefficiente di sfruttamento nel piano XZ	: 0.776
fs	: 1.288		

Colonna 39 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.848 (fs=1.179)
 Sforzo Normale di Progetto [daN] : -60 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 34
 Momento Flettente Mz di Progetto [daNm] : 10414

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.01
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.000
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 0.16
Tensione di Progetto relativa a Mz [N/mm ²]	: 15.62
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.848
fs	: 1.18
Coefficiente di Sfruttamento a pressoflessione	: 0.848
fs	: 1.18

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.166 (fs=6.04)

Taglio Ty di Progetto [daN]	: -2344
Taglio Tz di Progetto [daN]	: 43
Momento Torcente Mt di Progetto [daNm]	: 6431

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.44
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.166
fs	: 6.04

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.848	Coefficiente di sfruttamento nel piano XZ	: 0.849
fs	: 1.178		

Colonna 93 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.291 (fs=3.438)

Sforzo Normale di Progetto [daN]	: -138 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -15
Momento Flettente Mz di Progetto [daNm]	: -3566

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.02
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.001
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 0.07
Tensione di Progetto relativa a Mz [N/mm ²]	: 5.35

Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.291
f_s	: 3.44
Coefficiente di Sfruttamento a pressoflessione	: 0.291
f_s	: 3.44

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 ($f_s=9.403$)

Taglio T_y di Progetto [daN]	: -958
Taglio T_z di Progetto [daN]	: -16
Momento Torcente M_t di Progetto [daNm]	: -1203

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.18
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.106
f_s	: 9.4

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente K_c nel piano XY	: 1.00	Coefficiente K_c nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.306	Coefficiente di sfruttamento nel piano XZ	: 0.306
f_s	: 3.270		

Colonna 114 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**
Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.635 ($f_s=1.574$)

Sforzo Normale di Progetto [daN]	: 658 (TRAZIONE)
Momento Flettente M_y di Progetto [daNm]	: 162
Momento Flettente M_z di Progetto [daNm]	: -7458

Tipo Verifica : TRAZIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: 0.08
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.006
f_s	: 180.24
Tensione di Progetto relativa a M_y [N/mm ²]	: 0.76
Tensione di Progetto relativa a M_z [N/mm ²]	: 11.19
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.63
f_s	: 1.59
Coefficiente di Sfruttamento	: 0.635
f_s	: 1.57

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.392)

Taglio Ty di Progetto [daN]	: -958
Taglio Tz di Progetto [daN]	: -49
Momento Torcente Mt di Progetto [daNm]	: -2021

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm²]	: 0.01
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.106
fs	: 9.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.630	Coefficiente di sfruttamento nel piano XZ	: 0.630
fs	: 1.587		

Colonna 174 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa: 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.781 (fs=1.281)

Sforzo Normale di Progetto [daN]	: -227 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 176
Momento Flettente Mz di Progetto [daNm]	: -9296

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.03
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.002
fs	: 642.77
Tensione di Progetto relativa a My [N/mm²]	: 0.82
Tensione di Progetto relativa a Mz [N/mm²]	: 13.94
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.781
fs	: 1.28
Coefficiente di Sfruttamento a pressoflessione	: 0.781
fs	: 1.28

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.205 (fs=4.87)

Taglio Ty di Progetto [daN]	: -2908
Taglio Tz di Progetto [daN]	: 21
Momento Torcente Mt di Progetto [daNm]	: -7356

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.55
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.205
fs	: 4.87

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.782	Coefficiente di sfruttamento nel piano XZ	: 0.782
fs	: 1.278		

Colonna 39 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.765 (fs=1.308)

Sforzo Normale di Progetto [daN]	: 5217 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 144
Momento Flettente Mz di Progetto [daNm]	: -8615

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.65
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.044
fs	: 22.75
Tensione di Progetto relativa a My [N/mm ²]	: 0.68
Tensione di Progetto relativa a Mz [N/mm ²]	: 12.92
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.721
fs	: 1.39
Coefficiente di Sfruttamento	: 0.765
fs	: 1.31

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.351 (fs=2.846)

Taglio Ty di Progetto [daN]	: 3164
Taglio Tz di Progetto [daN]	: 126
Momento Torcente Mt di Progetto [daNm]	: -3854

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.59
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.02
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.351
fs	: 2.85

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.721	Coefficiente di sfruttamento nel piano XZ	: 0.721
fs	: 1.388		

Colonna 40 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.862 (fs=1.16)

Sforzo Normale di Progetto [daN]	: -1036 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -130
Momento Flettente Mz di Progetto [daNm]	: -10397

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.13
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.007
fs	: 140.54
Tensione di Progetto relativa a My [N/mm²]	: 0.61
Tensione di Progetto relativa a Mz [N/mm²]	: 15.6
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.862
fs	: 1.16
Coefficiente di Sfruttamento a pressoflessione	: 0.862
fs	: 1.16

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.399)

Taglio Ty di Progetto [daN]	: 959
Taglio Tz di Progetto [daN]	: 0
Momento Torcente Mt di Progetto [daNm]	: -2394

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm²]	: 0
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.106
fs	: 9.4

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 18

Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.869	Coefficiente di sfruttamento nel piano XZ	: 0.871
fs	: 1.148		

Colonna 172 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.844 (fs=1.185)

Sforzo Normale di Progetto [daN]	: -3428 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 3090
Momento Flettente Mz di Progetto [daNm]	: 2116

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.43
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.024
fs	: 42.49
Tensione di Progetto relativa a My [N/mm²]	: 14.49
Tensione di Progetto relativa a Mz [N/mm²]	: 3.17
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.843
fs	: 1.19
Coefficiente di Sfruttamento a pressoflessione	: 0.844
fs	: 1.19

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.144 (fs=6.967)

Taglio Ty di Progetto [daN]	: -1992
Taglio Tz di Progetto [daN]	: 406
Momento Torcente Mt di Progetto [daNm]	: 2383

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.37
Tensione di Progetto relativa a Tz [N/mm²]	: 0.08
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.144
fs	: 6.97

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 41
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.867	Coefficiente di sfruttamento nel piano XZ	: 0.869
fs	: 1.151		

Colonna 40 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.799 (fs=1.252)

Sforzo Normale di Progetto [daN] : 5654 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : -616
Momento Flettente Mz di Progetto [daNm] : 8037

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.71
Tensione Resistente [N/mm²] : 14.83
Coefficiente di Sfruttamento a trazione : 0.048
fs : 20.99
Tensione di Progetto relativa a My [N/mm²] : 2.89
Tensione di Progetto relativa a Mz [N/mm²] : 12.06
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 18.54
Coefficiente di Sfruttamento a flessione : 0.751
fs : 1.33
Coefficiente di Sfruttamento : 0.799
fs : 1.25

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.496 (fs=2.014)

Taglio Ty di Progetto [daN] : -7031
Taglio Tz di Progetto [daN] : 4
Momento Torcente Mt di Progetto [daNm] : 8240

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 1.32
Tensione di Progetto relativa a Tz [N/mm²] : 0
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.496
fs : 2.01

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.777	Coefficiente di sfruttamento nel piano XZ	: 0.777
fs	: 1.286		

Colonna 41 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.829 ($f_s=1.206$)

Sforzo Normale di Progetto [daN] : -1050 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 43
 Momento Flettente Mz di Progetto [daNm] : 10164

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.13
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.007
 f_s : 138.76
 Tensione di Progetto relativa a My [N/mm²] : 0.2
 Tensione di Progetto relativa a Mz [N/mm²] : 15.25
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.829
 f_s : 1.21
 Coefficiente di Sfruttamento a pressoflessione : 0.829
 f_s : 1.21

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 ($f_s=9.432$)

Taglio Ty di Progetto [daN] : -955
 Taglio Tz di Progetto [daN] : 2
 Momento Torcente Mt di Progetto [daNm] : 2391

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.106
 f_s : 9.43

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.837	Coefficiente di sfruttamento nel piano XZ	: 0.838
f_s	: 1.193		

Colonna 94 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.29 ($f_s=3.449$)

Sforzo Normale di Progetto [daN] : -241 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 44
 Momento Flettente Mz di Progetto [daNm] : -3495

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.03

Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.002
fs	: 604.67
Tensione di Progetto relativa a My [N/mm ²]	: 0.21
Tensione di Progetto relativa a Mz [N/mm ²]	: 5.24
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.29
fs	: 3.45
Coefficiente di Sfruttamento a pressoflessione	: 0.29
fs	: 3.45

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.383)

Taglio Ty di Progetto [daN]	: -959
Taglio Tz di Progetto [daN]	: -44
Momento Torcente Mt di Progetto [daNm]	: -1201

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.107
fs	: 9.38

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.305	Coefficiente di sfruttamento nel piano XZ	: 0.305
fs	: 3.275		

Colonna 115 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**
Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.603 (fs=1.657)

Sforzo Normale di Progetto [daN]	: 356 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 53
Momento Flettente Mz di Progetto [daNm]	: -7313

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.04
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.003
fs	: 332.93
Tensione di Progetto relativa a My [N/mm ²]	: 0.25
Tensione di Progetto relativa a Mz [N/mm ²]	: 10.97
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54

Coefficiente di Sfruttamento a flessione	: 0.6
fs	: 1.67
Coefficiente di Sfruttamento	: 0.603
fs	: 1.66

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.393)

Taglio Ty di Progetto [daN]	: -959
Taglio Tz di Progetto [daN]	: -10
Momento Torcente Mt di Progetto [daNm]	: -2019

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.106
fs	: 9.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.600	Coefficiente di sfruttamento nel piano XZ	: 0.600
fs	: 1.666		

Colonna 179 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.772 (fs=1.295)

Sforzo Normale di Progetto [daN]	: 623 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 157
Momento Flettente Mz di Progetto [daNm]	: -9161

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.08
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.005
fs	: 190.48
Tensione di Progetto relativa a My [N/mm²]	: 0.73
Tensione di Progetto relativa a Mz [N/mm²]	: 13.74
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.767
fs	: 1.3
Coefficiente di Sfruttamento	: 0.772
fs	: 1.3

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.196 (fs=5.11)

Taglio Ty di Progetto [daN] : -2769
 Taglio Tz di Progetto [daN] : -113
 Momento Torcente Mt di Progetto [daNm] : -6959

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.52
 Tensione di Progetto relativa a Tz [N/mm²] : 0.02
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.196
 fs : 5.11

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.767	Coefficiente di sfruttamento nel piano XZ	: 0.767
fs	: 1.304		

Colonna 41 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.75 (fs=1.333)

Sforzo Normale di Progetto [daN] : 5182 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 124
 Momento Flettente Mz di Progetto [daNm] : -8483

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.65
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.044
 fs : 22.9
 Tensione di Progetto relativa a My [N/mm²] : 0.58
 Tensione di Progetto relativa a Mz [N/mm²] : 12.72
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.707
 fs : 1.42
 Coefficiente di Sfruttamento : 0.75
 fs : 1.33

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.486 (fs=2.057)

Taglio Ty di Progetto [daN] : 6883
 Taglio Tz di Progetto [daN] : 177
 Momento Torcente Mt di Progetto [daNm] : -8483

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 1.29
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.03
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.486
fs	: 2.06

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.707	Coefficiente di sfruttamento nel piano XZ	: 0.707
fs	: 1.415		

Colonna 42 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)
L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.789 (fs=1.267)

Sforzo Normale di Progetto [daN]	: -1861 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -119
Momento Flettente Mz di Progetto [daNm]	: -9514

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.23
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.013
fs	: 78.27
Tensione di Progetto relativa a My [N/mm ²]	: 0.56
Tensione di Progetto relativa a Mz [N/mm ²]	: 14.27
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.789
fs	: 1.27
Coefficiente di Sfruttamento a pressoflessione	: 0.789
fs	: 1.27

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 48 [SLV] [IN] " - Coeff. Sfruttamento : 0.113 (fs=8.814)

Taglio Ty di Progetto [daN]	: 1593
Taglio Tz di Progetto [daN]	: 206
Momento Torcente Mt di Progetto [daNm]	: -3875

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.3
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.04
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.113
fs	: 8.81

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 18
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.802	Coefficiente di sfruttamento nel piano XZ	: 0.804
fs	: 1.243		

Colonna 176 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.803 (fs=1.245)

Sforzo Normale di Progetto [daN]	: -6144 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 3080
Momento Flettente Mz di Progetto [daNm]	: 1421

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.77
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.042
fs	: 23.71
Tensione di Progetto relativa a My [N/mm²]	: 14.44
Tensione di Progetto relativa a Mz [N/mm²]	: 2.13
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.801
fs	: 1.25
Coefficiente di Sfruttamento a pressoflessione	: 0.803
fs	: 1.25

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 36 [SLD] [IN] " - Coeff. Sfruttamento : 0.127 (fs=7.875)

Taglio Ty di Progetto [daN]	: 1258
Taglio Tz di Progetto [daN]	: -1285
Momento Torcente Mt di Progetto [daNm]	: 199

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.24
Tensione di Progetto relativa a Tz [N/mm²]	: 0.24
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.127
fs	: 7.87

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 41
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92

Coefficiente di sfruttamento nel piano XY : 0.843
fs : 1.180

Coefficiente di sfruttamento nel piano XZ : 0.847

Colonna 42 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.787 (fs=1.271)

Sforzo Normale di Progetto [daN] : 3108 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 3069
Momento Flettente Mz di Progetto [daNm] : 750

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.39
Tensione Resistente [N/mm²] : 14.83
Coefficiente di Sfruttamento a trazione : 0.026
fs : 38.18
Tensione di Progetto relativa a My [N/mm²] : 14.38
Tensione di Progetto relativa a Mz [N/mm²] : 1.12
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 18.54
Coefficiente di Sfruttamento a flessione : 0.761
fs : 1.31
Coefficiente di Sfruttamento : 0.787
fs : 1.27

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.484 (fs=2.066)

Taglio Ty di Progetto [daN] : -6855
Taglio Tz di Progetto [daN] : -4
Momento Torcente Mt di Progetto [daNm] : 7866

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 1.29
Tensione di Progetto relativa a Tz [N/mm²] : 0
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.484
fs : 2.07

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 25
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.766	Coefficiente di sfruttamento nel piano XZ	: 0.766
fs	: 1.305		

Colonna 43 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.782 (fs=1.279)
 Sforzo Normale di Progetto [daN] : -1237 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -108
 Momento Flettente Mz di Progetto [daNm] : -9447

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.15
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.008
 fs : 117.7
 Tensione di Progetto relativa a My [N/mm²] : 0.51
 Tensione di Progetto relativa a Mz [N/mm²] : 14.17
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.782
 fs : 1.28
 Coefficiente di Sfruttamento a pressoflessione : 0.782
 fs : 1.28

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.105 (fs=9.489)
 Taglio Ty di Progetto [daN] : 950
 Taglio Tz di Progetto [daN] : 2
 Momento Torcente Mt di Progetto [daNm] : -2368

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.105
 fs : 9.49

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 18
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.790	Coefficiente di sfruttamento nel piano XZ	: 0.792
fs	: 1.263		

Colonna 180 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**
Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.824 (fs=1.214)
 Sforzo Normale di Progetto [daN] : -5037 (COMPRESSIONE)

Momento Flettente My di Progetto [daNm] : -3084
 Momento Flettente Mz di Progetto [daNm] : 1775

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.63
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.035
 fs : 28.92
 Tensione di Progetto relativa a My [N/mm²] : 14.46
 Tensione di Progetto relativa a Mz [N/mm²] : 2.66
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.822
 fs : 1.22
 Coefficiente di Sfruttamento a pressoflessione : 0.824
 fs : 1.21

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.123 (fs=8.139)

Taglio Ty di Progetto [daN] : 1086
 Taglio Tz di Progetto [daN] : -1360
 Momento Torcente Mt di Progetto [daNm] : 1045

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.2
 Tensione di Progetto relativa a Tz [N/mm²] : 0.25
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.123
 fs : 8.14

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.857	Coefficiente di sfruttamento nel piano XZ	: 0.860
fs	: 1.163		

Colonna 43 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.742 (fs=1.347)

Sforzo Normale di Progetto [daN] : 5376 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -325
 Momento Flettente Mz di Progetto [daNm] : 7955

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.67
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.045

fs	: 22.07
Tensione di Progetto relativa a My [N/mm ²]	: 1.53
Tensione di Progetto relativa a Mz [N/mm ²]	: 11.93
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.697
fs	: 1.43
Coefficiente di Sfruttamento	: 0.742
fs	: 1.35

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.44 (fs=2.274)

Taglio Ty di Progetto [daN]	: -6206
Taglio Tz di Progetto [daN]	: 504
Momento Torcente Mt di Progetto [daNm]	: 7576

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 1.16
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.09
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.44
fs	: 2.27

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.719	Coefficiente di sfruttamento nel piano XZ	: 0.719
fs	: 1.391		

Colonna 44 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.784 (fs=1.276)

Sforzo Normale di Progetto [daN]	: -1525 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 36
Momento Flettente Mz di Progetto [daNm]	: 9610

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.19
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.01
fs	: 95.51
Tensione di Progetto relativa a My [N/mm ²]	: 0.17
Tensione di Progetto relativa a Mz [N/mm ²]	: 14.42
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.783
fs	: 1.28

Coefficiente di Sfruttamento a pressoflessione : 0.784
fs : 1.28

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.418)
Taglio Ty di Progetto [daN] : -957
Taglio Tz di Progetto [daN] : 0
Momento Torcente Mt di Progetto [daNm] : 2404

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
Tensione di Progetto relativa a Tz [N/mm²] : 0
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a taglio : 0.106
fs : 9.42

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.794	Coefficiente di sfruttamento nel piano XZ	: 0.796
fs	: 1.256		

Colonna 95 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.263 (fs=3.801)
Sforzo Normale di Progetto [daN] : -4617 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : -14
Momento Flettente Mz di Progetto [daNm] : -2022

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -0.58
Tensione Resistente [N/mm²] : 11.59
Coefficiente di Sfruttamento a compressione : 0.05
fs : 20.08
Tensione di Progetto relativa a My [N/mm²] : 0.07
Tensione di Progetto relativa a Mz [N/mm²] : 3.03
Tensione Resistente relativa a My [N/mm²] : 12.74
Tensione Resistente relativa a Mz [N/mm²] : 11.8
Coefficiente di Sfruttamento a flessione : 0.261
fs : 3.84
Coefficiente di Sfruttamento a pressoflessione : 0.263
fs : 3.8

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.4)

Taglio Ty di Progetto [daN]	: -958
Taglio Tz di Progetto [daN]	: 16
Momento Torcente Mt di Progetto [daNm]	: -1204

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.106
fs	: 9.4

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.310	Coefficiente di sfruttamento nel piano XZ	: 0.310
fs	: 3.221		

Colonna 116 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.594 (fs=1.684)

Sforzo Normale di Progetto [daN]	: 723 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 105
Momento Flettente Mz di Progetto [daNm]	: -7054

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.09
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.006
fs	: 164.24
Tensione di Progetto relativa a My [N/mm ²]	: 0.49
Tensione di Progetto relativa a Mz [N/mm ²]	: 10.58
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.588
fs	: 1.7
Coefficiente di Sfruttamento	: 0.594
fs	: 1.68

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.393)

Taglio Ty di Progetto [daN]	: -959
Taglio Tz di Progetto [daN]	: -40
Momento Torcente Mt di Progetto [daNm]	: -2022

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.01

Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.106
fs	: 9.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.588	Coefficiente di sfruttamento nel piano XZ	: 0.588
fs	: 1.701		

Colonna 183 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.715 (fs=1.398)

Sforzo Normale di Progetto [daN]	: 313 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 27
Momento Flettente Mz di Progetto [daNm]	: -8754

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.04
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.003
fs	: 379.44
Tensione di Progetto relativa a My [N/mm ²]	: 0.13
Tensione di Progetto relativa a Mz [N/mm ²]	: 13.13
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.713
fs	: 1.4
Coefficiente di Sfruttamento	: 0.715
fs	: 1.4

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.397)

Taglio Ty di Progetto [daN]	: -958
Taglio Tz di Progetto [daN]	: 46
Momento Torcente Mt di Progetto [daNm]	: -3600

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.106
fs	: 9.4

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
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Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.713	Coefficiente di sfruttamento nel piano XZ	: 0.713
fs	: 1.403		

Colonna 44 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.703 (fs=1.423)

Sforzo Normale di Progetto [daN]	: 4604 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 42
Momento Flettente Mz di Progetto [daNm]	: -8122

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.58
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.039
fs	: 25.78
Tensione di Progetto relativa a My [N/mm²]	: 0.2
Tensione di Progetto relativa a Mz [N/mm²]	: 12.18
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.664
fs	: 1.51
Coefficiente di Sfruttamento	: 0.703
fs	: 1.42

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.454 (fs=2.202)

Taglio Ty di Progetto [daN]	: 6430
Taglio Tz di Progetto [daN]	: 68
Momento Torcente Mt di Progetto [daNm]	: -8122

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 1.21
Tensione di Progetto relativa a Tz [N/mm²]	: 0.01
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.454
fs	: 2.2

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.664	Coefficiente di sfruttamento nel piano XZ	: 0.664
fs	: 1.506		

Colonna 45 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.755 (fs=1.325)

Sforzo Normale di Progetto [daN]	: -283 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -109
Momento Flettente Mz di Progetto [daNm]	: -9111

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.04
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.002
fs	: 515.33
Tensione di Progetto relativa a My [N/mm²]	: 0.51
Tensione di Progetto relativa a Mz [N/mm²]	: 13.67
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.755
fs	: 1.32
Coefficiente di Sfruttamento a pressoflessione	: 0.755
fs	: 1.32

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.115 (fs=8.691)

Taglio Ty di Progetto [daN]	: 1617
Taglio Tz di Progetto [daN]	: -203
Momento Torcente Mt di Progetto [daNm]	: -4543

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.3
Tensione di Progetto relativa a Tz [N/mm²]	: 0.04
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.115
fs	: 8.69

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 18
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.757	Coefficiente di sfruttamento nel piano XZ	: 0.757
fs	: 1.321		

Colonna 184 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**
Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.83 (fs=1.205)
 Sforzo Normale di Progetto [daN] : -7543 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -3114
 Momento Flettente Mz di Progetto [daNm] : 1734

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.94
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.052
 fs : 19.31
 Tensione di Progetto relativa a My [N/mm²] : 14.6
 Tensione di Progetto relativa a Mz [N/mm²] : 2.6
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.827
 fs : 1.21
 Coefficiente di Sfruttamento a pressoflessione : 0.83
 fs : 1.21

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**
Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.133 (fs=7.514)
 Taglio Ty di Progetto [daN] : 1295
 Taglio Tz di Progetto [daN] : -1370
 Momento Torcente Mt di Progetto [daNm] : 730

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.24
 Tensione di Progetto relativa a Tz [N/mm²] : 0.26
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.133
 fs : 7.51

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.879	Coefficiente di sfruttamento nel piano XZ	: 0.884
fs	: 1.132		

Colonna 45 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1300 mm] - **R 500x160**
Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.743 (fs=1.347)
 Sforzo Normale di Progetto [daN] : 3826 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -2998
 Momento Flettente Mz di Progetto [daNm] : -150

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.48
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.032
fs	: 31.02
Tensione di Progetto relativa a My [N/mm ²]	: 14.05
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.23
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.71
fs	: 1.41
Coefficiente di Sfruttamento	: 0.743
fs	: 1.35

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 15 [SLD] [IN] " - Coeff. Sfruttamento : 0.413 (fs=2.423)

Taglio Ty di Progetto [daN]	: -5825
Taglio Tz di Progetto [daN]	: 484
Momento Torcente Mt di Progetto [daNm]	: 7312

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 1.09
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.09
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.413
fs	: 2.42

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.745	Coefficiente di sfruttamento nel piano XZ	: 0.745
fs	: 1.342		

Colonna 46 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.754 (fs=1.327)

Sforzo Normale di Progetto [daN]	: -1329 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 35
Momento Flettente Mz di Progetto [daNm]	: 9244

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.17
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.009
fs	: 109.59
Tensione di Progetto relativa a My [N/mm ²]	: 0.17

Tensione di Progetto relativa a M_z [N/mm ²]	: 13.87
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.754
f_s	: 1.33
Coefficiente di Sfruttamento a pressoflessione	: 0.754
f_s	: 1.33

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.137 ($f_s=7.294$)

Taglio T_y di Progetto [daN]	: -1941
Taglio T_z di Progetto [daN]	: -37
Momento Torcente M_t di Progetto [daNm]	: 3567

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.36
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.137
f_s	: 7.29

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente K_c nel piano XY	: 1.00	Coefficiente K_c nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.763	Coefficiente di sfruttamento nel piano XZ	: 0.765
f_s	: 1.308		

Colonna 96 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.274 ($f_s=3.645$)

Sforzo Normale di Progetto [daN]	: -911 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: 53
Momento Flettente M_z di Progetto [daNm]	: -3284

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: -0.11
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.006
f_s	: 159.86
Tensione di Progetto relativa a M_y [N/mm ²]	: 0.25
Tensione di Progetto relativa a M_z [N/mm ²]	: 4.93
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.274
f_s	: 3.65
Coefficiente di Sfruttamento a pressoflessione	: 0.274
f_s	: 3.64

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.376)

Taglio Ty di Progetto [daN] : -960
 Taglio Tz di Progetto [daN] : -48
 Momento Torcente Mt di Progetto [daNm] : -1197

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0.01
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.107
 fs : 9.38

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.309	Coefficiente di sfruttamento nel piano XZ	: 0.309
fs	: 3.233		

Colonna 117 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.565 (fs=1.77)

Sforzo Normale di Progetto [daN] : -1066 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -98
 Momento Flettente Mz di Progetto [daNm] : -6783

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.13
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.007
 fs : 136.6
 Tensione di Progetto relativa a My [N/mm²] : 0.46
 Tensione di Progetto relativa a Mz [N/mm²] : 10.17
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.565
 fs : 1.77
 Coefficiente di Sfruttamento a pressoflessione : 0.565
 fs : 1.77

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.149 (fs=6.713)

Taglio Ty di Progetto [daN] : -2086
 Taglio Tz di Progetto [daN] : 317

Momento Torcente Mt di Progetto [daNm] : -2916

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.39
 Tensione di Progetto relativa a Tz [N/mm²] : 0.06
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.149
 fs : 6.71

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.572	Coefficiente di sfruttamento nel piano XZ	: 0.572
fs	: 1.748		

Colonna 187 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)
 L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.689 (fs=1.452)

Sforzo Normale di Progetto [daN] : -712 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -1
 Momento Flettente Mz di Progetto [daNm] : -8511

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.09
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.005
 fs : 204.49
 Tensione di Progetto relativa a My [N/mm²] : 0.00
 Tensione di Progetto relativa a Mz [N/mm²] : 12.77
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.689
 fs : 1.45
 Coefficiente di Sfruttamento a pressoflessione : 0.689
 fs : 1.45

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.207 (fs=4.837)

Taglio Ty di Progetto [daN] : -2925
 Taglio Tz di Progetto [daN] : 126
 Momento Torcente Mt di Progetto [daNm] : -6781

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.55
 Tensione di Progetto relativa a Tz [N/mm²] : 0.02
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.207

fs

: 4.84

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.693	Coefficiente di sfruttamento nel piano XZ	: 0.693
fs	: 1.442		

Colonna 46 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.674 (fs=1.485)

Sforzo Normale di Progetto [daN]	: 4192 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 3
Momento Flettente Mz di Progetto [daNm]	: -7882

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.52
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.035
fs	: 28.31
Tensione di Progetto relativa a My [N/mm²]	: 0.02
Tensione di Progetto relativa a Mz [N/mm²]	: 11.82
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.638
fs	: 1.57
Coefficiente di Sfruttamento	: 0.674
fs	: 1.48

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.454 (fs=2.202)

Taglio Ty di Progetto [daN]	: 6430
Taglio Tz di Progetto [daN]	: 121
Momento Torcente Mt di Progetto [daNm]	: -7882

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 1.21
Tensione di Progetto relativa a Tz [N/mm²]	: 0.02
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.454
fs	: 2.2

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31

Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.638	Coefficiente di sfruttamento nel piano XZ	: 0.638
fs	: 1.567		

Colonna 47 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.681 (fs=1.469)

Sforzo Normale di Progetto [daN]	: -2025 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -106
Momento Flettente Mz di Progetto [daNm]	: -8197

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.25
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.014
fs	: 71.92
Tensione di Progetto relativa a My [N/mm²]	: 0.5
Tensione di Progetto relativa a Mz [N/mm²]	: 12.29
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.68
fs	: 1.47
Coefficiente di Sfruttamento a pressoflessione	: 0.681
fs	: 1.47

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.127 (fs=7.872)

Taglio Ty di Progetto [daN]	: 1788
Taglio Tz di Progetto [daN]	: -199
Momento Torcente Mt di Progetto [daNm]	: -4679

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.34
Tensione di Progetto relativa a Tz [N/mm²]	: 0.04
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.127
fs	: 7.87

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 18
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.694	Coefficiente di sfruttamento nel piano XZ	: 0.697
fs	: 1.435		

Colonna 188 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.853 (fs=1.173)

Sforzo Normale di Progetto [daN]	: -2802 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -3107
Momento Flettente Mz di Progetto [daNm]	: 2210

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.35
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.019
fs	: 51.99
Tensione di Progetto relativa a My [N/mm²]	: 14.56
Tensione di Progetto relativa a Mz [N/mm²]	: 3.31
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.852
fs	: 1.17
Coefficiente di Sfruttamento a pressoflessione	: 0.853
fs	: 1.17

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.155 (fs=6.452)

Taglio Ty di Progetto [daN]	: 1705
Taglio Tz di Progetto [daN]	: 1382
Momento Torcente Mt di Progetto [daNm]	: -229

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.32
Tensione di Progetto relativa a Tz [N/mm²]	: 0.26
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.155
fs	: 6.45

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.872	Coefficiente di sfruttamento nel piano XZ	: 0.873
fs	: 1.145		

Colonna 47 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.723 (fs=1.384)

Sforzo Normale di Progetto [daN] : 2302 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 2934
 Momento Flettente Mz di Progetto [daNm] : -290

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.29
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.019
 fs : 51.55
 Tensione di Progetto relativa a My [N/mm²] : 13.76
 Tensione di Progetto relativa a Mz [N/mm²] : 0.43
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.703
 fs : 1.42
 Coefficiente di Sfruttamento : 0.723
 fs : 1.38

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.354 (fs=2.828)

Taglio Ty di Progetto [daN] : -3187
 Taglio Tz di Progetto [daN] : 1
 Momento Torcente Mt di Progetto [daNm] : 3858

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.6
 Tensione di Progetto relativa a Tz [N/mm²] : 0
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.354
 fs : 2.83

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.723	Coefficiente di sfruttamento nel piano XZ	: 0.723
fs	: 1.384		

Colonna 48 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.681 (fs=1.468)

Sforzo Normale di Progetto [daN] : -804 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -7
 Momento Flettente Mz di Progetto [daNm] : 8406

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.1
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.006
fs	: 181.26
Tensione di Progetto relativa a My [N/mm ²]	: 0.03
Tensione di Progetto relativa a Mz [N/mm ²]	: 12.61
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.681
fs	: 1.47
Coefficiente di Sfruttamento a pressoflessione	: 0.681
fs	: 1.47

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.105 (fs=9.52)

Taglio Ty di Progetto [daN]	: -947
Taglio Tz di Progetto [daN]	: -1
Momento Torcente Mt di Progetto [daNm]	: 2371

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm ²]	: 0
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.105
fs	: 9.52

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.687	Coefficiente di sfruttamento nel piano XZ	: 0.688
fs	: 1.454		

Colonna 97 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.259 (fs=3.866)

Sforzo Normale di Progetto [daN]	: -4360 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -1
Momento Flettente Mz di Progetto [daNm]	: -2016

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.55
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.047
fs	: 21.26
Tensione di Progetto relativa a My [N/mm ²]	: 0.00
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.02
Tensione Resistente relativa a My [N/mm ²]	: 12.74

Tensione Resistente relativa a M_z [N/mm ²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.256
f_s	: 3.9
Coefficiente di Sfruttamento a pressoflessione	: 0.259
f_s	: 3.87

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 ($f_s=9.4$)

Taglio T_y di Progetto [daN]	: -959
Taglio T_z di Progetto [daN]	: 1
Momento Torcente M_t di Progetto [daNm]	: -1198

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.18
Tensione di Progetto relativa a T_z [N/mm ²]	: 0
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.106
f_s	: 9.4

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente K_c nel piano XY	: 1.00	Coefficiente K_c nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.303	Coefficiente di sfruttamento nel piano XZ	: 0.303
f_s	: 3.295		

Colonna 118 Copertur[Colonna]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $-\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**
Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.515 ($f_s=1.941$)

Sforzo Normale di Progetto [daN]	: -568 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: -88
Momento Flettente M_z di Progetto [daNm]	: -6190

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: -0.07
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.004
f_s	: 256.29
Tensione di Progetto relativa a M_y [N/mm ²]	: 0.41
Tensione di Progetto relativa a M_z [N/mm ²]	: 9.29
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.515
f_s	: 1.94
Coefficiente di Sfruttamento a pressoflessione	: 0.515
f_s	: 1.94

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.4)

Taglio Ty di Progetto [daN] : -959
 Taglio Tz di Progetto [daN] : -1
 Momento Torcente Mt di Progetto [daNm] : -2016

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.106
 fs : 9.4

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.519	Coefficiente di sfruttamento nel piano XZ	: 0.519
fs	: 1.926		

Colonna 191 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.631 (fs=1.584)

Sforzo Normale di Progetto [daN] : -726 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 12
 Momento Flettente Mz di Progetto [daNm] : -7780

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.09
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.005
 fs : 200.54
 Tensione di Progetto relativa a My [N/mm²] : 0.05
 Tensione di Progetto relativa a Mz [N/mm²] : 11.67
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.631
 fs : 1.58
 Coefficiente di Sfruttamento a pressoflessione : 0.631
 fs : 1.58

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.106 (fs=9.401)

Taglio Ty di Progetto [daN] : -959
 Taglio Tz di Progetto [daN] : 6
 Momento Torcente Mt di Progetto [daNm] : -3595

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.106
fs	: 9.4

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.636	Coefficiente di sfruttamento nel piano XZ	: 0.636
fs	: 1.572		

Colonna 48 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.62 (fs=1.614)

Sforzo Normale di Progetto [daN]	: 4180 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 8
Momento Flettente Mz di Progetto [daNm]	: -7209

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.52
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.035
fs	: 28.39
Tensione di Progetto relativa a My [N/mm ²]	: 0.04
Tensione di Progetto relativa a Mz [N/mm ²]	: 10.81
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.584
fs	: 1.71
Coefficiente di Sfruttamento	: 0.62
fs	: 1.61

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.353 (fs=2.833)

Taglio Ty di Progetto [daN]	: 3181
Taglio Tz di Progetto [daN]	: 6
Momento Torcente Mt di Progetto [daNm]	: -3851

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.6
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.353
fs	: 2.83

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.584	Coefficiente di sfruttamento nel piano XZ	: 0.584
fs	: 1.711		

Colonna 49 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.596 (fs=1.679)

Sforzo Normale di Progetto [daN]	: -636 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -103
Momento Flettente Mz di Progetto [daNm]	: -7155

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.08
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.004
fs	: 229.08
Tensione di Progetto relativa a My [N/mm²]	: 0.48
Tensione di Progetto relativa a Mz [N/mm²]	: 10.73
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.596
fs	: 1.68
Coefficiente di Sfruttamento a pressoflessione	: 0.596
fs	: 1.68

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.357)

Taglio Ty di Progetto [daN]	: 963
Taglio Tz di Progetto [daN]	: 3
Momento Torcente Mt di Progetto [daNm]	: -2413

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm²]	: 0
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.107
fs	: 9.36

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 18
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94

Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.600	Coefficiente di sfruttamento nel piano XZ	: 0.601
fs	: 1.664		

Colonna 192 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.822 (fs=1.217)

Sforzo Normale di Progetto [daN]	: -5795 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -3043
Momento Flettente Mz di Progetto [daNm]	: 1907

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.72
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.04
fs	: 25.13
Tensione di Progetto relativa a My [N/mm²]	: 14.27
Tensione di Progetto relativa a Mz [N/mm²]	: 2.86
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.82
fs	: 1.22
Coefficiente di Sfruttamento a pressoflessione	: 0.822
fs	: 1.22

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.116 (fs=8.607)

Taglio Ty di Progetto [daN]	: 854
Taglio Tz di Progetto [daN]	: -1406
Momento Torcente Mt di Progetto [daNm]	: 1907

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.16
Tensione di Progetto relativa a Tz [N/mm²]	: 0.26
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.116
fs	: 8.61

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.862	Coefficiente di sfruttamento nel piano XZ	: 0.867
fs	: 1.154		

Colonna 49 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7
VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1300 mm] - **R 500x160**
Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.737 (fs=1.357)
 Sforzo Normale di Progetto [daN] : 3221 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -2999
 Momento Flettente Mz di Progetto [daNm] : -139

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.4
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.027
 fs : 36.85
 Tensione di Progetto relativa a My [N/mm²] : 14.06
 Tensione di Progetto relativa a Mz [N/mm²] : 0.21
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.71
 fs : 1.41
 Coefficiente di Sfruttamento : 0.737
 fs : 1.36

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.353 (fs=2.831)
 Taglio Ty di Progetto [daN] : -3183
 Taglio Tz di Progetto [daN] : 3
 Momento Torcente Mt di Progetto [daNm] : 3855

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.6
 Tensione di Progetto relativa a Tz [N/mm²] : 0
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.353
 fs : 2.83

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.740	Coefficiente di sfruttamento nel piano XZ	: 0.740
fs	: 1.352		

Colonna 50 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.569 (fs=1.758)

Sforzo Normale di Progetto [daN] : -4551 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -2
 Momento Flettente Mz di Progetto [daNm] : 7015

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.57
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.031
 fs : 32.01
 Tensione di Progetto relativa a My [N/mm²] : 0.01
 Tensione di Progetto relativa a Mz [N/mm²] : 10.52
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.568
 fs : 1.76
 Coefficiente di Sfruttamento a pressoflessione : 0.569
 fs : 1.76

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.107 (fs=9.364)

Taglio Ty di Progetto [daN] : -962
 Taglio Tz di Progetto [daN] : 1
 Momento Torcente Mt di Progetto [daNm] : 2408

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.107
 fs : 9.36

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.599	Coefficiente di sfruttamento nel piano XZ	: 0.605
fs	: 1.652		

Colonna 106 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.261 (fs=3.838)

Sforzo Normale di Progetto [daN] : -4248 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 1
 Momento Flettente Mz di Progetto [daNm] : -2032

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -0.53
 Tensione Resistente [N/mm²] : 11.59

Coefficiente di Sfruttamento a compressione	: 0.046
fs	: 21.82
Tensione di Progetto relativa a My [N/mm ²]	: 0.00
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.05
Tensione Resistente relativa a My [N/mm ²]	: 12.74
Tensione Resistente relativa a Mz [N/mm ²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.258
fs	: 3.87
Coefficiente di Sfruttamento a pressoflessione	: 0.261
fs	: 3.84

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.105 (fs=9.482)

Taglio Ty di Progetto [daN]	: -950
Taglio Tz di Progetto [daN]	: 4
Momento Torcente Mt di Progetto [daNm]	: -1221

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.18
Tensione di Progetto relativa a Tz [N/mm ²]	: 0
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.105
fs	: 9.48

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.304	Coefficiente di sfruttamento nel piano XZ	: 0.304
fs	: 3.287		

Colonna 119 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.46 (fs=2.172)

Sforzo Normale di Progetto [daN]	: -4164 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -4
Momento Flettente Mz di Progetto [daNm]	: -3597

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.52
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.045
fs	: 22.26
Tensione di Progetto relativa a My [N/mm ²]	: 0.02
Tensione di Progetto relativa a Mz [N/mm ²]	: 5.4
Tensione Resistente relativa a My [N/mm ²]	: 12.74
Tensione Resistente relativa a Mz [N/mm ²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.458

fs	: 2.18
Coefficiente di Sfruttamento a pressoflessione	: 0.46
fs	: 2.17

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**
Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.126 (fs=7.926)

Taglio Ty di Progetto [daN]	: -1759
Taglio Tz di Progetto [daN]	: 313
Momento Torcente Mt di Progetto [daNm]	: -1776

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.33
Tensione di Progetto relativa a Tz [N/mm²]	: 0.06
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.126
fs	: 7.93

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.503	Coefficiente di sfruttamento nel piano XZ	: 0.504
fs	: 1.985		

Colonna 194 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**
Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.543 (fs=1.84)

Sforzo Normale di Progetto [daN]	: -4577 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 1
Momento Flettente Mz di Progetto [daNm]	: -6704

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.57
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.031
fs	: 31.83
Tensione di Progetto relativa a My [N/mm²]	: 0.00
Tensione di Progetto relativa a Mz [N/mm²]	: 10.06
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.542
fs	: 1.84
Coefficiente di Sfruttamento a pressoflessione	: 0.543
fs	: 1.84

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.105 (fs=9.502)

Taglio Ty di Progetto [daN] : -948
 Taglio Tz di Progetto [daN] : 7
 Momento Torcente Mt di Progetto [daNm] : -3597

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.105
 fs : 9.5

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.574	Coefficiente di sfruttamento nel piano XZ	: 0.574
fs	: 1.741		

Colonna 50 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.53 (fs=1.887)

Sforzo Normale di Progetto [daN] : 3234 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 2
 Momento Flettente Mz di Progetto [daNm] : -6209

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.4
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.027
 fs : 36.7
 Tensione di Progetto relativa a My [N/mm²] : 0.01
 Tensione di Progetto relativa a Mz [N/mm²] : 9.31
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.503
 fs : 1.99
 Coefficiente di Sfruttamento : 0.53
 fs : 1.89

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.353 (fs=2.836)

Taglio Ty di Progetto [daN] : 3177
 Taglio Tz di Progetto [daN] : 7
 Momento Torcente Mt di Progetto [daNm] : -3847

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.6

Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.353
f_s	: 2.84

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.503	Coefficiente di sfruttamento nel piano XZ	: 0.503
f_s	: 1.990		

Colonna 51 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.528 ($f_s=1.894$)

Sforzo Normale di Progetto [daN]	: -499 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: 127
Momento Flettente M_z di Progetto [daNm]	: -6268

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.003
f_s	: 292.01
Tensione di Progetto relativa a M_y [N/mm ²]	: 0.59
Tensione di Progetto relativa a M_z [N/mm ²]	: 9.4
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.528
f_s	: 1.89
Coefficiente di Sfruttamento a pressoflessione	: 0.528
f_s	: 1.89

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.112 ($f_s=8.955$)

Taglio T_y di Progetto [daN]	: 1006
Taglio T_z di Progetto [daN]	: 5
Momento Torcente M_t di Progetto [daNm]	: -2509

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.19
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.112
f_s	: 8.96

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 14
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.531	Coefficiente di sfruttamento nel piano XZ	: 0.532
fs	: 1.880		

Colonna 196 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.802 (fs=1.247)

Sforzo Normale di Progetto [daN]	: -361 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -3034
Momento Flettente Mz di Progetto [daNm]	: 1623

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.05
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.002
fs	: 403.61
Tensione di Progetto relativa a My [N/mm²]	: 14.22
Tensione di Progetto relativa a Mz [N/mm²]	: 2.43
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.802
fs	: 1.25
Coefficiente di Sfruttamento a pressoflessione	: 0.802
fs	: 1.25

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.145 (fs=6.903)

Taglio Ty di Progetto [daN]	: 1537
Taglio Tz di Progetto [daN]	: -1359
Momento Torcente Mt di Progetto [daNm]	: 1757

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.29
Tensione di Progetto relativa a Tz [N/mm²]	: 0.25
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.145
fs	: 6.9

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 50
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.804	Coefficiente di sfruttamento nel piano XZ	: 0.805

fs : 1.243

Colonna 51 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.72 (fs=1.389)

Sforzo Normale di Progetto [daN]	: -1122 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -2990
Momento Flettente Mz di Progetto [daNm]	: -355

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.14
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.008
fs	: 129.81
Tensione di Progetto relativa a My [N/mm²]	: 14.02
Tensione di Progetto relativa a Mz [N/mm²]	: 0.53
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.72
fs	: 1.39
Coefficiente di Sfruttamento a pressoflessione	: 0.72
fs	: 1.39

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.352 (fs=2.842)

Taglio Ty di Progetto [daN]	: -3171
Taglio Tz di Progetto [daN]	: 5
Momento Torcente Mt di Progetto [daNm]	: 3837

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.59
Tensione di Progetto relativa a Tz [N/mm²]	: 0
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.352
fs	: 2.84

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.728	Coefficiente di sfruttamento nel piano XZ	: 0.728
fs	: 1.374		

Colonna 52 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.498 (fs=2.009)
 Sforzo Normale di Progetto [daN] : -4861 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 2
 Momento Flettente Mz di Progetto [daNm] : 6136

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.61
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.033
 fs : 29.96
 Tensione di Progetto relativa a My [N/mm²] : 0.01
 Tensione di Progetto relativa a Mz [N/mm²] : 9.2
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.497
 fs : 2.01
 Coefficiente di Sfruttamento a pressoflessione : 0.498
 fs : 2.01

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.112 (fs=8.907)
 Taglio Ty di Progetto [daN] : -1012
 Taglio Tz di Progetto [daN] : 4
 Momento Torcente Mt di Progetto [daNm] : 2515

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.19
 Tensione di Progetto relativa a Tz [N/mm²] : 0
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.112
 fs : 8.91

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.531	Coefficiente di sfruttamento nel piano XZ	: 0.539
fs	: 1.856		

Colonna 107 Copetur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)
 L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.266 (fs=3.753)
 Sforzo Normale di Progetto [daN] : -3914 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 3

Momento Flettente Mz di Progetto [daNm] : -2077

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -0.49
 Tensione Resistente [N/mm²] : 11.59
 Coefficiente di Sfruttamento a compressione : 0.042
 fs : 23.68
 Tensione di Progetto relativa a My [N/mm²] : 0.01
 Tensione di Progetto relativa a Mz [N/mm²] : 3.12
 Tensione Resistente relativa a My [N/mm²] : 12.74
 Tensione Resistente relativa a Mz [N/mm²] : 11.8
 Coefficiente di Sfruttamento a flessione : 0.265
 fs : 3.78
 Coefficiente di Sfruttamento a pressoflessione : 0.266
 fs : 3.75

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.106 (fs=9.461)

Taglio Ty di Progetto [daN] : -1462
 Taglio Tz di Progetto [daN] : 321
 Momento Torcente Mt di Progetto [daNm] : -686

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.27
 Tensione di Progetto relativa a Tz [N/mm²] : 0.06
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.106
 fs : 9.46

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.307	Coefficiente di sfruttamento nel piano XZ	: 0.307
fs	: 3.258		

Colonna 120 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.46 (fs=2.173)

Sforzo Normale di Progetto [daN] : -3855 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -8
 Momento Flettente Mz di Progetto [daNm] : -3589

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -0.48
 Tensione Resistente [N/mm²] : 11.59
 Coefficiente di Sfruttamento a compressione : 0.042
 fs : 24.05

Tensione di Progetto relativa a M_y [N/mm ²]	: 0.04
Tensione di Progetto relativa a M_z [N/mm ²]	: 5.38
Tensione Resistente relativa a M_y [N/mm ²]	: 12.74
Tensione Resistente relativa a M_z [N/mm ²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.458
f_s	: 2.18
Coefficiente di Sfruttamento a pressoflessione	: 0.46
f_s	: 2.17

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.102 ($f_s=9.813$)

Taglio T_y di Progetto [daN]	: -918
Taglio T_z di Progetto [daN]	: 14
Momento Torcente M_t di Progetto [daNm]	: -2077

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.17
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.102
f_s	: 9.81

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente K_c nel piano XY	: 1.00	Coefficiente K_c nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.500	Coefficiente di sfruttamento nel piano XZ	: 0.500
f_s	: 1.998		

Colonna 198 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.529 ($f_s=1.892$)

Sforzo Normale di Progetto [daN]	: -3803 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: -2
Momento Flettente M_z di Progetto [daNm]	: -4141

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 0.7$

Tensione di Progetto [N/mm ²]	: -0.48
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.041
f_s	: 24.37
Tensione di Progetto relativa a M_y [N/mm ²]	: 0.01
Tensione di Progetto relativa a M_z [N/mm ²]	: 6.21
Tensione Resistente relativa a M_y [N/mm ²]	: 12.74
Tensione Resistente relativa a M_z [N/mm ²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.527
f_s	: 1.9
Coefficiente di Sfruttamento a pressoflessione	: 0.529

fs : 1.89

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.102 (fs=9.793)
 Taglio Ty di Progetto [daN] : -920
 Taglio Tz di Progetto [daN] : 12
 Momento Torcente Mt di Progetto [daNm] : -3589

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.17
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.102
 fs : 9.79

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.568	Coefficiente di sfruttamento nel piano XZ	: 0.568
fs	: 1.761		

Colonna 52 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.487 (fs=2.053)
 Sforzo Normale di Progetto [daN] : 35 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -1
 Momento Flettente Mz di Progetto [daNm] : -3825

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : 0.00
 Tensione Resistente [N/mm²] : 9.44
 Coefficiente di Sfruttamento a trazione : 0.000
 fs : 1000
 Tensione di Progetto relativa a My [N/mm²] : 0.01
 Tensione di Progetto relativa a Mz [N/mm²] : 5.74
 Tensione Resistente relativa a My [N/mm²] : 12.74
 Tensione Resistente relativa a Mz [N/mm²] : 11.8
 Coefficiente di Sfruttamento a flessione : 0.487
 fs : 2.06
 Coefficiente di Sfruttamento : 0.487
 fs : 2.05

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.35 (fs=2.855)
 Taglio Ty di Progetto [daN] : 3156

Taglio Tz di Progetto [daN] : 12
 Momento Torcente Mt di Progetto [daNm] : -3825

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.59
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.35
 fs : 2.85

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.487	Coefficiente di sfruttamento nel piano XZ	: 0.487
fs	: 2.055		

Colonna 53 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.477 (fs=2.097)

Sforzo Normale di Progetto [daN] : -1453 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 122
 Momento Flettente Mz di Progetto [daNm] : -5647

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.18
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.01
 fs : 100.22
 Tensione di Progetto relativa a My [N/mm²] : 0.57
 Tensione di Progetto relativa a Mz [N/mm²] : 8.47
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.477
 fs : 2.1
 Coefficiente di Sfruttamento a pressoflessione : 0.477
 fs : 2.1

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.11 (fs=9.072)

Taglio Ty di Progetto [daN] : 993
 Taglio Tz di Progetto [daN] : 8
 Momento Torcente Mt di Progetto [daNm] : -2497

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.19
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 1.69

Coefficiente di Sfruttamento a taglio : 0.11
fs : 9.07

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 14
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.487	Coefficiente di sfruttamento nel piano XZ	: 0.489
fs	: 2.046		

Colonna 200 Copertur[Colonna]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.832 (fs=1.201)

Sforzo Normale di Progetto [daN]	: 568 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 3089
Momento Flettente Mz di Progetto [daNm]	: 1849

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.07
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.005
fs	: 208.85
Tensione di Progetto relativa a My [N/mm²]	: 14.48
Tensione di Progetto relativa a Mz [N/mm²]	: 2.77
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.828
fs	: 1.21
Coefficiente di Sfruttamento	: 0.832
fs	: 1.2

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.119 (fs=8.414)

Taglio Ty di Progetto [daN]	: 906
Taglio Tz di Progetto [daN]	: -1418
Momento Torcente Mt di Progetto [daNm]	: -1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.17
Tensione di Progetto relativa a Tz [N/mm²]	: 0.27
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.119
fs	: 8.41

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98

Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.828	Coefficiente di sfruttamento nel piano XZ	: 0.828
fs	: 1.208		

Colonna 53 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.727 (fs=1.375)

Sforzo Normale di Progetto [daN]	: 2092 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -2966
Momento Flettente Mz di Progetto [daNm]	: -274

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.26
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.018
fs	: 56.73
Tensione di Progetto relativa a My [N/mm²]	: 13.9
Tensione di Progetto relativa a Mz [N/mm²]	: 0.41
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.71
fs	: 1.41
Coefficiente di Sfruttamento	: 0.727
fs	: 1.37

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.35 (fs=2.857)

Taglio Ty di Progetto [daN]	: -3154
Taglio Tz di Progetto [daN]	: 6
Momento Torcente Mt di Progetto [daNm]	: 3819

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.59
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.35
fs	: 2.86

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.710	Coefficiente di sfruttamento nel piano XZ	: 0.710
fs	: 1.409		

Colonna 54 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.418 (fs=2.394)

Sforzo Normale di Progetto [daN] : -4924 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : 4
Momento Flettente Mz di Progetto [daNm] : 5142

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.62
Tensione Resistente [N/mm²] : 18.21
Coefficiente di Sfruttamento a compressione : 0.034
fs : 29.58
Tensione di Progetto relativa a My [N/mm²] : 0.02
Tensione di Progetto relativa a Mz [N/mm²] : 7.71
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 18.54
Coefficiente di Sfruttamento a flessione : 0.417
fs : 2.4
Coefficiente di Sfruttamento a pressoflessione : 0.418
fs : 2.39

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.111 (fs=9.046)

Taglio Ty di Progetto [daN] : -996
Taglio Tz di Progetto [daN] : 8
Momento Torcente Mt di Progetto [daNm] : 2499

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.19
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a taglio : 0.111
fs : 9.05

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.450	Coefficiente di sfruttamento nel piano XZ	: 0.457
fs	: 2.188		

Colonna 108 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.26 (fs=3.847)

Sforzo Normale di Progetto [daN] : -3638 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : -2033

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -0.45
 Tensione Resistente [N/mm²] : 11.59
 Coefficiente di Sfruttamento a compressione : 0.039
 fs : 25.48
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 3.05
 Tensione Resistente relativa a My [N/mm²] : 12.74
 Tensione Resistente relativa a Mz [N/mm²] : 11.8
 Coefficiente di Sfruttamento a flessione : 0.258
 fs : 3.87
 Coefficiente di Sfruttamento a pressoflessione : 0.26
 fs : 3.85

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 24 [CAR] [ST] " - Coeff. Sfruttamento : 0.068 (fs=14.725)

Taglio Ty di Progetto [daN] : -786
 Taglio Tz di Progetto [daN] : 24
 Momento Torcente Mt di Progetto [daNm] : -1049

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.15
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.17
 Coefficiente di Sfruttamento a taglio : 0.068
 fs : 14.72

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.298	Coefficiente di sfruttamento nel piano XZ	: 0.298
fs	: 3.359		

Colonna 121 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.459 (fs=2.179)

Sforzo Normale di Progetto [daN] : -3535 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -15
 Momento Flettente Mz di Progetto [daNm] : -3568

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.44
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.038
fs	: 26.22
Tensione di Progetto relativa a My [N/mm ²]	: 0.07
Tensione di Progetto relativa a Mz [N/mm ²]	: 5.35
Tensione Resistente relativa a My [N/mm ²]	: 12.74
Tensione Resistente relativa a Mz [N/mm ²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.458
fs	: 2.19
Coefficiente di Sfruttamento a pressoflessione	: 0.459
fs	: 2.18

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.103 (fs=9.665)

Taglio Ty di Progetto [daN]	: -932
Taglio Tz di Progetto [daN]	: 20
Momento Torcente Mt di Progetto [daNm]	: -2033

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.17
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.103
fs	: 9.67

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.496	Coefficiente di sfruttamento nel piano XZ	: 0.496
fs	: 2.016		

Colonna 203 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.526 (fs=1.899)

Sforzo Normale di Progetto [daN]	: -3548 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -4129

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.44
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.038
fs	: 26.12
Tensione di Progetto relativa a My [N/mm ²]	: 0.00
Tensione di Progetto relativa a Mz [N/mm ²]	: 6.19

Tensione Resistente relativa a M_y [N/mm ²]	: 12.74
Tensione Resistente relativa a M_z [N/mm ²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.525
f_s	: 1.9
Coefficiente di Sfruttamento a pressoflessione	: 0.526
f_s	: 1.9

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.031 ($f_s=32.324$)

Taglio T_y di Progetto [daN]	: -1800
Taglio T_z di Progetto [daN]	: -46
Momento Torcente M_t di Progetto [daNm]	: -4261

Tipo Verifica	: TAGLIO+TORSIONE
Tensione di Progetto relativa a T_y [N/mm ²]	: 0.34
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.127
f_s	: 7.86
Tensione di Progetto [N/mm ²]	: 0.06
Modulo di resistenza a torsione [mm ³]	: 3579418.25
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.015
f_s	: 67.7
Coefficiente di Sfruttamento a taglio+torsione	: 0.031
f_s	: 32.32

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.563	Coefficiente di sfruttamento nel piano XZ	: 0.563
f_s	: 1.775		

Colonna 54 Copertura[Colonna]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.49 ($f_s=2.04$)

Sforzo Normale di Progetto [daN]	: 291 (TRAZIONE)
Momento Flettente M_y di Progetto [daNm]	: -5
Momento Flettente M_z di Progetto [daNm]	: -3815

Tipo Verifica : TRAZIONE+FLESSIONE - $K_{mod} = 0.7$

Tensione di Progetto [N/mm ²]	: 0.04
Tensione Resistente [N/mm ²]	: 9.44
Coefficiente di Sfruttamento a trazione	: 0.004
f_s	: 259.64
Tensione di Progetto relativa a M_y [N/mm ²]	: 0.02
Tensione di Progetto relativa a M_z [N/mm ²]	: 5.72

Tensione Resistente relativa a M_y [N/mm ²]	: 12.74
Tensione Resistente relativa a M_z [N/mm ²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.486
f_s	: 2.06
Coefficiente di Sfruttamento	: 0.49
f_s	: 2.04

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLD] [LT] " - Coeff. Sfruttamento : 0.244 ($f_s=4.106$)

Taglio T_y di Progetto [daN]	: 2195
Taglio T_z di Progetto [daN]	: 10
Momento Torcente M_t di Progetto [daNm]	: -2657

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.41
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.244
f_s	: 4.11

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente K_c nel piano XY	: 1.00	Coefficiente K_c nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.486	Coefficiente di sfruttamento nel piano XZ	: 0.486
f_s	: 2.056		

Colonna 55 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.331 ($f_s=3.018$)

Sforzo Normale di Progetto [daN]	: -4147 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: 119
Momento Flettente M_z di Progetto [daNm]	: -3845

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: -0.52
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.028
f_s	: 35.12
Tensione di Progetto relativa a M_y [N/mm ²]	: 0.56
Tensione di Progetto relativa a M_z [N/mm ²]	: 5.77
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.331
f_s	: 3.03
Coefficiente di Sfruttamento a pressoflessione	: 0.331
f_s	: 3.02

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**
Comb. più gravosa : " Comb 29 [SLD] [IN] " - Coeff. Sfruttamento : 0.045 (fs=22.385)
 Taglio Ty di Progetto [daN] : -605
 Taglio Tz di Progetto [daN] : -186
 Momento Torcente Mt di Progetto [daNm] : 983

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.11
 Tensione di Progetto relativa a Tz [N/mm²] : 0.03
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.045
 fs : 22.38

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 14
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.359	Coefficiente di sfruttamento nel piano XZ	: 0.365
fs	: 2.743		

Colonna 204 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
 L= 3100 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**
Comb. più gravosa : " Comb 34 [SLD] [IN] " - Coeff. Sfruttamento : 0.843 (fs=1.186)
 Sforzo Normale di Progetto [daN] : 3680 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -3050
 Momento Flettente Mz di Progetto [daNm] : 1741

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.46
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.031
 fs : 32.25
 Tensione di Progetto relativa a My [N/mm²] : 14.3
 Tensione di Progetto relativa a Mz [N/mm²] : 2.61
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.812
 fs : 1.23
 Coefficiente di Sfruttamento : 0.843
 fs : 1.19

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3100 mm / 3100 mm] - **R 500x160**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.169 (fs=5.911)
 Taglio Ty di Progetto [daN] : 1958
 Taglio Tz di Progetto [daN] : 1380
 Momento Torcente Mt di Progetto [daNm] : -533

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.37
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.26
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.169
fs	: 5.91

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 15.03	Snellezza nel piano XZ	: 46.98
Snellezza relativa nel piano XY	: 0.24	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 25
Coefficiente K nel piano XY	: 0.53	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.848	Coefficiente di sfruttamento nel piano XZ	: 0.853
fs	: 1.173		

Colonna 55 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.746 (fs=1.341)

Sforzo Normale di Progetto [daN]	: 6313 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 2942
Momento Flettente Mz di Progetto [daNm]	: -71

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.79
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.053
fs	: 18.8
Tensione di Progetto relativa a My [N/mm ²]	: 13.79
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.11
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.693
fs	: 1.44
Coefficiente di Sfruttamento	: 0.746
fs	: 1.34

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 15 [SLD] [IN] " - Coeff. Sfruttamento : 0.238 (fs=4.204)

Taglio Ty di Progetto [daN]	: -3333
Taglio Tz di Progetto [daN]	: 487
Momento Torcente Mt di Progetto [daNm]	: 4160

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.63
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.09
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.238
fs	: 4.2

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.747	Coefficiente di sfruttamento nel piano XZ	: 0.747
fs	: 1.339		

Colonna 56 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.272 (fs=3.671)

Sforzo Normale di Progetto [daN]	: -4609 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 42
Momento Flettente Mz di Progetto [daNm]	: 3269

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.58
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.032
fs	: 31.61
Tensione di Progetto relativa a My [N/mm²]	: 0.2
Tensione di Progetto relativa a Mz [N/mm²]	: 4.9
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54
Coefficiente di Sfruttamento a flessione	: 0.271
fs	: 3.68
Coefficiente di Sfruttamento a pressoflessione	: 0.272
fs	: 3.67

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x160**

Comb. più gravosa : " Comb 47 [SLV] [IN] " - Coeff. Sfruttamento : 0.038 (fs=26.154)

Taglio Ty di Progetto [daN]	: -540
Taglio Tz di Progetto [daN]	: 35
Momento Torcente Mt di Progetto [daNm]	: 1417

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.1
Tensione di Progetto relativa a Tz [N/mm²]	: 0.01
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.038
fs	: 26.15

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 56.98
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.91
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9

Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.94
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.84
Coefficiente di sfruttamento nel piano XY	: 0.303	Coefficiente di sfruttamento nel piano XZ	: 0.309
fs	: 3.234		

Colonna 109 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.177 (fs=5.651)

Sforzo Normale di Progetto [daN]	: -3316 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 7
Momento Flettente Mz di Progetto [daNm]	: -1368

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²]	: -0.41
Tensione Resistente [N/mm²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.036
fs	: 27.95
Tensione di Progetto relativa a My [N/mm²]	: 0.03
Tensione di Progetto relativa a Mz [N/mm²]	: 2.05
Tensione Resistente relativa a My [N/mm²]	: 12.74
Tensione Resistente relativa a Mz [N/mm²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.176
fs	: 5.69
Coefficiente di Sfruttamento a pressoflessione	: 0.177
fs	: 5.65

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 853.13 mm] - **R 500x160**

Comb. più gravosa : " Comb 43 [SLV] [IN] " - Coeff. Sfruttamento : 0.092 (fs=10.854)

Taglio Ty di Progetto [daN]	: -1278
Taglio Tz di Progetto [daN]	: -262
Momento Torcente Mt di Progetto [daNm]	: -453

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.24
Tensione di Progetto relativa a Tz [N/mm²]	: 0.05
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.092
fs	: 10.85

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 12.93
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.21
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.52
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.211	Coefficiente di sfruttamento nel piano XZ	: 0.211
fs	: 4.729		

Colonna 122 Copertur[Colonna]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1646.87 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.457 (fs=2.189)

Sforzo Normale di Progetto [daN] : -3264 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : -19
Momento Flettente Mz di Progetto [daNm] : -3545

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -0.41
Tensione Resistente [N/mm²] : 11.59
Coefficiente di Sfruttamento a compressione : 0.035
fs : 28.4
Tensione di Progetto relativa a My [N/mm²] : 0.09
Tensione di Progetto relativa a Mz [N/mm²] : 5.32
Tensione Resistente relativa a My [N/mm²] : 12.74
Tensione Resistente relativa a Mz [N/mm²] : 11.8
Coefficiente di Sfruttamento a flessione : 0.456
fs : 2.19
Coefficiente di Sfruttamento a pressoflessione : 0.457
fs : 2.19

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1646.87 mm / 1646.87 mm] - **R 500x160**

Comb. più gravosa : " Comb 8 [SLD] [IN] " - Coeff. Sfruttamento : 0.107 (fs=9.38)

Taglio Ty di Progetto [daN] : -1491
Taglio Tz di Progetto [daN] : 237
Momento Torcente Mt di Progetto [daNm] : -1455

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.28
Tensione di Progetto relativa a Tz [N/mm²] : 0.04
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.107
fs : 9.38

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 7.99	Snellezza nel piano XZ	: 24.96
Snellezza relativa nel piano XY	: 0.13	Snellezza relativa nel piano XZ	: 0.40
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.58
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.491	Coefficiente di sfruttamento nel piano XZ	: 0.491
fs	: 2.036		

Colonna 207 Copertur[Colonna]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 600 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.553 ($f_s=1.809$)

Sforzo Normale di Progetto [daN] : -3181 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -1
 Momento Flettente Mz di Progetto [daNm] : -4338

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 0.7$

Tensione di Progetto [N/mm²] : -0.4
 Tensione Resistente [N/mm²] : 11.59
 Coefficiente di Sfruttamento a compressione : 0.034
 f_s : 29.14
 Tensione di Progetto relativa a My [N/mm²] : 0.00
 Tensione di Progetto relativa a Mz [N/mm²] : 6.51
 Tensione Resistente relativa a My [N/mm²] : 12.74
 Tensione Resistente relativa a Mz [N/mm²] : 11.8
 Coefficiente di Sfruttamento a flessione : 0.552
 f_s : 1.81
 Coefficiente di Sfruttamento a pressoflessione : 0.553
 f_s : 1.81

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=600 mm / 600 mm] - **R 500x160**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.081 ($f_s=12.346$)

Taglio Ty di Progetto [daN] : -1116
 Taglio Tz di Progetto [daN] : -266
 Momento Torcente Mt di Progetto [daNm] : -2778

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.21
 Tensione di Progetto relativa a Tz [N/mm²] : 0.05
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.081
 f_s : 12.35

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 2.91	Snellezza nel piano XZ	: 9.09
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.14
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.586	Coefficiente di sfruttamento nel piano XZ	: 0.586
f_s	: 1.706		

Colonna 56 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1300 mm - **R 500x160** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.529 ($f_s=1.891$)

Sforzo Normale di Progetto [daN] : 1140 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -14
 Momento Flettente Mz di Progetto [daNm] : -4012

Tipo Verifica : TRAZIONE+FLESSIONE - $K_{mod} = 0.7$

Tensione di Progetto [N/mm²] : 0.14

Tensione Resistente [N/mm ²]	: 9.44
Coefficiente di Sfruttamento a trazione	: 0.015
fs	: 66.21
Tensione di Progetto relativa a My [N/mm ²]	: 0.06
Tensione di Progetto relativa a Mz [N/mm ²]	: 6.02
Tensione Resistente relativa a My [N/mm ²]	: 12.74
Tensione Resistente relativa a Mz [N/mm ²]	: 11.8
Coefficiente di Sfruttamento a flessione	: 0.514
fs	: 1.95
Coefficiente di Sfruttamento	: 0.529
fs	: 1.89

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1300 mm / 1300 mm] - **R 500x160**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.239 (fs=4.185)

Taglio Ty di Progetto [daN]	: 3383
Taglio Tz di Progetto [daN]	: -30
Momento Torcente Mt di Progetto [daNm]	: -4228

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.63
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.239
fs	: 4.19

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 6.30	Snellezza nel piano XZ	: 19.70
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.50	Coefficiente K nel piano XZ	: 0.55
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.514	Coefficiente di sfruttamento nel piano XZ	: 0.514
fs	: 1.947		

Colonna 57 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x220** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x220**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.108 (fs=9.257)

Sforzo Normale di Progetto [daN]	: 6602 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -250
Momento Flettente Mz di Progetto [daNm]	: 781

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.6
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.04
fs	: 24.71
Tensione di Progetto relativa a My [N/mm ²]	: 0.62
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.85
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 18.54

Coefficiente di Sfruttamento a flessione	: 0.068
fs	: 14.8
Coefficiente di Sfruttamento	: 0.108
fs	: 9.26

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x220**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.054 (fs=18.431)

Taglio Ty di Progetto [daN]	: -313
Taglio Tz di Progetto [daN]	: 56
Momento Torcente Mt di Progetto [daNm]	: 591

Tipo Verifica		: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm²]	: 0.04	
Tensione di Progetto relativa a Tz [N/mm²]	: 0.01	
Tensione tang. Resistente [N/mm²]	: 2.66	
Coefficiente di Sfruttamento a taglio	: 0.016	
fs	: 61.19	
Tensione di Progetto [N/mm²]	: 0.19	
Modulo di resistenza a torsione [mm³]	: 6381856.5	
Tensione tang. Resistente [N/mm²]	: 2.66	
Coefficiente di Sfruttamento a torsione	: 0.054	
fs	: 18.52	
Coefficiente di Sfruttamento a taglio+torsione	: 0.054	
fs	: 18.43	

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 41.44
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.66
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.74
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.94
Coefficiente di sfruttamento nel piano XY	: 0.104	Coefficiente di sfruttamento nel piano XZ	: 0.107
fs	: 9.358		

Colonna 57 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 500x220** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 4400 mm] - **R 500x220**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.984 (fs=1.017)

Sforzo Normale di Progetto [daN]	: -907 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -7363
Momento Flettente Mz di Progetto [daNm]	: -1751

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.08
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 220.74
Tensione di Progetto relativa a My [N/mm²]	: 18.26
Tensione di Progetto relativa a Mz [N/mm²]	: 1.91
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 18.54

Coefficiente di Sfruttamento a flessione	: 0.984
fs	: 1.02
Coefficiente di Sfruttamento a pressoflessione	: 0.984
fs	: 1.02

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - R 500x220	
<i>Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.084 (fs=11.968)</i>	
Taglio Ty di Progetto [daN]	: 707
Taglio Tz di Progetto [daN]	: -3206
Momento Torcente Mt di Progetto [daNm]	: -1243

Tipo Verifica		: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm²]	: 0.1	
Tensione di Progetto relativa a Tz [N/mm²]	: 0.44	
Tensione tang. Resistente [N/mm²]	: 2.66	
Coefficiente di Sfruttamento a taglio	: 0.169	
fs	: 5.93	
Tensione di Progetto [N/mm²]	: 0.2	
Modulo di resistenza a torsione [mm³]	: 6381856.5	
Tensione tang. Resistente [N/mm²]	: 2.66	
Coefficiente di Sfruttamento a torsione	: 0.055	
fs	: 18.14	
Coefficiente di Sfruttamento a taglio+torsione	: 0.084	
fs	: 11.97	

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 21.34	Snellezza nel piano XZ	: 48.50
Snellezza relativa nel piano XY	: 0.34	Snellezza relativa nel piano XZ	: 0.77
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.56	Coefficiente K nel piano XZ	: 0.82
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.91
Coefficiente di sfruttamento nel piano XY	: 0.988	Coefficiente di sfruttamento nel piano XZ	: 0.989
fs	: 1.011		

Colonna 58 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 3760 mm] - R 120x400	
<i>Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.359 (fs=2.782)</i>	
Sforzo Normale di Progetto [daN]	: -925 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 2127
Momento Flettente Mz di Progetto [daNm]	: -24

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.19
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.011
fs	: 94.5
Tensione di Progetto relativa a My [N/mm²]	: 6.65
Tensione di Progetto relativa a Mz [N/mm²]	: 0.25
Tensione Resistente relativa a My [N/mm²]	: 18.96
Tensione Resistente relativa a Mz [N/mm²]	: 20.03

Coefficiente di Sfruttamento a flessione	: 0.359
fs	: 2.78
Coefficiente di Sfruttamento a pressoflessione	: 0.359
fs	: 2.78

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - R 120x400	
<i>Comb. più gravosa : " Comb 35 [CAR] [ST] " - Coeff. Sfruttamento : 0.054 (fs=18.682)</i>	
Taglio Ty di Progetto [daN]	: -2
Taglio Tz di Progetto [daN]	: -372
Momento Torcente Mt di Progetto [daNm]	: 3

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0
Tensione di Progetto relativa a Tz [N/mm²]	: 0.12
Tensione tang. Resistente [N/mm²]	: 2.17
Coefficiente di Sfruttamento a taglio	: 0.054
fs	: 18.68

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 41
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.377	Coefficiente di sfruttamento nel piano XZ	: 0.370
fs	: 2.651		

Colonna 58 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - R 120x400	
<i>Comb. più gravosa : " Comb 25 [SLD] [IN] " - Coeff. Sfruttamento : 0.39 (fs=2.563)</i>	
Sforzo Normale di Progetto [daN]	: 913 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 2220
Momento Flettente Mz di Progetto [daNm]	: 32

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.19
Tensione Resistente [N/mm²]	: 15.17
Coefficiente di Sfruttamento a trazione	: 0.013
fs	: 79.74
Tensione di Progetto relativa a My [N/mm²]	: 6.94
Tensione di Progetto relativa a Mz [N/mm²]	: 0.34
Tensione Resistente relativa a My [N/mm²]	: 18.96
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.378
fs	: 2.65
Coefficiente di Sfruttamento	: 0.39
fs	: 2.56

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**
Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.049 (fs=20.47)
 Taglio Ty di Progetto [daN] : -14
 Taglio Tz di Progetto [daN] : 415
 Momento Torcente Mt di Progetto [daNm] : 39

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
 Tensione di Progetto relativa a Tz [N/mm²] : 0.13
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.049
 fs : 20.47

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 34
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.393	Coefficiente di sfruttamento nel piano XZ	: 0.368
fs	: 2.547		

Colonna 59 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
 L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.417 (fs=2.398)
 Sforzo Normale di Progetto [daN] : -1762 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 2465
 Momento Flettente Mz di Progetto [daNm] : -29

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.37
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.02
 fs : 49.6
 Tensione di Progetto relativa a My [N/mm²] : 7.7
 Tensione di Progetto relativa a Mz [N/mm²] : 0.3
 Tensione Resistente relativa a My [N/mm²] : 18.96
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.417
 fs : 2.4
 Coefficiente di Sfruttamento a pressoflessione : 0.417
 fs : 2.4

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**
Comb. più gravosa : " Comb 35 [CAR] [ST] " - Coeff. Sfruttamento : 0.064 (fs=15.664)
 Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : -444
 Momento Torcente Mt di Progetto [daNm] : 1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.14
Tensione tang. Resistente [N/mm ²]	: 2.17
Coefficiente di Sfruttamento a taglio	: 0.064
fs	: 15.66

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.451	Coefficiente di sfruttamento nel piano XZ	: 0.437
fs	: 2.219		

Colonna 59 Copertura[Colonna]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $-\gamma_M=1.45$ (FC=1)
L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.171 (fs=5.837)

Sforzo Normale di Progetto [daN]	: -1247 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: 1037
Momento Flettente M_z di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: -0.26
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.014
fs	: 70.08
Tensione di Progetto relativa a M_y [N/mm ²]	: 3.24
Tensione di Progetto relativa a M_z [N/mm ²]	: 0.00
Tensione Resistente relativa a M_y [N/mm ²]	: 18.96
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.171
fs	: 5.84
Coefficiente di Sfruttamento a pressoflessione	: 0.171
fs	: 5.84

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.035 (fs=28.898)

Taglio T_y di Progetto [daN]	: 11
Taglio T_z di Progetto [daN]	: 294
Momento Torcente M_t di Progetto [daNm]	: -26

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.00
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.09
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.035
fs	: 28.9

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 49
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.203	Coefficiente di sfruttamento nel piano XZ	: 0.186
fs	: 4.936		

Colonna 60 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.46 (fs=2.175)

Sforzo Normale di Progetto [daN]	: -1874 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 2712
Momento Flettente Mz di Progetto [daNm]	: -34

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.39
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.021
fs	: 46.64
Tensione di Progetto relativa a My [N/mm²]	: 8.47
Tensione di Progetto relativa a Mz [N/mm²]	: 0.36
Tensione Resistente relativa a My [N/mm²]	: 18.96
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.459
fs	: 2.18
Coefficiente di Sfruttamento a pressoflessione	: 0.46
fs	: 2.17

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 35 [CAR] [ST] " - Coeff. Sfruttamento : 0.067 (fs=14.873)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: -467
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0
Tensione di Progetto relativa a Tz [N/mm²]	: 0.15
Tensione tang. Resistente [N/mm²]	: 2.17
Coefficiente di Sfruttamento a taglio	: 0.067
fs	: 14.87

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99

Coefficiente di sfruttamento nel piano XY : 0.496
fs : 2.018

Coefficiente di sfruttamento nel piano XZ : 0.481

Colonna 60 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.145 (fs=6.897)

Sforzo Normale di Progetto [daN] : -1261 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : 876
Momento Flettente Mz di Progetto [daNm] : -1

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.26
Tensione Resistente [N/mm²] : 18.21
Coefficiente di Sfruttamento a compressione : 0.014
fs : 69.32
Tensione di Progetto relativa a My [N/mm²] : 2.74
Tensione di Progetto relativa a Mz [N/mm²] : 0.01
Tensione Resistente relativa a My [N/mm²] : 18.96
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.145
fs : 6.91
Coefficiente di Sfruttamento a pressoflessione : 0.145
fs : 6.9

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.025 (fs=39.364)

Taglio Ty di Progetto [daN] : 12
Taglio Tz di Progetto [daN] : 216
Momento Torcente Mt di Progetto [daNm] : -27

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
Tensione di Progetto relativa a Tz [N/mm²] : 0.07
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.025
fs : 39.36

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 49
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.177	Coefficiente di sfruttamento nel piano XZ	: 0.159
fs	: 5.662		

Colonna 61 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.465 (fs=2.151)
 Sforzo Normale di Progetto [daN] : -1764 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 2749
 Momento Flettente Mz di Progetto [daNm] : -31

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.37
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.02
 fs : 49.55
 Tensione di Progetto relativa a My [N/mm²] : 8.59
 Tensione di Progetto relativa a Mz [N/mm²] : 0.32
 Tensione Resistente relativa a My [N/mm²] : 18.96
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.464
 fs : 2.15
 Coefficiente di Sfruttamento a pressoflessione : 0.465
 fs : 2.15

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.085 (fs=11.699)
 Taglio Ty di Progetto [daN] : 16
 Taglio Tz di Progetto [daN] : 726
 Momento Torcente Mt di Progetto [daNm] : -31

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.01
 Tensione di Progetto relativa a Tz [N/mm²] : 0.23
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.085
 fs : 11.7

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.498	Coefficiente di sfruttamento nel piano XZ	: 0.485
fs	: 2.006		

Colonna 61 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**
Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.16 (fs=6.251)
 Sforzo Normale di Progetto [daN] : -664 (COMPRESSIONE)

Momento Flettente My di Progetto [daNm] : 964
 Momento Flettente Mz di Progetto [daNm] : -3

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.14
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.008
 fs : 131.57
 Tensione di Progetto relativa a My [N/mm²] : 3.01
 Tensione di Progetto relativa a Mz [N/mm²] : 0.03
 Tensione Resistente relativa a My [N/mm²] : 18.96
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.16
 fs : 6.25
 Coefficiente di Sfruttamento a pressoflessione : 0.16
 fs : 6.25

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.039 (fs=25.454)

Taglio Ty di Progetto [daN] : 11
 Taglio Tz di Progetto [daN] : 334
 Momento Torcente Mt di Progetto [daNm] : -24

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
 Tensione di Progetto relativa a Tz [N/mm²] : 0.1
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.039
 fs : 25.45

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 49
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.177	Coefficiente di sfruttamento nel piano XZ	: 0.168
fs	: 5.660		

Colonna 62 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.447 (fs=2.238)

Sforzo Normale di Progetto [daN] : -483 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 2643
 Momento Flettente Mz di Progetto [daNm] : -31

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.1
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.006

fs	: 180.87
Tensione di Progetto relativa a My [N/mm ²]	: 8.26
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.32
Tensione Resistente relativa a My [N/mm ²]	: 18.96
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.447
fs	: 2.24
Coefficiente di Sfruttamento a pressoflessione	: 0.447
fs	: 2.24

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.081 (fs=12.378)

Taglio Ty di Progetto [daN]	: 16
Taglio Tz di Progetto [daN]	: 686
Momento Torcente Mt di Progetto [daNm]	: -31

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.21
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.081
fs	: 12.38

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.456	Coefficiente di sfruttamento nel piano XZ	: 0.452
fs	: 2.192		

Colonna 62 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.139 (fs=7.173)

Sforzo Normale di Progetto [daN]	: -367 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -835
Momento Flettente Mz di Progetto [daNm]	: 5

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.08
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.004
fs	: 238.42
Tensione di Progetto relativa a My [N/mm ²]	: 2.61
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.05
Tensione Resistente relativa a My [N/mm ²]	: 18.96
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.139
fs	: 7.17

Coefficiente di Sfruttamento a pressoflessione : 0.139
fs : 7.17

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.039 (fs=25.371)
Taglio Ty di Progetto [daN] : 12
Taglio Tz di Progetto [daN] : 335
Momento Torcente Mt di Progetto [daNm] : -25

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
Tensione di Progetto relativa a Tz [N/mm²] : 0.1
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.039
fs : 25.37

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.158	Coefficiente di sfruttamento nel piano XZ	: 0.144
fs	: 6.322		

Colonna 63 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.458 (fs=2.185)
Sforzo Normale di Progetto [daN] : -904 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : 2700
Momento Flettente Mz di Progetto [daNm] : -34

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.19
Tensione Resistente [N/mm²] : 18.21
Coefficiente di Sfruttamento a compressione : 0.01
fs : 96.71
Tensione di Progetto relativa a My [N/mm²] : 8.44
Tensione di Progetto relativa a Mz [N/mm²] : 0.36
Tensione Resistente relativa a My [N/mm²] : 18.96
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.457
fs : 2.19
Coefficiente di Sfruttamento a pressoflessione : 0.458
fs : 2.19

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.086 (fs=11.571)

Taglio Ty di Progetto [daN]	: 18
Taglio Tz di Progetto [daN]	: 734
Momento Torcente Mt di Progetto [daNm]	: -34

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.23
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.086
fs	: 11.57

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.475	Coefficiente di sfruttamento nel piano XZ	: 0.468
fs	: 2.106		

Colonna 63 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.141 (fs=7.09)

Sforzo Normale di Progetto [daN]	: -607 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 791
Momento Flettente Mz di Progetto [daNm]	: -29

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.13
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.007
fs	: 143.94
Tensione di Progetto relativa a My [N/mm ²]	: 2.47
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.31
Tensione Resistente relativa a My [N/mm ²]	: 18.96
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.141
fs	: 7.09
Coefficiente di Sfruttamento a pressoflessione	: 0.141
fs	: 7.09

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 35 [CAR] [ST] " - Coeff. Sfruttamento : 0.025 (fs=39.253)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: -177
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.06

Tensione tang. Resistente [N/mm ²]	: 2.17
Coefficiente di Sfruttamento a taglio	: 0.025
fs	: 39.25

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.156	Coefficiente di sfruttamento nel piano XZ	: 0.148
fs	: 6.397		

Colonna 64 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.437 (fs=2.288)

Sforzo Normale di Progetto [daN]	: -1290 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 2575
Momento Flettente Mz di Progetto [daNm]	: -34

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.27
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.015
fs	: 67.77
Tensione di Progetto relativa a My [N/mm ²]	: 8.05
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.35
Tensione Resistente relativa a My [N/mm ²]	: 18.96
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.437
fs	: 2.29
Coefficiente di Sfruttamento a pressoflessione	: 0.437
fs	: 2.29

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.086 (fs=11.616)

Taglio Ty di Progetto [daN]	: 18
Taglio Tz di Progetto [daN]	: 731
Momento Torcente Mt di Progetto [daNm]	: -34

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.23
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.086
fs	: 11.62

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
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Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.462	Coefficiente di sfruttamento nel piano XZ	: 0.452
fs	: 2.166		

Colonna 64 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.137 (fs=7.291)

Sforzo Normale di Progetto [daN]	: -380 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -808
Momento Flettente Mz di Progetto [daNm]	: -11

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.08
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.004
fs	: 230.2
Tensione di Progetto relativa a My [N/mm²]	: 2.52
Tensione di Progetto relativa a Mz [N/mm²]	: 0.11
Tensione Resistente relativa a My [N/mm²]	: 18.96
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.137
fs	: 7.29
Coefficiente di Sfruttamento a pressoflessione	: 0.137
fs	: 7.29

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 35 [CAR] [ST] " - Coeff. Sfruttamento : 0.025 (fs=39.331)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: -177
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0
Tensione di Progetto relativa a Tz [N/mm²]	: 0.06
Tensione tang. Resistente [N/mm²]	: 2.17
Coefficiente di Sfruttamento a taglio	: 0.025
fs	: 39.33

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 50
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.147	Coefficiente di sfruttamento nel piano XZ	: 0.142
fs	: 6.816		

Colonna 65 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.383 (fs=2.61)

Sforzo Normale di Progetto [daN] : -1652 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : 2257
Momento Flettente Mz di Progetto [daNm] : -29

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.34
Tensione Resistente [N/mm²] : 18.21
Coefficiente di Sfruttamento a compressione : 0.019
fs : 52.89
Tensione di Progetto relativa a My [N/mm²] : 7.05
Tensione di Progetto relativa a Mz [N/mm²] : 0.31
Tensione Resistente relativa a My [N/mm²] : 18.96
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.383
fs : 2.61
Coefficiente di Sfruttamento a pressoflessione : 0.383
fs : 2.61

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 35 [CAR] [ST] " - Coeff. Sfruttamento : 0.07 (fs=14.21)

Taglio Ty di Progetto [daN] : 0
Taglio Tz di Progetto [daN] : -489
Momento Torcente Mt di Progetto [daNm] : 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
Tensione di Progetto relativa a Tz [N/mm²] : 0.15
Tensione tang. Resistente [N/mm²] : 2.17
Coefficiente di Sfruttamento a taglio : 0.07
fs : 14.21

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.415	Coefficiente di sfruttamento nel piano XZ	: 0.402
fs	: 2.412		

Colonna 65 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**
Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.107 (fs=9.303)
 Sforzo Normale di Progetto [daN] : -248 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -633
 Momento Flettente Mz di Progetto [daNm] : -9

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.05
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.003
 fs : 352.41
 Tensione di Progetto relativa a My [N/mm²] : 1.98
 Tensione di Progetto relativa a Mz [N/mm²] : 0.09
 Tensione Resistente relativa a My [N/mm²] : 18.96
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.107
 fs : 9.3
 Coefficiente di Sfruttamento a pressoflessione : 0.107
 fs : 9.3

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=4400 mm / 4400 mm] - **R 120x400**
Comb. più gravosa : " Comb 35 [CAR] [ST] " - Coeff. Sfruttamento : 0.025 (fs=40.779)
 Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : -170
 Momento Torcente Mt di Progetto [daNm] : -1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.05
 Tensione tang. Resistente [N/mm²] : 2.17
 Coefficiente di Sfruttamento a taglio : 0.025
 fs : 40.78

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 40
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.122	Coefficiente di sfruttamento nel piano XZ	: 0.111
fs	: 8.193		

Colonna 66 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.355 (fs=2.814)
 Sforzo Normale di Progetto [daN] : -661 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 2092
 Momento Flettente Mz di Progetto [daNm] : -29

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.14
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.008
fs	: 132.24
Tensione di Progetto relativa a My [N/mm ²]	: 6.54
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.3
Tensione Resistente relativa a My [N/mm ²]	: 18.96
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.355
fs	: 2.81
Coefficiente di Sfruttamento a pressoflessione	: 0.355
fs	: 2.81

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 35 [CAR] [ST] " - Coeff. Sfruttamento : 0.068 (fs=14.651)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: -474
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.15
Tensione tang. Resistente [N/mm ²]	: 2.17
Coefficiente di Sfruttamento a taglio	: 0.068
fs	: 14.65

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.368	Coefficiente di sfruttamento nel piano XZ	: 0.363
fs	: 2.717		

Colonna 66 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.1 (fs=10.021)

Sforzo Normale di Progetto [daN]	: -907 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -585
Momento Flettente Mz di Progetto [daNm]	: -9

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.19
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.01
fs	: 96.32
Tensione di Progetto relativa a My [N/mm ²]	: 1.83

Tensione di Progetto relativa a M_z [N/mm ²]	: 0.1
Tensione Resistente relativa a M_y [N/mm ²]	: 18.96
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.1
f_s	: 10.03
Coefficiente di Sfruttamento a pressoflessione	: 0.1
f_s	: 10.02

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.03 ($f_s=32.866$)

Taglio T_y di Progetto [daN]	: 3
Taglio T_z di Progetto [daN]	: 259
Momento Torcente M_t di Progetto [daNm]	: 7

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.08
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.03
f_s	: 32.87

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 50
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente K_c nel piano XY	: 0.45	Coefficiente K_c nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.123	Coefficiente di sfruttamento nel piano XZ	: 0.110
f_s	: 8.157		

Colonna 67 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.291 ($f_s=3.439$)

Sforzo Normale di Progetto [daN]	: -1153 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: 1692
Momento Flettente M_z di Progetto [daNm]	: -32

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: -0.24
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.013
f_s	: 75.78
Tensione di Progetto relativa a M_y [N/mm ²]	: 5.29
Tensione di Progetto relativa a M_z [N/mm ²]	: 0.34
Tensione Resistente relativa a M_y [N/mm ²]	: 18.96
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.291
f_s	: 3.44
Coefficiente di Sfruttamento a pressoflessione	: 0.291
f_s	: 3.44

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 35 [CAR] [ST] " - Coeff. Sfruttamento : 0.067 (fs=15.009)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: -463
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0
Tensione di Progetto relativa a Tz [N/mm²]	: 0.14
Tensione tang. Resistente [N/mm²]	: 2.17
Coefficiente di Sfruttamento a taglio	: 0.067
fs	: 15.01

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.313	Coefficiente di sfruttamento nel piano XZ	: 0.304
fs	: 3.196		

Colonna 67 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 6 - [X=3666.67 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.099 (fs=10.058)

Sforzo Normale di Progetto [daN]	: -731 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 593
Momento Flettente Mz di Progetto [daNm]	: -5

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.15
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.008
fs	: 119.53
Tensione di Progetto relativa a My [N/mm²]	: 1.85
Tensione di Progetto relativa a Mz [N/mm²]	: 0.05
Tensione Resistente relativa a My [N/mm²]	: 18.96
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.099
fs	: 10.07
Coefficiente di Sfruttamento a pressoflessione	: 0.099
fs	: 10.06

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.034 (fs=29.629)

Taglio Ty di Progetto [daN]	: 3
Taglio Tz di Progetto [daN]	: 287

Momento Torcente Mt di Progetto [daNm] : 7

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
 Tensione di Progetto relativa a Tz [N/mm²] : 0.09
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.034
 fs : 29.63

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 49
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.118	Coefficiente di sfruttamento nel piano XZ	: 0.108
fs	: 8.488		

Colonna 68 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)
 L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**
 Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.239 (fs=4.176)

Sforzo Normale di Progetto [daN] : -1323 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 1378
 Momento Flettente Mz di Progetto [daNm] : -33

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.28
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.015
 fs : 66.05
 Tensione di Progetto relativa a My [N/mm²] : 4.31
 Tensione di Progetto relativa a Mz [N/mm²] : 0.35
 Tensione Resistente relativa a My [N/mm²] : 18.96
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.239
 fs : 4.18
 Coefficiente di Sfruttamento a pressoflessione : 0.239
 fs : 4.18

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**
 Comb. più gravosa : " Comb 35 [CAR] [ST] " - Coeff. Sfruttamento : 0.063 (fs=15.766)

Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : -441
 Momento Torcente Mt di Progetto [daNm] : -1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.14
 Tensione tang. Resistente [N/mm²] : 2.17
 Coefficiente di Sfruttamento a taglio : 0.063

fs

: 15.77

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 75.98	Snellezza nel piano XZ	: 22.79
Snellezza relativa nel piano XY	: 1.21	Snellezza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.265	Coefficiente di sfruttamento nel piano XZ	: 0.254
fs	: 3.777		

Colonna 68 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 6 - [X=3666.67 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.093 (fs=10.719)

Sforzo Normale di Progetto [daN]	: -579 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 554
Momento Flettente Mz di Progetto [daNm]	: -5

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.12
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.007
fs	: 150.98
Tensione di Progetto relativa a My [N/mm²]	: 1.73
Tensione di Progetto relativa a Mz [N/mm²]	: 0.06
Tensione Resistente relativa a My [N/mm²]	: 18.96
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.093
fs	: 10.72
Coefficiente di Sfruttamento a pressoflessione	: 0.093
fs	: 10.72

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.034 (fs=29.433)

Taglio Ty di Progetto [daN]	: 4
Taglio Tz di Progetto [daN]	: 289
Momento Torcente Mt di Progetto [daNm]	: 8

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm²]	: 0.09
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.034
fs	: 29.43

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42

Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 49
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.108	Coefficiente di sfruttamento nel piano XZ	: 0.100
fs	: 9.271		

Colonna 69 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.156 (fs=6.408)

Sforzo Normale di Progetto [daN]	: -1542 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 872
Momento Flettente Mz di Progetto [daNm]	: -33

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.32
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.018
fs	: 56.69
Tensione di Progetto relativa a My [N/mm²]	: 2.73
Tensione di Progetto relativa a Mz [N/mm²]	: 0.34
Tensione Resistente relativa a My [N/mm²]	: 18.96
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.156
fs	: 6.42
Coefficiente di Sfruttamento a pressoflessione	: 0.156
fs	: 6.41

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 120x400**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.076 (fs=13.123)

Taglio Ty di Progetto [daN]	: 7
Taglio Tz di Progetto [daN]	: -647
Momento Torcente Mt di Progetto [daNm]	: -13

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm²]	: 0.2
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.076
fs	: 13.12

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellenza nel piano XY	: 75.98	Snellenza nel piano XZ	: 22.79
Snellenza relativa nel piano XY	: 1.21	Snellenza relativa nel piano XZ	: 0.36
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 1.28	Coefficiente K nel piano XZ	: 0.57
Coefficiente Kc nel piano XY	: 0.59	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.185	Coefficiente di sfruttamento nel piano XZ	: 0.174
fs	: 5.392		

Colonna 69 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 4400 mm - **R 120x400** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=4400 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 47 [SLV] [IN] " - Coeff. Sfruttamento : 0.124 (fs=8.076)

Sforzo Normale di Progetto [daN]	: 359 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 667
Momento Flettente Mz di Progetto [daNm]	: -24

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.07
Tensione Resistente [N/mm²]	: 15.17
Coefficiente di Sfruttamento a trazione	: 0.005
fs	: 202.66
Tensione di Progetto relativa a My [N/mm²]	: 2.09
Tensione di Progetto relativa a Mz [N/mm²]	: 0.25
Tensione Resistente relativa a My [N/mm²]	: 18.96
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.119
fs	: 8.41
Coefficiente di Sfruttamento	: 0.124
fs	: 8.08

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 4400 mm] - **R 120x400**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.044 (fs=22.709)

Taglio Ty di Progetto [daN]	: 5
Taglio Tz di Progetto [daN]	: 374
Momento Torcente Mt di Progetto [daNm]	: 10

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm²]	: 0.12
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.044
fs	: 22.71

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 88.91	Snellezza nel piano XZ	: 26.67
Snellezza relativa nel piano XY	: 1.42	Snellezza relativa nel piano XZ	: 0.42
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 47
Coefficiente K nel piano XY	: 1.56	Coefficiente K nel piano XZ	: 0.60
Coefficiente Kc nel piano XY	: 0.45	Coefficiente Kc nel piano XZ	: 0.99
Coefficiente di sfruttamento nel piano XY	: 0.119	Coefficiente di sfruttamento nel piano XZ	: 0.119
fs	: 8.412		

Colonna 70 Primo Imp[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 3760 mm - **R 500x220** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=3760 mm / 3760 mm] - **R 500x220**
Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.071 (fs=14.145)
 Sforzo Normale di Progetto [daN] : -282 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -66
 Momento Flettente Mz di Progetto [daNm] : -1105

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1
 Tensione di Progetto [N/mm²] : -0.03
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.001
 fs : 711.23
 Tensione di Progetto relativa a My [N/mm²] : 0.16
 Tensione di Progetto relativa a Mz [N/mm²] : 1.21
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.071
 fs : 14.15
 Coefficiente di Sfruttamento a pressoflessione : 0.071
 fs : 14.15

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=3760 mm / 3760 mm] - **R 500x220**
Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.036 (fs=27.869)
 Taglio Ty di Progetto [daN] : 314
 Taglio Tz di Progetto [daN] : 38
 Momento Torcente Mt di Progetto [daNm] : -590

Tipo Verifica : TAGLIO+TORSIONE
 Tensione di Progetto relativa a Ty [N/mm²] : 0.04
 Tensione di Progetto relativa a Tz [N/mm²] : 0.01
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.016
 fs : 61.64
 Tensione di Progetto [N/mm²] : 0.13
 Modulo di resistenza a torsione [mm³] : 6381856.5
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.036
 fs : 28.07
 Coefficiente di Sfruttamento a taglio+torsione : 0.036
 fs : 27.87

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 18.24	Snellezza nel piano XZ	: 41.44
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.66
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 10
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.74
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.94
Coefficiente di sfruttamento nel piano XY	: 0.077	Coefficiente di sfruttamento nel piano XZ	: 0.078
fs	: 12.901		

Colonna 110 Copertur[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 853.13 mm - **R 500x220** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=853.13 mm / 853.13 mm] - **R 500x220**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.114 (fs=8.788)

Sforzo Normale di Progetto [daN] : -2500 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 704
 Momento Flettente Mz di Progetto [daNm] : -644

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.23
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.012
 fs : 80.1
 Tensione di Progetto relativa a My [N/mm²] : 1.74
 Tensione di Progetto relativa a Mz [N/mm²] : 0.7
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.114
 fs : 8.8
 Coefficiente di Sfruttamento a pressoflessione : 0.114
 fs : 8.79

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=853.13 mm / 853.13 mm] - **R 500x220**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.058 (fs=17.344)

Taglio Ty di Progetto [daN] : -368
 Taglio Tz di Progetto [daN] : 139
 Momento Torcente Mt di Progetto [daNm] : 597

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.05
 Tensione di Progetto relativa a Tz [N/mm²] : 0.02
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.02
 fs : 49.45
 Tensione di Progetto [N/mm²] : 0.2
 Modulo di resistenza a torsione [mm³] : 6381856.5
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.057
 fs : 17.47
 Coefficiente di Sfruttamento a taglio+torsione : 0.058
 fs : 17.34

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 4.14	Snellezza nel piano XZ	: 9.40
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.15
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.49	Coefficiente K nel piano XZ	: 0.50
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 1.00
Coefficiente di sfruttamento nel piano XY	: 0.126	Coefficiente di sfruttamento nel piano XZ	: 0.126
fs	: 7.929		

Colonna 70 Copertura[Colonna]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 3546.87 mm - **R 500x220** - SEZIONI UTILIZZATE : 8

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 3546.87 mm] - **R 500x220**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.153 (fs=6.516)

Sforzo Normale di Progetto [daN] : -2003 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -937
 Momento Flettente Mz di Progetto [daNm] : 907

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.18
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.01
 fs : 100.01
 Tensione di Progetto relativa a My [N/mm²] : 2.32
 Tensione di Progetto relativa a Mz [N/mm²] : 0.99
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 18.54
 Coefficiente di Sfruttamento a flessione : 0.153
 fs : 6.52
 Coefficiente di Sfruttamento a pressoflessione : 0.153
 fs : 6.52

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 8 - [X=3546.87 mm / 3546.87 mm] - **R 500x220**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.046 (fs=21.768)

Taglio Ty di Progetto [daN] : 376
 Taglio Tz di Progetto [daN] : 515
 Momento Torcente Mt di Progetto [daNm] : -414

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.05
 Tensione di Progetto relativa a Tz [N/mm²] : 0.07
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.033
 fs : 30.54
 Tensione di Progetto [N/mm²] : 0.16
 Modulo di resistenza a torsione [mm³] : 6381856.5
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.045
 fs : 22.29
 Coefficiente di Sfruttamento a taglio+torsione : 0.046
 fs : 21.77

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.70
Snellezza nel piano XY	: 17.20	Snellezza nel piano XZ	: 39.09
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.62
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.54	Coefficiente K nel piano XZ	: 0.71
Coefficiente Kc nel piano XY	: 1.00	Coefficiente Kc nel piano XZ	: 0.95
Coefficiente di sfruttamento nel piano XY	: 0.163	Coefficiente di sfruttamento nel piano XZ	: 0.164
fs	: 6.103		

Campata 1-2 Primo Im[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1662.44 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1662.44 mm] - **R 160x500**
Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.417 (fs=2.396)
 Sforzo Normale di Progetto [daN] : 1724 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 1063
 Momento Flettente Mz di Progetto [daNm] : 1464

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.22
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.015
 fs : 68.81
 Tensione di Progetto relativa a My [N/mm²] : 1.59
 Tensione di Progetto relativa a Mz [N/mm²] : 6.86
 Tensione Resistente relativa a My [N/mm²] : 18.54
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.403
 fs : 2.48
 Coefficiente di Sfruttamento : 0.417
 fs : 2.4

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1662.44 mm] - **R 160x500**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.104 (fs=9.634)
 Taglio Ty di Progetto [daN] : -1493
 Taglio Tz di Progetto [daN] : 717
 Momento Torcente Mt di Progetto [daNm] : -891

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.28
 Tensione di Progetto relativa a Tz [N/mm²] : 0.13
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.117
 fs : 8.55
 Tensione di Progetto [N/mm²] : 0.35
 Modulo di resistenza a torsione [mm³] : 3579418.25
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.09
 fs : 11.1
 Coefficiente di Sfruttamento a taglio+torsione : 0.104
 fs : 9.63

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 51	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1662.4	Lunghezza efficace nel piano XZ	: 1662.4
Momento Critico nel piano XY	: 421380 daNm	Momento Critico nel piano XZ	: 134842 daNm
Tensione Critica nel piano XY	: 1975.22 N/mm ²	Tensione Critica nel piano XZ	: 202.26 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 6.98 N/mm ²	Tensione fless. piano XZ	: 1.39 N/mm ²
Snellezza relativa nel piano XY	: 0.11	Snellezza relativa nel piano XZ	: 0.34
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.349	Coefficiente sfrutt. nel piano XZ	: 0.075
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.349	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.075
fs	: 2.868		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto			
Lunghezza elemento	: 1662.4 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.0 daN/m	-	
-		Carico distribuito Finale	: -441.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.005 mm	Limite Freccia Istantanea L/500	: 3.325 mm
Freccia Netta Finale	: -0.009 mm	Limite Freccia Netta Fin. L/ 350	: 4.750 mm
Freccia Finale	: -0.009 mm	Limite Freccia Finale L/ 300	: 5.541 mm
Fatt. sicurezza freccia Istantanea	: 679.066	Fatt. sicurezza freccia Netta Finale	: 538.941
Fatt. sicurezza freccia Finale	: 628.765	Fatt. sicurezza	: 538.941

Campata 1-15 Primo I[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1590 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1590 mm] - **R 160x500**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.831 (fs=1.203)

Sforzo Normale di Progetto [daN]	: 2752 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -7084
Momento Flettente Mz di Progetto [daNm]	: -1435

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.34
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.023
fs	: 43.12
Tensione di Progetto relativa a My [N/mm ²]	: 10.63
Tensione di Progetto relativa a Mz [N/mm ²]	: 6.73
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.808
fs	: 1.24
Coefficiente di Sfruttamento	: 0.831
fs	: 1.2

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1590 mm / 1590 mm] - **R 160x500**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.4 (fs=2.5)

Taglio Ty di Progetto [daN]	: 368
Taglio Tz di Progetto [daN]	: -5651
Momento Torcente Mt di Progetto [daNm]	: 592

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.07
Tensione di Progetto relativa a Tz [N/mm ²]	: 1.06
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.4
fs	: 2.5

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1590.0	Lunghezza efficace nel piano XZ	: 1590.0
Momento Critico nel piano XY	: 440578 daNm	Momento Critico nel piano XZ	: 140985 daNm
Tensione Critica nel piano XY	: 2065.21 N/mm ²	Tensione Critica nel piano XZ	: 211.48 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 2.21 N/mm ²	Tensione fless. piano XZ	: 10.57 N/mm ²
Snellezza relativa nel piano XY	: 0.11	Snellezza relativa nel piano XZ	: 0.34
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.110	Coefficiente sfrutt. nel piano XZ	: 0.570
Coeff. sfrutt. max euleriano	: 0.019		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.129	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.589
fs	: 1.699		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1590.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.004 mm	Limite Freccia Istantanea L/500	: 3.180 mm
Freccia Netta Finale	: -0.007 mm	Limite Freccia Netta Fin. L/ 350	: 4.543 mm
Freccia Finale	: -0.007 mm	Limite Freccia Finale L/ 300	: 5.300 mm
Fatt. sicurezza freccia Istantanea	: 775.261	Fatt. sicurezza freccia Netta Finale	: 615.286
Fatt. sicurezza freccia Finale	: 717.834	Fatt. sicurezza	: 615.286

Campata 2-3 Primo Im[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.311 (fs=3.215)

Sforzo Normale di Progetto [daN]	: 1413 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -136
Momento Flettente Mz di Progetto [daNm]	: -1245

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.18
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.012
fs	: 83.98
Tensione di Progetto relativa a My [N/mm ²]	: 0.2
Tensione di Progetto relativa a Mz [N/mm ²]	: 5.84
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.299
fs	: 3.34
Coefficiente di Sfruttamento	: 0.311
fs	: 3.22

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.091 (fs=11.043)

Taglio Ty di Progetto [daN] : 1232
 Taglio Tz di Progetto [daN] : 357
 Momento Torcente Mt di Progetto [daNm] : 1289

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.23
 Tensione di Progetto relativa a Tz [N/mm²] : 0.07
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.091
 fs : 11.04

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mmq	Tensione Critica nel piano XZ	: 243.66 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.54 N/mmq
Tensione fless. piano XY	: 6.04 N/mmq	Tensione fless. piano XZ	: 0.11 N/mmq
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.302	Coefficiente sfrutt. nel piano XZ	: 0.006
Coeff. sfrutt. max euleriano	: 0.003		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.305	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.009
fs	: 3.283		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 3-4 Primo Im[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.246 (fs=4.072)

Sforzo Normale di Progetto [daN] : 1719 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -191
 Momento Flettente Mz di Progetto [daNm] : -941

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.21
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.014
fs	: 69.03
Tensione di Progetto relativa a My [N/mm ²]	: 0.29
Tensione di Progetto relativa a Mz [N/mm ²]	: 4.41
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.231
fs	: 4.33
Coefficiente di Sfruttamento	: 0.246
fs	: 4.07

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.053 (fs=18.84)

Taglio Ty di Progetto [daN]	: -6
Taglio Tz di Progetto [daN]	: 478
Momento Torcente Mt di Progetto [daNm]	: -29

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.09
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.053
fs	: 18.84

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 50	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 4.41 N/mm ²	Tensione fless. piano XZ	: 0.29 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.220	Coefficiente sfrutt. nel piano XZ	: 0.015
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.220	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.015
fs	: 4.540		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001

Fatt. sicurezza freccia Finale : 1000.000 Fatt. sicurezza : 941.001

Campata 4-5 Primo Im[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)
L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 43 [SLV] [IN] " - Coeff. Sfruttamento : 0.231 (fs=4.332)

Sforzo Normale di Progetto [daN] : 1293 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : -93
Momento Flettente Mz di Progetto [daNm] : -917

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.16
Tensione Resistente [N/mm²] : 14.83
Coefficiente di Sfruttamento a trazione : 0.011
fs : 91.79
Tensione di Progetto relativa a My [N/mm²] : 0.14
Tensione di Progetto relativa a Mz [N/mm²] : 4.3
Tensione Resistente relativa a My [N/mm²] : 18.54
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.22
fs : 4.55
Coefficiente di Sfruttamento : 0.231
fs : 4.33

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.051 (fs=19.509)

Taglio Ty di Progetto [daN] : -10
Taglio Tz di Progetto [daN] : 462
Momento Torcente Mt di Progetto [daNm] : -20

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
Tensione di Progetto relativa a Tz [N/mm²] : 0.09
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a taglio : 0.051
fs : 19.51

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mmq	Tensione Critica nel piano XZ	: 243.66 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.54 N/mmq
Tensione fless. piano XY	: 4.42 N/mmq	Tensione fless. piano XZ	: 0.04 N/mmq
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.221	Coefficiente sfrutt. nel piano XZ	: 0.002
Coeff. sfrutt. max euleriano	: 0.001		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.222	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.004
fs	: 4.503		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 5-6 Primo Im[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 29 [SLD] [IN] " - Coeff. Sfruttamento : 0.233 (fs=4.29)

Sforzo Normale di Progetto [daN]	: 1303 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -136
Momento Flettente Mz di Progetto [daNm]	: -916

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.16
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.011
fs	: 91.11
Tensione di Progetto relativa a My [N/mm ²]	: 0.2
Tensione di Progetto relativa a Mz [N/mm ²]	: 4.3
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.222
fs	: 4.5
Coefficiente di Sfruttamento	: 0.233
fs	: 4.29

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.073 (fs=13.617)

Taglio Ty di Progetto [daN]	: 913
Taglio Tz di Progetto [daN]	: -498
Momento Torcente Mt di Progetto [daNm]	: -236

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.17
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.09
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.073
fs	: 13.62

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 4.44 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.222	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.224	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.002
fs	: 4.470		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 6-7 Primo Im[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.208 (fs=4.805)

Sforzo Normale di Progetto [daN]	: 1388 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -239
Momento Flettente Mz di Progetto [daNm]	: 781

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.17
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.012
fs	: 85.47
Tensione di Progetto relativa a My [N/mm ²]	: 0.36
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.66
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.196
fs	: 5.09
Coefficiente di Sfruttamento	: 0.208
fs	: 4.81

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.05 (fs=19.851)

Taglio Ty di Progetto [daN] : -1
 Taglio Tz di Progetto [daN] : 454
 Momento Torcente Mt di Progetto [daNm] : 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.09
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.05
 fs : 19.85

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 45	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mmq	Tensione Critica nel piano XZ	: 243.66 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.54 N/mmq
Tensione fless. piano XY	: 3.66 N/mmq	Tensione fless. piano XZ	: 0.36 N/mmq
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.183	Coefficiente sfrutt. nel piano XZ	: 0.019
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.183	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.019
fs	: 5.469		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 7-8 Primo Im[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.207 (fs=4.833)

Sforzo Normale di Progetto [daN] : 983 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : -263
 Momento Flettente Mz di Progetto [daNm] : 785

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.12
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.008
 fs : 120.71
 Tensione di Progetto relativa a My [N/mm²] : 0.39
 Tensione di Progetto relativa a Mz [N/mm²] : 3.68
 Tensione Resistente relativa a My [N/mm²] : 18.54
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.199
 fs : 5.04
 Coefficiente di Sfruttamento : 0.207
 fs : 4.83

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.052 (fs=19.337)

Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : 466
 Momento Torcente Mt di Progetto [daNm] : 1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.09
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.052
 fs : 19.34

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 3.82 N/mm ²	Tensione fless. piano XZ	: 0.12 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.191	Coefficiente sfrutt. nel piano XZ	: 0.007
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.191	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.007
fs	: 5.237		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1380.0 mm
 Comb. di carico più gravosa : 142
 Carico distribuito Istantaneo : -441.6 daN/m
 -
 Freccia Istantanea - COMBINAZIONE
 Freccia Finale - COMBINAZIONE
 Modulo Elastico istantaneo : 11500.0 N/mm²
 Controfreccia : 0.000 mm
 Freccia Istantanea : -0.002 mm

Schema adottato Doppio Incastro
 Peso proprio : -30.8 daN/m
 -
 Carico distribuito Finale : -441.6 daN/m
 Comb 42 [CAR] [ST]
 Comb 2 [SLEQP] [LT]
 Modulo Elastico finale : 6388.9 N/mm²
 Limite Freccia Istantanea L/500 : 2.760 mm

Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 8-9 Primo Im[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.192 (fs=5.211)

Sforzo Normale di Progetto [daN]	: 1406 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -59
Momento Flettente Mz di Progetto [daNm]	: -755

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.18
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.012
fs	: 84.4
Tensione di Progetto relativa a My [N/mm²]	: 0.09
Tensione di Progetto relativa a Mz [N/mm²]	: 3.54
Tensione Resistente relativa a My [N/mm²]	: 18.54
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.18
fs	: 5.55
Coefficiente di Sfruttamento	: 0.192
fs	: 5.21

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.052 (fs=19.326)

Taglio Ty di Progetto [daN]	: 1
Taglio Tz di Progetto [daN]	: -466
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0
Tensione di Progetto relativa a Tz [N/mm²]	: 0.09
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.052
fs	: 19.33

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm²	Tensione Critica nel piano XZ	: 243.66 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.54 N/mm²
Tensione fless. piano XY	: 3.78 N/mm²	Tensione fless. piano XZ	: 0.08 N/mm²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.189	Coefficiente sfrutt. nel piano XZ	: 0.004
Coeff. sfrutt. max euleriano	: 0.002		

Coeff. sfrutt. TOTALE (Piano XY) : 0.191
fs : 5.237

Coeff. sfrutt. TOTALE (Piano XZ) : 0.007

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1380.0 mm
Comb. di carico più gravosa : 142
Carico distribuito Istantaneo : -441.6 daN/m

Schema adottato Doppio Incastro
Peso proprio : -30.8 daN/m

-
Freccia Istantanea - COMBINAZIONE
Freccia Finale - COMBINAZIONE
Modulo Elastico istantaneo : 11500.0 N/mm²

Carico distribuito Finale : -441.6 daN/m
Comb 42 [CAR] [ST]
Comb 2 [SLEQP] [LT]
Modulo Elastico finale : 6388.9 N/mm²

Controfreccia : 0.000 mm
Freccia Istantanea : -0.002 mm
Freccia Netta Finale : -0.004 mm
Freccia Finale : -0.004 mm
Fatt. sicurezza freccia Istantanea : 1000.000
Fatt. sicurezza freccia Finale : 1000.000

Limite Freccia Istantanea L/500 : 2.760 mm
Limite Freccia Netta Fin. L/350 : 3.943 mm
Limite Freccia Finale L/300 : 4.600 mm
Fatt. sicurezza freccia Netta Finale : 941.001
Fatt. sicurezza : 941.001

Campata 9-10 Primo I[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.238 (fs=4.202)

Sforzo Normale di Progetto [daN] : 1425 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : -247
Momento Flettente Mz di Progetto [daNm] : 906

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.18
Tensione Resistente [N/mm²] : 14.83
Coefficiente di Sfruttamento a trazione : 0.012
fs : 83.29
Tensione di Progetto relativa a My [N/mm²] : 0.37
Tensione di Progetto relativa a Mz [N/mm²] : 4.25
Tensione Resistente relativa a My [N/mm²] : 18.54
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.226
fs : 4.42
Coefficiente di Sfruttamento : 0.238
fs : 4.2

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.062 (fs=16.178)

Taglio Ty di Progetto [daN] : 266
Taglio Tz di Progetto [daN] : -834
Momento Torcente Mt di Progetto [daNm] : -298

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.05
Tensione di Progetto relativa a Tz [N/mm²] : 0.16
Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a taglio : 0.062
fs : 16.18

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 49	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 4.27 N/mm ²	Tensione fless. piano XZ	: 0.29 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.213	Coefficiente sfrutt. nel piano XZ	: 0.015
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.213	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.015
fs	: 4.685		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 10-11 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.239 (fs=4.184)

Sforzo Normale di Progetto [daN]	: 1195 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -272
Momento Flettente Mz di Progetto [daNm]	: 912

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.15
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.01
fs	: 99.31
Tensione di Progetto relativa a My [N/mm ²]	: 0.41
Tensione di Progetto relativa a Mz [N/mm ²]	: 4.28
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.229

fs	: 4.37
Coefficiente di Sfruttamento	: 0.239
fs	: 4.18

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.056 (fs=17.862)

Taglio Ty di Progetto [daN]	: -335
Taglio Tz di Progetto [daN]	: 718
Momento Torcente Mt di Progetto [daNm]	: -304

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.06
Tensione di Progetto relativa a Tz [N/mm²]	: 0.13
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.056
fs	: 17.86

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 49	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm²	Tensione Critica nel piano XZ	: 243.66 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.54 N/mm²
Tensione fless. piano XY	: 4.31 N/mm²	Tensione fless. piano XZ	: 0.31 N/mm²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.215	Coefficiente sfrutt. nel piano XZ	: 0.017
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.215	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.017
fs	: 4.646		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 11-12 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 160x500**
Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.178 (fs=5.606)
 Sforzo Normale di Progetto [daN] : 966 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -147
 Momento Flettente Mz di Progetto [daNm] : -692

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.12
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.008
 fs : 122.9
 Tensione di Progetto relativa a My [N/mm²] : 0.22
 Tensione di Progetto relativa a Mz [N/mm²] : 3.24
 Tensione Resistente relativa a My [N/mm²] : 18.54
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.17
 fs : 5.87
 Coefficiente di Sfruttamento : 0.178
 fs : 5.61

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 160x500**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.054 (fs=18.561)
 Taglio Ty di Progetto [daN] : 6
 Taglio Tz di Progetto [daN] : -485
 Momento Torcente Mt di Progetto [daNm] : -29

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
 Tensione di Progetto relativa a Tz [N/mm²] : 0.09
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.054
 fs : 18.56

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 37	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 3.24 N/mm ²	Tensione fless. piano XZ	: 0.22 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.162	Coefficiente sfrutt. nel piano XZ	: 0.012
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.162	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.012
fs	: 6.176		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1380.0 mm
 Comb. di carico più gravosa : 142
 Carico distribuito Istantaneo : -441.6 daN/m
 -
 Freccia Istantanea - COMBINAZIONE
 Freccia Finale - COMBINAZIONE

Schema adottato Doppio Incastro
 Peso proprio : -30.8 daN/m
 -
 Carico distribuito Finale : -441.6 daN/m
 Comb 42 [CAR] [ST]
 Comb 2 [SLEQP] [LT]

Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 12-13 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.214 (fs=4.676)

Sforzo Normale di Progetto [daN]	: 1233 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -339
Momento Flettente Mz di Progetto [daNm]	: 787

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.15
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.01
fs	: 96.26
Tensione di Progetto relativa a My [N/mm ²]	: 0.51
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.69
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.203
fs	: 4.91
Coefficiente di Sfruttamento	: 0.214
fs	: 4.68

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.084 (fs=11.837)

Taglio Ty di Progetto [daN]	: -1126
Taglio Tz di Progetto [daN]	: 403
Momento Torcente Mt di Progetto [daNm]	: -443

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.21
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.08
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.084
fs	: 11.84

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 44	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 4.05 N/mm ²	Tensione fless. piano XZ	: 0.14 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31

TABULATI DI CALCOLO -

Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.202	Coefficiente sfrutt. nel piano XZ	: 0.008
Coeff. sfrutt. max euleriano	: 0.001		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.203	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.008
fs	: 4.924		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 13-14 Primo [Travel]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1662.44 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1662.44 mm / 1662.44 mm] - **R 160x500**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.227 (fs=4.414)

Sforzo Normale di Progetto [daN]	: -468 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 573
Momento Flettente Mz di Progetto [daNm]	: 829

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.003
fs	: 310.96
Tensione di Progetto relativa a My [N/mm ²]	: 0.86
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.89
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.227
fs	: 4.41
Coefficiente di Sfruttamento a pressoflessione	: 0.227
fs	: 4.41

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1662.44 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.078 (fs=12.841)

Taglio Ty di Progetto [daN]	: -254
Taglio Tz di Progetto [daN]	: 654
Momento Torcente Mt di Progetto [daNm]	: 30

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.05
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.12
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.078
f_s	: 12.84

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1662.4	Lunghezza efficace nel piano XZ	: 1662.4
Momento Critico nel piano XY	: 421380 daNm	Momento Critico nel piano XZ	: 134842 daNm
Tensione Critica nel piano XY	: 1975.22 N/mm ²	Tensione Critica nel piano XZ	: 202.26 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 3.99 N/mm ²	Tensione fless. piano XZ	: 0.26 N/mm ²
Snellezza relativa nel piano XY	: 0.11	Snellezza relativa nel piano XZ	: 0.34
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.199	Coefficiente sfrutt. nel piano XZ	: 0.014
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.199	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.014
f_s	: 5.022		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1662.4 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.0 daN/m	-	
-		Carico distribuito Finale	: -441.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.005 mm	Limite Freccia Istantanea L/500	: 3.325 mm
Freccia Netta Finale	: -0.009 mm	Limite Freccia Netta Fin. L/ 350	: 4.750 mm
Freccia Finale	: -0.009 mm	Limite Freccia Finale L/ 300	: 5.541 mm
Fatt. sicurezza freccia Istantanea	: 679.066	Fatt. sicurezza freccia Netta Finale	: 538.941
Fatt. sicurezza freccia Finale	: 628.765	Fatt. sicurezza	: 538.941

Campata 14-16 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1590 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1590 mm] - **R 160x500**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.243 ($f_s=4.118$)

Sforzo Normale di Progetto [daN]	: 855 (TRAZIONE)
Momento Flettente M_y di Progetto [daNm]	: -704
Momento Flettente M_z di Progetto [daNm]	: 837

Tipo Verifica : TRAZIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: 0.11
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.007
f_s	: 138.82
Tensione di Progetto relativa a M_y [N/mm ²]	: 1.06
Tensione di Progetto relativa a M_z [N/mm ²]	: 3.92

Tensione Resistente relativa a M_y [N/mm ²]	: 18.54
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.236
f_s	: 4.24
Coefficiente di Sfruttamento	: 0.243
f_s	: 4.12

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1590 mm] - **R 160x500**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.09 ($f_s=11.089$)

Taglio T_y di Progetto [daN]	: 679
Taglio T_z di Progetto [daN]	: 1082
Momento Torcente M_t di Progetto [daNm]	: 597

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.13
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.2
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.09
f_s	: 11.09

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 18	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1590.0	Lunghezza efficace nel piano XZ	: 1590.0
Momento Critico nel piano XY	: 440578 daNm	Momento Critico nel piano XZ	: 140985 daNm
Tensione Critica nel piano XY	: 2065.21 N/mm ²	Tensione Critica nel piano XZ	: 211.48 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 3.98 N/mm ²	Tensione fless. piano XZ	: 0.48 N/mm ²
Snellezza relativa nel piano XY	: 0.11	Snellezza relativa nel piano XZ	: 0.34
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.199	Coefficiente sfrutt. nel piano XZ	: 0.026
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.199	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.026
f_s	: 5.037		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale ($t \rightarrow \infty$)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1590.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.004 mm	Limite Freccia Istantanea L/500	: 3.180 mm
Freccia Netta Finale	: -0.007 mm	Limite Freccia Netta Fin. L/ 350	: 4.543 mm
Freccia Finale	: -0.007 mm	Limite Freccia Finale L/ 300	: 5.300 mm
Fatt. sicurezza freccia Istantanea	: 775.261	Fatt. sicurezza freccia Netta Finale	: 615.286
Fatt. sicurezza freccia Finale	: 717.834	Fatt. sicurezza	: 615.286

Campata 15-17 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 160x500**
Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.286 (fs=3.502)

Sforzo Normale di Progetto [daN]	: 1653 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 2429
Momento Flettente Mz di Progetto [daNm]	: 459

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.21
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.014
fs	: 71.78
Tensione di Progetto relativa a My [N/mm ²]	: 3.64
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.15
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.272
fs	: 3.68
Coefficiente di Sfruttamento	: 0.286
fs	: 3.5

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**
Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.249 (fs=4.022)

Taglio Ty di Progetto [daN]	: -417
Taglio Tz di Progetto [daN]	: 3496
Momento Torcente Mt di Progetto [daNm]	: -114

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.08
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.66
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.249
fs	: 4.02

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 0.75 N/mm ²	Tensione fless. piano XZ	: 3.79 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.037	Coefficiente sfrutt. nel piano XZ	: 0.204
Coeff. sfrutt. max euleriano	: 0.013		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.051	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.218
fs	: 4.590		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m		

-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 16-18 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.201 (fs=4.969)

Sforzo Normale di Progetto [daN]	: 697 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -296
Momento Flettente Mz di Progetto [daNm]	: -763

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.09
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.006
fs	: 170.18
Tensione di Progetto relativa a My [N/mm ²]	: 0.44
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.58
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.195
fs	: 5.12
Coefficiente di Sfruttamento	: 0.201
fs	: 4.97

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 29 [SLD] [IN] " - Coeff. Sfruttamento : 0.067 (fs=14.87)

Taglio Ty di Progetto [daN]	: -613
Taglio Tz di Progetto [daN]	: 729
Momento Torcente Mt di Progetto [daNm]	: -514

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.11
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.14
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.067
fs	: 14.87

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 51	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²

Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 3.58 N/mm ²	Tensione fless. piano XZ	: 0.44 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.179	Coefficiente sfrutt. nel piano XZ	: 0.024
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.179	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.024
fs	: 5.598		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 17-19 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.168 (fs=5.938)

Sforzo Normale di Progetto [daN]	: 1092 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -947
Momento Flettente Mz di Progetto [daNm]	: 451

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.14
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.009
fs	: 108.63
Tensione di Progetto relativa a My [N/mm ²]	: 1.42
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.11
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.159
fs	: 6.28
Coefficiente di Sfruttamento	: 0.168
fs	: 5.94

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.11 (fs=9.052)

Taglio Ty di Progetto [daN]	: 92
Taglio Tz di Progetto [daN]	: 1562

Momento Torcente Mt di Progetto [daNm] : 354

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
 Tensione di Progetto relativa a Tz [N/mm²] : 0.29
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.11
 fs : 9.05

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 51	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 2.11 N/mm ²	Tensione fless. piano XZ	: 1.42 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.106	Coefficiente sfrutt. nel piano XZ	: 0.077
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.106	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.077
fs	: 9.472		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 18-20 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 39 [SLV] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.142)

Sforzo Normale di Progetto [daN] : -579 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 113
 Momento Flettente Mz di Progetto [daNm] : -440

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.07
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.004

fs	: 251.66
Tensione di Progetto relativa a My [N/mm ²]	: 0.17
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.06
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.109
fs	: 9.14
Coefficiente di Sfruttamento a pressoflessione	: 0.109
fs	: 9.14

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.05 (fs=19.825)

Taglio Ty di Progetto [daN]	: -109
Taglio Tz di Progetto [daN]	: -441
Momento Torcente Mt di Progetto [daNm]	: -2

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.08
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.05
fs	: 19.83

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 39	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 2.06 N/mm ²	Tensione fless. piano XZ	: 0.17 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.103	Coefficiente sfrutt. nel piano XZ	: 0.009
Coeff. sfrutt. max euleriano	: 0.004		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.107	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.013
fs	: 9.351		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.297 (fs=3.367)

Sforzo Normale di Progetto [daN] : 616 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : -2877
Momento Flettente Mz di Progetto [daNm] : 360

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.08
Tensione Resistente [N/mm²] : 14.83
Coefficiente di Sfruttamento a trazione : 0.005
fs : 192.63
Tensione di Progetto relativa a My [N/mm²] : 4.32
Tensione di Progetto relativa a Mz [N/mm²] : 1.69
Tensione Resistente relativa a My [N/mm²] : 18.54
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.292
fs : 3.43
Coefficiente di Sfruttamento : 0.297
fs : 3.37

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.314 (fs=3.185)

Taglio Ty di Progetto [daN] : 430
Taglio Tz di Progetto [daN] : 4426
Momento Torcente Mt di Progetto [daNm] : 237

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.08
Tensione di Progetto relativa a Tz [N/mm²] : 0.83
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.314
fs : 3.18

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.66 N/mm ²	Tensione fless. piano XZ	: 4.32 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.083	Coefficiente sfrutt. nel piano XZ	: 0.233
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.083	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.233
fs	: 4.294		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)
· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 20-22 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.113 (fs=8.853)

Sforzo Normale di Progetto [daN]	: -1083 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -484
Momento Flettente Mz di Progetto [daNm]	: 365

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.14
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.007
fs	: 134.52
Tensione di Progetto relativa a My [N/mm ²]	: 0.73
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.71
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.113
fs	: 8.86
Coefficiente di Sfruttamento a pressoflessione	: 0.113
fs	: 8.85

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.07 (fs=14.351)

Taglio Ty di Progetto [daN]	: 387
Taglio Tz di Progetto [daN]	: 908
Momento Torcente Mt di Progetto [daNm]	: 219

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.07
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.17
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.07
fs	: 14.35

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 33

Sezione più sfavorevole : 7

Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.77 N/mm ²	Tensione fless. piano XZ	: 0.40 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.089	Coefficiente sfrutt. nel piano XZ	: 0.021
Coeff. sfrutt. max euleriano	: 0.005		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.094	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.027
fs	: 10.630		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 21-23 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.137 (fs=7.309)

Sforzo Normale di Progetto [daN]	: -726 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -854
Momento Flettente Mz di Progetto [daNm]	: -378

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.09
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 200.71
Tensione di Progetto relativa a My [N/mm ²]	: 1.28
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.77
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.137
fs	: 7.31
Coefficiente di Sfruttamento a pressoflessione	: 0.137
fs	: 7.31

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.048 (fs=20.733)

Taglio Ty di Progetto [daN] : -6
 Taglio Tz di Progetto [daN] : -435
 Momento Torcente Mt di Progetto [daNm] : -4

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
 Tensione di Progetto relativa a Tz [N/mm²] : 0.08
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.048
 fs : 20.73

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm²	Tensione Critica nel piano XZ	: 254.73 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.54 N/mm²
Tensione fless. piano XY	: 1.77 N/mm²	Tensione fless. piano XZ	: 1.28 N/mm²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.088	Coefficiente sfrutt. nel piano XZ	: 0.069
Coeff. sfrutt. max euleriano	: 0.005		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.093	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.074
fs	: 10.702		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 22-24 Primo [Travel]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 34 [SLD] [IN] " - Coeff. Sfruttamento : 0.099 (fs=10.083)

Sforzo Normale di Progetto [daN] : 529 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -140
 Momento Flettente Mz di Progetto [daNm] : -371

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.07
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.004
fs	: 224.47
Tensione di Progetto relativa a My [N/mm ²]	: 0.21
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.74
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.095
fs	: 10.56
Coefficiente di Sfruttamento	: 0.099
fs	: 10.08

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : "Comb 1 [SLV] [LT]" - Coeff. Sfruttamento : 0.05 (fs=20.01)

Taglio Ty di Progetto [daN]	: 6
Taglio Tz di Progetto [daN]	: -450
Momento Torcente Mt di Progetto [daNm]	: 4

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.08
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.05
fs	: 20.01

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 41	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.82 N/mm ²	Tensione fless. piano XZ	: 0.08 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.091	Coefficiente sfrutt. nel piano XZ	: 0.004
Coeff. sfrutt. max euleriano	: 0.003		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.094	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.007
fs	: 10.684		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 23-25 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.327 (fs=3.054)

Sforzo Normale di Progetto [daN]	: 1630 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -2961
Momento Flettente Mz di Progetto [daNm]	: -452

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.2
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.014
fs	: 72.81
Tensione di Progetto relativa a My [N/mm²]	: 4.44
Tensione di Progetto relativa a Mz [N/mm²]	: 2.12
Tensione Resistente relativa a My [N/mm²]	: 18.54
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.314
fs	: 3.19
Coefficiente di Sfruttamento	: 0.327
fs	: 3.05

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.329 (fs=3.043)

Taglio Ty di Progetto [daN]	: 500
Taglio Tz di Progetto [daN]	: -4627
Momento Torcente Mt di Progetto [daNm]	: -452

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.09
Tensione di Progetto relativa a Tz [N/mm²]	: 0.87
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.329
fs	: 3.04

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm²	Tensione Critica nel piano XZ	: 254.73 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.54 N/mm²
Tensione fless. piano XY	: 0.67 N/mm²	Tensione fless. piano XZ	: 4.28 N/mm²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.033	Coefficiente sfrutt. nel piano XZ	: 0.231
Coeff. sfrutt. max euleriano	: 0.011		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.045	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.242
fs	: 4.127		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 24-26 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.127 (fs=7.89)

Sforzo Normale di Progetto [daN]	: -1011 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -528
Momento Flettente Mz di Progetto [daNm]	: -414

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.13
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.007
fs	: 144.13
Tensione di Progetto relativa a My [N/mm ²]	: 0.79
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.94
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.127
fs	: 7.89
Coefficiente di Sfruttamento a pressoflessione	: 0.127
fs	: 7.89

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.077 (fs=12.909)

Taglio Ty di Progetto [daN]	: 464
Taglio Tz di Progetto [daN]	: -994
Momento Torcente Mt di Progetto [daNm]	: -414

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.09
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.19
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.077
fs	: 12.91

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.94 N/mm ²	Tensione fless. piano XZ	: 0.79 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.097	Coefficiente sfrutt. nel piano XZ	: 0.043
Coeff. sfrutt. max euleriano	: 0.007		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.104	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.050
fs	: 9.639		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 25-28 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1700 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1700 mm] - **R 160x500**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.171 (fs=5.84)

Sforzo Normale di Progetto [daN]	: 3984 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 607
Momento Flettente Mz di Progetto [daNm]	: -441

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.5
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.034
fs	: 29.79
Tensione di Progetto relativa a My [N/mm ²]	: 0.91
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.07
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.138
fs	: 7.26
Coefficiente di Sfruttamento	: 0.171
fs	: 5.84

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1700 mm / 1700 mm] - **R 160x500**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.095 (fs=10.519)

Taglio Ty di Progetto [daN] : -164
 Taglio Tz di Progetto [daN] : -1336
 Momento Torcente Mt di Progetto [daNm] : -113

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.25
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.095
 fs : 10.52

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1700.0	Lunghezza efficace nel piano XZ	: 1700.0
Momento Critico nel piano XY	: 412070 daNm	Momento Critico nel piano XZ	: 131862 daNm
Tensione Critica nel piano XY	: 1931.58 N/mmq	Tensione Critica nel piano XZ	: 197.79 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.54 N/mmq
Tensione fless. piano XY	: 2.04 N/mmq	Tensione fless. piano XZ	: 1.23 N/mmq
Snellezza relativa nel piano XY	: 0.11	Snellezza relativa nel piano XZ	: 0.35
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.102	Coefficiente sfrutt. nel piano XZ	: 0.066
Coeff. sfrutt. max euleriano	: 0.025		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.127	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.091
fs	: 7.885		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1700.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.005 mm	Limite Freccia Istantanea L/500	: 3.400 mm
Freccia Netta Finale	: -0.010 mm	Limite Freccia Netta Fin. L/ 350	: 4.857 mm
Freccia Finale	: -0.010 mm	Limite Freccia Finale L/ 300	: 5.667 mm
Fatt. sicurezza freccia Istantanea	: 634.236	Fatt. sicurezza freccia Netta Finale	: 503.362
Fatt. sicurezza freccia Finale	: 587.256	Fatt. sicurezza	: 503.362

Campata 26-27 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 29 [SLD] [IN] " - Coeff. Sfruttamento : 0.115 (fs=8.689)

Sforzo Normale di Progetto [daN] : 507 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -182

Momento Flettente Mz di Progetto [daNm] : 429

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.06
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.004
fs	: 234.02
Tensione di Progetto relativa a My [N/mm ²]	: 0.27
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.01
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.111
fs	: 9.02
Coefficiente di Sfruttamento	: 0.115
fs	: 8.69

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.05 (fs=19.923)

Taglio Ty di Progetto [daN]	: 3
Taglio Tz di Progetto [daN]	: 452
Momento Torcente Mt di Progetto [daNm]	: 4

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.08
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.05
fs	: 19.92

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.99 N/mm ²	Tensione fless. piano XZ	: 0.03 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.099	Coefficiente sfrutt. nel piano XZ	: 0.002
Coeff. sfrutt. max euleriano	: 0.004		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.103	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.005
fs	: 9.697		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/350	: 3.771 mm

Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 27-29 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 22 [SLD] [IN] " - Coeff. Sfruttamento : 0.117 (fs=8.578)

Sforzo Normale di Progetto [daN]	: -508 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -454
Momento Flettente Mz di Progetto [daNm]	: 388

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.003
fs	: 286.69
Tensione di Progetto relativa a My [N/mm ²]	: 0.68
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.82
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.117
fs	: 8.58
Coefficiente di Sfruttamento a pressoflessione	: 0.117
fs	: 8.58

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.069 (fs=14.418)

Taglio Ty di Progetto [daN]	: 341
Taglio Tz di Progetto [daN]	: 921
Momento Torcente Mt di Progetto [daNm]	: 29

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.06
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.17
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.069
fs	: 14.42

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 25	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.82 N/mm ²	Tensione fless. piano XZ	: 0.52 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.091	Coefficiente sfrutt. nel piano XZ	: 0.028
Coeff. sfrutt. max euleriano	: 0.004		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.095	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.032

fs : 10.550

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 28-30 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)
L= 1460 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1460 mm / 1460 mm] - **R 160x500**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.286 (fs=3.502)

Sforzo Normale di Progetto [daN]	: 5571 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -2087
Momento Flettente Mz di Progetto [daNm]	: 426

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.7
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.047
fs	: 21.3
Tensione di Progetto relativa a My [N/mm ²]	: 3.13
Tensione di Progetto relativa a Mz [N/mm ²]	: 2
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.239
fs	: 4.19
Coefficiente di Sfruttamento	: 0.286
fs	: 3.5

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1460 mm] - **R 160x500**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.243 (fs=4.12)

Taglio Ty di Progetto [daN]	: 313
Taglio Tz di Progetto [daN]	: 3423
Momento Torcente Mt di Progetto [daNm]	: -40

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.06
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.64
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.243

fs

: 4.12

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 42	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1460.0	Lunghezza efficace nel piano XZ	: 1460.0
Momento Critico nel piano XY	: 479807 daNm	Momento Critico nel piano XZ	: 153538 daNm
Tensione Critica nel piano XY	: 2249.10 N/mm ²	Tensione Critica nel piano XZ	: 230.31 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 0.52 N/mm ²	Tensione fless. piano XZ	: 4.03 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.32
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.026	Coefficiente sfrutt. nel piano XZ	: 0.217
Coeff. sfrutt. max euleriano	: 0.039		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.064	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.256
fs	: 3.905		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1460.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.003 mm	Limite Freccia Istantanea L/500	: 2.920 mm
Freccia Netta Finale	: -0.005 mm	Limite Freccia Netta Fin. L/ 350	: 4.171 mm
Freccia Finale	: -0.005 mm	Limite Freccia Finale L/ 300	: 4.867 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 794.637
Fatt. sicurezza freccia Finale	: 927.077	Fatt. sicurezza	: 794.637

Campata 29-31 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.111 (fs=9.016)

Sforzo Normale di Progetto [daN]	: 585 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -178
Momento Flettente Mz di Progetto [daNm]	: -410

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.07
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.005
fs	: 202.78
Tensione di Progetto relativa a My [N/mm ²]	: 0.27
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.92
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.106
fs	: 9.44

Coefficiente di Sfruttamento : 0.111
fs : 9.02

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.049 (fs=20.397)
Taglio Ty di Progetto [daN] : 0
Taglio Tz di Progetto [daN] : 442
Momento Torcente Mt di Progetto [daNm] : 1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
Tensione di Progetto relativa a Tz [N/mm²] : 0.08
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a taglio : 0.049
fs : 20.4

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 25	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mmq	Tensione Critica nel piano XZ	: 254.73 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.54 N/mmq
Tensione fless. piano XY	: 1.92 N/mmq	Tensione fless. piano XZ	: 0.06 N/mmq
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.096	Coefficiente sfrutt. nel piano XZ	: 0.004
Coeff. sfrutt. max euleriano	: 0.004		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.100	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.007
fs	: 10.042		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 30-32 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1370 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1370 mm] - **R 160x500**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.23 (fs=4.341)

Sforzo Normale di Progetto [daN] : 4240 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 1529
 Momento Flettente Mz di Progetto [daNm] : 433

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.53
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.036
 fs : 27.99
 Tensione di Progetto relativa a My [N/mm²] : 2.29
 Tensione di Progetto relativa a Mz [N/mm²] : 2.03
 Tensione Resistente relativa a My [N/mm²] : 18.54
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.195
 fs : 5.14
 Coefficiente di Sfruttamento : 0.23
 fs : 4.34

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1370 mm / 1370 mm] - **R 160x500**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.196 (fs=5.1)

Taglio Ty di Progetto [daN] : 424
 Taglio Tz di Progetto [daN] : -2744
 Momento Torcente Mt di Progetto [daNm] : -69

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.08
 Tensione di Progetto relativa a Tz [N/mm²] : 0.51
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.196
 fs : 5.1

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1370.0	Lunghezza efficace nel piano XZ	: 1370.0
Momento Critico nel piano XY	: 511327 daNm	Momento Critico nel piano XZ	: 163625 daNm
Tensione Critica nel piano XY	: 2396.85 N/mm ²	Tensione Critica nel piano XZ	: 245.44 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 0.33 N/mm ²	Tensione fless. piano XZ	: 2.53 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.016	Coefficiente sfrutt. nel piano XZ	: 0.136
Coeff. sfrutt. max euleriano	: 0.030		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.046	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.166
fs	: 6.025		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1370.0 mm
 Comb. di carico più gravosa : 142
 Carico distribuito Istantaneo : -441.6 daN/m
 -
 Freccia Istantanea - COMBINAZIONE
 Freccia Finale - COMBINAZIONE
 Modulo Elastico istantaneo : 11500.0 N/mm²

Schema adottato Doppio Incastro
 Peso proprio : -30.8 daN/m
 -
 Carico distribuito Finale : -441.6 daN/m
 Comb 42 [CAR] [ST]
 Comb 2 [SLEQP] [LT]
 Modulo Elastico finale : 6388.9 N/mm²

Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.740 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.914 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.567 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 961.758
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 961.758

Campata 31-33 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 22 [SLD] [IN] " - Coeff. Sfruttamento : 0.108 (fs=9.302)

Sforzo Normale di Progetto [daN]	: -642 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -458
Momento Flettente Mz di Progetto [daNm]	: -349

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.08
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.004
fs	: 226.74
Tensione di Progetto relativa a My [N/mm²]	: 0.69
Tensione di Progetto relativa a Mz [N/mm²]	: 1.63
Tensione Resistente relativa a My [N/mm²]	: 18.54
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.107
fs	: 9.3
Coefficiente di Sfruttamento a pressoflessione	: 0.108
fs	: 9.3

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.066 (fs=15.09)

Taglio Ty di Progetto [daN]	: -197
Taglio Tz di Progetto [daN]	: 918
Momento Torcente Mt di Progetto [daNm]	: 35

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm²]	: 0.17
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.066
fs	: 15.09

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 41	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm²	Tensione Critica nel piano XZ	: 254.73 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.54 N/mm²
Tensione fless. piano XY	: 1.67 N/mm²	Tensione fless. piano XZ	: 0.52 N/mm²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000

Coefficiente sfrutt. nel piano XY	: 0.083	Coefficiente sfrutt. nel piano XZ	: 0.028
Coeff. sfrutt. max euleriano	: 0.005		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.089	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.033
fs	: 11.296		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 32-34 Primo [Travel]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.232 (fs=4.308)

Sforzo Normale di Progetto [daN]	: 2586 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -1802
Momento Flettente Mz di Progetto [daNm]	: -394

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.32
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.022
fs	: 45.89
Tensione di Progetto relativa a My [N/mm ²]	: 2.7
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.85
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.21
fs	: 4.75
Coefficiente di Sfruttamento	: 0.232
fs	: 4.31

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.204 (fs=4.893)

Taglio Ty di Progetto [daN]	: 67
Taglio Tz di Progetto [daN]	: -2893
Momento Torcente Mt di Progetto [daNm]	: -234

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
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Tensione di Progetto relativa a Tz [N/mm ²]	: 0.54
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.204
fs	: 4.89

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 0.23 N/mm ²	Tensione fless. piano XZ	: 2.76 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.012	Coefficiente sfrutt. nel piano XZ	: 0.149
Coeff. sfrutt. max euleriano	: 0.021		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.032	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.170
fs	: 5.886		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.002
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.002

Campata 33-35 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.106 (fs=9.466)

Sforzo Normale di Progetto [daN]	: 849 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -193
Momento Flettente Mz di Progetto [daNm]	: 374

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.11
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.007
fs	: 139.75
Tensione di Progetto relativa a My [N/mm ²]	: 0.29
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.75
Tensione Resistente relativa a My [N/mm ²]	: 18.54

Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.098
f_s	: 10.15
Coefficiente di Sfruttamento	: 0.106
f_s	: 9.47

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.051 ($f_s=19.602$)

Taglio T_y di Progetto [daN]	: 0
Taglio T_z di Progetto [daN]	: 460
Momento Torcente M_t di Progetto [daNm]	: 2

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.09
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.051
f_s	: 19.6

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 41	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.78 N/mm ²	Tensione fless. piano XZ	: 0.06 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.089	Coefficiente sfrutt. nel piano XZ	: 0.003
Coeff. sfrutt. max euleriano	: 0.005		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.093	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.008
f_s	: 10.703		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale ($t > \text{inf.}$)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 34-36 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 160x500**
 Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.213 (fs=4.695)
 Sforzo Normale di Progetto [daN] : 1602 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -1855
 Momento Flettente Mz di Progetto [daNm] : 301

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.2
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.014
 fs : 74.07
 Tensione di Progetto relativa a My [N/mm²] : 2.78
 Tensione di Progetto relativa a Mz [N/mm²] : 1.41
 Tensione Resistente relativa a My [N/mm²] : 18.54
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.199
 fs : 5.01
 Coefficiente di Sfruttamento : 0.213
 fs : 4.7

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 160x500**
 Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.207 (fs=4.829)
 Taglio Ty di Progetto [daN] : -456
 Taglio Tz di Progetto [daN] : -2897
 Momento Torcente Mt di Progetto [daNm] : 301

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.09
 Tensione di Progetto relativa a Tz [N/mm²] : 0.54
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.207
 fs : 4.83

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.15 N/mm ²	Tensione fless. piano XZ	: 2.75 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.057	Coefficiente sfrutt. nel piano XZ	: 0.149
Coeff. sfrutt. max euleriano	: 0.012		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.069	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.161
fs	: 6.228		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m

Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 35-37 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 29 [SLD] [IN] " - Coeff. Sfruttamento : 0.103 (fs=9.756)

Sforzo Normale di Progetto [daN]	: 922 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -427
Momento Flettente Mz di Progetto [daNm]	: -301

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.12
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.008
fs	: 128.73
Tensione di Progetto relativa a My [N/mm ²]	: 0.64
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.41
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.095
fs	: 10.56
Coefficiente di Sfruttamento	: 0.103
fs	: 9.76

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.069 (fs=14.421)

Taglio Ty di Progetto [daN]	: -119
Taglio Tz di Progetto [daN]	: -975
Momento Torcente Mt di Progetto [daNm]	: 295

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.18
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.069
fs	: 14.42

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 49	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²

Tensione fless. piano XY	: 1.40 N/mm ²	Tensione fless. piano XZ	: 0.09 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.070	Coefficiente sfrutt. nel piano XZ	: 0.005
Coeff. sfrutt. max euleriano	: 0.009		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.079	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.014
fs	: 12.595		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 36-38 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.196 (fs=5.095)

Sforzo Normale di Progetto [daN]	: -530 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -1830
Momento Flettente Mz di Progetto [daNm]	: -294

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.07
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.004
fs	: 274.64
Tensione di Progetto relativa a My [N/mm ²]	: 2.75
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.38
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.196
fs	: 5.09
Coefficiente di Sfruttamento a pressoflessione	: 0.196
fs	: 5.09

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.205 (fs=4.867)

Taglio Ty di Progetto [daN]	: 46
Taglio Tz di Progetto [daN]	: -2909
Momento Torcente Mt di Progetto [daNm]	: 146

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.01
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.55
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.205
f_s	: 4.87

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.36 N/mm ²	Tensione fless. piano XZ	: 2.75 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.068	Coefficiente sfrutt. nel piano XZ	: 0.149
Coeff. sfrutt. max euleriano	: 0.003		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.071	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.152
f_s	: 6.579		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 37-39 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.104 ($f_s=9.633$)

Sforzo Normale di Progetto [daN]	: 1269 (TRAZIONE)
Momento Flettente M_y di Progetto [daNm]	: 62
Momento Flettente M_z di Progetto [daNm]	: 383

Tipo Verifica : TRAZIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: 0.16
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.011
f_s	: 93.52

Tensione di Progetto relativa a M_y [N/mm ²]	: 0.09
Tensione di Progetto relativa a M_z [N/mm ²]	: 1.79
Tensione Resistente relativa a M_y [N/mm ²]	: 18.54
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.093
f_s	: 10.74
Coefficiente di Sfruttamento	: 0.104
f_s	: 9.63

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.049 ($f_s=20.45$)

Taglio T_y di Progetto [daN]	: 0
Taglio T_z di Progetto [daN]	: 441
Momento Torcente M_t di Progetto [daNm]	: 2

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.08
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.049
f_s	: 20.45

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 49	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.78 N/mm ²	Tensione fless. piano XZ	: 0.25 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.089	Coefficiente sfrutt. nel piano XZ	: 0.013
Coeff. sfrutt. max euleriano	: 0.009		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.098	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.022
f_s	: 10.193		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale ($t > \inf$)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 38-40 Primo [Travel]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

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L= 1370 mm - **R 160x500** - SEZIONI UTILIZZATE : 7
VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1370 mm / 1370 mm] - **R 160x500**
Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.199 (fs=5.028)

Sforzo Normale di Progetto [daN]	: -1649 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -1687
Momento Flettente Mz di Progetto [daNm]	: -380

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.21
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.011
fs	: 88.33
Tensione di Progetto relativa a My [N/mm ²]	: 2.53
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.78
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.199
fs	: 5.03
Coefficiente di Sfruttamento a pressoflessione	: 0.199
fs	: 5.03

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1370 mm / 1370 mm] - **R 160x500**
Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.194 (fs=5.155)

Taglio Ty di Progetto [daN]	: 480
Taglio Tz di Progetto [daN]	: -2705
Momento Torcente Mt di Progetto [daNm]	: -265

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.09
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.51
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.194
fs	: 5.15

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1370.0	Lunghezza efficace nel piano XZ	: 1370.0
Momento Critico nel piano XY	: 511327 daNm	Momento Critico nel piano XZ	: 163625 daNm
Tensione Critica nel piano XY	: 2396.85 N/mm ²	Tensione Critica nel piano XZ	: 245.44 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 0.75 N/mm ²	Tensione fless. piano XZ	: 2.57 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.037	Coefficiente sfrutt. nel piano XZ	: 0.139
Coeff. sfrutt. max euleriano	: 0.011		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.049	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.150
fs	: 6.665		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1370.0 mm

Schema adottato Doppio Incastro

Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.740 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.914 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.567 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 961.758
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 961.758

Campata 39-41 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 29 [SLD] [IN] " - Coeff. Sfruttamento : 0.113 (fs=8.88)

Sforzo Normale di Progetto [daN]	: 1078 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -396
Momento Flettente Mz di Progetto [daNm]	: 346

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.13
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.009
fs	: 110.07
Tensione di Progetto relativa a My [N/mm ²]	: 0.59
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.62
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.104
fs	: 9.66
Coefficiente di Sfruttamento	: 0.113
fs	: 8.88

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.054 (fs=18.391)

Taglio Ty di Progetto [daN]	: 1
Taglio Tz di Progetto [daN]	: 490
Momento Torcente Mt di Progetto [daNm]	: -1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.09
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.054
fs	: 18.39

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 49	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0

Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.64 N/mm ²	Tensione fless. piano XZ	: 0.06 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.082	Coefficiente sfrutt. nel piano XZ	: 0.003
Coeff. sfrutt. max euleriano	: 0.011		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.093	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.014
fs	: 10.764		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 40-42 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.248 (fs=4.035)

Sforzo Normale di Progetto [daN]	: 2740 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -2025
Momento Flettente Mz di Progetto [daNm]	: 372

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.34
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.023
fs	: 43.31
Tensione di Progetto relativa a My [N/mm ²]	: 3.04
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.74
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.225
fs	: 4.45
Coefficiente di Sfruttamento	: 0.248
fs	: 4.03

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.235 (fs=4.247)

TABULATI DI CALCOLO -

Taglio Ty di Progetto [daN]	: -96
Taglio Tz di Progetto [daN]	: 3333
Momento Torcente Mt di Progetto [daNm]	: 372

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.62
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.235
fs	: 4.25

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 0.17 N/mm ²	Tensione fless. piano XZ	: 3.38 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.008	Coefficiente sfrutt. nel piano XZ	: 0.182
Coeff. sfrutt. max euleriano	: 0.021		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.029	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.203
fs	: 4.929		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 41-44 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.075 (fs=13.41)

Sforzo Normale di Progetto [daN]	: -661 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -520
Momento Flettente Mz di Progetto [daNm]	: 193

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.08
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Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 220.36
Tensione di Progetto relativa a My [N/mm ²]	: 0.78
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.9
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.075
fs	: 13.41
Coefficiente di Sfruttamento a pressoflessione	: 0.075
fs	: 13.41

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.061 (fs=16.326)

Taglio Ty di Progetto [daN]	: -309
Taglio Tz di Progetto [daN]	: -810
Momento Torcente Mt di Progetto [daNm]	: 82

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.06
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.15
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.061
fs	: 16.33

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 18	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.22 N/mm ²	Tensione fless. piano XZ	: 0.24 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.061	Coefficiente sfrutt. nel piano XZ	: 0.013
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.062	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.014
fs	: 16.017		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 42-43 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 460 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=460 mm / 460 mm] - **R 160x500**

Comb. più gravosa : " Comb 34 [SLD] [IN] " - Coeff. Sfruttamento : 0.228 (fs=4.394)

Sforzo Normale di Progetto [daN]	: 3523 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 2032
Momento Flettente Mz di Progetto [daNm]	: -204

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.44
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.03
fs	: 33.68
Tensione di Progetto relativa a My [N/mm²]	: 3.05
Tensione di Progetto relativa a Mz [N/mm²]	: 0.96
Tensione Resistente relativa a My [N/mm²]	: 18.54
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.198
fs	: 5.05
Coefficiente di Sfruttamento	: 0.228
fs	: 4.39

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=460 mm / 460 mm] - **R 160x500**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.317 (fs=3.158)

Taglio Ty di Progetto [daN]	: -453
Taglio Tz di Progetto [daN]	: -7860
Momento Torcente Mt di Progetto [daNm]	: 100

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²]	: 0.08
Tensione di Progetto relativa a Tz [N/mm²]	: 1.47
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.556
fs	: 1.8
Tensione di Progetto [N/mm²]	: 0.03
Modulo di resistenza a torsione [mm³]	: 3579418.25
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.008
fs	: 132.79
Coefficiente di Sfruttamento a taglio+torsione	: 0.317
fs	: 3.16

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 460.0	Lunghezza efficace nel piano XZ	: 460.0
Momento Critico nel piano XY	: 1522866 daNm	Momento Critico nel piano XZ	: 487317 daNm
Tensione Critica nel piano XY	: 7138.43 N/mmq	Tensione Critica nel piano XZ	: 730.98 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.54 N/mmq
Tensione fless. piano XY	: 0.47 N/mmq	Tensione fless. piano XZ	: 3.36 N/mmq
Snellezza relativa nel piano XY	: 0.06	Snellezza relativa nel piano XZ	: 0.18
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000

TABULATI DI CALCOLO -

Coefficiente sfrutt. nel piano XY	: 0.023	Coefficiente sfrutt. nel piano XZ	: 0.181
Coeff. sfrutt. max euleriano	: 0.030		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.053	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.211
fs	: 4.734		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 460.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 0.920 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 1.314 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 1.533 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 43-45 Primo [Travel]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.174 (fs=5.756)

Sforzo Normale di Progetto [daN]	: 3208 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -1422
Momento Flettente Mz di Progetto [daNm]	: 193

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.4
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.027
fs	: 36.99
Tensione di Progetto relativa a My [N/mm ²]	: 2.13
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.9
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.147
fs	: 6.82
Coefficiente di Sfruttamento	: 0.174
fs	: 5.76

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 43 [SLV] [IN] " - Coeff. Sfruttamento : 0.139 (fs=7.191)

Taglio Ty di Progetto [daN]	: 7
Taglio Tz di Progetto [daN]	: 1969
Momento Torcente Mt di Progetto [daNm]	: 170

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.00
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Tensione di Progetto relativa a T_z [N/mm ²]	: 0.37
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.139
f_s	: 7.19

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 0.90 N/mm ²	Tensione fless. piano XZ	: 1.91 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.045	Coefficiente sfrutt. nel piano XZ	: 0.103
Coeff. sfrutt. max euleriano	: 0.022		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.067	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.125
f_s	: 7.981		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 44-46 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 22 [SLD] [IN] " - Coeff. Sfruttamento : 0.095 ($f_s=10.503$)

Sforzo Normale di Progetto [daN]	: -343 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: -127
Momento Flettente M_z di Progetto [daNm]	: 376

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: -0.04
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.002
f_s	: 425.13
Tensione di Progetto relativa a M_y [N/mm ²]	: 0.19
Tensione di Progetto relativa a M_z [N/mm ²]	: 1.76
Tensione Resistente relativa a M_y [N/mm ²]	: 18.54

Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.095
f_s	: 10.5
Coefficiente di Sfruttamento a pressoflessione	: 0.095
f_s	: 10.5

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.053 ($f_s=18.89$)

Taglio T_y di Progetto [daN]	: 3
Taglio T_z di Progetto [daN]	: 477
Momento Torcente M_t di Progetto [daNm]	: 5

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.09
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.053
f_s	: 18.89

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 22	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.76 N/mm ²	Tensione fless. piano XZ	: 0.19 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.088	Coefficiente sfrutt. nel piano XZ	: 0.010
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.090	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.013
f_s	: 11.065		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 45-47 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 34 [SLD] [IN] " - Coeff. Sfruttamento : 0.288 (fs=3.477)

Sforzo Normale di Progetto [daN] : 1719 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -2622
 Momento Flettente Mz di Progetto [daNm] : -373

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.21
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.014
 fs : 69.02
 Tensione di Progetto relativa a My [N/mm²] : 3.93
 Tensione di Progetto relativa a Mz [N/mm²] : 1.75
 Tensione Resistente relativa a My [N/mm²] : 18.54
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.273
 fs : 3.66
 Coefficiente di Sfruttamento : 0.288
 fs : 3.48

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.313 (fs=3.192)

Taglio Ty di Progetto [daN] : 305
 Taglio Tz di Progetto [daN] : -4426
 Momento Torcente Mt di Progetto [daNm] : -153

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.06
 Tensione di Progetto relativa a Tz [N/mm²] : 0.83
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.313
 fs : 3.19

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 0.72 N/mm ²	Tensione fless. piano XZ	: 4.29 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.036	Coefficiente sfrutt. nel piano XZ	: 0.231
Coeff. sfrutt. max euleriano	: 0.017		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.053	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.248
fs	: 4.026		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m

Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 46-48 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.131 (fs=7.639)

Sforzo Normale di Progetto [daN]	: 569 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -532
Momento Flettente Mz di Progetto [daNm]	: -410

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.07
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.005
fs	: 208.41
Tensione di Progetto relativa a My [N/mm ²]	: 0.8
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.92
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.126
fs	: 7.93
Coefficiente di Sfruttamento	: 0.131
fs	: 7.64

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.075 (fs=13.34)

Taglio Ty di Progetto [daN]	: 315
Taglio Tz di Progetto [daN]	: -1014
Momento Torcente Mt di Progetto [daNm]	: -288

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.06
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.19
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.075
fs	: 13.34

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 22	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²

Tensione fless. piano XY	: 1.91 N/mm ²	Tensione fless. piano XZ	: 0.57 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.095	Coefficiente sfrutt. nel piano XZ	: 0.031
Coeff. sfrutt. max euleriano	: 0.004		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.099	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.034
fs	: 10.120		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 47-49 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 34 [SLD] [IN] " - Coeff. Sfruttamento : 0.121 (fs=8.238)

Sforzo Normale di Progetto [daN]	: 1078 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 716
Momento Flettente Mz di Progetto [daNm]	: 307

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.13
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.009
fs	: 110.07
Tensione di Progetto relativa a My [N/mm ²]	: 1.07
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.44
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.112
fs	: 8.9
Coefficiente di Sfruttamento	: 0.121
fs	: 8.24

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 43 [SLV] [IN] " - Coeff. Sfruttamento : 0.101 (fs=9.925)

Taglio Ty di Progetto [daN]	: -7
Taglio Tz di Progetto [daN]	: 1427
Momento Torcente Mt di Progetto [daNm]	: 142

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.00
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.27
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.101
fs	: 9.92

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 25	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.52 N/mm ²	Tensione fless. piano XZ	: 1.21 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.076	Coefficiente sfrutt. nel piano XZ	: 0.065
Coeff. sfrutt. max euleriano	: 0.007		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.083	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.072
fs	: 12.095		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 48-50 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.084 (fs=11.965)

Sforzo Normale di Progetto [daN]	: 1042 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -102
Momento Flettente Mz di Progetto [daNm]	: 295

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.13
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.009
fs	: 113.85

Tensione di Progetto relativa a M_y [N/mm ²]	: 0.15
Tensione di Progetto relativa a M_z [N/mm ²]	: 1.38
Tensione Resistente relativa a M_y [N/mm ²]	: 18.54
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.075
f_s	: 13.37
Coefficiente di Sfruttamento	: 0.084
f_s	: 11.96

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.05 ($f_s=19.914$)

Taglio T_y di Progetto [daN]	: -6
Taglio T_z di Progetto [daN]	: -452
Momento Torcente M_t di Progetto [daNm]	: 13

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.00
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.08
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.05
f_s	: 19.91

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 50	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.48 N/mm ²	Tensione fless. piano XZ	: 0.04 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.074	Coefficiente sfrutt. nel piano XZ	: 0.002
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.074	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.002
f_s	: 13.574		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale ($t > \inf$)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 49-51 Primo [Travel]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7
VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 160x500**
Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.285 (fs=3.509)

Sforzo Normale di Progetto [daN]	: -10 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -2839
Momento Flettente Mz di Progetto [daNm]	: 338

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.00
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 4.26
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.58
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.285
fs	: 3.51
Coefficiente di Sfruttamento a pressoflessione	: 0.285
fs	: 3.51

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 160x500**
Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.324 (fs=3.082)

Taglio Ty di Progetto [daN]	: -328
Taglio Tz di Progetto [daN]	: -4583
Momento Torcente Mt di Progetto [daNm]	: 214

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.06
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.86
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.324
fs	: 3.08

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 33 Lunghezza efficace nel piano XY : 1320.0 Momento Critico nel piano XY : 530696 daNm Tensione Critica nel piano XY : 2487.64 N/mm ² Resistenza fless. piano XY : 20.03 N/mm ² Tensione fless. piano XY : 1.00 N/mm ² Snellezza relativa nel piano XY : 0.10 Coeff. Riduttivo nel piano XY : 1.000 Coefficiente sfrutt. nel piano XY : 0.050 Coeff. sfrutt. max euleriano : 0.000 Coeff. sfrutt. TOTALE (Piano XY) : 0.050 fs : 4.221	Sezione più sfavorevole : 7 Lunghezza efficace nel piano XZ : 1320.0 Momento Critico nel piano XZ : 169823 daNm Tensione Critica nel piano XZ : 254.73 N/mm ² Resistenza fless. piano XZ : 18.54 N/mm ² Tensione fless. piano XZ : 4.39 N/mm ² Snellezza relativa nel piano XZ : 0.31 Coeff. Riduttivo nel piano XZ : 1.000 Coefficiente sfrutt. nel piano XZ : 0.237 Coeff. sfrutt. TOTALE (Piano XZ) : 0.237
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VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1320.0 mm

Schema adottato Doppio Incastro

Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 50-52 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 22 [SLD] [IN] " - Coeff. Sfruttamento : 0.108 (fs=9.29)

Sforzo Normale di Progetto [daN] : 1068 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : -340

Momento Flettente Mz di Progetto [daNm] : 339

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.13

Tensione Resistente [N/mm²] : 14.83

Coefficiente di Sfruttamento a trazione : 0.009

fs : 111.1

Tensione di Progetto relativa a My [N/mm²] : 0.51

Tensione di Progetto relativa a Mz [N/mm²] : 1.59

Tensione Resistente relativa a My [N/mm²] : 18.54

Tensione Resistente relativa a Mz [N/mm²] : 20.03

Coefficiente di Sfruttamento a flessione : 0.099

fs : 10.14

Coefficiente di Sfruttamento : 0.108

fs : 9.29

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.062 (fs=16.075)

Taglio Ty di Progetto [daN] : -306

Taglio Tz di Progetto [daN] : -826

Momento Torcente Mt di Progetto [daNm] : 193

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.06

Tensione di Progetto relativa a Tz [N/mm²] : 0.15

Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a taglio : 0.062

fs : 16.08

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 37

Lunghezza efficace nel piano XY : 1320.0

Sezione più sfavorevole : 7

Lunghezza efficace nel piano XZ : 1320.0

Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.63 N/mm ²	Tensione fless. piano XZ	: 0.41 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.082	Coefficiente sfrutt. nel piano XZ	: 0.022
Coeff. sfrutt. max euleriano	: 0.007		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.089	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.029
fs	: 11.296		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto			
Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 51-53 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.157 (fs=6.365)

Sforzo Normale di Progetto [daN]	: 869 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -941
Momento Flettente Mz di Progetto [daNm]	: 412

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.11
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.007
fs	: 136.51
Tensione di Progetto relativa a My [N/mm ²]	: 1.41
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.93
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.15
fs	: 6.68
Coefficiente di Sfruttamento	: 0.157
fs	: 6.36

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.107 (fs=9.323)

TABULATI DI CALCOLO -

Taglio Ty di Progetto [daN]	: -57
Taglio Tz di Progetto [daN]	: 1518
Momento Torcente Mt di Progetto [daNm]	: -190

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.28
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.107
fs	: 9.32

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.93 N/mm ²	Tensione fless. piano XZ	: 1.41 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.097	Coefficiente sfrutt. nel piano XZ	: 0.076
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.097	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.076
fs	: 10.361		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 52-54 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.091 (fs=11.038)

Sforzo Normale di Progetto [daN]	: 606 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -215
Momento Flettente Mz di Progetto [daNm]	: -313

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.08
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Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.005
fs	: 195.94
Tensione di Progetto relativa a My [N/mm ²]	: 0.32
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.47
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.085
fs	: 11.7
Coefficiente di Sfruttamento	: 0.091
fs	: 11.04

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.052 (fs=19.15)

Taglio Ty di Progetto [daN]	: 101
Taglio Tz di Progetto [daN]	: -460
Momento Torcente Mt di Progetto [daNm]	: -138

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.09
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.052
fs	: 19.15

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 45	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 1.65 N/mm ²	Tensione fless. piano XZ	: 0.11 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.083	Coefficiente sfrutt. nel piano XZ	: 0.006
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.083	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.006
fs	: 12.106		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 53-55 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.284 (fs=3.523)

Sforzo Normale di Progetto [daN]	: 1811 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 2436
Momento Flettente Mz di Progetto [daNm]	: 436

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.23
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.015
fs	: 65.52
Tensione di Progetto relativa a My [N/mm²]	: 3.65
Tensione di Progetto relativa a Mz [N/mm²]	: 2.05
Tensione Resistente relativa a My [N/mm²]	: 18.54
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.269
fs	: 3.72
Coefficiente di Sfruttamento	: 0.284
fs	: 3.52

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.246 (fs=4.058)

Taglio Ty di Progetto [daN]	: 377
Taglio Tz di Progetto [daN]	: -3469
Momento Torcente Mt di Progetto [daNm]	: -161

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.07
Tensione di Progetto relativa a Tz [N/mm²]	: 0.65
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.246
fs	: 4.06

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm²	Tensione Critica nel piano XZ	: 254.73 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.54 N/mm²
Tensione fless. piano XY	: 0.96 N/mm²	Tensione fless. piano XZ	: 3.84 N/mm²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.048	Coefficiente sfrutt. nel piano XZ	: 0.207
Coeff. sfrutt. max euleriano	: 0.012		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.059	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.219
fs	: 4.572		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 54-56 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 39 [SLV] [IN] " - Coeff. Sfruttamento : 0.202 (fs=4.959)

Sforzo Normale di Progetto [daN]	: -373 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -389
Momento Flettente Mz di Progetto [daNm]	: -768

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.05
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.003
fs	: 390.78
Tensione di Progetto relativa a My [N/mm ²]	: 0.58
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.6
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.202
fs	: 4.96
Coefficiente di Sfruttamento a pressoflessione	: 0.202
fs	: 4.96

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 160x500**

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.064 (fs=15.697)

Taglio Ty di Progetto [daN]	: 629
Taglio Tz di Progetto [daN]	: -646
Momento Torcente Mt di Progetto [daNm]	: -695

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.12
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.12
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.064
fs	: 15.7

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 39	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 530696 daNm	Momento Critico nel piano XZ	: 169823 daNm
Tensione Critica nel piano XY	: 2487.64 N/mm ²	Tensione Critica nel piano XZ	: 254.73 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 3.60 N/mm ²	Tensione fless. piano XZ	: 0.58 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.180	Coefficiente sfrutt. nel piano XZ	: 0.031
Coeff. sfrutt. max euleriano	: 0.003		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.182	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.034
fs	: 5.488		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 55-57 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1590 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1590 mm / 1590 mm] - **R 160x500**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.845 (fs=1.184)

Sforzo Normale di Progetto [daN]	: 2681 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -6897
Momento Flettente Mz di Progetto [daNm]	: -1611

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.34
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.023
fs	: 44.25
Tensione di Progetto relativa a My [N/mm ²]	: 10.35
Tensione di Progetto relativa a Mz [N/mm ²]	: 7.55
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.822
fs	: 1.22
Coefficiente di Sfruttamento	: 0.845
fs	: 1.18

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1590 mm / 1590 mm] - **R 160x500**
 Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.203 (fs=4.92)
 Taglio Ty di Progetto [daN] : 916
 Taglio Tz di Progetto [daN] : -5990
 Momento Torcente Mt di Progetto [daNm] : -1415

Tipo Verifica : TAGLIO+TORSIONE
 Tensione di Progetto relativa a Ty [N/mm²] : 0.17
 Tensione di Progetto relativa a Tz [N/mm²] : 1.12
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.428
 fs : 2.34
 Tensione di Progetto [N/mm²] : 0.08
 Modulo di resistenza a torsione [mm³] : 3579418.25
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.02
 fs : 49.68
 Coefficiente di Sfruttamento a taglio+torsione : 0.203
 fs : 4.92

VERIFICA A SVERGOLAMENTO
 Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 26	Sezione più sfavorevole : 7
Lunghezza efficace nel piano XY : 1590.0	Lunghezza efficace nel piano XZ : 1590.0
Momento Critico nel piano XY : 440578 daNm	Momento Critico nel piano XZ : 140985 daNm
Tensione Critica nel piano XY : 2065.21 N/mmq	Tensione Critica nel piano XZ : 211.48 N/mmq
Resistenza fless. piano XY : 20.03 N/mmq	Resistenza fless. piano XZ : 18.54 N/mmq
Tensione fless. piano XY : 3.48 N/mmq	Tensione fless. piano XZ : 10.55 N/mmq
Snellezza relativa nel piano XY : 0.11	Snellezza relativa nel piano XZ : 0.34
Coeff. Riduttivo nel piano XY : 1.000	Coeff. Riduttivo nel piano XZ : 1.000
Coefficiente sfrutt. nel piano XY : 0.174	Coefficiente sfrutt. nel piano XZ : 0.569
Coeff. sfrutt. max euleriano : 0.015	
Coeff. sfrutt. TOTALE (Piano XY) : 0.189	Coeff. sfrutt. TOTALE (Piano XZ) : 0.584
fs : 1.713	

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto	
Lunghezza elemento : 1590.0 mm	Schema adottato Doppio Incastro
Comb. di carico più gravosa : 142	Peso proprio : -30.8 daN/m
Carico distribuito Istantaneo : -441.6 daN/m	-
-	Carico distribuito Finale : -441.6 daN/m
Freccia Istantanea - COMBINAZIONE	Comb 42 [CAR] [ST]
Freccia Finale - COMBINAZIONE	Comb 2 [SLEQP] [LT]
Modulo Elastico istantaneo : 11500.0 N/mmq	Modulo Elastico finale : 6388.9 N/mmq
Controfreccia : 0.000 mm	
Freccia Istantanea : -0.004 mm	Limite Freccia Istantanea L/500 : 3.180 mm
Freccia Netta Finale : -0.007 mm	Limite Freccia Netta Fin. L/ 350 : 4.543 mm
Freccia Finale : -0.007 mm	Limite Freccia Finale L/ 300 : 5.300 mm
Fatt. sicurezza freccia Istantanea : 775.261	Fatt. sicurezza freccia Netta Finale : 615.286
Fatt. sicurezza freccia Finale : 717.834	Fatt. sicurezza : 615.286

Campata 56-70 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1590 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1590 mm / 1590 mm] - **R 160x500**
Comb. più gravosa : " Comb 39 [SLV] [IN] " - Coeff. Sfruttamento : 0.201 (fs=4.968)
 Sforzo Normale di Progetto [daN] : -220 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -714
 Momento Flettente Mz di Progetto [daNm] : 687

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.03
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.002
 fs : 660.79
 Tensione di Progetto relativa a My [N/mm²] : 1.07
 Tensione di Progetto relativa a Mz [N/mm²] : 3.22
 Tensione Resistente relativa a My [N/mm²] : 18.54
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.201
 fs : 4.97
 Coefficiente di Sfruttamento a pressoflessione : 0.201
 fs : 4.97

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1590 mm / 1590 mm] - **R 160x500**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.081 (fs=12.308)
 Taglio Ty di Progetto [daN] : -561
 Taglio Tz di Progetto [daN] : -1004
 Momento Torcente Mt di Progetto [daNm] : 536

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.11
 Tensione di Progetto relativa a Tz [N/mm²] : 0.19
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.081
 fs : 12.31

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 39	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1590.0	Lunghezza efficace nel piano XZ	: 1590.0
Momento Critico nel piano XY	: 440578 daNm	Momento Critico nel piano XZ	: 140985 daNm
Tensione Critica nel piano XY	: 2065.21 N/mm ²	Tensione Critica nel piano XZ	: 211.48 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 3.42 N/mm ²	Tensione fless. piano XZ	: 0.20 N/mm ²
Snellezza relativa nel piano XY	: 0.11	Snellezza relativa nel piano XZ	: 0.34
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.171	Coefficiente sfrutt. nel piano XZ	: 0.011
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.172	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.012
fs	: 5.803		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1590.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m

Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.004 mm	Limite Freccia Istantanea L/500	: 3.180 mm
Freccia Netta Finale	: -0.007 mm	Limite Freccia Netta Fin. L/ 350	: 4.543 mm
Freccia Finale	: -0.007 mm	Limite Freccia Finale L/ 300	: 5.300 mm
Fatt. sicurezza freccia Istantanea	: 775.261	Fatt. sicurezza freccia Netta Finale	: 615.286
Fatt. sicurezza freccia Finale	: 717.834	Fatt. sicurezza	: 615.286

Campata 57-58 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1662.44 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1662.44 mm] - **R 160x500**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.426 (fs=2.347)

Sforzo Normale di Progetto [daN]	: 1838 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 608
Momento Flettente Mz di Progetto [daNm]	: -1607

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.23
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.015
fs	: 64.57
Tensione di Progetto relativa a My [N/mm ²]	: 0.91
Tensione di Progetto relativa a Mz [N/mm ²]	: 7.53
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.411
fs	: 2.44
Coefficiente di Sfruttamento	: 0.426
fs	: 2.35

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1662.44 mm / 1662.44 mm] - **R 160x500**

Comb. più gravosa : " Comb 25 [SLD] [IN] " - Coeff. Sfruttamento : 0.098 (fs=10.243)

Taglio Ty di Progetto [daN]	: -1466
Taglio Tz di Progetto [daN]	: -1142
Momento Torcente Mt di Progetto [daNm]	: 1115

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.27
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.21
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.131
fs	: 7.62
Tensione di Progetto [N/mm ²]	: 0.31
Modulo di resistenza a torsione [mm ³]	: 3579418.25
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.08
fs	: 12.44
Coefficiente di Sfruttamento a taglio+torsione	: 0.098
fs	: 10.24

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1662.4	Lunghezza efficace nel piano XZ	: 1662.4
Momento Critico nel piano XY	: 421380 daNm	Momento Critico nel piano XZ	: 134842 daNm
Tensione Critica nel piano XY	: 1975.22 N/mm ²	Tensione Critica nel piano XZ	: 202.26 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 7.53 N/mm ²	Tensione fless. piano XZ	: 0.91 N/mm ²
Snellezza relativa nel piano XY	: 0.11	Snellezza relativa nel piano XZ	: 0.34
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.376	Coefficiente sfrutt. nel piano XZ	: 0.049
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.376	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.049
fs	: 2.658		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1662.4 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.0 daN/m	-	
-		Carico distribuito Finale	: -441.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.005 mm	Limite Freccia Istantanea L/500	: 3.325 mm
Freccia Netta Finale	: -0.009 mm	Limite Freccia Netta Fin. L/ 350	: 4.750 mm
Freccia Finale	: -0.009 mm	Limite Freccia Finale L/ 300	: 5.541 mm
Fatt. sicurezza freccia Istantanea	: 679.066	Fatt. sicurezza freccia Netta Finale	: 538.941
Fatt. sicurezza freccia Finale	: 628.765	Fatt. sicurezza	: 538.941

Campata 58-59 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 25 [SLD] [IN] " - Coeff. Sfruttamento : 0.266 (fs=3.757)

Sforzo Normale di Progetto [daN]	: 1338 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -129
Momento Flettente Mz di Progetto [daNm]	: 1058

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.17
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.011
fs	: 88.7
Tensione di Progetto relativa a My [N/mm ²]	: 0.19
Tensione di Progetto relativa a Mz [N/mm ²]	: 4.96
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.255
fs	: 3.92
Coefficiente di Sfruttamento	: 0.266
fs	: 3.76

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.073 (fs=13.645)

Taglio Ty di Progetto [daN] : -973
 Taglio Tz di Progetto [daN] : 361
 Momento Torcente Mt di Progetto [daNm] : -1107

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
 Tensione di Progetto relativa a Tz [N/mm²] : 0.07
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.073
 fs : 13.65

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato 1 (0 - 6)

Combinazione più sfavorevole	: 50	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mmq	Tensione Critica nel piano XZ	: 243.66 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.54 N/mmq
Tensione fless. piano XY	: 5.19 N/mmq	Tensione fless. piano XZ	: 0.13 N/mmq
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.259	Coefficiente sfrutt. nel piano XZ	: 0.007
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.261	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.008
fs	: 3.836		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 59-60 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.21 (fs=4.77)

Sforzo Normale di Progetto [daN] : 1835 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -165

Momento Flettente Mz di Progetto [daNm] : 790

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.23
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.015
fs	: 64.67
Tensione di Progetto relativa a My [N/mm ²]	: 0.25
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.7
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.194
fs	: 5.15
Coefficiente di Sfruttamento	: 0.21
fs	: 4.77

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.054 (fs=18.536)

Taglio Ty di Progetto [daN]	: 6
Taglio Tz di Progetto [daN]	: 486
Momento Torcente Mt di Progetto [daNm]	: 28

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.09
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.054
fs	: 18.54

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 3.70 N/mm ²	Tensione fless. piano XZ	: 0.25 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.185	Coefficiente sfrutt. nel piano XZ	: 0.013
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.185	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.013
fs	: 5.411		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/350	: 3.943 mm

Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 60-61 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.193 (fs=5.188)

Sforzo Normale di Progetto [daN]	: 273 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -482
Momento Flettente Mz di Progetto [daNm]	: 697

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.03
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 435.07
Tensione di Progetto relativa a My [N/mm ²]	: 0.72
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.27
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.19
fs	: 5.25
Coefficiente di Sfruttamento	: 0.193
fs	: 5.19

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.059 (fs=16.949)

Taglio Ty di Progetto [daN]	: -368
Taglio Tz di Progetto [daN]	: -750
Momento Torcente Mt di Progetto [daNm]	: 373

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.07
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.14
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.059
fs	: 16.95

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 3.31 N/mm ²	Tensione fless. piano XZ	: 0.42 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.165	Coefficiente sfrutt. nel piano XZ	: 0.023
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.165	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.023

fs : 6.052

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 61-62 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.19 (fs=5.258)

Sforzo Normale di Progetto [daN]	: 371 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -429
Momento Flettente Mz di Progetto [daNm]	: 695

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.05
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.003
fs	: 319.71
Tensione di Progetto relativa a My [N/mm ²]	: 0.64
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.26
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.187
fs	: 5.35
Coefficiente di Sfruttamento	: 0.19
fs	: 5.26

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.065 (fs=15.288)

Taglio Ty di Progetto [daN]	: 319
Taglio Tz di Progetto [daN]	: 870
Momento Torcente Mt di Progetto [daNm]	: 370

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.06
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.16
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.065

fs

: 15.29

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 3.32 N/mm ²	Tensione fless. piano XZ	: 0.38 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.166	Coefficiente sfrutt. nel piano XZ	: 0.020
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.166	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.020
fs	: 6.040		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 62-63 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.149 (fs=6.72)

Sforzo Normale di Progetto [daN]	: 962 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -134
Momento Flettente Mz di Progetto [daNm]	: -569

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.12
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.008
fs	: 123.4
Tensione di Progetto relativa a My [N/mm ²]	: 0.2
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.67
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.141
fs	: 7.11

Coefficiente di Sfruttamento : 0.149
fs : 6.72

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 160x500**
Comb. più gravosa : " Comb 11 [SLD] [IN] " - Coeff. Sfruttamento : 0.052 (fs=19.123)
Taglio Ty di Progetto [daN] : -314
Taglio Tz di Progetto [daN] : -671
Momento Torcente Mt di Progetto [daNm] : -299

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.06
Tensione di Progetto relativa a Tz [N/mm²] : 0.13
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.052
fs : 19.12

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 22	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm²	Tensione Critica nel piano XZ	: 243.66 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.54 N/mm²
Tensione fless. piano XY	: 2.69 N/mm²	Tensione fless. piano XZ	: 0.02 N/mm²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.134	Coefficiente sfrutt. nel piano XZ	: 0.001
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.134	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.001
fs	: 7.440		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 63-64 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 22 [SLD] [IN] " - Coeff. Sfruttamento : 0.153 (fs=6.519)

Sforzo Normale di Progetto [daN] : 877 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -96
 Momento Flettente Mz di Progetto [daNm] : 601

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.11
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.007
 fs : 135.29
 Tensione di Progetto relativa a My [N/mm²] : 0.14
 Tensione di Progetto relativa a Mz [N/mm²] : 2.82
 Tensione Resistente relativa a My [N/mm²] : 18.54
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.146
 fs : 6.85
 Coefficiente di Sfruttamento : 0.153
 fs : 6.52

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.05 (fs=19.917)

Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : -452
 Momento Torcente Mt di Progetto [daNm] : -1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.08
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.05
 fs : 19.92

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 50	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 2.84 N/mm ²	Tensione fless. piano XZ	: 0.14 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.142	Coefficiente sfrutt. nel piano XZ	: 0.008
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.142	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.008
fs	: 7.058		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1380.0 mm
 Comb. di carico più gravosa : 142
 Carico distribuito Istantaneo : -441.6 daN/m
 -
 Freccia Istantanea - COMBINAZIONE
 Freccia Finale - COMBINAZIONE
 Modulo Elastico istantaneo : 11500.0 N/mm²

Schema adottato Doppio Incastro
 Peso proprio : -30.8 daN/m
 -
 Carico distribuito Finale : -441.6 daN/m
 Comb 42 [CAR] [ST]
 Comb 2 [SLEQP] [LT]
 Modulo Elastico finale : 6388.9 N/mm²

Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 64-65 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 22 [SLD] [IN] " - Coeff. Sfruttamento : 0.156 (fs=6.426)

Sforzo Normale di Progetto [daN]	: 1189 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -121
Momento Flettente Mz di Progetto [daNm]	: 593

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.15
Tensione Resistente [N/mm²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.01
fs	: 99.83
Tensione di Progetto relativa a My [N/mm²]	: 0.18
Tensione di Progetto relativa a Mz [N/mm²]	: 2.78
Tensione Resistente relativa a My [N/mm²]	: 18.54
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.146
fs	: 6.87
Coefficiente di Sfruttamento	: 0.156
fs	: 6.43

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.054 (fs=18.631)

Taglio Ty di Progetto [daN]	: -153
Taglio Tz di Progetto [daN]	: -745
Momento Torcente Mt di Progetto [daNm]	: -218

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm²]	: 0.14
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.054
fs	: 18.63

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 34	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mmq	Tensione Critica nel piano XZ	: 243.66 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.54 N/mmq
Tensione fless. piano XY	: 2.80 N/mmq	Tensione fless. piano XZ	: 0.18 N/mmq
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000

Coefficiente sfrutt. nel piano XY	: 0.140	Coefficiente sfrutt. nel piano XZ	: 0.010
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.141	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.012
fs	: 7.067		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 65-66 Primo [Travel]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.188 (fs=5.328)

Sforzo Normale di Progetto [daN]	: 1278 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 286
Momento Flettente Mz di Progetto [daNm]	: -687

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.16
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.011
fs	: 92.87
Tensione di Progetto relativa a My [N/mm ²]	: 0.43
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.22
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.177
fs	: 5.65
Coefficiente di Sfruttamento	: 0.188
fs	: 5.33

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.066 (fs=15.136)

Taglio Ty di Progetto [daN]	: -330
Taglio Tz di Progetto [daN]	: -876
Momento Torcente Mt di Progetto [daNm]	: 374

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.06
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Tensione di Progetto relativa a Tz [N/mm ²]	: 0.16
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.066
fs	: 15.14

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 51	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 3.28 N/mm ²	Tensione fless. piano XZ	: 0.19 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.164	Coefficiente sfrutt. nel piano XZ	: 0.010
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.164	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.010
fs	: 6.100		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 66-67 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.192 (fs=5.218)

Sforzo Normale di Progetto [daN]	: -93 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -491
Momento Flettente Mz di Progetto [daNm]	: 700

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.01
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.001
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 0.74
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.28
Tensione Resistente relativa a My [N/mm ²]	: 18.54

Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.192
f_s	: 5.22
Coefficiente di Sfruttamento a pressoflessione	: 0.192
f_s	: 5.22

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.059 ($f_s=16.851$)

Taglio T_y di Progetto [daN]	: 377
Taglio T_z di Progetto [daN]	: 751
Momento Torcente M_t di Progetto [daNm]	: 377

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.07
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.14
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.059
f_s	: 16.85

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 34	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 3.30 N/mm ²	Tensione fless. piano XZ	: 0.35 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.165	Coefficiente sfrutt. nel piano XZ	: 0.019
Coeff. sfrutt. max euleriano	: 0.001		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.165	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.020
f_s	: 6.050		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale ($t > \text{inf.}$)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 67-68 Primo [Trave]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 160x500**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.149 (fs=6.728)
 Sforzo Normale di Progetto [daN] : 965 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -128
 Momento Flettente Mz di Progetto [daNm] : 569

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.12
 Tensione Resistente [N/mm²] : 14.83
 Coefficiente di Sfruttamento a trazione : 0.008
 fs : 122.98
 Tensione di Progetto relativa a My [N/mm²] : 0.19
 Tensione di Progetto relativa a Mz [N/mm²] : 2.67
 Tensione Resistente relativa a My [N/mm²] : 18.54
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.141
 fs : 7.12
 Coefficiente di Sfruttamento : 0.149
 fs : 6.73

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 160x500**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.054 (fs=18.552)
 Taglio Ty di Progetto [daN] : -6
 Taglio Tz di Progetto [daN] : -486
 Momento Torcente Mt di Progetto [daNm] : 30

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
 Tensione di Progetto relativa a Tz [N/mm²] : 0.09
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.054
 fs : 18.55

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 2.67 N/mm ²	Tensione fless. piano XZ	: 0.19 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.133	Coefficiente sfrutt. nel piano XZ	: 0.010
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.133	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.010
fs	: 7.506		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m

Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 68-69 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.208 (fs=4.816)

Sforzo Normale di Progetto [daN]	: 1898 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -389
Momento Flettente Mz di Progetto [daNm]	: -725

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.24
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.016
fs	: 62.51
Tensione di Progetto relativa a My [N/mm ²]	: 0.58
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.4
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.192
fs	: 5.22
Coefficiente di Sfruttamento	: 0.208
fs	: 4.82

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 160x500**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.074 (fs=13.605)

Taglio Ty di Progetto [daN]	: 860
Taglio Tz di Progetto [daN]	: -586
Momento Torcente Mt di Progetto [daNm]	: -725

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.16
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.11
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.074
fs	: 13.61

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 9	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 507622 daNm	Momento Critico nel piano XZ	: 162439 daNm
Tensione Critica nel piano XY	: 2379.48 N/mm ²	Tensione Critica nel piano XZ	: 243.66 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²

Tensione fless. piano XY	: 3.40 N/mm ²	Tensione fless. piano XZ	: 0.58 N/mm ²
Snellezza relativa nel piano XY	: 0.10	Snellezza relativa nel piano XZ	: 0.31
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.170	Coefficiente sfrutt. nel piano XZ	: 0.031
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.170	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.031
fs	: 5.894		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.6 daN/m	-	
-		Carico distribuito Finale	: -441.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 941.001
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 941.001

Campata 69-70 Primo [Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1662.44 mm - **R 160x500** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1662.44 mm / 1662.44 mm] - **R 160x500**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.214 (fs=4.663)

Sforzo Normale di Progetto [daN]	: 1463 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -428
Momento Flettente Mz di Progetto [daNm]	: -760

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.18
Tensione Resistente [N/mm ²]	: 14.83
Coefficiente di Sfruttamento a trazione	: 0.012
fs	: 81.12
Tensione di Progetto relativa a My [N/mm ²]	: 0.64
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.56
Tensione Resistente relativa a My [N/mm ²]	: 18.54
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.202
fs	: 4.95
Coefficiente di Sfruttamento	: 0.214
fs	: 4.66

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1662.44 mm] - **R 160x500**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.078 (fs=12.758)

Taglio Ty di Progetto [daN]	: 260
Taglio Tz di Progetto [daN]	: 657
Momento Torcente Mt di Progetto [daNm]	: -29

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.05
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.12
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.078
fs	: 12.76

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 9	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1662.4	Lunghezza efficace nel piano XZ	: 1662.4
Momento Critico nel piano XY	: 421380 daNm	Momento Critico nel piano XZ	: 134842 daNm
Tensione Critica nel piano XY	: 1975.22 N/mm ²	Tensione Critica nel piano XZ	: 202.26 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.54 N/mm ²
Tensione fless. piano XY	: 3.56 N/mm ²	Tensione fless. piano XZ	: 0.64 N/mm ²
Snellezza relativa nel piano XY	: 0.11	Snellezza relativa nel piano XZ	: 0.34
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.178	Coefficiente sfrutt. nel piano XZ	: 0.035
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.178	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.035
fs	: 5.620		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1662.4 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -30.8 daN/m
Carico distribuito Istantaneo	: -441.0 daN/m	-	
-		Carico distribuito Finale	: -441.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.005 mm	Limite Freccia Istantanea L/500	: 3.325 mm
Freccia Netta Finale	: -0.009 mm	Limite Freccia Netta Fin. L/ 350	: 4.750 mm
Freccia Finale	: -0.009 mm	Limite Freccia Finale L/ 300	: 5.541 mm
Fatt. sicurezza freccia Istantanea	: 679.066	Fatt. sicurezza freccia Netta Finale	: 538.941
Fatt. sicurezza freccia Finale	: 628.765	Fatt. sicurezza	: 538.941

Campata 1-71 Primo I[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.263 (fs=3.805)

Sforzo Normale di Progetto [daN]	: 5349 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -18

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 3.71
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.232
fs	: 4.31

Tensione di Progetto relativa a M_y [N/mm ²]	: 0
Tensione di Progetto relativa a M_z [N/mm ²]	: 0.62
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.031
f_s	: 32.28
Coefficiente di Sfruttamento	: 0.263
f_s	: 3.8

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.008 ($f_s=132.746$)

Taglio T_y di Progetto [daN]	: 19
Taglio T_z di Progetto [daN]	: -2
Momento Torcente M_t di Progetto [daNm]	: -21

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.02
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.008
f_s	: 132.75

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.25	Snellezza nel piano XZ	: 58.92
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.97
Coefficiente K_c nel piano XY	: 0.94	Coefficiente K_c nel piano XZ	: 0.82
Coefficiente di sfruttamento nel piano XY	: 0.290	Coefficiente di sfruttamento nel piano XZ	: 0.330
f_s	: 3.033		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 42	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mm ²	Tensione Critica nel piano XZ	: 333.25 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.66 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.033	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.297		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.330	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.297
f_s	: 3.033		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale ($t > inf.$)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2041.2 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -6.0 daN/m

-

Freccia Istantanea - COMBINAZIONE

Freccia Finale - COMBINAZIONE

Schema adottato Doppia Cerniera

Peso proprio : -5.5 daN/m

-

Carico distribuito Finale : -6.0 daN/m

Comb 42 [CAR] [ST]

Comb 2 [SLEQP] [LT]

Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.132 mm	Limite Freccia Istantanea L/500	: 4.082 mm
Freccia Netta Finale	: -0.237 mm	Limite Freccia Netta Fin. L/350	: 5.832 mm
Freccia Finale	: -0.237 mm	Limite Freccia Finale L/300	: 6.804 mm
Fatt. sicurezza freccia Istantanea	: 30.962	Fatt. sicurezza freccia Netta Finale	: 24.573
Fatt. sicurezza freccia Finale	: 28.669	Fatt. sicurezza	: 24.573

Campata 1-92 Primo I[Asta GEN.]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)
L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**
Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.125 (fs=7.982)

Sforzo Normale di Progetto [daN]	: 1164 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 43

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.81
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.05
fs	: 19.83
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.5
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.075
fs	: 13.36
Coefficiente di Sfruttamento	: 0.125
fs	: 7.98

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.011 (fs=88.387)

Taglio Ty di Progetto [daN]	: 29
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: -58

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.011
fs	: 88.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 59.34
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.98
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.81
Coefficiente di sfruttamento nel piano XY	: 0.129	Coefficiente di sfruttamento nel piano XZ	: 0.137
fs	: 7.276		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2055.6	Lunghezza efficace nel piano XZ	: 2055.6
Momento Critico nel piano XY	: 9530 daNm	Momento Critico nel piano XZ	: 9530 daNm
Tensione Critica nel piano XY	: 330.92 N/mm ²	Tensione Critica nel piano XZ	: 330.92 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.56 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.078	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.060		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.137	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.060
fs	: 7.276		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2055.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.136 mm	Limite Freccia Istantanea L/500	: 4.111 mm
Freccia Netta Finale	: -0.244 mm	Limite Freccia Netta Fin. L/ 350	: 5.873 mm
Freccia Finale	: -0.244 mm	Limite Freccia Finale L/ 300	: 6.852 mm
Fatt. sicurezza freccia Istantanea	: 30.317	Fatt. sicurezza freccia Netta Finale	: 24.061
Fatt. sicurezza freccia Finale	: 28.071	Fatt. sicurezza	: 24.061

Campata 92-2 Primo I[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.149 (fs=6.722)

Sforzo Normale di Progetto [daN]	: 1435 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -50

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.062
fs	: 16.07
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.73
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.087
fs	: 11.55
Coefficiente di Sfruttamento	: 0.149

fs

: 6.72

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.017 (fs=58.258)

Taglio Ty di Progetto [daN]	: 44
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: -60

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.05
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.017
fs	: 58.26

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 59.34
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 26
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.98
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.81
Coefficiente di sfruttamento nel piano XY	: 0.167	Coefficiente di sfruttamento nel piano XZ	: 0.183
fs	: 5.459		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2055.6	Lunghezza efficace nel piano XZ	: 2055.6
Momento Critico nel piano XY	: 9530 daNm	Momento Critico nel piano XZ	: 9530 daNm
Tensione Critica nel piano XY	: 330.92 N/mm²	Tensione Critica nel piano XZ	: 330.92 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 1.40 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.070	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.113		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.183	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.113
fs	: 5.459		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2055.6 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -6.0 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm²
Controfreccia	: 0.000 mm
Freccia Istantanea	: -0.136 mm
Freccia Netta Finale	: -0.244 mm
Freccia Finale	: -0.244 mm
Fatt. sicurezza freccia Istantanea	: 30.317
Fatt. sicurezza freccia Finale	: 28.071

Schema adottato Doppia Cerniera	
Peso proprio	: -5.5 daN/m
-	
Carico distribuito Finale	: -6.0 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [LT]	
Modulo Elastico finale	: 6388.9 N/mm²
Limite Freccia Istantanea L/500	: 4.111 mm
Limite Freccia Netta Fin. L/ 350	: 5.873 mm
Limite Freccia Finale L/ 300	: 6.852 mm
Fatt. sicurezza freccia Netta Finale	: 24.061
Fatt. sicurezza	: 24.061

Campata 6-89 Primo I[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2002.62 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.18 (fs=5.544)

Sforzo Normale di Progetto [daN]	: 545 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -90

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.38
Tensione Resistente [N/mm²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.024
fs	: 42.31
Tensione di Progetto relativa a My [N/mm²]	: 0
Tensione di Progetto relativa a Mz [N/mm²]	: 3.14
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.157
fs	: 6.38
Coefficiente di Sfruttamento	: 0.18
fs	: 5.54

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.011 (fs=94.561)

Taglio Ty di Progetto [daN]	: -27
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -51

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.011
fs	: 94.56

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 57.81
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 37
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.162	Coefficiente di sfruttamento nel piano XZ	: 0.171
fs	: 5.831		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 37	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2002.6	Lunghezza efficace nel piano XZ	: 2002.6
Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm

Tensione Critica nel piano XY	: 339.67 N/mm ²	Tensione Critica nel piano XZ	: 339.67 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.84 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.092	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.079		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.171	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.079
fs	: 5.831		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2002.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.122 mm	Limite Freccia Istantanea L/500	: 4.005 mm
Freccia Netta Finale	: -0.220 mm	Limite Freccia Netta Fin. L/ 350	: 5.722 mm
Freccia Finale	: -0.220 mm	Limite Freccia Finale L/ 300	: 6.675 mm
Fatt. sicurezza freccia Istantanea	: 32.785	Fatt. sicurezza freccia Netta Finale	: 26.020
Fatt. sicurezza freccia Finale	: 30.357	Fatt. sicurezza	: 26.020

Campata 89-7 Primo I[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2002.62 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.161 (fs=6.198)

Sforzo Normale di Progetto [daN]	: -1111 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -92

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.77
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.042
fs	: 23.6
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.2
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.16
fs	: 6.27
Coefficiente di Sfruttamento a pressoflessione	: 0.161
fs	: 6.2

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 44 [SLV] [IN] " - Coeff. Sfruttamento : 0.013 (fs=77.199)

Taglio Ty di Progetto [daN]	: 33
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Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : 18

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.013
 fs : 77.2

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 57.81
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.204	Coefficiente di sfruttamento nel piano XZ	: 0.211
fs	: 4.746		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2002.6	Lunghezza efficace nel piano XZ	: 2002.6
Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm
Tensione Critica nel piano XY	: 339.67 N/mm ²	Tensione Critica nel piano XZ	: 339.67 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 3.20 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.160	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.051		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.211	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.051
fs	: 4.746		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2002.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.122 mm	Limite Freccia Istantanea L/500	: 4.005 mm
Freccia Netta Finale	: -0.220 mm	Limite Freccia Netta Fin. L/ 350	: 5.722 mm
Freccia Finale	: -0.220 mm	Limite Freccia Finale L/ 300	: 6.675 mm
Fatt. sicurezza freccia Istantanea	: 32.785	Fatt. sicurezza freccia Netta Finale	: 26.020
Fatt. sicurezza freccia Finale	: 30.357	Fatt. sicurezza	: 26.020

Campata 9-90 Primo I[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2002.62 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.148 (fs=6.767)

Sforzo Normale di Progetto [daN] : 514 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : -72

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.36
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.022
 fs : 44.89
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 2.51
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.125
 fs : 7.97
 Coefficiente di Sfruttamento : 0.148
 fs : 6.77

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.009 (fs=113.477)

Taglio Ty di Progetto [daN] : -22
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : -26

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.009
 fs : 113.48

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 57.81
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 37
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.128	Coefficiente di sfruttamento nel piano XZ	: 0.138
fs	: 7.241		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 37	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2002.6	Lunghezza efficace nel piano XZ	: 2002.6
Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm
Tensione Critica nel piano XY	: 339.67 N/mm²	Tensione Critica nel piano XZ	: 339.67 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 1.20 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.060	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.078		

Coeff. sfrutt. TOTALE (Piano XY) : 0.138
fs : 7.241

Coeff. sfrutt. TOTALE (Piano XZ) : 0.078

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 2002.6 mm
Comb. di carico più gravosa : 142
Carico distribuito Istantaneo : -6.0 daN/m

Schema adottato Doppia Cerniera

Peso proprio : -5.5 daN/m

-

Carico distribuito Finale : -6.0 daN/m

Freccia Istantanea - COMBINAZIONE

Comb 42 [CAR] [ST]

Freccia Finale - COMBINAZIONE

Comb 2 [SLEQP] [LT]

Modulo Elastico istantaneo : 11500.0 N/mm²

Modulo Elastico finale : 6388.9 N/mm²

Controfreccia : 0.000 mm

Freccia Istantanea : -0.122 mm

Limite Freccia Istantanea L/500 : 4.005 mm

Freccia Netta Finale : -0.220 mm

Limite Freccia Netta Fin. L/ 350 : 5.722 mm

Freccia Finale : -0.220 mm

Limite Freccia Finale L/ 300 : 6.675 mm

Fatt. sicurezza freccia Istantanea : 32.785

Fatt. sicurezza freccia Netta Finale : 26.020

Fatt. sicurezza freccia Finale : 30.357

Fatt. sicurezza : 26.020

Campata 90-10 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2002.62 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.124 (fs=8.049)

Sforzo Normale di Progetto [daN]

: -1092 (COMPRESSIONE)

Momento Flettente My di Progetto [daNm]

: 0

Momento Flettente Mz di Progetto [daNm]

: -71

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]

: -0.76

Tensione Resistente [N/mm²]

: 18.21

Coefficiente di Sfruttamento a compressione

: 0.042

fs

: 24

Tensione di Progetto relativa a My [N/mm²]

: 0

Tensione di Progetto relativa a Mz [N/mm²]

: 2.45

Tensione Resistente relativa a My [N/mm²]

: 20.03

Tensione Resistente relativa a Mz [N/mm²]

: 20.03

Coefficiente di Sfruttamento a flessione

: 0.123

fs

: 8.16

Coefficiente di Sfruttamento a pressoflessione

: 0.124

fs

: 8.05

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 44 [SLV] [IN] " - Coeff. Sfruttamento : 0.011 (fs=91.886)

Taglio Ty di Progetto [daN]

: 28

Taglio Tz di Progetto [daN]

: -2

Momento Torcente Mt di Progetto [daNm]

: 4

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]

: 0.03

Tensione di Progetto relativa a Tz [N/mm²]

: 0.00

Tensione tang. Resistente [N/mm²]

: 2.66

Coefficiente di Sfruttamento a taglio : 0.011
fs : 91.89

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 57.81
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.167	Coefficiente di sfruttamento nel piano XZ	: 0.173
fs	: 5.787		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2002.6	Lunghezza efficace nel piano XZ	: 2002.6
Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm
Tensione Critica nel piano XY	: 339.67 N/mm ²	Tensione Critica nel piano XZ	: 339.67 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 2.45 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.123	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.050		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.173	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.050
fs	: 5.787		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2002.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.122 mm	Limite Freccia Istantanea L/500	: 4.005 mm
Freccia Netta Finale	: -0.220 mm	Limite Freccia Netta Fin. L/ 350	: 5.722 mm
Freccia Finale	: -0.220 mm	Limite Freccia Finale L/ 300	: 6.675 mm
Fatt. sicurezza freccia Istantanea	: 32.785	Fatt. sicurezza freccia Netta Finale	: 26.020
Fatt. sicurezza freccia Finale	: 30.357	Fatt. sicurezza	: 26.020

Campata 13-91 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.102 (fs=9.797)

Sforzo Normale di Progetto [daN]	: 1275 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 27

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.89
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.055
fs	: 18.1
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.94
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.047
fs	: 21.35
Coefficiente di Sfruttamento	: 0.102
fs	: 9.8

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.014 (fs=71.754)

Taglio Ty di Progetto [daN]	: -35
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: -7

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.014
fs	: 71.75

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 59.34
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 45
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.98
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.81
Coefficiente di sfruttamento nel piano XY	: 0.138	Coefficiente di sfruttamento nel piano XZ	: 0.148
fs	: 6.742		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 45	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2055.6	Lunghezza efficace nel piano XZ	: 2055.6
Momento Critico nel piano XY	: 9530 daNm	Momento Critico nel piano XZ	: 9530 daNm
Tensione Critica nel piano XY	: 330.92 N/mm ²	Tensione Critica nel piano XZ	: 330.92 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.43 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.071	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.077		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.148	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.077
fs	: 6.742		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)
· Modulo Elastico Ridotto

Lunghezza elemento	: 2055.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.136 mm	Limite Freccia Istantanea L/500	: 4.111 mm
Freccia Netta Finale	: -0.244 mm	Limite Freccia Netta Fin. L/ 350	: 5.873 mm
Freccia Finale	: -0.244 mm	Limite Freccia Finale L/ 300	: 6.852 mm
Fatt. sicurezza freccia Istantanea	: 30.317	Fatt. sicurezza freccia Netta Finale	: 24.061
Fatt. sicurezza freccia Finale	: 28.071	Fatt. sicurezza	: 24.061

Campata 88-14 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.074 (fs=13.527)

Sforzo Normale di Progetto [daN]	: 734 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -24

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.51
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.032
fs	: 31.45
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.84
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.042
fs	: 23.74
Coefficiente di Sfruttamento	: 0.074
fs	: 13.53

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 39 [SLV] [IN] " - Coeff. Sfruttamento : 0.006 (fs=161.031)

Taglio Ty di Progetto [daN]	: -16
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 11

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.006
fs	: 161.03

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.25	Snellezza nel piano XZ	: 58.92

Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.97
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.82
Coefficiente di sfruttamento nel piano XY	: 0.094	Coefficiente di sfruttamento nel piano XZ	: 0.101
fs	: 9.857		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mm ²	Tensione Critica nel piano XZ	: 333.25 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 12.74 N/mm ²
Tensione fless. piano XY	: 0.60 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.047	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.054		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.101	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.054
fs	: 9.857		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2041.2 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.132 mm	Limite Freccia Istantanea L/500	: 4.082 mm
Freccia Netta Finale	: -0.237 mm	Limite Freccia Netta Fin. L/ 350	: 5.832 mm
Freccia Finale	: -0.237 mm	Limite Freccia Finale L/ 300	: 6.804 mm
Fatt. sicurezza freccia Istantanea	: 30.962	Fatt. sicurezza freccia Netta Finale	: 24.573
Fatt. sicurezza freccia Finale	: 28.669	Fatt. sicurezza	: 24.573

Campata 91-14 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.094 (fs=10.592)

Sforzo Normale di Progetto [daN]	: 1590 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -15

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1.1
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.069
fs	: 14.51
Tensione di Progetto relativa a My [N/mm ²]	: 0

Tensione di Progetto relativa a M_z [N/mm ²]	: 0.51
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.025
f_s	: 39.23
Coefficiente di Sfruttamento	: 0.094
f_s	: 10.59

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.006 ($f_s=155.558$)

Taglio T_y di Progetto [daN]	: -16
Taglio T_z di Progetto [daN]	: -3
Momento Torcente M_t di Progetto [daNm]	: 8

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.02
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.006
f_s	: 155.56

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 59.34
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 38
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.98
Coefficiente K_c nel piano XY	: 0.94	Coefficiente K_c nel piano XZ	: 0.81
Coefficiente di sfruttamento nel piano XY	: 0.094	Coefficiente di sfruttamento nel piano XZ	: 0.105
f_s	: 9.536		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 38	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2055.6	Lunghezza efficace nel piano XZ	: 2055.6
Momento Critico nel piano XY	: 9530 daNm	Momento Critico nel piano XZ	: 9530 daNm
Tensione Critica nel piano XY	: 330.92 N/mm ²	Tensione Critica nel piano XZ	: 330.92 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.51 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.026	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.079		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.105	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.079
f_s	: 9.536		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale ($t > inf.$)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2055.6 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -6.0 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm ²

Schema adottato Doppia Cerniera	
Peso proprio	: -5.5 daN/m
-	
Carico distribuito Finale	: -6.0 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [LT]	
Modulo Elastico finale	: 6388.9 N/mm ²

Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.136 mm	Limite Freccia Istantanea L/500	: 4.111 mm
Freccia Netta Finale	: -0.244 mm	Limite Freccia Netta Fin. L/ 350	: 5.873 mm
Freccia Finale	: -0.244 mm	Limite Freccia Finale L/ 300	: 6.852 mm
Fatt. sicurezza freccia Istantanea	: 30.317	Fatt. sicurezza freccia Netta Finale	: 24.061
Fatt. sicurezza freccia Finale	: 28.071	Fatt. sicurezza	: 24.061

Campata 71-15 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.252 (fs=3.968)

Sforzo Normale di Progetto [daN]	: 5184 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 16

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 3.6
Tensione Resistente [N/mm²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.225
fs	: 4.45
Tensione di Progetto relativa a My [N/mm²]	: 0
Tensione di Progetto relativa a Mz [N/mm²]	: 0.55
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.027
fs	: 36.61
Coefficiente di Sfruttamento	: 0.252
fs	: 3.97

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.012 (fs=85.868)

Taglio Ty di Progetto [daN]	: 30
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -31

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.012
fs	: 85.87

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.25	Snellezza nel piano XZ	: 58.92
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.97
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.82
Coefficiente di sfruttamento nel piano XY	: 0.270	Coefficiente di sfruttamento nel piano XZ	: 0.304
fs	: 3.294		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mm ²	Tensione Critica nel piano XZ	: 333.25 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.06 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.053	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.251		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.304	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.251
fs	: 3.294		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2041.2 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.132 mm	Limite Freccia Istantanea L/500	: 4.082 mm
Freccia Netta Finale	: -0.237 mm	Limite Freccia Netta Fin. L/ 350	: 5.832 mm
Freccia Finale	: -0.237 mm	Limite Freccia Finale L/ 300	: 6.804 mm
Fatt. sicurezza freccia Istantanea	: 30.962	Fatt. sicurezza freccia Netta Finale	: 24.573
Fatt. sicurezza freccia Finale	: 28.669	Fatt. sicurezza	: 24.573

Campata 16-88 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.079 (fs=12.697)

Sforzo Normale di Progetto [daN]	: 1204 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 15

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.84
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.052
fs	: 19.16
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.53
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.027
fs	: 37.63
Coefficiente di Sfruttamento	: 0.079
fs	: 12.7

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 39 [SLV] [IN] " - Coeff. Sfruttamento : 0.012 (fs=82.02)

Taglio Ty di Progetto [daN]	: -31
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 29

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.012
fs	: 82.02

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.25	Snellezza nel piano XZ	: 58.92
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 38
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.97
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.82
Coefficiente di sfruttamento nel piano XY	: 0.113	Coefficiente di sfruttamento nel piano XZ	: 0.122
fs	: 8.228		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 38	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mmq	Tensione Critica nel piano XZ	: 333.25 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 1.18 N/mmq	Tensione fless. piano XZ	: 0.00 N/mmq
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.059	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.063		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.122	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.063
fs	: 8.228		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2041.2 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.132 mm	Limite Freccia Istantanea L/500	: 4.082 mm
Freccia Netta Finale	: -0.237 mm	Limite Freccia Netta Fin. L/ 350	: 5.832 mm
Freccia Finale	: -0.237 mm	Limite Freccia Finale L/ 300	: 6.804 mm
Fatt. sicurezza freccia Istantanea	: 30.962	Fatt. sicurezza freccia Netta Finale	: 24.573
Fatt. sicurezza freccia Finale	: 28.669	Fatt. sicurezza	: 24.573

Campata 17-72 Primo [Asta GEN.]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.319 (fs=3.139)

Sforzo Normale di Progetto [daN] : 5815 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 0
Momento Flettente Mz di Progetto [daNm] : -38

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 4.04
Tensione Resistente [N/mm²] : 16.02
Coefficiente di Sfruttamento a trazione : 0.252
fs : 3.97
Tensione di Progetto relativa a My [N/mm²] : 0
Tensione di Progetto relativa a Mz [N/mm²] : 1.33
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.067
fs : 15.03
Coefficiente di Sfruttamento : 0.319
fs : 3.14

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.009 (fs=110.028)

Taglio Ty di Progetto [daN] : -23
Taglio Tz di Progetto [daN] : -2
Momento Torcente Mt di Progetto [daNm] : -31

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.009
fs : 110.03

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 51
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.316	Coefficiente di sfruttamento nel piano XZ	: 0.353
fs	: 2.829		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 51	Sezione più sfavorevole	: 3
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mmq	Tensione Critica nel piano XZ	: 341.39 N/mmq

Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.95 N/mm ²	Tensione fless. piano XZ	: 0.03 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.047	Coefficiente sfrutt. nel piano XZ	: 0.002
Coeff. sfrutt. max euleriano	: 0.305		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.352	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.306
fs	: 2.838		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 87-18 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.126 (fs=7.925)

Sforzo Normale di Progetto [daN]	: 321 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -65

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.22
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.014
fs	: 71.98
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.25
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.112
fs	: 8.91
Coefficiente di Sfruttamento	: 0.126
fs	: 7.92

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.012 (fs=80.245)

Taglio Ty di Progetto [daN]	: 32
Taglio Tz di Progetto [daN]	: -2

Momento Torcente Mt di Progetto [daNm] : -65

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.012
 fs : 80.24

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.121	Coefficiente di sfruttamento nel piano XZ	: 0.129
fs	: 7.777		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm²	Tensione Critica nel piano XZ	: 341.39 N/mm²
Resistenza fless. piano XY	: 12.74 N/mm²	Resistenza fless. piano XZ	: 12.74 N/mm²
Tensione fless. piano XY	: 0.84 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.066	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.063		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.129	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.063
fs	: 7.777		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 72-19 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.311 (fs=3.22)

Sforzo Normale di Progetto [daN] : 5658 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : -38

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 3.93
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.245
 fs : 4.08
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 1.31
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.065
 fs : 15.3
 Coefficiente di Sfruttamento : 0.311
 fs : 3.22

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.012 (fs=81.791)

Taglio Ty di Progetto [daN] : 31
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : -53

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.012
 fs : 81.79

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.298	Coefficiente di sfruttamento nel piano XZ	: 0.335
fs	: 2.981		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm²	Tensione Critica nel piano XZ	: 341.39 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 0.60 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.030	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.306		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.335	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.306

fs : 2.981

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 20-87 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.122 (fs=8.214)

Sforzo Normale di Progetto [daN]	: -1470 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -68

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -1.02
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.056
fs	: 17.83
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.38
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.119
fs	: 8.43
Coefficiente di Sfruttamento a pressoflessione	: 0.122
fs	: 8.21

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.014 (fs=69.085)

Taglio Ty di Progetto [daN]	: -37
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 10

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.014

fs

: 69.08

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.178	Coefficiente di sfruttamento nel piano XZ	: 0.186
fs	: 5.375		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 2.38 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.119	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.067		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.186	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.067
fs	: 5.375		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 21-73 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.352 (fs=2.838)

Sforzo Normale di Progetto [daN]	: 6083 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -51

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 4.22
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.264
fs	: 3.79
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.78
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.089
fs	: 11.27
Coefficiente di Sfruttamento	: 0.352
fs	: 2.84

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 48 [SLV] [IN] " - Coeff. Sfruttamento : 0.01 (fs=96.148)

Taglio Ty di Progetto [daN]	: -26
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -3

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.01
fs	: 96.15

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 26
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.321	Coefficiente di sfruttamento nel piano XZ	: 0.360
fs	: 2.777		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.80 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.040	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.320		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.360	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.320
fs	: 2.777		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1992.5 mm

Schema adottato Doppia Cerniera

Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 86-22 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.145 (fs=6.902)

Sforzo Normale di Progetto [daN]	: 459 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -72

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.32
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.02
fs	: 50.32
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.5
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.125
fs	: 8
Coefficiente di Sfruttamento	: 0.145
fs	: 6.9

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 39 [SLV] [IN] " - Coeff. Sfruttamento : 0.012 (fs=84.901)

Taglio Ty di Progetto [daN]	: 30
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -63

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.012
fs	: 84.9

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92

Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.135	Coefficiente di sfruttamento nel piano XZ	: 0.143
fs	: 6.976		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 21	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.52 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.076	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.067		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.143	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.067
fs	: 6.976		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 73-23 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.315 (fs=3.176)

Sforzo Normale di Progetto [daN]	: 6272 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 25

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 4.36
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.272
fs	: 3.68
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.86

Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.043
f_s	: 23.23
Coefficiente di Sfruttamento	: 0.315
f_s	: 3.18

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**
Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.015 ($f_s=67.907$)

Taglio T_y di Progetto [daN]	: 37
Taglio T_z di Progetto [daN]	: -2
Momento Torcente M_t di Progetto [daNm]	: -80

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.04
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.015
f_s	: 67.91

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente K_c nel piano XY	: 0.95	Coefficiente K_c nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.388	Coefficiente di sfruttamento nel piano XZ	: 0.429
f_s	: 2.332		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.83 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.092	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.337		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.429	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.337
f_s	: 2.332		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -6.0 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm ²
Controfreccia	: 0.000 mm

Schema adottato Doppia Cerniera	
Peso proprio	: -5.5 daN/m
-	
Carico distribuito Finale	: -6.0 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [LT]	
Modulo Elastico finale	: 6388.9 N/mm ²

Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 24-86 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.14 (fs=7.132)

Sforzo Normale di Progetto [daN]	: -1681 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -78

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -1.17
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.064
fs	: 15.6
Tensione di Progetto relativa a My [N/mm²]	: 0
Tensione di Progetto relativa a Mz [N/mm²]	: 2.73
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.136
fs	: 7.35
Coefficiente di Sfruttamento a pressoflessione	: 0.14
fs	: 7.13

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.014 (fs=70.803)

Taglio Ty di Progetto [daN]	: -36
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -27

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.014
fs	: 70.8

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.204	Coefficiente di sfruttamento nel piano XZ	: 0.213
fs	: 4.690		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 2.73 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.136	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.077		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.213	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.077
fs	: 4.690		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 25-74 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2063.23 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2063.23 mm / 2063.23 mm] - **R 120x120**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.367 (fs=2.727)

Sforzo Normale di Progetto [daN]	: 7322 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -28

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 5.08
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.317
fs	: 3.15
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.99
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.049
fs	: 20.29
Coefficiente di Sfruttamento	: 0.367
fs	: 2.73

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2063.23 mm / 2063.23 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.014 (fs=70.137)

Taglio Ty di Progetto [daN]	: -36
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: -44

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.014
fs	: 70.14

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.69	Snellezza nel piano XZ	: 59.56
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.95
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 50
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.98
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.81
Coefficiente di sfruttamento nel piano XY	: 0.414	Coefficiente di sfruttamento nel piano XZ	: 0.468
fs	: 2.138		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 50	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2063.2	Lunghezza efficace nel piano XZ	: 2063.2
Momento Critico nel piano XY	: 9495 daNm	Momento Critico nel piano XZ	: 9495 daNm
Tensione Critica nel piano XY	: 329.69 N/mm²	Tensione Critica nel piano XZ	: 329.69 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 1.71 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.086	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.382		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.468	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.382
fs	: 2.138		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2063.2 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.138 mm	Limite Freccia Istantanea L/500	: 4.126 mm
Freccia Netta Finale	: -0.248 mm	Limite Freccia Netta Fin. L/ 350	: 5.895 mm
Freccia Finale	: -0.248 mm	Limite Freccia Finale L/ 300	: 6.877 mm
Fatt. sicurezza freccia Istantanea	: 29.980	Fatt. sicurezza freccia Netta Finale	: 23.794
Fatt. sicurezza freccia Finale	: 27.759	Fatt. sicurezza	: 23.794

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.159 (fs=6.28)

Sforzo Normale di Progetto [daN]	: -1188 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -91

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.83
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.045
fs	: 22.06
Tensione di Progetto relativa a My [N/mm²]	: 0
Tensione di Progetto relativa a Mz [N/mm²]	: 3.15
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.157
fs	: 6.36
Coefficiente di Sfruttamento a pressoflessione	: 0.159
fs	: 6.28

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.013 (fs=79.016)

Taglio Ty di Progetto [daN]	: 32
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -91

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.013
fs	: 79.02

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.211	Coefficiente di sfruttamento nel piano XZ	: 0.220
fs	: 4.546		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm²	Tensione Critica nel piano XZ	: 341.39 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²

Tensione fless. piano XY	: 2.94 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.147	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.073		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.220	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.073
fs	: 4.546		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 27-85 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.163 (fs=6.141)

Sforzo Normale di Progetto [daN]	: -858 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -93

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.6
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.033
fs	: 30.56
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.24
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.162
fs	: 6.18
Coefficiente di Sfruttamento a pressoflessione	: 0.163
fs	: 6.14

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.015 (fs=66.127)

Taglio Ty di Progetto [daN]	: -38
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -32

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.04
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.015
fs	: 66.13

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.221	Coefficiente di sfruttamento nel piano XZ	: 0.230
fs	: 4.352		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 3.12 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.156	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.074		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.230	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.074
fs	: 4.352		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 74-28 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2063.23 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2063.23 mm / 2063.23 mm] - **R 120x120**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.389 (fs=2.573)

Sforzo Normale di Progetto [daN] : 7031 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : -48

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 4.88
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.305
 fs : 3.28
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 1.68
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.084
 fs : 11.93
 Coefficiente di Sfruttamento : 0.389
 fs : 2.57

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2063.23 mm / 2063.23 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.016 (fs=63.007)

Taglio Ty di Progetto [daN] : 40
 Taglio Tz di Progetto [daN] : -3
 Momento Torcente Mt di Progetto [daNm] : -93

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.04
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.016
 fs : 63.01

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.69	Snellezza nel piano XZ	: 59.56
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.95
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.98
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.81
Coefficiente di sfruttamento nel piano XY	: 0.385	Coefficiente di sfruttamento nel piano XZ	: 0.442
fs	: 2.264		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2063.2	Lunghezza efficace nel piano XZ	: 2063.2
Momento Critico nel piano XY	: 9495 daNm	Momento Critico nel piano XZ	: 9495 daNm
Tensione Critica nel piano XY	: 329.69 N/mmq	Tensione Critica nel piano XZ	: 329.69 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 0.85 N/mmq	Tensione fless. piano XZ	: 0.00 N/mmq
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.042	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.399		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.442	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.399
fs	: 2.264		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2063.2 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.138 mm	Limite Freccia Istantanea L/500	: 4.126 mm
Freccia Netta Finale	: -0.248 mm	Limite Freccia Netta Fin. L/ 350	: 5.895 mm
Freccia Finale	: -0.248 mm	Limite Freccia Finale L/ 300	: 6.877 mm
Fatt. sicurezza freccia Istantanea	: 29.980	Fatt. sicurezza freccia Netta Finale	: 23.794
Fatt. sicurezza freccia Finale	: 27.759	Fatt. sicurezza	: 23.794

Campata 84-29 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.185 (fs=5.392)

Sforzo Normale di Progetto [daN]	: -1161 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -106

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.81
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.044
fs	: 22.58
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.67
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.183
fs	: 5.45
Coefficiente di Sfruttamento a pressoflessione	: 0.185
fs	: 5.39

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.016 (fs=64.026)

Taglio Ty di Progetto [daN]	: 40
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -106

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.016
fs	: 64.03

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.241	Coefficiente di sfruttamento nel piano XZ	: 0.250
fs	: 3.998		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 3.56 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.178	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.072		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.250	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.072
fs	: 3.998		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 31-84 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.19 (fs=5.266)

Sforzo Normale di Progetto [daN]	: -839 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -109

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.58
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.032
fs	: 31.24
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.78
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.189
fs	: 5.29
Coefficiente di Sfruttamento a pressoflessione	: 0.19
fs	: 5.27

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**
Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.018 (fs=56.164)

Taglio Ty di Progetto [daN]	: -45
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -43

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.05
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.018
fs	: 56.16

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.243	Coefficiente di sfruttamento nel piano XZ	: 0.252
fs	: 3.967		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 3.56 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.178	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.074		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.252	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.074
fs	: 3.967		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m

Carico distribuito Istantaneo	: -6.0 daN/m	-	Carico distribuito Finale	: -6.0 daN/m
-			Comb 42 [CAR] [ST]	
Freccia Istantanea - COMBINAZIONE			Comb 2 [SLEQP] [LT]	
Freccia Finale - COMBINAZIONE			Modulo Elastico finale	: 6388.9 N/mm ²
Modulo Elastico istantaneo	: 11500.0 N/mm ²			
Controfreccia	: 0.000 mm			
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm	
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm	
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm	
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419	
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419	

Campata 83-33 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.214 (fs=4.682)

Sforzo Normale di Progetto [daN]	: 631 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -107

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.44
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.027
fs	: 36.58
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.73
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.186
fs	: 5.37
Coefficiente di Sfruttamento	: 0.214
fs	: 4.68

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.016 (fs=62.114)

Taglio Ty di Progetto [daN]	: 41
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -107

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.016
fs	: 62.11

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21

Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.203	Coefficiente di sfruttamento nel piano XZ	: 0.213
fs	: 4.704		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 21	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 2.76 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.138	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.075		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.213	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.075
fs	: 4.704		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 35-83 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.192 (fs=5.204)

Sforzo Normale di Progetto [daN]	: -1729 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -108

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -1.2
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.066
fs	: 15.16
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.76
Tensione Resistente relativa a My [N/mm ²]	: 20.03

Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.188
f_s	: 5.32
Coefficiente di Sfruttamento a pressoflessione	: 0.192
f_s	: 5.2

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**
Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.017 ($f_s=58.492$)

Taglio T_y di Progetto [daN]	: -44
Taglio T_z di Progetto [daN]	: -2
Momento Torcente M_t di Progetto [daNm]	: -45

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.05
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.017
f_s	: 58.49

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente K_c nel piano XY	: 0.95	Coefficiente K_c nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.257	Coefficiente di sfruttamento nel piano XZ	: 0.267
f_s	: 3.743		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 3.76 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.188	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.079		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.267	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.079
f_s	: 3.743		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -6.0 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm ²
Controfreccia	: 0.000 mm
Freccia Istantanea	: -0.120 mm

Schema adottato Doppia Cerniera	
Peso proprio	: -5.5 daN/m
-	
Carico distribuito Finale	: -6.0 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [LT]	
Modulo Elastico finale	: 6388.9 N/mm ²
Limite Freccia Istantanea L/500	: 3.985 mm

Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 82-37 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.206 (fs=4.862)

Sforzo Normale di Progetto [daN]	: 617 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -103

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.43
Tensione Resistente [N/mm²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.027
fs	: 37.4
Tensione di Progetto relativa a My [N/mm²]	: 0
Tensione di Progetto relativa a Mz [N/mm²]	: 3.58
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.179
fs	: 5.59
Coefficiente di Sfruttamento	: 0.206
fs	: 4.86

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.016 (fs=63.137)

Taglio Ty di Progetto [daN]	: 40
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -103

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.016
fs	: 63.14

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.201	Coefficiente di sfruttamento nel piano XZ	: 0.204
fs	: 4.905		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 3.53 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.176	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.028		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.204	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.028
fs	: 4.905		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 39-82 Primo [Asta GEN.]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.186 (fs=5.376)

Sforzo Normale di Progetto [daN]	: -1391 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -106

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.97
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.053
fs	: 18.84
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.67
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.183
fs	: 5.46
Coefficiente di Sfruttamento a pressoflessione	: 0.186
fs	: 5.38

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**
 Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.016 (fs=61.72)

Taglio Ty di Progetto [daN] : -41
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : -47

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.04
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.016
 fs : 61.72

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.252	Coefficiente di sfruttamento nel piano XZ	: 0.262
fs	: 3.811		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm²	Tensione Critica nel piano XZ	: 341.39 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 3.59 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.179	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.083		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.262	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.083
fs	: 3.811		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.348 (fs=2.871)

Sforzo Normale di Progetto [daN] : 6213 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 0
Momento Flettente Mz di Progetto [daNm] : 46

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 4.31
Tensione Resistente [N/mm²] : 16.02
Coefficiente di Sfruttamento a trazione : 0.269
fs : 3.71
Tensione di Progetto relativa a My [N/mm²] : 0
Tensione di Progetto relativa a Mz [N/mm²] : 1.58
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.079
fs : 12.66
Coefficiente di Sfruttamento : 0.348
fs : 2.87

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.016 (fs=63.531)

Taglio Ty di Progetto [daN] : -40
Taglio Tz di Progetto [daN] : -2
Momento Torcente Mt di Progetto [daNm] : 96

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.04
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.016
fs : 63.53

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 50
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.351	Coefficiente di sfruttamento nel piano XZ	: 0.390
fs	: 2.563		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 50	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mmq	Tensione Critica nel piano XZ	: 341.39 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 1.35 N/mmq	Tensione fless. piano XZ	: 0.00 N/mmq

Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.067	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.323		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.390	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.323
fs	: 2.563		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 81-44 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.186 (fs=5.364)

Sforzo Normale di Progetto [daN]	: 517 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -95

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.36
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.022
fs	: 44.62
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.29
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.164
fs	: 6.1
Coefficiente di Sfruttamento	: 0.186
fs	: 5.36

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.016 (fs=63.292)

Taglio Ty di Progetto [daN]	: 40
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -99

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.04
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.016
fs	: 63.29

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.189	Coefficiente di sfruttamento nel piano XZ	: 0.193
fs	: 5.181		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 3.19 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.159	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.034		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.193	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.034
fs	: 5.181		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 45-78 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 2 - [X=332.08 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.333 (fs=3.006)

Sforzo Normale di Progetto [daN]	: 6021 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 1
Momento Flettente Mz di Progetto [daNm]	: 41

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 4.18
Tensione Resistente [N/mm²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.261
fs	: 3.83
Tensione di Progetto relativa a My [N/mm²]	: 0.02
Tensione di Progetto relativa a Mz [N/mm²]	: 1.42
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.072
fs	: 13.95
Coefficiente di Sfruttamento	: 0.333
fs	: 3.01

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.015 (fs=68.425)

Taglio Ty di Progetto [daN]	: 37
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 48

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.015
fs	: 68.43

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.385	Coefficiente di sfruttamento nel piano XZ	: 0.427
fs	: 2.340		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm²	Tensione Critica nel piano XZ	: 341.39 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 1.65 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.083	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.345		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.427	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.345
fs	: 2.340		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 46-81 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.169 (fs=5.906)

Sforzo Normale di Progetto [daN]	: -1366 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -96

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.95
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.052
fs	: 19.2
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.34
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.167
fs	: 6
Coefficiente di Sfruttamento a pressoflessione	: 0.169
fs	: 5.91

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.015 (fs=67.218)

Taglio Ty di Progetto [daN]	: -38
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -47

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.015
fs	: 67.22

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.229	Coefficiente di sfruttamento nel piano XZ	: 0.239
fs	: 4.189		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mmq	Tensione Critica nel piano XZ	: 341.39 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 3.14 N/mmq	Tensione fless. piano XZ	: 0.00 N/mmq
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.157	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.082		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.239	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.082
fs	: 4.189		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 77-47 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.316 (fs=3.168)

Sforzo Normale di Progetto [daN]	: 5922 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -34

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 4.11
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Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.257
fs	: 3.9
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.18
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.059
fs	: 16.97
Coefficiente di Sfruttamento	: 0.316
fs	: 3.17

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.016 (fs=64.461)

Taglio Ty di Progetto [daN]	: -39
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 84

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.016
fs	: 64.46

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellenza nel piano XY	: 40.26	Snellenza nel piano XZ	: 57.52
Snellenza relativa nel piano XY	: 0.64	Snellenza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 50
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.379	Coefficiente di sfruttamento nel piano XZ	: 0.419
fs	: 2.386		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 50	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.87 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellenza relativa nel piano XY	: 0.27	Snellenza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.093	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.326		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.419	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.326
fs	: 2.386		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	

-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 80-48 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.149 (fs=6.725)

Sforzo Normale di Progetto [daN]	: -553 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -86

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.38
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.021
fs	: 47.38
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.97
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.148
fs	: 6.75
Coefficiente di Sfruttamento a pressoflessione	: 0.149
fs	: 6.73

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.016 (fs=62.185)

Taglio Ty di Progetto [daN]	: 41
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -86

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.016
fs	: 62.18

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 45
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95

Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.170	Coefficiente di sfruttamento nel piano XZ	: 0.180
fs	: 5.571		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 45	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 2.07 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.103	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.076		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.180	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.076
fs	: 5.571		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 49-77 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.339 (fs=2.953)

Sforzo Normale di Progetto [daN]	: 5717 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 52

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 3.97
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.248
fs	: 4.04
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.82
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03

Coefficiente di Sfruttamento a flessione	: 0.091
fs	: 11.01
Coefficiente di Sfruttamento	: 0.339
fs	: 2.95

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**
Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.011 (fs=90.479)

Taglio Ty di Progetto [daN]	: 28
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 38

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.011
fs	: 90.48

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.337	Coefficiente di sfruttamento nel piano XZ	: 0.378
fs	: 2.646		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm²	Tensione Critica nel piano XZ	: 341.39 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 0.90 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.045	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.333		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.378	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.333
fs	: 2.646		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -6.0 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm²
Controfreccia	: 0.000 mm
Freccia Istantanea	: -0.120 mm
Freccia Netta Finale	: -0.215 mm

Schema adottato Doppia Cerniera	
Peso proprio	: -5.5 daN/m
-	
Carico distribuito Finale	: -6.0 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [LT]	
Modulo Elastico finale	: 6388.9 N/mm²
Limite Freccia Istantanea L/500	: 3.985 mm
Limite Freccia Netta Fin. L/350	: 5.693 mm

Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 50-80 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.133 (fs=7.511)

Sforzo Normale di Progetto [daN]	: -683 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -76

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.47
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.026
fs	: 38.39
Tensione di Progetto relativa a My [N/mm²]	: 0
Tensione di Progetto relativa a Mz [N/mm²]	: 2.65
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.132
fs	: 7.55
Coefficiente di Sfruttamento a pressoflessione	: 0.133
fs	: 7.51

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.011 (fs=93.617)

Taglio Ty di Progetto [daN]	: -27
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -27

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.011
fs	: 93.62

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.174	Coefficiente di sfruttamento nel piano XZ	: 0.184
fs	: 5.437		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 2.01 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.100	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.084		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.184	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.084
fs	: 5.437		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto			
Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 76-51 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.302 (fs=3.306)

Sforzo Normale di Progetto [daN]	: 5986 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 25

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 4.16
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.259
fs	: 3.85
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.86
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.043
fs	: 23.22
Coefficiente di Sfruttamento	: 0.302
fs	: 3.31

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.015 (fs=67.212)

Taglio Ty di Progetto [daN] : -38
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : 72

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.04
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.015
 fs : 67.21

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 50
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.339	Coefficiente di sfruttamento nel piano XZ	: 0.376
fs	: 2.662		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 50	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm²	Tensione Critica nel piano XZ	: 341.39 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 1.58 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.079	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.297		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.376	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.297
fs	: 2.662		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 53-76 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

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L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.32 (fs=3.126)

Sforzo Normale di Progetto [daN] : 5584 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 0
Momento Flettente Mz di Progetto [daNm] : 45

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 3.88
Tensione Resistente [N/mm²] : 16.02
Coefficiente di Sfruttamento a trazione : 0.242
fs : 4.13
Tensione di Progetto relativa a My [N/mm²] : 0
Tensione di Progetto relativa a Mz [N/mm²] : 1.56
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.078
fs : 12.84
Coefficiente di Sfruttamento : 0.32
fs : 3.13

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.013 (fs=77.803)

Taglio Ty di Progetto [daN] : 33
Taglio Tz di Progetto [daN] : -2
Momento Torcente Mt di Progetto [daNm] : 40

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.013
fs : 77.8

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.330	Coefficiente di sfruttamento nel piano XZ	: 0.371
fs	: 2.697		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mmq	Tensione Critica nel piano XZ	: 341.39 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 0.82 N/mmq	Tensione fless. piano XZ	: 0.00 N/mmq
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27

Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.041	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.330		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.371	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.330
fs	: 2.697		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 75-55 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.283 (fs=3.53)

Sforzo Normale di Progetto [daN]	: 5386 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 29

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 3.74
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.233
fs	: 4.28
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.05
fs	: 20.07
Coefficiente di Sfruttamento	: 0.283
fs	: 3.53

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 48 [SLV] [IN] " - Coeff. Sfruttamento : 0.013 (fs=76.471)

Taglio Ty di Progetto [daN]	: -33
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 35

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.03
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.013
f_s	: 76.47

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.25	Snellezza nel piano XZ	: 58.92
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.97
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.82
Coefficiente di sfruttamento nel piano XY	: 0.254	Coefficiente di sfruttamento nel piano XZ	: 0.288
f_s	: 3.469		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 42	Sezione più sfavorevole	: 6
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mm ²	Tensione Critica nel piano XZ	: 333.25 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.63 N/mm ²	Tensione fless. piano XZ	: 0.02 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.032	Coefficiente sfrutt. nel piano XZ	: 0.001
Coeff. sfrutt. max euleriano	: 0.256		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.287	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.257
f_s	: 3.479		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2041.2 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.132 mm	Limite Freccia Istantanea L/500	: 4.082 mm
Freccia Netta Finale	: -0.237 mm	Limite Freccia Netta Fin. L/ 350	: 5.832 mm
Freccia Finale	: -0.237 mm	Limite Freccia Finale L/ 300	: 6.804 mm
Fatt. sicurezza freccia Istantanea	: 30.962	Fatt. sicurezza freccia Netta Finale	: 24.573
Fatt. sicurezza freccia Finale	: 28.669	Fatt. sicurezza	: 24.573

Campata 56-79 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.108 ($f_s=9.241$)

Sforzo Normale di Progetto [daN] : 1387 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : 28

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.96
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.06
 fs : 16.64
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 0.96
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.048
 fs : 20.79
 Coefficiente di Sfruttamento : 0.108
 fs : 9.24

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.011 (fs=87.047)

Taglio Ty di Progetto [daN] : 29
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : -27

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.011
 fs : 87.05

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.25	Snellezza nel piano XZ	: 58.92
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 37
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.97
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.82
Coefficiente di sfruttamento nel piano XY	: 0.079	Coefficiente di sfruttamento nel piano XZ	: 0.089
fs	: 11.245		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 37	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mm ²	Tensione Critica nel piano XZ	: 333.25 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.32 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.016	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.073		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.089	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.073
fs	: 11.245		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 2041.2 mm

Comb. di carico più gravosa : 142

Carico distribuito Istantaneo : -6.0 daN/m

-

Freccia Istantanea - COMBINAZIONE

Freccia Finale - COMBINAZIONE

Modulo Elastico istantaneo : 11500.0 N/mm²

Controfreccia : 0.000 mm

Freccia Istantanea : -0.132 mm

Freccia Netta Finale : -0.237 mm

Freccia Finale : -0.237 mm

Fatt. sicurezza freccia Istantanea : 30.962

Fatt. sicurezza freccia Finale : 28.669

Schema adottato Doppia Cerniera

Peso proprio : -5.5 daN/m

-

Carico distribuito Finale : -6.0 daN/m

Comb 42 [CAR] [ST]

Comb 2 [SLEQP] [LT]

Modulo Elastico finale : 6388.9 N/mm²

Limite Freccia Istantanea L/500 : 4.082 mm

Limite Freccia Netta Fin. L/ 350 : 5.832 mm

Limite Freccia Finale L/ 300 : 6.804 mm

Fatt. sicurezza freccia Netta Finale : 24.573

Fatt. sicurezza : 24.573

Campata 57-75 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.262 (fs=3.814)

Sforzo Normale di Progetto [daN] : 5539 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : 0

Momento Flettente Mz di Progetto [daNm] : 13

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 3.85

Tensione Resistente [N/mm²] : 16.02

Coefficiente di Sfruttamento a trazione : 0.24

fs : 4.17

Tensione di Progetto relativa a My [N/mm²] : 0

Tensione di Progetto relativa a Mz [N/mm²] : 0.44

Tensione Resistente relativa a My [N/mm²] : 20.03

Tensione Resistente relativa a Mz [N/mm²] : 20.03

Coefficiente di Sfruttamento a flessione : 0.022

fs : 45.25

Coefficiente di Sfruttamento : 0.262

fs : 3.81

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.007 (fs=139.795)

Taglio Ty di Progetto [daN] : -18

Taglio Tz di Progetto [daN] : -2

Momento Torcente Mt di Progetto [daNm] : 21

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02

Tensione di Progetto relativa a Tz [N/mm²] : 0.00

Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a taglio : 0.007

fs : 139.8

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.25	Snellezza nel piano XZ	: 58.92
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.97
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.82
Coefficiente di sfruttamento nel piano XY	: 0.296	Coefficiente di sfruttamento nel piano XZ	: 0.336
fs	: 2.974		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mm ²	Tensione Critica nel piano XZ	: 333.25 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.72 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.036	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.300		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.336	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.300
fs	: 2.974		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2041.2 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.132 mm	Limite Freccia Istantanea L/500	: 4.082 mm
Freccia Netta Finale	: -0.237 mm	Limite Freccia Netta Fin. L/ 350	: 5.832 mm
Freccia Finale	: -0.237 mm	Limite Freccia Finale L/ 300	: 6.804 mm
Fatt. sicurezza freccia Istantanea	: 30.962	Fatt. sicurezza freccia Netta Finale	: 24.573
Fatt. sicurezza freccia Finale	: 28.669	Fatt. sicurezza	: 24.573

Campata 57-93 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.13 (fs=7.718)

Sforzo Normale di Progetto [daN]	: 1293 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -42

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.9
Tensione Resistente [N/mm ²]	: 16.02

Coefficiente di Sfruttamento a trazione	: 0.056
fs	: 17.84
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.47
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.074
fs	: 13.61
Coefficiente di Sfruttamento	: 0.13
fs	: 7.72

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**
Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.01 (fs=100.841)

Taglio Ty di Progetto [daN]	: 25
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: -42

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.01
fs	: 100.84

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 59.34
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 34
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.98
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.81
Coefficiente di sfruttamento nel piano XY	: 0.126	Coefficiente di sfruttamento nel piano XZ	: 0.134
fs	: 7.467		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 34	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2055.6	Lunghezza efficace nel piano XZ	: 2055.6
Momento Critico nel piano XY	: 9530 daNm	Momento Critico nel piano XZ	: 9530 daNm
Tensione Critica nel piano XY	: 330.92 N/mm ²	Tensione Critica nel piano XZ	: 330.92 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.55 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.077	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.057		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.134	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.057
fs	: 7.467		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2055.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m

Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.136 mm	Limite Freccia Istantanea L/500	: 4.111 mm
Freccia Netta Finale	: -0.244 mm	Limite Freccia Netta Fin. L/ 350	: 5.873 mm
Freccia Finale	: -0.244 mm	Limite Freccia Finale L/ 300	: 6.852 mm
Fatt. sicurezza freccia Istantanea	: 30.317	Fatt. sicurezza freccia Netta Finale	: 24.061
Fatt. sicurezza freccia Finale	: 28.071	Fatt. sicurezza	: 24.061

Campata 93-58 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.135 (fs=7.427)

Sforzo Normale di Progetto [daN]	: 1541 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 39

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1.07
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.067
fs	: 14.97
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.36
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.068
fs	: 14.74
Coefficiente di Sfruttamento	: 0.135
fs	: 7.43

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.012 (fs=80.28)

Taglio Ty di Progetto [daN]	: -32
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: 47

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.012
fs	: 80.28

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 59.34
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.98
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.81

Coefficiente di sfruttamento nel piano XY : 0.142
fs : 6.360

Coefficiente di sfruttamento nel piano XZ : 0.157

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 33
Lunghezza efficace nel piano XY : 2055.6
Momento Critico nel piano XY : 9530 daNm
Tensione Critica nel piano XY : 330.92 N/mm²
Resistenza fless. piano XY : 20.03 N/mm²
Tensione fless. piano XY : 0.94 N/mm²
Snellezza relativa nel piano XY : 0.27
Coeff. Riduttivo nel piano XY : 1.000
Coefficiente sfrutt. nel piano XY : 0.047
Coeff. sfrutt. max euleriano : 0.111
Coeff. sfrutt. TOTALE (Piano XY) : 0.157
fs : 6.360

Sezione più sfavorevole : 7
Lunghezza efficace nel piano XZ : 2055.6
Momento Critico nel piano XZ : 9530 daNm
Tensione Critica nel piano XZ : 330.92 N/mm²
Resistenza fless. piano XZ : 20.03 N/mm²
Tensione fless. piano XZ : 0.00 N/mm²
Snellezza relativa nel piano XZ : 0.27
Coeff. Riduttivo nel piano XZ : 1.000
Coefficiente sfrutt. nel piano XZ : 0.000
Coeff. sfrutt. TOTALE (Piano XZ) : 0.111

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 2055.6 mm
Comb. di carico più gravosa : 142
Carico distribuito Istantaneo : -6.0 daN/m

Schema adottato Doppia Cerniera
Peso proprio : -5.5 daN/m

Freccia Istantanea - COMBINAZIONE

Freccia Finale - COMBINAZIONE

Modulo Elastico istantaneo : 11500.0 N/mm²
Controfreccia : 0.000 mm
Freccia Istantanea : -0.136 mm
Freccia Netta Finale : -0.244 mm
Freccia Finale : -0.244 mm
Fatt. sicurezza freccia Istantanea : 30.317
Fatt. sicurezza freccia Finale : 28.071

-
Carico distribuito Finale : -6.0 daN/m
Comb 42 [CAR] [ST]
Comb 2 [SLEQP] [LT]
Modulo Elastico finale : 6388.9 N/mm²

Limite Freccia Istantanea L/500 : 4.111 mm
Limite Freccia Netta Fin. L/ 350 : 5.873 mm
Limite Freccia Finale L/ 300 : 6.852 mm
Fatt. sicurezza freccia Netta Finale : 24.061
Fatt. sicurezza : 24.061

Campata 61-95 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2002.62 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 29 [SLD] [IN] " - Coeff. Sfruttamento : 0.125 (fs=8.024)

Sforzo Normale di Progetto [daN] : 1135 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 0
Momento Flettente Mz di Progetto [daNm] : 44

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.79
Tensione Resistente [N/mm²] : 16.02
Coefficiente di Sfruttamento a trazione : 0.049
fs : 20.33
Tensione di Progetto relativa a My [N/mm²] : 0
Tensione di Progetto relativa a Mz [N/mm²] : 1.51
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.075

fs	: 13.26
Coefficiente di Sfruttamento	: 0.125
fs	: 8.02

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.009 (fs=110.232)

Taglio Ty di Progetto [daN]	: -23
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -28

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.009
fs	: 110.23

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 57.81
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.183	Coefficiente di sfruttamento nel piano XZ	: 0.193
fs	: 5.190		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2002.6	Lunghezza efficace nel piano XZ	: 2002.6
Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm
Tensione Critica nel piano XY	: 339.67 N/mm²	Tensione Critica nel piano XZ	: 339.67 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 2.25 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.112	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.080		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.193	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.080
fs	: 5.190		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2002.6 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -6.0 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm²
Controfreccia	: 0.000 mm
Freccia Istantanea	: -0.122 mm
Freccia Netta Finale	: -0.220 mm
Freccia Finale	: -0.220 mm

Schema adottato Doppia Cerniera	
Peso proprio	: -5.5 daN/m
-	
Carico distribuito Finale	: -6.0 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [LT]	
Modulo Elastico finale	: 6388.9 N/mm²
Limite Freccia Istantanea L/500	: 4.005 mm
Limite Freccia Netta Fin. L/ 350	: 5.722 mm
Limite Freccia Finale L/ 300	: 6.675 mm

Fatt. sicurezza freccia Istantanea : 32.785
Fatt. sicurezza freccia Finale : 30.357

Fatt. sicurezza freccia Netta Finale : 26.020
Fatt. sicurezza : 26.020

Campata 95-62 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 2002.62 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.167 (fs=5.981)

Sforzo Normale di Progetto [daN] : 1144 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 0
Momento Flettente Mz di Progetto [daNm] : -68

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.79
Tensione Resistente [N/mm²] : 16.02
Coefficiente di Sfruttamento a trazione : 0.05
fs : 20.16
Tensione di Progetto relativa a My [N/mm²] : 0
Tensione di Progetto relativa a Mz [N/mm²] : 2.36
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.118
fs : 8.5
Coefficiente di Sfruttamento : 0.167
fs : 5.98

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa : 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.007 (fs=147.087)

Taglio Ty di Progetto [daN] : 17
Taglio Tz di Progetto [daN] : -2
Momento Torcente Mt di Progetto [daNm] : -68

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.007
fs : 147.09

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 57.81
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 29
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.145	Coefficiente di sfruttamento nel piano XZ	: 0.154
fs	: 6.475		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 29

Sezione più sfavorevole : 7

Lunghezza efficace nel piano XY	: 2002.6	Lunghezza efficace nel piano XZ	: 2002.6
Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm
Tensione Critica nel piano XY	: 339.67 N/mm ²	Tensione Critica nel piano XZ	: 339.67 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.56 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.078	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.077		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.154	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.077
fs	: 6.475		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2002.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.122 mm	Limite Freccia Istantanea L/500	: 4.005 mm
Freccia Netta Finale	: -0.220 mm	Limite Freccia Netta Fin. L/ 350	: 5.722 mm
Freccia Finale	: -0.220 mm	Limite Freccia Finale L/ 300	: 6.675 mm
Fatt. sicurezza freccia Istantanea	: 32.785	Fatt. sicurezza freccia Netta Finale	: 26.020
Fatt. sicurezza freccia Finale	: 30.357	Fatt. sicurezza	: 26.020

Campata 96-65 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2002.62 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.106 (fs=9.431)

Sforzo Normale di Progetto [daN]	: 1780 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -17

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1.24
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.077
fs	: 12.96
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.58
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.029
fs	: 34.63
Coefficiente di Sfruttamento	: 0.106
fs	: 9.43

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.006 (fs=164.763)

Taglio Ty di Progetto [daN] : -15
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : 55

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.006
 fs : 164.76

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 57.81
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.161	Coefficiente di sfruttamento nel piano XZ	: 0.171
fs	: 5.850		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2002.6	Lunghezza efficace nel piano XZ	: 2002.6
Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm
Tensione Critica nel piano XY	: 339.67 N/mm²	Tensione Critica nel piano XZ	: 339.67 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 1.90 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.095	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.076		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.171	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.076
fs	: 5.850		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2002.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.122 mm	Limite Freccia Istantanea L/500	: 4.005 mm
Freccia Netta Finale	: -0.220 mm	Limite Freccia Netta Fin. L/ 350	: 5.722 mm
Freccia Finale	: -0.220 mm	Limite Freccia Finale L/ 300	: 6.675 mm
Fatt. sicurezza freccia Istantanea	: 32.785	Fatt. sicurezza freccia Netta Finale	: 26.020
Fatt. sicurezza freccia Finale	: 30.357	Fatt. sicurezza	: 26.020

Campata 66-96 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
 L= 2002.62 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2002.62 mm] - **R 120x120**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.143 (fs=6.971)
 Sforzo Normale di Progetto [daN] : 1074 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : 56

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.75
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.047
 fs : 21.49
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 1.94
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.097
 fs : 10.32
 Coefficiente di Sfruttamento : 0.143
 fs : 6.97

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**
Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.007 (fs=136.074)
 Taglio Ty di Progetto [daN] : -19
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : 5

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.007
 fs : 136.07

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 57.81
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.136	Coefficiente di sfruttamento nel piano XZ	: 0.149
fs	: 6.723		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2002.6	Lunghezza efficace nel piano XZ	: 2002.6
Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm
Tensione Critica nel piano XY	: 339.67 N/mm ²	Tensione Critica nel piano XZ	: 339.67 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.86 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000

Coefficiente sfrutt. nel piano XY	: 0.043	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.106		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.149	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.106
fs	: 6.723		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2002.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.122 mm	Limite Freccia Istantanea L/500	: 4.005 mm
Freccia Netta Finale	: -0.220 mm	Limite Freccia Netta Fin. L/ 350	: 5.722 mm
Freccia Finale	: -0.220 mm	Limite Freccia Finale L/ 300	: 6.675 mm
Fatt. sicurezza freccia Istantanea	: 32.785	Fatt. sicurezza freccia Netta Finale	: 26.020
Fatt. sicurezza freccia Finale	: 30.357	Fatt. sicurezza	: 26.020

Campata 69-94 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=1027.78 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.09 (fs=11.068)

Sforzo Normale di Progetto [daN]	: -2369 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 1
Momento Flettente Mz di Progetto [daNm]	: 1

Tipo Verifica : COMPRESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -1.64
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.09
fs	: 11.07

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.011 (fs=94.395)

Taglio Ty di Progetto [daN]	: 27
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: 6

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.011
fs	: 94.4

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
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Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 59.34
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.98
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.81
Coefficiente di sfruttamento nel piano XY	: 0.141	Coefficiente di sfruttamento nel piano XZ	: 0.157
fs	: 6.383		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2055.6	Lunghezza efficace nel piano XZ	: 2055.6
Momento Critico nel piano XY	: 9530 daNm	Momento Critico nel piano XZ	: 9530 daNm
Tensione Critica nel piano XY	: 330.92 N/mm ²	Tensione Critica nel piano XZ	: 330.92 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.90 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.045	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.112		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.157	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.112
fs	: 6.383		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2055.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.136 mm	Limite Freccia Istantanea L/500	: 4.111 mm
Freccia Netta Finale	: -0.244 mm	Limite Freccia Netta Fin. L/ 350	: 5.873 mm
Freccia Finale	: -0.244 mm	Limite Freccia Finale L/ 300	: 6.852 mm
Fatt. sicurezza freccia Istantanea	: 30.317	Fatt. sicurezza freccia Netta Finale	: 24.061
Fatt. sicurezza freccia Finale	: 28.071	Fatt. sicurezza	: 24.061

Campata 79-70 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 5 - [X=1360.79 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.08 (fs=12.524)

Sforzo Normale di Progetto [daN]	: -2093 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 1
Momento Flettente Mz di Progetto [daNm]	: 5

Tipo Verifica : COMPRESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -1.45
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.08
fs	: 12.52

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.006 (fs=158.891)

Taglio Ty di Progetto [daN]	: 16
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -9

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.006
fs	: 158.89

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.25	Snellezza nel piano XZ	: 58.92
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 39
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.97
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.82
Coefficiente di sfruttamento nel piano XY	: 0.112	Coefficiente di sfruttamento nel piano XZ	: 0.124
fs	: 8.037		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 39	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mmq	Tensione Critica nel piano XZ	: 333.25 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 0.64 N/mmq	Tensione fless. piano XZ	: 0.00 N/mmq
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.032	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.092		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.124	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.092
fs	: 8.037		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2041.2 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.132 mm	Limite Freccia Istantanea L/500	: 4.082 mm
Freccia Netta Finale	: -0.237 mm	Limite Freccia Netta Fin. L/ 350	: 5.832 mm
Freccia Finale	: -0.237 mm	Limite Freccia Finale L/ 300	: 6.804 mm
Fatt. sicurezza freccia Istantanea	: 30.962	Fatt. sicurezza freccia Netta Finale	: 24.573
Fatt. sicurezza freccia Finale	: 28.669	Fatt. sicurezza	: 24.573

Campata 94-70 Primo [Asta GEN.]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)
L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.096 (fs=10.457)

Sforzo Normale di Progetto [daN] : 1661 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 0
Momento Flettente Mz di Progetto [daNm] : 14

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 1.15
Tensione Resistente [N/mm²] : 16.02
Coefficiente di Sfruttamento a trazione : 0.072
fs : 13.89
Tensione di Progetto relativa a My [N/mm²] : 0
Tensione di Progetto relativa a Mz [N/mm²] : 0.47
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.024
fs : 42.29
Coefficiente di Sfruttamento : 0.096
fs : 10.46

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.006 (fs=179.413)

Taglio Ty di Progetto [daN] : -14
Taglio Tz di Progetto [daN] : -3
Momento Torcente Mt di Progetto [daNm] : 15

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.01
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.006
fs : 179.41

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 59.34
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.98
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.81
Coefficiente di sfruttamento nel piano XY	: 0.092	Coefficiente di sfruttamento nel piano XZ	: 0.103
fs	: 9.663		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 2055.6	Lunghezza efficace nel piano XZ	: 2055.6
Momento Critico nel piano XY	: 9530 daNm	Momento Critico nel piano XZ	: 9530 daNm
Tensione Critica nel piano XY	: 330.92 N/mmq	Tensione Critica nel piano XZ	: 330.92 N/mmq

Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.37 N/mm ²	Tensione fless. piano XZ	: 0.04 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.018	Coefficiente sfrutt. nel piano XZ	: 0.002
Coeff. sfrutt. max euleriano	: 0.084		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.102	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.086
fs	: 9.812		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2055.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.136 mm	Limite Freccia Istantanea L/500	: 4.111 mm
Freccia Netta Finale	: -0.244 mm	Limite Freccia Netta Fin. L/ 350	: 5.873 mm
Freccia Finale	: -0.244 mm	Limite Freccia Finale L/ 300	: 6.852 mm
Fatt. sicurezza freccia Istantanea	: 30.317	Fatt. sicurezza freccia Netta Finale	: 24.061
Fatt. sicurezza freccia Finale	: 28.071	Fatt. sicurezza	: 24.061

Campata 1-71 Primo I[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.271 (fs=3.697)

Sforzo Normale di Progetto [daN]	: 5210 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -26

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 3.62
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.226
fs	: 4.43
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.9
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.045
fs	: 22.38
Coefficiente di Sfruttamento	: 0.271
fs	: 3.7

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.008 (fs=126.041)

Taglio Ty di Progetto [daN]	: -20
Taglio Tz di Progetto [daN]	: -2

Momento Torcente Mt di Progetto [daNm] : -2

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.008
 fs : 126.04

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.25	Snellezza nel piano XZ	: 58.92
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.97
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.82
Coefficiente di sfruttamento nel piano XY	: 0.268	Coefficiente di sfruttamento nel piano XZ	: 0.302
fs	: 3.314		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mm²	Tensione Critica nel piano XZ	: 333.25 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 1.04 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.052	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.250		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.302	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.250
fs	: 3.314		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2041.2 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.132 mm	Limite Freccia Istantanea L/500	: 4.082 mm
Freccia Netta Finale	: -0.237 mm	Limite Freccia Netta Fin. L/350	: 5.832 mm
Freccia Finale	: -0.237 mm	Limite Freccia Finale L/300	: 6.804 mm
Fatt. sicurezza freccia Istantanea	: 30.962	Fatt. sicurezza freccia Netta Finale	: 24.573
Fatt. sicurezza freccia Finale	: 28.669	Fatt. sicurezza	: 24.573

Campata 1-92 Primo I[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.113 (fs=8.861)

Sforzo Normale di Progetto [daN] : 1455 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : 29

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 1.01
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.063
 fs : 15.86
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 1
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.05
 fs : 20.08
 Coefficiente di Sfruttamento : 0.113
 fs : 8.86

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.009 (fs=109.224)

Taglio Ty di Progetto [daN] : 23
 Taglio Tz di Progetto [daN] : -3
 Momento Torcente Mt di Progetto [daNm] : 18

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.009
 fs : 109.22

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 59.34
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 26
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.98
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.81
Coefficiente di sfruttamento nel piano XY	: 0.133	Coefficiente di sfruttamento nel piano XZ	: 0.149
fs	: 6.713		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2055.6	Lunghezza efficace nel piano XZ	: 2055.6
Momento Critico nel piano XY	: 9530 daNm	Momento Critico nel piano XZ	: 9530 daNm
Tensione Critica nel piano XY	: 330.92 N/mm²	Tensione Critica nel piano XZ	: 330.92 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 0.74 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.037	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.112		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.149	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.112

fs : 6.713

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2055.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.136 mm	Limite Freccia Istantanea L/500	: 4.111 mm
Freccia Netta Finale	: -0.244 mm	Limite Freccia Netta Fin. L/350	: 5.873 mm
Freccia Finale	: -0.244 mm	Limite Freccia Finale L/300	: 6.852 mm
Fatt. sicurezza freccia Istantanea	: 30.317	Fatt. sicurezza freccia Netta Finale	: 24.061
Fatt. sicurezza freccia Finale	: 28.071	Fatt. sicurezza	: 24.061

Campata 92-2 Primo I[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.201 (fs=4.978)

Sforzo Normale di Progetto [daN]	: 1170 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 87

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.81
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.051
fs	: 19.72
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.01
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.15
fs	: 6.66
Coefficiente di Sfruttamento	: 0.201
fs	: 4.98

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 44 [SLV] [IN] " - Coeff. Sfruttamento : 0.01 (fs=104.551)

Taglio Ty di Progetto [daN]	: -24
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: 78

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.01

fs

: 104.55

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 47.47
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.76
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.81
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.91
Coefficiente di sfruttamento nel piano XY	: 0.186	Coefficiente di sfruttamento nel piano XZ	: 0.188
fs	: 5.317		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2055.6	Lunghezza efficace nel piano XZ	: 2055.6
Momento Critico nel piano XY	: 9530 daNm	Momento Critico nel piano XZ	: 9530 daNm
Tensione Critica nel piano XY	: 330.92 N/mm ²	Tensione Critica nel piano XZ	: 330.92 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 2.72 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.136	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.052		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.188	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.052
fs	: 5.317		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2055.6 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.056 mm	Limite Freccia Istantanea L/500	: 4.111 mm
Freccia Netta Finale	: -0.101 mm	Limite Freccia Netta Fin. L/ 350	: 5.873 mm
Freccia Finale	: -0.101 mm	Limite Freccia Finale L/ 300	: 6.852 mm
Fatt. sicurezza freccia Istantanea	: 73.029	Fatt. sicurezza freccia Netta Finale	: 57.959
Fatt. sicurezza freccia Finale	: 67.619	Fatt. sicurezza	: 57.959

Campata 6-89 Primo I[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 2002.62 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.112 (fs=8.893)

Sforzo Normale di Progetto [daN]	: 1203 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 35

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.84
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.052
fs	: 19.19
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.21
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.06
fs	: 16.58
Coefficiente di Sfruttamento	: 0.112
fs	: 8.89

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.011 (fs=94.367)

Taglio Ty di Progetto [daN]	: 27
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -63

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.011
fs	: 94.37

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 57.81
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.153	Coefficiente di sfruttamento nel piano XZ	: 0.160
fs	: 6.268		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2002.6	Lunghezza efficace nel piano XZ	: 2002.6
Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm
Tensione Critica nel piano XY	: 339.67 N/mm ²	Tensione Critica nel piano XZ	: 339.67 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 2.19 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.109	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.050		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.160	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.050
fs	: 6.268		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 2002.6 mm

Schema adottato Doppia Cerniera

Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.122 mm	Limite Freccia Istantanea L/500	: 4.005 mm
Freccia Netta Finale	: -0.220 mm	Limite Freccia Netta Fin. L/ 350	: 5.722 mm
Freccia Finale	: -0.220 mm	Limite Freccia Finale L/ 300	: 6.675 mm
Fatt. sicurezza freccia Istantanea	: 32.785	Fatt. sicurezza freccia Netta Finale	: 26.020
Fatt. sicurezza freccia Finale	: 30.357	Fatt. sicurezza	: 26.020

Campata 89-7 Primo I[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2002.62 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.112 (fs=8.905)

Sforzo Normale di Progetto [daN]	: 554 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -51

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.38
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.024
fs	: 41.66
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.77
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.088
fs	: 11.33
Coefficiente di Sfruttamento	: 0.112
fs	: 8.9

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.008 (fs=122.084)

Taglio Ty di Progetto [daN]	: -21
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -10

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.008
fs	: 122.08

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 46.25
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.74

Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 37
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.111	Coefficiente di sfruttamento nel piano XZ	: 0.113
fs	: 8.825		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 37	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2002.6	Lunghezza efficace nel piano XZ	: 2002.6
Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm
Tensione Critica nel piano XY	: 339.67 N/mm ²	Tensione Critica nel piano XZ	: 339.67 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.85 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.043	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.071		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.113	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.071
fs	: 8.825		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2002.6 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.051 mm	Limite Freccia Istantanea L/500	: 4.005 mm
Freccia Netta Finale	: -0.091 mm	Limite Freccia Netta Fin. L/ 350	: 5.722 mm
Freccia Finale	: -0.091 mm	Limite Freccia Finale L/ 300	: 6.675 mm
Fatt. sicurezza freccia Istantanea	: 78.975	Fatt. sicurezza freccia Netta Finale	: 62.678
Fatt. sicurezza freccia Finale	: 73.125	Fatt. sicurezza	: 62.678

Campata 9-90 Primo I[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2002.62 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.108 (fs=9.234)

Sforzo Normale di Progetto [daN]	: -1075 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -61

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.75
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.041
fs	: 24.38
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.14

Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.107
fs	: 9.38
Coefficiente di Sfruttamento a pressoflessione	: 0.108
fs	: 9.23

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 44 [SLV] [IN] " - Coeff. Sfruttamento : 0.007 (fs=141.103)

Taglio T_y di Progetto [daN]	: 18
Taglio T_z di Progetto [daN]	: -2
Momento Torcente M_t di Progetto [daNm]	: 26

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.02
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.007
fs	: 141.1

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 57.81
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente K_c nel piano XY	: 0.95	Coefficiente K_c nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.150	Coefficiente di sfruttamento nel piano XZ	: 0.156
fs	: 6.405		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2002.6	Lunghezza efficace nel piano XZ	: 2002.6
Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm
Tensione Critica nel piano XY	: 339.67 N/mm ²	Tensione Critica nel piano XZ	: 339.67 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 2.14 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.107	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.050		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.156	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.050
fs	: 6.405		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2002.6 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -6.0 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm ²
Controfreccia	: 0.000 mm

Schema adottato Doppia Cerniera	
Peso proprio	: -5.5 daN/m
-	
Carico distribuito Finale	: -6.0 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [LT]	
Modulo Elastico finale	: 6388.9 N/mm ²

Freccia Istantanea	: -0.122 mm	Limite Freccia Istantanea L/500	: 4.005 mm
Freccia Netta Finale	: -0.220 mm	Limite Freccia Netta Fin. L/ 350	: 5.722 mm
Freccia Finale	: -0.220 mm	Limite Freccia Finale L/ 300	: 6.675 mm
Fatt. sicurezza freccia Istantanea	: 32.785	Fatt. sicurezza freccia Netta Finale	: 26.020
Fatt. sicurezza freccia Finale	: 30.357	Fatt. sicurezza	: 26.020

Campata 90-10 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 2002.62 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.097 (fs=10.352)

Sforzo Normale di Progetto [daN]	: 1643 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -15

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 1.14
Tensione Resistente [N/mm²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.071
fs	: 14.04
Tensione di Progetto relativa a My [N/mm²]	: 0
Tensione di Progetto relativa a Mz [N/mm²]	: 0.51
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.025
fs	: 39.41
Coefficiente di Sfruttamento	: 0.097
fs	: 10.35

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.01 (fs=99.787)

Taglio Ty di Progetto [daN]	: -25
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 3

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.01
fs	: 99.79

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 46.25
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.74
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.109	Coefficiente di sfruttamento nel piano XZ	: 0.111
fs	: 8.971		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 21	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2002.6	Lunghezza efficace nel piano XZ	: 2002.6
Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm
Tensione Critica nel piano XY	: 339.67 N/mm ²	Tensione Critica nel piano XZ	: 339.67 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.49 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.024	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.087		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.111	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.087
fs	: 8.971		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2002.6 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.051 mm	Limite Freccia Istantanea L/500	: 4.005 mm
Freccia Netta Finale	: -0.091 mm	Limite Freccia Netta Fin. L/ 350	: 5.722 mm
Freccia Finale	: -0.091 mm	Limite Freccia Finale L/ 300	: 6.675 mm
Fatt. sicurezza freccia Istantanea	: 78.975	Fatt. sicurezza freccia Netta Finale	: 62.678
Fatt. sicurezza freccia Finale	: 73.125	Fatt. sicurezza	: 62.678

Campata 13-91 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.137)

Sforzo Normale di Progetto [daN]	: 1612 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 23

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1.12
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.07
fs	: 14.31
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.79
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.04
fs	: 25.27
Coefficiente di Sfruttamento	: 0.109
fs	: 9.14

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.005 (fs=200.168)

Taglio Ty di Progetto [daN]	: 12
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: -2

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.005
fs	: 200.17

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 59.34
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 38
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.98
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.81
Coefficiente di sfruttamento nel piano XY	: 0.100	Coefficiente di sfruttamento nel piano XZ	: 0.111
fs	: 9.015		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 38	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2055.6	Lunghezza efficace nel piano XZ	: 2055.6
Momento Critico nel piano XY	: 9530 daNm	Momento Critico nel piano XZ	: 9530 daNm
Tensione Critica nel piano XY	: 330.92 N/mm²	Tensione Critica nel piano XZ	: 330.92 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 0.65 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.033	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.078		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.111	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.078
fs	: 9.015		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2055.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.136 mm	Limite Freccia Istantanea L/500	: 4.111 mm
Freccia Netta Finale	: -0.244 mm	Limite Freccia Netta Fin. L/ 350	: 5.873 mm
Freccia Finale	: -0.244 mm	Limite Freccia Finale L/ 300	: 6.852 mm
Fatt. sicurezza freccia Istantanea	: 30.317	Fatt. sicurezza freccia Netta Finale	: 24.061
Fatt. sicurezza freccia Finale	: 28.071	Fatt. sicurezza	: 24.061

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 3 - [X=680.39 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.079 ($f_s=12.59$)

Sforzo Normale di Progetto [daN] : 879 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 1
Momento Flettente Mz di Progetto [daNm] : 23

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.61
Tensione Resistente [N/mm²] : 16.02
Coefficiente di Sfruttamento a trazione : 0.038
 f_s : 26.26
Tensione di Progetto relativa a My [N/mm²] : 0.04
Tensione di Progetto relativa a Mz [N/mm²] : 0.8
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.041
 f_s : 24.19
Coefficiente di Sfruttamento : 0.079
 f_s : 12.59

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.008 ($f_s=125.189$)

Taglio Ty di Progetto [daN] : 20
Taglio Tz di Progetto [daN] : -2
Momento Torcente Mt di Progetto [daNm] : 22

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.008
 f_s : 125.19

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 41.25	Snellezza nel piano XZ	: 47.14
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 38
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.104	Coefficiente di sfruttamento nel piano XZ	: 0.106
f_s	: 9.443		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 38	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mm ²	Tensione Critica nel piano XZ	: 333.25 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²

Tensione fless. piano XY	: 1.01 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.051	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.055		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.106	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.055
fs	: 9.443		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2041.2 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.055 mm	Limite Freccia Istantanea L/500	: 4.082 mm
Freccia Netta Finale	: -0.099 mm	Limite Freccia Netta Fin. L/ 350	: 5.832 mm
Freccia Finale	: -0.099 mm	Limite Freccia Finale L/ 300	: 6.804 mm
Fatt. sicurezza freccia Istantanea	: 74.583	Fatt. sicurezza freccia Netta Finale	: 59.193
Fatt. sicurezza freccia Finale	: 69.058	Fatt. sicurezza	: 59.193

Campata 91-14 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.214)

Sforzo Normale di Progetto [daN]	: 1345 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 29

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.93
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.058
fs	: 17.16
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.01
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.05
fs	: 19.9
Coefficiente di Sfruttamento	: 0.109
fs	: 9.21

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.009 (fs=117.232)

Taglio Ty di Progetto [daN]	: -22
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: -6

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.02
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.009
fs	: 117.23

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 47.47
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.76
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.81
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.91
Coefficiente di sfruttamento nel piano XY	: 0.122	Coefficiente di sfruttamento nel piano XZ	: 0.125
fs	: 7.981		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 21	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2055.6	Lunghezza efficace nel piano XZ	: 2055.6
Momento Critico nel piano XY	: 9530 daNm	Momento Critico nel piano XZ	: 9530 daNm
Tensione Critica nel piano XY	: 330.92 N/mm ²	Tensione Critica nel piano XZ	: 330.92 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.60 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.030	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.095		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.125	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.095
fs	: 7.981		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2055.6 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.056 mm	Limite Freccia Istantanea L/500	: 4.111 mm
Freccia Netta Finale	: -0.101 mm	Limite Freccia Netta Fin. L/ 350	: 5.873 mm
Freccia Finale	: -0.101 mm	Limite Freccia Finale L/ 300	: 6.852 mm
Fatt. sicurezza freccia Istantanea	: 73.029	Fatt. sicurezza freccia Netta Finale	: 57.959
Fatt. sicurezza freccia Finale	: 67.619	Fatt. sicurezza	: 57.959

Campata 71-15 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.254 (fs=3.936)

Sforzo Normale di Progetto [daN] : 5363 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : -12

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 3.72
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.232
 fs : 4.3
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 0.43
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.022
 fs : 46.31
 Coefficiente di Sfruttamento : 0.254
 fs : 3.94

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.005 (fs=202.03)

Taglio Ty di Progetto [daN] : -12
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : 10

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.01
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.005
 fs : 202.03

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 41.25	Snellezza nel piano XZ	: 47.14
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.287	Coefficiente di sfruttamento nel piano XZ	: 0.295
fs	: 3.388		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 42	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mm ²	Tensione Critica nel piano XZ	: 333.25 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.62 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.031	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.264		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.295	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.264
fs	: 3.388		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2041.2 mm	Schema adottato	Incastro-Cerniera
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.055 mm	Limite Freccia Istantanea L/500	: 4.082 mm
Freccia Netta Finale	: -0.099 mm	Limite Freccia Netta Fin. L/ 350	: 5.832 mm
Freccia Finale	: -0.099 mm	Limite Freccia Finale L/ 300	: 6.804 mm
Fatt. sicurezza freccia Istantanea	: 74.583	Fatt. sicurezza freccia Netta Finale	: 59.193
Fatt. sicurezza freccia Finale	: 69.058	Fatt. sicurezza	: 59.193

Campata 16-88 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.075 (fs=13.34)

Sforzo Normale di Progetto [daN]	: 736 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -25

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.51
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.032
fs	: 31.36
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.86
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.043
fs	: 23.21
Coefficiente di Sfruttamento	: 0.075
fs	: 13.34

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.005 (fs=208.939)

Taglio Ty di Progetto [daN]	: 7
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: -18

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.005
fs	: 208.94

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.25	Snellezza nel piano XZ	: 58.92
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 1
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.97
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.82
Coefficiente di sfruttamento nel piano XY	: 0.096	Coefficiente di sfruttamento nel piano XZ	: 0.104
fs	: 9.657		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mm ²	Tensione Critica nel piano XZ	: 333.25 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 12.74 N/mm ²
Tensione fless. piano XY	: 0.63 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.049	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.054		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.104	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.054
fs	: 9.657		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2041.2 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.132 mm	Limite Freccia Istantanea L/500	: 4.082 mm
Freccia Netta Finale	: -0.237 mm	Limite Freccia Netta Fin. L/ 350	: 5.832 mm
Freccia Finale	: -0.237 mm	Limite Freccia Finale L/ 300	: 6.804 mm
Fatt. sicurezza freccia Istantanea	: 30.962	Fatt. sicurezza freccia Netta Finale	: 24.573
Fatt. sicurezza freccia Finale	: 28.669	Fatt. sicurezza	: 24.573

Campata 17-72 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.278 (fs=3.603)

Sforzo Normale di Progetto [daN]	: 5863 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -14

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 4.07
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.254
fs	: 3.94
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.47
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.023
fs	: 42.7
Coefficiente di Sfruttamento	: 0.278
fs	: 3.6

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.007 (fs=148.843)

Taglio Ty di Progetto [daN]	: 17
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 3

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.007
fs	: 148.84

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.285	Coefficiente di sfruttamento nel piano XZ	: 0.322
fs	: 3.102		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.36 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.018	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.304		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.322	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.304
fs	: 3.102		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m

Carico distribuito Istantaneo	: -6.0 daN/m	-	Carico distribuito Finale	: -6.0 daN/m
-			Comb 42 [CAR] [ST]	
Freccia Istantanea - COMBINAZIONE			Comb 2 [SLEQP] [LT]	
Freccia Finale - COMBINAZIONE			Modulo Elastico finale	: 6388.9 N/mm ²
Modulo Elastico istantaneo	: 11500.0 N/mm ²			
Controfreccia	: 0.000 mm			
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm	
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm	
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm	
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419	
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419	

Campata 87-18 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.069 (fs=14.472)

Sforzo Normale di Progetto [daN]	: -1812 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -3

Tipo Verifica : COMPRESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -1.26
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.069
fs	: 14.47

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.007 (fs=138.799)

Taglio Ty di Progetto [daN]	: -18
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 23

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.007
fs	: 138.8

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 46.01
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.73
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 38
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.106	Coefficiente di sfruttamento nel piano XZ	: 0.108
fs	: 9.253		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 38	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.70 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.035	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.073		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.108	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.073
fs	: 9.253		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto			
Lunghezza elemento	: 1992.5 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.050 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.089 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.089 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 80.186	Fatt. sicurezza freccia Netta Finale	: 63.640
Fatt. sicurezza freccia Finale	: 74.246	Fatt. sicurezza	: 63.640

Campata 72-19 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 6 - [X=1660.4 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 25 [SLD] [IN] " - Coeff. Sfruttamento : 0.268 (fs=3.736)

Sforzo Normale di Progetto [daN]	: 5657 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 1
Momento Flettente Mz di Progetto [daNm]	: 13

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 3.93
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.245
fs	: 4.08
Tensione di Progetto relativa a My [N/mm ²]	: 0.02
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.44
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.022
fs	: 44.47
Coefficiente di Sfruttamento	: 0.268
fs	: 3.74

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.007 (fs=150.284)

Taglio Ty di Progetto [daN] : -17
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : -5

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.007
 fs : 150.28

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 46.01
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.73
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.311	Coefficiente di sfruttamento nel piano XZ	: 0.318
fs	: 3.140		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 42	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm²	Tensione Critica nel piano XZ	: 341.39 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 0.59 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.029	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.289		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.318	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.289
fs	: 3.140		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.050 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.089 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.089 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 80.186	Fatt. sicurezza freccia Netta Finale	: 63.640
Fatt. sicurezza freccia Finale	: 74.246	Fatt. sicurezza	: 63.640

Campata 20-87 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

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L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.077 (fs=12.911)

Sforzo Normale di Progetto [daN] : 331 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 0
Momento Flettente Mz di Progetto [daNm] : -36

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.23
Tensione Resistente [N/mm²] : 16.02
Coefficiente di Sfruttamento a trazione : 0.014
fs : 69.7
Tensione di Progetto relativa a My [N/mm²] : 0
Tensione di Progetto relativa a Mz [N/mm²] : 1.26
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.063
fs : 15.85
Coefficiente di Sfruttamento : 0.077
fs : 12.91

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.008 (fs=125.788)

Taglio Ty di Progetto [daN] : 20
Taglio Tz di Progetto [daN] : -2
Momento Torcente Mt di Progetto [daNm] : -40

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.008
fs : 125.79

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.109	Coefficiente di sfruttamento nel piano XZ	: 0.118
fs	: 8.506		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 21	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.02 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27

Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.051	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.066		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.118	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.066
fs	: 8.506		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 21-73 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.298 (fs=3.357)

Sforzo Normale di Progetto [daN]	: 6285 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 15

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 4.36
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.272
fs	: 3.67
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.51
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.026
fs	: 39.19
Coefficiente di Sfruttamento	: 0.298
fs	: 3.36

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.01 (fs=100.128)

Taglio Ty di Progetto [daN]	: 25
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -30

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.03
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.01
f_s	: 100.13

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.334	Coefficiente di sfruttamento nel piano XZ	: 0.375
f_s	: 2.666		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.77 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.038	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.337		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.375	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.337
f_s	: 2.666		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 86-22 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 5 - [X=1328.32 mm / 1992.49 mm] - **R 120x120**
 Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.081 ($f_s=12.4$)

Sforzo Normale di Progetto [daN] : -2114 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 1
 Momento Flettente Mz di Progetto [daNm] : -4

Tipo Verifica : COMPRESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -1.47
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.081
 fs : 12.4

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.009 (fs=106.828)

Taglio Ty di Progetto [daN] : -24
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : 20

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.009
 fs : 106.83

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 46.01
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.73
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 38
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.127	Coefficiente di sfruttamento nel piano XZ	: 0.129
fs	: 7.751		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 38	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.86 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.043	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.086		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.129	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.086
fs	: 7.751		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1992.5 mm
 Comb. di carico più gravosa : 142
 Carico distribuito Istantaneo : -6.0 daN/m
 -
 Freccia Istantanea - COMBINAZIONE

Schema adottato Incastro-Cerniera
 Peso proprio : -5.5 daN/m
 -
 Carico distribuito Finale : -6.0 daN/m
 Comb 42 [CAR] [ST]

Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.050 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.089 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.089 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 80.186	Fatt. sicurezza freccia Netta Finale	: 63.640
Fatt. sicurezza freccia Finale	: 74.246	Fatt. sicurezza	: 63.640

Campata 73-23 Primo [Asta GEN.]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.285 (fs=3.509)

Sforzo Normale di Progetto [daN]	: 5664 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 23

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 3.93
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.245
fs	: 4.07
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.79
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.04
fs	: 25.3
Coefficiente di Sfruttamento	: 0.285
fs	: 3.51

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.007 (fs=136.448)

Taglio Ty di Progetto [daN]	: -19
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -4

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.007
fs	: 136.45

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 46.01
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.73
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 50
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.315	Coefficiente di sfruttamento nel piano XZ	: 0.322

fs : 3.102

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 50	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.84 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.042	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.281		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.322	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.281
fs	: 3.102		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.050 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.089 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.089 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 80.186	Fatt. sicurezza freccia Netta Finale	: 63.640
Fatt. sicurezza freccia Finale	: 74.246	Fatt. sicurezza	: 63.640

Campata 24-86 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE GL24h (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - R 120x120 - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - R 120x120

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.079 (fs=12.681)

Sforzo Normale di Progetto [daN]	: 471 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -34

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.33
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.02
fs	: 49.02
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.17
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.058
fs	: 17.11

Coefficiente di Sfruttamento : 0.079
fs : 12.68

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**
Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.008 (fs=126.532)
Taglio Ty di Progetto [daN] : 20
Taglio Tz di Progetto [daN] : -2
Momento Torcente Mt di Progetto [daNm] : -41

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.008
fs : 126.53

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 29
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.109	Coefficiente di sfruttamento nel piano XZ	: 0.118
fs	: 8.494		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 29	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm²	Tensione Critica nel piano XZ	: 341.39 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 0.86 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.043	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.075		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.118	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.075
fs	: 8.494		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1992.5 mm
Comb. di carico più gravosa : 142
Carico distribuito Istantaneo : -6.0 daN/m
-
Freccia Istantanea - COMBINAZIONE
Freccia Finale - COMBINAZIONE
Modulo Elastico istantaneo : 11500.0 N/mm²
Controfreccia : 0.000 mm
Freccia Istantanea : -0.120 mm
Freccia Netta Finale : -0.215 mm
Freccia Finale : -0.215 mm
Fatt. sicurezza freccia Istantanea : 33.288

Schema adottato Doppia Cerniera
Peso proprio : -5.5 daN/m
-
Carico distribuito Finale : -6.0 daN/m
Comb 42 [CAR] [ST]
Comb 2 [SLEQP] [LT]
Modulo Elastico finale : 6388.9 N/mm²
Limite Freccia Istantanea L/500 : 3.985 mm
Limite Freccia Netta Fin. L/ 350 : 5.693 mm
Limite Freccia Finale L/ 300 : 6.642 mm
Fatt. sicurezza freccia Netta Finale : 26.419

Fatt. sicurezza freccia Finale : 30.822

Fatt. sicurezza : 26.419

Campata 25-74 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2063.23 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2063.23 mm / 2063.23 mm] - **R 120x120**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.343 (fs=2.914)

Sforzo Normale di Progetto [daN] : 7446 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : 0

Momento Flettente Mz di Progetto [daNm] : 12

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 5.17

Tensione Resistente [N/mm²] : 16.02

Coefficiente di Sfruttamento a trazione : 0.323

fs : 3.1

Tensione di Progetto relativa a My [N/mm²] : 0

Tensione di Progetto relativa a Mz [N/mm²] : 0.41

Tensione Resistente relativa a My [N/mm²] : 20.03

Tensione Resistente relativa a Mz [N/mm²] : 20.03

Coefficiente di Sfruttamento a flessione : 0.02

fs : 48.95

Coefficiente di Sfruttamento : 0.343

fs : 2.91

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2063.23 mm / 2063.23 mm] - **R 120x120**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.011 (fs=89.212)

Taglio Ty di Progetto [daN] : 28

Taglio Tz di Progetto [daN] : -3

Momento Torcente Mt di Progetto [daNm] : -37

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03

Tensione di Progetto relativa a Tz [N/mm²] : 0.00

Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a taglio : 0.011

fs : 89.21

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.69	Snellezza nel piano XZ	: 59.56
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.95
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 33
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.98
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.81
Coefficiente di sfruttamento nel piano XY	: 0.375	Coefficiente di sfruttamento nel piano XZ	: 0.431
fs	: 2.319		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2063.2	Lunghezza efficace nel piano XZ	: 2063.2

Momento Critico nel piano XY	: 9495 daNm	Momento Critico nel piano XZ	: 9495 daNm
Tensione Critica nel piano XY	: 329.69 N/mm ²	Tensione Critica nel piano XZ	: 329.69 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.65 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.032	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.399		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.431	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.399
fs	: 2.319		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto			
Lunghezza elemento	: 2063.2 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.138 mm	Limite Freccia Istantanea L/500	: 4.126 mm
Freccia Netta Finale	: -0.248 mm	Limite Freccia Netta Fin. L/ 350	: 5.895 mm
Freccia Finale	: -0.248 mm	Limite Freccia Finale L/ 300	: 6.877 mm
Fatt. sicurezza freccia Istantanea	: 29.980	Fatt. sicurezza freccia Netta Finale	: 23.794
Fatt. sicurezza freccia Finale	: 27.759	Fatt. sicurezza	: 23.794

Campata 85-26 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.083 (fs=12.095)

Sforzo Normale di Progetto [daN]	: -2168 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -1.51
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.083
fs	: 12.1

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.01 (fs=101.007)

Taglio Ty di Progetto [daN]	: -25
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 17

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66

Coefficiente di Sfruttamento a taglio : 0.01
fs : 101.01

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 46.01
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.73
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.125	Coefficiente di sfruttamento nel piano XZ	: 0.127
fs	: 7.878		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.22 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.061	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.066		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.127	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.066
fs	: 7.878		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.050 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.089 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.089 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 80.186	Fatt. sicurezza freccia Netta Finale	: 63.640
Fatt. sicurezza freccia Finale	: 74.246	Fatt. sicurezza	: 63.640

Campata 27-85 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.084 (fs=11.88)

Sforzo Normale di Progetto [daN]	: -479 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -48

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.33
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.018
fs	: 54.74
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.68
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.084
fs	: 11.93
Coefficiente di Sfruttamento a pressoflessione	: 0.084
fs	: 11.88

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**
Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.01 (fs=100.186)

Taglio Ty di Progetto [daN]	: 25
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -48

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.01
fs	: 100.19

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.138	Coefficiente di sfruttamento nel piano XZ	: 0.147
fs	: 6.811		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.49 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.074	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.072		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.147	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.072
fs	: 6.811		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)
 · Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 74-28 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2063.23 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2063.23 mm] - **R 120x120**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.368 (fs=2.717)

Sforzo Normale di Progetto [daN]	: 7324 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -29

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 5.09
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.317
fs	: 3.15
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.01
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.051
fs	: 19.77
Coefficiente di Sfruttamento	: 0.368
fs	: 2.72

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2063.23 mm / 2063.23 mm] - **R 120x120**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.011 (fs=88.895)

Taglio Ty di Progetto [daN]	: -29
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: -7

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.011
fs	: 88.9

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 41.69	Snellezza nel piano XZ	: 47.65

Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.76
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 26
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.81
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.91
Coefficiente di sfruttamento nel piano XY	: 0.376	Coefficiente di sfruttamento nel piano XZ	: 0.387
fs	: 2.586		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2063.2	Lunghezza efficace nel piano XZ	: 2063.2
Momento Critico nel piano XY	: 9495 daNm	Momento Critico nel piano XZ	: 9495 daNm
Tensione Critica nel piano XY	: 329.69 N/mm ²	Tensione Critica nel piano XZ	: 329.69 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.77 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.039	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.348		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.387	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.348
fs	: 2.586		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2063.2 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.057 mm	Limite Freccia Istantanea L/500	: 4.126 mm
Freccia Netta Finale	: -0.103 mm	Limite Freccia Netta Fin. L/ 350	: 5.895 mm
Freccia Finale	: -0.103 mm	Limite Freccia Finale L/ 300	: 6.877 mm
Fatt. sicurezza freccia Istantanea	: 72.218	Fatt. sicurezza freccia Netta Finale	: 57.316
Fatt. sicurezza freccia Finale	: 66.868	Fatt. sicurezza	: 57.316

Campata 84-29 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.099 (fs=10.119)

Sforzo Normale di Progetto [daN]	: 716 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 39

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.5
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.031
fs	: 32.24
Tensione di Progetto relativa a My [N/mm ²]	: 0

Tensione di Progetto relativa a M_z [N/mm ²]	: 1.36
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.068
f_s	: 14.75
Coefficiente di Sfruttamento	: 0.099
f_s	: 10.12

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**
Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.012 ($f_s=86.3$)

Taglio T_y di Progetto [daN]	: -29
Taglio T_z di Progetto [daN]	: -2
Momento Torcente M_t di Progetto [daNm]	: 15

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.03
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.012
f_s	: 86.3

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 46.01
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.73
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente K_c nel piano XY	: 0.95	Coefficiente K_c nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.145	Coefficiente di sfruttamento nel piano XZ	: 0.146
f_s	: 6.829		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.60 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.080	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.066		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.146	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.066
f_s	: 6.829		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale ($t > inf.$)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -6.0 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm ²

Schema adottato Incastro-Cerniera	
Peso proprio	: -5.5 daN/m
-	
Carico distribuito Finale	: -6.0 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [LT]	
Modulo Elastico finale	: 6388.9 N/mm ²

Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.050 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.089 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.089 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 80.186	Fatt. sicurezza freccia Netta Finale	: 63.640
Fatt. sicurezza freccia Finale	: 74.246	Fatt. sicurezza	: 63.640

Campata 31-84 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.089 (fs=11.178)

Sforzo Normale di Progetto [daN]	: 541 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 38

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.38
Tensione Resistente [N/mm²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.023
fs	: 42.61
Tensione di Progetto relativa a My [N/mm²]	: 0
Tensione di Progetto relativa a Mz [N/mm²]	: 1.32
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.066
fs	: 15.15
Coefficiente di Sfruttamento	: 0.089
fs	: 11.18

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.011 (fs=91.11)

Taglio Ty di Progetto [daN]	: 28
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -51

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.011
fs	: 91.11

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.141	Coefficiente di sfruttamento nel piano XZ	: 0.150
fs	: 6.678		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.57 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.078	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.072		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.150	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.072
fs	: 6.678		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 83-33 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.102 (fs=9.788)

Sforzo Normale di Progetto [daN]	: 785 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 39

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.55
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.034
fs	: 29.38
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.36
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.068
fs	: 14.68
Coefficiente di Sfruttamento	: 0.102
fs	: 9.79

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.012 (fs=82.322)

Taglio Ty di Progetto [daN]	: -31
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 13

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.012
fs	: 82.32

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 46.01
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.73
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.149	Coefficiente di sfruttamento nel piano XZ	: 0.151
fs	: 6.614		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mmq	Tensione Critica nel piano XZ	: 341.39 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 1.61 N/mmq	Tensione fless. piano XZ	: 0.00 N/mmq
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.080	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.071		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.151	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.071
fs	: 6.614		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.050 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.089 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.089 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 80.186	Fatt. sicurezza freccia Netta Finale	: 63.640
Fatt. sicurezza freccia Finale	: 74.246	Fatt. sicurezza	: 63.640

Campata 35-83 Primo [Asta GEN.]Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7**VERIFICHE EFFETTUATE CON ESITO POSITIVO****VERIFICHE DI RESISTENZA NORMALE**Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120***Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.112 (fs=8.89)*

Sforzo Normale di Progetto [daN] : 638 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : -49

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.44
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.028
 fs : 36.14
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 1.7
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.085
 fs : 11.79
 Coefficiente di Sfruttamento : 0.112
 fs : 8.89

VERIFICHE DI RESISTENZA TANGENZIALESezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120***Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.012 (fs=85.943)*

Taglio Ty di Progetto [daN] : 30
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : -49

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.012
 fs : 85.94

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.137	Coefficiente di sfruttamento nel piano XZ	: 0.147
fs	: 6.824		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 21	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²

Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.46 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.073	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.074		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.147	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.074
fs	: 6.824		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 82-37 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.106 (fs=9.466)

Sforzo Normale di Progetto [daN]	: 817 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 41

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.57
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.035
fs	: 28.24
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.41
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.07
fs	: 14.24
Coefficiente di Sfruttamento	: 0.106
fs	: 9.47

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.012 (fs=82.808)

Taglio Ty di Progetto [daN]	: -31
Taglio Tz di Progetto [daN]	: -2

Momento Torcente Mt di Progetto [daNm] : 5

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.012
 fs : 82.81

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 46.01
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.73
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.155	Coefficiente di sfruttamento nel piano XZ	: 0.157
fs	: 6.378		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm²	Tensione Critica nel piano XZ	: 341.39 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 1.65 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.082	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.074		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.157	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.074
fs	: 6.378		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.050 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.089 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.089 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 80.186	Fatt. sicurezza freccia Netta Finale	: 63.640
Fatt. sicurezza freccia Finale	: 74.246	Fatt. sicurezza	: 63.640

Campata 39-82 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.096 (fs=10.433)

Sforzo Normale di Progetto [daN] : 625 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : -40

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.43
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.027
 fs : 36.93
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 1.38
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.069
 fs : 14.54
 Coefficiente di Sfruttamento : 0.096
 fs : 10.43

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.011 (fs=87.798)

Taglio Ty di Progetto [daN] : 29
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : -42

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.011
 fs : 87.8

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.120	Coefficiente di sfruttamento nel piano XZ	: 0.129
fs	: 7.778		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 21	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm²	Tensione Critica nel piano XZ	: 341.39 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 1.13 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.057	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.072		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.129	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.072

fs : 7.778

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t>inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 78-43 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 34 [SLD] [IN] " - Coeff. Sfruttamento : 0.304 (fs=3.286)

Sforzo Normale di Progetto [daN]	: 6096 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 23

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 4.23
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.264
fs	: 3.78
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.8
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.04
fs	: 24.94
Coefficiente di Sfruttamento	: 0.304
fs	: 3.29

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.011 (fs=91.631)

Taglio Ty di Progetto [daN]	: 28
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.011

fs

: 91.63

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 46.01
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.73
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.324	Coefficiente di sfruttamento nel piano XZ	: 0.333
fs	: 3.007		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.44 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.022	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.311		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.333	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.311
fs	: 3.007		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.050 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.089 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.089 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 80.186	Fatt. sicurezza freccia Netta Finale	: 63.640
Fatt. sicurezza freccia Finale	: 74.246	Fatt. sicurezza	: 63.640

Campata 81-44 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.102 (fs=9.851)

Sforzo Normale di Progetto [daN]	: 831 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 38

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.58
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.036
fs	: 27.76
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.31
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.065
fs	: 15.27
Coefficiente di Sfruttamento	: 0.102
fs	: 9.85

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.011 (fs=90.185)

Taglio Ty di Progetto [daN]	: -28
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -2

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.011
fs	: 90.18

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 46.01
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.73
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.149	Coefficiente di sfruttamento nel piano XZ	: 0.151
fs	: 6.615		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.56 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.078	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.073		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.151	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.073
fs	: 6.615		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1992.5 mm

Schema adottato Incastro-Cerniera

Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.050 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.089 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.089 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 80.186	Fatt. sicurezza freccia Netta Finale	: 63.640
Fatt. sicurezza freccia Finale	: 74.246	Fatt. sicurezza	: 63.640

Campata 45-78 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.304 (fs=3.29)

Sforzo Normale di Progetto [daN]	: 6393 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -16

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 4.44
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.277
fs	: 3.61
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.54
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.027
fs	: 37.19
Coefficiente di Sfruttamento	: 0.304
fs	: 3.29

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.01 (fs=98.952)

Taglio Ty di Progetto [daN]	: -26
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 36

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.01
fs	: 98.95

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92

Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 50
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.312	Coefficiente di sfruttamento nel piano XZ	: 0.351
fs	: 2.850		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 50	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.57 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.029	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.322		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.351	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.322
fs	: 2.850		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 46-81 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.084 (fs=11.863)

Sforzo Normale di Progetto [daN]	: -2210 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -1.53
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.084
fs	: 11.86

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**
 Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.011 (fs=95.013)

Taglio Ty di Progetto [daN] : 27
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : -35

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.011
 fs : 95.01

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 29
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.111	Coefficiente di sfruttamento nel piano XZ	: 0.122
fs	: 8.187		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 29	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm²	Tensione Critica nel piano XZ	: 341.39 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 0.67 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.033	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.089		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.122	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.089
fs	: 8.187		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.298 (fs=3.356)

Sforzo Normale di Progetto [daN] : 6225 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 0
Momento Flettente Mz di Progetto [daNm] : -16

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 4.32
Tensione Resistente [N/mm²] : 16.02
Coefficiente di Sfruttamento a trazione : 0.27
fs : 3.71
Tensione di Progetto relativa a My [N/mm²] : 0
Tensione di Progetto relativa a Mz [N/mm²] : 0.56
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.028
fs : 35.51
Coefficiente di Sfruttamento : 0.298
fs : 3.36

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.008 (fs=121.015)

Taglio Ty di Progetto [daN] : 21
Taglio Tz di Progetto [daN] : -2
Momento Torcente Mt di Progetto [daNm] : 4

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.008
fs : 121.01

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 46.01
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.73
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.338	Coefficiente di sfruttamento nel piano XZ	: 0.346
fs	: 2.892		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mmq	Tensione Critica nel piano XZ	: 341.39 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 0.91 N/mmq	Tensione fless. piano XZ	: 0.00 N/mmq

Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.045	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.301		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.346	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.301
fs	: 2.892		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.050 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.089 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.089 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 80.186	Fatt. sicurezza freccia Netta Finale	: 63.640
Fatt. sicurezza freccia Finale	: 74.246	Fatt. sicurezza	: 63.640

Campata 80-48 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 3 - [X=664.16 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.084 (fs=11.897)

Sforzo Normale di Progetto [daN]	: 833 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 1
Momento Flettente Mz di Progetto [daNm]	: 27

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.58
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.036
fs	: 27.7
Tensione di Progetto relativa a My [N/mm ²]	: 0.03
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.94
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.048
fs	: 20.85
Coefficiente di Sfruttamento	: 0.084
fs	: 11.9

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.008 (fs=130.41)

Taglio Ty di Progetto [daN]	: -19
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -4

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.008
fs	: 130.41

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 46.01
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.73
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.127	Coefficiente di sfruttamento nel piano XZ	: 0.129
fs	: 7.765		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.08 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.054	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.075		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.129	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.075
fs	: 7.765		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.050 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.089 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.089 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 80.186	Fatt. sicurezza freccia Netta Finale	: 63.640
Fatt. sicurezza freccia Finale	: 74.246	Fatt. sicurezza	: 63.640

Campata 49-77 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.314 ($f_s=3.184$)
 Sforzo Normale di Progetto [daN] : 6502 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : 19

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 4.52
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.282
 f_s : 3.55
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 0.65
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.032
 f_s : 31.04
 Coefficiente di Sfruttamento : 0.314
 f_s : 3.18

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**
 Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.01 ($f_s=99.085$)

Taglio Ty di Progetto [daN] : -26
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : 32

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.01
 f_s : 99.08

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.317	Coefficiente di sfruttamento nel piano XZ	: 0.358
f_s	: 2.791		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 42	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.34 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.017	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.342		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.358	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.342
f_s	: 2.791		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 50-80 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.09 (fs=11.08)

Sforzo Normale di Progetto [daN]	: 1104 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -24

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.77
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.048
fs	: 20.9
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.85
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.042
fs	: 23.58
Coefficiente di Sfruttamento	: 0.09
fs	: 11.08

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.011 (fs=94.983)

Taglio Ty di Progetto [daN]	: 27
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -33

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.011
fs	: 94.98

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 37
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.109	Coefficiente di sfruttamento nel piano XZ	: 0.121
fs	: 8.249		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 37	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.49 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.025	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.097		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.121	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.097
fs	: 8.249		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 76-51 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.288 (fs=3.47)

Sforzo Normale di Progetto [daN]	: 6042 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -15

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 4.2
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Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.262
fs	: 3.82
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.53
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.026
fs	: 38
Coefficiente di Sfruttamento	: 0.288
fs	: 3.47

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.008 (fs=118.444)

Taglio Ty di Progetto [daN]	: 21
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 6

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.008
fs	: 118.44

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 46.01
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.73
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.329	Coefficiente di sfruttamento nel piano XZ	: 0.337
fs	: 2.968		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.80 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.040	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.297		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.337	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.297
fs	: 2.968		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	

-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.050 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.089 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.089 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 80.186	Fatt. sicurezza freccia Netta Finale	: 63.640
Fatt. sicurezza freccia Finale	: 74.246	Fatt. sicurezza	: 63.640

Campata 53-76 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1992.49 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 2 - [X=332.08 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.292 (fs=3.419)

Sforzo Normale di Progetto [daN]	: 6169 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 1
Momento Flettente Mz di Progetto [daNm]	: -14

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 4.28
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.267
fs	: 3.74
Tensione di Progetto relativa a My [N/mm ²]	: 0.02
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.49
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.025
fs	: 39.84
Coefficiente di Sfruttamento	: 0.292
fs	: 3.42

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1992.49 mm / 1992.49 mm] - **R 120x120**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.007 (fs=135.209)

Taglio Ty di Progetto [daN]	: -19
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 20

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.007
fs	: 135.21

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.26	Snellezza nel piano XZ	: 57.52
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 42
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95

Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.297	Coefficiente di sfruttamento nel piano XZ	: 0.336
fs	: 2.979		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 42	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1992.5	Lunghezza efficace nel piano XZ	: 1992.5
Momento Critico nel piano XY	: 9832 daNm	Momento Critico nel piano XZ	: 9832 daNm
Tensione Critica nel piano XY	: 341.39 N/mm ²	Tensione Critica nel piano XZ	: 341.39 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.45 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.022	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.313		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.336	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.313
fs	: 2.979		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1992.5 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.120 mm	Limite Freccia Istantanea L/500	: 3.985 mm
Freccia Netta Finale	: -0.215 mm	Limite Freccia Netta Fin. L/ 350	: 5.693 mm
Freccia Finale	: -0.215 mm	Limite Freccia Finale L/ 300	: 6.642 mm
Fatt. sicurezza freccia Istantanea	: 33.288	Fatt. sicurezza freccia Netta Finale	: 26.419
Fatt. sicurezza freccia Finale	: 30.822	Fatt. sicurezza	: 26.419

Campata 75-55 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.269 (fs=3.717)

Sforzo Normale di Progetto [daN]	: 5563 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -16

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 3.86
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.241
fs	: 4.15
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.56
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03

Coefficiente di Sfruttamento a flessione	: 0.028
fs	: 35.89
Coefficiente di Sfruttamento	: 0.269
fs	: 3.72

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.006 (fs=181.814)

Taglio Ty di Progetto [daN]	: 14
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -4

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.006
fs	: 181.81

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 41.25	Snellezza nel piano XZ	: 47.14
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.301	Coefficiente di sfruttamento nel piano XZ	: 0.309
fs	: 3.232		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mm²	Tensione Critica nel piano XZ	: 333.25 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 0.85 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.042	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.267		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.309	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.267
fs	: 3.232		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2041.2 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -6.0 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm²
Controfreccia	: 0.000 mm
Freccia Istantanea	: -0.055 mm
Freccia Netta Finale	: -0.099 mm

Schema adottato Incastro-Cerniera	
Peso proprio	: -5.5 daN/m
-	
Carico distribuito Finale	: -6.0 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [LT]	
Modulo Elastico finale	: 6388.9 N/mm²
Limite Freccia Istantanea L/500	: 4.082 mm
Limite Freccia Netta Fin. L/350	: 5.832 mm

Freccia Finale	: -0.099 mm	Limite Freccia Finale L/ 300	: 6.804 mm
Fatt. sicurezza freccia Istantanea	: 74.583	Fatt. sicurezza freccia Netta Finale	: 59.193
Fatt. sicurezza freccia Finale	: 69.058	Fatt. sicurezza	: 59.193

Campata 56-79 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 6 - [X=1700.99 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.079 (fs=12.592)

Sforzo Normale di Progetto [daN]	: -2082 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 1
Momento Flettente Mz di Progetto [daNm]	: 4

Tipo Verifica : COMPRESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -1.45
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.079
fs	: 12.59

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.005 (fs=221.262)

Taglio Ty di Progetto [daN]	: -7
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: 18

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.005
fs	: 221.26

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.25	Snellezza nel piano XZ	: 58.92
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 39
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.97
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.82
Coefficiente di sfruttamento nel piano XY	: 0.114	Coefficiente di sfruttamento nel piano XZ	: 0.126
fs	: 7.914		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 39	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mm²	Tensione Critica nel piano XZ	: 333.25 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 0.68 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000

Coefficiente sfrutt. nel piano XY	: 0.034	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.092		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.126	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.092
fs	: 7.914		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2041.2 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.132 mm	Limite Freccia Istantanea L/500	: 4.082 mm
Freccia Netta Finale	: -0.237 mm	Limite Freccia Netta Fin. L/ 350	: 5.832 mm
Freccia Finale	: -0.237 mm	Limite Freccia Finale L/ 300	: 6.804 mm
Fatt. sicurezza freccia Istantanea	: 30.962	Fatt. sicurezza freccia Netta Finale	: 24.573
Fatt. sicurezza freccia Finale	: 28.669	Fatt. sicurezza	: 24.573

Campata 57-75 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.284 (fs=3.516)

Sforzo Normale di Progetto [daN]	: 5400 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -29

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 3.75
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.234
fs	: 4.27
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.01
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.05
fs	: 19.87
Coefficiente di Sfruttamento	: 0.284
fs	: 3.52

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.009 (fs=109.381)

Taglio Ty di Progetto [daN]	: 23
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -30

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
---	--------

Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.009
fs	: 109.38

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellenza nel piano XY	: 41.25	Snellenza nel piano XZ	: 58.92
Snellenza relativa nel piano XY	: 0.66	Snellenza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 34
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.97
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.82
Coefficiente di sfruttamento nel piano XY	: 0.268	Coefficiente di sfruttamento nel piano XZ	: 0.301
fs	: 3.320		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato 1 (0 - 6)

Combinazione più sfavorevole	: 34	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mm ²	Tensione Critica nel piano XZ	: 333.25 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.13 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellenza relativa nel piano XY	: 0.27	Snellenza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.056	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.245		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.301	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.245
fs	: 3.320		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2041.2 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.132 mm	Limite Freccia Istantanea L/500	: 4.082 mm
Freccia Netta Finale	: -0.237 mm	Limite Freccia Netta Fin. L/ 350	: 5.832 mm
Freccia Finale	: -0.237 mm	Limite Freccia Finale L/ 300	: 6.804 mm
Fatt. sicurezza freccia Istantanea	: 30.962	Fatt. sicurezza freccia Netta Finale	: 24.573
Fatt. sicurezza freccia Finale	: 28.669	Fatt. sicurezza	: 24.573

Campata 57-93 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.112 (fs=8.958)

Sforzo Normale di Progetto [daN] : 1562 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : -25

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 1.08
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.068
 fs : 14.77
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 0.88
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.044
 fs : 22.77
 Coefficiente di Sfruttamento : 0.112
 fs : 8.96

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.009 (fs=117.341)

Taglio Ty di Progetto [daN] : -22
 Taglio Tz di Progetto [daN] : -3
 Momento Torcente Mt di Progetto [daNm] : -15

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.009
 fs : 117.34

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 59.34
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 17
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.98
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.81
Coefficiente di sfruttamento nel piano XY	: 0.130	Coefficiente di sfruttamento nel piano XZ	: 0.146
fs	: 6.832		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2055.6	Lunghezza efficace nel piano XZ	: 2055.6
Momento Critico nel piano XY	: 9530 daNm	Momento Critico nel piano XZ	: 9530 daNm
Tensione Critica nel piano XY	: 330.92 N/mm ²	Tensione Critica nel piano XZ	: 330.92 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.55 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.028	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.119		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.146	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.119
fs	: 6.832		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2055.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.136 mm	Limite Freccia Istantanea L/500	: 4.111 mm
Freccia Netta Finale	: -0.244 mm	Limite Freccia Netta Fin. L/ 350	: 5.873 mm
Freccia Finale	: -0.244 mm	Limite Freccia Finale L/ 300	: 6.852 mm
Fatt. sicurezza freccia Istantanea	: 30.317	Fatt. sicurezza freccia Netta Finale	: 24.061
Fatt. sicurezza freccia Finale	: 28.071	Fatt. sicurezza	: 24.061

Campata 93-58 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.199 (fs=5.015)

Sforzo Normale di Progetto [daN]	: 1301 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -83

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.9
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.056
fs	: 17.74
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.86
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.143
fs	: 6.99
Coefficiente di Sfruttamento	: 0.199
fs	: 5.01

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.01 (fs=95.982)

Taglio Ty di Progetto [daN]	: 26
Taglio Tz di Progetto [daN]	: 3
Momento Torcente Mt di Progetto [daNm]	: -22

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.01
fs	: 95.98

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 47.47
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.76
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 34
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.81
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.91
Coefficiente di sfruttamento nel piano XY	: 0.180	Coefficiente di sfruttamento nel piano XZ	: 0.182
fs	: 5.505		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 34	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2055.6	Lunghezza efficace nel piano XZ	: 2055.6
Momento Critico nel piano XY	: 9530 daNm	Momento Critico nel piano XZ	: 9530 daNm
Tensione Critica nel piano XY	: 330.92 N/mm ²	Tensione Critica nel piano XZ	: 330.92 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 2.65 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.132	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.050		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.182	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.050
fs	: 5.505		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2055.6 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.056 mm	Limite Freccia Istantanea L/500	: 4.111 mm
Freccia Netta Finale	: -0.101 mm	Limite Freccia Netta Fin. L/ 350	: 5.873 mm
Freccia Finale	: -0.101 mm	Limite Freccia Finale L/ 300	: 6.852 mm
Fatt. sicurezza freccia Istantanea	: 73.029	Fatt. sicurezza freccia Netta Finale	: 57.959
Fatt. sicurezza freccia Finale	: 67.619	Fatt. sicurezza	: 57.959

Campata 61-95 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2002.62 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.12 (fs=8.356)

Sforzo Normale di Progetto [daN]	: 1152 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -40

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.8
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.05

fs	: 20.02
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.4
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.07
fs	: 14.34
Coefficiente di Sfruttamento	: 0.12
fs	: 8.36

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.008 (fs=123.181)

Taglio Ty di Progetto [daN]	: 21
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -40

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.008
fs	: 123.18

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 57.81
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.119	Coefficiente di sfruttamento nel piano XZ	: 0.132
fs	: 7.591		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2002.6	Lunghezza efficace nel piano XZ	: 2002.6
Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm
Tensione Critica nel piano XY	: 339.67 N/mm ²	Tensione Critica nel piano XZ	: 339.67 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.53 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.027	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.105		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.132	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.105
fs	: 7.591		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2002.6 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -6.0 daN/m
-	
Freccia Istantanea - COMBINAZIONE	

Schema adottato Doppia Cerniera	
Peso proprio	: -5.5 daN/m
-	
Carico distribuito Finale	: -6.0 daN/m
Comb 42 [CAR] [ST]	

Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.122 mm	Limite Freccia Istantanea L/500	: 4.005 mm
Freccia Netta Finale	: -0.220 mm	Limite Freccia Netta Fin. L/ 350	: 5.722 mm
Freccia Finale	: -0.220 mm	Limite Freccia Finale L/ 300	: 6.675 mm
Fatt. sicurezza freccia Istantanea	: 32.785	Fatt. sicurezza freccia Netta Finale	: 26.020
Fatt. sicurezza freccia Finale	: 30.357	Fatt. sicurezza	: 26.020

Campata 95-62 Primo [Asta GEN.]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 2002.62 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.112 ($f_s=8.94$)

Sforzo Normale di Progetto [daN]	: 1719 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 22

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1.19
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.075
f_s	: 13.42
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.75
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.037
f_s	: 26.78
Coefficiente di Sfruttamento	: 0.112
f_s	: 8.94

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.008 ($f_s=120.4$)

Taglio Ty di Progetto [daN]	: -21
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -16

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.008
f_s	: 120.4

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 46.25
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.74
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.150	Coefficiente di sfruttamento nel piano XZ	: 0.152

fs : 6.575

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2002.6	Lunghezza efficace nel piano XZ	: 2002.6
Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm
Tensione Critica nel piano XY	: 339.67 N/mm ²	Tensione Critica nel piano XZ	: 339.67 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.61 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.081	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.071		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.152	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.071
fs	: 6.575		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2002.6 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.051 mm	Limite Freccia Istantanea L/500	: 4.005 mm
Freccia Netta Finale	: -0.091 mm	Limite Freccia Netta Fin. L/ 350	: 5.722 mm
Freccia Finale	: -0.091 mm	Limite Freccia Finale L/ 300	: 6.675 mm
Fatt. sicurezza freccia Istantanea	: 78.975	Fatt. sicurezza freccia Netta Finale	: 62.678
Fatt. sicurezza freccia Finale	: 73.125	Fatt. sicurezza	: 62.678

Campata 96-65 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE GL24h (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 2002.62 mm - R 120x120 - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2002.62 mm] - R 120x120

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.112 (fs=8.939)

Sforzo Normale di Progetto [daN]	: 1082 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 37

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.75
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.047
fs	: 21.32
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.3
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.065
fs	: 15.39

Coefficiente di Sfruttamento : 0.112
fs : 8.94

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**
Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.01 (fs=103.572)

Taglio Ty di Progetto [daN] : -25
Taglio Tz di Progetto [daN] : -2
Momento Torcente Mt di Progetto [daNm] : 20

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.01
fs : 103.57

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 46.25
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.74
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.79
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.120	Coefficiente di sfruttamento nel piano XZ	: 0.122
fs	: 8.190		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 9	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2002.6	Lunghezza efficace nel piano XZ	: 2002.6
Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm
Tensione Critica nel piano XY	: 339.67 N/mm²	Tensione Critica nel piano XZ	: 339.67 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 0.83 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.041	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.081		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.122	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.081
fs	: 8.190		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 2002.6 mm
Comb. di carico più gravosa : 142
Carico distribuito Istantaneo : -6.0 daN/m
-
Freccia Istantanea - COMBINAZIONE
Freccia Finale - COMBINAZIONE
Modulo Elastico istantaneo : 11500.0 N/mm²
Controfreccia : 0.000 mm
Freccia Istantanea : -0.051 mm
Freccia Netta Finale : -0.091 mm
Freccia Finale : -0.091 mm
Fatt. sicurezza freccia Istantanea : 78.975

Schema adottato Incastro-Cerniera
Peso proprio : -5.5 daN/m
-
Carico distribuito Finale : -6.0 daN/m
Comb 42 [CAR] [ST]
Comb 2 [SLEQP] [LT]
Modulo Elastico finale : 6388.9 N/mm²
Limite Freccia Istantanea L/500 : 4.005 mm
Limite Freccia Netta Fin. L/350 : 5.722 mm
Limite Freccia Finale L/300 : 6.675 mm
Fatt. sicurezza freccia Netta Finale : 62.678

Fatt. sicurezza freccia Finale : 73.125 Fatt. sicurezza : 62.678

Campata 66-96 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 2002.62 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 2 - [X=333.77 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.098 (fs=10.188)

Sforzo Normale di Progetto [daN] : 1798 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 1
Momento Flettente Mz di Progetto [daNm] : -11

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 1.25
Tensione Resistente [N/mm²] : 16.02
Coefficiente di Sfruttamento a trazione : 0.078
fs : 12.83
Tensione di Progetto relativa a My [N/mm²] : 0.02
Tensione di Progetto relativa a Mz [N/mm²] : 0.39
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.02
fs : 49.49
Coefficiente di Sfruttamento : 0.098
fs : 10.19

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2002.62 mm / 2002.62 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.007 (fs=142.619)

Taglio Ty di Progetto [daN] : -18
Taglio Tz di Progetto [daN] : -2
Momento Torcente Mt di Progetto [daNm] : 24

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.007
fs : 142.62

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 40.47	Snellezza nel piano XZ	: 57.81
Snellezza relativa nel piano XY	: 0.64	Snellezza relativa nel piano XZ	: 0.92
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 14
Coefficiente K nel piano XY	: 0.72	Coefficiente K nel piano XZ	: 0.95
Coefficiente Kc nel piano XY	: 0.95	Coefficiente Kc nel piano XZ	: 0.83
Coefficiente di sfruttamento nel piano XY	: 0.110	Coefficiente di sfruttamento nel piano XZ	: 0.123
fs	: 8.098		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 14 Sezione più sfavorevole : 2
Lunghezza efficace nel piano XY : 2002.6 Lunghezza efficace nel piano XZ : 2002.6

Momento Critico nel piano XY	: 9782 daNm	Momento Critico nel piano XZ	: 9782 daNm
Tensione Critica nel piano XY	: 339.67 N/mm ²	Tensione Critica nel piano XZ	: 339.67 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.37 N/mm ²	Tensione fless. piano XZ	: 0.02 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.019	Coefficiente sfrutt. nel piano XZ	: 0.001
Coeff. sfrutt. max euleriano	: 0.104		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.123	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.105
fs	: 8.144		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2002.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.122 mm	Limite Freccia Istantanea L/500	: 4.005 mm
Freccia Netta Finale	: -0.220 mm	Limite Freccia Netta Fin. L/ 350	: 5.722 mm
Freccia Finale	: -0.220 mm	Limite Freccia Finale L/ 300	: 6.675 mm
Fatt. sicurezza freccia Istantanea	: 32.785	Fatt. sicurezza freccia Netta Finale	: 26.020
Fatt. sicurezza freccia Finale	: 30.357	Fatt. sicurezza	: 26.020

Campata 69-94 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.164)

Sforzo Normale di Progetto [daN]	: 1682 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -21

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1.17
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.073
fs	: 13.72
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.73
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.036
fs	: 27.61
Coefficiente di Sfruttamento	: 0.109
fs	: 9.16

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2055.56 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.006 (fs=167.194)

TABULATI DI CALCOLO -

Taglio Ty di Progetto [daN]	: -15
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: 8

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.006
fs	: 167.19

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 59.34
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.94
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.98
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.81
Coefficiente di sfruttamento nel piano XY	: 0.092	Coefficiente di sfruttamento nel piano XZ	: 0.104
fs	: 9.627		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2055.6	Lunghezza efficace nel piano XZ	: 2055.6
Momento Critico nel piano XY	: 9530 daNm	Momento Critico nel piano XZ	: 9530 daNm
Tensione Critica nel piano XY	: 330.92 N/mm ²	Tensione Critica nel piano XZ	: 330.92 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.43 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.021	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.083		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.104	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.083
fs	: 9.627		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2055.6 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.136 mm	Limite Freccia Istantanea L/500	: 4.111 mm
Freccia Netta Finale	: -0.244 mm	Limite Freccia Netta Fin. L/ 350	: 5.873 mm
Freccia Finale	: -0.244 mm	Limite Freccia Finale L/ 300	: 6.852 mm
Fatt. sicurezza freccia Istantanea	: 30.317	Fatt. sicurezza freccia Netta Finale	: 24.061
Fatt. sicurezza freccia Finale	: 28.071	Fatt. sicurezza	: 24.061

Campata 79-70 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 2041.18 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2041.18 mm] - **R 120x120**
Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.108 (fs=9.24)
 Sforzo Normale di Progetto [daN] : 1401 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : -27

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.97
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.061
 fs : 16.47
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 0.95
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.048
 fs : 21.05
 Coefficiente di Sfruttamento : 0.108
 fs : 9.24

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2041.18 mm / 2041.18 mm] - **R 120x120**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.007 (fs=151.179)
 Taglio Ty di Progetto [daN] : -17
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : 14

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.007
 fs : 151.18

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 41.25	Snellezza nel piano XZ	: 47.14
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.75
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 37
Coefficiente K nel piano XY	: 0.73	Coefficiente K nel piano XZ	: 0.80
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.92
Coefficiente di sfruttamento nel piano XY	: 0.082	Coefficiente di sfruttamento nel piano XZ	: 0.084
fs	: 11.911		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 37	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 2041.2	Lunghezza efficace nel piano XZ	: 2041.2
Momento Critico nel piano XY	: 9598 daNm	Momento Critico nel piano XZ	: 9598 daNm
Tensione Critica nel piano XY	: 333.25 N/mmq	Tensione Critica nel piano XZ	: 333.25 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 0.37 N/mmq	Tensione fless. piano XZ	: 0.04 N/mmq
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.018	Coefficiente sfrutt. nel piano XZ	: 0.002

Coeff. sfrutt. max euleriano	: 0.064	
Coeff. sfrutt. TOTALE (Piano XY)	: 0.082	Coeff. sfrutt. TOTALE (Piano XZ) : 0.066
fs	: 12.126	

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2041.2 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.055 mm	Limite Freccia Istantanea L/500	: 4.082 mm
Freccia Netta Finale	: -0.099 mm	Limite Freccia Netta Fin. L/ 350	: 5.832 mm
Freccia Finale	: -0.099 mm	Limite Freccia Finale L/ 300	: 6.804 mm
Fatt. sicurezza freccia Istantanea	: 74.583	Fatt. sicurezza freccia Netta Finale	: 59.193
Fatt. sicurezza freccia Finale	: 69.058	Fatt. sicurezza	: 59.193

Campata 94-70 Primo [Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2055.56 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 2 - [X=342.59 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.085 (fs=11.785)

Sforzo Normale di Progetto [daN]	: 1414 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 1
Momento Flettente Mz di Progetto [daNm]	: 13

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.98
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.061
fs	: 16.32
Tensione di Progetto relativa a My [N/mm ²]	: 0.02
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.45
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.024
fs	: 42.42
Coefficiente di Sfruttamento	: 0.085
fs	: 11.79

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 2055.56 mm] - **R 120x120**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.008 (fs=131.649)

Taglio Ty di Progetto [daN]	: 19
Taglio Tz di Progetto [daN]	: 3
Momento Torcente Mt di Progetto [daNm]	: 18

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00

Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.008
fs	: 131.65

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 41.54	Snellezza nel piano XZ	: 47.47
Snellezza relativa nel piano XY	: 0.66	Snellezza relativa nel piano XZ	: 0.76
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.74	Coefficiente K nel piano XZ	: 0.81
Coefficiente Kc nel piano XY	: 0.94	Coefficiente Kc nel piano XZ	: 0.91
Coefficiente di sfruttamento nel piano XY	: 0.130	Coefficiente di sfruttamento nel piano XZ	: 0.133
fs	: 7.507		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 2
Lunghezza efficace nel piano XY	: 2055.6	Lunghezza efficace nel piano XZ	: 2055.6
Momento Critico nel piano XY	: 9530 daNm	Momento Critico nel piano XZ	: 9530 daNm
Tensione Critica nel piano XY	: 330.92 N/mm ²	Tensione Critica nel piano XZ	: 330.92 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.68 N/mm ²	Tensione fless. piano XZ	: 0.02 N/mm ²
Snellezza relativa nel piano XY	: 0.27	Snellezza relativa nel piano XZ	: 0.27
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.034	Coefficiente sfrutt. nel piano XZ	: 0.001
Coeff. sfrutt. max euleriano	: 0.098		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.132	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.100
fs	: 7.556		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2055.6 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [LT]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.056 mm	Limite Freccia Istantanea L/500	: 4.111 mm
Freccia Netta Finale	: -0.101 mm	Limite Freccia Netta Fin. L/ 350	: 5.873 mm
Freccia Finale	: -0.101 mm	Limite Freccia Finale L/ 300	: 6.852 mm
Fatt. sicurezza freccia Istantanea	: 73.029	Fatt. sicurezza freccia Netta Finale	: 57.959
Fatt. sicurezza freccia Finale	: 67.619	Fatt. sicurezza	: 57.959

Campata 1-2 Copertur[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1662.44 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1662.44 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.134 (fs=7.462)

Sforzo Normale di Progetto [daN]	: -3967 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -905

Momento Flettente Mz di Progetto [daNm] : -3590

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.11
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.006
 fs : 171.66
 Tensione di Progetto relativa a My [N/mm²] : 0.09
 Tensione di Progetto relativa a Mz [N/mm²] : 2.62
 Tensione Resistente relativa a My [N/mm²] : 18.21
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.134
 fs : 7.46
 Coefficiente di Sfruttamento a pressoflessione : 0.134
 fs : 7.46

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1662.44 mm / 1662.44 mm] - **R 220x1700**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.133 (fs=7.546)

Taglio Ty di Progetto [daN] : 55
 Taglio Tz di Progetto [daN] : -641
 Momento Torcente Mt di Progetto [daNm] : 168

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
 Tensione di Progetto relativa a Tz [N/mm²] : 0.03
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.01
 fs : 102.82
 Tensione di Progetto [N/mm²] : 0.7
 Modulo di resistenza a torsione [mm³] : 25450510
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.132
 fs : 7.55
 Coefficiente di Sfruttamento a taglio+torsione : 0.133
 fs : 7.55

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1662.4	Lunghezza efficace nel piano XZ	: 1662.4
Momento Critico nel piano XY	: 9685836 daNm	Momento Critico nel piano XZ	: 1253461 daNm
Tensione Critica nel piano XY	: 7063.08 N/mm ²	Tensione Critica nel piano XZ	: 118.29 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.62 N/mm ²	Tensione fless. piano XZ	: 0.09 N/mm ²
Snellezza relativa nel piano XY	: 0.06	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.131	Coefficiente sfrutt. nel piano XZ	: 0.005
Coeff. sfrutt. max euleriano	: 0.006		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.137	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.011
fs	: 7.325		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1662.4 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	

-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.325 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.750 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.541 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 15-1 Copertu[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1590 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1590 mm / 1590 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.165 (fs=6.047)

Sforzo Normale di Progetto [daN]	: 1500 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 8793
Momento Flettente Mz di Progetto [daNm]	: -3590

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.04
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.003
fs	: 363.09
Tensione di Progetto relativa a My [N/mm ²]	: 0.83
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.62
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.163
fs	: 6.15
Coefficiente di Sfruttamento	: 0.165
fs	: 6.05

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1590 mm / 1590 mm] - **R 220x1700**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.098 (fs=10.194)

Taglio Ty di Progetto [daN]	: 93
Taglio Tz di Progetto [daN]	: -1698
Momento Torcente Mt di Progetto [daNm]	: -99

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.07
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.04
fs	: 24.77
Tensione di Progetto [N/mm ²]	: 0.33
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a torsione	: 0.096
fs	: 10.37
Coefficiente di Sfruttamento a taglio+torsione	: 0.098
fs	: 10.19

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1590.0	Lunghezza efficace nel piano XZ	: 1590.0
Momento Critico nel piano XY	: 10127108 daNm	Momento Critico nel piano XZ	: 1310567 daNm
Tensione Critica nel piano XY	: 7384.86 N/mm ²	Tensione Critica nel piano XZ	: 123.68 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.62 N/mm ²	Tensione fless. piano XZ	: 0.83 N/mm ²
Snellezza relativa nel piano XY	: 0.06	Snellezza relativa nel piano XZ	: 0.44
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.131	Coefficiente sfrutt. nel piano XZ	: 0.046
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.131	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.046
fs	: 7.650		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1590.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.180 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.543 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.300 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 2-3 Copertur[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.095 (fs=10.492)

Sforzo Normale di Progetto [daN]	: 212 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -2725
Momento Flettente Mz di Progetto [daNm]	: 2335

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.01
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.000
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 0.26
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.7
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.095
fs	: 10.54
Coefficiente di Sfruttamento	: 0.095
fs	: 10.49

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.032 (fs=31.542)

Taglio Ty di Progetto [daN] : -1342
 Taglio Tz di Progetto [daN] : 440
 Momento Torcente Mt di Progetto [daNm] : -1765

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.05
 Tensione di Progetto relativa a Tz [N/mm²] : 0.02
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.021
 fs : 46.87
 Tensione di Progetto [N/mm²] : 0.17
 Modulo di resistenza a torsione [mm³] : 25450510
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.031
 fs : 32
 Coefficiente di Sfruttamento a taglio+torsione : 0.032
 fs : 31.54

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm²	Tensione Critica nel piano XZ	: 142.50 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 1.70 N/mm²	Tensione fless. piano XZ	: 0.26 N/mm²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.085	Coefficiente sfrutt. nel piano XZ	: 0.014
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.085	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.014
fs	: 11.760		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 3-4 Copertur[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
 L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.095 (fs=10.504)

Sforzo Normale di Progetto [daN] : 109 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : -2745
Momento Flettente Mz di Progetto [daNm] : 2336

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.00
Tensione Resistente [N/mm²] : 14.57
Coefficiente di Sfruttamento a trazione : 0.000
fs : 1000
Tensione di Progetto relativa a My [N/mm²] : 0.26
Tensione di Progetto relativa a Mz [N/mm²] : 1.7
Tensione Resistente relativa a My [N/mm²] : 18.21
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.095
fs : 10.53
Coefficiente di Sfruttamento : 0.095
fs : 10.5

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.019 (fs=54.024)

Taglio Ty di Progetto [daN] : -649
Taglio Tz di Progetto [daN] : 1039
Momento Torcente Mt di Progetto [daNm] : 558

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
Tensione di Progetto relativa a Tz [N/mm²] : 0.04
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.019
fs : 54.02

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mmq	Tensione Critica nel piano XZ	: 142.50 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.21 N/mmq
Tensione fless. piano XY	: 1.70 N/mmq	Tensione fless. piano XZ	: 0.26 N/mmq
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.085	Coefficiente sfrutt. nel piano XZ	: 0.014
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.085	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.014
fs	: 11.758		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m

Carico distribuito Istantaneo	: -361.8 daN/m	-	Carico distribuito Finale	: -263.8 daN/m
-			Comb 42 [CAR] [ST]	
Freccia Istantanea - COMBINAZIONE			Comb 2 [SLEQP] [PE]	
Freccia Finale - COMBINAZIONE			Modulo Elastico finale	: 6388.9 N/mm ²
Modulo Elastico istantaneo	: 11500.0 N/mm ²			
Controfreccia	: 0.000 mm		Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Istantanea	: 0.000 mm		Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Netta Finale	: 0.000 mm		Limite Freccia Finale L/ 300	: 4.600 mm
Freccia Finale	: 0.000 mm		Fatt. sicurezza freccia Istantanea	: 1000.000
Fatt. sicurezza freccia Istantanea	: 1000.000		Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000		Fatt. sicurezza	: 1000.000

Campata 4-5 Copertur[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.104 (fs=9.636)

Sforzo Normale di Progetto [daN]	: -3651 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 209
Momento Flettente Mz di Progetto [daNm]	: 2829

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.1
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 186.52
Tensione di Progetto relativa a My [N/mm ²]	: 0.02
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.06
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.104
fs	: 9.64
Coefficiente di Sfruttamento a pressoflessione	: 0.104
fs	: 9.64

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 44 [SLV] [IN] " - Coeff. Sfruttamento : 0.024 (fs=41.017)

Taglio Ty di Progetto [daN]	: -1115
Taglio Tz di Progetto [daN]	: 352
Momento Torcente Mt di Progetto [daNm]	: -606

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.018
fs	: 56.63
Tensione di Progetto [N/mm ²]	: 0.13
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.024
fs	: 41.55
Coefficiente di Sfruttamento a taglio+torsione	: 0.024
fs	: 41.02

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.06 N/mm ²	Tensione fless. piano XZ	: 0.02 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.103	Coefficiente sfrutt. nel piano XZ	: 0.001
Coeff. sfrutt. max euleriano	: 0.005		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.108	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.006
fs	: 9.229		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 5-6 Copertur[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.126 (fs=7.915)

Sforzo Normale di Progetto [daN]	: -3576 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -68
Momento Flettente Mz di Progetto [daNm]	: 3462

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.1
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 190.43
Tensione di Progetto relativa a My [N/mm ²]	: 0.01
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.52
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.126
fs	: 7.92
Coefficiente di Sfruttamento a pressoflessione	: 0.126

fs : 7.92

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 44 [SLV] [IN] " - Coeff. Sfruttamento : 0.024 (fs=41.717)

Taglio Ty di Progetto [daN] : -198
 Taglio Tz di Progetto [daN] : 396
 Momento Torcente Mt di Progetto [daNm] : -599

Tipo Verifica	: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm²]	: 0.02
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.007
fs	: 149.71
Tensione di Progetto [N/mm²]	: 0.13
Modulo di resistenza a torsione [mm³]	: 25450510
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.024
fs	: 41.79
Coefficiente di Sfruttamento a taglio+torsione	: 0.024
fs	: 41.72

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm²	Tensione Critica nel piano XZ	: 142.50 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 2.52 N/mm²	Tensione fless. piano XZ	: 0.01 N/mm²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.126	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.005		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.131	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.006
fs	: 7.615		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 6-7 Copertur[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) -γ_M=1.45 (FC=1)

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L= 1380 mm - R 220x1700 - SEZIONI UTILIZZATE : 7
VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 220x1700**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.126 (fs=7.932)

Sforzo Normale di Progetto [daN]	: -3513 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -69
Momento Flettente Mz di Progetto [daNm]	: 3455

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.09
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 193.86
Tensione di Progetto relativa a My [N/mm ²]	: 0.01
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.52
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.126
fs	: 7.93
Coefficiente di Sfruttamento a pressoflessione	: 0.126
fs	: 7.93

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 220x1700**
Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.021 (fs=48.229)

Taglio Ty di Progetto [daN]	: -37
Taglio Tz di Progetto [daN]	: -525
Momento Torcente Mt di Progetto [daNm]	: -122

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.02
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.008
fs	: 125.75
Tensione di Progetto [N/mm ²]	: 0.11
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.021
fs	: 48.38
Coefficiente di Sfruttamento a taglio+torsione	: 0.021
fs	: 48.23

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.52 N/mm ²	Tensione fless. piano XZ	: 0.01 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.126	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.005		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.131	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.006

fs : 7.636

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 7-8 Copertur[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.113 (fs=8.879)

Sforzo Normale di Progetto [daN]	: -3566 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -48
Momento Flettente Mz di Progetto [daNm]	: 3088

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.1
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 190.95
Tensione di Progetto relativa a My [N/mm ²]	: 0.00
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.25
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.113
fs	: 8.88
Coefficiente di Sfruttamento a pressoflessione	: 0.113
fs	: 8.88

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.027 (fs=36.643)

Taglio Ty di Progetto [daN]	: 190
Taglio Tz di Progetto [daN]	: 332
Momento Torcente Mt di Progetto [daNm]	: 893

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.006

fs	: 173.27
Tensione di Progetto [N/mm ²]	: 0.14
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.027
fs	: 36.69
Coefficiente di Sfruttamento a taglio+torsione	: 0.027
fs	: 36.64

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.25 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.112	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.005		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.118	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.005
fs	: 8.499		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 8-9 Copertur[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=690 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.114 (fs=8.739)

Sforzo Normale di Progetto [daN]	: -3534 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -141
Momento Flettente Mz di Progetto [daNm]	: 3128

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.09
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.005

fs	: 192.68
Tensione di Progetto relativa a My [N/mm ²]	: 0.01
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.28
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.114
fs	: 8.74
Coefficiente di Sfruttamento a pressoflessione	: 0.114
fs	: 8.74

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.029 (fs=34.936)

Taglio Ty di Progetto [daN]	: 664
Taglio Tz di Progetto [daN]	: -681
Momento Torcente Mt di Progetto [daNm]	: 2310

Tipo Verifica	: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.03
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.014
fs	: 69.64
Tensione di Progetto [N/mm ²]	: 0.15
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.028
fs	: 35.19
Coefficiente di Sfruttamento a taglio+torsione	: 0.029
fs	: 34.94

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.28 N/mm ²	Tensione fless. piano XZ	: 0.01 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.114	Coefficiente sfrutt. nel piano XZ	: 0.001
Coeff. sfrutt. max euleriano	: 0.005		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.119	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.006
fs	: 8.397		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm

Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 9-10 Copertu[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.088 (fs=11.427)

Sforzo Normale di Progetto [daN]	: -3633 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -702
Momento Flettente Mz di Progetto [daNm]	: 2333

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.1
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 187.41
Tensione di Progetto relativa a My [N/mm²]	: 0.07
Tensione di Progetto relativa a Mz [N/mm²]	: 1.7
Tensione Resistente relativa a My [N/mm²]	: 18.21
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.087
fs	: 11.43
Coefficiente di Sfruttamento a pressoflessione	: 0.088
fs	: 11.43

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.039 (fs=25.889)

Taglio Ty di Progetto [daN]	: 778
Taglio Tz di Progetto [daN]	: 878
Momento Torcente Mt di Progetto [daNm]	: 2333

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm²]	: 0.04
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.018
fs	: 56.44
Tensione di Progetto [N/mm²]	: 0.2
Modulo di resistenza a torsione [mm³]	: 25450510
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.038
fs	: 26.1
Coefficiente di Sfruttamento a taglio+torsione	: 0.039
fs	: 25.89

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm

Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.70 N/mm ²	Tensione fless. piano XZ	: 0.07 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.085	Coefficiente sfrutt. nel piano XZ	: 0.004
Coeff. sfrutt. max euleriano	: 0.005		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.090	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.009
fs	: 11.077		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 10-11 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.06 (fs=16.766)

Sforzo Normale di Progetto [daN]	: -212 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -2118
Momento Flettente Mz di Progetto [daNm]	: -1427

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.01
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.000
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 0.2
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.04
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.06
fs	: 16.77
Coefficiente di Sfruttamento a pressoflessione	: 0.06
fs	: 16.77

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.046 (fs=21.878)

Taglio Ty di Progetto [daN]	: 1427
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Taglio Tz di Progetto [daN]	: -584	
Momento Torcente Mt di Progetto [daNm]	: 17	
Tipo Verifica		: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.06	
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.02	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a taglio	: 0.023	
fs	: 42.94	
Tensione di Progetto [N/mm ²]	: 0.24	
Modulo di resistenza a torsione [mm ³]	: 25450510	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a torsione	: 0.045	
fs	: 22.14	
Coefficiente di Sfruttamento a taglio+torsione	: 0.046	
fs	: 21.88	

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.16 N/mm ²	Tensione fless. piano XZ	: 0.01 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.058	Coefficiente sfrutt. nel piano XZ	: 0.001
Coeff. sfrutt. max euleriano	: 0.005		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.063	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.006
fs	: 15.816		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 11-12 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.105 (fs=9.559)

Sforzo Normale di Progetto [daN]	: 1241 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -2470
Momento Flettente Mz di Progetto [daNm]	: 2564

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.03
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 438.9
Tensione di Progetto relativa a My [N/mm ²]	: 0.23
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.87
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.102
fs	: 9.77
Coefficiente di Sfruttamento	: 0.105
fs	: 9.56

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.037 (fs=26.889)

Taglio Ty di Progetto [daN]	: 1424
Taglio Tz di Progetto [daN]	: -653
Momento Torcente Mt di Progetto [daNm]	: -1892

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.06
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.03
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.024
fs	: 42.27
Tensione di Progetto [N/mm ²]	: 0.19
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.037
fs	: 27.3
Coefficiente di Sfruttamento a taglio+torsione	: 0.037
fs	: 26.89

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.85 N/mm ²	Tensione fless. piano XZ	: 0.18 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.092	Coefficiente sfrutt. nel piano XZ	: 0.010
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.094	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.012
fs	: 10.650		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1380.0 mm

Schema adottato Doppio Incastro

Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 12-13 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.129 (fs=7.739)

Sforzo Normale di Progetto [daN] : -4061 (COMPRESSIONE)

Momento Flettente My di Progetto [daNm] : -1193

Momento Flettente Mz di Progetto [daNm] : -3429

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.11
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.006
fs	: 167.67
Tensione di Progetto relativa a My [N/mm ²]	: 0.11
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.5
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.129
fs	: 7.74
Coefficiente di Sfruttamento a pressoflessione	: 0.129
fs	: 7.74

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.035 (fs=28.927)

Taglio Ty di Progetto [daN] : 1563

Taglio Tz di Progetto [daN] : -366

Momento Torcente Mt di Progetto [daNm] : -3429

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.06
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.024
fs	: 41.24
Tensione di Progetto [N/mm ²]	: 0.18
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.034
fs	: 29.43
Coefficiente di Sfruttamento a taglio+torsione	: 0.035

fs

: 28.93

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.50 N/mm ²	Tensione fless. piano XZ	: 0.11 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.125	Coefficiente sfrutt. nel piano XZ	: 0.006
Coeff. sfrutt. max euleriano	: 0.006		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.131	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.012
fs	: 7.644		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 13-14 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1662.44 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1662.44 mm / 1662.44 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.233 (fs=4.295)

Sforzo Normale di Progetto [daN]	: -4009 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 256
Momento Flettente Mz di Progetto [daNm]	: -6368

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.11
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.006
fs	: 169.84
Tensione di Progetto relativa a My [N/mm ²]	: 0.02
Tensione di Progetto relativa a Mz [N/mm ²]	: 4.64
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.233
fs	: 4.3

Coefficiente di Sfruttamento a pressoflessione : 0.233
fs : 4.3

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1662.44 mm / 1662.44 mm] - **R 220x1700**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.03 (fs=33.103)

Taglio Ty di Progetto [daN] : -926
Taglio Tz di Progetto [daN] : -1168
Momento Torcente Mt di Progetto [daNm] : 1077

Tipo Verifica	:	TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	:	0.04
Tensione di Progetto relativa a Tz [N/mm ²]	:	0.05
Tensione tang. Resistente [N/mm ²]	:	2.66
Coefficiente di Sfruttamento a taglio	:	0.023
fs	:	44.41
Tensione di Progetto [N/mm ²]	:	0.16
Modulo di resistenza a torsione [mm ³]	:	25450510
Tensione tang. Resistente [N/mm ²]	:	2.66
Coefficiente di Sfruttamento a torsione	:	0.03
fs	:	33.67
Coefficiente di Sfruttamento a taglio+torsione	:	0.03
fs	:	33.1

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1662.4	Lunghezza efficace nel piano XZ	: 1662.4
Momento Critico nel piano XY	: 9685836 daNm	Momento Critico nel piano XZ	: 1253461 daNm
Tensione Critica nel piano XY	: 7063.08 N/mm ²	Tensione Critica nel piano XZ	: 118.29 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 4.64 N/mm ²	Tensione fless. piano XZ	: 0.02 N/mm ²
Snellezza relativa nel piano XY	: 0.06	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.232	Coefficiente sfrutt. nel piano XZ	: 0.001
Coeff. sfrutt. max euleriano	: 0.006		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.238	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.007
fs	: 4.206		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1662.4 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.325 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.750 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.541 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1590 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1590 mm / 1590 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.236 (fs=4.228)

Sforzo Normale di Progetto [daN] : -997 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : 1147
Momento Flettente Mz di Progetto [daNm] : 6381

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.03
Tensione Resistente [N/mm²] : 18.21
Coefficiente di Sfruttamento a compressione : 0.001
fs : 683.23
Tensione di Progetto relativa a My [N/mm²] : 0.11
Tensione di Progetto relativa a Mz [N/mm²] : 4.65
Tensione Resistente relativa a My [N/mm²] : 18.21
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.236
fs : 4.23
Coefficiente di Sfruttamento a pressoflessione : 0.236
fs : 4.23

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1590 mm / 1590 mm] - **R 220x1700**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.097 (fs=10.261)

Taglio Ty di Progetto [daN] : -200
Taglio Tz di Progetto [daN] : -1653
Momento Torcente Mt di Progetto [daNm] : 182

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.01
Tensione di Progetto relativa a Tz [N/mm²] : 0.07
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a taglio : 0.04
fs : 25.3
Tensione di Progetto [N/mm²] : 0.32
Modulo di resistenza a torsione [mm³] : 25450510
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a torsione : 0.096
fs : 10.43
Coefficiente di Sfruttamento a taglio+torsione : 0.097
fs : 10.26

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 46
Lunghezza efficace nel piano XY : 1590.0
Momento Critico nel piano XY : 10127108 daNm
Tensione Critica nel piano XY : 7384.86 N/mmq
Resistenza fless. piano XY : 20.03 N/mmq
Tensione fless. piano XY : 4.65 N/mmq
Snellezza relativa nel piano XY : 0.06
Coeff. Riduttivo nel piano XY : 1.000
Coefficiente sfrutt. nel piano XY : 0.232
Coeff. sfrutt. max euleriano : 0.001

Sezione più sfavorevole : 7
Lunghezza efficace nel piano XZ : 1590.0
Momento Critico nel piano XZ : 1310567 daNm
Tensione Critica nel piano XZ : 123.68 N/mmq
Resistenza fless. piano XZ : 18.21 N/mmq
Tensione fless. piano XZ : 0.11 N/mmq
Snellezza relativa nel piano XZ : 0.44
Coeff. Riduttivo nel piano XZ : 1.000
Coefficiente sfrutt. nel piano XZ : 0.006

Coeff. sfrutt. TOTALE (Piano XY) : 0.234
fs : 4.277

Coeff. sfrutt. TOTALE (Piano XZ) : 0.007

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1590.0 mm
Comb. di carico più gravosa : 142
Carico distribuito Istantaneo : -157.1 daN/m

Schema adottato Doppio Incastro
Peso proprio : -144.0 daN/m
-
Carico distribuito Finale : -157.1 daN/m

Freccia Istantanea - COMBINAZIONE

Comb 42 [CAR] [ST]

Freccia Finale - COMBINAZIONE

Comb 2 [SLEQP] [PE]

Modulo Elastico istantaneo : 11500.0 N/mm²

Modulo Elastico finale : 6388.9 N/mm²

Controfreccia : 0.000 mm

Freccia Istantanea : 0.000 mm

Limite Freccia Istantanea L/500 : 3.180 mm

Freccia Netta Finale : 0.000 mm

Limite Freccia Netta Fin. L/ 350 : 4.543 mm

Freccia Finale : 0.000 mm

Limite Freccia Finale L/ 300 : 5.300 mm

Fatt. sicurezza freccia Istantanea : 1000.000

Fatt. sicurezza freccia Netta Finale : 1000.000

Fatt. sicurezza freccia Finale : 1000.000

Fatt. sicurezza : 1000.000

Campata 15-17 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.123 (fs=8.148)

Sforzo Normale di Progetto [daN] : 1256 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : 14342

Momento Flettente Mz di Progetto [daNm] : -1808

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.03

Tensione Resistente [N/mm²] : 14.57

Coefficiente di Sfruttamento a trazione : 0.002

fs : 433.6

Tensione di Progetto relativa a My [N/mm²] : 1.35

Tensione di Progetto relativa a Mz [N/mm²] : 1.32

Tensione Resistente relativa a My [N/mm²] : 18.21

Tensione Resistente relativa a Mz [N/mm²] : 20.03

Coefficiente di Sfruttamento a flessione : 0.12

fs : 8.3

Coefficiente di Sfruttamento : 0.123

fs : 8.15

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.031 (fs=32.759)

Taglio Ty di Progetto [daN] : -1315

Taglio Tz di Progetto [daN] : 6392

Momento Torcente Mt di Progetto [daNm] : 1265

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.05

Tensione di Progetto relativa a Tz [N/mm²] : 0.26

Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a taglio	: 0.099
fs	: 10.15
Tensione di Progetto [N/mm ²]	: 0.11
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.021
fs	: 48.05
Coefficiente di Sfruttamento a taglio+torsione	: 0.031
fs	: 32.76

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 41	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 0.45 N/mm ²	Tensione fless. piano XZ	: 1.46 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.022	Coefficiente sfrutt. nel piano XZ	: 0.080
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.022	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.080
fs	: 12.477		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 16-18 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.088 (fs=11.315)

Sforzo Normale di Progetto [daN]	: -913 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 986
Momento Flettente Mz di Progetto [daNm]	: 2329

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.02
Tensione Resistente [N/mm ²]	: 18.21

Coefficiente di Sfruttamento a compressione	: 0.001
fs	: 746.06
Tensione di Progetto relativa a My [N/mm ²]	: 0.09
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.7
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.088
fs	: 11.32
Coefficiente di Sfruttamento a pressoflessione	: 0.088
fs	: 11.31

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 48 [SLV] [IN] " - Coeff. Sfruttamento : 0.022 (fs=45.01)

Taglio Ty di Progetto [daN]	: -1676
Taglio Tz di Progetto [daN]	: -1484
Momento Torcente Mt di Progetto [daNm]	: -428

Tipo Verifica	: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.07
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.06
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.034
fs	: 29.58
Tensione di Progetto [N/mm ²]	: 0.11
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.021
fs	: 47.45
Coefficiente di Sfruttamento a taglio+torsione	: 0.022
fs	: 45.01

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 45	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.70 N/mm ²	Tensione fless. piano XZ	: 0.09 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.085	Coefficiente sfrutt. nel piano XZ	: 0.005
Coeff. sfrutt. max euleriano	: 0.001		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.086	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.006
fs	: 11.609		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		

Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 17-19 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.103 (fs=9.728)

Sforzo Normale di Progetto [daN]	: 2641 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 11965
Momento Flettente Mz di Progetto [daNm]	: 1410

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.07
Tensione Resistente [N/mm²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.005
fs	: 206.25
Tensione di Progetto relativa a My [N/mm²]	: 1.13
Tensione di Progetto relativa a Mz [N/mm²]	: 1.03
Tensione Resistente relativa a My [N/mm²]	: 18.21
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.098
fs	: 10.21
Coefficiente di Sfruttamento	: 0.103
fs	: 9.73

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.015 (fs=67.227)

Taglio Ty di Progetto [daN]	: 2113
Taglio Tz di Progetto [daN]	: -4868
Momento Torcente Mt di Progetto [daNm]	: -1652

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²]	: 0.08
Tensione di Progetto relativa a Tz [N/mm²]	: 0.2
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.08
fs	: 12.47
Tensione di Progetto [N/mm²]	: 0.04
Modulo di resistenza a torsione [mm³]	: 25450510
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.008
fs	: 118.35
Coefficiente di Sfruttamento a taglio+torsione	: 0.015
fs	: 67.23

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 43	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0

Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.38 N/mm ²	Tensione fless. piano XZ	: 0.26 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.069	Coefficiente sfrutt. nel piano XZ	: 0.014
Coeff. sfrutt. max euleriano	: 0.003		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.072	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.017
fs	: 13.925		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 18-20 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.073 (fs=13.741)

Sforzo Normale di Progetto [daN]	: 994 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 4754
Momento Flettente Mz di Progetto [daNm]	: -1475

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.03
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 547.83
Tensione di Progetto relativa a My [N/mm ²]	: 0.45
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.08
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.071
fs	: 14.09
Coefficiente di Sfruttamento	: 0.073
fs	: 13.74

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.01 (fs=99.17)

Taglio Ty di Progetto [daN] : -1338
 Taglio Tz di Progetto [daN] : 847
 Momento Torcente Mt di Progetto [daNm] : -391

Tipo Verifica : TAGLIO+TORSIONE
 Tensione di Progetto relativa a Ty [N/mm²] : 0.05
 Tensione di Progetto relativa a Tz [N/mm²] : 0.03
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.024
 fs : 41.81
 Tensione di Progetto [N/mm²] : 0.05
 Modulo di resistenza a torsione [mm³] : 25450510
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.01
 fs : 105.13
 Coefficiente di Sfruttamento a taglio+torsione : 0.01
 fs : 99.17

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 45	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.18 N/mm ²	Tensione fless. piano XZ	: 0.04 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.059	Coefficiente sfrutt. nel piano XZ	: 0.002
Coeff. sfrutt. max euleriano	: 0.001		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.060	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.004
fs	: 16.558		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 19-21 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.092 ($f_s=10.861$)

Sforzo Normale di Progetto [daN]	: 2355 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 9849
Momento Flettente Mz di Progetto [daNm]	: 1429

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.06
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.004
f_s	: 231.28
Tensione di Progetto relativa a My [N/mm ²]	: 0.93
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.04
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.088
f_s	: 11.4
Coefficiente di Sfruttamento	: 0.092
f_s	: 10.86

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.021 ($f_s=47.657$)

Taglio Ty di Progetto [daN]	: 1462
Taglio Tz di Progetto [daN]	: -5825
Momento Torcente Mt di Progetto [daNm]	: -1665

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.06
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.23
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.091
f_s	: 11.02
Tensione di Progetto [N/mm ²]	: 0.07
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.013
f_s	: 78.4
Coefficiente di Sfruttamento a taglio+torsione	: 0.021
f_s	: 47.66

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 38	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.24 N/mm ²	Tensione fless. piano XZ	: 0.05 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.062	Coefficiente sfrutt. nel piano XZ	: 0.003
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.062	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.003
f_s	: 16.152		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)
· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 20-22 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.058 (fs=17.113)

Sforzo Normale di Progetto [daN]	: 1183 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 2774
Momento Flettente Mz di Progetto [daNm]	: 1269

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.03
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 460.37
Tensione di Progetto relativa a My [N/mm ²]	: 0.26
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.93
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.056
fs	: 17.77
Coefficiente di Sfruttamento	: 0.058
fs	: 17.11

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.015 (fs=67.347)

Taglio Ty di Progetto [daN]	: -582
Taglio Tz di Progetto [daN]	: -2184
Momento Torcente Mt di Progetto [daNm]	: -1397

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.09
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.034
fs	: 29.29
Tensione di Progetto [N/mm ²]	: 0.07
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.014
fs	: 73.08

Coefficiente di Sfruttamento a taglio+torsione : 0.015
fs : 67.35

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 38	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.05 N/mm ²	Tensione fless. piano XZ	: 0.08 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.052	Coefficiente sfrutt. nel piano XZ	: 0.004
Coeff. sfrutt. max euleriano	: 0.001		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.053	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.005
fs	: 18.769		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 21-23 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.074 (fs=13.426)

Sforzo Normale di Progetto [daN]	: 2032 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 3821
Momento Flettente Mz di Progetto [daNm]	: 1562

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.05
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.004
fs	: 268.09
Tensione di Progetto relativa a My [N/mm ²]	: 0.36
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.14
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.071

fs	: 14.13
Coefficiente di Sfruttamento	: 0.074
fs	: 13.43

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.053 (fs=18.94)

Taglio Ty di Progetto [daN]	: 1294
Taglio Tz di Progetto [daN]	: -3247
Momento Torcente Mt di Progetto [daNm]	: -827

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.05
Tensione di Progetto relativa a Tz [N/mm²]	: 0.13
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.053
fs	: 18.94

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 41	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm²	Tensione Critica nel piano XZ	: 148.97 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 1.14 N/mm²	Tensione fless. piano XZ	: 0.36 N/mm²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.057	Coefficiente sfrutt. nel piano XZ	: 0.020
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.057	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.020
fs	: 17.579		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 22-24 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 43 [SLV] [IN] " - Coeff. Sfruttamento : 0.049 (fs=20.387)

Sforzo Normale di Progetto [daN] : -457 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 1682
 Momento Flettente Mz di Progetto [daNm] : 1180

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.01
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.001
 fs : 1000
 Tensione di Progetto relativa a My [N/mm²] : 0.16
 Tensione di Progetto relativa a Mz [N/mm²] : 0.86
 Tensione Resistente relativa a My [N/mm²] : 18.21
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.049
 fs : 20.39
 Coefficiente di Sfruttamento a pressoflessione : 0.049
 fs : 20.39

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.017 (fs=58.695)

Taglio Ty di Progetto [daN] : 3
 Taglio Tz di Progetto [daN] : -718
 Momento Torcente Mt di Progetto [daNm] : -4

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.03
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.017
 fs : 58.69

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 43
 Lunghezza efficace nel piano XY : 1320.0
 Momento Critico nel piano XY : 12198561 daNm
 Tensione Critica nel piano XY : 8895.40 N/mm²
 Resistenza fless. piano XY : 20.03 N/mm²
 Tensione fless. piano XY : 0.86 N/mm²
 Snellezza relativa nel piano XY : 0.05
 Coeff. Riduttivo nel piano XY : 1.000
 Coefficiente sfrutt. nel piano XY : 0.043
 Coeff. sfrutt. max euleriano : 0.001
 Coeff. sfrutt. TOTALE (Piano XY) : 0.044
 fs : 22.926

Sezione più sfavorevole : 1
 Lunghezza efficace nel piano XZ : 1320.0
 Momento Critico nel piano XZ : 1578637 daNm
 Tensione Critica nel piano XZ : 148.97 N/mm²
 Resistenza fless. piano XZ : 18.21 N/mm²
 Tensione fless. piano XZ : 0.16 N/mm²
 Snellezza relativa nel piano XZ : 0.40
 Coeff. Riduttivo nel piano XZ : 1.000
 Coefficiente sfrutt. nel piano XZ : 0.009
 Coeff. sfrutt. TOTALE (Piano XZ) : 0.009

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1320.0 mm
 Comb. di carico più gravosa : 142
 Carico distribuito Istantaneo : -157.1 daN/m

Freccia Istantanea - COMBINAZIONE
 Freccia Finale - COMBINAZIONE

Schema adottato Doppio Incastro
 Peso proprio : -144.0 daN/m
 -
 Carico distribuito Finale : -157.1 daN/m
 Comb 42 [CAR] [ST]
 Comb 2 [SLEQP] [PE]

Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 23-25 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.08 (fs=12.575)

Sforzo Normale di Progetto [daN]	: 1093 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -1618
Momento Flettente Mz di Progetto [daNm]	: -1968

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.03
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 498.58
Tensione di Progetto relativa a My [N/mm ²]	: 0.15
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.43
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.078
fs	: 12.9
Coefficiente di Sfruttamento	: 0.08
fs	: 12.58

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.015 (fs=66.967)

Taglio Ty di Progetto [daN]	: 387
Taglio Tz di Progetto [daN]	: -3869
Momento Torcente Mt di Progetto [daNm]	: 1137

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.16
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.059
fs	: 17.02
Tensione di Progetto [N/mm ²]	: 0.06
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.011
fs	: 87.09
Coefficiente di Sfruttamento a taglio+torsione	: 0.015
fs	: 66.97

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.43 N/mm ²	Tensione fless. piano XZ	: 0.12 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.071	Coefficiente sfrutt. nel piano XZ	: 0.007
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.073	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.008
fs	: 13.657		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 24-26 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.047 (fs=21.198)

Sforzo Normale di Progetto [daN]	: -801 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 834
Momento Flettente Mz di Progetto [daNm]	: -1212

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.02
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.001
fs	: 850.25
Tensione di Progetto relativa a My [N/mm ²]	: 0.08
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.88
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.047
fs	: 21.2
Coefficiente di Sfruttamento a pressoflessione	: 0.047
fs	: 21.2

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.014 (fs=73.799)

Taglio Ty di Progetto [daN] : -305
 Taglio Tz di Progetto [daN] : -1420
 Momento Torcente Mt di Progetto [daNm] : 832

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.01
 Tensione di Progetto relativa a Tz [N/mm²] : 0.06
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.022
 fs : 45.58
 Tensione di Progetto [N/mm²] : 0.07
 Modulo di resistenza a torsione [mm³] : 25450510
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.013
 fs : 76.52
 Coefficiente di Sfruttamento a taglio+torsione : 0.014
 fs : 73.8

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 38	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm²	Tensione Critica nel piano XZ	: 148.97 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 0.88 N/mm²	Tensione fless. piano XZ	: 0.08 N/mm²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.044	Coefficiente sfrutt. nel piano XZ	: 0.004
Coeff. sfrutt. max euleriano	: 0.001		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.045	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.006
fs	: 22.065		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 25-28 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1700 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1700 mm] - **R 220x1700**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.101 (fs=9.869)

Sforzo Normale di Progetto [daN] : -770 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -2942
 Momento Flettente Mz di Progetto [daNm] : -2490

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.02
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.001
 fs : 884.78
 Tensione di Progetto relativa a My [N/mm²] : 0.28
 Tensione di Progetto relativa a Mz [N/mm²] : 1.82
 Tensione Resistente relativa a My [N/mm²] : 18.21
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.101
 fs : 9.87
 Coefficiente di Sfruttamento a pressoflessione : 0.101
 fs : 9.87

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1700 mm] - **R 220x1700**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.007 (fs=143.365)

Taglio Ty di Progetto [daN] : -2215
 Taglio Tz di Progetto [daN] : 971
 Momento Torcente Mt di Progetto [daNm] : -2367

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.09
 Tensione di Progetto relativa a Tz [N/mm²] : 0.04
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.037
 fs : 27.37
 Tensione di Progetto [N/mm²] : 0.03
 Modulo di resistenza a torsione [mm³] : 25450510
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.006
 fs : 177.3
 Coefficiente di Sfruttamento a taglio+torsione : 0.007
 fs : 143.37

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 26
 Lunghezza efficace nel piano XY : 1700.0
 Momento Critico nel piano XY : 9471824 daNm
 Tensione Critica nel piano XY : 6907.02 N/mmq
 Resistenza fless. piano XY : 20.03 N/mmq
 Tensione fless. piano XY : 1.82 N/mmq
 Snellezza relativa nel piano XY : 0.06
 Coeff. Riduttivo nel piano XY : 1.000
 Coefficiente sfrutt. nel piano XY : 0.091
 Coeff. sfrutt. max euleriano : 0.001
 Coeff. sfrutt. TOTALE (Piano XY) : 0.092
 fs : 10.896

Sezione più sfavorevole : 1
 Lunghezza efficace nel piano XZ : 1700.0
 Momento Critico nel piano XZ : 1225765 daNm
 Tensione Critica nel piano XZ : 115.67 N/mmq
 Resistenza fless. piano XZ : 18.21 N/mmq
 Tensione fless. piano XZ : 0.28 N/mmq
 Snellezza relativa nel piano XZ : 0.46
 Coeff. Riduttivo nel piano XZ : 1.000
 Coefficiente sfrutt. nel piano XZ : 0.015
 Coeff. sfrutt. TOTALE (Piano XZ) : 0.016

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1700.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.400 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.857 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.667 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 26-27 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.081 (fs=12.314)

Sforzo Normale di Progetto [daN]	: 1156 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 1868
Momento Flettente Mz di Progetto [daNm]	: 1986

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.03
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 471.09
Tensione di Progetto relativa a My [N/mm ²]	: 0.18
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.45
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.079
fs	: 12.64
Coefficiente di Sfruttamento	: 0.081
fs	: 12.31

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.015 (fs=65.345)

Taglio Ty di Progetto [daN]	: 578
Taglio Tz di Progetto [daN]	: 1183
Momento Torcente Mt di Progetto [daNm]	: -1045

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.05
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.02
fs	: 50.27
Tensione di Progetto [N/mm ²]	: 0.08
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66

Coefficiente di Sfruttamento a torsione	: 0.015
fs	: 67.08
Coefficiente di Sfruttamento a taglio+torsione	: 0.015
fs	: 65.34

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.45 N/mm ²	Tensione fless. piano XZ	: 0.20 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.073	Coefficiente sfrutt. nel piano XZ	: 0.011
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.074	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.013
fs	: 13.440		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 27-29 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.075 (fs=13.269)

Sforzo Normale di Progetto [daN]	: 1345 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 1467
Momento Flettente Mz di Progetto [daNm]	: 1856

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.04
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 404.9
Tensione di Progetto relativa a My [N/mm ²]	: 0.14
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.35
Tensione Resistente relativa a My [N/mm ²]	: 18.21

Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.073
f_s	: 13.72
Coefficiente di Sfruttamento	: 0.075
f_s	: 13.27

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.013 ($f_s=76.554$)

Taglio T_y di Progetto [daN]	: 823
Taglio T_z di Progetto [daN]	: 1373
Momento Torcente M_t di Progetto [daNm]	: -1604

Tipo Verifica		: TAGLIO+TORSIONE
Tensione di Progetto relativa a T_y [N/mm ²]	: 0.03	
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.06	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a taglio	: 0.024	
f_s	: 41.35	
Tensione di Progetto [N/mm ²]	: 0.07	
Modulo di resistenza a torsione [mm ³]	: 25450510	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a torsione	: 0.012	
f_s	: 80.14	
Coefficiente di Sfruttamento a taglio+torsione	: 0.013	
f_s	: 76.55	

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 9	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.36 N/mm ²	Tensione fless. piano XZ	: 0.15 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.068	Coefficiente sfrutt. nel piano XZ	: 0.008
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.070	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.010
f_s	: 14.308		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 28-30 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1460 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1460 mm / 1460 mm] - **R 220x1700**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.072 ($f_s=13.876$)

Sforzo Normale di Progetto [daN]	: 1236 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -17
Momento Flettente Mz di Progetto [daNm]	: -1915

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.03
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.002
f_s	: 440.86
Tensione di Progetto relativa a My [N/mm ²]	: 0.00
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.4
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.07
f_s	: 14.33
Coefficiente di Sfruttamento	: 0.072
f_s	: 13.88

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1460 mm] - **R 220x1700**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.011 ($f_s=94.483$)

Taglio Ty di Progetto [daN]	: 1222
Taglio Tz di Progetto [daN]	: 705
Momento Torcente Mt di Progetto [daNm]	: 568

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.05
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.03
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.021
f_s	: 46.92
Tensione di Progetto [N/mm ²]	: 0.05
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.01
f_s	: 98.72
Coefficiente di Sfruttamento a taglio+torsione	: 0.011
f_s	: 94.48

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1460.0	Lunghezza efficace nel piano XZ	: 1460.0
Momento Critico nel piano XY	: 11028836 daNm	Momento Critico nel piano XZ	: 1427261 daNm
Tensione Critica nel piano XY	: 8042.42 N/mm ²	Tensione Critica nel piano XZ	: 134.69 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.40 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.42

Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.070	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.070	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.000
fs	: 14.340		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1460.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.920 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.171 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.867 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 29-31 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.068 (fs=14.738)

Sforzo Normale di Progetto [daN]	: 1552 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 1818
Momento Flettente Mz di Progetto [daNm]	: 1604

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.04
Tensione Resistente [N/mm²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.003
fs	: 351.07
Tensione di Progetto relativa a My [N/mm²]	: 0.17
Tensione di Progetto relativa a Mz [N/mm²]	: 1.17
Tensione Resistente relativa a My [N/mm²]	: 18.21
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.065
fs	: 15.38
Coefficiente di Sfruttamento	: 0.068
fs	: 14.74

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.013 (fs=79.036)

Taglio Ty di Progetto [daN]	: -1225
Taglio Tz di Progetto [daN]	: -1293
Momento Torcente Mt di Progetto [daNm]	: 899

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.05
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.05
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.027
f_s	: 37.18
Tensione di Progetto [N/mm ²]	: 0.06
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.012
f_s	: 83.83
Coefficiente di Sfruttamento a taglio+torsione	: 0.013
f_s	: 79.04

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.17 N/mm ²	Tensione fless. piano XZ	: 0.17 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.059	Coefficiente sfrutt. nel piano XZ	: 0.010
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.061	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.012
f_s	: 16.384		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 30-32 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1370 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1370 mm / 1370 mm] - **R 220x1700**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.071 ($f_s=14.035$)

Sforzo Normale di Progetto [daN]	: 1697 (TRAZIONE)
Momento Flettente M_y di Progetto [daNm]	: 2991
Momento Flettente M_z di Progetto [daNm]	: -1573

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.05
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.003
fs	: 321
Tensione di Progetto relativa a My [N/mm ²]	: 0.28
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.15
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.068
fs	: 14.68
Coefficiente di Sfruttamento	: 0.071
fs	: 14.03

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1370 mm] - **R 220x1700**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.013 (fs=78.003)

Taglio Ty di Progetto [daN]	: -1663
Taglio Tz di Progetto [daN]	: 3934
Momento Torcente Mt di Progetto [daNm]	: -851

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.07
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.16
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.065
fs	: 15.5
Tensione di Progetto [N/mm ²]	: 0.05
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.009
fs	: 115.5
Coefficiente di Sfruttamento a taglio+torsione	: 0.013
fs	: 78

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 18	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1370.0	Lunghezza efficace nel piano XZ	: 1370.0
Momento Critico nel piano XY	: 11753358 daNm	Momento Critico nel piano XZ	: 1521023 daNm
Tensione Critica nel piano XY	: 8570.75 N/mm ²	Tensione Critica nel piano XZ	: 143.54 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.15 N/mm ²	Tensione fless. piano XZ	: 0.27 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.057	Coefficiente sfrutt. nel piano XZ	: 0.015
Coeff. sfrutt. max euleriano	: 0.003		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.060	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.017
fs	: 16.706		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1370.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	

Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.740 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.914 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.567 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 31-33 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.07 (fs=14.306)

Sforzo Normale di Progetto [daN]	: 1577 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -2753
Momento Flettente Mz di Progetto [daNm]	: 1566

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.04
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.003
fs	: 345.41
Tensione di Progetto relativa a My [N/mm ²]	: 0.26
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.14
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.067
fs	: 14.92
Coefficiente di Sfruttamento	: 0.07
fs	: 14.31

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.01 (fs=96.579)

Taglio Ty di Progetto [daN]	: -391
Taglio Tz di Progetto [daN]	: 1229
Momento Torcente Mt di Progetto [daNm]	: -1140

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.05
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.019
fs	: 51.32
Tensione di Progetto [N/mm ²]	: 0.05
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.01
fs	: 100.26
Coefficiente di Sfruttamento a taglio+torsione	: 0.01
fs	: 96.58

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 9	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.14 N/mm ²	Tensione fless. piano XZ	: 0.27 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.057	Coefficiente sfrutt. nel piano XZ	: 0.015
Coeff. sfrutt. max euleriano	: 0.003		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.060	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.018
fs	: 16.760		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 32-34 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.074 (fs=13.544)

Sforzo Normale di Progetto [daN]	: 1780 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -2877
Momento Flettente Mz di Progetto [daNm]	: -1651

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.05
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.003
fs	: 306.08
Tensione di Progetto relativa a My [N/mm ²]	: 0.27
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.2
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.071
fs	: 14.17
Coefficiente di Sfruttamento	: 0.074
fs	: 13.54

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.009 (fs=105.577)

Taglio Ty di Progetto [daN] : -233
 Taglio Tz di Progetto [daN] : 824
 Momento Torcente Mt di Progetto [daNm] : -972

Tipo Verifica	: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm²]	: 0.03
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.013
fs	: 77.33
Tensione di Progetto [N/mm²]	: 0.05
Modulo di resistenza a torsione [mm³]	: 25450510
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.009
fs	: 107.47
Coefficiente di Sfruttamento a taglio+torsione	: 0.009
fs	: 105.58

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 50	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm²	Tensione Critica nel piano XZ	: 142.50 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 1.22 N/mm²	Tensione fless. piano XZ	: 0.27 N/mm²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.061	Coefficiente sfrutt. nel piano XZ	: 0.015
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.063	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.017
fs	: 15.873		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 33-35 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.072 (fs=13.902)

Sforzo Normale di Progetto [daN] : 1389 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -2234
 Momento Flettente Mz di Progetto [daNm] : 1683

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.04
 Tensione Resistente [N/mm²] : 14.57
 Coefficiente di Sfruttamento a trazione : 0.003
 fs : 392.31
 Tensione di Progetto relativa a My [N/mm²] : 0.21
 Tensione di Progetto relativa a Mz [N/mm²] : 1.23
 Tensione Resistente relativa a My [N/mm²] : 18.21
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.069
 fs : 14.41
 Coefficiente di Sfruttamento : 0.072
 fs : 13.9

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.013 (fs=77.857)

Taglio Ty di Progetto [daN] : -1675
 Taglio Tz di Progetto [daN] : 508
 Momento Torcente Mt di Progetto [daNm] : -1756

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.07
 Tensione di Progetto relativa a Tz [N/mm²] : 0.02
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.026
 fs : 37.82
 Tensione di Progetto [N/mm²] : 0.06
 Modulo di resistenza a torsione [mm³] : 25450510
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.012
 fs : 82.34
 Coefficiente di Sfruttamento a taglio+torsione : 0.013
 fs : 77.86

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 45
 Lunghezza efficace nel piano XY : 1320.0
 Momento Critico nel piano XY : 12198561 daNm
 Tensione Critica nel piano XY : 8895.40 N/mmq
 Resistenza fless. piano XY : 20.03 N/mmq
 Tensione fless. piano XY : 1.30 N/mmq
 Snellezza relativa nel piano XY : 0.05
 Coeff. Riduttivo nel piano XY : 1.000
 Coefficiente sfrutt. nel piano XY : 0.065
 Coeff. sfrutt. max euleriano : 0.000
 Coeff. sfrutt. TOTALE (Piano XY) : 0.065
 fs : 15.357

Sezione più sfavorevole : 1
 Lunghezza efficace nel piano XZ : 1320.0
 Momento Critico nel piano XZ : 1578637 daNm
 Tensione Critica nel piano XZ : 148.97 N/mmq
 Resistenza fless. piano XZ : 18.21 N/mmq
 Tensione fless. piano XZ : 0.02 N/mmq
 Snellezza relativa nel piano XZ : 0.40
 Coeff. Riduttivo nel piano XZ : 1.000
 Coefficiente sfrutt. nel piano XZ : 0.001
 Coeff. sfrutt. TOTALE (Piano XZ) : 0.001

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 34-36 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.077 (fs=13.005)

Sforzo Normale di Progetto [daN]	: 26 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 2915
Momento Flettente Mz di Progetto [daNm]	: 1820

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 0.28
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.33
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.077
fs	: 13.01
Coefficiente di Sfruttamento	: 0.077
fs	: 13.01

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.013 (fs=74.143)

Taglio Ty di Progetto [daN]	: -1878
Taglio Tz di Progetto [daN]	: 3522
Momento Torcente Mt di Progetto [daNm]	: -1812

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.08
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.14
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.06
fs	: 16.59
Tensione di Progetto [N/mm ²]	: 0.05
Modulo di resistenza a torsione [mm ³]	: 25450510

Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.01
fs	: 101.5
Coefficiente di Sfruttamento a taglio+torsione	: 0.013
fs	: 74.14

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 45	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.34 N/mm ²	Tensione fless. piano XZ	: 0.24 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.067	Coefficiente sfrutt. nel piano XZ	: 0.013
Coeff. sfrutt. max euleriano	: 0.001		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.068	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.014
fs	: 14.778		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 35-37 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.072 (fs=13.848)

Sforzo Normale di Progetto [daN]	: 1693 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -2476
Momento Flettente Mz di Progetto [daNm]	: 1651

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.05
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.003
fs	: 321.78
Tensione di Progetto relativa a My [N/mm ²]	: 0.23
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.2

Tensione Resistente relativa a M_y [N/mm ²]	: 18.21
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.069
f_s	: 14.47
Coefficiente di Sfruttamento	: 0.072
f_s	: 13.85

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 32 [SLD] [IN] " - Coeff. Sfruttamento : 0.024 ($f_s=42.138$)

Taglio T_y di Progetto [daN]	: 1546
Taglio T_z di Progetto [daN]	: -281
Momento Torcente M_t di Progetto [daNm]	: -1006

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.06
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.024
f_s	: 42.14

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.20 N/mm ²	Tensione fless. piano XZ	: 0.25 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.060	Coefficiente sfrutt. nel piano XZ	: 0.014
Coeff. sfrutt. max euleriano	: 0.003		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.063	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.017
f_s	: 15.909		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale ($t \rightarrow \infty$)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 36-38 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.07 (fs=14.361)

Sforzo Normale di Progetto [daN]	: -104 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 2237
Momento Flettente Mz di Progetto [daNm]	: 1690

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.00
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.000
fs	: 1000
Tensione di Progetto relativa a My [N/mm²]	: 0.21
Tensione di Progetto relativa a Mz [N/mm²]	: 1.23
Tensione Resistente relativa a My [N/mm²]	: 18.21
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.07
fs	: 14.36
Coefficiente di Sfruttamento a pressoflessione	: 0.07
fs	: 14.36

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.049 (fs=20.282)

Taglio Ty di Progetto [daN]	: -1395
Taglio Tz di Progetto [daN]	: 2951
Momento Torcente Mt di Progetto [daNm]	: -403

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.06
Tensione di Progetto relativa a Tz [N/mm²]	: 0.12
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.049
fs	: 20.28

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 22	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mmq	Tensione Critica nel piano XZ	: 142.50 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.21 N/mmq
Tensione fless. piano XY	: 1.24 N/mmq	Tensione fless. piano XZ	: 0.17 N/mmq
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.062	Coefficiente sfrutt. nel piano XZ	: 0.009
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.062	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.009
fs	: 16.119		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	

-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 37-39 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.068 ($f_s=14.812$)

Sforzo Normale di Progetto [daN]	: 1624 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -3179
Momento Flettente Mz di Progetto [daNm]	: 1456

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.04
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.003
f_s	: 335.49
Tensione di Progetto relativa a My [N/mm ²]	: 0.3
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.06
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.065
f_s	: 15.5
Coefficiente di Sfruttamento	: 0.068
f_s	: 14.81

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.012 ($f_s=83.926$)

Taglio Ty di Progetto [daN]	: -792
Taglio Tz di Progetto [daN]	: -687
Momento Torcente Mt di Progetto [daNm]	: 962

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.03
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.016
f_s	: 63.14
Tensione di Progetto [N/mm ²]	: 0.06
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.012
f_s	: 85.73
Coefficiente di Sfruttamento a taglio+torsione	: 0.012
f_s	: 83.93

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.06 N/mm ²	Tensione fless. piano XZ	: 0.31 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.053	Coefficiente sfrutt. nel piano XZ	: 0.017
Coeff. sfrutt. max euleriano	: 0.003		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.056	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.020
fs	: 18.010		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 38-40 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1370 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1370 mm] - **R 220x1700**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.065 (fs=15.494)

Sforzo Normale di Progetto [daN]	: 1150 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -833
Momento Flettente Mz di Progetto [daNm]	: -1632

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.03
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 473.8
Tensione di Progetto relativa a My [N/mm ²]	: 0.08
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.19
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.062
fs	: 16.02
Coefficiente di Sfruttamento	: 0.065
fs	: 15.49

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1370 mm] - **R 220x1700**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.014 (fs=69.781)

Taglio Ty di Progetto [daN] : -1250
 Taglio Tz di Progetto [daN] : 4053
 Momento Torcente Mt di Progetto [daNm] : -1627

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.05
 Tensione di Progetto relativa a Tz [N/mm²] : 0.16
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.064
 fs : 15.61
 Tensione di Progetto [N/mm²] : 0.05
 Modulo di resistenza a torsione [mm³] : 25450510
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.01
 fs : 97.79
 Coefficiente di Sfruttamento a taglio+torsione : 0.014
 fs : 69.78

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 49	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1370.0	Lunghezza efficace nel piano XZ	: 1370.0
Momento Critico nel piano XY	: 11753358 daNm	Momento Critico nel piano XZ	: 1521023 daNm
Tensione Critica nel piano XY	: 8570.75 N/mm²	Tensione Critica nel piano XZ	: 143.54 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 1.19 N/mm²	Tensione fless. piano XZ	: 0.08 N/mm²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.060	Coefficiente sfrutt. nel piano XZ	: 0.005
Coeff. sfrutt. max euleriano	: 0.003		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.062	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.007
fs	: 16.078		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1370.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.740 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.914 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.567 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 39-41 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
 L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 220x1700**
Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.117 (fs=8.578)
 Sforzo Normale di Progetto [daN] : -1202 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 2207
 Momento Flettente Mz di Progetto [daNm] : 2982

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.03
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.002
 fs : 566.42
 Tensione di Progetto relativa a My [N/mm²] : 0.21
 Tensione di Progetto relativa a Mz [N/mm²] : 2.17
 Tensione Resistente relativa a My [N/mm²] : 18.21
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.117
 fs : 8.58
 Coefficiente di Sfruttamento a pressoflessione : 0.117
 fs : 8.58

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 220x1700**
Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.015 (fs=68.476)
 Taglio Ty di Progetto [daN] : -956
 Taglio Tz di Progetto [daN] : -2177
 Momento Torcente Mt di Progetto [daNm] : 258

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.04
 Tensione di Progetto relativa a Tz [N/mm²] : 0.09
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.036
 fs : 27.85
 Tensione di Progetto [N/mm²] : 0.07
 Modulo di resistenza a torsione [mm³] : 25450510
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.013
 fs : 75.11
 Coefficiente di Sfruttamento a taglio+torsione : 0.015
 fs : 68.48

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 40
 Lunghezza efficace nel piano XY : 1320.0
 Momento Critico nel piano XY : 12198561 daNm
 Tensione Critica nel piano XY : 8895.40 N/mm²
 Resistenza fless. piano XY : 20.03 N/mm²
 Tensione fless. piano XY : 2.17 N/mm²
 Snellezza relativa nel piano XY : 0.05
 Coeff. Riduttivo nel piano XY : 1.000
 Coefficiente sfrutt. nel piano XY : 0.109
 Coeff. sfrutt. max euleriano : 0.002
 Coeff. sfrutt. TOTALE (Piano XY) : 0.110
 fs : 9.064

Sezione più sfavorevole : 7
 Lunghezza efficace nel piano XZ : 1320.0
 Momento Critico nel piano XZ : 1578637 daNm
 Tensione Critica nel piano XZ : 148.97 N/mm²
 Resistenza fless. piano XZ : 18.21 N/mm²
 Tensione fless. piano XZ : 0.21 N/mm²
 Snellezza relativa nel piano XZ : 0.40
 Coeff. Riduttivo nel piano XZ : 1.000
 Coefficiente sfrutt. nel piano XZ : 0.011
 Coeff. sfrutt. TOTALE (Piano XZ) : 0.013

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 40-42 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.139 (fs=7.198)

Sforzo Normale di Progetto [daN]	: 726 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 5573
Momento Flettente Mz di Progetto [daNm]	: 3224

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.02
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.001
fs	: 749.85
Tensione di Progetto relativa a My [N/mm ²]	: 0.53
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.35
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.138
fs	: 7.27
Coefficiente di Sfruttamento	: 0.139
fs	: 7.2

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.012 (fs=84.416)

Taglio Ty di Progetto [daN]	: 2823
Taglio Tz di Progetto [daN]	: -3235
Momento Torcente Mt di Progetto [daNm]	: -3197

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.11
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.13
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.065
fs	: 15.42

Tensione di Progetto [N/mm ²]	: 0.04
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.008
fs	: 130.88
Coefficiente di Sfruttamento a taglio+torsione	: 0.012
fs	: 84.42

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 22	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.34 N/mm ²	Tensione fless. piano XZ	: 0.48 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.117	Coefficiente sfrutt. nel piano XZ	: 0.026
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.119	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.028
fs	: 8.428		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 41-44 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.162)

Sforzo Normale di Progetto [daN]	: 1848 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 1439
Momento Flettente Mz di Progetto [daNm]	: 2761

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.05
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.003
fs	: 294.83

Tensione di Progetto relativa a M_y [N/mm ²]	: 0.14
Tensione di Progetto relativa a M_z [N/mm ²]	: 2.01
Tensione Resistente relativa a M_y [N/mm ²]	: 18.21
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.106
f_s	: 9.46
Coefficiente di Sfruttamento	: 0.109
f_s	: 9.16

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.011 ($f_s=94.631$)

Taglio T_y di Progetto [daN]	: -3044
Taglio T_z di Progetto [daN]	: 1810
Momento Torcente M_t di Progetto [daNm]	: -1443

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.12
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.07
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.053
f_s	: 18.69
Tensione di Progetto [N/mm ²]	: 0.04
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.008
f_s	: 129.78
Coefficiente di Sfruttamento a taglio+torsione	: 0.011
f_s	: 94.63

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 9	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.01 N/mm ²	Tensione fless. piano XZ	: 0.16 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.100	Coefficiente sfrutt. nel piano XZ	: 0.009
Coeff. sfrutt. max euleriano	: 0.003		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.104	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.012
f_s	: 9.638		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -157.1 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm ²
Controfreccia	: 0.000 mm
Freccia Istantanea	: 0.000 mm
Freccia Netta Finale	: 0.000 mm

Schema adottato Doppio Incastro	
Peso proprio	: -144.0 daN/m
-	
Carico distribuito Finale	: -157.1 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [PE]	
Modulo Elastico finale	: 6388.9 N/mm ²
Limite Freccia Istantanea L/500	: 2.640 mm
Limite Freccia Netta Fin. L/350	: 3.771 mm

Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 42-43 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 460 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 460 mm] - **R 220x1700**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.098 (fs=10.182)

Sforzo Normale di Progetto [daN]	: 857 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -2396
Momento Flettente Mz di Progetto [daNm]	: -2415

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.02
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 635.85
Tensione di Progetto relativa a My [N/mm ²]	: 0.23
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.76
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.097
fs	: 10.35
Coefficiente di Sfruttamento	: 0.098
fs	: 10.18

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 460 mm] - **R 220x1700**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.052 (fs=19.373)

Taglio Ty di Progetto [daN]	: 3895
Taglio Tz di Progetto [daN]	: 2013
Momento Torcente Mt di Progetto [daNm]	: 2172

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.16
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.08
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.066
fs	: 15.1
Tensione di Progetto [N/mm ²]	: 0.25
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.047
fs	: 21.17
Coefficiente di Sfruttamento a taglio+torsione	: 0.052
fs	: 19.37

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 21	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 460.0	Lunghezza efficace nel piano XZ	: 460.0
Momento Critico nel piano XY	: 35004567 daNm	Momento Critico nel piano XZ	: 4530003 daNm
Tensione Critica nel piano XY	: 25525.94 N/mm ²	Tensione Critica nel piano XZ	: 427.49 N/mm ²

Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.77 N/mm ²	Tensione fless. piano XZ	: 0.21 N/mm ²
Snellezza relativa nel piano XY	: 0.03	Snellezza relativa nel piano XZ	: 0.24
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.088	Coefficiente sfrutt. nel piano XZ	: 0.012
Coeff. sfrutt. max euleriano	: 0.001		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.090	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.013
fs	: 11.145		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 460.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 0.920 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 1.314 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 1.533 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 43-45 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 29 [SLD] [IN] " - Coeff. Sfruttamento : 0.106 (fs=9.444)

Sforzo Normale di Progetto [daN]	: 2024 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -1002
Momento Flettente Mz di Progetto [daNm]	: -2706

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.05
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.004
fs	: 269.18
Tensione di Progetto relativa a My [N/mm ²]	: 0.09
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.97
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.102
fs	: 9.79
Coefficiente di Sfruttamento	: 0.106
fs	: 9.44

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.011 (fs=90.311)

Taglio Ty di Progetto [daN]	: 1492
Taglio Tz di Progetto [daN]	: 959

Momento Torcente Mt di Progetto [daNm]	: 1486	
Tipo Verifica		: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.06	
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.04	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a taglio	: 0.027	
fs	: 37.32	
Tensione di Progetto [N/mm ²]	: 0.05	
Modulo di resistenza a torsione [mm ³]	: 25450510	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a torsione	: 0.01	
fs	: 96.57	
Coefficiente di Sfruttamento a taglio+torsione	: 0.011	
fs	: 90.31	

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.99 N/mm ²	Tensione fless. piano XZ	: 0.09 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.099	Coefficiente sfrutt. nel piano XZ	: 0.005
Coeff. sfrutt. max euleriano	: 0.003		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.103	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.008
fs	: 9.751		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 44-46 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.14 (fs=7.158)

Sforzo Normale di Progetto [daN] : 901 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : -1415
 Momento Flettente Mz di Progetto [daNm] : 3651

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.02
 Tensione Resistente [N/mm²] : 14.57
 Coefficiente di Sfruttamento a trazione : 0.002
 fs : 604.84
 Tensione di Progetto relativa a My [N/mm²] : 0.13
 Tensione di Progetto relativa a Mz [N/mm²] : 2.66
 Tensione Resistente relativa a My [N/mm²] : 18.21
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.138
 fs : 7.24
 Coefficiente di Sfruttamento : 0.14
 fs : 7.16

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.013 (fs=79.761)

Taglio Ty di Progetto [daN] : -3073
 Taglio Tz di Progetto [daN] : 733
 Momento Torcente Mt di Progetto [daNm] : -3672

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.12
 Tensione di Progetto relativa a Tz [N/mm²] : 0.03
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.048
 fs : 20.95
 Tensione di Progetto [N/mm²] : 0.05
 Modulo di resistenza a torsione [mm³] : 25450510
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.01
 fs : 97.47
 Coefficiente di Sfruttamento a taglio+torsione : 0.013
 fs : 79.76

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 38	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.69 N/mm ²	Tensione fless. piano XZ	: 0.10 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.134	Coefficiente sfrutt. nel piano XZ	: 0.005
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.136	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.007
fs	: 7.361		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m

Carico distribuito Istantaneo	: -157.1 daN/m	-	Carico distribuito Finale	: -157.1 daN/m
-			Comb 42 [CAR] [ST]	
Freccia Istantanea - COMBINAZIONE			Comb 2 [SLEQP] [PE]	
Freccia Finale - COMBINAZIONE			Modulo Elastico finale	: 6388.9 N/mm ²
Modulo Elastico istantaneo	: 11500.0 N/mm ²			
Controfreccia	: 0.000 mm			
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm	
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm	
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm	
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000	
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000	

Campata 45-47 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.084 ($f_s=11.961$)

Sforzo Normale di Progetto [daN]	: 955 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 3760
Momento Flettente Mz di Progetto [daNm]	: 1873

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.03
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.002
f_s	: 570.24
Tensione di Progetto relativa a My [N/mm ²]	: 0.35
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.37
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.082
f_s	: 12.22
Coefficiente di Sfruttamento	: 0.084
f_s	: 11.96

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.015 ($f_s=67.443$)

Taglio Ty di Progetto [daN]	: -1172
Taglio Tz di Progetto [daN]	: 4162
Momento Torcente Mt di Progetto [daNm]	: -317

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.05
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.17
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.065
f_s	: 15.31
Tensione di Progetto [N/mm ²]	: 0.06
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.011
f_s	: 94.69
Coefficiente di Sfruttamento a taglio+torsione	: 0.015
f_s	: 67.44

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.46 N/mm ²	Tensione fless. piano XZ	: 0.26 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.073	Coefficiente sfrutt. nel piano XZ	: 0.014
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.075	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.016
fs	: 13.345		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 46-48 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.084 (fs=11.97)

Sforzo Normale di Progetto [daN]	: 1774 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 2230
Momento Flettente Mz di Progetto [daNm]	: 1983

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.05
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.003
fs	: 307.12
Tensione di Progetto relativa a My [N/mm ²]	: 0.21
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.45
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.08
fs	: 12.46
Coefficiente di Sfruttamento	: 0.084

fs

: 11.97

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.015 (fs=66.726)

Taglio Ty di Progetto [daN] : 3
 Taglio Tz di Progetto [daN] : 631
 Momento Torcente Mt di Progetto [daNm] : 5

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.03
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.015
 fs : 66.73

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 9	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm²	Tensione Critica nel piano XZ	: 148.97 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 1.44 N/mm²	Tensione fless. piano XZ	: 0.22 N/mm²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.072	Coefficiente sfrutt. nel piano XZ	: 0.012
Coeff. sfrutt. max euleriano	: 0.003		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.075	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.015
fs	: 13.356		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 47-49 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.066 (fs=15.117)

Sforzo Normale di Progetto [daN]	: 1982 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -1855
Momento Flettente Mz di Progetto [daNm]	: -1532

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.05
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.004
fs	: 274.84
Tensione di Progetto relativa a My [N/mm ²]	: 0.18
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.12
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.063
fs	: 16
Coefficiente di Sfruttamento	: 0.066
fs	: 15.12

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.014 (fs=72.441)

Taglio Ty di Progetto [daN]	: 4
Taglio Tz di Progetto [daN]	: 582
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.02
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.014
fs	: 72.44

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 30	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.15 N/mm ²	Tensione fless. piano XZ	: 0.18 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.057	Coefficiente sfrutt. nel piano XZ	: 0.010
Coeff. sfrutt. max euleriano	: 0.004		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.061	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.013
fs	: 16.361		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		

Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 48-50 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.066 (fs=15.084)

Sforzo Normale di Progetto [daN]	: 1277 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 3202
Momento Flettente Mz di Progetto [daNm]	: 1437

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.03
Tensione Resistente [N/mm²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 426.68
Tensione di Progetto relativa a My [N/mm²]	: 0.3
Tensione di Progetto relativa a Mz [N/mm²]	: 1.05
Tensione Resistente relativa a My [N/mm²]	: 18.21
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.064
fs	: 15.64
Coefficiente di Sfruttamento	: 0.066
fs	: 15.08

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.017 (fs=57.601)

Taglio Ty di Progetto [daN]	: 2
Taglio Tz di Progetto [daN]	: 731
Momento Torcente Mt di Progetto [daNm]	: 1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0
Tensione di Progetto relativa a Tz [N/mm²]	: 0.03
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.017
fs	: 57.6

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm²	Tensione Critica nel piano XZ	: 148.97 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 1.05 N/mm²	Tensione fless. piano XZ	: 0.24 N/mm²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.052	Coefficiente sfrutt. nel piano XZ	: 0.013

Coeff. sfrutt. max euleriano	: 0.002	
Coeff. sfrutt. TOTALE (Piano XY)	: 0.054	Coeff. sfrutt. TOTALE (Piano XZ) : 0.015
fs	: 18.377	

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 49-51 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.102 (fs=9.795)

Sforzo Normale di Progetto [daN]	: 2705 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 10597
Momento Flettente Mz di Progetto [daNm]	: 1612

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.07
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.005
fs	: 201.39
Tensione di Progetto relativa a My [N/mm ²]	: 1
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.18
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.097
fs	: 10.3
Coefficiente di Sfruttamento	: 0.102
fs	: 9.8

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.023 (fs=44.227)

Taglio Ty di Progetto [daN]	: -1648
Taglio Tz di Progetto [daN]	: 6585
Momento Torcente Mt di Progetto [daNm]	: -1100

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.07
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.26

Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.103
fs	: 9.75
Tensione di Progetto [N/mm ²]	: 0.06
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.012
fs	: 82.66
Coefficiente di Sfruttamento a taglio+torsione	: 0.023
fs	: 44.23

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 42	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.18 N/mm ²	Tensione fless. piano XZ	: 1.00 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.059	Coefficiente sfrutt. nel piano XZ	: 0.055
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.059	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.055
fs	: 17.043		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 50-52 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.064 (fs=15.672)

Sforzo Normale di Progetto [daN]	: 1591 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 2749
Momento Flettente Mz di Progetto [daNm]	: 1398

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.04
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Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.003
fs	: 342.46
Tensione di Progetto relativa a My [N/mm ²]	: 0.26
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.02
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.061
fs	: 16.42
Coefficiente di Sfruttamento	: 0.064
fs	: 15.67

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.013 (fs=74.498)

Taglio Ty di Progetto [daN]	: 769
Taglio Tz di Progetto [daN]	: 2149
Momento Torcente Mt di Progetto [daNm]	: 89

Tipo Verifica	: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.09
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.034
fs	: 29
Tensione di Progetto [N/mm ²]	: 0.06
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.012
fs	: 81.74
Coefficiente di Sfruttamento a taglio+torsione	: 0.013
fs	: 74.5

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 22	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.05 N/mm ²	Tensione fless. piano XZ	: 0.28 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.052	Coefficiente sfrutt. nel piano XZ	: 0.015
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.054	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.017
fs	: 18.401		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -157.1 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm ²

Schema adottato Doppio Incastro	
Peso proprio	: -144.0 daN/m
-	
Carico distribuito Finale	: -157.1 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [PE]	
Modulo Elastico finale	: 6388.9 N/mm ²

Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 51-53 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.106 (fs=9.394)

Sforzo Normale di Progetto [daN]	: 3348 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 7498
Momento Flettente Mz di Progetto [daNm]	: -2008

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.09
Tensione Resistente [N/mm²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.006
fs	: 162.73
Tensione di Progetto relativa a My [N/mm²]	: 0.71
Tensione di Progetto relativa a Mz [N/mm²]	: 1.46
Tensione Resistente relativa a My [N/mm²]	: 18.21
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.1
fs	: 9.97
Coefficiente di Sfruttamento	: 0.106
fs	: 9.39

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.066 (fs=15.125)

Taglio Ty di Progetto [daN]	: 1152
Taglio Tz di Progetto [daN]	: -4223
Momento Torcente Mt di Progetto [daNm]	: -461

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.05
Tensione di Progetto relativa a Tz [N/mm²]	: 0.17
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.066
fs	: 15.12

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 30	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm²	Tensione Critica nel piano XZ	: 148.97 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 1.46 N/mm²	Tensione fless. piano XZ	: 0.48 N/mm²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000

Coefficiente sfrutt. nel piano XY	: 0.073	Coefficiente sfrutt. nel piano XZ	: 0.027
Coeff. sfrutt. max euleriano	: 0.005		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.078	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.031
fs	: 12.842		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 52-54 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.076 (fs=13.075)

Sforzo Normale di Progetto [daN]	: -1284 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 3115
Momento Flettente Mz di Progetto [daNm]	: -1790

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.03
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.002
fs	: 530.23
Tensione di Progetto relativa a My [N/mm ²]	: 0.29
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.31
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.076
fs	: 13.08
Coefficiente di Sfruttamento a pressoflessione	: 0.076
fs	: 13.08

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.012 (fs=80.201)

Taglio Ty di Progetto [daN]	: 618
Taglio Tz di Progetto [daN]	: -1731
Momento Torcente Mt di Progetto [daNm]	: -430

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
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Tensione di Progetto relativa a Tz [N/mm ²]	: 0.07
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.028
fs	: 36.01
Tensione di Progetto [N/mm ²]	: 0.06
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.012
fs	: 85.49
Coefficiente di Sfruttamento a taglio+torsione	: 0.012
fs	: 80.2

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.31 N/mm ²	Tensione fless. piano XZ	: 0.29 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.065	Coefficiente sfrutt. nel piano XZ	: 0.016
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.067	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.018
fs	: 14.912		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 53-55 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.124 (fs=8.042)

Sforzo Normale di Progetto [daN]	: 2529 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 15456
Momento Flettente Mz di Progetto [daNm]	: -1554

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.07
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.005
fs	: 215.37
Tensione di Progetto relativa a My [N/mm ²]	: 1.46
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.13
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.12
fs	: 8.35
Coefficiente di Sfruttamento	: 0.124
fs	: 8.04

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.029 (fs=34.81)

Taglio Ty di Progetto [daN]	: -1861
Taglio Tz di Progetto [daN]	: 5678
Momento Torcente Mt di Progetto [daNm]	: -810

Tipo Verifica	: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.07
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.23
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.09
fs	: 11.08
Tensione di Progetto [N/mm ²]	: 0.11
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.021
fs	: 48.59
Coefficiente di Sfruttamento a taglio+torsione	: 0.029
fs	: 34.81

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 50	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.09 N/mm ²	Tensione fless. piano XZ	: 1.47 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.054	Coefficiente sfrutt. nel piano XZ	: 0.081
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.054	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.081
fs	: 12.420		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	

Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 54-56 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.096 (fs=10.439)

Sforzo Normale di Progetto [daN]	: 901 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 2424
Momento Flettente Mz di Progetto [daNm]	: -2344

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.02
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 604.34
Tensione di Progetto relativa a My [N/mm ²]	: 0.23
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.71
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.094
fs	: 10.62
Coefficiente di Sfruttamento	: 0.096
fs	: 10.44

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1320 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.023 (fs=44.185)

Taglio Ty di Progetto [daN]	: -1362
Taglio Tz di Progetto [daN]	: 625
Momento Torcente Mt di Progetto [daNm]	: -463

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.05
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.03
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.023
fs	: 44.18

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 38	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 12198561 daNm	Momento Critico nel piano XZ	: 1578637 daNm
Tensione Critica nel piano XY	: 8895.40 N/mm ²	Tensione Critica nel piano XZ	: 148.97 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.76 N/mm ²	Tensione fless. piano XZ	: 0.03 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.40

Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.088	Coefficiente sfrutt. nel piano XZ	: 0.002
Coeff. sfrutt. max euleriano	: 0.001		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.089	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.003
fs	: 11.191		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 55-57 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1590 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1590 mm / 1590 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.146 (fs=6.838)

Sforzo Normale di Progetto [daN]	: -3319 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -9020
Momento Flettente Mz di Progetto [daNm]	: -3117

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.09
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 205.17
Tensione di Progetto relativa a My [N/mm ²]	: 0.85
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.27
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.146
fs	: 6.84
Coefficiente di Sfruttamento a pressoflessione	: 0.146
fs	: 6.84

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1590 mm / 1590 mm] - **R 220x1700**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.098 (fs=10.19)

Taglio Ty di Progetto [daN]	: -104
Taglio Tz di Progetto [daN]	: -1612
Momento Torcente Mt di Progetto [daNm]	: 105

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.06
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.038
fs	: 26.09
Tensione di Progetto [N/mm ²]	: 0.33
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a torsione	: 0.097
fs	: 10.34
Coefficiente di Sfruttamento a taglio+torsione	: 0.098
fs	: 10.19

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1590.0	Lunghezza efficace nel piano XZ	: 1590.0
Momento Critico nel piano XY	: 10127108 daNm	Momento Critico nel piano XZ	: 1310567 daNm
Tensione Critica nel piano XY	: 7384.86 N/mm ²	Tensione Critica nel piano XZ	: 123.68 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.27 N/mm ²	Tensione fless. piano XZ	: 0.85 N/mm ²
Snellezza relativa nel piano XY	: 0.06	Snellezza relativa nel piano XZ	: 0.44
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.114	Coefficiente sfrutt. nel piano XZ	: 0.047
Coeff. sfrutt. max euleriano	: 0.005		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.118	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.052
fs	: 8.448		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1590.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -157.1 daN/m	-	
-		Carico distribuito Finale	: -157.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.180 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.543 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.300 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 56-70 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1590 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1590 mm / 1590 mm] - **R 220x1700**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.136 (fs=7.327)

Sforzo Normale di Progetto [daN]	: -1006 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -1080
Momento Flettente Mz di Progetto [daNm]	: 3641

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.03
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.001
fs	: 677.21
Tensione di Progetto relativa a My [N/mm ²]	: 0.1
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.65
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.136
fs	: 7.33
Coefficiente di Sfruttamento a pressoflessione	: 0.136
fs	: 7.33

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1590 mm / 1590 mm] - **R 220x1700**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.098 (fs=10.201)

Taglio Ty di Progetto [daN]	: 139
Taglio Tz di Progetto [daN]	: -1679
Momento Torcente Mt di Progetto [daNm]	: -139

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.07
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.04
fs	: 25
Tensione di Progetto [N/mm ²]	: 0.33
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a torsione	: 0.096
fs	: 10.37
Coefficiente di Sfruttamento a taglio+torsione	: 0.098
fs	: 10.2

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1590.0	Lunghezza efficace nel piano XZ	: 1590.0
Momento Critico nel piano XY	: 10127108 daNm	Momento Critico nel piano XZ	: 1310567 daNm
Tensione Critica nel piano XY	: 7384.86 N/mm ²	Tensione Critica nel piano XZ	: 123.68 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.65 N/mm ²	Tensione fless. piano XZ	: 0.10 N/mm ²
Snellezza relativa nel piano XY	: 0.06	Snellezza relativa nel piano XZ	: 0.44
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.133	Coefficiente sfrutt. nel piano XZ	: 0.006
Coeff. sfrutt. max euleriano	: 0.001		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.134	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.007
fs	: 7.460		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1590.0 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -157.1 daN/m
-	
Freccia Istantanea - COMBINAZIONE	

Schema adottato Doppio Incastro	
Peso proprio	: -144.0 daN/m
-	
Carico distribuito Finale	: -157.1 daN/m
Comb 42 [CAR] [ST]	

Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.180 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.543 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.300 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 57-58 Copert[Trave]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1662.44 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1662.44 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.129 (fs=7.772)

Sforzo Normale di Progetto [daN]	: 3063 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 1944
Momento Flettente Mz di Progetto [daNm]	: -3185

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.08
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.006
fs	: 177.83
Tensione di Progetto relativa a My [N/mm ²]	: 0.18
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.32
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.123
fs	: 8.13
Coefficiente di Sfruttamento	: 0.129
fs	: 7.77

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1662.44 mm / 1662.44 mm] - **R 220x1700**

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.133 (fs=7.547)

Taglio Ty di Progetto [daN]	: -1258
Taglio Tz di Progetto [daN]	: -399
Momento Torcente Mt di Progetto [daNm]	: 1330

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.05
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.02
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.02
fs	: 50.15
Tensione di Progetto [N/mm ²]	: 0.7
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.132
fs	: 7.57
Coefficiente di Sfruttamento a taglio+torsione	: 0.133
fs	: 7.55

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1662.4	Lunghezza efficace nel piano XZ	: 1662.4
Momento Critico nel piano XY	: 9685836 daNm	Momento Critico nel piano XZ	: 1253461 daNm
Tensione Critica nel piano XY	: 7063.08 N/mm ²	Tensione Critica nel piano XZ	: 118.29 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.32 N/mm ²	Tensione fless. piano XZ	: 0.18 N/mm ²
Snellezza relativa nel piano XY	: 0.06	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.116	Coefficiente sfrutt. nel piano XZ	: 0.010
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.116	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.010
fs	: 8.622		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1662.4 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.325 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.750 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.541 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 58-59 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.102 (fs=9.761)

Sforzo Normale di Progetto [daN]	: 372 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -2988
Momento Flettente Mz di Progetto [daNm]	: -2497

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.01
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.001
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 0.28
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.82
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.102
fs	: 9.83
Coefficiente di Sfruttamento	: 0.102
fs	: 9.76

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.023 (fs=43.791)

Taglio Ty di Progetto [daN] : 455
 Taglio Tz di Progetto [daN] : 1237
 Momento Torcente Mt di Progetto [daNm] : -1604

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
 Tensione di Progetto relativa a Tz [N/mm²] : 0.05
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.02
 fs : 50.22
 Tensione di Progetto [N/mm²] : 0.12
 Modulo di resistenza a torsione [mm³] : 25450510
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.022
 fs : 44.57
 Coefficiente di Sfruttamento a taglio+torsione : 0.023
 fs : 43.79

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 18	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mmq	Tensione Critica nel piano XZ	: 142.50 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.21 N/mmq
Tensione fless. piano XY	: 1.82 N/mmq	Tensione fless. piano XZ	: 0.28 N/mmq
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.091	Coefficiente sfrutt. nel piano XZ	: 0.015
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.091	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.015
fs	: 10.998		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 59-60 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.102 (fs=9.782)

Sforzo Normale di Progetto [daN] : 216 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -3011
 Momento Flettente Mz di Progetto [daNm] : -2497

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.01
 Tensione Resistente [N/mm²] : 14.57
 Coefficiente di Sfruttamento a trazione : 0.000
 fs : 1000
 Tensione di Progetto relativa a My [N/mm²] : 0.28
 Tensione di Progetto relativa a Mz [N/mm²] : 1.82
 Tensione Resistente relativa a My [N/mm²] : 18.21
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.102
 fs : 9.82
 Coefficiente di Sfruttamento : 0.102
 fs : 9.78

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.024 (fs=41.421)

Taglio Ty di Progetto [daN] : 1287
 Taglio Tz di Progetto [daN] : -1187
 Momento Torcente Mt di Progetto [daNm] : 36

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.05
 Tensione di Progetto relativa a Tz [N/mm²] : 0.05
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.026
 fs : 37.81
 Tensione di Progetto [N/mm²] : 0.12
 Modulo di resistenza a torsione [mm³] : 25450510
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.023
 fs : 42.66
 Coefficiente di Sfruttamento a taglio+torsione : 0.024
 fs : 41.42

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 18
 Lunghezza efficace nel piano XY : 1380.0
 Momento Critico nel piano XY : 11668189 daNm
 Tensione Critica nel piano XY : 8508.65 N/mmq
 Resistenza fless. piano XY : 20.03 N/mmq
 Tensione fless. piano XY : 1.82 N/mmq
 Snellezza relativa nel piano XY : 0.05
 Coeff. Riduttivo nel piano XY : 1.000
 Coefficiente sfrutt. nel piano XY : 0.091
 Coeff. sfrutt. max euleriano : 0.000
 Coeff. sfrutt. TOTALE (Piano XY) : 0.091
 fs : 11.001

Sezione più sfavorevole : 1
 Lunghezza efficace nel piano XZ : 1380.0
 Momento Critico nel piano XZ : 1510001 daNm
 Tensione Critica nel piano XZ : 142.50 N/mmq
 Resistenza fless. piano XZ : 18.21 N/mmq
 Tensione fless. piano XZ : 0.28 N/mmq
 Snellezza relativa nel piano XZ : 0.41
 Coeff. Riduttivo nel piano XZ : 1.000
 Coefficiente sfrutt. nel piano XZ : 0.016
 Coeff. sfrutt. TOTALE (Piano XZ) : 0.016

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 60-61 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.084 (fs=11.888)

Sforzo Normale di Progetto [daN]	: 943 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -2023
Momento Flettente Mz di Progetto [daNm]	: 2061

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.03
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 577.37
Tensione di Progetto relativa a My [N/mm ²]	: 0.19
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.5
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.082
fs	: 12.14
Coefficiente di Sfruttamento	: 0.084
fs	: 11.89

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.03 (fs=33.533)

Taglio Ty di Progetto [daN]	: 1197
Taglio Tz di Progetto [daN]	: -631
Momento Torcente Mt di Progetto [daNm]	: -100

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.05
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.03
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.02
fs	: 48.92
Tensione di Progetto [N/mm ²]	: 0.16
Modulo di resistenza a torsione [mm ³]	: 25450510

Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.029
fs	: 34.01
Coefficiente di Sfruttamento a taglio+torsione	: 0.03
fs	: 33.53

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 50	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.49 N/mm ²	Tensione fless. piano XZ	: 0.10 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.074	Coefficiente sfrutt. nel piano XZ	: 0.005
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.076	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.007
fs	: 13.162		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 61-62 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.093 (fs=10.75)

Sforzo Normale di Progetto [daN]	: 2601 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -1877
Momento Flettente Mz di Progetto [daNm]	: 2237

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.07
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.005
fs	: 209.42
Tensione di Progetto relativa a My [N/mm ²]	: 0.18
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.63

Tensione Resistente relativa a M_y [N/mm ²]	: 18.21
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.088
f_s	: 11.33
Coefficiente di Sfruttamento	: 0.093
f_s	: 10.75

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.025 ($f_s=39.945$)

Taglio T_y di Progetto [daN]	: 513
Taglio T_z di Progetto [daN]	: 262
Momento Torcente M_t di Progetto [daNm]	: -81

Tipo Verifica	: TAGLIO+TORSIONE
Tensione di Progetto relativa a T_y [N/mm ²]	: 0.02
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.01
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.009
f_s	: 114.97
Tensione di Progetto [N/mm ²]	: 0.13
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.025
f_s	: 40.07
Coefficiente di Sfruttamento a taglio+torsione	: 0.025
f_s	: 39.94

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 50	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.78 N/mm ²	Tensione fless. piano XZ	: 0.05 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.089	Coefficiente sfrutt. nel piano XZ	: 0.003
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.091	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.004
f_s	: 11.006		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000

Fatt. sicurezza freccia Finale : 1000.000

Fatt. sicurezza : 1000.000

Campata 62-63 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 25 [SLD] [IN] " - Coeff. Sfruttamento : 0.093 (fs=10.808)

Sforzo Normale di Progetto [daN] : 1537 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : -110

Momento Flettente Mz di Progetto [daNm] : 2453

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.04

Tensione Resistente [N/mm²] : 14.57

Coefficiente di Sfruttamento a trazione : 0.003

fs : 354.49

Tensione di Progetto relativa a My [N/mm²] : 0.01

Tensione di Progetto relativa a Mz [N/mm²] : 1.79

Tensione Resistente relativa a My [N/mm²] : 18.21

Tensione Resistente relativa a Mz [N/mm²] : 20.03

Coefficiente di Sfruttamento a flessione : 0.09

fs : 11.15

Coefficiente di Sfruttamento : 0.093

fs : 10.81

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.02 (fs=49.784)

Taglio Ty di Progetto [daN] : -488

Taglio Tz di Progetto [daN] : 460

Momento Torcente Mt di Progetto [daNm] : -207

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.02

Tensione di Progetto relativa a Tz [N/mm²] : 0.02

Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a taglio : 0.01

fs : 98.78

Tensione di Progetto [N/mm²] : 0.11

Modulo di resistenza a torsione [mm³] : 25450510

Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a torsione : 0.02

fs : 50.04

Coefficiente di Sfruttamento a taglio+torsione : 0.02

fs : 49.78

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 50

Lunghezza efficace nel piano XY : 1380.0

Momento Critico nel piano XY : 11668189 daNm

Tensione Critica nel piano XY : 8508.65 N/mmq

Resistenza fless. piano XY : 20.03 N/mmq

Tensione fless. piano XY : 1.78 N/mmq

Sezione più sfavorevole : 1

Lunghezza efficace nel piano XZ : 1380.0

Momento Critico nel piano XZ : 1510001 daNm

Tensione Critica nel piano XZ : 142.50 N/mmq

Resistenza fless. piano XZ : 18.21 N/mmq

Tensione fless. piano XZ : 0.05 N/mmq

Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.089	Coefficiente sfrutt. nel piano XZ	: 0.003
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.091	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.005
fs	: 10.986		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 63-64 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.086 (fs=11.572)

Sforzo Normale di Progetto [daN]	: 2360 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 13
Momento Flettente Mz di Progetto [daNm]	: 2253

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.06
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.004
fs	: 230.87
Tensione di Progetto relativa a My [N/mm ²]	: 0.00
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.64
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.082
fs	: 12.18
Coefficiente di Sfruttamento	: 0.086
fs	: 11.57

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.03 (fs=33.46)

Taglio Ty di Progetto [daN]	: -562
Taglio Tz di Progetto [daN]	: -597
Momento Torcente Mt di Progetto [daNm]	: 915

Tipo Verifica		: TAGLIO+TORSIONE
Tensione di Progetto relativa a T_y [N/mm ²]		: 0.02
Tensione di Progetto relativa a T_z [N/mm ²]		: 0.02
Tensione tang. Resistente [N/mm ²]		: 2.66
Coefficiente di Sfruttamento a taglio		: 0.012
f_s		: 80.7
Tensione di Progetto [N/mm ²]		: 0.16
Modulo di resistenza a torsione [mm ³]		: 25450510
Tensione tang. Resistente [N/mm ²]		: 2.66
Coefficiente di Sfruttamento a torsione		: 0.03
f_s		: 33.63
Coefficiente di Sfruttamento a taglio+torsione		: 0.03
f_s		: 33.46

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.64 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.082	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.082	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.000
f_s	: 12.190		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 64-65 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.109 ($f_s=9.137$)

Sforzo Normale di Progetto [daN]	: 2451 (TRAZIONE)
Momento Flettente M_y di Progetto [daNm]	: 772
Momento Flettente M_z di Progetto [daNm]	: 2805

Tipo Verifica : TRAZIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto $[N/mm^2]$: 0.07
Tensione Resistente $[N/mm^2]$: 14.57
Coefficiente di Sfruttamento a trazione	: 0.004
f_s	: 222.24
Tensione di Progetto relativa a M_y $[N/mm^2]$: 0.07
Tensione di Progetto relativa a M_z $[N/mm^2]$: 2.05
Tensione Resistente relativa a M_y $[N/mm^2]$: 18.21
Tensione Resistente relativa a M_z $[N/mm^2]$: 20.03
Coefficiente di Sfruttamento a flessione	: 0.105
f_s	: 9.53
Coefficiente di Sfruttamento	: 0.109
f_s	: 9.14

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - $[X=1380 \text{ mm} / 1380 \text{ mm}]$ - **R 220x1700**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.024 ($f_s=41.159$)

Taglio T_y di Progetto [daN]	: -378
Taglio T_z di Progetto [daN]	: -621
Momento Torcente M_t di Progetto [daNm]	: 1001

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a T_y $[N/mm^2]$: 0.02
Tensione di Progetto relativa a T_z $[N/mm^2]$: 0.02
Tensione tang. Resistente $[N/mm^2]$: 2.66
Coefficiente di Sfruttamento a taglio	: 0.011
f_s	: 91.1
Tensione di Progetto $[N/mm^2]$: 0.13
Modulo di resistenza a torsione $[mm^3]$: 25450510
Tensione tang. Resistente $[N/mm^2]$: 2.66
Coefficiente di Sfruttamento a torsione	: 0.024
f_s	: 41.36
Coefficiente di Sfruttamento a taglio+torsione	: 0.024
f_s	: 41.16

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.05 N/mm ²	Tensione fless. piano XZ	: 0.07 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.102	Coefficiente sfrutt. nel piano XZ	: 0.004
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.102	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.004
f_s	: 9.790		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale ($t \rightarrow \infty$)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m

Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 65-66 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.11 ($f_s=9.112$)

Sforzo Normale di Progetto [daN]	: 2253 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 751
Momento Flettente Mz di Progetto [daNm]	: 2826

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.06
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.004
f_s	: 241.76
Tensione di Progetto relativa a My [N/mm ²]	: 0.07
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.06
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.106
f_s	: 9.47
Coefficiente di Sfruttamento	: 0.11
f_s	: 9.11

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.029 ($f_s=34.852$)

Taglio Ty di Progetto [daN]	: -705
Taglio Tz di Progetto [daN]	: -813
Momento Torcente Mt di Progetto [daNm]	: -376

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.03
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.016
f_s	: 61.52
Tensione di Progetto [N/mm ²]	: 0.15
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.028
f_s	: 35.18
Coefficiente di Sfruttamento a taglio+torsione	: 0.029
f_s	: 34.85

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.06 N/mm ²	Tensione fless. piano XZ	: 0.07 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.103	Coefficiente sfrutt. nel piano XZ	: 0.004
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.103	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.004
fs	: 9.719		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 66-67 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.076 (fs=13.097)

Sforzo Normale di Progetto [daN]	: 2126 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -734
Momento Flettente Mz di Progetto [daNm]	: 1917

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.06
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.004
fs	: 256.26
Tensione di Progetto relativa a My [N/mm ²]	: 0.07
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.4
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.072
fs	: 13.8
Coefficiente di Sfruttamento	: 0.076
fs	: 13.1

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.028 (fs=35.467)

Taglio Ty di Progetto [daN] : -1388
 Taglio Tz di Progetto [daN] : 523
 Momento Torcente Mt di Progetto [daNm] : -379

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.06
 Tensione di Progetto relativa a Tz [N/mm²] : 0.02
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.022
 fs : 44.63
 Tensione di Progetto [N/mm²] : 0.15
 Modulo di resistenza a torsione [mm³] : 25450510
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.028
 fs : 36.11
 Coefficiente di Sfruttamento a taglio+torsione : 0.028
 fs : 35.47

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.40 N/mm ²	Tensione fless. piano XZ	: 0.07 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.070	Coefficiente sfrutt. nel piano XZ	: 0.004
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.070	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.004
fs	: 14.329		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 67-68 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.133)

Sforzo Normale di Progetto [daN]	: 1347 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -2693
Momento Flettente Mz di Progetto [daNm]	: -2671

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.04
Tensione Resistente [N/mm²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 404.3
Tensione di Progetto relativa a My [N/mm²]	: 0.25
Tensione di Progetto relativa a Mz [N/mm²]	: 1.95
Tensione Resistente relativa a My [N/mm²]	: 18.21
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.107
fs	: 9.34
Coefficiente di Sfruttamento	: 0.109
fs	: 9.13

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.03 (fs=32.981)

Taglio Ty di Progetto [daN]	: 930
Taglio Tz di Progetto [daN]	: 1278
Momento Torcente Mt di Progetto [daNm]	: 64

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm²]	: 0.05
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.024
fs	: 41.89
Tensione di Progetto [N/mm²]	: 0.16
Modulo di resistenza a torsione [mm³]	: 25450510
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.03
fs	: 33.61
Coefficiente di Sfruttamento a taglio+torsione	: 0.03
fs	: 32.98

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mmq	Tensione Critica nel piano XZ	: 142.50 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.21 N/mmq
Tensione fless. piano XY	: 2.03 N/mmq	Tensione fless. piano XZ	: 0.12 N/mmq
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.101	Coefficiente sfrutt. nel piano XZ	: 0.007
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.101	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.007
fs	: 9.875		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 68-69 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1380 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1380 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.114 (fs=8.806)

Sforzo Normale di Progetto [daN]	: 1552 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -3173
Momento Flettente Mz di Progetto [daNm]	: -2724

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.04
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.003
fs	: 351
Tensione di Progetto relativa a My [N/mm ²]	: 0.3
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.99
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.111
fs	: 9.03
Coefficiente di Sfruttamento	: 0.114
fs	: 8.81

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1380 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.032 (fs=31.617)

Taglio Ty di Progetto [daN]	: 972
Taglio Tz di Progetto [daN]	: 1452
Momento Torcente Mt di Progetto [daNm]	: -1234

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.06
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.026
fs	: 37.89
Tensione di Progetto [N/mm ²]	: 0.16

Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.031
fs	: 32.33
Coefficiente di Sfruttamento a taglio+torsione	: 0.032
fs	: 31.62

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1380.0	Lunghezza efficace nel piano XZ	: 1380.0
Momento Critico nel piano XY	: 11668189 daNm	Momento Critico nel piano XZ	: 1510001 daNm
Tensione Critica nel piano XY	: 8508.65 N/mm ²	Tensione Critica nel piano XZ	: 142.50 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.13 N/mm ²	Tensione fless. piano XZ	: 0.10 N/mm ²
Snellezza relativa nel piano XY	: 0.05	Snellezza relativa nel piano XZ	: 0.41
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.106	Coefficiente sfrutt. nel piano XZ	: 0.005
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.106	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.005
fs	: 9.413		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1380.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 2.760 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 3.943 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 4.600 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 69-70 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1662.44 mm - **R 220x1700** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1662.44 mm / 1662.44 mm] - **R 220x1700**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.142 (fs=7.067)

Sforzo Normale di Progetto [daN]	: 2001 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 665
Momento Flettente Mz di Progetto [daNm]	: -3719

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.05
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.004
fs	: 272.19
Tensione di Progetto relativa a My [N/mm ²]	: 0.06

Tensione di Progetto relativa a M_z [N/mm ²]	: 2.71
Tensione Resistente relativa a M_y [N/mm ²]	: 18.21
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.138
f_s	: 7.25
Coefficiente di Sfruttamento	: 0.142
f_s	: 7.07

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1662.44 mm / 1662.44 mm] - **R 220x1700**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.035 ($f_s=28.903$)

Taglio T_y di Progetto [daN]	: -264
Taglio T_z di Progetto [daN]	: -1050
Momento Torcente M_t di Progetto [daNm]	: -3414

Tipo Verifica	: TAGLIO+TORSIONE
Tensione di Progetto relativa a T_y [N/mm ²]	: 0.01
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.04
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.016
f_s	: 61.16
Tensione di Progetto [N/mm ²]	: 0.18
Modulo di resistenza a torsione [mm ³]	: 25450510
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.034
f_s	: 29.13
Coefficiente di Sfruttamento a taglio+torsione	: 0.035
f_s	: 28.9

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1662.4	Lunghezza efficace nel piano XZ	: 1662.4
Momento Critico nel piano XY	: 9685836 daNm	Momento Critico nel piano XZ	: 1253461 daNm
Tensione Critica nel piano XY	: 7063.08 N/mm ²	Tensione Critica nel piano XZ	: 118.29 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.71 N/mm ²	Tensione fless. piano XZ	: 0.06 N/mm ²
Snellezza relativa nel piano XY	: 0.06	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.135	Coefficiente sfrutt. nel piano XZ	: 0.003
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.135	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.003
f_s	: 7.384		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1662.4 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -144.0 daN/m
Carico distribuito Istantaneo	: -361.8 daN/m	-	
-		Carico distribuito Finale	: -263.8 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.325 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.750 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.541 mm

Fatt. sicurezza freccia Istantanea : 1000.000
Fatt. sicurezza freccia Finale : 1000.000

Fatt. sicurezza freccia Netta Finale : 1000.000
Fatt. sicurezza : 1000.000

Campata 1-74 Copertu[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.525 (fs=1.905)

Sforzo Normale di Progetto [daN] : 1233 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 0
Momento Flettente Mz di Progetto [daNm] : -272

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.86
Tensione Resistente [N/mm²] : 16.02
Coefficiente di Sfruttamento a trazione : 0.053
fs : 18.71
Tensione di Progetto relativa a My [N/mm²] : 0
Tensione di Progetto relativa a Mz [N/mm²] : 9.44
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.472
fs : 2.12
Coefficiente di Sfruttamento : 0.525
fs : 1.9

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa : 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.069 (fs=14.5)

Taglio Ty di Progetto [daN] : 176
Taglio Tz di Progetto [daN] : -3
Momento Torcente Mt di Progetto [daNm] : -122

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.069
fs : 14.5

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 47.52	Snellezza nel piano XZ	: 67.89
Snellezza relativa nel piano XY	: 0.76	Snellezza relativa nel piano XZ	: 1.08
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 43
Coefficiente K nel piano XY	: 0.81	Coefficiente K nel piano XZ	: 1.12
Coefficiente Kc nel piano XY	: 0.91	Coefficiente Kc nel piano XZ	: 0.70
Coefficiente di sfruttamento nel piano XY	: 0.524	Coefficiente di sfruttamento nel piano XZ	: 0.534
fs	: 1.874		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 43

Sezione più sfavorevole : 1

Lunghezza efficace nel piano XY	: 2351.8	Lunghezza efficace nel piano XZ	: 2351.8
Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mm ²	Tensione Critica nel piano XZ	: 289.24 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 9.85 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.492	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.042		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.534	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.042
fs	: 1.874		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto			
Lunghezza elemento	: 2351.8 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.232 mm	Limite Freccia Istantanea L/500	: 4.704 mm
Freccia Netta Finale	: -0.418 mm	Limite Freccia Netta Fin. L/ 350	: 6.719 mm
Freccia Finale	: -0.418 mm	Limite Freccia Finale L/ 300	: 7.839 mm
Fatt. sicurezza freccia Istantanea	: 20.243	Fatt. sicurezza freccia Netta Finale	: 16.066
Fatt. sicurezza freccia Finale	: 18.744	Fatt. sicurezza	: 16.066

Campata 74-2 Copertu[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.233 (fs=4.291)

Sforzo Normale di Progetto [daN]	: 1461 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 98

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1.01
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.063
fs	: 15.8
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.4
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.17
fs	: 5.89
Coefficiente di Sfruttamento	: 0.233
fs	: 4.29

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.014 (fs=72.501)

Taglio Ty di Progetto [daN] : -35
 Taglio Tz di Progetto [daN] : -3
 Momento Torcente Mt di Progetto [daNm] : -29

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.04
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.014
 fs : 72.5

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 47.52	Snellezza nel piano XZ	: 67.89
Snellezza relativa nel piano XY	: 0.76	Snellezza relativa nel piano XZ	: 1.08
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 38
Coefficiente K nel piano XY	: 0.81	Coefficiente K nel piano XZ	: 1.12
Coefficiente Kc nel piano XY	: 0.91	Coefficiente Kc nel piano XZ	: 0.70
Coefficiente di sfruttamento nel piano XY	: 0.257	Coefficiente di sfruttamento nel piano XZ	: 0.284
fs	: 3.517		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 38	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2351.8	Lunghezza efficace nel piano XZ	: 2351.8
Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mm²	Tensione Critica nel piano XZ	: 289.24 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 3.37 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.168	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.116		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.284	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.116
fs	: 3.517		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2351.8 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.232 mm	Limite Freccia Istantanea L/500	: 4.704 mm
Freccia Netta Finale	: -0.418 mm	Limite Freccia Netta Fin. L/ 350	: 6.719 mm
Freccia Finale	: -0.418 mm	Limite Freccia Finale L/ 300	: 7.839 mm
Fatt. sicurezza freccia Istantanea	: 20.243	Fatt. sicurezza freccia Netta Finale	: 16.066
Fatt. sicurezza freccia Finale	: 18.744	Fatt. sicurezza	: 16.066

Campata 6-71 Copertu[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
 L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**
Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.138 (fs=7.254)
 Sforzo Normale di Progetto [daN] : 1378 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : 45

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.96
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.06
 fs : 16.74
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 1.56
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.078
 fs : 12.8
 Coefficiente di Sfruttamento : 0.138
 fs : 7.25

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**
Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.014 (fs=72.385)
 Taglio Ty di Progetto [daN] : -35
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : 45

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.04
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.014
 fs : 72.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 66.56
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 1.06
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 1.10
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.72
Coefficiente di sfruttamento nel piano XY	: 0.138	Coefficiente di sfruttamento nel piano XZ	: 0.160
fs	: 6.251		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 21	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm
Tensione Critica nel piano XY	: 295.02 N/mm ²	Tensione Critica nel piano XZ	: 295.02 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.20 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000

Coefficiente sfrutt. nel piano XY	: 0.060	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.100		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.160	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.100
fs	: 6.251		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2305.7 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.215 mm	Limite Freccia Istantanea L/500	: 4.611 mm
Freccia Netta Finale	: -0.386 mm	Limite Freccia Netta Fin. L/ 350	: 6.588 mm
Freccia Finale	: -0.386 mm	Limite Freccia Finale L/ 300	: 7.686 mm
Fatt. sicurezza freccia Istantanea	: 21.482	Fatt. sicurezza freccia Netta Finale	: 17.050
Fatt. sicurezza freccia Finale	: 19.891	Fatt. sicurezza	: 17.050

Campata 71-7 Copertu[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.125 (fs=7.971)

Sforzo Normale di Progetto [daN]	: 1341 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -39

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.93
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.058
fs	: 17.21
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.35
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.067
fs	: 14.85
Coefficiente di Sfruttamento	: 0.125
fs	: 7.97

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa : 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.01 (fs=96.388)

Taglio Ty di Progetto [daN]	: 26
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -16

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
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TABULATI DI CALCOLO -

Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.01
f_s	: 96.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 66.56
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 1.06
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 1.10
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.72
Coefficiente di sfruttamento nel piano XY	: 0.130	Coefficiente di sfruttamento nel piano XZ	: 0.152
f_s	: 6.562		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm
Tensione Critica nel piano XY	: 295.02 N/mm ²	Tensione Critica nel piano XZ	: 295.02 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.01 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.051	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.102		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.152	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.102
f_s	: 6.562		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2305.7 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.215 mm	Limite Freccia Istantanea L/500	: 4.611 mm
Freccia Netta Finale	: -0.386 mm	Limite Freccia Netta Fin. L/ 350	: 6.588 mm
Freccia Finale	: -0.386 mm	Limite Freccia Finale L/ 300	: 7.686 mm
Fatt. sicurezza freccia Istantanea	: 21.482	Fatt. sicurezza freccia Netta Finale	: 17.050
Fatt. sicurezza freccia Finale	: 19.891	Fatt. sicurezza	: 17.050

Campata 9-72 Copertu[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.132 ($f_s=7.557$)

Sforzo Normale di Progetto [daN] : 1499 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : -39

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 1.04
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.065
 fs : 15.4
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 1.35
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.067
 fs : 14.84
 Coefficiente di Sfruttamento : 0.132
 fs : 7.56

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.012 (fs=86.72)

Taglio Ty di Progetto [daN] : -29
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : 38

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.012
 fs : 86.72

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 66.56
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 1.06
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 1.10
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.72
Coefficiente di sfruttamento nel piano XY	: 0.134	Coefficiente di sfruttamento nel piano XZ	: 0.157
fs	: 6.389		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 21	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm
Tensione Critica nel piano XY	: 295.02 N/mm ²	Tensione Critica nel piano XZ	: 295.02 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.07 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.054	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.103		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.157	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.103
fs	: 6.389		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 2305.7 mm

Comb. di carico più gravosa : 142

Carico distribuito Istantaneo : -6.0 daN/m

-

Freccia Istantanea - COMBINAZIONE

Freccia Finale - COMBINAZIONE

Modulo Elastico istantaneo : 11500.0 N/mm²

Controfreccia : 0.000 mm

Freccia Istantanea : -0.215 mm

Freccia Netta Finale : -0.386 mm

Freccia Finale : -0.386 mm

Fatt. sicurezza freccia Istantanea : 21.482

Fatt. sicurezza freccia Finale : 19.891

Schema adottato Doppia Cerniera

Peso proprio : -5.5 daN/m

-

Carico distribuito Finale : -6.0 daN/m

Comb 42 [CAR] [ST]

Comb 2 [SLEQP] [PE]

Modulo Elastico finale : 6388.9 N/mm²

Limite Freccia Istantanea L/500 : 4.611 mm

Limite Freccia Netta Fin. L/ 350 : 6.588 mm

Limite Freccia Finale L/ 300 : 7.686 mm

Fatt. sicurezza freccia Netta Finale : 17.050

Fatt. sicurezza : 17.050

Campata 72-10 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.11 (fs=9.058)

Sforzo Normale di Progetto [daN] : 1691 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : 0

Momento Flettente Mz di Progetto [daNm] : 21

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 1.17

Tensione Resistente [N/mm²] : 16.02

Coefficiente di Sfruttamento a trazione : 0.073

fs : 13.65

Tensione di Progetto relativa a My [N/mm²] : 0

Tensione di Progetto relativa a Mz [N/mm²] : 0.74

Tensione Resistente relativa a My [N/mm²] : 20.03

Tensione Resistente relativa a Mz [N/mm²] : 20.03

Coefficiente di Sfruttamento a flessione : 0.037

fs : 26.94

Coefficiente di Sfruttamento : 0.11

fs : 9.06

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.006 (fs=171.545)

Taglio Ty di Progetto [daN] : 15

Taglio Tz di Progetto [daN] : -2

Momento Torcente Mt di Progetto [daNm] : 10

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02

Tensione di Progetto relativa a Tz [N/mm²] : 0.00

Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a taglio : 0.006

fs : 171.54

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 66.56
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 1.06
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 38
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 1.10
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.72
Coefficiente di sfruttamento nel piano XY	: 0.118	Coefficiente di sfruttamento nel piano XZ	: 0.138
fs	: 7.262		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 38	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm
Tensione Critica nel piano XY	: 295.02 N/mm ²	Tensione Critica nel piano XZ	: 295.02 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.92 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.046	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.092		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.138	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.092
fs	: 7.262		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2305.7 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.215 mm	Limite Freccia Istantanea L/500	: 4.611 mm
Freccia Netta Finale	: -0.386 mm	Limite Freccia Netta Fin. L/ 350	: 6.588 mm
Freccia Finale	: -0.386 mm	Limite Freccia Finale L/ 300	: 7.686 mm
Fatt. sicurezza freccia Istantanea	: 21.482	Fatt. sicurezza freccia Netta Finale	: 17.050
Fatt. sicurezza freccia Finale	: 19.891	Fatt. sicurezza	: 17.050

Campata 73-13 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.095 (fs=10.524)

Sforzo Normale di Progetto [daN]	: 1006 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -30

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.7
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.044

fs	: 22.94
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.03
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.051
fs	: 19.44
Coefficiente di Sfruttamento	: 0.095
fs	: 10.52

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.011 (fs=92.75)

Taglio Ty di Progetto [daN]	: 27
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: -17

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.011
fs	: 92.75

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 47.52	Snellezza nel piano XZ	: 67.89
Snellezza relativa nel piano XY	: 0.76	Snellezza relativa nel piano XZ	: 1.08
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.81	Coefficiente K nel piano XZ	: 1.12
Coefficiente Kc nel piano XY	: 0.91	Coefficiente Kc nel piano XZ	: 0.70
Coefficiente di sfruttamento nel piano XY	: 0.109	Coefficiente di sfruttamento nel piano XZ	: 0.132
fs	: 7.589		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 21	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2351.8	Lunghezza efficace nel piano XZ	: 2351.8
Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mm ²	Tensione Critica nel piano XZ	: 289.24 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.64 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.032	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.100		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.132	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.100
fs	: 7.589		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2351.8 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -6.0 daN/m
-	
Freccia Istantanea - COMBINAZIONE	

Schema adottato Doppia Cerniera	
Peso proprio	: -5.5 daN/m
-	
Carico distribuito Finale	: -6.0 daN/m
Comb 42 [CAR] [ST]	

Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.232 mm	Limite Freccia Istantanea L/500	: 4.704 mm
Freccia Netta Finale	: -0.418 mm	Limite Freccia Netta Fin. L/ 350	: 6.719 mm
Freccia Finale	: -0.418 mm	Limite Freccia Finale L/ 300	: 7.839 mm
Fatt. sicurezza freccia Istantanea	: 20.243	Fatt. sicurezza freccia Netta Finale	: 16.066
Fatt. sicurezza freccia Finale	: 18.744	Fatt. sicurezza	: 16.066

Campata 14-73 Copert[Asta GEN.]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.178 (fs=5.609)

Sforzo Normale di Progetto [daN]	: 1779 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -58

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1.24
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.077
fs	: 12.97
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.03
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.101
fs	: 9.88
Coefficiente di Sfruttamento	: 0.178
fs	: 5.61

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.02 (fs=50.299)

Taglio Ty di Progetto [daN]	: -51
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: 46

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.05
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.02
fs	: 50.3

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 47.52	Snellezza nel piano XZ	: 67.89
Snellezza relativa nel piano XY	: 0.76	Snellezza relativa nel piano XZ	: 1.08
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 6
Coefficiente K nel piano XY	: 0.81	Coefficiente K nel piano XZ	: 1.12
Coefficiente Kc nel piano XY	: 0.91	Coefficiente Kc nel piano XZ	: 0.70
Coefficiente di sfruttamento nel piano XY	: 0.151	Coefficiente di sfruttamento nel piano XZ	: 0.174

fs : 5.764

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2351.8	Lunghezza efficace nel piano XZ	: 2351.8
Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mm ²	Tensione Critica nel piano XZ	: 289.24 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.58 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.079	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.095		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.174	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.095
fs	: 5.764		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2351.8 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.232 mm	Limite Freccia Istantanea L/500	: 4.704 mm
Freccia Netta Finale	: -0.418 mm	Limite Freccia Netta Fin. L/ 350	: 6.719 mm
Freccia Finale	: -0.418 mm	Limite Freccia Finale L/ 300	: 7.839 mm
Fatt. sicurezza freccia Istantanea	: 20.243	Fatt. sicurezza freccia Netta Finale	: 16.066
Fatt. sicurezza freccia Finale	: 18.744	Fatt. sicurezza	: 16.066

Campata 57-75 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE GL24h (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - R 120x120 - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2351.79 mm] - R 120x120

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.492 (fs=2.033)

Sforzo Normale di Progetto [daN]	: -147 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -284

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.1
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.006
fs	: 178.19
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 9.85
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.492
fs	: 2.03

Coefficiente di Sfruttamento a pressoflessione : 0.492
fs : 2.03

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**
Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.066 (fs=15.146)
Taglio Ty di Progetto [daN] : -168
Taglio Tz di Progetto [daN] : -3
Momento Torcente Mt di Progetto [daNm] : 113

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.18
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.066
fs : 15.15

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 47.52	Snellezza nel piano XZ	: 67.89
Snellezza relativa nel piano XY	: 0.76	Snellezza relativa nel piano XZ	: 1.08
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.81	Coefficiente K nel piano XZ	: 1.12
Coefficiente Kc nel piano XY	: 0.91	Coefficiente Kc nel piano XZ	: 0.70
Coefficiente di sfruttamento nel piano XY	: 0.518	Coefficiente di sfruttamento nel piano XZ	: 0.538
fs	: 1.858		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2351.8	Lunghezza efficace nel piano XZ	: 2351.8
Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mm²	Tensione Critica nel piano XZ	: 289.24 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 9.07 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.453	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.086		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.538	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.086
fs	: 1.858		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 2351.8 mm
Comb. di carico più gravosa : 142
Carico distribuito Istantaneo : -6.0 daN/m
-
Freccia Istantanea - COMBINAZIONE
Freccia Finale - COMBINAZIONE
Modulo Elastico istantaneo : 11500.0 N/mm²
Controfreccia : 0.000 mm
Freccia Istantanea : -0.232 mm
Freccia Netta Finale : -0.418 mm
Freccia Finale : -0.418 mm
Fatt. sicurezza freccia Istantanea : 20.243

Schema adottato Doppia Cerniera
Peso proprio : -5.5 daN/m
-
Carico distribuito Finale : -6.0 daN/m
Comb 42 [CAR] [ST]
Comb 2 [SLEQP] [PE]
Modulo Elastico finale : 6388.9 N/mm²
Limite Freccia Istantanea L/500 : 4.704 mm
Limite Freccia Netta Fin. L/ 350 : 6.719 mm
Limite Freccia Finale L/ 300 : 7.839 mm
Fatt. sicurezza freccia Netta Finale : 16.066

Fatt. sicurezza freccia Finale : 18.744

Fatt. sicurezza : 16.066

Campata 75-58 Copert[Asta GEN.]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $-\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.227 (fs=4.404)

Sforzo Normale di Progetto [daN] : 1387 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : 0

Momento Flettente Mz di Progetto [daNm] : -96

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.96

Tensione Resistente [N/mm²] : 16.02

Coefficiente di Sfruttamento a trazione : 0.06

fs : 16.63

Tensione di Progetto relativa a My [N/mm²] : 0

Tensione di Progetto relativa a Mz [N/mm²] : 3.34

Tensione Resistente relativa a My [N/mm²] : 20.03

Tensione Resistente relativa a Mz [N/mm²] : 20.03

Coefficiente di Sfruttamento a flessione : 0.167

fs : 5.99

Coefficiente di Sfruttamento : 0.227

fs : 4.4

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.012 (fs=82.281)

Taglio Ty di Progetto [daN] : -31

Taglio Tz di Progetto [daN] : -3

Momento Torcente Mt di Progetto [daNm] : -35

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03

Tensione di Progetto relativa a Tz [N/mm²] : 0.00

Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a taglio : 0.012

fs : 82.28

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY : 0.70 Coefficiente Beta nel piano XZ : 1.00

Snellezza nel piano XY : 47.52 Snellezza nel piano XZ : 67.89

Snellezza relativa nel piano XY : 0.76 Snellezza relativa nel piano XZ : 1.08

Coefficiente Beta c : 0.10 Combinazione più sfavorevole : 29

Coefficiente K nel piano XY : 0.81 Coefficiente K nel piano XZ : 1.12

Coefficiente Kc nel piano XY : 0.91 Coefficiente Kc nel piano XZ : 0.70

Coefficiente di sfruttamento nel piano XY : 0.232 Coefficiente di sfruttamento nel piano XZ : 0.255

fs : 3.925

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 29

Lunghezza efficace nel piano XY : 2351.8

Sezione più sfavorevole : 1

Lunghezza efficace nel piano XZ : 2351.8

Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mm ²	Tensione Critica nel piano XZ	: 289.24 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 3.10 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.155	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.100		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.255	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.100
fs	: 3.925		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto			
Lunghezza elemento	: 2351.8 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.232 mm	Limite Freccia Istantanea L/500	: 4.704 mm
Freccia Netta Finale	: -0.418 mm	Limite Freccia Netta Fin. L/ 350	: 6.719 mm
Freccia Finale	: -0.418 mm	Limite Freccia Finale L/ 300	: 7.839 mm
Fatt. sicurezza freccia Istantanea	: 20.243	Fatt. sicurezza freccia Netta Finale	: 16.066
Fatt. sicurezza freccia Finale	: 18.744	Fatt. sicurezza	: 16.066

Campata 77-61 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.115 (fs=8.723)

Sforzo Normale di Progetto [daN]	: 1778 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -22

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1.23
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.077
fs	: 12.97
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.75
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.038
fs	: 26.62
Coefficiente di Sfruttamento	: 0.115
fs	: 8.72

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa : 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 22 [SLD] [IN] " - Coeff. Sfruttamento : 0.01 (fs=102.427)

Taglio Ty di Progetto [daN] : 25
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : 23

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.01
 fs : 102.43

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 66.56
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 1.06
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 14
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 1.10
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.72
Coefficiente di sfruttamento nel piano XY	: 0.118	Coefficiente di sfruttamento nel piano XZ	: 0.141
fs	: 7.113		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 14	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm
Tensione Critica nel piano XY	: 295.02 N/mm ²	Tensione Critica nel piano XZ	: 295.02 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.74 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.037	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.104		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.141	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.104
fs	: 7.113		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2305.7 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.215 mm	Limite Freccia Istantanea L/500	: 4.611 mm
Freccia Netta Finale	: -0.386 mm	Limite Freccia Netta Fin. L/ 350	: 6.588 mm
Freccia Finale	: -0.386 mm	Limite Freccia Finale L/ 300	: 7.686 mm
Fatt. sicurezza freccia Istantanea	: 21.482	Fatt. sicurezza freccia Netta Finale	: 17.050
Fatt. sicurezza freccia Finale	: 19.891	Fatt. sicurezza	: 17.050

Campata 62-77 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2305.67 mm] - **R 120x120**
Comb. più gravosa : " Comb 30 [SLD] [IN] " - Coeff. Sfruttamento : 0.144 (fs=6.942)
 Sforzo Normale di Progetto [daN] : 1150 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : 54

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.8
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.05
 fs : 20.06
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 1.89
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.094
 fs : 10.62
 Coefficiente di Sfruttamento : 0.144
 fs : 6.94

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**
Comb. più gravosa : " Comb 22 [SLD] [IN] " - Coeff. Sfruttamento : 0.016 (fs=61.971)
 Taglio Ty di Progetto [daN] : -41
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : 47

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.04
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.016
 fs : 61.97

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 66.56
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 1.06
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 45
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 1.10
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.72
Coefficiente di sfruttamento nel piano XY	: 0.160	Coefficiente di sfruttamento nel piano XZ	: 0.177
fs	: 5.660		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 45	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm
Tensione Critica nel piano XY	: 295.02 N/mmq	Tensione Critica nel piano XZ	: 295.02 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 1.97 N/mmq	Tensione fless. piano XZ	: 0.00 N/mmq
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.099	Coefficiente sfrutt. nel piano XZ	: 0.000

Coeff. sfrutt. max euleriano	: 0.078	
Coeff. sfrutt. TOTALE (Piano XY)	: 0.177	Coeff. sfrutt. TOTALE (Piano XZ) : 0.078
fs	: 5.660	

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2305.7 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.215 mm	Limite Freccia Istantanea L/500	: 4.611 mm
Freccia Netta Finale	: -0.386 mm	Limite Freccia Netta Fin. L/ 350	: 6.588 mm
Freccia Finale	: -0.386 mm	Limite Freccia Finale L/ 300	: 7.686 mm
Fatt. sicurezza freccia Istantanea	: 21.482	Fatt. sicurezza freccia Netta Finale	: 17.050
Fatt. sicurezza freccia Finale	: 19.891	Fatt. sicurezza	: 17.050

Campata 65-78 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.133 (fs=7.526)

Sforzo Normale di Progetto [daN]	: 1546 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 38

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1.07
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.067
fs	: 14.93
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.32
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.066
fs	: 15.18
Coefficiente di Sfruttamento	: 0.133
fs	: 7.53

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.015 (fs=65.154)

Taglio Ty di Progetto [daN]	: 39
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -48

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00

Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.015
fs	: 65.15

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 66.56
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 1.06
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 18
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 1.10
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.72
Coefficiente di sfruttamento nel piano XY	: 0.141	Coefficiente di sfruttamento nel piano XZ	: 0.161
fs	: 6.193		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 18	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm
Tensione Critica nel piano XY	: 295.02 N/mm ²	Tensione Critica nel piano XZ	: 295.02 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.31 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.065	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.096		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.161	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.096
fs	: 6.193		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2305.7 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.215 mm	Limite Freccia Istantanea L/500	: 4.611 mm
Freccia Netta Finale	: -0.386 mm	Limite Freccia Netta Fin. L/ 350	: 6.588 mm
Freccia Finale	: -0.386 mm	Limite Freccia Finale L/ 300	: 7.686 mm
Fatt. sicurezza freccia Istantanea	: 21.482	Fatt. sicurezza freccia Netta Finale	: 17.050
Fatt. sicurezza freccia Finale	: 19.891	Fatt. sicurezza	: 17.050

Campata 78-66 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.118 (fs=8.503)

Sforzo Normale di Progetto [daN]	: 1816 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0

Momento Flettente Mz di Progetto [daNm] : -22

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1.26
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.079
fs	: 12.71
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.78
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.039
fs	: 25.7
Coefficiente di Sfruttamento	: 0.118
fs	: 8.5

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.009 (fs=112.928)

Taglio Ty di Progetto [daN]	: -22
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: 35

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.009
fs	: 112.93

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 66.56
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 1.06
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 1.10
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.72
Coefficiente di sfruttamento nel piano XY	: 0.120	Coefficiente di sfruttamento nel piano XZ	: 0.143
fs	: 6.997		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm
Tensione Critica nel piano XY	: 295.02 N/mm ²	Tensione Critica nel piano XZ	: 295.02 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.78 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.039	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.104		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.143	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.104
fs	: 6.997		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto			
Lunghezza elemento	: 2305.7 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.215 mm	Limite Freccia Istantanea L/500	: 4.611 mm
Freccia Netta Finale	: -0.386 mm	Limite Freccia Netta Fin. L/ 350	: 6.588 mm
Freccia Finale	: -0.386 mm	Limite Freccia Finale L/ 300	: 7.686 mm
Fatt. sicurezza freccia Istantanea	: 21.482	Fatt. sicurezza freccia Netta Finale	: 17.050
Fatt. sicurezza freccia Finale	: 19.891	Fatt. sicurezza	: 17.050

Campata 69-76 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.101 (fs=9.915)

Sforzo Normale di Progetto [daN]	: 1172 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -29

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.81
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.051
fs	: 19.69
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.05
fs	: 19.97
Coefficiente di Sfruttamento	: 0.101
fs	: 9.92

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.006 (fs=154.293)

Taglio Ty di Progetto [daN]	: -16
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: -20

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.006
fs	: 154.29

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
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Snellezza nel piano XY	: 47.52	Snellezza nel piano XZ	: 67.89
Snellezza relativa nel piano XY	: 0.76	Snellezza relativa nel piano XZ	: 1.08
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 14
Coefficiente K nel piano XY	: 0.81	Coefficiente K nel piano XZ	: 1.12
Coefficiente Kc nel piano XY	: 0.91	Coefficiente Kc nel piano XZ	: 0.70
Coefficiente di sfruttamento nel piano XY	: 0.112	Coefficiente di sfruttamento nel piano XZ	: 0.136
fs	: 7.333		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 14	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2351.8	Lunghezza efficace nel piano XZ	: 2351.8
Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mm ²	Tensione Critica nel piano XZ	: 289.24 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.64 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.032	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.105		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.136	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.105
fs	: 7.333		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2351.8 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.232 mm	Limite Freccia Istantanea L/500	: 4.704 mm
Freccia Netta Finale	: -0.418 mm	Limite Freccia Netta Fin. L/ 350	: 6.719 mm
Freccia Finale	: -0.418 mm	Limite Freccia Finale L/ 300	: 7.839 mm
Fatt. sicurezza freccia Istantanea	: 20.243	Fatt. sicurezza freccia Netta Finale	: 16.066
Fatt. sicurezza freccia Finale	: 18.744	Fatt. sicurezza	: 16.066

Campata 76-70 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.172 (fs=5.812)

Sforzo Normale di Progetto [daN]	: 1298 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -67

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.9
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.056
fs	: 17.77

Tensione di Progetto relativa a M_y [N/mm ²]	: 0
Tensione di Progetto relativa a M_z [N/mm ²]	: 2.32
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.116
f_s	: 8.64
Coefficiente di Sfruttamento	: 0.172
f_s	: 5.81

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.015 ($f_s=68.087$)

Taglio T_y di Progetto [daN]	: 37
Taglio T_z di Progetto [daN]	: -3
Momento Torcente M_t di Progetto [daNm]	: 14

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.04
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.015
f_s	: 68.09

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 47.52	Snellezza nel piano XZ	: 67.89
Snellezza relativa nel piano XY	: 0.76	Snellezza relativa nel piano XZ	: 1.08
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.81	Coefficiente K nel piano XZ	: 1.12
Coefficiente K_c nel piano XY	: 0.91	Coefficiente K_c nel piano XZ	: 0.70
Coefficiente di sfruttamento nel piano XY	: 0.136	Coefficiente di sfruttamento nel piano XZ	: 0.159
f_s	: 6.273		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2351.8	Lunghezza efficace nel piano XZ	: 2351.8
Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mm ²	Tensione Critica nel piano XZ	: 289.24 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.21 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.061	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.099		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.159	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.099
f_s	: 6.273		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale ($t > \inf$)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2351.8 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	

Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.232 mm	Limite Freccia Istantanea L/500	: 4.704 mm
Freccia Netta Finale	: -0.418 mm	Limite Freccia Netta Fin. L/350	: 6.719 mm
Freccia Finale	: -0.418 mm	Limite Freccia Finale L/300	: 7.839 mm
Fatt. sicurezza freccia Istantanea	: 20.243	Fatt. sicurezza freccia Netta Finale	: 16.066
Fatt. sicurezza freccia Finale	: 18.744	Fatt. sicurezza	: 16.066

Campata 1-74 Copertu[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.564 (fs=1.772)

Sforzo Normale di Progetto [daN]	: 605 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -310

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.42
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.026
fs	: 38.16
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 10.78
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.538
fs	: 1.86
Coefficiente di Sfruttamento	: 0.564
fs	: 1.77

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.06 (fs=16.69)

Taglio Ty di Progetto [daN]	: 147
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: -86

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.15
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.058
fs	: 17.37
Tensione di Progetto [N/mm ²]	: 0.17
Modulo di resistenza a torsione [mm ³]	: 360000
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.057
fs	: 17.67
Coefficiente di Sfruttamento a taglio+torsione	: 0.06
fs	: 16.69

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY : 0.70

Coefficiente Beta nel piano XZ : 1.00

Snellezza nel piano XY	: 47.52	Snellezza nel piano XZ	: 67.89
Snellezza relativa nel piano XY	: 0.76	Snellezza relativa nel piano XZ	: 1.08
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 40
Coefficiente K nel piano XY	: 0.81	Coefficiente K nel piano XZ	: 1.12
Coefficiente Kc nel piano XY	: 0.91	Coefficiente Kc nel piano XZ	: 0.70
Coefficiente di sfruttamento nel piano XY	: 0.571	Coefficiente di sfruttamento nel piano XZ	: 0.593
fs	: 1.687		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2351.8	Lunghezza efficace nel piano XZ	: 2351.8
Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mm ²	Tensione Critica nel piano XZ	: 289.24 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 10.05 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.502	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.091		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.593	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.091
fs	: 1.687		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2351.8 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.232 mm	Limite Freccia Istantanea L/500	: 4.704 mm
Freccia Netta Finale	: -0.418 mm	Limite Freccia Netta Fin. L/ 350	: 6.719 mm
Freccia Finale	: -0.418 mm	Limite Freccia Finale L/ 300	: 7.839 mm
Fatt. sicurezza freccia Istantanea	: 20.243	Fatt. sicurezza freccia Netta Finale	: 16.066
Fatt. sicurezza freccia Finale	: 18.744	Fatt. sicurezza	: 16.066

Campata 74-2 Copertu[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.253 (fs=3.952)

Sforzo Normale di Progetto [daN]	: 1247 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 115

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.87
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.054
fs	: 18.5

Tensione di Progetto relativa a M_y [N/mm ²]	: 0
Tensione di Progetto relativa a M_z [N/mm ²]	: 3.98
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.199
f_s	: 5.03
Coefficiente di Sfruttamento	: 0.253
f_s	: 3.95

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.025 ($f_s=39.781$)

Taglio T_y di Progetto [daN]	: 64
Taglio T_z di Progetto [daN]	: -3
Momento Torcente M_t di Progetto [daNm]	: -51

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.07
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.025
f_s	: 39.78

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 47.52	Snellezza nel piano XZ	: 54.31
Snellezza relativa nel piano XY	: 0.76	Snellezza relativa nel piano XZ	: 0.86
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 29
Coefficiente K nel piano XY	: 0.81	Coefficiente K nel piano XZ	: 0.90
Coefficiente K_c nel piano XY	: 0.91	Coefficiente K_c nel piano XZ	: 0.86
Coefficiente di sfruttamento nel piano XY	: 0.236	Coefficiente di sfruttamento nel piano XZ	: 0.239
f_s	: 4.190		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 29	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2351.8	Lunghezza efficace nel piano XZ	: 2351.8
Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mm ²	Tensione Critica nel piano XZ	: 289.24 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 3.83 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.191	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.047		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.239	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.047
f_s	: 4.190		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2351.8 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -6.0 daN/m

Freccia Istantanea - COMBINAZIONE
Freccia Finale - COMBINAZIONE

Schema adottato Incastro-Cerniera	
Peso proprio	: -5.5 daN/m
-	
Carico distribuito Finale	: -6.0 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [PE]	

Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.096 mm	Limite Freccia Istantanea L/500	: 4.704 mm
Freccia Netta Finale	: -0.174 mm	Limite Freccia Netta Fin. L/350	: 6.719 mm
Freccia Finale	: -0.174 mm	Limite Freccia Finale L/300	: 7.839 mm
Fatt. sicurezza freccia Istantanea	: 48.763	Fatt. sicurezza freccia Netta Finale	: 38.701
Fatt. sicurezza freccia Finale	: 45.151	Fatt. sicurezza	: 38.701

Campata 6-71 Copertu[Asta GEN.]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)
L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.13 (fs=7.678)

Sforzo Normale di Progetto [daN]	: 1357 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 41

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.94
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.059
fs	: 17
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.43
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.071
fs	: 14
Coefficiente di Sfruttamento	: 0.13
fs	: 7.68

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.013 (fs=74.847)

Taglio Ty di Progetto [daN]	: 34
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -30

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.013
fs	: 74.85

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 66.56
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 1.06
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 10
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 1.10
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.72
Coefficiente di sfruttamento nel piano XY	: 0.135	Coefficiente di sfruttamento nel piano XZ	: 0.153
fs	: 6.526		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 10	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm
Tensione Critica nel piano XY	: 295.02 N/mm ²	Tensione Critica nel piano XZ	: 295.02 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.43 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.071	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.082		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.153	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.082
fs	: 6.526		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2305.7 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.215 mm	Limite Freccia Istantanea L/500	: 4.611 mm
Freccia Netta Finale	: -0.386 mm	Limite Freccia Netta Fin. L/ 350	: 6.588 mm
Freccia Finale	: -0.386 mm	Limite Freccia Finale L/ 300	: 7.686 mm
Fatt. sicurezza freccia Istantanea	: 21.482	Fatt. sicurezza freccia Netta Finale	: 17.050
Fatt. sicurezza freccia Finale	: 19.891	Fatt. sicurezza	: 17.050

Campata 71-7 Copertu[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.136 (fs=7.351)

Sforzo Normale di Progetto [daN]	: 1382 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 44

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.96
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.06
fs	: 16.7
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.53
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.076
fs	: 13.13
Coefficiente di Sfruttamento	: 0.136

fs

: 7.35

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.014 (fs=69.511)

Taglio Ty di Progetto [daN] : -37
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : 47

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.04
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.014
 fs : 69.51

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 53.25
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 0.85
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 17
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 0.89
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.87
Coefficiente di sfruttamento nel piano XY	: 0.140	Coefficiente di sfruttamento nel piano XZ	: 0.143
fs	: 6.996		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm
Tensione Critica nel piano XY	: 295.02 N/mm²	Tensione Critica nel piano XZ	: 295.02 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 1.53 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.076	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.067		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.143	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.067
fs	: 6.996		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 2305.7 mm
 Comb. di carico più gravosa : 142
 Carico distribuito Istantaneo : -6.0 daN/m
 -
 Freccia Istantanea - COMBINAZIONE
 Freccia Finale - COMBINAZIONE
 Modulo Elastico istantaneo : 11500.0 N/mm²
 Controfreccia : 0.000 mm
 Freccia Istantanea : -0.089 mm
 Freccia Netta Finale : -0.160 mm
 Freccia Finale : -0.160 mm
 Fatt. sicurezza freccia Istantanea : 51.748
 Fatt. sicurezza freccia Finale : 47.915

Schema adottato Incastro-Cerniera
 Peso proprio : -5.5 daN/m
 -
 Carico distribuito Finale : -6.0 daN/m
 Comb 42 [CAR] [ST]
 Comb 2 [SLEQP] [PE]
 Modulo Elastico finale : 6388.9 N/mm²
 Limite Freccia Istantanea L/500 : 4.611 mm
 Limite Freccia Netta Fin. L/ 350 : 6.588 mm
 Limite Freccia Finale L/ 300 : 7.686 mm
 Fatt. sicurezza freccia Netta Finale : 41.070
 Fatt. sicurezza : 41.070

Campata 9-72 Copertu[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.122 (fs=8.173)

Sforzo Normale di Progetto [daN]	: 1719 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -28

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 1.19
Tensione Resistente [N/mm²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.075
fs	: 13.42
Tensione di Progetto relativa a My [N/mm²]	: 0
Tensione di Progetto relativa a Mz [N/mm²]	: 0.96
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.048
fs	: 20.9
Coefficiente di Sfruttamento	: 0.122
fs	: 8.17

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.008 (fs=130.846)

Taglio Ty di Progetto [daN]	: 19
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -26

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.008
fs	: 130.85

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 66.56
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 1.06
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 38
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 1.10
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.72
Coefficiente di sfruttamento nel piano XY	: 0.131	Coefficiente di sfruttamento nel piano XZ	: 0.150
fs	: 6.657		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 38	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm

Tensione Critica nel piano XY	: 295.02 N/mm ²	Tensione Critica nel piano XZ	: 295.02 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.20 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.060	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.090		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.150	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.090
fs	: 6.657		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2305.7 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.215 mm	Limite Freccia Istantanea L/500	: 4.611 mm
Freccia Netta Finale	: -0.386 mm	Limite Freccia Netta Fin. L/ 350	: 6.588 mm
Freccia Finale	: -0.386 mm	Limite Freccia Finale L/ 300	: 7.686 mm
Fatt. sicurezza freccia Istantanea	: 21.482	Fatt. sicurezza freccia Netta Finale	: 17.050
Fatt. sicurezza freccia Finale	: 19.891	Fatt. sicurezza	: 17.050

Campata 72-10 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.127 (fs=7.883)

Sforzo Normale di Progetto [daN]	: 1498 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -36

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1.04
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.065
fs	: 15.4
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.24
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.062
fs	: 16.15
Coefficiente di Sfruttamento	: 0.127
fs	: 7.88

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.01 (fs=103.013)

Taglio Ty di Progetto [daN]	: -25
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TABULATI DI CALCOLO -

Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : 29

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.01
 fs : 103.01

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 53.25
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 0.85
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 0.89
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.87
Coefficiente di sfruttamento nel piano XY	: 0.130	Coefficiente di sfruttamento nel piano XZ	: 0.134
fs	: 7.451		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 21	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm
Tensione Critica nel piano XY	: 295.02 N/mm ²	Tensione Critica nel piano XZ	: 295.02 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.99 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.049	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.085		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.134	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.085
fs	: 7.451		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2305.7 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.089 mm	Limite Freccia Istantanea L/500	: 4.611 mm
Freccia Netta Finale	: -0.160 mm	Limite Freccia Netta Fin. L/ 350	: 6.588 mm
Freccia Finale	: -0.160 mm	Limite Freccia Finale L/ 300	: 7.686 mm
Fatt. sicurezza freccia Istantanea	: 51.748	Fatt. sicurezza freccia Netta Finale	: 41.070
Fatt. sicurezza freccia Finale	: 47.915	Fatt. sicurezza	: 41.070

Campata 73-13 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.133 (fs=7.511)

Sforzo Normale di Progetto [daN] : 1029 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 0
Momento Flettente Mz di Progetto [daNm] : 51

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.71
Tensione Resistente [N/mm²] : 16.02
Coefficiente di Sfruttamento a trazione : 0.045
fs : 22.41
Tensione di Progetto relativa a My [N/mm²] : 0
Tensione di Progetto relativa a Mz [N/mm²] : 1.77
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.089
fs : 11.3
Coefficiente di Sfruttamento : 0.133
fs : 7.51

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.015 (fs=65.516)

Taglio Ty di Progetto [daN] : -39
Taglio Tz di Progetto [daN] : -3
Momento Torcente Mt di Progetto [daNm] : 51

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.04
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.015
fs : 65.52

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 47.52	Snellezza nel piano XZ	: 54.31
Snellezza relativa nel piano XY	: 0.76	Snellezza relativa nel piano XZ	: 0.86
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 10
Coefficiente K nel piano XY	: 0.81	Coefficiente K nel piano XZ	: 0.90
Coefficiente Kc nel piano XY	: 0.91	Coefficiente Kc nel piano XZ	: 0.86
Coefficiente di sfruttamento nel piano XY	: 0.123	Coefficiente di sfruttamento nel piano XZ	: 0.126
fs	: 7.922		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 10	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2351.8	Lunghezza efficace nel piano XZ	: 2351.8
Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mmq	Tensione Critica nel piano XZ	: 289.24 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 1.34 N/mmq	Tensione fless. piano XZ	: 0.00 N/mmq
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.067	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.059		

Coeff. sfrutt. TOTALE (Piano XY) : 0.126
fs : 7.922

Coeff. sfrutt. TOTALE (Piano XZ) : 0.059

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 2351.8 mm
Comb. di carico più gravosa : 142
Carico distribuito Istantaneo : -6.0 daN/m

Schema adottato Incastro-Cerniera

Peso proprio : -5.5 daN/m

-

Carico distribuito Finale : -6.0 daN/m

Freccia Istantanea - COMBINAZIONE

Comb 42 [CAR] [ST]

Freccia Finale - COMBINAZIONE

Comb 2 [SLEQP] [PE]

Modulo Elastico istantaneo : 11500.0 N/mm²

Modulo Elastico finale : 6388.9 N/mm²

Controfreccia : 0.000 mm

Freccia Istantanea : -0.096 mm

Limite Freccia Istantanea L/500 : 4.704 mm

Freccia Netta Finale : -0.174 mm

Limite Freccia Netta Fin. L/ 350 : 6.719 mm

Freccia Finale : -0.174 mm

Limite Freccia Finale L/ 300 : 7.839 mm

Fatt. sicurezza freccia Istantanea : 48.763

Fatt. sicurezza freccia Netta Finale : 38.701

Fatt. sicurezza freccia Finale : 45.151

Fatt. sicurezza : 38.701

Campata 14-73 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.145 (fs=6.877)

Sforzo Normale di Progetto [daN] : 1170 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : 0

Momento Flettente Mz di Progetto [daNm] : -55

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.81

Tensione Resistente [N/mm²] : 16.02

Coefficiente di Sfruttamento a trazione : 0.051

fs : 19.72

Tensione di Progetto relativa a My [N/mm²] : 0

Tensione di Progetto relativa a Mz [N/mm²] : 1.9

Tensione Resistente relativa a My [N/mm²] : 20.03

Tensione Resistente relativa a Mz [N/mm²] : 20.03

Coefficiente di Sfruttamento a flessione : 0.095

fs : 10.56

Coefficiente di Sfruttamento : 0.145

fs : 6.88

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.016 (fs=61.71)

Taglio Ty di Progetto [daN] : 41

Taglio Tz di Progetto [daN] : -3

Momento Torcente Mt di Progetto [daNm] : -33

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.04

Tensione di Progetto relativa a Tz [N/mm²] : 0.00

Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a taglio : 0.016
fs : 61.71

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 47.52	Snellezza nel piano XZ	: 67.89
Snellezza relativa nel piano XY	: 0.76	Snellezza relativa nel piano XZ	: 1.08
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 21
Coefficiente K nel piano XY	: 0.81	Coefficiente K nel piano XZ	: 1.12
Coefficiente Kc nel piano XY	: 0.91	Coefficiente Kc nel piano XZ	: 0.70
Coefficiente di sfruttamento nel piano XY	: 0.174	Coefficiente di sfruttamento nel piano XZ	: 0.197
fs	: 5.083		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 21	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2351.8	Lunghezza efficace nel piano XZ	: 2351.8
Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mm ²	Tensione Critica nel piano XZ	: 289.24 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.97 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.099	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.098		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.197	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.098
fs	: 5.083		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2351.8 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.232 mm	Limite Freccia Istantanea L/500	: 4.704 mm
Freccia Netta Finale	: -0.418 mm	Limite Freccia Netta Fin. L/ 350	: 6.719 mm
Freccia Finale	: -0.418 mm	Limite Freccia Finale L/ 300	: 7.839 mm
Fatt. sicurezza freccia Istantanea	: 20.243	Fatt. sicurezza freccia Netta Finale	: 16.066
Fatt. sicurezza freccia Finale	: 18.744	Fatt. sicurezza	: 16.066

Campata 15-125 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.246 (fs=4.072)

Sforzo Normale di Progetto [daN]	: 3383 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -632
Momento Flettente Mz di Progetto [daNm]	: -1897

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.21
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.015
fs	: 68.89
Tensione di Progetto relativa a My [N/mm ²]	: 0.24
Tensione di Progetto relativa a Mz [N/mm ²]	: 4.45
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.231
fs	: 4.33
Coefficiente di Sfruttamento	: 0.246
fs	: 4.07

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.044 (fs=22.596)

Taglio Ty di Progetto [daN]	: -1531
Taglio Tz di Progetto [daN]	: -2743
Momento Torcente Mt di Progetto [daNm]	: 656

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.14
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.26
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.111
fs	: 9.01
Tensione di Progetto [N/mm ²]	: 0.16
Modulo di resistenza a torsione [mm ³]	: 7785888
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.032
fs	: 31.3
Coefficiente di Sfruttamento a taglio+torsione	: 0.044
fs	: 22.6

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 4.45 N/mm ²	Tensione fless. piano XZ	: 0.24 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.222	Coefficiente sfrutt. nel piano XZ	: 0.013
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.222	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.013
fs	: 4.505		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -342.1 daN/m	-	
-		Carico distribuito Finale	: -238.1 daN/m

Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 127-16 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.14 (fs=7.122)

Sforzo Normale di Progetto [daN]	: 6128 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -97
Momento Flettente Mz di Progetto [daNm]	: -963

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.38
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.026
fs	: 38.03
Tensione di Progetto relativa a My [N/mm ²]	: 0.04
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.26
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.114
fs	: 8.76
Coefficiente di Sfruttamento	: 0.14
fs	: 7.12

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 39 [SLV] [IN] " - Coeff. Sfruttamento : 0.098 (fs=10.185)

Taglio Ty di Progetto [daN]	: 493
Taglio Tz di Progetto [daN]	: 2737
Momento Torcente Mt di Progetto [daNm]	: -103

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.05
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.26
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.098
fs	: 10.18

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²

Tensione fless. piano XY	: 2.26 N/mm ²	Tensione fless. piano XZ	: 0.04 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.113	Coefficiente sfrutt. nel piano XZ	: 0.002
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.113	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.002
fs	: 8.871		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -342.1 daN/m	-	
-		Carico distribuito Finale	: -238.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 17-129 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.235 (fs=4.259)

Sforzo Normale di Progetto [daN]	: 1144 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 151
Momento Flettente Mz di Progetto [daNm]	: -1946

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.07
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.005
fs	: 203.78
Tensione di Progetto relativa a My [N/mm ²]	: 0.06
Tensione di Progetto relativa a Mz [N/mm ²]	: 4.56
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.23
fs	: 4.35
Coefficiente di Sfruttamento	: 0.235
fs	: 4.26

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.042 (fs=23.615)

Taglio Ty di Progetto [daN]	: -1586
Taglio Tz di Progetto [daN]	: -2197
Momento Torcente Mt di Progetto [daNm]	: 703

Tipo Verifica		: TAGLIO+TORSIONE
Tensione di Progetto relativa a T_y [N/mm ²]		: 0.15
Tensione di Progetto relativa a T_z [N/mm ²]		: 0.21
Tensione tang. Resistente [N/mm ²]		: 2.66
Coefficiente di Sfruttamento a taglio		: 0.096
f_s		: 10.45
Tensione di Progetto [N/mm ²]		: 0.17
Modulo di resistenza a torsione [mm ³]		: 7785888
Tensione tang. Resistente [N/mm ²]		: 2.66
Coefficiente di Sfruttamento a torsione		: 0.033
f_s		: 30.13
Coefficiente di Sfruttamento a taglio+torsione		: 0.042
f_s		: 23.62

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 4.56 N/mm ²	Tensione fless. piano XZ	: 0.06 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.228	Coefficiente sfrutt. nel piano XZ	: 0.003
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.228	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.003
f_s	: 4.391		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 130-18 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.154 ($f_s=6.512$)

Sforzo Normale di Progetto [daN]	: 2720 (TRAZIONE)
Momento Flettente M_y di Progetto [daNm]	: 393

Momento Flettente Mz di Progetto [daNm] : 1164

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.17
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.012
fs	: 85.66
Tensione di Progetto relativa a My [N/mm ²]	: 0.15
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.73
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.142
fs	: 7.05
Coefficiente di Sfruttamento	: 0.154
fs	: 6.51

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.085 (fs=11.819)

Taglio Ty di Progetto [daN]	: 673
Taglio Tz di Progetto [daN]	: 2300
Momento Torcente Mt di Progetto [daNm]	: 611

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.06
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.22
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.085
fs	: 11.82

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.77 N/mm ²	Tensione fless. piano XZ	: 0.03 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.138	Coefficiente sfrutt. nel piano XZ	: 0.002
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.138	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.002
fs	: 7.221		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/350	: 4.286 mm

Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 19-135 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.226 (fs=4.423)

Sforzo Normale di Progetto [daN]	: 4562 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 53
Momento Flettente Mz di Progetto [daNm]	: 1758

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.29
Tensione Resistente [N/mm²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.02
fs	: 51.09
Tensione di Progetto relativa a My [N/mm²]	: 0.02
Tensione di Progetto relativa a Mz [N/mm²]	: 4.12
Tensione Resistente relativa a My [N/mm²]	: 18.21
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.206
fs	: 4.84
Coefficiente di Sfruttamento	: 0.226
fs	: 4.42

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 51 [SLV] [IN] " - Coeff. Sfruttamento : 0.043 (fs=23.253)

Taglio Ty di Progetto [daN]	: 1368
Taglio Tz di Progetto [daN]	: -2957
Momento Torcente Mt di Progetto [daNm]	: -371

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²]	: 0.13
Tensione di Progetto relativa a Tz [N/mm²]	: 0.28
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.115
fs	: 8.69
Tensione di Progetto [N/mm²]	: 0.15
Modulo di resistenza a torsione [mm³]	: 7785888
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.03
fs	: 33.59
Coefficiente di Sfruttamento a taglio+torsione	: 0.043
fs	: 23.25

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm²	Tensione Critica nel piano XZ	: 116.89 N/mm²

Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 4.35 N/mm ²	Tensione fless. piano XZ	: 0.10 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.217	Coefficiente sfrutt. nel piano XZ	: 0.005
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.217	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.005
fs	: 4.604		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 134-20 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.163 (fs=6.154)

Sforzo Normale di Progetto [daN]	: 4362 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -5206
Momento Flettente Mz di Progetto [daNm]	: 446

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.27
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.019
fs	: 53.43
Tensione di Progetto relativa a My [N/mm ²]	: 1.95
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.05
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.144
fs	: 6.95
Coefficiente di Sfruttamento	: 0.163
fs	: 6.15

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 47 [SLV] [IN] " - Coeff. Sfruttamento : 0.051 (fs=19.734)

Taglio Ty di Progetto [daN]	: -574
Taglio Tz di Progetto [daN]	: 1315

Momento Torcente Mt di Progetto [daNm] : -559

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.05
 Tensione di Progetto relativa a Tz [N/mm²] : 0.12
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.051
 fs : 19.73

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.70 N/mm ²	Tensione fless. piano XZ	: 0.13 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.135	Coefficiente sfrutt. nel piano XZ	: 0.007
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.135	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.007
fs	: 7.426		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 21-136 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.2 (fs=5)

Sforzo Normale di Progetto [daN] : 2237 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 171
 Momento Flettente Mz di Progetto [daNm] : -1606

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.14
 Tensione Resistente [N/mm²] : 14.57
 Coefficiente di Sfruttamento a trazione : 0.01

fs	: 104.18
Tensione di Progetto relativa a My [N/mm ²]	: 0.06
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.76
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.19
fs	: 5.25
Coefficiente di Sfruttamento	: 0.2
fs	: 5

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.044 (fs=22.737)

Taglio Ty di Progetto [daN]	: -1362
Taglio Tz di Progetto [daN]	: -2541
Momento Torcente Mt di Progetto [daNm]	: 673

Tipo Verifica	: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.13
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.24
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.102
fs	: 9.82
Tensione di Progetto [N/mm ²]	: 0.17
Modulo di resistenza a torsione [mm ³]	: 7785888
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.034
fs	: 29.75
Coefficiente di Sfruttamento a taglio+torsione	: 0.044
fs	: 22.74

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 3.76 N/mm ²	Tensione fless. piano XZ	: 0.06 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.188	Coefficiente sfrutt. nel piano XZ	: 0.004
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.188	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.004
fs	: 5.321		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm

Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 138-22 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.193 (fs=5.194)

Sforzo Normale di Progetto [daN]	: 5547 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -5547
Momento Flettente Mz di Progetto [daNm]	: 665

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.35
Tensione Resistente [N/mm²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.024
fs	: 42.01
Tensione di Progetto relativa a My [N/mm²]	: 2.08
Tensione di Progetto relativa a Mz [N/mm²]	: 1.56
Tensione Resistente relativa a My [N/mm²]	: 18.21
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.169
fs	: 5.93
Coefficiente di Sfruttamento	: 0.193
fs	: 5.19

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.094 (fs=10.602)

Taglio Ty di Progetto [daN]	: -160
Taglio Tz di Progetto [daN]	: 2667
Momento Torcente Mt di Progetto [daNm]	: 579

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm²]	: 0.25
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.094
fs	: 10.6

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm²	Tensione Critica nel piano XZ	: 116.89 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 1.56 N/mm²	Tensione fless. piano XZ	: 1.97 N/mm²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.078	Coefficiente sfrutt. nel piano XZ	: 0.108
Coeff. sfrutt. max euleriano	: 0.007		

Coeff. sfrutt. TOTALE (Piano XY) : 0.085
fs : 8.656

Coeff. sfrutt. TOTALE (Piano XZ) : 0.116

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1500.0 mm
Comb. di carico più gravosa : 142
Carico distribuito Istantaneo : -322.3 daN/m

Schema adottato Doppio Incastro
Peso proprio : -61.6 daN/m

-
Freccia Istantanea - COMBINAZIONE
Freccia Finale - COMBINAZIONE
Modulo Elastico istantaneo : 11500.0 N/mm²

Carico distribuito Finale : -223.6 daN/m
Comb 42 [CAR] [ST]
Comb 2 [SLEQP] [PE]
Modulo Elastico finale : 6388.9 N/mm²

Controfreccia : 0.000 mm
Freccia Istantanea : 0.000 mm
Freccia Netta Finale : 0.000 mm
Freccia Finale : 0.000 mm
Fatt. sicurezza freccia Istantanea : 1000.000
Fatt. sicurezza freccia Finale : 1000.000

Limite Freccia Istantanea L/500 : 3.000 mm
Limite Freccia Netta Fin. L/ 350 : 4.286 mm
Limite Freccia Finale L/ 300 : 5.000 mm
Fatt. sicurezza freccia Netta Finale : 1000.000
Fatt. sicurezza : 1000.000

Campata 23-141 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.203 (fs=4.924)

Sforzo Normale di Progetto [daN] : 2741 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 185
Momento Flettente Mz di Progetto [daNm] : 1612

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.17
Tensione Resistente [N/mm²] : 14.57
Coefficiente di Sfruttamento a trazione : 0.012
fs : 85.02
Tensione di Progetto relativa a My [N/mm²] : 0.07
Tensione di Progetto relativa a Mz [N/mm²] : 3.78
Tensione Resistente relativa a My [N/mm²] : 18.21
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.191
fs : 5.23
Coefficiente di Sfruttamento : 0.203
fs : 4.92

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.039 (fs=25.639)

Taglio Ty di Progetto [daN] : 0
Taglio Tz di Progetto [daN] : -703
Momento Torcente Mt di Progetto [daNm] : -1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
Tensione di Progetto relativa a Tz [N/mm²] : 0.07
Tensione tang. Resistente [N/mm²] : 1.69

Coefficiente di Sfruttamento a taglio : 0.039
fs : 25.64

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 3.83 N/mm ²	Tensione fless. piano XZ	: 0.04 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.191	Coefficiente sfrutt. nel piano XZ	: 0.002
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.191	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.002
fs	: 5.228		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 142-24 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.19 (fs=5.252)

Sforzo Normale di Progetto [daN]	: 5071 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -5680
Momento Flettente Mz di Progetto [daNm]	: 631

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.32
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.022
fs	: 45.96
Tensione di Progetto relativa a My [N/mm ²]	: 2.13
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.48
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.169

fs	: 5.93
Coefficiente di Sfruttamento	: 0.19
fs	: 5.25

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.044 (fs=22.569)

Taglio Ty di Progetto [daN]	: -165
Taglio Tz di Progetto [daN]	: 1244
Momento Torcente Mt di Progetto [daNm]	: 561

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm²]	: 0.12
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.044
fs	: 22.57

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 21	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm²	Tensione Critica nel piano XZ	: 116.89 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 0.91 N/mm²	Tensione fless. piano XZ	: 2.16 N/mm²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.046	Coefficiente sfrutt. nel piano XZ	: 0.119
Coeff. sfrutt. max euleriano	: 0.007		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.053	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.126
fs	: 7.916		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 25-145 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.226 (fs=4.425)

Sforzo Normale di Progetto [daN] : 5179 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -7567
 Momento Flettente Mz di Progetto [daNm] : 585

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.32
 Tensione Resistente [N/mm²] : 14.57
 Coefficiente di Sfruttamento a trazione : 0.022
 fs : 45
 Tensione di Progetto relativa a My [N/mm²] : 2.84
 Tensione di Progetto relativa a Mz [N/mm²] : 1.37
 Tensione Resistente relativa a My [N/mm²] : 18.21
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.204
 fs : 4.91
 Coefficiente di Sfruttamento : 0.226
 fs : 4.42

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.056 (fs=17.865)

Taglio Ty di Progetto [daN] : -674
 Taglio Tz di Progetto [daN] : -5719
 Momento Torcente Mt di Progetto [daNm] : 585

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.06
 Tensione di Progetto relativa a Tz [N/mm²] : 0.54
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.203
 fs : 4.92
 Tensione di Progetto [N/mm²] : 0.08
 Modulo di resistenza a torsione [mm³] : 7785888
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.015
 fs : 68.34
 Coefficiente di Sfruttamento a taglio+torsione : 0.056
 fs : 17.86

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 4.11 N/mm ²	Tensione fless. piano XZ	: 0.05 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.205	Coefficiente sfrutt. nel piano XZ	: 0.003
Coeff. sfrutt. max euleriano	: 0.001		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.207	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.004
fs	: 4.839		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto			
Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 146-26 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.23 (fs=4.355)

Sforzo Normale di Progetto [daN]	: 7068 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -7349
Momento Flettente Mz di Progetto [daNm]	: 585

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.44
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.03
fs	: 32.97
Tensione di Progetto relativa a My [N/mm ²]	: 2.76
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.37
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.199
fs	: 5.02
Coefficiente di Sfruttamento	: 0.23
fs	: 4.35

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.131 (fs=7.657)

Taglio Ty di Progetto [daN]	: 628
Taglio Tz di Progetto [daN]	: 3645
Momento Torcente Mt di Progetto [daNm]	: 566

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.06
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.34
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.131
fs	: 7.66

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.37 N/mm ²	Tensione fless. piano XZ	: 2.64 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.069	Coefficiente sfrutt. nel piano XZ	: 0.145
Coeff. sfrutt. max euleriano	: 0.012		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.081	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.157
fs	: 6.356		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 150-27 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.215 (fs=4.657)

Sforzo Normale di Progetto [daN]	: 5275 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -7285
Momento Flettente Mz di Progetto [daNm]	: 513

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.33
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.023
fs	: 44.18
Tensione di Progetto relativa a My [N/mm ²]	: 2.73
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.2
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.192
fs	: 5.21
Coefficiente di Sfruttamento	: 0.215
fs	: 4.66

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.051 (fs=19.489)

Taglio Ty di Progetto [daN] : 112
 Taglio Tz di Progetto [daN] : 6076
 Momento Torcente Mt di Progetto [daNm] : 254

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.01
 Tensione di Progetto relativa a Tz [N/mm²] : 0.57
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.215
 fs : 4.66
 Tensione di Progetto [N/mm²] : 0.03
 Modulo di resistenza a torsione [mm³] : 7785888
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.005
 fs : 189.65
 Coefficiente di Sfruttamento a taglio+torsione : 0.051
 fs : 19.49

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 21	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm²	Tensione Critica nel piano XZ	: 116.89 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 0.60 N/mm²	Tensione fless. piano XZ	: 2.90 N/mm²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.030	Coefficiente sfrutt. nel piano XZ	: 0.159
Coeff. sfrutt. max euleriano	: 0.010		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.039	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.169
fs	: 5.915		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 28-149 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 41 [SLV] [IN] " - Coeff. Sfruttamento : 0.232 (fs=4.302)

Sforzo Normale di Progetto [daN] : 2465 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 598
 Momento Flettente Mz di Progetto [daNm] : -1822

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.15
 Tensione Resistente [N/mm²] : 14.57
 Coefficiente di Sfruttamento a trazione : 0.011
 fs : 94.53
 Tensione di Progetto relativa a My [N/mm²] : 0.22
 Tensione di Progetto relativa a Mz [N/mm²] : 4.27
 Tensione Resistente relativa a My [N/mm²] : 18.21
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.222
 fs : 4.51
 Coefficiente di Sfruttamento : 0.232
 fs : 4.3

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.051 (fs=19.488)

Taglio Ty di Progetto [daN] : 267
 Taglio Tz di Progetto [daN] : -6091
 Momento Torcente Mt di Progetto [daNm] : 193

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
 Tensione di Progetto relativa a Tz [N/mm²] : 0.57
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.215
 fs : 4.65
 Tensione di Progetto [N/mm²] : 0.03
 Modulo di resistenza a torsione [mm³] : 7785888
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.005
 fs : 201.24
 Coefficiente di Sfruttamento a taglio+torsione : 0.051
 fs : 19.49

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 25
 Lunghezza efficace nel piano XY : 1500.0
 Momento Critico nel piano XY : 1948144 daNm
 Tensione Critica nel piano XY : 4565.96 N/mmq
 Resistenza fless. piano XY : 20.03 N/mmq
 Tensione fless. piano XY : 4.28 N/mmq
 Snellezza relativa nel piano XY : 0.07
 Coeff. Riduttivo nel piano XY : 1.000
 Coefficiente sfrutt. nel piano XY : 0.214
 Coeff. sfrutt. max euleriano : 0.000
 Coeff. sfrutt. TOTALE (Piano XY) : 0.214
 fs : 4.675

Sezione più sfavorevole : 1
 Lunghezza efficace nel piano XZ : 1500.0
 Momento Critico nel piano XZ : 311703 daNm
 Tensione Critica nel piano XZ : 116.89 N/mmq
 Resistenza fless. piano XZ : 18.21 N/mmq
 Tensione fless. piano XZ : 0.18 N/mmq
 Snellezza relativa nel piano XZ : 0.45
 Coeff. Riduttivo nel piano XZ : 1.000
 Coefficiente sfrutt. nel piano XZ : 0.010
 Coeff. sfrutt. TOTALE (Piano XZ) : 0.010

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1500.0 mm
Comb. di carico più gravosa : 142
Carico distribuito Istantaneo : -322.3 daN/m

-

Freccia Istantanea - COMBINAZIONE

Freccia Finale - COMBINAZIONE

Modulo Elastico istantaneo : 11500.0 N/mm²

Controfreccia : 0.000 mm

Freccia Istantanea : 0.000 mm

Freccia Netta Finale : 0.000 mm

Freccia Finale : 0.000 mm

Fatt. sicurezza freccia Istantanea : 1000.000

Fatt. sicurezza freccia Finale : 1000.000

Schema adottato Doppio Incastro

Peso proprio : -61.6 daN/m

-

Carico distribuito Finale : -223.6 daN/m

Comb 42 [CAR] [ST]

Comb 2 [SLEQP] [PE]

Modulo Elastico finale : 6388.9 N/mm²

Limite Freccia Istantanea L/500 : 3.000 mm

Limite Freccia Netta Fin. L/ 350 : 4.286 mm

Limite Freccia Finale L/ 300 : 5.000 mm

Fatt. sicurezza freccia Netta Finale : 1000.000

Fatt. sicurezza : 1000.000

Campata 154-29 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.244 (fs=4.096)

Sforzo Normale di Progetto [daN] : 7621 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : -8652

Momento Flettente Mz di Progetto [daNm] : 406

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.48

Tensione Resistente [N/mm²] : 14.57

Coefficiente di Sfruttamento a trazione : 0.033

fs : 30.58

Tensione di Progetto relativa a My [N/mm²] : 3.24

Tensione di Progetto relativa a Mz [N/mm²] : 0.95

Tensione Resistente relativa a My [N/mm²] : 18.21

Tensione Resistente relativa a Mz [N/mm²] : 20.03

Coefficiente di Sfruttamento a flessione : 0.211

fs : 4.73

Coefficiente di Sfruttamento : 0.244

fs : 4.1

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.121 (fs=8.281)

Taglio Ty di Progetto [daN] : -270

Taglio Tz di Progetto [daN] : 3409

Momento Torcente Mt di Progetto [daNm] : 481

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03

Tensione di Progetto relativa a Tz [N/mm²] : 0.32

Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a taglio : 0.121

fs : 8.28

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 0.96 N/mm ²	Tensione fless. piano XZ	: 3.13 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.048	Coefficiente sfrutt. nel piano XZ	: 0.172
Coeff. sfrutt. max euleriano	: 0.014		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.062	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.186
fs	: 5.369		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 30-153 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.248 (fs=4.029)

Sforzo Normale di Progetto [daN]	: 7637 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -8802
Momento Flettente Mz di Progetto [daNm]	: 416

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.48
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.033
fs	: 30.51
Tensione di Progetto relativa a My [N/mm ²]	: 3.3
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.98
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.215
fs	: 4.64
Coefficiente di Sfruttamento	: 0.248
fs	: 4.03

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.068 (fs=14.725)

Taglio Ty di Progetto [daN] : -499
 Taglio Tz di Progetto [daN] : -6641
 Momento Torcente Mt di Progetto [daNm] : 416

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.05
 Tensione di Progetto relativa a Tz [N/mm²] : 0.62
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.235
 fs : 4.25
 Tensione di Progetto [N/mm²] : 0.06
 Modulo di resistenza a torsione [mm³] : 7785888
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.013
 fs : 79.27
 Coefficiente di Sfruttamento a taglio+torsione : 0.068
 fs : 14.72

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 10	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm²	Tensione Critica nel piano XZ	: 116.89 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 0.97 N/mm²	Tensione fless. piano XZ	: 3.19 N/mm²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.048	Coefficiente sfrutt. nel piano XZ	: 0.175
Coeff. sfrutt. max euleriano	: 0.014		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.063	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.189
fs	: 5.279		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 158-31 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.24 (fs=4.172)

Sforzo Normale di Progetto [daN] : 7479 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -8789
 Momento Flettente Mz di Progetto [daNm] : 324

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.47
 Tensione Resistente [N/mm²] : 14.57
 Coefficiente di Sfruttamento a trazione : 0.032
 fs : 31.16
 Tensione di Progetto relativa a My [N/mm²] : 3.3
 Tensione di Progetto relativa a Mz [N/mm²] : 0.76
 Tensione Resistente relativa a My [N/mm²] : 18.21
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.208
 fs : 4.82
 Coefficiente di Sfruttamento : 0.24
 fs : 4.17

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.212 (fs=4.727)

Taglio Ty di Progetto [daN] : -145
 Taglio Tz di Progetto [daN] : -5990
 Momento Torcente Mt di Progetto [daNm] : -396

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.01
 Tensione di Progetto relativa a Tz [N/mm²] : 0.56
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.212
 fs : 4.73

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 0.77 N/mm ²	Tensione fless. piano XZ	: 3.18 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.038	Coefficiente sfrutt. nel piano XZ	: 0.175
Coeff. sfrutt. max euleriano	: 0.014		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.052	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.189
fs	: 5.301		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m

Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 32-157 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.246 (fs=4.057)

Sforzo Normale di Progetto [daN]	: 7575 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -9029
Momento Flettente Mz di Progetto [daNm]	: 342

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.47
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.033
fs	: 30.77
Tensione di Progetto relativa a My [N/mm ²]	: 3.39
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.8
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.214
fs	: 4.67
Coefficiente di Sfruttamento	: 0.246
fs	: 4.06

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.07 (fs=14.238)

Taglio Ty di Progetto [daN]	: -247
Taglio Tz di Progetto [daN]	: -6844
Momento Torcente Mt di Progetto [daNm]	: 342

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.64
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.242
fs	: 4.14
Tensione di Progetto [N/mm ²]	: 0.06
Modulo di resistenza a torsione [mm ³]	: 7785888
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.012
fs	: 84.97
Coefficiente di Sfruttamento a taglio+torsione	: 0.07
fs	: 14.24

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 10	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 0.79 N/mm ²	Tensione fless. piano XZ	: 3.27 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.040	Coefficiente sfrutt. nel piano XZ	: 0.180
Coeff. sfrutt. max euleriano	: 0.014		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.054	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.194
fs	: 5.156		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 162-33 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.237 (fs=4.224)

Sforzo Normale di Progetto [daN]	: 7187 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -9018
Momento Flettente Mz di Progetto [daNm]	: 246

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.45
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.031
fs	: 32.43
Tensione di Progetto relativa a My [N/mm ²]	: 3.38
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.58
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.206
fs	: 4.86
Coefficiente di Sfruttamento	: 0.237
fs	: 4.22

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 45 [SLV] [IN] " - Coeff. Sfruttamento : 0.126 (fs=7.913)

Taglio Ty di Progetto [daN] : -381
 Taglio Tz di Progetto [daN] : 3559
 Momento Torcente Mt di Progetto [daNm] : 454

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.04
 Tensione di Progetto relativa a Tz [N/mm²] : 0.33
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.126
 fs : 7.91

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mmq	Tensione Critica nel piano XZ	: 116.89 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.21 N/mmq
Tensione fless. piano XY	: 0.59 N/mmq	Tensione fless. piano XZ	: 3.27 N/mmq
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.029	Coefficiente sfrutt. nel piano XZ	: 0.180
Coeff. sfrutt. max euleriano	: 0.013		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.042	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.192
fs	: 5.198		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 34-161 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.233 (fs=4.286)

Sforzo Normale di Progetto [daN] : 7003 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -8812

Momento Flettente Mz di Progetto [daNm] : 266

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.44
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.03
fs	: 33.28
Tensione di Progetto relativa a My [N/mm ²]	: 3.3
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.62
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.203
fs	: 4.92
Coefficiente di Sfruttamento	: 0.233
fs	: 4.29

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.067 (fs=14.935)

Taglio Ty di Progetto [daN]	: -579
Taglio Tz di Progetto [daN]	: -6677
Momento Torcente Mt di Progetto [daNm]	: 266

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.05
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.63
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.237
fs	: 4.23
Tensione di Progetto [N/mm ²]	: 0.06
Modulo di resistenza a torsione [mm ³]	: 7785888
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.011
fs	: 91.28
Coefficiente di Sfruttamento a taglio+torsione	: 0.067
fs	: 14.94

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 49	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 3.93 N/mm ²	Tensione fless. piano XZ	: 0.47 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.196	Coefficiente sfrutt. nel piano XZ	: 0.026
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.196	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.026
fs	: 5.096		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	

-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 166-35 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.222 ($f_s=4.5$)

Sforzo Normale di Progetto [daN]	: 7302 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -8842
Momento Flettente Mz di Progetto [daNm]	: -107

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.46
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.031
f_s	: 31.91
Tensione di Progetto relativa a My [N/mm ²]	: 3.32
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.25
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.191
f_s	: 5.24
Coefficiente di Sfruttamento	: 0.222
f_s	: 4.5

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.203 ($f_s=4.915$)

Taglio Ty di Progetto [daN]	: -379
Taglio Tz di Progetto [daN]	: -5750
Momento Torcente Mt di Progetto [daNm]	: -108

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.54
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.203
f_s	: 4.91

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 18	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²

Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 0.22 N/mm ²	Tensione fless. piano XZ	: 3.21 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.011	Coefficiente sfrutt. nel piano XZ	: 0.176
Coeff. sfrutt. max euleriano	: 0.013		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.024	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.190
fs	: 5.268		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 36-165 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 48 [SLV] [IN] " - Coeff. Sfruttamento : 0.242 (fs=4.127)

Sforzo Normale di Progetto [daN]	: 5037 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 1320
Momento Flettente Mz di Progetto [daNm]	: -1723

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.31
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.022
fs	: 46.26
Tensione di Progetto relativa a My [N/mm ²]	: 0.49
Tensione di Progetto relativa a Mz [N/mm ²]	: 4.04
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.221
fs	: 4.53
Coefficiente di Sfruttamento	: 0.242
fs	: 4.13

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.068 (fs=14.756)

Taglio Ty di Progetto [daN]	: -541
Taglio Tz di Progetto [daN]	: -6817

Momento Torcente Mt di Progetto [daNm]	: 178	
Tipo Verifica		: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.05	
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.64	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a taglio	: 0.241	
fs	: 4.14	
Tensione di Progetto [N/mm ²]	: 0.05	
Modulo di resistenza a torsione [mm ³]	: 7785888	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a torsione	: 0.009	
fs	: 105.63	
Coefficiente di Sfruttamento a taglio+torsione	: 0.068	
fs	: 14.76	

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 41	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 4.21 N/mm ²	Tensione fless. piano XZ	: 0.38 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.210	Coefficiente sfrutt. nel piano XZ	: 0.021
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.210	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.021
fs	: 4.758		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 170-37 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.234 (fs=4.281)

Sforzo Normale di Progetto [daN] : 6902 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : -9075
 Momento Flettente Mz di Progetto [daNm] : -208

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.43
 Tensione Resistente [N/mm²] : 14.57
 Coefficiente di Sfruttamento a trazione : 0.03
 fs : 33.77
 Tensione di Progetto relativa a My [N/mm²] : 3.4
 Tensione di Progetto relativa a Mz [N/mm²] : 0.49
 Tensione Resistente relativa a My [N/mm²] : 18.21
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.204
 fs : 4.9
 Coefficiente di Sfruttamento : 0.234
 fs : 4.28

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.204 (fs=4.9)

Taglio Ty di Progetto [daN] : -72
 Taglio Tz di Progetto [daN] : -5779
 Momento Torcente Mt di Progetto [daNm] : 61

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.01
 Tensione di Progetto relativa a Tz [N/mm²] : 0.54
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.204
 fs : 4.9

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 18	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948145 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 0.48 N/mm ²	Tensione fless. piano XZ	: 3.29 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.024	Coefficiente sfrutt. nel piano XZ	: 0.181
Coeff. sfrutt. max euleriano	: 0.012		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.036	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.193
fs	: 5.192		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1500.0 mm
 Comb. di carico più gravosa : 142
 Carico distribuito Istantaneo : -322.3 daN/m
 -
 Freccia Istantanea - COMBINAZIONE
 Freccia Finale - COMBINAZIONE
 Modulo Elastico istantaneo : 11500.0 N/mm²
 Controfreccia : 0.000 mm
 Freccia Istantanea : 0.000 mm

Schema adottato Doppio Incastro
 Peso proprio : -61.6 daN/m
 -
 Carico distribuito Finale : -223.6 daN/m
 Comb 42 [CAR] [ST]
 Comb 2 [SLEQP] [PE]
 Modulo Elastico finale : 6388.9 N/mm²
 Limite Freccia Istantanea L/500 : 3.000 mm

Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 38-169 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 48 [SLV] [IN] " - Coeff. Sfruttamento : 0.23 (fs=4.342)

Sforzo Normale di Progetto [daN]	: 5695 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 1378
Momento Flettente Mz di Progetto [daNm]	: -1590

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.36
Tensione Resistente [N/mm²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.024
fs	: 40.92
Tensione di Progetto relativa a My [N/mm²]	: 0.52
Tensione di Progetto relativa a Mz [N/mm²]	: 3.73
Tensione Resistente relativa a My [N/mm²]	: 18.21
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.206
fs	: 4.86
Coefficiente di Sfruttamento	: 0.23
fs	: 4.34

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.065 (fs=15.272)

Taglio Ty di Progetto [daN]	: -566
Taglio Tz di Progetto [daN]	: -6718
Momento Torcente Mt di Progetto [daNm]	: 66

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²]	: 0.05
Tensione di Progetto relativa a Tz [N/mm²]	: 0.63
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.238
fs	: 4.2
Tensione di Progetto [N/mm²]	: 0.05
Modulo di resistenza a torsione [mm³]	: 7785888
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.009
fs	: 113.4
Coefficiente di Sfruttamento a taglio+torsione	: 0.065
fs	: 15.27

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm

Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 0.18 N/mm ²	Tensione fless. piano XZ	: 3.23 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.009	Coefficiente sfrutt. nel piano XZ	: 0.177
Coeff. sfrutt. max euleriano	: 0.015		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.024	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.192
fs	: 5.200		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 175-39 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.216 (fs=4.639)

Sforzo Normale di Progetto [daN]	: 7368 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -8848
Momento Flettente Mz di Progetto [daNm]	: -21

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.46
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.032
fs	: 31.63
Tensione di Progetto relativa a My [N/mm ²]	: 3.32
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.05
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.184
fs	: 5.44
Coefficiente di Sfruttamento	: 0.216
fs	: 4.64

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.235 (fs=4.25)

Taglio Ty di Progetto [daN]	: 30
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Taglio Tz di Progetto [daN] : 6664
 Momento Torcente Mt di Progetto [daNm] : -21

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
 Tensione di Progetto relativa a Tz [N/mm²] : 0.62
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.235
 fs : 4.25

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 14	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948143 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mmq	Tensione Critica nel piano XZ	: 116.89 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.21 N/mmq
Tensione fless. piano XY	: 0.04 N/mmq	Tensione fless. piano XZ	: 3.20 N/mmq
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.002	Coefficiente sfrutt. nel piano XZ	: 0.176
Coeff. sfrutt. max euleriano	: 0.014		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.016	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.190
fs	: 5.276		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 40-173 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
 L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.217 (fs=4.618)

Sforzo Normale di Progetto [daN] : 8134 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -7706
 Momento Flettente Mz di Progetto [daNm] : -280

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.51
 Tensione Resistente [N/mm²] : 14.57

Coefficiente di Sfruttamento a trazione	: 0.035
fs	: 28.65
Tensione di Progetto relativa a My [N/mm ²]	: 2.89
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.66
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.182
fs	: 5.51
Coefficiente di Sfruttamento	: 0.217
fs	: 4.62

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.059 (fs=17.071)

Taglio Ty di Progetto [daN]	: -320
Taglio Tz di Progetto [daN]	: -6339
Momento Torcente Mt di Progetto [daNm]	: -1

Tipo Verifica	: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.59
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.224
fs	: 4.46
Tensione di Progetto [N/mm ²]	: 0.04
Modulo di resistenza a torsione [mm ³]	: 7785888
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.008
fs	: 119.63
Coefficiente di Sfruttamento a taglio+torsione	: 0.059
fs	: 17.07

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 0.02 N/mm ²	Tensione fless. piano XZ	: 3.09 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.001	Coefficiente sfrutt. nel piano XZ	: 0.169
Coeff. sfrutt. max euleriano	: 0.015		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.016	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.184
fs	: 5.426		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		

Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 178-41 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.223 (fs=4.48)

Sforzo Normale di Progetto [daN]	: 11873 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -7223
Momento Flettente Mz di Progetto [daNm]	: -287

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.74
Tensione Resistente [N/mm²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.051
fs	: 19.63
Tensione di Progetto relativa a My [N/mm²]	: 2.71
Tensione di Progetto relativa a Mz [N/mm²]	: 0.67
Tensione Resistente relativa a My [N/mm²]	: 18.21
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.172
fs	: 5.8
Coefficiente di Sfruttamento	: 0.223
fs	: 4.48

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.21 (fs=4.758)

Taglio Ty di Progetto [daN]	: 100
Taglio Tz di Progetto [daN]	: 5952
Momento Torcente Mt di Progetto [daNm]	: -67

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm²]	: 0.56
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.21
fs	: 4.76

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 14	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948145 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm²	Tensione Critica nel piano XZ	: 116.89 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 0.15 N/mm²	Tensione fless. piano XZ	: 2.86 N/mm²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.008	Coefficiente sfrutt. nel piano XZ	: 0.157

TABULATI DI CALCOLO -

Coeff. sfrutt. max euleriano : 0.019
 Coeff. sfrutt. TOTALE (Piano XY) : 0.027
 fs : 5.676

Coeff. sfrutt. TOTALE (Piano XZ) : 0.176

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 42-177 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
 L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 48 [SLV] [IN] " - Coeff. Sfruttamento : 0.256 (fs=3.906)

Sforzo Normale di Progetto [daN]	: 9057 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 1804
Momento Flettente Mz di Progetto [daNm]	: -1633

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.57
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.039
fs	: 25.73
Tensione di Progetto relativa a My [N/mm ²]	: 0.68
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.83
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.217
fs	: 4.61
Coefficiente di Sfruttamento	: 0.256
fs	: 3.91

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.056 (fs=17.749)

Taglio Ty di Progetto [daN]	: -195
Taglio Tz di Progetto [daN]	: -6246
Momento Torcente Mt di Progetto [daNm]	: -78

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.59

Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.221
fs	: 4.53
Tensione di Progetto [N/mm ²]	: 0.04
Modulo di resistenza a torsione [mm ³]	: 7785888
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.008
fs	: 130.64
Coefficiente di Sfruttamento a taglio+torsione	: 0.056
fs	: 17.75

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 3.84 N/mm ²	Tensione fless. piano XZ	: 0.57 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.192	Coefficiente sfrutt. nel piano XZ	: 0.032
Coeff. sfrutt. max euleriano	: 0.016		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.208	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.048
fs	: 4.807		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 43-181 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.246 (fs=4.066)

Sforzo Normale di Progetto [daN]	: 5554 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 650
Momento Flettente Mz di Progetto [daNm]	: 1818

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.35
---	--------

Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.024
fs	: 41.96
Tensione di Progetto relativa a My [N/mm ²]	: 0.24
Tensione di Progetto relativa a Mz [N/mm ²]	: 4.26
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.222
fs	: 4.5
Coefficiente di Sfruttamento	: 0.246
fs	: 4.07

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.053 (fs=18.83)

Taglio Ty di Progetto [daN]	: -605
Taglio Tz di Progetto [daN]	: -6112
Momento Torcente Mt di Progetto [daNm]	: -104

Tipo Verifica	: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.06
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.57
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.217
fs	: 4.61
Tensione di Progetto [N/mm ²]	: 0.03
Modulo di resistenza a torsione [mm ³]	: 7785888
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.006
fs	: 164.32
Coefficiente di Sfruttamento a taglio+torsione	: 0.053
fs	: 18.83

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 33	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 4.28 N/mm ²	Tensione fless. piano XZ	: 0.07 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.214	Coefficiente sfrutt. nel piano XZ	: 0.004
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.216	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.006
fs	: 4.632		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -322.3 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm ²

Schema adottato Doppio Incastro	
Peso proprio	: -61.6 daN/m
-	
Carico distribuito Finale	: -223.6 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [PE]	
Modulo Elastico finale	: 6388.9 N/mm ²

Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 182-44 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.198 (fs=5.054)

Sforzo Normale di Progetto [daN]	: 5523 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -7975
Momento Flettente Mz di Progetto [daNm]	: -121

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.35
Tensione Resistente [N/mm²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.024
fs	: 42.2
Tensione di Progetto relativa a My [N/mm²]	: 2.99
Tensione di Progetto relativa a Mz [N/mm²]	: 0.28
Tensione Resistente relativa a My [N/mm²]	: 18.21
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.174
fs	: 5.74
Coefficiente di Sfruttamento	: 0.198
fs	: 5.05

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 12 [SLD] [IN] " - Coeff. Sfruttamento : 0.204 (fs=4.906)

Taglio Ty di Progetto [daN]	: 355
Taglio Tz di Progetto [daN]	: 5763
Momento Torcente Mt di Progetto [daNm]	: -115

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm²]	: 0.54
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.204
fs	: 4.91

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 14	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm²	Tensione Critica nel piano XZ	: 116.89 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 0.28 N/mm²	Tensione fless. piano XZ	: 2.88 N/mm²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000

TABULATI DI CALCOLO -

Coefficiente sfrutt. nel piano XY	: 0.014	Coefficiente sfrutt. nel piano XZ	: 0.158
Coeff. sfrutt. max euleriano	: 0.007		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.021	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.165
fs	: 6.056		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 45-185 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.238 (fs=4.195)

Sforzo Normale di Progetto [daN]	: 4761 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 141
Momento Flettente Mz di Progetto [daNm]	: -1845

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.3
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.02
fs	: 48.95
Tensione di Progetto relativa a My [N/mm ²]	: 0.05
Tensione di Progetto relativa a Mz [N/mm ²]	: 4.32
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.218
fs	: 4.59
Coefficiente di Sfruttamento	: 0.238
fs	: 4.19

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.053 (fs=18.695)

Taglio Ty di Progetto [daN]	: 558
Taglio Tz di Progetto [daN]	: -5678
Momento Torcente Mt di Progetto [daNm]	: -512

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.05
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Tensione di Progetto relativa a Tz [N/mm ²]	: 0.53
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.201
fs	: 4.96
Tensione di Progetto [N/mm ²]	: 0.07
Modulo di resistenza a torsione [mm ³]	: 7785888
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.013
fs	: 77.48
Coefficiente di Sfruttamento a taglio+torsione	: 0.053
fs	: 18.7

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 4.30 N/mm ²	Tensione fless. piano XZ	: 0.09 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.215	Coefficiente sfrutt. nel piano XZ	: 0.005
Coeff. sfrutt. max euleriano	: 0.002		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.217	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.007
fs	: 4.606		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 186-46 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.231 (fs=4.333)

Sforzo Normale di Progetto [daN]	: 7815 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -7623
Momento Flettente Mz di Progetto [daNm]	: -491

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.49
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.034
fs	: 29.82
Tensione di Progetto relativa a My [N/mm ²]	: 2.86
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.15
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.197
fs	: 5.07
Coefficiente di Sfruttamento	: 0.231
fs	: 4.33

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.204 (fs=4.908)

Taglio Ty di Progetto [daN]	: -295
Taglio Tz di Progetto [daN]	: 5763
Momento Torcente Mt di Progetto [daNm]	: -491

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.54
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.204
fs	: 4.91

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 18	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.15 N/mm ²	Tensione fless. piano XZ	: 2.75 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.058	Coefficiente sfrutt. nel piano XZ	: 0.151
Coeff. sfrutt. max euleriano	: 0.015		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.073	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.166
fs	: 6.032		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 47-189 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.215 (fs=4.655)

Sforzo Normale di Progetto [daN]	: 6249 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -6753
Momento Flettente Mz di Progetto [daNm]	: -598

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.39
Tensione Resistente [N/mm²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.027
fs	: 37.3
Tensione di Progetto relativa a My [N/mm²]	: 2.53
Tensione di Progetto relativa a Mz [N/mm²]	: 1.4
Tensione Resistente relativa a My [N/mm²]	: 18.21
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.188
fs	: 5.32
Coefficiente di Sfruttamento	: 0.215
fs	: 4.65

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.047 (fs=21.373)

Taglio Ty di Progetto [daN]	: 257
Taglio Tz di Progetto [daN]	: -5157
Momento Torcente Mt di Progetto [daNm]	: -598

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm²]	: 0.48
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.182
fs	: 5.48
Tensione di Progetto [N/mm²]	: 0.07
Modulo di resistenza a torsione [mm³]	: 7785888
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.014
fs	: 73.82
Coefficiente di Sfruttamento a taglio+torsione	: 0.047
fs	: 21.37

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 49	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mmq	Tensione Critica nel piano XZ	: 116.89 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.21 N/mmq
Tensione fless. piano XY	: 3.73 N/mmq	Tensione fless. piano XZ	: 0.06 N/mmq
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45

Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.186	Coefficiente sfrutt. nel piano XZ	: 0.004
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.186	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.004
fs	: 5.369		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 190-48 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.206 (fs=4.861)

Sforzo Normale di Progetto [daN]	: 6413 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -6367
Momento Flettente Mz di Progetto [daNm]	: -574

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.4
Tensione Resistente [N/mm²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.028
fs	: 36.34
Tensione di Progetto relativa a My [N/mm²]	: 2.39
Tensione di Progetto relativa a Mz [N/mm²]	: 1.35
Tensione Resistente relativa a My [N/mm²]	: 18.21
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.178
fs	: 5.61
Coefficiente di Sfruttamento	: 0.206
fs	: 4.86

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 8 [SLD] [IN] " - Coeff. Sfruttamento : 0.156 (fs=6.394)

Taglio Ty di Progetto [daN]	: 287
Taglio Tz di Progetto [daN]	: 4420
Momento Torcente Mt di Progetto [daNm]	: -549

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.03
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.41
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.156
f_s	: 6.39

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 18	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 1.35 N/mm ²	Tensione fless. piano XZ	: 2.28 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.067	Coefficiente sfrutt. nel piano XZ	: 0.125
Coeff. sfrutt. max euleriano	: 0.010		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.077	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.135
f_s	: 7.395		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 49-193 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.204 ($f_s=4.897$)

Sforzo Normale di Progetto [daN]	: 3020 (TRAZIONE)
Momento Flettente M_y di Progetto [daNm]	: 351
Momento Flettente M_z di Progetto [daNm]	: 1591

Tipo Verifica : TRAZIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: 0.19
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.013
f_s	: 77.17
Tensione di Progetto relativa a M_y [N/mm ²]	: 0.13
Tensione di Progetto relativa a M_z [N/mm ²]	: 3.73

Tensione Resistente relativa a M_y [N/mm ²]	: 18.21
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.191
f_s	: 5.23
Coefficiente di Sfruttamento	: 0.204
f_s	: 4.9

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.044 ($f_s=22.791$)

Taglio T_y di Progetto [daN]	: 1387
Taglio T_z di Progetto [daN]	: -2546
Momento Torcente M_t di Progetto [daNm]	: -691

Tipo Verifica	: TAGLIO+TORSIONE
Tensione di Progetto relativa a T_y [N/mm ²]	: 0.13
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.24
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.102
f_s	: 9.77
Tensione di Progetto [N/mm ²]	: 0.17
Modulo di resistenza a torsione [mm ³]	: 7785888
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.033
f_s	: 29.94
Coefficiente di Sfruttamento a taglio+torsione	: 0.044
f_s	: 22.79

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 49	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 3.84 N/mm ²	Tensione fless. piano XZ	: 0.06 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.192	Coefficiente sfrutt. nel piano XZ	: 0.003
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.192	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.003
f_s	: 5.216		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000

Fatt. sicurezza freccia Finale : 1000.000

Fatt. sicurezza : 1000.000

Campata 195-50 Coper[Trave]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.186 (fs=5.365)

Sforzo Normale di Progetto [daN] : 5361 (TRAZIONE)

Momento Flettente My di Progetto [daNm] : -5395

Momento Flettente Mz di Progetto [daNm] : -638

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.34

Tensione Resistente [N/mm²] : 14.57

Coefficiente di Sfruttamento a trazione : 0.023

fs : 43.47

Tensione di Progetto relativa a My [N/mm²] : 2.02

Tensione di Progetto relativa a Mz [N/mm²] : 1.5

Tensione Resistente relativa a My [N/mm²] : 18.21

Tensione Resistente relativa a Mz [N/mm²] : 20.03

Coefficiente di Sfruttamento a flessione : 0.163

fs : 6.12

Coefficiente di Sfruttamento : 0.186

fs : 5.36

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 8 [SLD] [IN] " - Coeff. Sfruttamento : 0.129 (fs=7.731)

Taglio Ty di Progetto [daN] : -39

Taglio Tz di Progetto [daN] : 3663

Momento Torcente Mt di Progetto [daNm] : -592

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00

Tensione di Progetto relativa a Tz [N/mm²] : 0.34

Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a taglio : 0.129

fs : 7.73

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 13

Lunghezza efficace nel piano XY : 1500.0

Momento Critico nel piano XY : 1948144 daNm

Tensione Critica nel piano XY : 4565.96 N/mm²

Resistenza fless. piano XY : 20.03 N/mm²

Tensione fless. piano XY : 0.89 N/mm²

Snellezza relativa nel piano XY : 0.07

Coeff. Riduttivo nel piano XY : 1.000

Coefficiente sfrutt. nel piano XY : 0.044

Coeff. sfrutt. max euleriano : 0.000

Coeff. sfrutt. TOTALE (Piano XY) : 0.044

fs : 8.074

Sezione più sfavorevole : 1

Lunghezza efficace nel piano XZ : 1500.0

Momento Critico nel piano XZ : 311703 daNm

Tensione Critica nel piano XZ : 116.89 N/mm²

Resistenza fless. piano XZ : 18.21 N/mm²

Tensione fless. piano XZ : 2.25 N/mm²

Snellezza relativa nel piano XZ : 0.45

Coeff. Riduttivo nel piano XZ : 1.000

Coefficiente sfrutt. nel piano XZ : 0.124

Coeff. sfrutt. TOTALE (Piano XZ) : 0.124

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 51-197 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 26 [SLD] [IN] " - Coeff. Sfruttamento : 0.215 (fs=4.646)

Sforzo Normale di Progetto [daN]	: 2744 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -227
Momento Flettente Mz di Progetto [daNm]	: 1710

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.17
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.012
fs	: 84.92
Tensione di Progetto relativa a My [N/mm ²]	: 0.09
Tensione di Progetto relativa a Mz [N/mm ²]	: 4.01
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.203
fs	: 4.92
Coefficiente di Sfruttamento	: 0.215
fs	: 4.65

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.047 (fs=21.192)

Taglio Ty di Progetto [daN]	: -1387
Taglio Tz di Progetto [daN]	: -3444
Momento Torcente Mt di Progetto [daNm]	: 359

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.13
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.32
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.131
fs	: 7.63
Tensione di Progetto [N/mm ²]	: 0.15

Modulo di resistenza a torsione [mm ³]	: 7785888
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.03
fs	: 33.33
Coefficiente di Sfruttamento a taglio+torsione	: 0.047
fs	: 21.19

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 49	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 4.04 N/mm ²	Tensione fless. piano XZ	: 0.22 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.201	Coefficiente sfrutt. nel piano XZ	: 0.012
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.201	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.012
fs	: 4.963		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 199-52 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.16 (fs=6.232)

Sforzo Normale di Progetto [daN]	: 4957 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 108
Momento Flettente Mz di Progetto [daNm]	: -1176

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.31
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.021
fs	: 47.02
Tensione di Progetto relativa a My [N/mm ²]	: 0.04

Tensione di Progetto relativa a M_z [N/mm ²]	: 2.76
Tensione Resistente relativa a M_y [N/mm ²]	: 18.21
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.139
f_s	: 7.18
Coefficiente di Sfruttamento	: 0.16
f_s	: 6.23

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 8 [SLD] [IN] " - Coeff. Sfruttamento : 0.086 ($f_s=11.686$)

Taglio T_y di Progetto [daN]	: 367
Taglio T_z di Progetto [daN]	: 2396
Momento Torcente M_t di Progetto [daNm]	: -619

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.03
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.22
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.086
f_s	: 11.69

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.76 N/mm ²	Tensione fless. piano XZ	: 0.04 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.138	Coefficiente sfrutt. nel piano XZ	: 0.002
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.138	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.002
f_s	: 7.266		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 53-201 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 48 [SLV] [IN] " - Coeff. Sfruttamento : 0.238 (fs=4.202)

Sforzo Normale di Progetto [daN]	: 2803 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 424
Momento Flettente Mz di Progetto [daNm]	: -1879

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.18
Tensione Resistente [N/mm²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.012
fs	: 83.15
Tensione di Progetto relativa a My [N/mm²]	: 0.16
Tensione di Progetto relativa a Mz [N/mm²]	: 4.4
Tensione Resistente relativa a My [N/mm²]	: 18.21
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.226
fs	: 4.43
Coefficiente di Sfruttamento	: 0.238
fs	: 4.2

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.039 (fs=25.406)

Taglio Ty di Progetto [daN]	: -1396
Taglio Tz di Progetto [daN]	: -2369
Momento Torcente Mt di Progetto [daNm]	: 341

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²]	: 0.13
Tensione di Progetto relativa a Tz [N/mm²]	: 0.22
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.097
fs	: 10.3
Tensione di Progetto [N/mm²]	: 0.15
Modulo di resistenza a torsione [mm³]	: 7785888
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.03
fs	: 33.41
Coefficiente di Sfruttamento a taglio+torsione	: 0.039
fs	: 25.41

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 49	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mmq	Tensione Critica nel piano XZ	: 116.89 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.21 N/mmq
Tensione fless. piano XY	: 4.44 N/mmq	Tensione fless. piano XZ	: 0.15 N/mmq
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.222	Coefficiente sfrutt. nel piano XZ	: 0.008
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.222	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.008
fs	: 4.506		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 202-54 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.182 (fs=5.506)

Sforzo Normale di Progetto [daN]	: 2888 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 445
Momento Flettente Mz di Progetto [daNm]	: -1391

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.18
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.012
fs	: 80.71
Tensione di Progetto relativa a My [N/mm ²]	: 0.17
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.26
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.169
fs	: 5.91
Coefficiente di Sfruttamento	: 0.182
fs	: 5.51

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 8 [SLD] [IN] " - Coeff. Sfruttamento : 0.084 (fs=11.943)

Taglio Ty di Progetto [daN]	: -329
Taglio Tz di Progetto [daN]	: 2348
Momento Torcente Mt di Progetto [daNm]	: -597

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.22
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.084
fs	: 11.94

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 3.26 N/mm ²	Tensione fless. piano XZ	: 0.17 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.163	Coefficiente sfrutt. nel piano XZ	: 0.009
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.163	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.009
fs	: 6.142		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 55-205 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.234 (fs=4.277)

Sforzo Normale di Progetto [daN]	: 4502 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -182
Momento Flettente Mz di Progetto [daNm]	: -1810

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.28
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.019
fs	: 51.76
Tensione di Progetto relativa a My [N/mm ²]	: 0.07
Tensione di Progetto relativa a Mz [N/mm ²]	: 4.24
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.214
fs	: 4.66
Coefficiente di Sfruttamento	: 0.234

fs

: 4.28

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.051 (fs=19.502)

Taglio Ty di Progetto [daN] : 11
 Taglio Tz di Progetto [daN] : -924
 Momento Torcente Mt di Progetto [daNm] : -5

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
 Tensione di Progetto relativa a Tz [N/mm²] : 0.09
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.051
 fs : 19.5

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm²	Tensione Critica nel piano XZ	: 116.89 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 18.21 N/mm²
Tensione fless. piano XY	: 4.28 N/mm²	Tensione fless. piano XZ	: 0.17 N/mm²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.214	Coefficiente sfrutt. nel piano XZ	: 0.009
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.214	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.009
fs	: 4.679		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -342.1 daN/m	-	
-		Carico distribuito Finale	: -238.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 206-56 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1500 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.161 (fs=6.216)

Sforzo Normale di Progetto [daN]	: 4581 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -588
Momento Flettente Mz di Progetto [daNm]	: -1134

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.29
Tensione Resistente [N/mm ²]	: 14.57
Coefficiente di Sfruttamento a trazione	: 0.02
fs	: 50.88
Tensione di Progetto relativa a My [N/mm ²]	: 0.22
Tensione di Progetto relativa a Mz [N/mm ²]	: 2.66
Tensione Resistente relativa a My [N/mm ²]	: 18.21
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.141
fs	: 7.08
Coefficiente di Sfruttamento	: 0.161
fs	: 6.22

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.118 (fs=8.51)

Taglio Ty di Progetto [daN]	: -22
Taglio Tz di Progetto [daN]	: 3328
Momento Torcente Mt di Progetto [daNm]	: 491

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.31
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.118
fs	: 8.51

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 40	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1500.0	Lunghezza efficace nel piano XZ	: 1500.0
Momento Critico nel piano XY	: 1948144 daNm	Momento Critico nel piano XZ	: 311703 daNm
Tensione Critica nel piano XY	: 4565.96 N/mm ²	Tensione Critica nel piano XZ	: 116.89 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 2.66 N/mm ²	Tensione fless. piano XZ	: 0.22 N/mm ²
Snellezza relativa nel piano XY	: 0.07	Snellezza relativa nel piano XZ	: 0.45
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.133	Coefficiente sfrutt. nel piano XZ	: 0.012
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.133	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.012
fs	: 7.533		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -342.1 daN/m	-	
-		Carico distribuito Finale	: -238.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		

Freccia Istantanea	: 0.000 mm	Limite Freccia Istantanea L/500	: 3.000 mm
Freccia Netta Finale	: 0.000 mm	Limite Freccia Netta Fin. L/ 350	: 4.286 mm
Freccia Finale	: 0.000 mm	Limite Freccia Finale L/ 300	: 5.000 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 57-75 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.552 ($f_s=1.811$)

Sforzo Normale di Progetto [daN]	: 1401 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 284

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.97
Tensione Resistente [N/mm²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.061
f_s	: 16.46
Tensione di Progetto relativa a My [N/mm²]	: 0
Tensione di Progetto relativa a Mz [N/mm²]	: 9.85
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.492
f_s	: 2.03
Coefficiente di Sfruttamento	: 0.552
f_s	: 1.81

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 49 [SLV] [IN] " - Coeff. Sfruttamento : 0.065 ($f_s=15.39$)

Taglio Ty di Progetto [daN]	: 166
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: -96

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.17
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.065
f_s	: 15.39

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellenza nel piano XY	: 47.52	Snellenza nel piano XZ	: 67.89
Snellenza relativa nel piano XY	: 0.76	Snellenza relativa nel piano XZ	: 1.08
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 26
Coefficiente K nel piano XY	: 0.81	Coefficiente K nel piano XZ	: 1.12
Coefficiente Kc nel piano XY	: 0.91	Coefficiente Kc nel piano XZ	: 0.70
Coefficiente di sfruttamento nel piano XY	: 0.545	Coefficiente di sfruttamento nel piano XZ	: 0.558
f_s	: 1.792		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 26	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2351.8	Lunghezza efficace nel piano XZ	: 2351.8
Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mm ²	Tensione Critica nel piano XZ	: 289.24 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 10.05 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.502	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.056		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.558	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.056
fs	: 1.792		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2351.8 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.232 mm	Limite Freccia Istantanea L/500	: 4.704 mm
Freccia Netta Finale	: -0.418 mm	Limite Freccia Netta Fin. L/ 350	: 6.719 mm
Freccia Finale	: -0.418 mm	Limite Freccia Finale L/ 300	: 7.839 mm
Fatt. sicurezza freccia Istantanea	: 20.243	Fatt. sicurezza freccia Netta Finale	: 16.066
Fatt. sicurezza freccia Finale	: 18.744	Fatt. sicurezza	: 16.066

Campata 75-58 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.224 (fs=4.456)

Sforzo Normale di Progetto [daN]	: 968 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -105

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.67
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.042
fs	: 23.83
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 3.65
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.182
fs	: 5.48
Coefficiente di Sfruttamento	: 0.224
fs	: 4.46

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.022 (fs=45.895)

Taglio Ty di Progetto [daN]	: -55
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: 32

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.06
Tensione di Progetto relativa a Tz [N/mm²]	: 0.00
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.022
fs	: 45.89

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 47.52	Snellezza nel piano XZ	: 54.31
Snellezza relativa nel piano XY	: 0.76	Snellezza relativa nel piano XZ	: 0.86
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46
Coefficiente K nel piano XY	: 0.81	Coefficiente K nel piano XZ	: 0.90
Coefficiente Kc nel piano XY	: 0.91	Coefficiente Kc nel piano XZ	: 0.86
Coefficiente di sfruttamento nel piano XY	: 0.220	Coefficiente di sfruttamento nel piano XZ	: 0.223
fs	: 4.478		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2351.8	Lunghezza efficace nel piano XZ	: 2351.8
Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mm²	Tensione Critica nel piano XZ	: 289.24 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 3.09 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.154	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.069		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.223	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.069
fs	: 4.478		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2351.8 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -6.0 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm²
Controfreccia	: 0.000 mm
Freccia Istantanea	: -0.096 mm
Freccia Netta Finale	: -0.174 mm
Freccia Finale	: -0.174 mm
Fatt. sicurezza freccia Istantanea	: 48.763
Fatt. sicurezza freccia Finale	: 45.151

Schema adottato Incastro-Cerniera	
Peso proprio	: -5.5 daN/m
-	
Carico distribuito Finale	: -6.0 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [PE]	
Modulo Elastico finale	: 6388.9 N/mm²
Limite Freccia Istantanea L/500	: 4.704 mm
Limite Freccia Netta Fin. L/ 350	: 6.719 mm
Limite Freccia Finale L/ 300	: 7.839 mm
Fatt. sicurezza freccia Netta Finale	: 38.701
Fatt. sicurezza	: 38.701

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.131 (fs=7.619)

Sforzo Normale di Progetto [daN] : 1527 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 0
Momento Flettente Mz di Progetto [daNm] : -38

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 1.06
Tensione Resistente [N/mm²] : 16.02
Coefficiente di Sfruttamento a trazione : 0.066
fs : 15.11
Tensione di Progetto relativa a My [N/mm²] : 0
Tensione di Progetto relativa a Mz [N/mm²] : 1.3
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.065
fs : 15.37
Coefficiente di Sfruttamento : 0.131
fs : 7.62

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.013 (fs=78.272)

Taglio Ty di Progetto [daN] : -32
Taglio Tz di Progetto [daN] : -2
Momento Torcente Mt di Progetto [daNm] : 32

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
Tensione di Progetto relativa a Tz [N/mm²] : 0.00
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.013
fs : 78.27

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 53.25
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 0.85
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 9
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 0.89
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.87
Coefficiente di sfruttamento nel piano XY	: 0.139	Coefficiente di sfruttamento nel piano XZ	: 0.142
fs	: 7.021		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 9	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm
Tensione Critica nel piano XY	: 295.02 N/mmq	Tensione Critica nel piano XZ	: 295.02 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq

Tensione fless. piano XY	: 1.30 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.065	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.078		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.142	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.078
fs	: 7.021		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2305.7 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.089 mm	Limite Freccia Istantanea L/500	: 4.611 mm
Freccia Netta Finale	: -0.160 mm	Limite Freccia Netta Fin. L/ 350	: 6.588 mm
Freccia Finale	: -0.160 mm	Limite Freccia Finale L/ 300	: 7.686 mm
Fatt. sicurezza freccia Istantanea	: 51.748	Fatt. sicurezza freccia Netta Finale	: 41.070
Fatt. sicurezza freccia Finale	: 47.915	Fatt. sicurezza	: 41.070

Campata 62-77 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.123 (fs=8.152)

Sforzo Normale di Progetto [daN]	: 1551 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: -32

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1.08
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.067
fs	: 14.88
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.11
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.055
fs	: 18.03
Coefficiente di Sfruttamento	: 0.123
fs	: 8.15

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 34 [SLD] [IN] " - Coeff. Sfruttamento : 0.011 (fs=93.019)

Taglio Ty di Progetto [daN]	: 27
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -28

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.03
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.011
fs	: 93.02

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 66.56
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 1.06
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 18
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 1.10
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.72
Coefficiente di sfruttamento nel piano XY	: 0.125	Coefficiente di sfruttamento nel piano XZ	: 0.144
fs	: 6.935		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 18	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm
Tensione Critica nel piano XY	: 295.02 N/mm ²	Tensione Critica nel piano XZ	: 295.02 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.11 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.056	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.089		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.144	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.089
fs	: 6.935		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2305.7 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.215 mm	Limite Freccia Istantanea L/500	: 4.611 mm
Freccia Netta Finale	: -0.386 mm	Limite Freccia Netta Fin. L/ 350	: 6.588 mm
Freccia Finale	: -0.386 mm	Limite Freccia Finale L/ 300	: 7.686 mm
Fatt. sicurezza freccia Istantanea	: 21.482	Fatt. sicurezza freccia Netta Finale	: 17.050
Fatt. sicurezza freccia Finale	: 19.891	Fatt. sicurezza	: 17.050

Campata 65-78 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 18 [SLD] [IN] " - Coeff. Sfruttamento : 0.123 (fs=8.149)

Sforzo Normale di Progetto [daN] : 1565 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 0
 Momento Flettente Mz di Progetto [daNm] : 32

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 1.09
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.068
 fs : 14.75
 Tensione di Progetto relativa a My [N/mm²] : 0
 Tensione di Progetto relativa a Mz [N/mm²] : 1.1
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.055
 fs : 18.21
 Coefficiente di Sfruttamento : 0.123
 fs : 8.15

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.011 (fs=94.613)

Taglio Ty di Progetto [daN] : -27
 Taglio Tz di Progetto [daN] : -2
 Momento Torcente Mt di Progetto [daNm] : -25

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.00
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.011
 fs : 94.61

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 66.56
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 1.06
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 1.10
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.72
Coefficiente di sfruttamento nel piano XY	: 0.122	Coefficiente di sfruttamento nel piano XZ	: 0.145
fs	: 6.906		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm
Tensione Critica nel piano XY	: 295.02 N/mm²	Tensione Critica nel piano XZ	: 295.02 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 0.82 N/mm²	Tensione fless. piano XZ	: 0.00 N/mm²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.041	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.104		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.145	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.104
fs	: 6.906		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2305.7 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.215 mm	Limite Freccia Istantanea L/500	: 4.611 mm
Freccia Netta Finale	: -0.386 mm	Limite Freccia Netta Fin. L/ 350	: 6.588 mm
Freccia Finale	: -0.386 mm	Limite Freccia Finale L/ 300	: 7.686 mm
Fatt. sicurezza freccia Istantanea	: 21.482	Fatt. sicurezza freccia Netta Finale	: 17.050
Fatt. sicurezza freccia Finale	: 19.891	Fatt. sicurezza	: 17.050

Campata 78-66 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2305.67 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.129 (fs=7.748)

Sforzo Normale di Progetto [daN]	: 1546 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 36

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1.07
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.067
fs	: 14.92
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.24
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.062
fs	: 16.12
Coefficiente di Sfruttamento	: 0.129
fs	: 7.75

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2305.67 mm / 2305.67 mm] - **R 120x120**

Comb. più gravosa : " Comb 40 [SLV] [IN] " - Coeff. Sfruttamento : 0.013 (fs=79.499)

Taglio Ty di Progetto [daN]	: 32
Taglio Tz di Progetto [daN]	: -2
Momento Torcente Mt di Progetto [daNm]	: -35

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.013
fs	: 79.5

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 46.59	Snellezza nel piano XZ	: 53.25
Snellezza relativa nel piano XY	: 0.74	Snellezza relativa nel piano XZ	: 0.85
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 18
Coefficiente K nel piano XY	: 0.80	Coefficiente K nel piano XZ	: 0.89
Coefficiente Kc nel piano XY	: 0.92	Coefficiente Kc nel piano XZ	: 0.87
Coefficiente di sfruttamento nel piano XY	: 0.137	Coefficiente di sfruttamento nel piano XZ	: 0.141
fs	: 7.111		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 18	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2305.7	Lunghezza efficace nel piano XZ	: 2305.7
Momento Critico nel piano XY	: 8497 daNm	Momento Critico nel piano XZ	: 8497 daNm
Tensione Critica nel piano XY	: 295.02 N/mm ²	Tensione Critica nel piano XZ	: 295.02 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.23 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.062	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.079		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.141	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.079
fs	: 7.111		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2305.7 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.089 mm	Limite Freccia Istantanea L/500	: 4.611 mm
Freccia Netta Finale	: -0.160 mm	Limite Freccia Netta Fin. L/ 350	: 6.588 mm
Freccia Finale	: -0.160 mm	Limite Freccia Finale L/ 300	: 7.686 mm
Fatt. sicurezza freccia Istantanea	: 51.748	Fatt. sicurezza freccia Netta Finale	: 41.070
Fatt. sicurezza freccia Finale	: 47.915	Fatt. sicurezza	: 41.070

Campata 69-76 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.143 (fs=6.995)

Sforzo Normale di Progetto [daN]	: 1890 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 35

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 1.31
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.082
fs	: 12.21
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.22
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.061
fs	: 16.38
Coefficiente di Sfruttamento	: 0.143
fs	: 6.99

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**
Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.011 (fs=87.491)

Taglio Ty di Progetto [daN]	: 29
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: -34

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.011
fs	: 87.49

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 1.00
Snellezza nel piano XY	: 47.52	Snellezza nel piano XZ	: 67.89
Snellezza relativa nel piano XY	: 0.76	Snellezza relativa nel piano XZ	: 1.08
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 13
Coefficiente K nel piano XY	: 0.81	Coefficiente K nel piano XZ	: 1.12
Coefficiente Kc nel piano XY	: 0.91	Coefficiente Kc nel piano XZ	: 0.70
Coefficiente di sfruttamento nel piano XY	: 0.131	Coefficiente di sfruttamento nel piano XZ	: 0.153
fs	: 6.522		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 2351.8	Lunghezza efficace nel piano XZ	: 2351.8
Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mm ²	Tensione Critica nel piano XZ	: 289.24 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.12 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.056	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.097		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.153	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.097
fs	: 6.522		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2351.8 mm	Schema adottato Doppia Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m

Carico distribuito Istantaneo	: -6.0 daN/m	-	Carico distribuito Finale	: -6.0 daN/m
-			Comb 42 [CAR] [ST]	
Freccia Istantanea - COMBINAZIONE			Comb 2 [SLEQP] [PE]	
Freccia Finale - COMBINAZIONE			Modulo Elastico finale	: 6388.9 N/mm ²
Modulo Elastico istantaneo	: 11500.0 N/mm ²			
Controfreccia	: 0.000 mm			
Freccia Istantanea	: -0.232 mm	Limite Freccia Istantanea L/500	: 4.704 mm	
Freccia Netta Finale	: -0.418 mm	Limite Freccia Netta Fin. L/ 350	: 6.719 mm	
Freccia Finale	: -0.418 mm	Limite Freccia Finale L/ 300	: 7.839 mm	
Fatt. sicurezza freccia Istantanea	: 20.243	Fatt. sicurezza freccia Netta Finale	: 16.066	
Fatt. sicurezza freccia Finale	: 18.744	Fatt. sicurezza	: 16.066	

Campata 76-70 Copert[Asta GEN.]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 2351.79 mm - **R 120x120** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.107 (fs=9.371)

Sforzo Normale di Progetto [daN]	: 1184 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 0
Momento Flettente Mz di Progetto [daNm]	: 32

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.82
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.051
fs	: 19.49
Tensione di Progetto relativa a My [N/mm ²]	: 0
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.11
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.055
fs	: 18.05
Coefficiente di Sfruttamento	: 0.107
fs	: 9.37

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=2351.79 mm / 2351.79 mm] - **R 120x120**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.013 (fs=75.467)

Taglio Ty di Progetto [daN]	: -34
Taglio Tz di Progetto [daN]	: -3
Momento Torcente Mt di Progetto [daNm]	: 41

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.00
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.013
fs	: 75.47

VERIFICA DI INSTABILITA' EULERIANA

Coefficiente Beta nel piano XY	: 0.70	Coefficiente Beta nel piano XZ	: 0.80
Snellezza nel piano XY	: 47.52	Snellezza nel piano XZ	: 54.31
Snellezza relativa nel piano XY	: 0.76	Snellezza relativa nel piano XZ	: 0.86
Coefficiente Beta c	: 0.10	Combinazione più sfavorevole	: 46

Coefficiente K nel piano XY	: 0.81	Coefficiente K nel piano XZ	: 0.90
Coefficiente Kc nel piano XY	: 0.91	Coefficiente Kc nel piano XZ	: 0.86
Coefficiente di sfruttamento nel piano XY	: 0.130	Coefficiente di sfruttamento nel piano XZ	: 0.133
fs	: 7.513		

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 2351.8	Lunghezza efficace nel piano XZ	: 2351.8
Momento Critico nel piano XY	: 8330 daNm	Momento Critico nel piano XZ	: 8330 daNm
Tensione Critica nel piano XY	: 289.24 N/mm ²	Tensione Critica nel piano XZ	: 289.24 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.41 N/mm ²	Tensione fless. piano XZ	: 0.00 N/mm ²
Snellezza relativa nel piano XY	: 0.29	Snellezza relativa nel piano XZ	: 0.29
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.071	Coefficiente sfrutt. nel piano XZ	: 0.000
Coeff. sfrutt. max euleriano	: 0.062		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.133	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.062
fs	: 7.513		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 2351.8 mm	Schema adottato Incastro-Cerniera	
Comb. di carico più gravosa	: 142	Peso proprio	: -5.5 daN/m
Carico distribuito Istantaneo	: -6.0 daN/m	-	
-		Carico distribuito Finale	: -6.0 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.096 mm	Limite Freccia Istantanea L/500	: 4.704 mm
Freccia Netta Finale	: -0.174 mm	Limite Freccia Netta Fin. L/ 350	: 6.719 mm
Freccia Finale	: -0.174 mm	Limite Freccia Finale L/ 300	: 7.839 mm
Fatt. sicurezza freccia Istantanea	: 48.763	Fatt. sicurezza freccia Netta Finale	: 38.701
Fatt. sicurezza freccia Finale	: 45.151	Fatt. sicurezza	: 38.701

Campata 79-81 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1590 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1590 mm] - **R 140x180**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.337 (fs=2.968)

Sforzo Normale di Progetto [daN]	: 169 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -441
Momento Flettente Mz di Progetto [daNm]	: 70

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.07
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.004
fs	: 238.3
Tensione di Progetto relativa a My [N/mm ²]	: 5.83
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.18
Tensione Resistente relativa a My [N/mm ²]	: 20.03

Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.333
f_s	: 3.01
Coefficiente di Sfruttamento	: 0.337
f_s	: 2.97

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1590 mm] - **R 140x180**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.126 ($f_s=7.94$)

Taglio T_y di Progetto [daN]	: 85
Taglio T_z di Progetto [daN]	: 555
Momento Torcente M_t di Progetto [daNm]	: 70

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.05
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.33
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.126
f_s	: 7.94

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 37	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1590.0	Lunghezza efficace nel piano XZ	: 1590.0
Momento Critico nel piano XY	: 39411 daNm	Momento Critico nel piano XZ	: 30653 daNm
Tensione Critica nel piano XY	: 670.25 N/mm ²	Tensione Critica nel piano XZ	: 405.46 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 1.18 N/mm ²	Tensione fless. piano XZ	: 5.83 N/mm ²
Snellezza relativa nel piano XY	: 0.19	Snellezza relativa nel piano XZ	: 0.24
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.059	Coefficiente sfrutt. nel piano XZ	: 0.291
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.059	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.291
f_s	: 3.433		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale ($t > \inf$)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1590.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.004 mm	Limite Freccia Istantanea L/500	: 3.180 mm
Freccia Netta Finale	: -0.008 mm	Limite Freccia Netta Fin. L/ 350	: 4.543 mm
Freccia Finale	: -0.008 mm	Limite Freccia Finale L/ 300	: 5.300 mm
Fatt. sicurezza freccia Istantanea	: 736.946	Fatt. sicurezza freccia Netta Finale	: 584.878
Fatt. sicurezza freccia Finale	: 682.357	Fatt. sicurezza	: 584.878

Campata 80-82 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320.83 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320.83 mm] - **R 140x180**
 Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.281 (fs=3.552)
 Sforzo Normale di Progetto [daN] : 133 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : -357
 Momento Flettente Mz di Progetto [daNm] : -71

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.05
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.003
 fs : 303.99
 Tensione di Progetto relativa a My [N/mm²] : 4.73
 Tensione di Progetto relativa a Mz [N/mm²] : 1.21
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.278
 fs : 3.59
 Coefficiente di Sfruttamento : 0.281
 fs : 3.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320.83 mm / 1320.83 mm] - **R 140x180**
 Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.126 (fs=7.95)
 Taglio Ty di Progetto [daN] : 22
 Taglio Tz di Progetto [daN] : -561
 Momento Torcente Mt di Progetto [daNm] : -34

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.01
 Tensione di Progetto relativa a Tz [N/mm²] : 0.33
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.126
 fs : 7.95

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.8	Lunghezza efficace nel piano XZ	: 1320.8
Momento Critico nel piano XY	: 47442 daNm	Momento Critico nel piano XZ	: 36900 daNm
Tensione Critica nel piano XY	: 806.84 N/mmq	Tensione Critica nel piano XZ	: 488.09 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 0.11 N/mmq	Tensione fless. piano XZ	: 4.87 N/mmq
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.006	Coefficiente sfrutt. nel piano XZ	: 0.243
Coeff. sfrutt. max euleriano	: 0.004		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.010	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.247
fs	: 4.051		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.8 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m

Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.642 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.774 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.403 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 83-84 Copert[Trave]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.256 (fs=3.902)

Sforzo Normale di Progetto [daN]	: -26 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -353
Momento Flettente Mz di Progetto [daNm]	: 39

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.01
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.001
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 4.67
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.66
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.256
fs	: 3.9
Coefficiente di Sfruttamento a pressoflessione	: 0.256
fs	: 3.9

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.122 (fs=8.221)

Taglio Ty di Progetto [daN]	: -53
Taglio Tz di Progetto [daN]	: -540
Momento Torcente Mt di Progetto [daNm]	: 39

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.32
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.122
fs	: 8.22

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mm ²	Tensione Critica nel piano XZ	: 488.40 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²

Tensione fless. piano XY	: 0.66 N/mm ²	Tensione fless. piano XZ	: 4.67 N/mm ²
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.033	Coefficiente sfrutt. nel piano XZ	: 0.233
Coeff. sfrutt. max euleriano	: 0.001		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.033	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.234
fs	: 4.277		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 85-86 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.251 (fs=3.98)

Sforzo Normale di Progetto [daN]	: -22 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -351
Momento Flettente Mz di Progetto [daNm]	: -32

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.01
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.000
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 4.65
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.55
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.251
fs	: 3.98
Coefficiente di Sfruttamento a pressoflessione	: 0.251
fs	: 3.98

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.121 (fs=8.26)

Taglio Ty di Progetto [daN]	: 50
Taglio Tz di Progetto [daN]	: -538
Momento Torcente Mt di Progetto [daNm]	: -32

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.32
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.121
fs	: 8.26

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mm ²	Tensione Critica nel piano XZ	: 488.40 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.55 N/mm ²	Tensione fless. piano XZ	: 4.65 N/mm ²
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.027	Coefficiente sfrutt. nel piano XZ	: 0.232
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.028	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.233
fs	: 4.300		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 87-88 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)
L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.253 (fs=3.949)

Sforzo Normale di Progetto [daN]	: -23 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -344
Momento Flettente Mz di Progetto [daNm]	: 44

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.01
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.001
fs	: 1000

Tensione di Progetto relativa a M_y [N/mm ²]	: 4.55
Tensione di Progetto relativa a M_z [N/mm ²]	: 0.75
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.253
f_s	: 3.95
Coefficiente di Sfruttamento a pressoflessione	: 0.253
f_s	: 3.95

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.118 ($f_s=8.467$)

Taglio T_y di Progetto [daN]	: -18
Taglio T_z di Progetto [daN]	: -527
Momento Torcente M_t di Progetto [daNm]	: 44

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.01
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.31
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.118
f_s	: 8.47

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mm ²	Tensione Critica nel piano XZ	: 488.40 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.75 N/mm ²	Tensione fless. piano XZ	: 4.55 N/mm ²
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.037	Coefficiente sfrutt. nel piano XZ	: 0.227
Coeff. sfrutt. max euleriano	: 0.001		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.038	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.228
f_s	: 4.395		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale ($t > \inf$)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 89-90 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

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L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7
VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 140x180**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.24 (fs=4.163)

Sforzo Normale di Progetto [daN]	: 32 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -343
Momento Flettente Mz di Progetto [daNm]	: -22

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: 0.01
Tensione Resistente [N/mm²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.001
fs	: 1000
Tensione di Progetto relativa a My [N/mm²]	: 4.53
Tensione di Progetto relativa a Mz [N/mm²]	: 0.37
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.239
fs	: 4.18
Coefficiente di Sfruttamento	: 0.24
fs	: 4.16

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.117 (fs=8.522)

Taglio Ty di Progetto [daN]	: 7
Taglio Tz di Progetto [daN]	: -523
Momento Torcente Mt di Progetto [daNm]	: -22

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm²]	: 0.31
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.117
fs	: 8.52

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mmq	Tensione Critica nel piano XZ	: 488.40 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 0.37 N/mmq	Tensione fless. piano XZ	: 4.53 N/mmq
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.019	Coefficiente sfrutt. nel piano XZ	: 0.226
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.019	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.226
fs	: 4.417		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1320.0 mm

Schema adottato Doppio Incastro

Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 91-92 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.237 (fs=4.227)

Sforzo Normale di Progetto [daN]	: 55 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 326
Momento Flettente Mz di Progetto [daNm]	: 33

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.02
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.001
fs	: 739.47
Tensione di Progetto relativa a My [N/mm ²]	: 4.32
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.57
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.235
fs	: 4.25
Coefficiente di Sfruttamento	: 0.237
fs	: 4.23

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.113 (fs=8.846)

Taglio Ty di Progetto [daN]	: -13
Taglio Tz di Progetto [daN]	: -504
Momento Torcente Mt di Progetto [daNm]	: 18

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.3
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.113
fs	: 8.85

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0

Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mm ²	Tensione Critica nel piano XZ	: 488.40 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.31 N/mm ²	Tensione fless. piano XZ	: 4.36 N/mm ²
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.015	Coefficiente sfrutt. nel piano XZ	: 0.218
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.015	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.218
fs	: 4.589		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto			
Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 93-94 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.242 (fs=4.131)

Sforzo Normale di Progetto [daN]	: -19 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 329
Momento Flettente Mz di Progetto [daNm]	: -42

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.01
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.000
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 4.35
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.71
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.242
fs	: 4.13
Coefficiente di Sfruttamento a pressoflessione	: 0.242
fs	: 4.13

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.114 (fs=8.75)

TABULATI DI CALCOLO -

Taglio Ty di Progetto [daN]	: -16
Taglio Tz di Progetto [daN]	: -510
Momento Torcente Mt di Progetto [daNm]	: 21

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.3
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.114
fs	: 8.75

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mm ²	Tensione Critica nel piano XZ	: 488.40 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.35 N/mm ²	Tensione fless. piano XZ	: 4.42 N/mm ²
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.018	Coefficiente sfrutt. nel piano XZ	: 0.221
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.018	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.221
fs	: 4.519		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 95-96 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 37 [SLD] [IN] " - Coeff. Sfruttamento : 0.235 (fs=4.248)

Sforzo Normale di Progetto [daN]	: 23 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 316
Momento Flettente Mz di Progetto [daNm]	: -44

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.01
---	--------

Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.001
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 4.18
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.75
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.235
fs	: 4.26
Coefficiente di Sfruttamento	: 0.235
fs	: 4.25

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.114 (fs=8.795)

Taglio Ty di Progetto [daN]	: -17
Taglio Tz di Progetto [daN]	: -507
Momento Torcente Mt di Progetto [daNm]	: 25

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.3
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.114
fs	: 8.79

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mm ²	Tensione Critica nel piano XZ	: 488.40 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.43 N/mm ²	Tensione fless. piano XZ	: 4.39 N/mm ²
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.021	Coefficiente sfrutt. nel piano XZ	: 0.219
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.021	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.219
fs	: 4.565		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 97-106 Coper[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.234 (fs=4.278)

Sforzo Normale di Progetto [daN] : -15 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : -338
Momento Flettente Mz di Progetto [daNm] : -18

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.01
Tensione Resistente [N/mm²] : 18.21
Coefficiente di Sfruttamento a compressione : 0.000
fs : 1000
Tensione di Progetto relativa a My [N/mm²] : 4.47
Tensione di Progetto relativa a Mz [N/mm²] : 0.3
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.234
fs : 4.28
Coefficiente di Sfruttamento a pressoflessione : 0.234
fs : 4.28

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.116 (fs=8.623)

Taglio Ty di Progetto [daN] : -2
Taglio Tz di Progetto [daN] : -517
Momento Torcente Mt di Progetto [daNm] : -18

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
Tensione di Progetto relativa a Tz [N/mm²] : 0.31
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.116
fs : 8.62

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mm²	Tensione Critica nel piano XZ	: 488.40 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 0.30 N/mm²	Tensione fless. piano XZ	: 4.47 N/mm²
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.015	Coefficiente sfrutt. nel piano XZ	: 0.223
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.015	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.223
fs	: 4.475		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1320.0 mm
Comb. di carico più gravosa : 142
Carico distribuito Istantaneo : -10.6 daN/m

Freccia Istantanea - COMBINAZIONE

Freccia Finale - COMBINAZIONE

Modulo Elastico istantaneo : 11500.0 N/mm²
Controfreccia : 0.000 mm
Freccia Istantanea : -0.002 mm
Freccia Netta Finale : -0.004 mm
Freccia Finale : -0.004 mm
Fatt. sicurezza freccia Istantanea : 1000.000
Fatt. sicurezza freccia Finale : 1000.000

Schema adottato Doppio Incastro

Peso proprio : -9.7 daN/m

-

Carico distribuito Finale : -10.6 daN/m

Comb 42 [CAR] [ST]

Comb 2 [SLEQP] [PE]

Modulo Elastico finale : 6388.9 N/mm²

Limite Freccia Istantanea L/500 : 2.640 mm

Limite Freccia Netta Fin. L/ 350 : 3.771 mm

Limite Freccia Finale L/ 300 : 4.400 mm

Fatt. sicurezza freccia Netta Finale : 1000.000

Fatt. sicurezza : 1000.000

Campata 98-99 Copert[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.343 (fs=2.919)

Sforzo Normale di Progetto [daN] : -25 (COMPRESSIONE)

Momento Flettente My di Progetto [daNm] : 486

Momento Flettente Mz di Progetto [daNm] : -36

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -0.01

Tensione Resistente [N/mm²] : 18.21

Coefficiente di Sfruttamento a compressione : 0.001

fs : 1000

Tensione di Progetto relativa a My [N/mm²] : 6.43

Tensione di Progetto relativa a Mz [N/mm²] : 0.62

Tensione Resistente relativa a My [N/mm²] : 20.03

Tensione Resistente relativa a Mz [N/mm²] : 20.03

Coefficiente di Sfruttamento a flessione : 0.343

fs : 2.92

Coefficiente di Sfruttamento a pressoflessione : 0.343

fs : 2.92

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.168 (fs=5.942)

Taglio Ty di Progetto [daN] : -39

Taglio Tz di Progetto [daN] : -750

Momento Torcente Mt di Progetto [daNm] : 25

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02

Tensione di Progetto relativa a Tz [N/mm²] : 0.45

Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a taglio : 0.168

fs : 5.94

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mm ²	Tensione Critica nel piano XZ	: 488.40 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.42 N/mm ²	Tensione fless. piano XZ	: 6.54 N/mm ²
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.021	Coefficiente sfrutt. nel piano XZ	: 0.327
Coeff. sfrutt. max euleriano	: 0.001		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.021	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.327
fs	: 3.057		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 100-101 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.354 (fs=2.825)

Sforzo Normale di Progetto [daN]	: -6 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 504
Momento Flettente Mz di Progetto [daNm]	: -36

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.00
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.000
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 6.66
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.61
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.354
fs	: 2.82
Coefficiente di Sfruttamento a pressoflessione	: 0.354
fs	: 2.82

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**
 Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.174 (fs=5.762)
 Taglio Ty di Progetto [daN] : -38
 Taglio Tz di Progetto [daN] : -773
 Momento Torcente Mt di Progetto [daNm] : 26

Tipo Verifica : TAGLIO
 Tensione di Progetto relativa a Ty [N/mm²] : 0.02
 Tensione di Progetto relativa a Tz [N/mm²] : 0.46
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.174
 fs : 5.76

VERIFICA A SVERGOLAMENTO
 Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mmq	Tensione Critica nel piano XZ	: 488.40 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 0.44 N/mmq	Tensione fless. piano XZ	: 6.72 N/mmq
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.022	Coefficiente sfrutt. nel piano XZ	: 0.335
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.022	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.335
fs	: 2.981		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto		
Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro
Comb. di carico più gravosa	: 142	Peso proprio
Carico distribuito Istantaneo	: -10.6 daN/m	
-		Carico distribuito Finale
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale
Controfreccia	: 0.000 mm	
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza

Campata 102-103 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 140x180**
 Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.361 (fs=2.768)
 Sforzo Normale di Progetto [daN] : -18 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 502
 Momento Flettente Mz di Progetto [daNm] : -50

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -0.01
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.000
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 6.64
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.85
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.361
fs	: 2.77
Coefficiente di Sfruttamento a pressoflessione	: 0.361
fs	: 2.77

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.173 (fs=5.783)

Taglio Ty di Progetto [daN]	: -63
Taglio Tz di Progetto [daN]	: -769
Momento Torcente Mt di Progetto [daNm]	: 34

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.46
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.173
fs	: 5.78

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mm ²	Tensione Critica nel piano XZ	: 488.40 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.58 N/mm ²	Tensione fless. piano XZ	: 6.66 N/mm ²
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.029	Coefficiente sfrutt. nel piano XZ	: 0.332
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.029	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.333
fs	: 3.005		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm

Fatt. sicurezza freccia Istantanea : 1000.000
Fatt. sicurezza freccia Finale : 1000.000

Fatt. sicurezza freccia Netta Finale : 1000.000
Fatt. sicurezza : 1000.000

Campata 104-105 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.352 (fs=2.839)

Sforzo Normale di Progetto [daN] : 10 (TRAZIONE)
Momento Flettente My di Progetto [daNm] : 495
Momento Flettente Mz di Progetto [daNm] : 43

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.00
Tensione Resistente [N/mm²] : 16.02
Coefficiente di Sfruttamento a trazione : 0.000
fs : 1000
Tensione di Progetto relativa a My [N/mm²] : 6.54
Tensione di Progetto relativa a Mz [N/mm²] : 0.73
Tensione Resistente relativa a My [N/mm²] : 20.03
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.352
fs : 2.84
Coefficiente di Sfruttamento : 0.352
fs : 2.84

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.17 (fs=5.868)

Taglio Ty di Progetto [daN] : 54
Taglio Tz di Progetto [daN] : -758
Momento Torcente Mt di Progetto [daNm] : 35

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
Tensione di Progetto relativa a Tz [N/mm²] : 0.45
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.17
fs : 5.87

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 46
Lunghezza efficace nel piano XY : 1320.0
Momento Critico nel piano XY : 47472 daNm
Tensione Critica nel piano XY : 807.35 N/mmq
Resistenza fless. piano XY : 20.03 N/mmq
Tensione fless. piano XY : 0.60 N/mmq
Snellezza relativa nel piano XY : 0.17
Coeff. Riduttivo nel piano XY : 1.000
Coefficiente sfrutt. nel piano XY : 0.030
Coeff. sfrutt. max euleriano : 0.000
Coeff. sfrutt. TOTALE (Piano XY) : 0.030
fs : 3.046

Sezione più sfavorevole : 7
Lunghezza efficace nel piano XZ : 1320.0
Momento Critico nel piano XZ : 36923 daNm
Tensione Critica nel piano XZ : 488.40 N/mmq
Resistenza fless. piano XZ : 20.03 N/mmq
Tensione fless. piano XZ : 6.57 N/mmq
Snellezza relativa nel piano XZ : 0.22
Coeff. Riduttivo nel piano XZ : 1.000
Coefficiente sfrutt. nel piano XZ : 0.328

Coeff. sfrutt. TOTALE (Piano XZ) : 0.328

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 107-108 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.244 (fs=4.099)

Sforzo Normale di Progetto [daN]	: 22 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 355
Momento Flettente Mz di Progetto [daNm]	: 15

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.01
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.001
fs	: 1000
Tensione di Progetto relativa a My [N/mm ²]	: 4.7
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.25
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.243
fs	: 4.11
Coefficiente di Sfruttamento	: 0.244
fs	: 4.1

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.123 (fs=8.126)

Taglio Ty di Progetto [daN]	: 5
Taglio Tz di Progetto [daN]	: -549
Momento Torcente Mt di Progetto [daNm]	: 6

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.33
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.123
fs	: 8.13

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mm ²	Tensione Critica nel piano XZ	: 488.40 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.10 N/mm ²	Tensione fless. piano XZ	: 4.76 N/mm ²
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.005	Coefficiente sfrutt. nel piano XZ	: 0.238
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.005	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.238
fs	: 4.204		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 109-110 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1590 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1590 mm / 1590 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.276 (fs=3.624)

Sforzo Normale di Progetto [daN]	: 139 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -321
Momento Flettente Mz di Progetto [daNm]	: 102

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.05
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.003
fs	: 291.46
Tensione di Progetto relativa a My [N/mm ²]	: 4.24
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.74
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.273
fs	: 3.67
Coefficiente di Sfruttamento	: 0.276

fs

: 3.62

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1590 mm / 1590 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.094 (fs=10.59)

Taglio Ty di Progetto [daN] : -101
 Taglio Tz di Progetto [daN] : -409
 Momento Torcente Mt di Progetto [daNm] : 102

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.06
 Tensione di Progetto relativa a Tz [N/mm²] : 0.24
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.094
 fs : 10.59

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1590.0	Lunghezza efficace nel piano XZ	: 1590.0
Momento Critico nel piano XY	: 39411 daNm	Momento Critico nel piano XZ	: 30653 daNm
Tensione Critica nel piano XY	: 670.25 N/mmq	Tensione Critica nel piano XZ	: 405.46 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 1.74 N/mmq	Tensione fless. piano XZ	: 4.24 N/mmq
Snellezza relativa nel piano XY	: 0.19	Snellezza relativa nel piano XZ	: 0.24
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.087	Coefficiente sfrutt. nel piano XZ	: 0.212
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.087	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.212
fs	: 4.722		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1590.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.004 mm	Limite Freccia Istantanea L/500	: 3.180 mm
Freccia Netta Finale	: -0.008 mm	Limite Freccia Netta Fin. L/ 350	: 4.543 mm
Freccia Finale	: -0.008 mm	Limite Freccia Finale L/ 300	: 5.300 mm
Fatt. sicurezza freccia Istantanea	: 736.946	Fatt. sicurezza freccia Netta Finale	: 584.878
Fatt. sicurezza freccia Finale	: 682.357	Fatt. sicurezza	: 584.878

Campata 111-112 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1321.01 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1321.01 mm / 1321.01 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.353 (fs=2.83)

Sforzo Normale di Progetto [daN]	: 66 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -495
Momento Flettente Mz di Progetto [daNm]	: 42

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: 0.03
Tensione Resistente [N/mm ²]	: 16.02
Coefficiente di Sfruttamento a trazione	: 0.002
fs	: 611.7
Tensione di Progetto relativa a My [N/mm ²]	: 6.54
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.72
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.352
fs	: 2.84
Coefficiente di Sfruttamento	: 0.353
fs	: 2.83

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1321.01 mm / 1321.01 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.169 (fs=5.902)

Taglio Ty di Progetto [daN]	: -48
Taglio Tz di Progetto [daN]	: -754
Momento Torcente Mt di Progetto [daNm]	: 42

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.45
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.169
fs	: 5.9

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1321.0	Lunghezza efficace nel piano XZ	: 1321.0
Momento Critico nel piano XY	: 47436 daNm	Momento Critico nel piano XZ	: 36895 daNm
Tensione Critica nel piano XY	: 806.73 N/mm ²	Tensione Critica nel piano XZ	: 488.02 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.72 N/mm ²	Tensione fless. piano XZ	: 6.54 N/mm ²
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.036	Coefficiente sfrutt. nel piano XZ	: 0.327
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.036	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.327
fs	: 3.061		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1321.0 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -10.6 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm ²
Controfreccia	: 0.000 mm

Schema adottato Doppio Incastro	
Peso proprio	: -9.7 daN/m
-	
Carico distribuito Finale	: -10.6 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [PE]	
Modulo Elastico finale	: 6388.9 N/mm ²

Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.642 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.774 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.403 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 113-114 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.345 (fs=2.894)

Sforzo Normale di Progetto [daN]	: -19 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -487
Momento Flettente Mz di Progetto [daNm]	: -40

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -0.01
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.000
fs	: 1000
Tensione di Progetto relativa a My [N/mm²]	: 6.45
Tensione di Progetto relativa a Mz [N/mm²]	: 0.68
Tensione Resistente relativa a My [N/mm²]	: 20.03
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.345
fs	: 2.89
Coefficiente di Sfruttamento a pressoflessione	: 0.345
fs	: 2.89

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.167 (fs=5.973)

Taglio Ty di Progetto [daN]	: 59
Taglio Tz di Progetto [daN]	: -744
Momento Torcente Mt di Progetto [daNm]	: -40

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm²]	: 0.44
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.167
fs	: 5.97

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mm²	Tensione Critica nel piano XZ	: 488.40 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 20.03 N/mm²
Tensione fless. piano XY	: 0.68 N/mm²	Tensione fless. piano XZ	: 6.45 N/mm²
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.034	Coefficiente sfrutt. nel piano XZ	: 0.322

Coeff. sfrutt. max euleriano	: 0.000	
Coeff. sfrutt. TOTALE (Piano XY)	: 0.034	Coeff. sfrutt. TOTALE (Piano XZ) : 0.322
fs	: 3.103	

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 115-116 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.332 (fs=3.01)

Sforzo Normale di Progetto [daN]	: 4 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: -489
Momento Flettente Mz di Progetto [daNm]	: 16

Tipo Verifica : FLESSIONE - Kmod = 1.1

Tensione di Progetto relativa a My [N/mm ²]	: 6.46
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.27
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.332
fs	: 3.01

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.167 (fs=5.982)

Taglio Ty di Progetto [daN]	: -19
Taglio Tz di Progetto [daN]	: -745
Momento Torcente Mt di Progetto [daNm]	: 16

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.44
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.167
fs	: 5.98

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mm ²	Tensione Critica nel piano XZ	: 488.40 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.27 N/mm ²	Tensione fless. piano XZ	: 6.46 N/mm ²
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.014	Coefficiente sfrutt. nel piano XZ	: 0.323
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.014	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.323
fs	: 3.099		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 117-118 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 38 [SLV] [IN] " - Coeff. Sfruttamento : 0.342 (fs=2.923)

Sforzo Normale di Progetto [daN]	: 2 (TRAZIONE)
Momento Flettente My di Progetto [daNm]	: 473
Momento Flettente Mz di Progetto [daNm]	: -50

Tipo Verifica : FLESSIONE - Kmod = 1.1

Tensione di Progetto relativa a My [N/mm ²]	: 6.25
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.86
Tensione Resistente relativa a My [N/mm ²]	: 20.03
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.342
fs	: 2.92

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.169 (fs=5.911)

Taglio Ty di Progetto [daN]	: -36
Taglio Tz di Progetto [daN]	: -754
Momento Torcente Mt di Progetto [daNm]	: -20

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.02
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.45
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.169
f_s	: 5.91

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mm ²	Tensione Critica nel piano XZ	: 488.40 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.34 N/mm ²	Tensione fless. piano XZ	: 6.54 N/mm ²
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.017	Coefficiente sfrutt. nel piano XZ	: 0.326
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.017	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.326
f_s	: 3.063		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 119-120 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.351 ($f_s=2.852$)

Sforzo Normale di Progetto [daN]	: -4 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: -508
Momento Flettente M_z di Progetto [daNm]	: 26

Tipo Verifica : FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto relativa a M_y [N/mm ²]	: 6.72
Tensione di Progetto relativa a M_z [N/mm ²]	: 0.44
Tensione Resistente relativa a M_y [N/mm ²]	: 20.03
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03

Coefficiente di Sfruttamento a flessione : 0.351
fs : 2.85

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**
Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.173 (fs=5.765)
Taglio Ty di Progetto [daN] : -35
Taglio Tz di Progetto [daN] : -773
Momento Torcente Mt di Progetto [daNm] : 26

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
Tensione di Progetto relativa a Tz [N/mm²] : 0.46
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.173
fs : 5.77

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 7
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mmq	Tensione Critica nel piano XZ	: 488.40 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 20.03 N/mmq
Tensione fless. piano XY	: 0.44 N/mmq	Tensione fless. piano XZ	: 6.72 N/mmq
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.022	Coefficiente sfrutt. nel piano XZ	: 0.335
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.022	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.335
fs	: 2.981		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1320.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -9.7 daN/m
Carico distribuito Istantaneo	: -10.6 daN/m	-	
-		Carico distribuito Finale	: -10.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 121-122 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1320 mm - **R 140x180** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.355 (fs=2.82)

Sforzo Normale di Progetto [daN] : 38 (TRAZIONE)
 Momento Flettente My di Progetto [daNm] : 516
 Momento Flettente Mz di Progetto [daNm] : 22

Tipo Verifica : TRAZIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : 0.02
 Tensione Resistente [N/mm²] : 16.02
 Coefficiente di Sfruttamento a trazione : 0.001
 fs : 1000
 Tensione di Progetto relativa a My [N/mm²] : 6.82
 Tensione di Progetto relativa a Mz [N/mm²] : 0.37
 Tensione Resistente relativa a My [N/mm²] : 20.03
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.354
 fs : 2.83
 Coefficiente di Sfruttamento : 0.355
 fs : 2.82

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=1320 mm / 1320 mm] - **R 140x180**

Comb. più gravosa : " Comb 46 [SLV] [IN] " - Coeff. Sfruttamento : 0.176 (fs=5.666)

Taglio Ty di Progetto [daN] : -34
 Taglio Tz di Progetto [daN] : -787
 Momento Torcente Mt di Progetto [daNm] : 18

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.02
 Tensione di Progetto relativa a Tz [N/mm²] : 0.47
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.176
 fs : 5.67

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 46	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1320.0	Lunghezza efficace nel piano XZ	: 1320.0
Momento Critico nel piano XY	: 47472 daNm	Momento Critico nel piano XZ	: 36923 daNm
Tensione Critica nel piano XY	: 807.35 N/mm ²	Tensione Critica nel piano XZ	: 488.40 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 20.03 N/mm ²
Tensione fless. piano XY	: 0.37 N/mm ²	Tensione fless. piano XZ	: 6.82 N/mm ²
Snellezza relativa nel piano XY	: 0.17	Snellezza relativa nel piano XZ	: 0.22
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.019	Coefficiente sfrutt. nel piano XZ	: 0.341
Coeff. sfrutt. max euleriano	: 0.000		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.019	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.341
fs	: 2.936		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1320.0 mm
 Comb. di carico più gravosa : 142
 Carico distribuito Istantaneo : -10.6 daN/m
 -
 Freccia Istantanea - COMBINAZIONE
 Freccia Finale - COMBINAZIONE
 Modulo Elastico istantaneo : 11500.0 N/mm²

Schema adottato Doppio Incastro
 Peso proprio : -9.7 daN/m
 -
 Carico distribuito Finale : -10.6 daN/m
 Comb 42 [CAR] [ST]
 Comb 2 [SLEQP] [PE]
 Modulo Elastico finale : 6388.9 N/mm²

Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.002 mm	Limite Freccia Istantanea L/500	: 2.640 mm
Freccia Netta Finale	: -0.004 mm	Limite Freccia Netta Fin. L/ 350	: 3.771 mm
Freccia Finale	: -0.004 mm	Limite Freccia Finale L/ 300	: 4.400 mm
Fatt. sicurezza freccia Istantanea	: 1000.000	Fatt. sicurezza freccia Netta Finale	: 1000.000
Fatt. sicurezza freccia Finale	: 1000.000	Fatt. sicurezza	: 1000.000

Campata 124-125 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.27 (fs=3.697)

Sforzo Normale di Progetto [daN]	: -6260 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -323
Momento Flettente Mz di Progetto [daNm]	: 15

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²]	: -2.17
Tensione Resistente [N/mm²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.188
fs	: 5.33
Tensione di Progetto relativa a My [N/mm²]	: 2.81
Tensione di Progetto relativa a Mz [N/mm²]	: 0.26
Tensione Resistente relativa a My [N/mm²]	: 12.7
Tensione Resistente relativa a Mz [N/mm²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.235
fs	: 4.25
Coefficiente di Sfruttamento a pressoflessione	: 0.27
fs	: 3.7

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.111 (fs=8.984)

Taglio Ty di Progetto [daN]	: 68
Taglio Tz di Progetto [daN]	: 218
Momento Torcente Mt di Progetto [daNm]	: -43

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm²]	: 0.11
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.045
fs	: 22.28
Tensione di Progetto [N/mm²]	: 0.38
Modulo di resistenza a torsione [mm³]	: 886153.88
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.109
fs	: 9.15
Coefficiente di Sfruttamento a taglio+torsione	: 0.111
fs	: 8.98

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 1

Sezione più sfavorevole : 1

Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 12.70 N/mm ²
Tensione fless. piano XY	: 0.26 N/mm ²	Tensione fless. piano XZ	: 2.81 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.020	Coefficiente sfrutt. nel piano XZ	: 0.221
Coeff. sfrutt. max euleriano	: 0.198		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.218	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.419
fs	: 2.387		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 125-127 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 15500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7750 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.377 (fs=2.655)

Sforzo Normale di Progetto [daN]	: -1158 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 11630
Momento Flettente Mz di Progetto [daNm]	: 1

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.07
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.006
fs	: 160.05
Tensione di Progetto relativa a My [N/mm ²]	: 4.36
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.00
Tensione Resistente relativa a My [N/mm ²]	: 11.59
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.377
fs	: 2.66
Coefficiente di Sfruttamento a pressoflessione	: 0.377
fs	: 2.65

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=15500 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.185 (fs=5.402)

Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : -3336
 Momento Torcente Mt di Progetto [daNm] : 4

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.31
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.185
 fs : 5.4

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15500.0	Lunghezza efficace nel piano XZ	: 15500.0
Momento Critico nel piano XY	: 188530 daNm	Momento Critico nel piano XZ	: 30165 daNm
Tensione Critica nel piano XY	: 441.87 N/mmq	Tensione Critica nel piano XZ	: 11.31 N/mmq
Resistenza fless. piano XY	: 12.74 N/mmq	Resistenza fless. piano XZ	: 11.59 N/mmq
Tensione fless. piano XY	: 0.00 N/mmq	Tensione fless. piano XZ	: 4.36 N/mmq
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.269
Coeff. sfrutt. max euleriano	: 0.090		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.090	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.359
fs	: 2.789		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -342.1 daN/m	-	
-		Carico distribuito Finale	: -238.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.957 mm	Limite Freccia Istantanea L/500	: 31.000 mm
Freccia Netta Finale	: -5.288 mm	Limite Freccia Netta Fin. L/ 350	: 44.286 mm
Freccia Finale	: -5.288 mm	Limite Freccia Finale L/ 300	: 51.667 mm
Fatt. sicurezza freccia Istantanea	: 7.834	Fatt. sicurezza freccia Netta Finale	: 8.375
Fatt. sicurezza freccia Finale	: 9.771	Fatt. sicurezza	: 7.834

Campata 126-127 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.32 (fs=3.124)

Sforzo Normale di Progetto [daN] : -6381 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -324
 Momento Flettente Mz di Progetto [daNm] : -65

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -2.22
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.191
fs	: 5.23
Tensione di Progetto relativa a My [N/mm ²]	: 2.81
Tensione di Progetto relativa a Mz [N/mm ²]	: 1.13
Tensione Resistente relativa a My [N/mm ²]	: 12.7
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.284
fs	: 3.53
Coefficiente di Sfruttamento a pressoflessione	: 0.32
fs	: 3.12

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.071 (fs=14.073)

Taglio Ty di Progetto [daN]	: -44
Taglio Tz di Progetto [daN]	: 226
Momento Torcente Mt di Progetto [daNm]	: -65

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.02
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.12
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.071
fs	: 14.07

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 12.70 N/mm ²
Tensione fless. piano XY	: 1.13 N/mm ²	Tensione fless. piano XZ	: 2.81 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.088	Coefficiente sfrutt. nel piano XZ	: 0.222
Coeff. sfrutt. max euleriano	: 0.202		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.290	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.423
fs	: 2.362		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 128-129 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.245 ($f_s=4.076$)

Sforzo Normale di Progetto [daN]	: -5600 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -314
Momento Flettente Mz di Progetto [daNm]	: 2

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -1.94
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.168
f_s	: 5.96
Tensione di Progetto relativa a My [N/mm ²]	: 2.73
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.04
Tensione Resistente relativa a My [N/mm ²]	: 12.7
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.217
f_s	: 4.6
Coefficiente di Sfruttamento a pressoflessione	: 0.245
f_s	: 4.08

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.11 ($f_s=9.094$)

Taglio Ty di Progetto [daN]	: 61
Taglio Tz di Progetto [daN]	: 222
Momento Torcente Mt di Progetto [daNm]	: -60

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.12
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.045
f_s	: 22.11
Tensione di Progetto [N/mm ²]	: 0.37
Modulo di resistenza a torsione [mm ³]	: 886153.88
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.108
f_s	: 9.27
Coefficiente di Sfruttamento a taglio+torsione	: 0.11
f_s	: 9.09

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9
Momento Critico nel piano XY	: 43797 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²
Tensione fless. piano XY	: 0.04 N/mm ²
Snellezza relativa nel piano XY	: 0.18

Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XZ	: 12.70 N/mm ²
Tensione fless. piano XZ	: 2.73 N/mm ²
Snellezza relativa nel piano XZ	: 0.36

Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.003	Coefficiente sfrutt. nel piano XZ	: 0.215
Coeff. sfrutt. max euleriano	: 0.177		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.180	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.392
fs	: 2.551		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 129-130 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 15500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7750 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.391 (fs=2.555)

Sforzo Normale di Progetto [daN]	: -978 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 12090
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 189.64
Tensione di Progetto relativa a My [N/mm ²]	: 4.53
Tensione di Progetto relativa a Mz [N/mm ²]	: 0
Tensione Resistente relativa a My [N/mm ²]	: 11.59
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.391
fs	: 2.56
Coefficiente di Sfruttamento a pressoflessione	: 0.391
fs	: 2.56

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=15500 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.681)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: -3172
Momento Torcente Mt di Progetto [daNm]	: 1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.3
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.176
fs	: 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15500.0	Lunghezza efficace nel piano XZ	: 15500.0
Momento Critico nel piano XY	: 188530 daNm	Momento Critico nel piano XZ	: 30165 daNm
Tensione Critica nel piano XY	: 441.87 N/mm ²	Tensione Critica nel piano XZ	: 11.31 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 11.59 N/mm ²
Tensione fless. piano XY	: 0.00 N/mm ²	Tensione fless. piano XZ	: 4.53 N/mm ²
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.280
Coeff. sfrutt. max euleriano	: 0.076		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.076	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.355
fs	: 2.816		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.763 mm	Limite Freccia Istantanea L/500	: 31.000 mm
Freccia Netta Finale	: -5.032 mm	Limite Freccia Netta Fin. L/ 350	: 44.286 mm
Freccia Finale	: -5.032 mm	Limite Freccia Finale L/ 300	: 51.667 mm
Fatt. sicurezza freccia Istantanea	: 8.237	Fatt. sicurezza freccia Netta Finale	: 8.801
Fatt. sicurezza freccia Finale	: 10.268	Fatt. sicurezza	: 8.237

Campata 131-130 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.246 (fs=4.067)

Sforzo Normale di Progetto [daN]	: -5601 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -314
Momento Flettente Mz di Progetto [daNm]	: -3

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -1.94
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.168
fs	: 5.96
Tensione di Progetto relativa a My [N/mm ²]	: 2.73
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.05

Tensione Resistente relativa a M_y [N/mm ²]	: 12.7
Tensione Resistente relativa a M_z [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.218
f_s	: 4.59
Coefficiente di Sfruttamento a pressoflessione	: 0.246
f_s	: 4.07

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.07 ($f_s=14.245$)

Taglio T_y di Progetto [daN]	: -3
Taglio T_z di Progetto [daN]	: 228
Momento Torcente M_t di Progetto [daNm]	: -3

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.00
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.12
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.07
f_s	: 14.24

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 12.70 N/mm ²
Tensione fless. piano XY	: 0.05 N/mm ²	Tensione fless. piano XZ	: 2.73 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.004	Coefficiente sfrutt. nel piano XZ	: 0.215
Coeff. sfrutt. max euleriano	: 0.177		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.181	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.392
f_s	: 2.552		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 132-135 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.246 (fs=4.07)
 Sforzo Normale di Progetto [daN] : -5614 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -317
 Momento Flettente Mz di Progetto [daNm] : -1

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -1.95
 Tensione Resistente [N/mm²] : 11.59
 Coefficiente di Sfruttamento a compressione : 0.168
 fs : 5.94
 Tensione di Progetto relativa a My [N/mm²] : 2.75
 Tensione di Progetto relativa a Mz [N/mm²] : 0.01
 Tensione Resistente relativa a My [N/mm²] : 12.7
 Tensione Resistente relativa a Mz [N/mm²] : 12.74
 Coefficiente di Sfruttamento a flessione : 0.217
 fs : 4.6
 Coefficiente di Sfruttamento a pressoflessione : 0.246
 fs : 4.07

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**
Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.11 (fs=9.073)
 Taglio Ty di Progetto [daN] : 58
 Taglio Tz di Progetto [daN] : 250
 Momento Torcente Mt di Progetto [daNm] : -66

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.13
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.05
 fs : 19.82
 Tensione di Progetto [N/mm²] : 0.37
 Modulo di resistenza a torsione [mm³] : 886153.88
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.108
 fs : 9.29
 Coefficiente di Sfruttamento a taglio+torsione : 0.11
 fs : 9.07

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 12.70 N/mm ²
Tensione fless. piano XY	: 0.01 N/mm ²	Tensione fless. piano XZ	: 2.75 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.001	Coefficiente sfrutt. nel piano XZ	: 0.217
Coeff. sfrutt. max euleriano	: 0.178		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.179	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.394
fs	: 2.537		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 133-134 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.245 (fs=4.084)

Sforzo Normale di Progetto [daN]	: -5605 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -317
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -1.95
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.168
fs	: 5.95
Tensione di Progetto relativa a My [N/mm ²]	: 2.75
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.00
Tensione Resistente relativa a My [N/mm ²]	: 12.7
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.217
fs	: 4.62
Coefficiente di Sfruttamento a pressoflessione	: 0.245
fs	: 4.08

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.071 (fs=14.072)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: 231
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.12
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.071
fs	: 14.07

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 12.70 N/mm ²
Tensione fless. piano XY	: 0.00 N/mm ²	Tensione fless. piano XZ	: 2.75 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.216
Coeff. sfrutt. max euleriano	: 0.177		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.177	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.394
fs	: 2.540		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 135-134 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 15500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7750 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.394 (fs=2.539)

Sforzo Normale di Progetto [daN]	: -918 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 12167
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 202.02
Tensione di Progetto relativa a My [N/mm ²]	: 4.56
Tensione di Progetto relativa a Mz [N/mm ²]	: 0
Tensione Resistente relativa a My [N/mm ²]	: 11.59
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.394
fs	: 2.54
Coefficiente di Sfruttamento a pressoflessione	: 0.394
fs	: 2.54

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.681)

Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : 3173
 Momento Torcente Mt di Progetto [daNm] : -1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.3
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.176
 fs : 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15500.0	Lunghezza efficace nel piano XZ	: 15500.0
Momento Critico nel piano XY	: 188530 daNm	Momento Critico nel piano XZ	: 30165 daNm
Tensione Critica nel piano XY	: 441.87 N/mmq	Tensione Critica nel piano XZ	: 11.31 N/mmq
Resistenza fless. piano XY	: 12.74 N/mmq	Resistenza fless. piano XZ	: 11.59 N/mmq
Tensione fless. piano XY	: 0.00 N/mmq	Tensione fless. piano XZ	: 4.56 N/mmq
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.281
Coeff. sfrutt. max euleriano	: 0.071		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.071	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.352
fs	: 2.838		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.763 mm	Limite Freccia Istantanea L/500	: 31.000 mm
Freccia Netta Finale	: -5.032 mm	Limite Freccia Netta Fin. L/ 350	: 44.286 mm
Freccia Finale	: -5.032 mm	Limite Freccia Finale L/ 300	: 51.667 mm
Fatt. sicurezza freccia Istantanea	: 8.237	Fatt. sicurezza freccia Netta Finale	: 8.801
Fatt. sicurezza freccia Finale	: 10.268	Fatt. sicurezza	: 8.237

Campata 137-136 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 21 [SLD] [IN] " - Coeff. Sfruttamento : 0.251 (fs=3.987)

Sforzo Normale di Progetto [daN] : -9261 (COMPRESSIONE)

Momento Flettente My di Progetto [daNm] : -471
 Momento Flettente Mz di Progetto [daNm] : -24

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -3.22
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.177
 fs : 5.66
 Tensione di Progetto relativa a My [N/mm²] : 4.09
 Tensione di Progetto relativa a Mz [N/mm²] : 0.42
 Tensione Resistente relativa a My [N/mm²] : 19.95
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.22
 fs : 4.55
 Coefficiente di Sfruttamento a pressoflessione : 0.251
 fs : 3.99

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.11 (fs=9.119)

Taglio Ty di Progetto [daN] : 57
 Taglio Tz di Progetto [daN] : 243
 Momento Torcente Mt di Progetto [daNm] : -63

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.13
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.049
 fs : 20.41
 Tensione di Progetto [N/mm²] : 0.37
 Modulo di resistenza a torsione [mm³] : 886153.88
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.107
 fs : 9.32
 Coefficiente di Sfruttamento a taglio+torsione : 0.11
 fs : 9.12

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 12.70 N/mm ²
Tensione fless. piano XY	: 0.01 N/mm ²	Tensione fless. piano XZ	: 2.77 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.001	Coefficiente sfrutt. nel piano XZ	: 0.218
Coeff. sfrutt. max euleriano	: 0.179		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.180	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.397
fs	: 2.517		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1984.9 mm
 Comb. di carico più gravosa : 142

Schema adottato Doppio Incastro
 Peso proprio : -11.1 daN/m

Carico distribuito Istantaneo	: -12.1 daN/m	-	Carico distribuito Finale	: -12.1 daN/m
-			Comb 42 [CAR] [ST]	
Freccia Istantanea - COMBINAZIONE			Comb 2 [SLEQP] [PE]	
Freccia Finale - COMBINAZIONE			Modulo Elastico finale	: 6388.9 N/mm ²
Modulo Elastico istantaneo	: 11500.0 N/mm ²			
Controfreccia	: 0.000 mm			
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm	
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm	
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm	
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428	
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428	

Campata 136-138 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 15500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7750 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.393 ($f_s=2.548$)

Sforzo Normale di Progetto [daN]	: -949 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 12126
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.005
f_s	: 195.44
Tensione di Progetto relativa a My [N/mm ²]	: 4.55
Tensione di Progetto relativa a Mz [N/mm ²]	: 0
Tensione Resistente relativa a My [N/mm ²]	: 11.59
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.392
f_s	: 2.55
Coefficiente di Sfruttamento a pressoflessione	: 0.393
f_s	: 2.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 ($f_s=5.682$)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: 3172
Momento Torcente Mt di Progetto [daNm]	: -1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.3
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.176
f_s	: 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15500.0	Lunghezza efficace nel piano XZ	: 15500.0
Momento Critico nel piano XY	: 188530 daNm	Momento Critico nel piano XZ	: 30165 daNm

Tensione Critica nel piano XY	: 441.87 N/mm ²	Tensione Critica nel piano XZ	: 11.31 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 11.59 N/mm ²
Tensione fless. piano XY	: 0.00 N/mm ²	Tensione fless. piano XZ	: 4.55 N/mm ²
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.280
Coeff. sfrutt. max euleriano	: 0.073		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.073	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.354
fs	: 2.827		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.763 mm	Limite Freccia Istantanea L/500	: 31.000 mm
Freccia Netta Finale	: -5.032 mm	Limite Freccia Netta Fin. L/ 350	: 44.286 mm
Freccia Finale	: -5.032 mm	Limite Freccia Finale L/ 300	: 51.667 mm
Fatt. sicurezza freccia Istantanea	: 8.237	Fatt. sicurezza freccia Netta Finale	: 8.801
Fatt. sicurezza freccia Finale	: 10.268	Fatt. sicurezza	: 8.237

Campata 139-138 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.248 (fs=4.038)

Sforzo Normale di Progetto [daN]	: -9417 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -475
Momento Flettente Mz di Progetto [daNm]	: -14

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -3.27
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.18
fs	: 5.57
Tensione di Progetto relativa a My [N/mm ²]	: 4.13
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.25
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.215
fs	: 4.64
Coefficiente di Sfruttamento a pressoflessione	: 0.248
fs	: 4.04

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.071 (fs=13.989)

Taglio Ty di Progetto [daN]	: 0
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Taglio Tz di Progetto [daN] : 232
 Momento Torcente Mt di Progetto [daNm] : 1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.12
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.071
 fs : 13.99

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mmq	Tensione Critica nel piano XZ	: 190.09 N/mmq
Resistenza fless. piano XY	: 12.74 N/mmq	Resistenza fless. piano XZ	: 12.70 N/mmq
Tensione fless. piano XY	: 0.01 N/mmq	Tensione fless. piano XZ	: 2.77 N/mmq
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.001	Coefficiente sfrutt. nel piano XZ	: 0.218
Coeff. sfrutt. max euleriano	: 0.179		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.180	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.397
fs	: 2.518		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 140-141 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.28 (fs=3.566)

Sforzo Normale di Progetto [daN] : -10749 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -534
 Momento Flettente Mz di Progetto [daNm] : 10

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -3.73
 Tensione Resistente [N/mm²] : 18.21

Coefficiente di Sfruttamento a compressione	: 0.205
fs	: 4.88
Tensione di Progetto relativa a My [N/mm ²]	: 4.63
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.18
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.238
fs	: 4.19
Coefficiente di Sfruttamento a pressoflessione	: 0.28
fs	: 3.57

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.137)

Taglio Ty di Progetto [daN]	: 58
Taglio Tz di Progetto [daN]	: 191
Momento Torcente Mt di Progetto [daNm]	: -64

Tipo Verifica	: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.1
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.039
fs	: 25.55
Tensione di Progetto [N/mm ²]	: 0.37
Modulo di resistenza a torsione [mm ³]	: 886153.88
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.108
fs	: 9.27
Coefficiente di Sfruttamento a taglio+torsione	: 0.109
fs	: 9.14

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.18 N/mm ²	Tensione fless. piano XZ	: 4.63 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.009	Coefficiente sfrutt. nel piano XZ	: 0.232
Coeff. sfrutt. max euleriano	: 0.216		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.225	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.449
fs	: 2.229		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -12.1 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm ²
Controfreccia	: 0.000 mm

Schema adottato Doppio Incastro	
Peso proprio	: -11.1 daN/m
-	
Carico distribuito Finale	: -12.1 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [PE]	
Modulo Elastico finale	: 6388.9 N/mm ²

Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 141-142 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 15500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7750 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.392 (fs=2.552)

Sforzo Normale di Progetto [daN]	: -963 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 12106
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²]	: -0.06
Tensione Resistente [N/mm²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 192.43
Tensione di Progetto relativa a My [N/mm²]	: 4.54
Tensione di Progetto relativa a Mz [N/mm²]	: 0
Tensione Resistente relativa a My [N/mm²]	: 11.59
Tensione Resistente relativa a Mz [N/mm²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.392
fs	: 2.55
Coefficiente di Sfruttamento a pressoflessione	: 0.392
fs	: 2.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.682)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: 3172
Momento Torcente Mt di Progetto [daNm]	: -1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0
Tensione di Progetto relativa a Tz [N/mm²]	: 0.3
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.176
fs	: 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15500.0	Lunghezza efficace nel piano XZ	: 15500.0
Momento Critico nel piano XY	: 188530 daNm	Momento Critico nel piano XZ	: 30165 daNm
Tensione Critica nel piano XY	: 441.87 N/mmq	Tensione Critica nel piano XZ	: 11.31 N/mmq
Resistenza fless. piano XY	: 12.74 N/mmq	Resistenza fless. piano XZ	: 11.59 N/mmq
Tensione fless. piano XY	: 0.00 N/mmq	Tensione fless. piano XZ	: 4.54 N/mmq
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.280

Coeff. sfrutt. max euleriano	: 0.075	
Coeff. sfrutt. TOTALE (Piano XY)	: 0.075	Coeff. sfrutt. TOTALE (Piano XZ) : 0.354
fs	: 2.821	

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.763 mm	Limite Freccia Istantanea L/500	: 31.000 mm
Freccia Netta Finale	: -5.032 mm	Limite Freccia Netta Fin. L/ 350	: 44.286 mm
Freccia Finale	: -5.032 mm	Limite Freccia Finale L/ 300	: 51.667 mm
Fatt. sicurezza freccia Istantanea	: 8.237	Fatt. sicurezza freccia Netta Finale	: 8.801
Fatt. sicurezza freccia Finale	: 10.268	Fatt. sicurezza	: 8.237

Campata 143-142 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.28 (fs=3.565)

Sforzo Normale di Progetto [daN]	: -10480 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -524
Momento Flettente Mz di Progetto [daNm]	: -21

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -3.64
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.2
fs	: 5
Tensione di Progetto relativa a My [N/mm ²]	: 4.55
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.36
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.241
fs	: 4.16
Coefficiente di Sfruttamento a pressoflessione	: 0.28
fs	: 3.57

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.072 (fs=13.957)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: 232
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.12

Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.072
fs	: 13.96

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 10	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.36 N/mm ²	Tensione fless. piano XZ	: 4.55 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.018	Coefficiente sfrutt. nel piano XZ	: 0.228
Coeff. sfrutt. max euleriano	: 0.211		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.229	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.439
fs	: 2.278		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 144-145 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.329 (fs=3.036)

Sforzo Normale di Progetto [daN]	: -12299 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -608
Momento Flettente Mz di Progetto [daNm]	: 16

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -4.27
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.235
fs	: 4.26
Tensione di Progetto relativa a My [N/mm ²]	: 5.28
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.28
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03

Coefficiente di Sfruttamento a flessione	: 0.274
fs	: 3.65
Coefficiente di Sfruttamento a pressoflessione	: 0.329
fs	: 3.04

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - R 120x240	
Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.14)	
Taglio Ty di Progetto [daN]	: 56
Taglio Tz di Progetto [daN]	: 197
Momento Torcente Mt di Progetto [daNm]	: -65

Tipo Verifica		: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm²]	: 0.03	
Tensione di Progetto relativa a Tz [N/mm²]	: 0.1	
Tensione tang. Resistente [N/mm²]	: 2.66	
Coefficiente di Sfruttamento a taglio	: 0.04	
fs	: 24.87	
Tensione di Progetto [N/mm²]	: 0.37	
Modulo di resistenza a torsione [mm³]	: 886153.88	
Tensione tang. Resistente [N/mm²]	: 2.66	
Coefficiente di Sfruttamento a torsione	: 0.108	
fs	: 9.28	
Coefficiente di Sfruttamento a taglio+torsione	: 0.109	
fs	: 9.14	

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mmq	Tensione Critica nel piano XZ	: 190.09 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 19.95 N/mmq
Tensione fless. piano XY	: 0.28 N/mmq	Tensione fless. piano XZ	: 5.28 N/mmq
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.014	Coefficiente sfrutt. nel piano XZ	: 0.265
Coeff. sfrutt. max euleriano	: 0.247		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.261	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.512
fs	: 1.953		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 145-146 Cope[Trave]Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)L= 15500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7**VERIFICHE EFFETTUATE CON ESITO POSITIVO****VERIFICHE DI RESISTENZA NORMALE**Sezione più gravosa : 4 - [X=7750 mm / 15500 mm] - **R 160x1000***Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.392 (fs=2.553)*

Sforzo Normale di Progetto [daN] : -964 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 12102
 Momento Flettente Mz di Progetto [daNm] : 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -0.06
 Tensione Resistente [N/mm²] : 11.59
 Coefficiente di Sfruttamento a compressione : 0.005
 fs : 192.24
 Tensione di Progetto relativa a My [N/mm²] : 4.54
 Tensione di Progetto relativa a Mz [N/mm²] : 0
 Tensione Resistente relativa a My [N/mm²] : 11.59
 Tensione Resistente relativa a Mz [N/mm²] : 12.74
 Coefficiente di Sfruttamento a flessione : 0.392
 fs : 2.55
 Coefficiente di Sfruttamento a pressoflessione : 0.392
 fs : 2.55

VERIFICHE DI RESISTENZA TANGENZIALESezione più gravosa: 1 - [X=0 mm / 15500 mm] - **R 160x1000***Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.681)*

Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : 3172
 Momento Torcente Mt di Progetto [daNm] : 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.3
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.176
 fs : 5.68

VERIFICA A SVERGOLAMENTO*Tratto più sollecitato: 1 (0 - 6)*

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15500.0	Lunghezza efficace nel piano XZ	: 15500.0
Momento Critico nel piano XY	: 188530 daNm	Momento Critico nel piano XZ	: 30165 daNm
Tensione Critica nel piano XY	: 441.87 N/mm ²	Tensione Critica nel piano XZ	: 11.31 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 11.59 N/mm ²
Tensione fless. piano XY	: 0.00 N/mm ²	Tensione fless. piano XZ	: 4.54 N/mm ²
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.280
Coeff. sfrutt. max euleriano	: 0.075		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.075	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.354
fs	: 2.822		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.763 mm	Limite Freccia Istantanea L/500	: 31.000 mm
Freccia Netta Finale	: -5.032 mm	Limite Freccia Netta Fin. L/ 350	: 44.286 mm
Freccia Finale	: -5.032 mm	Limite Freccia Finale L/ 300	: 51.667 mm
Fatt. sicurezza freccia Istantanea	: 8.237	Fatt. sicurezza freccia Netta Finale	: 8.801
Fatt. sicurezza freccia Finale	: 10.268	Fatt. sicurezza	: 8.237

Campata 147-146 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.313 (fs=3.195)

Sforzo Normale di Progetto [daN]	: -11532 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -580
Momento Flettente Mz di Progetto [daNm]	: 20

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -4
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.22
fs	: 4.55
Tensione di Progetto relativa a My [N/mm ²]	: 5.04
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.35
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.265
fs	: 3.78
Coefficiente di Sfruttamento a pressoflessione	: 0.313
fs	: 3.2

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.077 (fs=13.063)

Taglio Ty di Progetto [daN]	: 27
Taglio Tz di Progetto [daN]	: 389
Momento Torcente Mt di Progetto [daNm]	: 20

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.2
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.077
fs	: 13.06

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.35 N/mm ²	Tensione fless. piano XZ	: 5.04 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.017	Coefficiente sfrutt. nel piano XZ	: 0.252
Coeff. sfrutt. max euleriano	: 0.232		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.249	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.484
fs	: 2.064		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 148-149 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.359 (fs=2.789)

Sforzo Normale di Progetto [daN]	: -12786 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -646
Momento Flettente Mz di Progetto [daNm]	: 29

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -4.44
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.244
fs	: 4.1
Tensione di Progetto relativa a My [N/mm ²]	: 5.61
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.51
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.299
fs	: 3.34
Coefficiente di Sfruttamento a pressoflessione	: 0.359
fs	: 2.79

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.11 (fs=9.072)

Taglio Ty di Progetto [daN] : 59
 Taglio Tz di Progetto [daN] : 198
 Momento Torcente Mt di Progetto [daNm] : -65

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.1
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.041
 fs : 24.68
 Tensione di Progetto [N/mm²] : 0.37
 Modulo di resistenza a torsione [mm³] : 886153.88
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.109
 fs : 9.21
 Coefficiente di Sfruttamento a taglio+torsione : 0.11
 fs : 9.07

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mmq	Tensione Critica nel piano XZ	: 190.09 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 19.95 N/mmq
Tensione fless. piano XY	: 0.51 N/mmq	Tensione fless. piano XZ	: 5.61 N/mmq
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.026	Coefficiente sfrutt. nel piano XZ	: 0.281
Coeff. sfrutt. max euleriano	: 0.257		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.283	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.538
fs	: 1.857		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 149-150 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 15503.9 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7751.95 mm / 15503.9 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.392 (fs=2.551)

Sforzo Normale di Progetto [daN] : -964 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : 12109
Momento Flettente Mz di Progetto [daNm] : 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -0.06
Tensione Resistente [N/mm²] : 11.59
Coefficiente di Sfruttamento a compressione : 0.005
fs : 192.39
Tensione di Progetto relativa a My [N/mm²] : 4.54
Tensione di Progetto relativa a Mz [N/mm²] : 0
Tensione Resistente relativa a My [N/mm²] : 11.59
Tensione Resistente relativa a Mz [N/mm²] : 12.74
Coefficiente di Sfruttamento a flessione : 0.392
fs : 2.55
Coefficiente di Sfruttamento a pressoflessione : 0.392
fs : 2.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 15503.9 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.68)

Taglio Ty di Progetto [daN] : 0
Taglio Tz di Progetto [daN] : 3173
Momento Torcente Mt di Progetto [daNm] : 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
Tensione di Progetto relativa a Tz [N/mm²] : 0.3
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a taglio : 0.176
fs : 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15503.9	Lunghezza efficace nel piano XZ	: 15503.9
Momento Critico nel piano XY	: 188483 daNm	Momento Critico nel piano XZ	: 30157 daNm
Tensione Critica nel piano XY	: 441.76 N/mm ²	Tensione Critica nel piano XZ	: 11.31 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 11.59 N/mm ²
Tensione fless. piano XY	: 0.00 N/mm ²	Tensione fless. piano XZ	: 4.54 N/mm ²
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.280
Coeff. sfrutt. max euleriano	: 0.075		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.075	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.355
fs	: 2.820		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15503.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m

Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.767 mm	Limite Freccia Istantanea L/500	: 31.008 mm
Freccia Netta Finale	: -5.037 mm	Limite Freccia Netta Fin. L/ 350	: 44.297 mm
Freccia Finale	: -5.037 mm	Limite Freccia Finale L/ 300	: 51.680 mm
Fatt. sicurezza freccia Istantanea	: 8.231	Fatt. sicurezza freccia Netta Finale	: 8.795
Fatt. sicurezza freccia Finale	: 10.260	Fatt. sicurezza	: 8.231

Campata 151-150 Cope[Trave]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.328 (fs=3.049)

Sforzo Normale di Progetto [daN]	: -12497 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -623
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -4.34
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.238
fs	: 4.2
Tensione di Progetto relativa a My [N/mm ²]	: 5.4
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.01
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.271
fs	: 3.69
Coefficiente di Sfruttamento a pressoflessione	: 0.328
fs	: 3.05

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.081 (fs=12.291)

Taglio Ty di Progetto [daN]	: 14
Taglio Tz di Progetto [daN]	: 415
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.22
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.081
fs	: 12.29

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²

Tensione fless. piano XY	: 0.01 N/mm ²	Tensione fless. piano XZ	: 5.40 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.271
Coeff. sfrutt. max euleriano	: 0.251		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.252	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.522
fs	: 1.914		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 152-153 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.372 (fs=2.69)

Sforzo Normale di Progetto [daN]	: -13405 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -666
Momento Flettente Mz di Progetto [daNm]	: 27

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -4.65
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.256
fs	: 3.91
Tensione di Progetto relativa a My [N/mm ²]	: 5.78
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.48
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.306
fs	: 3.26
Coefficiente di Sfruttamento a pressoflessione	: 0.372
fs	: 2.69

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.165)

Taglio Ty di Progetto [daN]	: 59
Taglio Tz di Progetto [daN]	: 211
Momento Torcente Mt di Progetto [daNm]	: -57

Tipo Verifica		: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]		: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]		: 0.11
Tensione tang. Resistente [N/mm ²]		: 2.66
Coefficiente di Sfruttamento a taglio		: 0.043
fs		: 23.3
Tensione di Progetto [N/mm ²]		: 0.37
Modulo di resistenza a torsione [mm ³]		: 886153.88
Tensione tang. Resistente [N/mm ²]		: 2.66
Coefficiente di Sfruttamento a torsione		: 0.107
fs		: 9.32
Coefficiente di Sfruttamento a taglio+torsione		: 0.109
fs		: 9.16

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.48 N/mm ²	Tensione fless. piano XZ	: 5.78 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.024	Coefficiente sfrutt. nel piano XZ	: 0.290
Coeff. sfrutt. max euleriano	: 0.270		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.294	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.559
fs	: 1.788		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 153-154 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 15507.31 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7753.65 mm / 15507.31 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.392 (fs=2.549)

Sforzo Normale di Progetto [daN]	: -959 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 12120

Momento Flettente Mz di Progetto [daNm] : 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 193.21
Tensione di Progetto relativa a My [N/mm ²]	: 4.55
Tensione di Progetto relativa a Mz [N/mm ²]	: 0
Tensione Resistente relativa a My [N/mm ²]	: 11.59
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.392
fs	: 2.55
Coefficiente di Sfruttamento a pressoflessione	: 0.392
fs	: 2.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=15507.31 mm / 15507.31 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.68)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: -3173
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.3
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.176
fs	: 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15507.3	Lunghezza efficace nel piano XZ	: 15507.3
Momento Critico nel piano XY	: 188441 daNm	Momento Critico nel piano XZ	: 30151 daNm
Tensione Critica nel piano XY	: 441.66 N/mm ²	Tensione Critica nel piano XZ	: 11.31 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 11.59 N/mm ²
Tensione fless. piano XY	: 0.00 N/mm ²	Tensione fless. piano XZ	: 4.55 N/mm ²
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.280
Coeff. sfrutt. max euleriano	: 0.074		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.074	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.355
fs	: 2.821		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15507.3 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -322.3 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm ²
Controfreccia	: 0.000 mm
Freccia Istantanea	: -3.770 mm
Freccia Netta Finale	: -5.041 mm

Schema adottato Doppio Incastro	
Peso proprio	: -61.6 daN/m
-	
Carico distribuito Finale	: -223.6 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [PE]	
Modulo Elastico finale	: 6388.9 N/mm ²
Limite Freccia Istantanea L/500	: 31.015 mm
Limite Freccia Netta Fin. L/350	: 44.307 mm

Freccia Finale	: -5.041 mm	Limite Freccia Finale L/ 300	: 51.691 mm
Fatt. sicurezza freccia Istantanea	: 8.226	Fatt. sicurezza freccia Netta Finale	: 8.789
Fatt. sicurezza freccia Finale	: 10.254	Fatt. sicurezza	: 8.226

Campata 155-154 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.364 (fs=2.749)

Sforzo Normale di Progetto [daN]	: -13317 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -659
Momento Flettente Mz di Progetto [daNm]	: 21

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -4.62
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.254
fs	: 3.94
Tensione di Progetto relativa a My [N/mm²]	: 5.72
Tensione di Progetto relativa a Mz [N/mm²]	: 0.36
Tensione Resistente relativa a My [N/mm²]	: 19.95
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.299
fs	: 3.34
Coefficiente di Sfruttamento a pressoflessione	: 0.364
fs	: 2.75

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.086 (fs=11.653)

Taglio Ty di Progetto [daN]	: 27
Taglio Tz di Progetto [daN]	: 437
Momento Torcente Mt di Progetto [daNm]	: 21

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm²]	: 0.23
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.086
fs	: 11.65

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 6	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mmq	Tensione Critica nel piano XZ	: 190.09 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 19.95 N/mmq
Tensione fless. piano XY	: 0.36 N/mmq	Tensione fless. piano XZ	: 5.72 N/mmq
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.018	Coefficiente sfrutt. nel piano XZ	: 0.287
Coeff. sfrutt. max euleriano	: 0.268		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.286	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.555

fs : 1.803

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 156-157 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.376 (fs=2.663)

Sforzo Normale di Progetto [daN]	: -13574 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -685
Momento Flettente Mz di Progetto [daNm]	: 18

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -4.71
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.259
fs	: 3.86
Tensione di Progetto relativa a My [N/mm ²]	: 5.94
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.31
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.309
fs	: 3.24
Coefficiente di Sfruttamento a pressoflessione	: 0.376
fs	: 2.66

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.137)

Taglio Ty di Progetto [daN]	: 63
Taglio Tz di Progetto [daN]	: 223
Momento Torcente Mt di Progetto [daNm]	: -64

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.12
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.045

fs	: 22.02
Tensione di Progetto [N/mm ²]	: 0.37
Modulo di resistenza a torsione [mm ³]	: 886153.88
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.107
fs	: 9.31
Coefficiente di Sfruttamento a taglio+torsione	: 0.109
fs	: 9.14

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.31 N/mm ²	Tensione fless. piano XZ	: 5.94 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.015	Coefficiente sfrutt. nel piano XZ	: 0.298
Coeff. sfrutt. max euleriano	: 0.273		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.288	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.571
fs	: 1.751		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 157-158 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 15508.78 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7754.39 mm / 15508.78 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.392 (fs=2.548)

Sforzo Normale di Progetto [daN]	: -960 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 12125
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.005

fs	: 193.17
Tensione di Progetto relativa a My [N/mm ²]	: 4.55
Tensione di Progetto relativa a Mz [N/mm ²]	: 0
Tensione Resistente relativa a My [N/mm ²]	: 11.59
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.392
fs	: 2.55
Coefficiente di Sfruttamento a pressoflessione	: 0.392
fs	: 2.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=15508.78 mm / 15508.78 mm] - **R 160x1000**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.679)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: -3173
Momento Torcente Mt di Progetto [daNm]	: -1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.3
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.176
fs	: 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15508.8	Lunghezza efficace nel piano XZ	: 15508.8
Momento Critico nel piano XY	: 188423 daNm	Momento Critico nel piano XZ	: 30148 daNm
Tensione Critica nel piano XY	: 441.62 N/mm ²	Tensione Critica nel piano XZ	: 11.31 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 11.59 N/mm ²
Tensione fless. piano XY	: 0.00 N/mm ²	Tensione fless. piano XZ	: 4.55 N/mm ²
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.280
Coeff. sfrutt. max euleriano	: 0.074		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.074	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.355
fs	: 2.820		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15508.8 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.772 mm	Limite Freccia Istantanea L/500	: 31.018 mm
Freccia Netta Finale	: -5.043 mm	Limite Freccia Netta Fin. L/ 350	: 44.311 mm
Freccia Finale	: -5.043 mm	Limite Freccia Finale L/ 300	: 51.696 mm
Fatt. sicurezza freccia Istantanea	: 8.224	Fatt. sicurezza freccia Netta Finale	: 8.786
Fatt. sicurezza freccia Finale	: 10.251	Fatt. sicurezza	: 8.224

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $-\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.365 (fs=2.738)

Sforzo Normale di Progetto [daN] : -13790 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : -677
Momento Flettente Mz di Progetto [daNm] : -2

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -4.79
Tensione Resistente [N/mm²] : 18.21
Coefficiente di Sfruttamento a compressione : 0.263
fs : 3.8
Tensione di Progetto relativa a My [N/mm²] : 5.88
Tensione di Progetto relativa a Mz [N/mm²] : 0.04
Tensione Resistente relativa a My [N/mm²] : 19.95
Tensione Resistente relativa a Mz [N/mm²] : 20.03
Coefficiente di Sfruttamento a flessione : 0.296
fs : 3.38
Coefficiente di Sfruttamento a pressoflessione : 0.365
fs : 2.74

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.087 (fs=11.467)

Taglio Ty di Progetto [daN] : 10
Taglio Tz di Progetto [daN] : 444
Momento Torcente Mt di Progetto [daNm] : -2

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.01
Tensione di Progetto relativa a Tz [N/mm²] : 0.23
Tensione tang. Resistente [N/mm²] : 2.66
Coefficiente di Sfruttamento a taglio : 0.087
fs : 11.47

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 10	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.04 N/mm ²	Tensione fless. piano XZ	: 5.88 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.002	Coefficiente sfrutt. nel piano XZ	: 0.295
Coeff. sfrutt. max euleriano	: 0.277		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.279	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.572
fs	: 1.748		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)
· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 160-161 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.38 (fs=2.629)

Sforzo Normale di Progetto [daN]	: -13657 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -674
Momento Flettente Mz di Progetto [daNm]	: 32

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -4.74
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.26
fs	: 3.84
Tensione di Progetto relativa a My [N/mm ²]	: 5.85
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.55
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.313
fs	: 3.2
Coefficiente di Sfruttamento a pressoflessione	: 0.38
fs	: 2.63

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 50 [SLV] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.164)

Taglio Ty di Progetto [daN]	: 63
Taglio Tz di Progetto [daN]	: 226
Momento Torcente Mt di Progetto [daNm]	: -60

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.12
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.046
fs	: 21.74
Tensione di Progetto [N/mm ²]	: 0.37
Modulo di resistenza a torsione [mm ³]	: 886153.88
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.107
fs	: 9.35

Coefficiente di Sfruttamento a taglio+torsione : 0.109
fs : 9.16

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 17	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.55 N/mm ²	Tensione fless. piano XZ	: 5.85 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.028	Coefficiente sfrutt. nel piano XZ	: 0.293
Coeff. sfrutt. max euleriano	: 0.275		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.302	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.568
fs	: 1.760		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 161-162 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 15510.72 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7755.36 mm / 15510.72 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.393 (fs=2.548)

Sforzo Normale di Progetto [daN]	: -960 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 12127
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 193.16
Tensione di Progetto relativa a My [N/mm ²]	: 4.55
Tensione di Progetto relativa a Mz [N/mm ²]	: 0
Tensione Resistente relativa a My [N/mm ²]	: 11.59
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.393

fs	: 2.55
Coefficiente di Sfruttamento a pressoflessione	: 0.393
fs	: 2.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 15510.72 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.678)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: 3174
Momento Torcente Mt di Progetto [daNm]	: 1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0
Tensione di Progetto relativa a Tz [N/mm²]	: 0.3
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.176
fs	: 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15510.7	Lunghezza efficace nel piano XZ	: 15510.7
Momento Critico nel piano XY	: 188400 daNm	Momento Critico nel piano XZ	: 30144 daNm
Tensione Critica nel piano XY	: 441.56 N/mm²	Tensione Critica nel piano XZ	: 11.30 N/mm²
Resistenza fless. piano XY	: 12.74 N/mm²	Resistenza fless. piano XZ	: 11.59 N/mm²
Tensione fless. piano XY	: 0.00 N/mm²	Tensione fless. piano XZ	: 4.55 N/mm²
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.280
Coeff. sfrutt. max euleriano	: 0.074		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.074	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.355
fs	: 2.819		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15510.7 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.774 mm	Limite Freccia Istantanea L/500	: 31.021 mm
Freccia Netta Finale	: -5.046 mm	Limite Freccia Netta Fin. L/ 350	: 44.316 mm
Freccia Finale	: -5.046 mm	Limite Freccia Finale L/ 300	: 51.702 mm
Fatt. sicurezza freccia Istantanea	: 8.221	Fatt. sicurezza freccia Netta Finale	: 8.783
Fatt. sicurezza freccia Finale	: 10.247	Fatt. sicurezza	: 8.221

Campata 163-162 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $-\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**
Comb. più gravosa : " Comb 10 [SLD] [IN] " - Coeff. Sfruttamento : 0.371 (fs=2.697)
 Sforzo Normale di Progetto [daN] : -13838 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -689
 Momento Flettente Mz di Progetto [daNm] : 3

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1
 Tensione di Progetto [N/mm²] : -4.8
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.264
 fs : 3.79
 Tensione di Progetto relativa a My [N/mm²] : 5.98
 Tensione di Progetto relativa a Mz [N/mm²] : 0.05
 Tensione Resistente relativa a My [N/mm²] : 19.95
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.301
 fs : 3.32
 Coefficiente di Sfruttamento a pressoflessione : 0.371
 fs : 2.7

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**
Comb. più gravosa : " Comb 6 [SLD] [IN] " - Coeff. Sfruttamento : 0.09 (fs=11.13)
 Taglio Ty di Progetto [daN] : 15
 Taglio Tz di Progetto [daN] : 458
 Momento Torcente Mt di Progetto [daNm] : 24

Tipo Verifica : TAGLIO
 Tensione di Progetto relativa a Ty [N/mm²] : 0.01
 Tensione di Progetto relativa a Tz [N/mm²] : 0.24
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.09
 fs : 11.13

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 10	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.05 N/mm ²	Tensione fless. piano XZ	: 5.98 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.002	Coefficiente sfrutt. nel piano XZ	: 0.300
Coeff. sfrutt. max euleriano	: 0.278		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.281	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.578
fs	: 1.730		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	

Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 164-165 Cope[Trave]

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.388 (fs=2.581)

Sforzo Normale di Progetto [daN]	: -13694 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -685
Momento Flettente Mz di Progetto [daNm]	: 35

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -4.75
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.261
fs	: 3.83
Tensione di Progetto relativa a My [N/mm ²]	: 5.95
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.61
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.319
fs	: 3.13
Coefficiente di Sfruttamento a pressoflessione	: 0.388
fs	: 2.58

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.144)

Taglio Ty di Progetto [daN]	: -59
Taglio Tz di Progetto [daN]	: 267
Momento Torcente Mt di Progetto [daNm]	: 69

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.14
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.054
fs	: 18.64
Tensione di Progetto [N/mm ²]	: 0.37
Modulo di resistenza a torsione [mm ³]	: 886153.88
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.106
fs	: 9.39
Coefficiente di Sfruttamento a taglio+torsione	: 0.109
fs	: 9.14

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 17
 Lunghezza efficace nel piano XY : 1984.9
 Momento Critico nel piano XY : 43797 daNm
 Tensione Critica nel piano XY : 760.36 N/mm²
 Resistenza fless. piano XY : 20.03 N/mm²
 Tensione fless. piano XY : 0.61 N/mm²
 Snellezza relativa nel piano XY : 0.18
 Coeff. Riduttivo nel piano XY : 1.000
 Coefficiente sfrutt. nel piano XY : 0.030
 Coeff. sfrutt. max euleriano : 0.276
 Coeff. sfrutt. TOTALE (Piano XY) : 0.306
 fs : 1.743

Sezione più sfavorevole : 1
 Lunghezza efficace nel piano XZ : 1984.9
 Momento Critico nel piano XZ : 21898 daNm
 Tensione Critica nel piano XZ : 190.09 N/mm²
 Resistenza fless. piano XZ : 19.95 N/mm²
 Tensione fless. piano XZ : 5.95 N/mm²
 Snellezza relativa nel piano XZ : 0.36
 Coeff. Riduttivo nel piano XZ : 1.000
 Coefficiente sfrutt. nel piano XZ : 0.298
 Coeff. sfrutt. TOTALE (Piano XZ) : 0.574

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1984.9 mm
 Comb. di carico più gravosa : 142
 Carico distribuito Istantaneo : -12.1 daN/m
 -
 Freccia Istantanea - COMBINAZIONE
 Freccia Finale - COMBINAZIONE
 Modulo Elastico istantaneo : 11500.0 N/mm²
 Controfreccia : 0.000 mm
 Freccia Istantanea : -0.006 mm
 Freccia Netta Finale : -0.011 mm
 Freccia Finale : -0.011 mm
 Fatt. sicurezza freccia Istantanea : 673.380
 Fatt. sicurezza freccia Finale : 623.500

Schema adottato Doppio Incastro
 Peso proprio : -11.1 daN/m
 -
 Carico distribuito Finale : -12.1 daN/m
 Comb 42 [CAR] [ST]
 Comb 2 [SLEQP] [PE]
 Modulo Elastico finale : 6388.9 N/mm²
 Limite Freccia Istantanea L/500 : 3.970 mm
 Limite Freccia Netta Fin. L/350 : 5.671 mm
 Limite Freccia Finale L/300 : 6.616 mm
 Fatt. sicurezza freccia Netta Finale : 534.428
 Fatt. sicurezza : 534.428

Campata 165-166 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 15512.86 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7756.43 mm / 15512.86 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.393 (fs=2.547)

Sforzo Normale di Progetto [daN] : -960 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 12130
 Momento Flettente Mz di Progetto [daNm] : 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -0.06
 Tensione Resistente [N/mm²] : 11.59
 Coefficiente di Sfruttamento a compressione : 0.005
 fs : 193.15
 Tensione di Progetto relativa a My [N/mm²] : 4.55
 Tensione di Progetto relativa a Mz [N/mm²] : 0
 Tensione Resistente relativa a My [N/mm²] : 11.59
 Tensione Resistente relativa a Mz [N/mm²] : 12.74
 Coefficiente di Sfruttamento a flessione : 0.393
 fs : 2.55
 Coefficiente di Sfruttamento a pressoflessione : 0.393
 fs : 2.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 15512.86 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.678)

Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : 3174
 Momento Torcente Mt di Progetto [daNm] : 1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.3
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.176
 fs : 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15512.9	Lunghezza efficace nel piano XZ	: 15512.9
Momento Critico nel piano XY	: 188374 daNm	Momento Critico nel piano XZ	: 30140 daNm
Tensione Critica nel piano XY	: 441.50 N/mmq	Tensione Critica nel piano XZ	: 11.30 N/mmq
Resistenza fless. piano XY	: 12.74 N/mmq	Resistenza fless. piano XZ	: 11.59 N/mmq
Tensione fless. piano XY	: 0.00 N/mmq	Tensione fless. piano XZ	: 4.55 N/mmq
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.280
Coeff. sfrutt. max euleriano	: 0.074		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.074	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.355
fs	: 2.818		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15512.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.776 mm	Limite Freccia Istantanea L/500	: 31.026 mm
Freccia Netta Finale	: -5.048 mm	Limite Freccia Netta Fin. L/ 350	: 44.322 mm
Freccia Finale	: -5.048 mm	Limite Freccia Finale L/ 300	: 51.710 mm
Fatt. sicurezza freccia Istantanea	: 8.218	Fatt. sicurezza freccia Netta Finale	: 8.779
Fatt. sicurezza freccia Finale	: 10.243	Fatt. sicurezza	: 8.218

Campata 167-166 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.371 (fs=2.698)

Sforzo Normale di Progetto [daN] : -13423 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -668
 Momento Flettente Mz di Progetto [daNm] : 24

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -4.66
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.256
fs	: 3.91
Tensione di Progetto relativa a My [N/mm ²]	: 5.8
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.42
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.305
fs	: 3.28
Coefficiente di Sfruttamento a pressoflessione	: 0.371
fs	: 2.7

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.088 (fs=11.398)

Taglio Ty di Progetto [daN]	: 14
Taglio Tz di Progetto [daN]	: 447
Momento Torcente Mt di Progetto [daNm]	: 1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.23
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.088
fs	: 11.4

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.01 N/mm ²	Tensione fless. piano XZ	: 5.88 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.001	Coefficiente sfrutt. nel piano XZ	: 0.295
Coeff. sfrutt. max euleriano	: 0.278		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.278	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.572
fs	: 1.747		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.429

Fatt. sicurezza freccia Finale : 623.500

Fatt. sicurezza : 534.429

Campata 168-169 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.387 (fs=2.583)

Sforzo Normale di Progetto [daN] : -13746 (COMPRESSIONE)

Momento Flettente My di Progetto [daNm] : -687

Momento Flettente Mz di Progetto [daNm] : 32

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -4.77

Tensione Resistente [N/mm²] : 18.21

Coefficiente di Sfruttamento a compressione : 0.262

fs : 3.81

Tensione di Progetto relativa a My [N/mm²] : 5.96

Tensione di Progetto relativa a Mz [N/mm²] : 0.56

Tensione Resistente relativa a My [N/mm²] : 19.95

Tensione Resistente relativa a Mz [N/mm²] : 20.03

Coefficiente di Sfruttamento a flessione : 0.318

fs : 3.14

Coefficiente di Sfruttamento a pressoflessione : 0.387

fs : 2.58

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.209)

Taglio Ty di Progetto [daN] : -58

Taglio Tz di Progetto [daN] : 272

Momento Torcente Mt di Progetto [daNm] : 65

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.03

Tensione di Progetto relativa a Tz [N/mm²] : 0.14

Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a taglio : 0.055

fs : 18.33

Tensione di Progetto [N/mm²] : 0.36

Modulo di resistenza a torsione [mm³] : 886153.88

Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a torsione : 0.106

fs : 9.47

Coefficiente di Sfruttamento a taglio+torsione : 0.109

fs : 9.21

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 14

Lunghezza efficace nel piano XY : 1984.9

Momento Critico nel piano XY : 43797 daNm

Tensione Critica nel piano XY : 760.36 N/mmq

Resistenza fless. piano XY : 20.03 N/mmq

Tensione fless. piano XY : 0.34 N/mmq

Sezione più sfavorevole : 1

Lunghezza efficace nel piano XZ : 1984.9

Momento Critico nel piano XZ : 21898 daNm

Tensione Critica nel piano XZ : 190.09 N/mmq

Resistenza fless. piano XZ : 19.95 N/mmq

Tensione fless. piano XZ : 5.98 N/mmq

Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.017	Coefficiente sfrutt. nel piano XZ	: 0.300
Coeff. sfrutt. max euleriano	: 0.278		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.295	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.577
fs	: 1.732		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 169-170 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 15515.2 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7757.6 mm / 15515.2 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.393 (fs=2.546)

Sforzo Normale di Progetto [daN]	: -959 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 12134
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 193.28
Tensione di Progetto relativa a My [N/mm ²]	: 4.55
Tensione di Progetto relativa a Mz [N/mm ²]	: 0
Tensione Resistente relativa a My [N/mm ²]	: 11.59
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.393
fs	: 2.55
Coefficiente di Sfruttamento a pressoflessione	: 0.393
fs	: 2.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 15515.2 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.677)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: 3175
Momento Torcente Mt di Progetto [daNm]	: 1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.3
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.176
fs	: 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15515.2	Lunghezza efficace nel piano XZ	: 15515.2
Momento Critico nel piano XY	: 188345 daNm	Momento Critico nel piano XZ	: 30135 daNm
Tensione Critica nel piano XY	: 441.43 N/mm ²	Tensione Critica nel piano XZ	: 11.30 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 11.59 N/mm ²
Tensione fless. piano XY	: 0.00 N/mm ²	Tensione fless. piano XZ	: 4.55 N/mm ²
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.281
Coeff. sfrutt. max euleriano	: 0.074		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.074	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.355
fs	: 2.818		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15515.2 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.778 mm	Limite Freccia Istantanea L/500	: 31.030 mm
Freccia Netta Finale	: -5.052 mm	Limite Freccia Netta Fin. L/ 350	: 44.329 mm
Freccia Finale	: -5.052 mm	Limite Freccia Finale L/ 300	: 51.717 mm
Fatt. sicurezza freccia Istantanea	: 8.214	Fatt. sicurezza freccia Netta Finale	: 8.775
Fatt. sicurezza freccia Finale	: 10.238	Fatt. sicurezza	: 8.214

Campata 171-170 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.377 (fs=2.655)

Sforzo Normale di Progetto [daN]	: -13534 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -675
Momento Flettente Mz di Progetto [daNm]	: 27

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -4.7
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.258
fs	: 3.87
Tensione di Progetto relativa a My [N/mm ²]	: 5.86

Tensione di Progetto relativa a M_z [N/mm ²]	: 0.48
Tensione Resistente relativa a M_y [N/mm ²]	: 19.95
Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.31
f_s	: 3.22
Coefficiente di Sfruttamento a pressoflessione	: 0.377
f_s	: 2.65

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.09 ($f_s=11.156$)

Taglio T_y di Progetto [daN]	: 18
Taglio T_z di Progetto [daN]	: 457
Momento Torcente M_t di Progetto [daNm]	: 8

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a T_y [N/mm ²]	: 0.01
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.24
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.09
f_s	: 11.16

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.14 N/mm ²	Tensione fless. piano XZ	: 5.99 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.007	Coefficiente sfrutt. nel piano XZ	: 0.300
Coeff. sfrutt. max euleriano	: 0.278		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.285	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.578
f_s	: 1.729		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale ($t \rightarrow \infty$)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.429
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.429

Campata 172-173 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**
Comb. più gravosa : " Comb 17 [SLD] [IN] " - Coeff. Sfruttamento : 0.371 (fs=2.697)
 Sforzo Normale di Progetto [daN] : -13355 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -658
 Momento Flettente Mz di Progetto [daNm] : 32

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -4.64
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.255
 fs : 3.93
 Tensione di Progetto relativa a My [N/mm²] : 5.71
 Tensione di Progetto relativa a Mz [N/mm²] : 0.56
 Tensione Resistente relativa a My [N/mm²] : 19.95
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.306
 fs : 3.27
 Coefficiente di Sfruttamento a pressoflessione : 0.371
 fs : 2.7

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**
Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.205)
 Taglio Ty di Progetto [daN] : -57
 Taglio Tz di Progetto [daN] : 259
 Momento Torcente Mt di Progetto [daNm] : 63

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.13
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.052
 fs : 19.22
 Tensione di Progetto [N/mm²] : 0.37
 Modulo di resistenza a torsione [mm³] : 886153.88
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.106
 fs : 9.44
 Coefficiente di Sfruttamento a taglio+torsione : 0.109
 fs : 9.21

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole : 14
 Lunghezza efficace nel piano XY : 1984.9
 Momento Critico nel piano XY : 43797 daNm
 Tensione Critica nel piano XY : 760.36 N/mm²
 Resistenza fless. piano XY : 20.03 N/mm²
 Tensione fless. piano XY : 0.35 N/mm²
 Snellezza relativa nel piano XY : 0.18
 Coeff. Riduttivo nel piano XY : 1.000
 Coefficiente sfrutt. nel piano XY : 0.018
 Coeff. sfrutt. max euleriano : 0.273
 Coeff. sfrutt. TOTALE (Piano XY) : 0.290
 fs : 1.777

Sezione più sfavorevole : 1
 Lunghezza efficace nel piano XZ : 1984.9
 Momento Critico nel piano XZ : 21898 daNm
 Tensione Critica nel piano XZ : 190.09 N/mm²
 Resistenza fless. piano XZ : 19.95 N/mm²
 Tensione fless. piano XZ : 5.79 N/mm²
 Snellezza relativa nel piano XZ : 0.36
 Coeff. Riduttivo nel piano XZ : 1.000
 Coefficiente sfrutt. nel piano XZ : 0.290
 Coeff. sfrutt. TOTALE (Piano XZ) : 0.563

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 173-175 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 15517.29 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7758.65 mm / 15517.29 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.393 (fs=2.545)

Sforzo Normale di Progetto [daN]	: -957 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 12139
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 193.76
Tensione di Progetto relativa a My [N/mm ²]	: 4.55
Tensione di Progetto relativa a Mz [N/mm ²]	: 0
Tensione Resistente relativa a My [N/mm ²]	: 11.59
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.393
fs	: 2.55
Coefficiente di Sfruttamento a pressoflessione	: 0.393
fs	: 2.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=15517.29 mm / 15517.29 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.676)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: -3175
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.3
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.176
fs	: 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15517.3	Lunghezza efficace nel piano XZ	: 15517.3
Momento Critico nel piano XY	: 188320 daNm	Momento Critico nel piano XZ	: 30131 daNm
Tensione Critica nel piano XY	: 441.38 N/mm ²	Tensione Critica nel piano XZ	: 11.30 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 11.59 N/mm ²
Tensione fless. piano XY	: 0.00 N/mm ²	Tensione fless. piano XZ	: 4.55 N/mm ²
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.281
Coeff. sfrutt. max euleriano	: 0.074		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.074	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.355
fs	: 2.818		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15517.3 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.780 mm	Limite Freccia Istantanea L/500	: 31.035 mm
Freccia Netta Finale	: -5.054 mm	Limite Freccia Netta Fin. L/ 350	: 44.335 mm
Freccia Finale	: -5.054 mm	Limite Freccia Finale L/ 300	: 51.724 mm
Fatt. sicurezza freccia Istantanea	: 8.211	Fatt. sicurezza freccia Netta Finale	: 8.772
Fatt. sicurezza freccia Finale	: 10.234	Fatt. sicurezza	: 8.211

Campata 174-175 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.375 (fs=2.667)

Sforzo Normale di Progetto [daN]	: -13711 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -683
Momento Flettente Mz di Progetto [daNm]	: -16

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -4.76
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.261
fs	: 3.82
Tensione di Progetto relativa a My [N/mm ²]	: 5.93
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.28
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.307
fs	: 3.26
Coefficiente di Sfruttamento a pressoflessione	: 0.375

fs

: 2.67

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.089 (fs=11.262)

Taglio Ty di Progetto [daN] : 12
 Taglio Tz di Progetto [daN] : 453
 Momento Torcente Mt di Progetto [daNm] : -16

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.01
 Tensione di Progetto relativa a Tz [N/mm²] : 0.24
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.089
 fs : 11.26

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mmq	Tensione Critica nel piano XZ	: 190.09 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 19.95 N/mmq
Tensione fless. piano XY	: 0.28 N/mmq	Tensione fless. piano XZ	: 5.93 N/mmq
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.014	Coefficiente sfrutt. nel piano XZ	: 0.297
Coeff. sfrutt. max euleriano	: 0.276		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.290	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.573
fs	: 1.746		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 176-177 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.356 (fs=2.809)

Sforzo Normale di Progetto [daN] : -13018 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -642
 Momento Flettente Mz di Progetto [daNm] : 25

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -4.52
 Tensione Resistente [N/mm²] : 18.21
 Coefficiente di Sfruttamento a compressione : 0.248
 fs : 4.03
 Tensione di Progetto relativa a My [N/mm²] : 5.57
 Tensione di Progetto relativa a Mz [N/mm²] : 0.43
 Tensione Resistente relativa a My [N/mm²] : 19.95
 Tensione Resistente relativa a Mz [N/mm²] : 20.03
 Coefficiente di Sfruttamento a flessione : 0.294
 fs : 3.4
 Coefficiente di Sfruttamento a pressoflessione : 0.356
 fs : 2.81

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.11 (fs=9.127)

Taglio Ty di Progetto [daN] : -59
 Taglio Tz di Progetto [daN] : 281
 Momento Torcente Mt di Progetto [daNm] : 63

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
 Tensione di Progetto relativa a Tz [N/mm²] : 0.15
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.056
 fs : 17.74
 Tensione di Progetto [N/mm²] : 0.37
 Modulo di resistenza a torsione [mm³] : 886153.88
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a torsione : 0.106
 fs : 9.4
 Coefficiente di Sfruttamento a taglio+torsione : 0.11
 fs : 9.13

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 14	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.43 N/mm ²	Tensione fless. piano XZ	: 5.57 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.022	Coefficiente sfrutt. nel piano XZ	: 0.279
Coeff. sfrutt. max euleriano	: 0.262		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.284	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.541
fs	: 1.848		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1984.9 mm

Schema adottato Doppio Incastro

Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 177-178 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)
L= 15519.98 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7759.99 mm / 15519.98 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.393 ($f_s=2.545$)

Sforzo Normale di Progetto [daN]	: -959 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 12137
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.005
f_s	: 193.31
Tensione di Progetto relativa a My [N/mm ²]	: 4.55
Tensione di Progetto relativa a Mz [N/mm ²]	: 0
Tensione Resistente relativa a My [N/mm ²]	: 11.59
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.393
f_s	: 2.55
Coefficiente di Sfruttamento a pressoflessione	: 0.393
f_s	: 2.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=15519.98 mm / 15519.98 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 ($f_s=5.675$)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: -3176
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.3
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.176
f_s	: 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 51	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15520.0	Lunghezza efficace nel piano XZ	: 15520.0

Momento Critico nel piano XY	: 188287 daNm	Momento Critico nel piano XZ	: 30126 daNm
Tensione Critica nel piano XY	: 441.30 N/mm ²	Tensione Critica nel piano XZ	: 11.30 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 18.21 N/mm ²
Tensione fless. piano XY	: 0.32 N/mm ²	Tensione fless. piano XZ	: 4.06 N/mm ²
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.016	Coefficiente sfrutt. nel piano XZ	: 0.159
Coeff. sfrutt. max euleriano	: 0.336		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.352	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.496
fs	: 2.017		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15520.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.782 mm	Limite Freccia Istantanea L/500	: 31.040 mm
Freccia Netta Finale	: -5.058 mm	Limite Freccia Netta Fin. L/ 350	: 44.343 mm
Freccia Finale	: -5.058 mm	Limite Freccia Finale L/ 300	: 51.733 mm
Fatt. sicurezza freccia Istantanea	: 8.207	Fatt. sicurezza freccia Netta Finale	: 8.767
Fatt. sicurezza freccia Finale	: 10.229	Fatt. sicurezza	: 8.207

Campata 179-178 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.367 (fs=2.724)

Sforzo Normale di Progetto [daN]	: -13550 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -679
Momento Flettente Mz di Progetto [daNm]	: 8

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -4.7
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.258
fs	: 3.87
Tensione di Progetto relativa a My [N/mm ²]	: 5.89
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.14
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.3
fs	: 3.33
Coefficiente di Sfruttamento a pressoflessione	: 0.367
fs	: 2.72

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.088 (fs=11.353)

Taglio Ty di Progetto [daN] : 4
 Taglio Tz di Progetto [daN] : 449
 Momento Torcente Mt di Progetto [daNm] : 8

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0.00
 Tensione di Progetto relativa a Tz [N/mm²] : 0.23
 Tensione tang. Resistente [N/mm²] : 2.66
 Coefficiente di Sfruttamento a taglio : 0.088
 fs : 11.35

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.14 N/mm ²	Tensione fless. piano XZ	: 5.89 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.007	Coefficiente sfrutt. nel piano XZ	: 0.295
Coeff. sfrutt. max euleriano	: 0.273		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.280	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.568
fs	: 1.761		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.429
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.429

Campata 180-181 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.347 (fs=2.883)

Sforzo Normale di Progetto [daN] : -12533 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -634
 Momento Flettente Mz di Progetto [daNm] : 23

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²] : -4.35

Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.239
fs	: 4.18
Tensione di Progetto relativa a My [N/mm ²]	: 5.5
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.4
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.29
fs	: 3.45
Coefficiente di Sfruttamento a pressoflessione	: 0.347
fs	: 2.88

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.111 (fs=8.987)

Taglio Ty di Progetto [daN]	: -63
Taglio Tz di Progetto [daN]	: 255
Momento Torcente Mt di Progetto [daNm]	: 63

Tipo Verifica	: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.13
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.051
fs	: 19.43
Tensione di Progetto [N/mm ²]	: 0.37
Modulo di resistenza a torsione [mm ³]	: 886153.88
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.109
fs	: 9.21
Coefficiente di Sfruttamento a taglio+torsione	: 0.111
fs	: 8.99

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 14	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.40 N/mm ²	Tensione fless. piano XZ	: 5.50 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.020	Coefficiente sfrutt. nel piano XZ	: 0.276
Coeff. sfrutt. max euleriano	: 0.252		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.272	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.528
fs	: 1.894		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm
Comb. di carico più gravosa	: 142
Carico distribuito Istantaneo	: -12.1 daN/m
-	
Freccia Istantanea - COMBINAZIONE	
Freccia Finale - COMBINAZIONE	
Modulo Elastico istantaneo	: 11500.0 N/mm ²

Schema adottato Doppio Incastro	
Peso proprio	: -11.1 daN/m
-	
Carico distribuito Finale	: -12.1 daN/m
Comb 42 [CAR] [ST]	
Comb 2 [SLEQP] [PE]	
Modulo Elastico finale	: 6388.9 N/mm ²

Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 181-182 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 15500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7750 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.392 (fs=2.549)

Sforzo Normale di Progetto [daN]	: -959 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 12122
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²]	: -0.06
Tensione Resistente [N/mm²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 193.36
Tensione di Progetto relativa a My [N/mm²]	: 4.55
Tensione di Progetto relativa a Mz [N/mm²]	: 0
Tensione Resistente relativa a My [N/mm²]	: 11.59
Tensione Resistente relativa a Mz [N/mm²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.392
fs	: 2.55
Coefficiente di Sfruttamento a pressoflessione	: 0.392
fs	: 2.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=15500 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.681)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: -3173
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0
Tensione di Progetto relativa a Tz [N/mm²]	: 0.3
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.176
fs	: 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 39	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15500.0	Lunghezza efficace nel piano XZ	: 15500.0
Momento Critico nel piano XY	: 188530 daNm	Momento Critico nel piano XZ	: 30165 daNm
Tensione Critica nel piano XY	: 441.87 N/mmq	Tensione Critica nel piano XZ	: 11.31 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 18.21 N/mmq
Tensione fless. piano XY	: 0.32 N/mmq	Tensione fless. piano XZ	: 3.99 N/mmq
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400

Coefficiente sfrutt. nel piano XY	: 0.016	Coefficiente sfrutt. nel piano XZ	: 0.157
Coeff. sfrutt. max euleriano	: 0.315		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.331	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.472
fs	: 2.121		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.763 mm	Limite Freccia Istantanea L/500	: 31.000 mm
Freccia Netta Finale	: -5.032 mm	Limite Freccia Netta Fin. L/ 350	: 44.286 mm
Freccia Finale	: -5.032 mm	Limite Freccia Finale L/ 300	: 51.667 mm
Fatt. sicurezza freccia Istantanea	: 8.237	Fatt. sicurezza freccia Netta Finale	: 8.801
Fatt. sicurezza freccia Finale	: 10.268	Fatt. sicurezza	: 8.237

Campata 183-182 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.34 (fs=2.941)

Sforzo Normale di Progetto [daN]	: -13032 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -633
Momento Flettente Mz di Progetto [daNm]	: 5

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -4.53
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.249
fs	: 4.02
Tensione di Progetto relativa a My [N/mm ²]	: 5.49
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.09
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.278
fs	: 3.59
Coefficiente di Sfruttamento a pressoflessione	: 0.34
fs	: 2.94

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 13 [SLD] [IN] " - Coeff. Sfruttamento : 0.082 (fs=12.172)

Taglio Ty di Progetto [daN]	: -12
Taglio Tz di Progetto [daN]	: 419
Momento Torcente Mt di Progetto [daNm]	: 5

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
---	--------

Tensione di Progetto relativa a T_z [N/mm ²]	: 0.22
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.082
f_s	: 12.17

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 13	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.09 N/mm ²	Tensione fless. piano XZ	: 5.49 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.004	Coefficiente sfrutt. nel piano XZ	: 0.275
Coeff. sfrutt. max euleriano	: 0.262		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.267	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.537
f_s	: 1.861		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 184-185 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.328 ($f_s=3.046$)

Sforzo Normale di Progetto [daN]	: -11902 (COMPRESSIONE)
Momento Flettente M_y di Progetto [daNm]	: -606
Momento Flettente M_z di Progetto [daNm]	: 22

Tipo Verifica : COMPRESSIONE+FLESSIONE - $K_{mod} = 1.1$

Tensione di Progetto [N/mm ²]	: -4.13
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.227
f_s	: 4.41
Tensione di Progetto relativa a M_y [N/mm ²]	: 5.26
Tensione di Progetto relativa a M_z [N/mm ²]	: 0.38
Tensione Resistente relativa a M_y [N/mm ²]	: 19.95

Tensione Resistente relativa a M_z [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.277
f_s	: 3.61
Coefficiente di Sfruttamento a pressoflessione	: 0.328
f_s	: 3.05

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.111 ($f_s=8.997$)

Taglio T_y di Progetto [daN]	: -60
Taglio T_z di Progetto [daN]	: 234
Momento Torcente M_t di Progetto [daNm]	: 64

Tipo Verifica		: TAGLIO+TORSIONE
Tensione di Progetto relativa a T_y [N/mm ²]	: 0.03	
Tensione di Progetto relativa a T_z [N/mm ²]	: 0.12	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a taglio	: 0.047	
f_s	: 21.14	
Tensione di Progetto [N/mm ²]	: 0.38	
Modulo di resistenza a torsione [mm ³]	: 886153.88	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a torsione	: 0.109	
f_s	: 9.18	
Coefficiente di Sfruttamento a taglio+torsione	: 0.111	
f_s	: 9	

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 14	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.38 N/mm ²	Tensione fless. piano XZ	: 5.26 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.019	Coefficiente sfrutt. nel piano XZ	: 0.263
Coeff. sfrutt. max euleriano	: 0.240		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.258	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.503
f_s	: 1.988		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 185-186 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 15500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7750 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.392 (fs=2.55)

Sforzo Normale di Progetto [daN]	: -958 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 12116
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²]	: -0.06
Tensione Resistente [N/mm²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 193.59
Tensione di Progetto relativa a My [N/mm²]	: 4.54
Tensione di Progetto relativa a Mz [N/mm²]	: 0
Tensione Resistente relativa a My [N/mm²]	: 11.59
Tensione Resistente relativa a Mz [N/mm²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.392
fs	: 2.55
Coefficiente di Sfruttamento a pressoflessione	: 0.392
fs	: 2.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=15500 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.682)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: -3172
Momento Torcente Mt di Progetto [daNm]	: 1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0
Tensione di Progetto relativa a Tz [N/mm²]	: 0.3
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.176
fs	: 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15500.0	Lunghezza efficace nel piano XZ	: 15500.0
Momento Critico nel piano XY	: 188530 daNm	Momento Critico nel piano XZ	: 30165 daNm
Tensione Critica nel piano XY	: 441.87 N/mmq	Tensione Critica nel piano XZ	: 11.31 N/mmq
Resistenza fless. piano XY	: 12.74 N/mmq	Resistenza fless. piano XZ	: 11.59 N/mmq
Tensione fless. piano XY	: 0.00 N/mmq	Tensione fless. piano XZ	: 4.54 N/mmq
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.280
Coeff. sfrutt. max euleriano	: 0.074		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.074	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.354
fs	: 2.823		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.763 mm	Limite Freccia Istantanea L/500	: 31.000 mm
Freccia Netta Finale	: -5.032 mm	Limite Freccia Netta Fin. L/ 350	: 44.286 mm
Freccia Finale	: -5.032 mm	Limite Freccia Finale L/ 300	: 51.667 mm
Fatt. sicurezza freccia Istantanea	: 8.237	Fatt. sicurezza freccia Netta Finale	: 8.801
Fatt. sicurezza freccia Finale	: 10.268	Fatt. sicurezza	: 8.237

Campata 187-186 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.346 (fs=2.891)

Sforzo Normale di Progetto [daN]	: -12645 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -629
Momento Flettente Mz di Progetto [daNm]	: 23

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -4.39
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.241
fs	: 4.15
Tensione di Progetto relativa a My [N/mm ²]	: 5.46
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.4
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.288
fs	: 3.48
Coefficiente di Sfruttamento a pressoflessione	: 0.346
fs	: 2.89

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.082 (fs=12.166)

Taglio Ty di Progetto [daN]	: -7
Taglio Tz di Progetto [daN]	: 419
Momento Torcente Mt di Progetto [daNm]	: 23

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.00
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.22
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.082
fs	: 12.17

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 9	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.40 N/mm ²	Tensione fless. piano XZ	: 5.46 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.020	Coefficiente sfrutt. nel piano XZ	: 0.274
Coeff. sfrutt. max euleriano	: 0.254		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.275	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.528
fs	: 1.894		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 188-189 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.308 (fs=3.251)

Sforzo Normale di Progetto [daN]	: -11363 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -566
Momento Flettente Mz di Progetto [daNm]	: 23

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -3.95
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.217
fs	: 4.61
Tensione di Progetto relativa a My [N/mm ²]	: 4.92
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.41
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.261
fs	: 3.84
Coefficiente di Sfruttamento a pressoflessione	: 0.308
fs	: 3.25

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - R 120x240	
Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.11 (fs=9.106)	
Taglio Ty di Progetto [daN]	: -59
Taglio Tz di Progetto [daN]	: 204
Momento Torcente Mt di Progetto [daNm]	: 62
Tipo Verifica : TAGLIO+TORSIONE	
Tensione di Progetto relativa a Ty [N/mm²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm²]	: 0.11
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.042
fs	: 23.99
Tensione di Progetto [N/mm²]	: 0.37
Modulo di resistenza a torsione [mm³]	: 886153.88
Tensione tang. Resistente [N/mm²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.108
fs	: 9.25
Coefficiente di Sfruttamento a taglio+torsione	: 0.11
fs	: 9.11

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 14	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm²	Tensione Critica nel piano XZ	: 190.09 N/mm²
Resistenza fless. piano XY	: 20.03 N/mm²	Resistenza fless. piano XZ	: 19.95 N/mm²
Tensione fless. piano XY	: 0.41 N/mm²	Tensione fless. piano XZ	: 4.92 N/mm²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.020	Coefficiente sfrutt. nel piano XZ	: 0.246
Coeff. sfrutt. max euleriano	: 0.229		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.249	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.475
fs	: 2.105		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 189-190 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 15500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7750 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.392 (fs=2.55)

Sforzo Normale di Progetto [daN] : -960 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : 12115
 Momento Flettente Mz di Progetto [daNm] : 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -0.06
 Tensione Resistente [N/mm²] : 11.59
 Coefficiente di Sfruttamento a compressione : 0.005
 fs : 193.12
 Tensione di Progetto relativa a My [N/mm²] : 4.54
 Tensione di Progetto relativa a Mz [N/mm²] : 0
 Tensione Resistente relativa a My [N/mm²] : 11.59
 Tensione Resistente relativa a Mz [N/mm²] : 12.74
 Coefficiente di Sfruttamento a flessione : 0.392
 fs : 2.55
 Coefficiente di Sfruttamento a pressoflessione : 0.392
 fs : 2.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.681)

Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : 3172
 Momento Torcente Mt di Progetto [daNm] : -1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.3
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.176
 fs : 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15500.0	Lunghezza efficace nel piano XZ	: 15500.0
Momento Critico nel piano XY	: 188530 daNm	Momento Critico nel piano XZ	: 30165 daNm
Tensione Critica nel piano XY	: 441.87 N/mm ²	Tensione Critica nel piano XZ	: 11.31 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 11.59 N/mm ²
Tensione fless. piano XY	: 0.00 N/mm ²	Tensione fless. piano XZ	: 4.54 N/mm ²
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.280
Coeff. sfrutt. max euleriano	: 0.074		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.074	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.354
fs	: 2.822		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	

-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.763 mm	Limite Freccia Istantanea L/500	: 31.000 mm
Freccia Netta Finale	: -5.032 mm	Limite Freccia Netta Fin. L/ 350	: 44.286 mm
Freccia Finale	: -5.032 mm	Limite Freccia Finale L/ 300	: 51.667 mm
Fatt. sicurezza freccia Istantanea	: 8.237	Fatt. sicurezza freccia Netta Finale	: 8.801
Fatt. sicurezza freccia Finale	: 10.268	Fatt. sicurezza	: 8.237

Campata 191-190 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.299 (fs=3.344)

Sforzo Normale di Progetto [daN]	: -11604 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -571
Momento Flettente Mz di Progetto [daNm]	: -3

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -4.03
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.221
fs	: 4.52
Tensione di Progetto relativa a My [N/mm ²]	: 4.96
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.05
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.25
fs	: 4
Coefficiente di Sfruttamento a pressoflessione	: 0.299
fs	: 3.34

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.072 (fs=13.982)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: 232
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.12
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.072
fs	: 13.98

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 9	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²

Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.05 N/mm ²	Tensione fless. piano XZ	: 4.96 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.002	Coefficiente sfrutt. nel piano XZ	: 0.248
Coeff. sfrutt. max euleriano	: 0.233		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.236	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.482
fs	: 2.075		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 192-193 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 14 [SLD] [IN] " - Coeff. Sfruttamento : 0.258 (fs=3.881)

Sforzo Normale di Progetto [daN]	: -9980 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -474
Momento Flettente Mz di Progetto [daNm]	: 25

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm ²]	: -3.47
Tensione Resistente [N/mm ²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.19
fs	: 5.25
Tensione di Progetto relativa a My [N/mm ²]	: 4.11
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.44
Tensione Resistente relativa a My [N/mm ²]	: 19.95
Tensione Resistente relativa a Mz [N/mm ²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.221
fs	: 4.52
Coefficiente di Sfruttamento a pressoflessione	: 0.258
fs	: 3.88

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.157)

Taglio Ty di Progetto [daN]	: -59
Taglio Tz di Progetto [daN]	: 141

Momento Torcente Mt di Progetto [daNm]	: 62	
Tipo Verifica		: TAGLIO+TORSIONE
Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03	
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.07	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a taglio	: 0.03	
fs	: 33.35	
Tensione di Progetto [N/mm ²]	: 0.37	
Modulo di resistenza a torsione [mm ³]	: 886153.88	
Tensione tang. Resistente [N/mm ²]	: 2.66	
Coefficiente di Sfruttamento a torsione	: 0.108	
fs	: 9.23	
Coefficiente di Sfruttamento a taglio+torsione	: 0.109	
fs	: 9.16	

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 14	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 20.03 N/mm ²	Resistenza fless. piano XZ	: 19.95 N/mm ²
Tensione fless. piano XY	: 0.44 N/mm ²	Tensione fless. piano XZ	: 4.11 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.022	Coefficiente sfrutt. nel piano XZ	: 0.206
Coeff. sfrutt. max euleriano	: 0.201		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.223	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.407
fs	: 2.458		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 193-195 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 15500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7750 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.393 (fs=2.547)

Sforzo Normale di Progetto [daN] : -947 (COMPRESSIONE)

Momento Flettente My di Progetto [daNm] : 12130
 Momento Flettente Mz di Progetto [daNm] : 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -0.06
 Tensione Resistente [N/mm²] : 11.59
 Coefficiente di Sfruttamento a compressione : 0.005
 fs : 195.76
 Tensione di Progetto relativa a My [N/mm²] : 4.55
 Tensione di Progetto relativa a Mz [N/mm²] : 0
 Tensione Resistente relativa a My [N/mm²] : 11.59
 Tensione Resistente relativa a Mz [N/mm²] : 12.74
 Coefficiente di Sfruttamento a flessione : 0.393
 fs : 2.55
 Coefficiente di Sfruttamento a pressoflessione : 0.393
 fs : 2.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.68)

Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : 3173
 Momento Torcente Mt di Progetto [daNm] : -1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.3
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.176
 fs : 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15500.0	Lunghezza efficace nel piano XZ	: 15500.0
Momento Critico nel piano XY	: 188530 daNm	Momento Critico nel piano XZ	: 30165 daNm
Tensione Critica nel piano XY	: 441.87 N/mm ²	Tensione Critica nel piano XZ	: 11.31 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 11.59 N/mm ²
Tensione fless. piano XY	: 0.00 N/mm ²	Tensione fless. piano XZ	: 4.55 N/mm ²
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.280
Coeff. sfrutt. max euleriano	: 0.073		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.073	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.354
fs	: 2.827		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 15500.0 mm
 Comb. di carico più gravosa : 142
 Carico distribuito Istantaneo : -322.3 daN/m
 -
 Freccia Istantanea - COMBINAZIONE
 Freccia Finale - COMBINAZIONE
 Modulo Elastico istantaneo : 11500.0 N/mm²
 Controfreccia : 0.000 mm
 Freccia Istantanea : -3.763 mm

Schema adottato Doppio Incastro
 Peso proprio : -61.6 daN/m
 -
 Carico distribuito Finale : -223.6 daN/m
 Comb 42 [CAR] [ST]
 Comb 2 [SLEQP] [PE]
 Modulo Elastico finale : 6388.9 N/mm²
 Limite Freccia Istantanea L/500 : 31.000 mm

Freccia Netta Finale	: -5.032 mm	Limite Freccia Netta Fin. L/ 350	: 44.286 mm
Freccia Finale	: -5.032 mm	Limite Freccia Finale L/ 300	: 51.667 mm
Fatt. sicurezza freccia Istantanea	: 8.237	Fatt. sicurezza freccia Netta Finale	: 8.801
Fatt. sicurezza freccia Finale	: 10.268	Fatt. sicurezza	: 8.237

Campata 194-195 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 9 [SLD] [IN] " - Coeff. Sfruttamento : 0.265 (fs=3.776)

Sforzo Normale di Progetto [daN]	: -9830 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -495
Momento Flettente Mz di Progetto [daNm]	: 23

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 1.1

Tensione di Progetto [N/mm²]	: -3.41
Tensione Resistente [N/mm²]	: 18.21
Coefficiente di Sfruttamento a compressione	: 0.187
fs	: 5.33
Tensione di Progetto relativa a My [N/mm²]	: 4.3
Tensione di Progetto relativa a Mz [N/mm²]	: 0.41
Tensione Resistente relativa a My [N/mm²]	: 19.95
Tensione Resistente relativa a Mz [N/mm²]	: 20.03
Coefficiente di Sfruttamento a flessione	: 0.23
fs	: 4.35
Coefficiente di Sfruttamento a pressoflessione	: 0.265
fs	: 3.78

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.071 (fs=13.999)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: 232
Momento Torcente Mt di Progetto [daNm]	: -1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0
Tensione di Progetto relativa a Tz [N/mm²]	: 0.12
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.071
fs	: 14

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 9	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mmq	Tensione Critica nel piano XZ	: 190.09 N/mmq
Resistenza fless. piano XY	: 20.03 N/mmq	Resistenza fless. piano XZ	: 19.95 N/mmq
Tensione fless. piano XY	: 0.41 N/mmq	Tensione fless. piano XZ	: 4.30 N/mmq
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.020	Coefficiente sfrutt. nel piano XZ	: 0.215
Coeff. sfrutt. max euleriano	: 0.198		

Coeff. sfrutt. TOTALE (Piano XY) : 0.218
fs : 2.420

Coeff. sfrutt. TOTALE (Piano XZ) : 0.413

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento : 1984.9 mm
Comb. di carico più gravosa : 142
Carico distribuito Istantaneo : -12.1 daN/m

Schema adottato Doppio Incastro
Peso proprio : -11.1 daN/m

-
Freccia Istantanea - COMBINAZIONE
Freccia Finale - COMBINAZIONE
Modulo Elastico istantaneo : 11500.0 N/mm²

Carico distribuito Finale : -12.1 daN/m
Comb 42 [CAR] [ST]
Comb 2 [SLEQP] [PE]
Modulo Elastico finale : 6388.9 N/mm²

Controfreccia : 0.000 mm
Freccia Istantanea : -0.006 mm
Freccia Netta Finale : -0.011 mm
Freccia Finale : -0.011 mm
Fatt. sicurezza freccia Istantanea : 673.380
Fatt. sicurezza freccia Finale : 623.500

Limite Freccia Istantanea L/500 : 3.970 mm
Limite Freccia Netta Fin. L/350 : 5.671 mm
Limite Freccia Finale L/300 : 6.616 mm
Fatt. sicurezza freccia Netta Finale : 534.428
Fatt. sicurezza : 534.428

Campata 196-197 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.246 (fs=4.064)

Sforzo Normale di Progetto [daN] : -5621 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : -317
Momento Flettente Mz di Progetto [daNm] : 1

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -1.95
Tensione Resistente [N/mm²] : 11.59
Coefficiente di Sfruttamento a compressione : 0.168
fs : 5.94
Tensione di Progetto relativa a My [N/mm²] : 2.75
Tensione di Progetto relativa a Mz [N/mm²] : 0.01
Tensione Resistente relativa a My [N/mm²] : 12.7
Tensione Resistente relativa a Mz [N/mm²] : 12.74
Coefficiente di Sfruttamento a flessione : 0.218
fs : 4.59
Coefficiente di Sfruttamento a pressoflessione : 0.246
fs : 4.06

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 42 [SLV] [IN] " - Coeff. Sfruttamento : 0.109 (fs=9.184)

Taglio Ty di Progetto [daN] : 61
Taglio Tz di Progetto [daN] : 231
Momento Torcente Mt di Progetto [daNm] : -64

Tipo Verifica : TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm²] : 0.03
Tensione di Progetto relativa a Tz [N/mm²] : 0.12
Tensione tang. Resistente [N/mm²] : 2.66

Coefficiente di Sfruttamento a taglio	: 0.047
fs	: 21.36
Tensione di Progetto [N/mm ²]	: 0.37
Modulo di resistenza a torsione [mm ³]	: 886153.88
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.107
fs	: 9.37
Coefficiente di Sfruttamento a taglio+torsione	: 0.109
fs	: 9.18

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 12.70 N/mm ²
Tensione fless. piano XY	: 0.01 N/mm ²	Tensione fless. piano XZ	: 2.75 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.001	Coefficiente sfrutt. nel piano XZ	: 0.217
Coeff. sfrutt. max euleriano	: 0.178		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.179	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.395
fs	: 2.534		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 197-199 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 15500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7750 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.394 (fs=2.539)

Sforzo Normale di Progetto [daN]	: -917 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 12168
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 11.59

Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 202.22
Tensione di Progetto relativa a My [N/mm ²]	: 4.56
Tensione di Progetto relativa a Mz [N/mm ²]	: 0
Tensione Resistente relativa a My [N/mm ²]	: 11.59
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.394
fs	: 2.54
Coefficiente di Sfruttamento a pressoflessione	: 0.394
fs	: 2.54

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.68)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: 3173
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.3
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.176
fs	: 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15500.0	Lunghezza efficace nel piano XZ	: 15500.0
Momento Critico nel piano XY	: 188530 daNm	Momento Critico nel piano XZ	: 30165 daNm
Tensione Critica nel piano XY	: 441.87 N/mm ²	Tensione Critica nel piano XZ	: 11.31 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 11.59 N/mm ²
Tensione fless. piano XY	: 0.00 N/mm ²	Tensione fless. piano XZ	: 4.56 N/mm ²
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.281
Coeff. sfrutt. max euleriano	: 0.071		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.071	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.352
fs	: 2.839		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.763 mm	Limite Freccia Istantanea L/500	: 31.000 mm
Freccia Netta Finale	: -5.032 mm	Limite Freccia Netta Fin. L/ 350	: 44.286 mm
Freccia Finale	: -5.032 mm	Limite Freccia Finale L/ 300	: 51.667 mm
Fatt. sicurezza freccia Istantanea	: 8.237	Fatt. sicurezza freccia Netta Finale	: 8.801
Fatt. sicurezza freccia Finale	: 10.268	Fatt. sicurezza	: 8.237

Classe di Servizio 2 (*Umidità relativa max: 85%*) LAMELLARE **GL24h** (*Tipo Omogeneo*) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.245 (fs=4.08)

Sforzo Normale di Progetto [daN] : -5594 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm] : -316
Momento Flettente Mz di Progetto [daNm] : -1

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm²] : -1.94
Tensione Resistente [N/mm²] : 11.59
Coefficiente di Sfruttamento a compressione : 0.168
fs : 5.97
Tensione di Progetto relativa a My [N/mm²] : 2.74
Tensione di Progetto relativa a Mz [N/mm²] : 0.02
Tensione Resistente relativa a My [N/mm²] : 12.7
Tensione Resistente relativa a Mz [N/mm²] : 12.74
Coefficiente di Sfruttamento a flessione : 0.217
fs : 4.61
Coefficiente di Sfruttamento a pressoflessione : 0.245
fs : 4.08

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.071 (fs=14.104)

Taglio Ty di Progetto [daN] : 0
Taglio Tz di Progetto [daN] : 230
Momento Torcente Mt di Progetto [daNm] : -1

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
Tensione di Progetto relativa a Tz [N/mm²] : 0.12
Tensione tang. Resistente [N/mm²] : 1.69
Coefficiente di Sfruttamento a taglio : 0.071
fs : 14.1

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 12.70 N/mm ²
Tensione fless. piano XY	: 0.02 N/mm ²	Tensione fless. piano XZ	: 2.74 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.001	Coefficiente sfrutt. nel piano XZ	: 0.216
Coeff. sfrutt. max euleriano	: 0.177		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.178	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.393
fs	: 2.545		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto			
Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 200-201 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.245 (fs=4.076)

Sforzo Normale di Progetto [daN]	: -5603 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -315
Momento Flettente Mz di Progetto [daNm]	: -2

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -1.95
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.168
fs	: 5.96
Tensione di Progetto relativa a My [N/mm ²]	: 2.73
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.04
Tensione Resistente relativa a My [N/mm ²]	: 12.7
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.217
fs	: 4.61
Coefficiente di Sfruttamento a pressoflessione	: 0.245
fs	: 4.08

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.11 (fs=9.117)

Taglio Ty di Progetto [daN]	: -61
Taglio Tz di Progetto [daN]	: 115
Momento Torcente Mt di Progetto [daNm]	: 61

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.03
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.06
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.026
fs	: 39.21
Tensione di Progetto [N/mm ²]	: 0.38
Modulo di resistenza a torsione [mm ³]	: 886153.88
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.109

fs	: 9.17
Coefficiente di Sfruttamento a taglio+torsione	: 0.11
fs	: 9.12

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 12.70 N/mm ²
Tensione fless. piano XY	: 0.04 N/mm ²	Tensione fless. piano XZ	: 2.73 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.003	Coefficiente sfrutt. nel piano XZ	: 0.215
Coeff. sfrutt. max euleriano	: 0.177		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.180	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.392
fs	: 2.550		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 201-202 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 15500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7750 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.392 (fs=2.554)

Sforzo Normale di Progetto [daN]	: -982 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 12093
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.06
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.005
fs	: 188.74
Tensione di Progetto relativa a My [N/mm ²]	: 4.54
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.00
Tensione Resistente relativa a My [N/mm ²]	: 11.59
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74

TABULATI DI CALCOLO -

Coefficiente di Sfruttamento a flessione	: 0.391
fs	: 2.55
Coefficiente di Sfruttamento a pressoflessione	: 0.392
fs	: 2.55

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.176 (fs=5.682)

Taglio Ty di Progetto [daN]	: 0
Taglio Tz di Progetto [daN]	: 3172
Momento Torcente Mt di Progetto [daNm]	: 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²]	: 0
Tensione di Progetto relativa a Tz [N/mm²]	: 0.3
Tensione tang. Resistente [N/mm²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.176
fs	: 5.68

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15500.0	Lunghezza efficace nel piano XZ	: 15500.0
Momento Critico nel piano XY	: 188530 daNm	Momento Critico nel piano XZ	: 30165 daNm
Tensione Critica nel piano XY	: 441.87 N/mm²	Tensione Critica nel piano XZ	: 11.31 N/mm²
Resistenza fless. piano XY	: 12.74 N/mm²	Resistenza fless. piano XZ	: 11.59 N/mm²
Tensione fless. piano XY	: 0.00 N/mm²	Tensione fless. piano XZ	: 4.54 N/mm²
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.280
Coeff. sfrutt. max euleriano	: 0.076		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.076	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.356
fs	: 2.812		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -322.3 daN/m	-	
-		Carico distribuito Finale	: -223.6 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm²	Modulo Elastico finale	: 6388.9 N/mm²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.763 mm	Limite Freccia Istantanea L/500	: 31.000 mm
Freccia Netta Finale	: -5.032 mm	Limite Freccia Netta Fin. L/ 350	: 44.286 mm
Freccia Finale	: -5.032 mm	Limite Freccia Finale L/ 300	: 51.667 mm
Fatt. sicurezza freccia Istantanea	: 8.237	Fatt. sicurezza freccia Netta Finale	: 8.801
Fatt. sicurezza freccia Finale	: 10.268	Fatt. sicurezza	: 8.237

Campata 203-202 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.252 (fs=3.972)
 Sforzo Normale di Progetto [daN] : -5599 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -314
 Momento Flettente Mz di Progetto [daNm] : 9

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7
 Tensione di Progetto [N/mm²] : -1.94
 Tensione Resistente [N/mm²] : 11.59
 Coefficiente di Sfruttamento a compressione : 0.168
 fs : 5.96
 Tensione di Progetto relativa a My [N/mm²] : 2.73
 Tensione di Progetto relativa a Mz [N/mm²] : 0.16
 Tensione Resistente relativa a My [N/mm²] : 12.7
 Tensione Resistente relativa a Mz [N/mm²] : 12.74
 Coefficiente di Sfruttamento a flessione : 0.224
 fs : 4.47
 Coefficiente di Sfruttamento a pressoflessione : 0.252
 fs : 3.97

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**
Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.07 (fs=14.234)
 Taglio Ty di Progetto [daN] : 7
 Taglio Tz di Progetto [daN] : 228
 Momento Torcente Mt di Progetto [daNm] : 9

Tipo Verifica : TAGLIO
 Tensione di Progetto relativa a Ty [N/mm²] : 0.00
 Tensione di Progetto relativa a Tz [N/mm²] : 0.12
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.07
 fs : 14.23

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mmq	Tensione Critica nel piano XZ	: 190.09 N/mmq
Resistenza fless. piano XY	: 12.74 N/mmq	Resistenza fless. piano XZ	: 12.70 N/mmq
Tensione fless. piano XY	: 0.16 N/mmq	Tensione fless. piano XZ	: 2.73 N/mmq
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.013	Coefficiente sfrutt. nel piano XZ	: 0.215
Coeff. sfrutt. max euleriano	: 0.177		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.190	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.392
fs	: 2.552		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto		Schema adottato Doppio Incastro	
Lunghezza elemento	: 1984.9 mm	Peso proprio	: -11.1 daN/m
Comb. di carico più gravosa	: 142	-	
Carico distribuito Istantaneo	: -12.1 daN/m	Carico distribuito Finale	: -12.1 daN/m
-		Comb 42 [CAR] [ST]	
Freccia Istantanea - COMBINAZIONE			

Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 204-205 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.271 (fs=3.687)

Sforzo Normale di Progetto [daN]	: -6275 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: -324
Momento Flettente Mz di Progetto [daNm]	: -15

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -2.18
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.188
fs	: 5.32
Tensione di Progetto relativa a My [N/mm ²]	: 2.81
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.26
Tensione Resistente relativa a My [N/mm ²]	: 12.7
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.236
fs	: 4.24
Coefficiente di Sfruttamento a pressoflessione	: 0.271
fs	: 3.69

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 33 [SLD] [IN] " - Coeff. Sfruttamento : 0.112 (fs=8.956)

Taglio Ty di Progetto [daN]	: -68
Taglio Tz di Progetto [daN]	: 189
Momento Torcente Mt di Progetto [daNm]	: 47

Tipo Verifica

: TAGLIO+TORSIONE

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.04
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.1
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a taglio	: 0.039
fs	: 25.38
Tensione di Progetto [N/mm ²]	: 0.38
Modulo di resistenza a torsione [mm ³]	: 886153.88
Tensione tang. Resistente [N/mm ²]	: 2.66
Coefficiente di Sfruttamento a torsione	: 0.11
fs	: 9.08
Coefficiente di Sfruttamento a taglio+torsione	: 0.112
fs	: 8.96

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 12.70 N/mm ²
Tensione fless. piano XY	: 0.26 N/mm ²	Tensione fless. piano XZ	: 2.81 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.021	Coefficiente sfrutt. nel piano XZ	: 0.221
Coeff. sfrutt. max euleriano	: 0.198		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.219	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.420
fs	: 2.382		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm
Fatt. sicurezza freccia Istantanea	: 673.380	Fatt. sicurezza freccia Netta Finale	: 534.428
Fatt. sicurezza freccia Finale	: 623.500	Fatt. sicurezza	: 534.428

Campata 205-206 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) $\gamma_M=1.45$ (FC=1)

L= 15500 mm - **R 160x1000** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 4 - [X=7750 mm / 15500 mm] - **R 160x1000**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.377 (fs=2.651)

Sforzo Normale di Progetto [daN]	: -1142 (COMPRESSIONE)
Momento Flettente My di Progetto [daNm]	: 11653
Momento Flettente Mz di Progetto [daNm]	: 0

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -0.07
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.006
fs	: 162.32
Tensione di Progetto relativa a My [N/mm ²]	: 4.37
Tensione di Progetto relativa a Mz [N/mm ²]	: 0
Tensione Resistente relativa a My [N/mm ²]	: 11.59
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.377
fs	: 2.65
Coefficiente di Sfruttamento a pressoflessione	: 0.377
fs	: 2.65

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 7 - [X=15500 mm / 15500 mm] - **R 160x1000**
 Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.185 (fs=5.409)

Taglio Ty di Progetto [daN] : 0
 Taglio Tz di Progetto [daN] : -3332
 Momento Torcente Mt di Progetto [daNm] : 0

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm²] : 0
 Tensione di Progetto relativa a Tz [N/mm²] : 0.31
 Tensione tang. Resistente [N/mm²] : 1.69
 Coefficiente di Sfruttamento a taglio : 0.185
 fs : 5.41

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 4
Lunghezza efficace nel piano XY	: 15500.0	Lunghezza efficace nel piano XZ	: 15500.0
Momento Critico nel piano XY	: 188530 daNm	Momento Critico nel piano XZ	: 30165 daNm
Tensione Critica nel piano XY	: 441.87 N/mmq	Tensione Critica nel piano XZ	: 11.31 N/mmq
Resistenza fless. piano XY	: 12.74 N/mmq	Resistenza fless. piano XZ	: 11.59 N/mmq
Tensione fless. piano XY	: 0.00 N/mmq	Tensione fless. piano XZ	: 4.37 N/mmq
Snellezza relativa nel piano XY	: 0.23	Snellezza relativa nel piano XZ	: 1.46
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.400
Coefficiente sfrutt. nel piano XY	: 0.000	Coefficiente sfrutt. nel piano XZ	: 0.269
Coeff. sfrutt. max euleriano	: 0.088		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.088	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.358
fs	: 2.795		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 15500.0 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -61.6 daN/m
Carico distribuito Istantaneo	: -342.1 daN/m	-	
-		Carico distribuito Finale	: -238.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mmq	Modulo Elastico finale	: 6388.9 N/mmq
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -3.957 mm	Limite Freccia Istantanea L/500	: 31.000 mm
Freccia Netta Finale	: -5.288 mm	Limite Freccia Netta Fin. L/ 350	: 44.286 mm
Freccia Finale	: -5.288 mm	Limite Freccia Finale L/ 300	: 51.667 mm
Fatt. sicurezza freccia Istantanea	: 7.834	Fatt. sicurezza freccia Netta Finale	: 8.375
Fatt. sicurezza freccia Finale	: 9.771	Fatt. sicurezza	: 7.834

Campata 207-206 Cope[Trave]

Classe di Servizio 2 (Umidità relativa max: 85%) LAMELLARE **GL24h** (Tipo Omogeneo) - $\gamma_M=1.45$ (FC=1)

L= 1984.94 mm - **R 120x240** - SEZIONI UTILIZZATE : 7

VERIFICHE EFFETTUATE CON ESITO POSITIVO

VERIFICHE DI RESISTENZA NORMALE

Sezione più gravosa : 1 - [X=0 mm / 1984.94 mm] - **R 120x240**
 Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.278 (fs=3.596)

Sforzo Normale di Progetto [daN] : -6336 (COMPRESSIONE)
 Momento Flettente My di Progetto [daNm] : -325
 Momento Flettente Mz di Progetto [daNm] : 20

Tipo Verifica : COMPRESSIONE+FLESSIONE - Kmod = 0.7

Tensione di Progetto [N/mm ²]	: -2.2
Tensione Resistente [N/mm ²]	: 11.59
Coefficiente di Sfruttamento a compressione	: 0.19
fs	: 5.27
Tensione di Progetto relativa a My [N/mm ²]	: 2.83
Tensione di Progetto relativa a Mz [N/mm ²]	: 0.36
Tensione Resistente relativa a My [N/mm ²]	: 12.7
Tensione Resistente relativa a Mz [N/mm ²]	: 12.74
Coefficiente di Sfruttamento a flessione	: 0.242
fs	: 4.13
Coefficiente di Sfruttamento a pressoflessione	: 0.278
fs	: 3.6

VERIFICHE DI RESISTENZA TANGENZIALE

Sezione più gravosa: 1 - [X=0 mm / 1984.94 mm] - **R 120x240**

Comb. più gravosa : " Comb 1 [SLV] [LT] " - Coeff. Sfruttamento : 0.07 (fs=14.22)

Taglio Ty di Progetto [daN]	: 15
Taglio Tz di Progetto [daN]	: 228
Momento Torcente Mt di Progetto [daNm]	: 20

Tipo Verifica : TAGLIO

Tensione di Progetto relativa a Ty [N/mm ²]	: 0.01
Tensione di Progetto relativa a Tz [N/mm ²]	: 0.12
Tensione tang. Resistente [N/mm ²]	: 1.69
Coefficiente di Sfruttamento a taglio	: 0.07
fs	: 14.22

VERIFICA A SVERGOLAMENTO

Tratto più sollecitato: 1 (0 - 6)

Combinazione più sfavorevole	: 1	Sezione più sfavorevole	: 1
Lunghezza efficace nel piano XY	: 1984.9	Lunghezza efficace nel piano XZ	: 1984.9
Momento Critico nel piano XY	: 43797 daNm	Momento Critico nel piano XZ	: 21898 daNm
Tensione Critica nel piano XY	: 760.36 N/mm ²	Tensione Critica nel piano XZ	: 190.09 N/mm ²
Resistenza fless. piano XY	: 12.74 N/mm ²	Resistenza fless. piano XZ	: 12.70 N/mm ²
Tensione fless. piano XY	: 0.36 N/mm ²	Tensione fless. piano XZ	: 2.83 N/mm ²
Snellezza relativa nel piano XY	: 0.18	Snellezza relativa nel piano XZ	: 0.36
Coeff. Riduttivo nel piano XY	: 1.000	Coeff. Riduttivo nel piano XZ	: 1.000
Coefficiente sfrutt. nel piano XY	: 0.028	Coefficiente sfrutt. nel piano XZ	: 0.223
Coeff. sfrutt. max euleriano	: 0.200		
Coeff. sfrutt. TOTALE (Piano XY)	: 0.228	Coeff. sfrutt. TOTALE (Piano XZ)	: 0.423
fs	: 2.365		

VERIFICA DI DEFORMABILITA'

Metodo di valutazione freccia finale (t->inf.)

· Modulo Elastico Ridotto

Lunghezza elemento	: 1984.9 mm	Schema adottato Doppio Incastro	
Comb. di carico più gravosa	: 142	Peso proprio	: -11.1 daN/m
Carico distribuito Istantaneo	: -12.1 daN/m	-	
-		Carico distribuito Finale	: -12.1 daN/m
Freccia Istantanea - COMBINAZIONE		Comb 42 [CAR] [ST]	
Freccia Finale - COMBINAZIONE		Comb 2 [SLEQP] [PE]	
Modulo Elastico istantaneo	: 11500.0 N/mm ²	Modulo Elastico finale	: 6388.9 N/mm ²
Controfreccia	: 0.000 mm		
Freccia Istantanea	: -0.006 mm	Limite Freccia Istantanea L/500	: 3.970 mm
Freccia Netta Finale	: -0.011 mm	Limite Freccia Netta Fin. L/ 350	: 5.671 mm
Freccia Finale	: -0.011 mm	Limite Freccia Finale L/ 300	: 6.616 mm

Fatt. sicurezza freccia Istantanea : 673.380
Fatt. sicurezza freccia Finale : 623.500

Fatt. sicurezza freccia Netta Finale : 534.428
Fatt. sicurezza : 534.428

1.6 Verifica Stati Limite di Danno.

Per edifici con il seguente tipo di elementi: tamponamenti progettati in modo da non subire danni a seguito di spostamenti di interpiano d_r , il controllo viene fatto tramite la seguente relazione:

$$d_r < 0.0075 h \leq 0.01 h$$

dove:

d_r : spostamento relativo tra due impalcati consecutivi;

h : altezza dell'impalcato;

Piano : piano considerato;

ELEMENTO : tipo e numero dell'elemento considerato;

d_{rx} : traslazione relativa X globale del piano considerato;

d_{ry} : traslazione relativa Y globale del piano considerato;

H : altezza del piano considerato;

d_{lim} : spostamento limite da normativa;

Esito : esito della verifica;

Tabella 45.II

Piano	ELEMENTO	d_{rx} [cm]	d_{ry} [cm]	H [cm]	d_{lim} [cm]	Esito
Primo Impalcato	Pilastro N° 1	0.0651	0.2511	376.0000	2.8200	Verificato
	Pilastro N° 2	0.0613	0.7653	376.0000	2.8200	Verificato
	Pilastro N° 3	0.0610	0.9074	376.0000	2.8200	Verificato
	Pilastro N° 4	0.0604	0.8720	376.0000	2.8200	Verificato
	Pilastro N° 5	0.0597	0.8456	376.0000	2.8200	Verificato
	Pilastro N° 6	0.0586	0.7366	376.0000	2.8200	Verificato
	Pilastro N° 7	0.0576	0.6838	376.0000	2.8200	Verificato
	Pilastro N° 8	0.0577	0.6066	376.0000	2.8200	Verificato
	Pilastro N° 9	0.0582	0.4972	376.0000	2.8200	Verificato
	Pilastro N° 10	0.0590	0.4409	376.0000	2.8200	Verificato
	Pilastro N° 11	0.0597	0.3311	376.0000	2.8200	Verificato
	Pilastro N° 12	0.0602	0.2903	376.0000	2.8200	Verificato
	Pilastro N° 13	0.0605	0.2428	376.0000	2.8200	Verificato
	Pilastro N° 14	0.0534	0.0361	376.0000	2.8200	Verificato
	Pilastro N° 15	0.4863	0.2492	376.0000	2.8200	Verificato
	Pilastro N° 16	0.5132	0.0358	376.0000	2.8200	Verificato
	Pilastro N° 17	0.7399	0.2481	376.0000	2.8200	Verificato
	Pilastro N° 18	0.7690	0.0359	376.0000	2.8200	Verificato
	Pilastro N° 19	0.8900	0.2476	376.0000	2.8200	Verificato
	Pilastro N° 20	0.9037	0.0359	376.0000	2.8200	Verificato
	Pilastro N° 21	1.0302	0.2475	376.0000	2.8200	Verificato
	Pilastro N° 22	1.0379	0.0360	376.0000	2.8200	Verificato
	Pilastro N° 23	1.1717	0.2483	376.0000	2.8200	Verificato
	Pilastro N° 24	1.1667	0.0361	376.0000	2.8200	Verificato
	Pilastro N° 25	1.2962	0.2496	376.0000	2.8200	Verificato
	Pilastro N° 26	1.2912	0.0363	376.0000	2.8200	Verificato
	Pilastro N° 27	1.3963	0.0363	376.0000	2.8200	Verificato
	Pilastro N° 28	1.4054	0.2533	376.0000	2.8200	Verificato
	Pilastro N° 29	1.4928	0.0366	376.0000	2.8200	Verificato
	Pilastro N° 30	1.4944	0.2578	376.0000	2.8200	Verificato
	Pilastro N° 31	1.5481	0.0368	376.0000	2.8200	Verificato
	Pilastro N° 32	1.5294	0.2608	376.0000	2.8200	Verificato
	Pilastro N° 33	1.5671	0.0372	376.0000	2.8200	Verificato
	Pilastro N° 34	1.5739	0.2628	376.0000	2.8200	Verificato
	Pilastro N° 35	1.5699	0.0374	376.0000	2.8200	Verificato
	Pilastro N° 36	1.5685	0.2637	376.0000	2.8200	Verificato
	Pilastro N° 37	1.5519	0.0379	376.0000	2.8200	Verificato
	Pilastro N° 38	1.5646	0.2636	376.0000	2.8200	Verificato
	Pilastro N° 39	1.5354	0.0382	376.0000	2.8200	Verificato
	Pilastro N° 40	1.5441	0.2623	376.0000	2.8200	Verificato
	Pilastro N° 41	1.4892	0.0387	376.0000	2.8200	Verificato
	Pilastro N° 42	1.4683	0.2599	376.0000	2.8200	Verificato

	Pilastro N° 43	1.4436	0.2587	376.0000	2.8200	Verificato
	Pilastro N° 44	1.4240	0.0390	376.0000	2.8200	Verificato
	Pilastro N° 45	1.3670	0.2564	376.0000	2.8200	Verificato
	Pilastro N° 46	1.3662	0.0390	376.0000	2.8200	Verificato
	Pilastro N° 47	1.2361	0.2545	376.0000	2.8200	Verificato
	Pilastro N° 48	1.2462	0.0393	376.0000	2.8200	Verificato
	Pilastro N° 49	1.0940	0.2535	376.0000	2.8200	Verificato
	Pilastro N° 50	1.0854	0.0395	376.0000	2.8200	Verificato
	Pilastro N° 51	0.9541	0.2531	376.0000	2.8200	Verificato
	Pilastro N° 52	0.9504	0.0400	376.0000	2.8200	Verificato
	Pilastro N° 53	0.8087	0.2535	376.0000	2.8200	Verificato
	Pilastro N° 54	0.7841	0.0403	376.0000	2.8200	Verificato
	Pilastro N° 55	0.5416	0.2544	376.0000	2.8200	Verificato
	Pilastro N° 56	0.5204	0.0402	376.0000	2.8200	Verificato
	Pilastro N° 57	0.0668	0.2567	376.0000	2.8200	Verificato
	Pilastro N° 58	0.0678	0.7527	376.0000	2.8200	Verificato
	Pilastro N° 59	0.0674	0.8961	376.0000	2.8200	Verificato
	Pilastro N° 60	0.0668	0.8670	376.0000	2.8200	Verificato
	Pilastro N° 61	0.0659	0.8367	376.0000	2.8200	Verificato
	Pilastro N° 62	0.0650	0.7432	376.0000	2.8200	Verificato
	Pilastro N° 63	0.0644	0.6775	376.0000	2.8200	Verificato
	Pilastro N° 64	0.0648	0.5969	376.0000	2.8200	Verificato
	Pilastro N° 65	0.0652	0.4899	376.0000	2.8200	Verificato
	Pilastro N° 66	0.0658	0.4204	376.0000	2.8200	Verificato
	Pilastro N° 67	0.0664	0.3139	376.0000	2.8200	Verificato
	Pilastro N° 68	0.0668	0.2664	376.0000	2.8200	Verificato
	Pilastro N° 69	0.0670	0.2232	376.0000	2.8200	Verificato
	Pilastro N° 70	0.0595	0.0405	376.0000	2.8200	Verificato
Copertura	Pilastro N° 1	0.0534	2.6340	440.0000	3.3000	Verificato
	Pilastro N° 2	0.0702	2.2203	440.0000	3.3000	Verificato
	Pilastro N° 3	0.0691	2.0032	440.0000	3.3000	Verificato
	Pilastro N° 4	0.0681	1.9267	440.0000	3.3000	Verificato
	Pilastro N° 5	0.0674	1.8445	440.0000	3.3000	Verificato
	Pilastro N° 6	0.0668	1.7736	440.0000	3.3000	Verificato
	Pilastro N° 7	0.0661	1.5566	440.0000	3.3000	Verificato
	Pilastro N° 8	0.0658	1.3654	440.0000	3.3000	Verificato
	Pilastro N° 9	0.0667	1.2087	440.0000	3.3000	Verificato
	Pilastro N° 10	0.0678	0.9426	440.0000	3.3000	Verificato
	Pilastro N° 11	0.0686	0.7520	440.0000	3.3000	Verificato
	Pilastro N° 12	0.0696	0.5692	440.0000	3.3000	Verificato
	Pilastro N° 13	0.0709	0.4082	440.0000	3.3000	Verificato
	Pilastro N° 14	0.0636	0.2657	440.0000	3.3000	Verificato
	Pilastro N° 15	0.4687	2.6365	440.0000	3.3000	Verificato
	Pilastro N° 16	0.4373	0.2655	440.0000	3.3000	Verificato
	Pilastro N° 17	0.7048	2.6380	440.0000	3.3000	Verificato
	Pilastro N° 18	0.6747	0.2654	440.0000	3.3000	Verificato
	Pilastro N° 19	0.8747	2.6390	440.0000	3.3000	Verificato
	Pilastro N° 20	0.8624	0.2651	440.0000	3.3000	Verificato
	Pilastro N° 21	1.0207	2.6394	440.0000	3.3000	Verificato
	Pilastro N° 22	1.0141	0.2652	440.0000	3.3000	Verificato
	Pilastro N° 23	1.1466	2.6392	440.0000	3.3000	Verificato
	Pilastro N° 24	1.1517	0.2649	440.0000	3.3000	Verificato
	Pilastro N° 25	1.2633	2.6382	440.0000	3.3000	Verificato
	Pilastro N° 26	1.2752	0.2648	440.0000	3.3000	Verificato
	Pilastro N° 27	1.3893	0.2645	440.0000	3.3000	Verificato
	Pilastro N° 28	1.3895	2.6353	440.0000	3.3000	Verificato
	Pilastro N° 29	1.4607	0.2644	440.0000	3.3000	Verificato
	Pilastro N° 30	1.4680	2.6311	440.0000	3.3000	Verificato
	Pilastro N° 31	1.5103	0.2640	440.0000	3.3000	Verificato
	Pilastro N° 32	1.5398	2.6280	440.0000	3.3000	Verificato
	Pilastro N° 33	1.5448	0.2637	440.0000	3.3000	Verificato
	Pilastro N° 34	1.5502	2.6259	440.0000	3.3000	Verificato
	Pilastro N° 35	1.5361	0.2631	440.0000	3.3000	Verificato
	Pilastro N° 36	1.5690	2.6247	440.0000	3.3000	Verificato
	Pilastro N° 37	1.5323	0.2627	440.0000	3.3000	Verificato
	Pilastro N° 38	1.5530	2.6245	440.0000	3.3000	Verificato
	Pilastro N° 39	1.4854	0.2620	440.0000	3.3000	Verificato
	Pilastro N° 40	1.5127	2.6253	440.0000	3.3000	Verificato
	Pilastro N° 41	1.4393	0.2613	440.0000	3.3000	Verificato
	Pilastro N° 42	1.4719	2.6270	440.0000	3.3000	Verificato
	Pilastro N° 43	1.4356	2.6280	440.0000	3.3000	Verificato
	Pilastro N° 44	1.4283	0.2609	440.0000	3.3000	Verificato

	Pilastro N° 45	1.3214	2.6301	440.0000	3.3000	Verificato
	Pilastro N° 46	1.3233	0.2603	440.0000	3.3000	Verificato
	Pilastro N° 47	1.2071	2.6316	440.0000	3.3000	Verificato
	Pilastro N° 48	1.1967	0.2599	440.0000	3.3000	Verificato
	Pilastro N° 49	1.0677	2.6322	440.0000	3.3000	Verificato
	Pilastro N° 50	1.0761	0.2591	440.0000	3.3000	Verificato
	Pilastro N° 51	0.9105	2.6322	440.0000	3.3000	Verificato
	Pilastro N° 52	0.9161	0.2584	440.0000	3.3000	Verificato
	Pilastro N° 53	0.7132	2.6313	440.0000	3.3000	Verificato
	Pilastro N° 54	0.7369	0.2581	440.0000	3.3000	Verificato
	Pilastro N° 55	0.4642	2.6299	440.0000	3.3000	Verificato
	Pilastro N° 56	0.4796	0.2581	440.0000	3.3000	Verificato
	Pilastro N° 57	0.0630	2.6271	440.0000	3.3000	Verificato
	Pilastro N° 58	0.0771	2.2249	440.0000	3.3000	Verificato
	Pilastro N° 59	0.0759	2.0264	440.0000	3.3000	Verificato
	Pilastro N° 60	0.0750	1.9411	440.0000	3.3000	Verificato
	Pilastro N° 61	0.0743	1.8715	440.0000	3.3000	Verificato
	Pilastro N° 62	0.0733	1.7904	440.0000	3.3000	Verificato
	Pilastro N° 63	0.0726	1.5746	440.0000	3.3000	Verificato
	Pilastro N° 64	0.0730	1.3750	440.0000	3.3000	Verificato
	Pilastro N° 65	0.0740	1.2107	440.0000	3.3000	Verificato
	Pilastro N° 66	0.0752	0.9405	440.0000	3.3000	Verificato
	Pilastro N° 67	0.0762	0.7375	440.0000	3.3000	Verificato
	Pilastro N° 68	0.0774	0.5701	440.0000	3.3000	Verificato
	Pilastro N° 69	0.0787	0.4005	440.0000	3.3000	Verificato
	Pilastro N° 70	0.0702	0.2577	440.0000	3.3000	Verificato

1.7 Verifica Stati Limite di Operatività.

Per edifici con il seguente tipo di elementi: tamponamenti progettati in modo da non subire danni a seguito di spostamenti di interpiano drp, il controllo viene fatto tramite la seguente relazione:

$$d_r < (2/3) \cdot 0.0075 h \leq 0.01 h$$

dove:

d_r è lo spostamento relativo tra due impalcati consecutivi;

h è l'altezza dell'impalcato;

Piano : piano considerato;

ELEMENTO : tipo e numero dell'elemento considerato;

drx : traslazione relativa X globale del piano considerato;

dry : traslazione relativa Y globale del piano considerato;

H : altezza del piano considerato;

dlim : spostamento limite da normativa;

Esito : esito della verifica;

Tabella 45.II

Piano	ELEMENTO	drx [cm]	dry [cm]	H [cm]	dlim [cm]	Esito
Primo Impalcato	Pilastro N° 1	0.0619	0.1797	376.0000	1.8800	Verificato
	Pilastro N° 2	0.0648	0.5779	376.0000	1.8800	Verificato
	Pilastro N° 3	0.0645	0.6727	376.0000	1.8800	Verificato
	Pilastro N° 4	0.0639	0.6383	376.0000	1.8800	Verificato
	Pilastro N° 5	0.0632	0.6247	376.0000	1.8800	Verificato
	Pilastro N° 6	0.0622	0.5364	376.0000	1.8800	Verificato
	Pilastro N° 7	0.0612	0.5010	376.0000	1.8800	Verificato
	Pilastro N° 8	0.0614	0.4435	376.0000	1.8800	Verificato
	Pilastro N° 9	0.0619	0.3565	376.0000	1.8800	Verificato
	Pilastro N° 10	0.0627	0.3207	376.0000	1.8800	Verificato
	Pilastro N° 11	0.0635	0.2401	376.0000	1.8800	Verificato
	Pilastro N° 12	0.0640	0.2257	376.0000	1.8800	Verificato
	Pilastro N° 13	0.0644	0.2038	376.0000	1.8800	Verificato
	Pilastro N° 14	0.0583	0.0278	376.0000	1.8800	Verificato
	Pilastro N° 15	0.4680	0.1784	376.0000	1.8800	Verificato
	Pilastro N° 16	0.4894	0.0275	376.0000	1.8800	Verificato
	Pilastro N° 17	0.6925	0.1776	376.0000	1.8800	Verificato
	Pilastro N° 18	0.7184	0.0276	376.0000	1.8800	Verificato

	Pilastro N° 19	0.8134	0.1773	376.0000	1.8800	Verificato
	Pilastro N° 20	0.8261	0.0276	376.0000	1.8800	Verificato
	Pilastro N° 21	0.9233	0.1772	376.0000	1.8800	Verificato
	Pilastro N° 22	0.9304	0.0277	376.0000	1.8800	Verificato
	Pilastro N° 23	1.0334	0.1778	376.0000	1.8800	Verificato
	Pilastro N° 24	1.0288	0.0278	376.0000	1.8800	Verificato
	Pilastro N° 25	1.1287	0.1788	376.0000	1.8800	Verificato
	Pilastro N° 26	1.1233	0.0280	376.0000	1.8800	Verificato
	Pilastro N° 27	1.2011	0.0280	376.0000	1.8800	Verificato
	Pilastro N° 28	1.2073	0.1816	376.0000	1.8800	Verificato
	Pilastro N° 29	1.2739	0.0283	376.0000	1.8800	Verificato
	Pilastro N° 30	1.2734	0.1848	376.0000	1.8800	Verificato
	Pilastro N° 31	1.3125	0.0284	376.0000	1.8800	Verificato
	Pilastro N° 32	1.2932	0.1870	376.0000	1.8800	Verificato
	Pilastro N° 33	1.3220	0.0288	376.0000	1.8800	Verificato
	Pilastro N° 34	1.3257	0.1884	376.0000	1.8800	Verificato
	Pilastro N° 35	1.3205	0.0290	376.0000	1.8800	Verificato
	Pilastro N° 36	1.3187	0.1891	376.0000	1.8800	Verificato
	Pilastro N° 37	1.3103	0.0294	376.0000	1.8800	Verificato
	Pilastro N° 38	1.3215	0.1889	376.0000	1.8800	Verificato
	Pilastro N° 39	1.3038	0.0296	376.0000	1.8800	Verificato
	Pilastro N° 40	1.3124	0.1880	376.0000	1.8800	Verificato
	Pilastro N° 41	1.2720	0.0301	376.0000	1.8800	Verificato
	Pilastro N° 42	1.2562	0.1861	376.0000	1.8800	Verificato
	Pilastro N° 43	1.2386	0.1853	376.0000	1.8800	Verificato
	Pilastro N° 44	1.2228	0.0302	376.0000	1.8800	Verificato
	Pilastro N° 45	1.1853	0.1835	376.0000	1.8800	Verificato
	Pilastro N° 46	1.1844	0.0302	376.0000	1.8800	Verificato
	Pilastro N° 47	1.0850	0.1821	376.0000	1.8800	Verificato
	Pilastro N° 48	1.0936	0.0304	376.0000	1.8800	Verificato
	Pilastro N° 49	0.9752	0.1814	376.0000	1.8800	Verificato
	Pilastro N° 50	0.9671	0.0306	376.0000	1.8800	Verificato
	Pilastro N° 51	0.8664	0.1810	376.0000	1.8800	Verificato
	Pilastro N° 52	0.8630	0.0310	376.0000	1.8800	Verificato
	Pilastro N° 53	0.7512	0.1813	376.0000	1.8800	Verificato
	Pilastro N° 54	0.7276	0.0312	376.0000	1.8800	Verificato
	Pilastro N° 55	0.5155	0.1819	376.0000	1.8800	Verificato
	Pilastro N° 56	0.4931	0.0311	376.0000	1.8800	Verificato
	Pilastro N° 57	0.0667	0.1836	376.0000	1.8800	Verificato
	Pilastro N° 58	0.0695	0.5661	376.0000	1.8800	Verificato
	Pilastro N° 59	0.0691	0.6627	376.0000	1.8800	Verificato
	Pilastro N° 60	0.0685	0.6343	376.0000	1.8800	Verificato
	Pilastro N° 61	0.0677	0.6170	376.0000	1.8800	Verificato
	Pilastro N° 62	0.0668	0.5431	376.0000	1.8800	Verificato
	Pilastro N° 63	0.0663	0.4958	376.0000	1.8800	Verificato
	Pilastro N° 64	0.0667	0.4351	376.0000	1.8800	Verificato
	Pilastro N° 65	0.0671	0.3508	376.0000	1.8800	Verificato
	Pilastro N° 66	0.0678	0.3031	376.0000	1.8800	Verificato
	Pilastro N° 67	0.0684	0.2263	376.0000	1.8800	Verificato
	Pilastro N° 68	0.0689	0.2057	376.0000	1.8800	Verificato
	Pilastro N° 69	0.0692	0.1874	376.0000	1.8800	Verificato
	Pilastro N° 70	0.0627	0.0314	376.0000	1.8800	Verificato
Copertura	Pilastro N° 1	0.0690	1.9067	440.0000	2.2000	Verificato
	Pilastro N° 2	0.0774	1.6219	440.0000	2.2000	Verificato
	Pilastro N° 3	0.0762	1.4639	440.0000	2.2000	Verificato
	Pilastro N° 4	0.0753	1.4070	440.0000	2.2000	Verificato
	Pilastro N° 5	0.0745	1.3423	440.0000	2.2000	Verificato
	Pilastro N° 6	0.0740	1.2959	440.0000	2.2000	Verificato
	Pilastro N° 7	0.0732	1.1235	440.0000	2.2000	Verificato
	Pilastro N° 8	0.0729	0.9781	440.0000	2.2000	Verificato
	Pilastro N° 9	0.0738	0.8676	440.0000	2.2000	Verificato
	Pilastro N° 10	0.0748	0.6606	440.0000	2.2000	Verificato
	Pilastro N° 11	0.0757	0.5334	440.0000	2.2000	Verificato
	Pilastro N° 12	0.0767	0.4176	440.0000	2.2000	Verificato
	Pilastro N° 13	0.0779	0.3145	440.0000	2.2000	Verificato
	Pilastro N° 14	0.0723	0.2131	440.0000	2.2000	Verificato
	Pilastro N° 15	0.4466	1.9084	440.0000	2.2000	Verificato
	Pilastro N° 16	0.4205	0.2128	440.0000	2.2000	Verificato
	Pilastro N° 17	0.6592	1.9094	440.0000	2.2000	Verificato
	Pilastro N° 18	0.6322	0.2127	440.0000	2.2000	Verificato
	Pilastro N° 19	0.7994	1.9101	440.0000	2.2000	Verificato
	Pilastro N° 20	0.7882	0.2125	440.0000	2.2000	Verificato

	Pilastro N° 21	0.9130	1.9103	440.0000	2.2000	Verificato
	Pilastro N° 22	0.9071	0.2125	440.0000	2.2000	Verificato
	Pilastro N° 23	1.0078	1.9102	440.0000	2.2000	Verificato
	Pilastro N° 24	1.0128	0.2122	440.0000	2.2000	Verificato
	Pilastro N° 25	1.0945	1.9094	440.0000	2.2000	Verificato
	Pilastro N° 26	1.1058	0.2121	440.0000	2.2000	Verificato
	Pilastro N° 27	1.1907	0.2118	440.0000	2.2000	Verificato
	Pilastro N° 28	1.1871	1.9075	440.0000	2.2000	Verificato
	Pilastro N° 29	1.2399	0.2117	440.0000	2.2000	Verificato
	Pilastro N° 30	1.2415	1.9043	440.0000	2.2000	Verificato
	Pilastro N° 31	1.2732	0.2114	440.0000	2.2000	Verificato
	Pilastro N° 32	1.2947	1.9021	440.0000	2.2000	Verificato
	Pilastro N° 33	1.2963	0.2111	440.0000	2.2000	Verificato
	Pilastro N° 34	1.2952	1.9005	440.0000	2.2000	Verificato
	Pilastro N° 35	1.2832	0.2106	440.0000	2.2000	Verificato
	Pilastro N° 36	1.3121	1.8996	440.0000	2.2000	Verificato
	Pilastro N° 37	1.2868	0.2102	440.0000	2.2000	Verificato
	Pilastro N° 38	1.3045	1.8995	440.0000	2.2000	Verificato
	Pilastro N° 39	1.2534	0.2096	440.0000	2.2000	Verificato
	Pilastro N° 40	1.2769	1.9000	440.0000	2.2000	Verificato
	Pilastro N° 41	1.2231	0.2090	440.0000	2.2000	Verificato
	Pilastro N° 42	1.2529	1.9012	440.0000	2.2000	Verificato
	Pilastro N° 43	1.2264	1.9019	440.0000	2.2000	Verificato
	Pilastro N° 44	1.2208	0.2087	440.0000	2.2000	Verificato
	Pilastro N° 45	1.1405	1.9035	440.0000	2.2000	Verificato
	Pilastro N° 46	1.1414	0.2081	440.0000	2.2000	Verificato
	Pilastro N° 47	1.0563	1.9047	440.0000	2.2000	Verificato
	Pilastro N° 48	1.0471	0.2078	440.0000	2.2000	Verificato
	Pilastro N° 49	0.9499	1.9051	440.0000	2.2000	Verificato
	Pilastro N° 50	0.9578	0.2071	440.0000	2.2000	Verificato
	Pilastro N° 51	0.8264	1.9052	440.0000	2.2000	Verificato
	Pilastro N° 52	0.8317	0.2065	440.0000	2.2000	Verificato
	Pilastro N° 53	0.6621	1.9045	440.0000	2.2000	Verificato
	Pilastro N° 54	0.6849	0.2062	440.0000	2.2000	Verificato
	Pilastro N° 55	0.4396	1.9036	440.0000	2.2000	Verificato
	Pilastro N° 56	0.4561	0.2062	440.0000	2.2000	Verificato
	Pilastro N° 57	0.0720	1.9016	440.0000	2.2000	Verificato
	Pilastro N° 58	0.0822	1.6297	440.0000	2.2000	Verificato
	Pilastro N° 59	0.0811	1.4875	440.0000	2.2000	Verificato
	Pilastro N° 60	0.0802	1.4219	440.0000	2.2000	Verificato
	Pilastro N° 61	0.0794	1.3690	440.0000	2.2000	Verificato
	Pilastro N° 62	0.0785	1.3123	440.0000	2.2000	Verificato
	Pilastro N° 63	0.0777	1.1404	440.0000	2.2000	Verificato
	Pilastro N° 64	0.0781	0.9881	440.0000	2.2000	Verificato
	Pilastro N° 65	0.0791	0.8715	440.0000	2.2000	Verificato
	Pilastro N° 66	0.0803	0.6619	440.0000	2.2000	Verificato
	Pilastro N° 67	0.0813	0.5246	440.0000	2.2000	Verificato
	Pilastro N° 68	0.0824	0.4240	440.0000	2.2000	Verificato
	Pilastro N° 69	0.0836	0.3135	440.0000	2.2000	Verificato
	Pilastro N° 70	0.0773	0.2059	440.0000	2.2000	Verificato

1.8 Verifica Elementi Bidimensionali.

1.8.1 Verifica Piastre.

1.8.1.1 Verifica Piastre in C.A..

1.8.1.1.1 Dati Generali

Piastra : numero della Piastra;
 Imp. : impalcato al quale appartiene la piastra;
 Fili : fili fissi ai quali appartiene la piastra;
 Sp. : spessore della Piastra;
 Largh. Striscia : Larghezza della striscia unitaria di Piastra rispetto alla quale sono state effettuate le verifiche;

Lungh. Concio : Lunghezza del concio di Piastra rispetto alla quale sono state effettuate le verifiche a taglio;

Tabella 46.I

Piastra	Imp.	Fili	Sp. [cm]	Largh. striscia [cm]	Lungh. concio [cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	40	100	100
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	40	100	100
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	40	100	100

Disposizione Armature

Piastra : numero della Piastra;
 Imp. : impalcato al quale appartiene la piastra;
 Fili : fili fissi ai quali appartiene la piastra;
 Dir. : Direzione rispetto alla quale disporre le armature;
 Diam. : diametro delle armature da disporre nella direzione indicata;
 Inter. intrad. : interasse rispetto al quale posizionare le armature all'intradosso nella direzione indicata;
 Inter. estrad. : interasse rispetto al quale posizionare le armature all'estradosso nella direzione indicata;

Tabella 46.II

Piastra	Imp.	Fili	Dir.	Diam. [mm]	Inter. intrad. [cm]	Inter. estrad. [cm]
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	X	12	22.0	22.0
			Y	12	25.0	25.0
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	X	12	24.0	24.0
			Y	12	25.0	25.0
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	X	12	25.0	25.0
			Y	12	25.0	25.0

1.8.1.1.2 Verifiche SLV - Flessione.

Piastra : numero della Piastra;
 Imp. : impalcato al quale appartiene la piastra;
 Fili : fili fissi ai quali appartiene la piastra;
 RCrit : regione critica;
 Dir. : direzione attorno alla quale sono valutate le caratteristiche flettenti;
 ϵ_{c2} : deformazione di contrazione del calcestruzzo al raggiungimento della massima tensione;
 ϵ_{cu2} : deformazione ultima di contrazione del calcestruzzo;
 Msd : momento sollecitante;
 ϵ_{cls} : deformazione massima del calcestruzzo compresso
 ϵ_{acc} : deformazione massima dell'armatura tesa
 MRd : momento resistente;
 S : Coefficiente di sicurezza;
 Esito : Esito della verifica : V = VERIFICATA;
 : NV = NON VERIFICATA;

Tabella 47.I

Piastra	Imp.	Fili	RCrit	Dir.	ϵ_{c2} [%]	ϵ_{cu2} [%]	Cop. sup. [cm]	Arm. sup.	Cop. inf. [cm]	Arm. inf.	Msd [daN m]	ϵ_{cls} [%]	ϵ_{acc} [%]	MRd [daN m]	S	Esito
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26		X	2.00	3.50	3.2	Ø 12 / 22.0	2.0	Ø 12 / 22.0	-6875	0.41	1.86	-6929	1.01	V
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44		X	2.00	3.50	3.2	Ø 12 / 24.0	2.0	Ø 12 / 24.0	-6351	0.39	1.86	-6367	1.00	V
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2		X	2.00	3.50	3.2	Ø 12 / 25.0	2.0	Ø 12 / 25.0	-4595	0.38	1.86	-6119	1.33	V
				Y	2.00	3.50	2.0	Ø 12 / 25.0	3.2	Ø 12 / 25.0	-2794	0.38	1.86	-6119	2.19	V
				Y	2.00	3.50	2.0	Ø 12 / 25.0	3.2	Ø 12 / 25.0	-2732	0.38	1.86	-6119	2.24	V

1.8.1.1.3 Verifiche SLV - Taglio

Piastra : numero della Piastra;
 Imp. : impalcato al quale appartiene la piastra;

Fili : fili fissi ai quali appartiene la piastra;
 RCrit : regione critica;
 cot(θ) : cotangente dell'angolo θ ;
 Diam. : diametro del braccio della staffa;
 AStaffe : area di armatura a taglio da disporre nell'unità di superficie;
 DLong : distanza longitudinale fra i bracci delle staffe;
 DTrasv : distanza trasversale fra i bracci delle staffe;
 VSd : Taglio sollecitante di calcolo;
 VRd : Taglio resistente di calcolo;
 Esito : Esito della verifica : V = VERIFICATA;
 : NV = NON VERIFICATA;

Tabella 48.I

Piastra	Imp.	Fili	RCrit	cot(θ)	Armature				Tagli		Esito
					Diam. [mm]	Dlong [cm]	Dtrasv [cm]	Area [cm ² /m ²]	Vsd [daN]	VRd [daN]	
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26		1.0	8	-	-	-	6715	10992	V
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44		1.0	8	-	-	-	7543	10678	V
3	Fondazione	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2		1.0	8	-	-	-	5039	10534	V

1.8.1.1.4 Verifiche SLE - Fessurazione

Piastra : numero della Piastra;
 Imp. : impalcato al quale appartiene la piastra;
 Fili : fili fissi ai quali appartiene la piastra;
 Comb. : combinazione di carico (Caratteristica, Frequente, Quasi Permanente);
 RCrit : regione critica;
 Dir. : direzione dell'asse attorno al quale viene valutata la caratteristica flettente;
 Msd : azione sollecitante flettente massima;
 MCr : momento di prima fessurazione;
 Fess. Calc. : fessura di calcolo;
 Fess. Lim. : fessura limite;
 S : Coefficiente di sicurezza;
 Esito : Esito della verifica : V = VERIFICATA;
 : NV = NON VERIFICATA;

Tabella 49.I

Piastra	Imp.	Fili	Comb.	RCrit	Dir.	Msd [daNm]	MCr [daNm]	Fess. Calc. [mm]	Fess. Lim. [mm]	S	Esito
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29,	Freq.		X	-1604.71	5456.71	0.00	0.40	-	V

		27, 26									
					Y	-497.27	5407.65	0.00	0.40	-	V
			Q. Perm.		X	-1481.75	5456.71	0.00	0.30	-	V
					Y	-476.75	5407.65	0.00	0.30	-	V
2	Fond azion e	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44	Freq.		X	-1441.75	5422.64	0.00	0.40	-	V
					Y	-490.83	5407.65	0.00	0.40	-	V
			Q. Perm.		X	-1337.51	5422.64	0.00	0.30	-	V
					Y	-466.11	5407.65	0.00	0.30	-	V
3	Fond azion e	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	Freq.		X	-1321.45	5407.65	0.00	0.40	-	V
					Y	-331.95	5407.65	0.00	0.40	-	V
			Q. Perm.		X	-1224.00	5407.65	0.00	0.30	-	V
					Y	-319.42	5407.65	0.00	0.30	-	V

1.8.1.1.5 Verifiche SLE - Tensioni di Esercizio

Piastra	: numero della Piastra;
Imp.	: impalcato al quale appartiene la piastra;
Fili	: fili fissi ai quali appartiene la piastra;
Comb.	: combinazione di carico (Caratteristica, Frequente, Quasi Permanente);
RCrit	: regione critica;
Dir.	: direzione dell'asse attorno al quale viene valutata la caratteristica flettente;
Msd	: valore massimo della caratteristica flettente di calcolo;
σ_c	: tensioni d'esercizio del calcestruzzo (compressione positiva);
$\sigma_{c,lim}$: Tensioni limite del calcestruzzo;
S cls	: coefficiente di sicurezza per la verifica del calcestruzzo;
σ_s	: tensioni d'esercizio dell'acciaio (trazione positiva);
$\sigma_{s,lim}$: Tensioni limite dell'acciaio;
S acc.	: coefficiente di sicurezza per la verifica dell'acciaio;
Esito	: Esito della verifica : V = VERIFICATA;
	: NV = NON VERIFICATA;

Tabella 50.I

Piastra	Imp.	Fili	Comb.	RCrit	Dir.	Msd [daNm]	σ_c [daN/cm ²]	$\sigma_{c,lim}$ [daN/cm ²]	S cls	σ_s [daN/cm ²]	$\sigma_{s,lim}$ [daN/cm ²]	S acc.	Esito
1	Fondazione	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26	Caratteristica		X	-2272.74	18.18	150.00	8.25	-1280.20	3600.00	2.81	V
					Y	-623.03	5.30	150.00	28.29	-397.53	3600.00	9.06	V
			Q. Perm.		X	-1481.75	11.85	112.50	9.49	-834.65	3600.00	4.31	V
					Y	-476.75	4.06	112.50	27.73	-304.19	3600.00	11.83	V
2	Fondazione	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70	Caratteristica		X	-2078.40	17.34	150.00	8.65	-1274.37	3600.00	2.82	V

		56, 54, 52, 50, 48, 46, 44											
					Y	684.48	5.82	150.00	25.75	-436.73	3600.00	8.24	V
			Q. Perm.		X	-1337.51	11.16	112.50	10.08	-820.09	3600.00	4.39	V
					Y	-466.11	3.97	112.50	28.36	-297.40	3600.00	12.10	V
3	Fon dazi one	1, 15, 17, 19, 21, 23, 25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2	Caratter istica		X	-1879.67	16.00	150.00	9.38	-1199.32	3600.00	3.00	V
					Y	765.23	6.51	150.00	23.03	-488.25	3600.00	7.37	V
			Q. Perm.		X	-1224.00	10.42	112.50	10.80	-780.97	3600.00	4.61	V
					Y	-319.42	2.72	112.50	41.39	-203.80	3600.00	17.66	V

1.8.1.1.6 Verifiche SLD - Resistenza a Flessione.

Piastra : numero della Piastra;
 Imp. : impalcato al quale appartiene la piastra;
 Fili : fili fissi ai quali appartiene la piastra;
 RCrit : regione critica;
 Dir. : direzione attorno alla quale sono valutate le caratteristiche flettenti;
 ϵ_{c2} : deformazione di contrazione del calcestruzzo al raggiungimento della massima tensione;
 ϵ_{cu2} : deformazione ultima di contrazione del calcestruzzo;
 Msd : momento sollecitante;
 ϵ_{cls} : deformazione massima del calcestruzzo compresso
 ϵ_{acc} : deformazione massima dell'armatura tesa
 MRd : momento resistente;
 S : Coefficiente di sicurezza;
 Esito : Esito della verifica : V = VERIFICATA;
 : NV = NON VERIFICATA;

Tabella 51.I

Piastra	Imp.	Fili	RCrit	Dir.	ϵ_{c2} [%]	ϵ_{cu2} [%]	Msd [daNm]	ϵ_{cls} [%]	ϵ_{acc} [%]	MRd [daNm]	S	Esito
1	Fondazi one	25, 28, 30, 32, 34, 36, 38, 40, 42, 43, 44, 41, 39, 37, 35, 33, 31, 29, 27, 26		X	2.00	3.50	-3420.8 4	0.88	10.00	-8288.4 5	2.42	V
				Y	2.00	3.50	-872	0.83	10.00	-7316	8.39	V
2	Fondazi one	43, 45, 47, 49, 51, 53, 55, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 56, 54, 52, 50, 48, 46, 44		X	2.00	3.50	-3118.2 1	0.85	10.00	-7613.8 6	2.44	V
				Y	2.00	3.50	-1085	0.83	10.00	-7316	6.74	V
3	Fondazi one	1, 15, 17, 19, 21, 23,		X	2.00	3.50	-2428.5 6	0.83	10.00	-7316.1 2	3.01	V

		25, 26, 24, 22, 20, 18, 16, 14, 13, 12, 11, 10, 9, 8, 7, 6, 5, 4, 3, 2										
				Y	2.00	3.50	-1113	0.83	10.00	-7316	6.57	V

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